MÈTODES NUMÈRICS:

Ex-Parcial Q2-2018-19 (a)

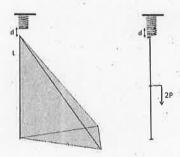
Name and surnames:

(1) Consider the piece of piramidal shape with triangular section as in the figure (on the left). Its hight is L = 2mm and the triangle in its base has area $A_0 mm^2$. It is made of a material whose Young modulus is $E \frac{N}{mm^2}$ and we consider it fixed on the bottom.

Over the piece, at distance d in mm, there is a spring of constant $K = \frac{N}{mm}$ fixed at the upper end.

The piece is deformed as a consequence of the forces on it caused because we attach the piece to the spring and we put a load 2 P in its midpoint (figure on the right).

We study this problem discretizing the piece in two linear 1-dimensional finite elements of equal length: Ω^1 at the lower part of the piece and Ω^2 at the upper part. We number the nodes from the bottom (where we take the origin x = 0).



Compute:

- (a) The shape functions $\psi_1^k(x)$, $\psi_2^k(x)$, of each element Ω^k . k=1,2.
- (b) Write the local stiffness matrices for both Ω^1 and Ω^2 .
- (e) Write the assembled system.
- (d) Set up boundary conditions
- (e) The displacement of the nodes Z and 3 of the piece when A=12, E=10, H=10, d=0.5, Note: You can use that:
 - The stregth produced by a string is -ke, where e is the extension of the spring.

Ex-Parcial QZ-2018-19. Exercise 1.

(6) Equation of the elasticity:
$$-\frac{d}{dx}\left(A\omega E(x)\frac{du}{dx}\right) = f(x)$$

Here: $A(x) = \varphi(x-L)^2$, $A(0) = \varphi(0-L)^2 = \varphi L^2 = A_0 \Rightarrow \alpha = \frac{A_0}{L^2}\frac{A_0}{4}$. Hence $A(x) = \frac{A_0}{4}(x-2)$.

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 $f(x) \equiv 0$ constant $\forall o \le x \le L = 2$ (reither weight nor other global forces are considered).

So, the corresponding coefficients on the model equation should be $q(x) = \frac{A_0 E(x-2)^2}{4}$ $q_0(x) = 0 \ \forall \ 0 \le x \le L = Z$, $f(x) = 0 \ \forall \ 0 \le x \le L = Z$.

$$\frac{1}{2} = \int_{1}^{2} \frac{1}{4} \frac{1}{4} \frac{1}{4} \frac{1}{4} \frac{1}{4} dx = \int_{1}^{2} \frac{1}{4} \frac{1}{4}$$

$$K_{12}^{1,1} = \int_{0_{1}(x)}^{x_{2}^{1}} \frac{dY_{1}^{1}}{dx} \frac{dY_{2}^{1}}{dx} dx = \int_{0}^{x_{2}^{1}} \frac{A_{0}E}{4} (x-z)^{2} (1) (1) dx = -\frac{A_{0}E}{4} \int_{0}^{1} (x-z)^{2} dx = -\frac{7A_{0}E}{12}$$

$$K_{21}^{1,1} = \int_{0}^{x_{2}^{1}} \frac{dY_{2}^{1}}{dx} \frac{dY_{2}^{1}}{dx} dx = \int_{0}^{x_{2}^{1}} \frac{A_{0}E}{4} (x-z)^{2} (1) (1) dx = -\frac{A_{0}E}{4} \int_{0}^{1} (x-z)^{2} dx = -\frac{7A_{0}E}{12}$$

$$K_{21}^{1,1} = \int_{0}^{x_{2}^{1}} \frac{A_{0}X_{2}}{dx} \frac{dY_{2}^{1}}{dx} dx = \int_{0}^{x_{2}^{1}} \frac{A_{0}E}{4} (x-z)^{2} (1) (1) dx = -\frac{A_{0}E}{4} \int_{0}^{1} (x-z)^{2} dx = -\frac{7A_{0}E}{12}$$

$$k_{22}^{1,1} = \int_{2}^{x_{2}^{\prime}} a_{1}(x) \frac{dy^{1}}{dx} \frac{dy^{1}}{dx} dx = \int_{0}^{x_{2}^{\prime}} \frac{A_{0}E}{4} (x-z)^{2} (1) \cdot (1) dx = \frac{A_{0}E}{4} \int_{0}^{1} (x-z)^{2} dx = \frac{7A_{0}E}{12}$$

On the other hand: Kij = 0 + inj=1,2, since &b)=0 + 0=x = 1/2 = 1. Therefore.

$$K^{4} = K^{2,4} = \frac{7A_{0}E}{12} \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$$

Let us compute now the components of K2,1:

$$K_{11}^{2,1} = \int_{\chi_{1}^{2}}^{\chi_{2}^{2}} \frac{d\psi_{1}^{2}}{dx} \frac{d\psi_{1}^{2}}{dx} dx = \int_{\chi_{2}^{2}}^{\chi_{2}^{2}} \frac{A_{0}E}{4} (x-2)^{2} (-1) (-1) dx = \frac{A_{0}E}{4} \int_{\chi_{2}^{2}}^{\chi_{2}^{2}} (x-2)^{2} dx = \frac{A_{0}E}{12}$$

$$(x) \int_{1}^{2} (x-2)^{2} dx = \left[\frac{(x-2)^{3}}{3} \right]_{1}^{2} = \frac{1}{3}$$

$$k^{2,1}_{12} = \int_{x^{2}}^{x^{2}} a_{1}(x) \frac{dV_{1}^{2}}{dx} \frac{dV_{2}^{2}}{dx} dx = \int_{12}^{4} \frac{A_{0}E}{4} (x-2)^{2} (-1)(1) dx = -\frac{A_{0}E}{4} \int_{12}^{4} (x-2)^{2} dx = -\frac{A_{0}E}{12}$$

$$k^{2,1}_{21} = \int_{x_{1}^{2}}^{x_{2}^{2}} a_{1}(x) \frac{dV_{2}^{2}}{dx} \frac{dV_{2}^{2}}{dx} dx = \int_{2}^{2} \frac{A_{0}E}{4} (x-2)^{2} (1)(1) dx = -\frac{A_{0}E}{4} \int_{12}^{2} (x-2)^{2} dx = -\frac{A_{0}E}{12}$$

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As for element 1, K2,0 = 0 since ob(x) = 0 also for all 1/2=1 = x \le L=Z. Therefore

$$\begin{bmatrix} K^2 = K^{2,1} = \frac{A_0 E}{12} \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix} \end{bmatrix}$$

(c) Assembled system:

$$\frac{A_{\circ}E}{12} \begin{pmatrix} 7 & -7 \\ -7 & 8 & -1 \\ -1 & 1 \end{pmatrix} \begin{pmatrix} \mathcal{U}_{1} \\ \mathcal{V}_{2} \\ \mathcal{U}_{3} \end{pmatrix} = \begin{pmatrix} \mathcal{Q}_{1} \\ \mathcal{Q}_{2} \\ \mathcal{Q}_{3} \end{pmatrix}$$

d
$$\begin{cases} 3 \\ -V_{2}V_{3} \end{cases}$$
foint force the spring:
$$Q = K(d-V_{3})$$

(d) Boundary Conditions:

Natural 8.C: O2=-21, Q3=K(d-U3) (See problem 10)

Essential B.C: U1=0

(e) $A_0=12$, E=10, K=10, $d=\frac{1}{2}$ and L=30.

Reduced system: $\begin{pmatrix} 80 & -10 \\ -10 & 10 \end{pmatrix}\begin{pmatrix} V_2 \\ V_3 \end{pmatrix} = \begin{pmatrix} -60 \\ 5-10V_3 \end{pmatrix} + \begin{pmatrix} 70 \\ 0 \end{pmatrix} \stackrel{?}{U} \Leftrightarrow \begin{pmatrix} 80-10 \\ -10 & 20 \end{pmatrix}\begin{pmatrix} V_2 \\ V_3 \end{pmatrix} = \begin{pmatrix} -60 \\ 5 \end{pmatrix}$

 $\Delta = \begin{vmatrix} 80 - 10 \\ -10 & 20 \end{vmatrix} = 1600 - 100 = 1500, \ \Delta_2 = \begin{vmatrix} -60 & -10 \\ 5 & 20 \end{vmatrix} = -1200 + 50 = -1150, \ \Delta_3 = \begin{vmatrix} 80 - 60 \\ -10 & 5 \end{vmatrix} = 400 - 600$

Hence, the displacements at nodes Z and 3 are:

$$\frac{U_2 = \Delta_2}{\Delta} = \frac{1150}{1500} = \frac{23}{30}, \quad U_3 = \frac{200}{1500} = \frac{2}{15}$$