METODES NUMERICS

| No. of the Control of | |
|--|---|
| $\psi_1^1(x) =$ | $\frac{3-x}{3}$ |
| $[K^1] =$ | $\frac{E}{2}\left(\begin{array}{cc}1 & -1\\-1 & 1\end{array}\right)$ |
| $[F^2] =$ | $-rac{\omega 2}{4}\left(egin{array}{c}2\\2\end{array} ight)$ |
| Assembled system: | $ \frac{E}{2} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix} \begin{pmatrix} U_1 \\ U_2 \\ U_3 \end{pmatrix} = \begin{pmatrix} Q_1 \\ Q_2 \\ Q_3 \end{pmatrix} - \frac{w^2}{4} \begin{pmatrix} 5 \\ 6 \\ 2 \end{pmatrix} $ |
| Boundary conditions: | $U_1 = 0, Q_2 = 0, Q_3 = -P$ |
| Displacement of the central point; | $-\frac{2}{E}(P+2\omega 2)$ |

(*Hint2:*The element K_{11} of the global matrix is one the values: E, E/2, E/3, E/4, E/5, E/6, E/7, E/8, E/9, E/10).

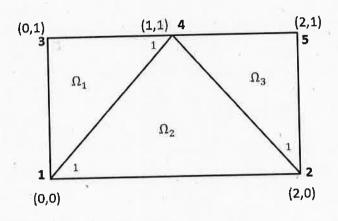
(*Hint3*:The component F_3 of the load vector is one the values: $-\omega/2$, $-\omega$, $-3\omega/2$, -2ω , $-5\omega/2$, -3ω , $-7\omega/2$, -4ω , $-9\omega/2$, -5ω).

(2 points)

(2) Let's consider the following problem in the domain $(0,2) \times (0,1)$:

$$\begin{cases}
-\Delta u = f, & \text{in } (0,2) \times (0,1) \\
u(x,0) = 2, & \text{for } 0 \le x \le 2 \\
u(2,y) = 2, & \text{for } 0 \le y \le 1 \\
\frac{\partial u}{\partial x}(0,y) = 4, & \text{for } 0 \le y \le 1 \\
\frac{\partial u}{\partial y}(x,1) = 6x, & \text{for } 0 \le x \le 2
\end{cases}$$

where f(x, y) = 6.



(2 points)

(i) Considering the mesh of the figure, fill the following table:

$$[K^{1}], \quad F^{1} = \frac{1}{2} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix}, \quad \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

$$[K^{2}], \quad F^{2} = \frac{1}{2} \begin{pmatrix} 1 & 0 & -1 \\ 0 & 1 & -1 \\ -1 & -1 & 2 \end{pmatrix}, \quad \begin{pmatrix} 2 \\ 2 \\ 2 \end{pmatrix}$$

$$[K^{3}], \quad F^{3} = \frac{1}{2} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix}, \quad \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$
Assembled system:
$$\frac{1}{2} \begin{pmatrix} 2 & 0 & -1 & -1 & 0 \\ 0 & 2 & 0 & -1 & -1 \\ -1 & 0 & 2 & -1 & 0 \\ -1 & -1 & -1 & 4 & -1 \\ 0 & -1 & 0 & -1 & 2 \end{pmatrix} \begin{pmatrix} U_{1} \\ U_{2} \\ U_{3} \\ U_{4} \\ U_{5} \end{pmatrix} = \begin{pmatrix} 3 \\ 3 \\ 1 \\ 4 \\ 1 \end{pmatrix} + \begin{pmatrix} Q_{1} \\ Q_{2} \\ Q_{3} \\ Q_{4} \\ Q_{5} \end{pmatrix}$$

(Hint1:The element K_{22} of the global matrix is one the values: 0, 1/2, 1, 3/2, 2, 5/2, 3, 7/2, 4, 9/2). (Hint2:The component F_2 of the load vector is one the values: 0,1,2,3,4,5,6,7,8,9).

(ii) Compute the values for Q_3 and Q_4 and the solution at the points U_3 , U_4 .

| $Q_3 =$ | 1 |
|---------|------|
| $Q_4 =$ | 6 |
| $U_3 =$ | 34/7 |
| $U_4 =$ | 54/7 |

- (3) Consider the mesh meshPlaca4foratsQuad.m.
 - (i) The quality of a quadrilateral element from a numerical point of view is defined as the ratio

$$R = \frac{longuestedge}{shortestedge},$$

it is considered good if $1 \le R \le 5$. Compute the maximum and minimum value of R for all the elements in this mesh.

| idElemMax= | 22 | MaxRatio= | 4.5572e+00 |
|------------|-----|-----------|------------|
| idElemMin= | 483 | MinRatio= | 1.0159e+00 |

(*Hint*: For element 27 we obtain R = 1.5344e + 00).

(ii) Compute the area of this object as the sum of the area of each element. Give the relative error obtained comparing this value with the true area.

| 2.8875e+01 | relError= | 5.59311e-04 |
|------------|------------|----------------------|
| | 2.8875e+01 | 2.8875e+01 relError= |

(*Hint*: For element 45 we obtain area = 1.9725e-02).

(2 points)

- (4) Consider again meshPlaca4foratsQuad.m as a four-holes aluminium plate, with thermal conductivity $k_c = 230.5$. The temperature at the boundaries of the holes is fixed at $T = 37.78^{\circ}$ C, whereas through the straight lines that form the upper and lower boundaries there is convection with the outer environment, at a bulk temperature $T_{\infty} = -17.78^{\circ}$ C and convection coefficient $\beta = 205.4$ (all units in the IS).
 - (i) Compute the maximum value on the convection boundaries.

| 63 | MaxTempConv= | 1.7268e+01 |
|----|--------------|-----------------|
| | 63 | 63 MaxTempConv= |

(Hint: For node 159 we obtain Temp= 3.7780e+01).

- (ii) Now we assign to each element a constant temperature T_e obtained from interpolation of the computed values in the center of the element (defined as the point with equal barycentric coordinates).
 - (a) Compute for the element e = 17 the coordinates of its center, (x_c, y_c) and the interpolated temperature value $T_e = T_{\text{interp}}(x_c, y_c)$ at that point.

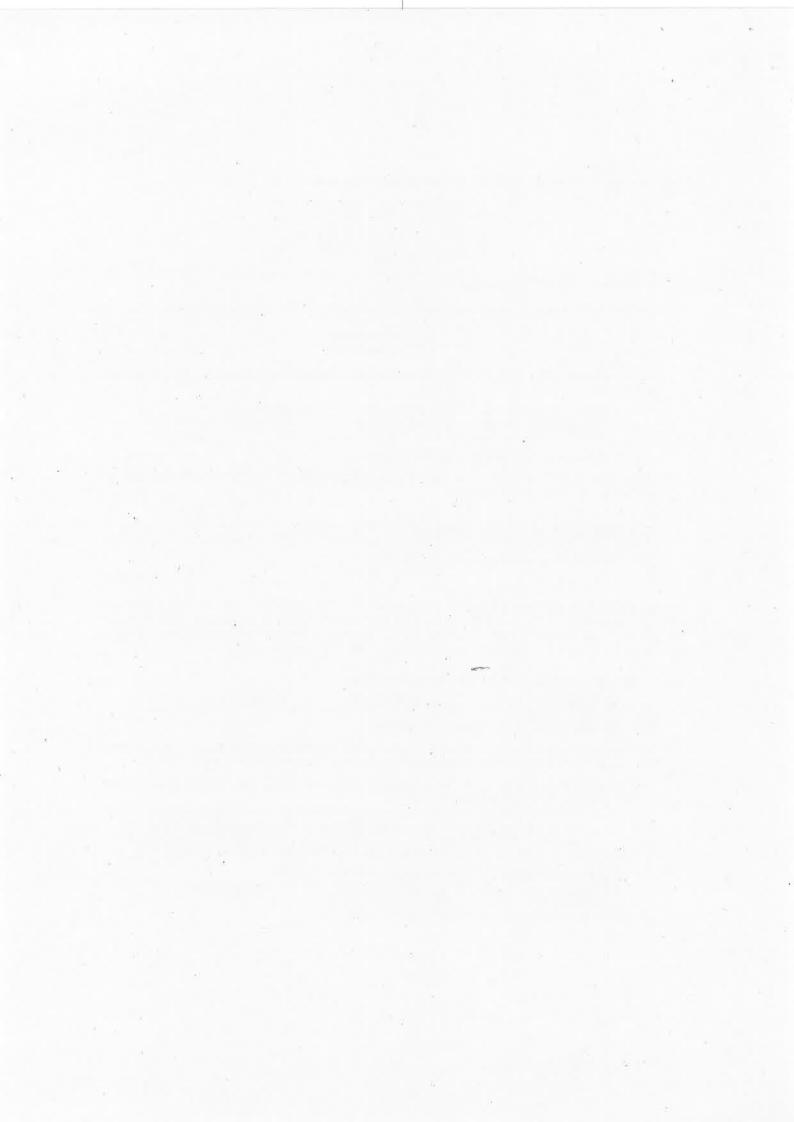
| x_c | y_c | T_e |
|------------|------------|------------|
| 5.4840e+00 | 2.0719e+00 | 3.4144e+01 |

(*Hint*: For the element 22 the center is at $(x_c, y_c) = (6.9147e + 00, 2.9503e + 00)$):

(b) Compute the element that have maximum temperature value:

| $idMaxT_e =$ | 653 | MaxTempElem= | 3.7413e+01 |
|--------------|-----|--------------|------------|
| | | | |

(*Hint*: For element 67 we obtain Temp= 2.4298e+01).



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$$\frac{2}{4} = \frac{c}{2ab} \left(\frac{b^2 - b^2}{-b^2} \frac{0}{a^2 + b^2} - a^2 \right) : \text{here } q = b = 1, c = k_c = 1$$

$$F^{-k} = \frac{f_{\kappa}A_{\kappa}}{3} \begin{pmatrix} 1\\1\\1 \end{pmatrix}$$

$$\beta_{2} = \gamma_{3}^{2} - \gamma_{1} = 1 - 0 = 1 \quad \gamma_{2}^{2}$$

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$$\beta_3^2 = \gamma_1^2 - \gamma_2^2 = 0 - 0 = 0$$
 $\gamma_3^2 = -(x_1^2 - x_2^2) = -(0 - 2) = 2$

$$K^{2,22} = \frac{a_{22}}{4A_{2}} \begin{pmatrix} \gamma_{i}^{2} \\ \gamma_{2}^{2} \\ \gamma_{3}^{2} \end{pmatrix} \cdot \begin{pmatrix} \gamma_{i}^{2} \\ \gamma_{2}^{2} \\ \gamma_{3}^{2} \end{pmatrix} = \left\{ a_{22} = a_{11} = 1 \right\} = \frac{1}{4} \begin{pmatrix} -1 \\ -1 \\ 2 \end{pmatrix} \begin{pmatrix} -1 - 1 \\ 2 \end{pmatrix} = \frac{1}{4} \begin{pmatrix} 1 & 1 - 2 \\ 1 & 1 - 2 \\ -2 - 2 & 4 \end{pmatrix}$$

Therefore
$$K = K^{2,11} + K^{2,12} + K^{2,21} + K^{2,22} + K^{2,00} = \frac{1}{4} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{1}{4} \begin{pmatrix} 1 & 1 & -2 \\ 1 & 1 & -2 \\ -1 & -1 & 2 \end{pmatrix}$$

$$=\frac{1}{2}\begin{pmatrix} 1 & 0 & -1 \\ 0 & 1 & -1 \\ -1 & -1 & 2 \end{pmatrix};$$

and:
$$F = \frac{4zA_2}{3} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \frac{6.1}{3} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} 2 \\ 2 \\ 2 \end{pmatrix}$$

(ti)
$$K^3 = K^1 = \frac{1}{2} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix}$$
, $F^3 = F^1 = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$.

$$k = \frac{1}{2} \begin{pmatrix} 1 & 0 & -1 \\ 0 & 1 & -1 \\ -1 & -1 & 2 \end{pmatrix}, F^{2} = \begin{pmatrix} 2 \\ 2 \\ 2 \end{pmatrix}$$

$$F = \begin{pmatrix} F_{1} \\ F_{2} \\ F_{2} \end{pmatrix} = \begin{pmatrix} F_{3}^{1} + F_{1}^{2} \\ F_{2}^{2} + F_{1}^{3} \\ F_{2}^{1} \\ F_{3}^{1} + F_{3}^{3} + F_{3}^{3} \\ F_{4}^{2} + F_{3}^{2} + F_{3}^{3} \\ F_{5}^{2} \end{pmatrix} = \begin{pmatrix} 3 \\ 3 \\ 4 \\ 4 \\ 1 \end{pmatrix}$$

Assembled system

$$\mathcal{A}_{nz}^{4}(s) = \begin{pmatrix} 1 \\ 1 \end{pmatrix} \begin{pmatrix} \frac{24}{9x}(0,s) \\ \frac{24}{9y}(0,s) \end{pmatrix} \cdot \begin{pmatrix} -\frac{24}{4} \end{pmatrix} = \begin{pmatrix} \frac{24}{9x}(0,s) \\ \frac{24}{9y}(0,s) \end{pmatrix} \cdot \begin{pmatrix} -\frac{1}{6} \\ 0 \end{pmatrix} \\
= -\frac{24}{9x}(0,s) = -4, \quad 0 \le S \le 1. \quad (*)$$

$$\mathcal{A}_{3} = \mathcal{A}_{21}^{4} + \mathcal{A}_{22}^{4}, \quad \mathcal{A}_{4} = \mathcal{A}_{11}^{4} + \mathcal{A}_{32}^{3}.$$

$$\mathcal{A}_{21}^{4} = \begin{pmatrix} \frac{9}{101}(0) \\ \frac{1}{3} \end{pmatrix} + \frac{9}{101}(1) \end{pmatrix} \begin{pmatrix} h_{1}^{4} = \begin{pmatrix} 0 \\ \frac{1}{3} \end{pmatrix} + \frac{6}{6} \end{pmatrix} \cdot 1 = 1.$$

$$\mathcal{A}_{22}^{4} = \frac{9}{102}(0) h_{2}^{4} = -\frac{4}{2} = -2$$

$$\mathcal{A}_{11}^{4} = \begin{pmatrix} \frac{9}{101}(1) \\ \frac{1}{3} \end{pmatrix} + \frac{9}{101}(0) \cdot h_{1}^{4} = \begin{pmatrix} \frac{6}{3} \cdot 1 + \frac{0}{6} \end{pmatrix} \cdot 1 = 2.$$

$$\mathcal{A}_{32}^{4} = \begin{pmatrix} \frac{9}{102}(1) \\ \frac{1}{3} \end{pmatrix} + \frac{9}{101}(1) \cdot h_{1}^{4} = \begin{pmatrix} \frac{6}{3} \cdot 1 + \frac{0}{6} \end{pmatrix} \cdot 1 = 2.$$

$$\mathcal{A}_{32}^{3} = \begin{pmatrix} \frac{9}{102}(1) \\ \frac{1}{3} \end{pmatrix} + \frac{9}{101}(1) \cdot h_{1}^{2} = \begin{pmatrix} \frac{6}{3} \cdot 1 + \frac{0}{6} \end{pmatrix} \cdot 1 = 4.$$

Boundary conditions:

- Natural:
$$Q_3 = Q_{21}^1 + Q_{22}^1 = 1 - 2 = -1$$
, $Q_4 = Q_{11}^1 + Q_{32}^3 = 2 + 2 = 6$

- Essential: $U_1 = U_2 = U_5 = 2$ (since u(x,0) = 2, for $0 \le x \le 2$, and u(z,y) = 2, for $0 \le y \le 1$, $U_1 = u(0,0) = 2$, $U_2 = u(z,0)$, $U_5 = u(z,1) = 2$).

Reduced system:
$$\frac{1}{2} \begin{pmatrix} 2 - 1 \\ -1 + 4 \end{pmatrix} \begin{pmatrix} V_3 \\ V_4 \end{pmatrix} = \begin{pmatrix} 4 \\ 4 \end{pmatrix} + \begin{pmatrix} -1 \\ 6 \end{pmatrix} - \frac{1}{2} \begin{pmatrix} -1 & 0 & 0 \\ -1 & -1 & -1 \end{pmatrix} \cdot \begin{pmatrix} V_4 = 2 \\ V_2 = 2 \\ V_5 = 2 \end{pmatrix}$$

$$\begin{pmatrix} -1 \\ -3 \end{pmatrix}$$

^(*) These parameterisations are not really necessary : Since the flows are either linear or constant, it's enough to know the values of quat the points coming from the corresponding edges.

$$U_1 = \frac{\Delta U_1}{\Delta} = \frac{34}{7}, \quad U_2 = \frac{\Delta U_2}{\Delta} = \frac{54}{7}$$