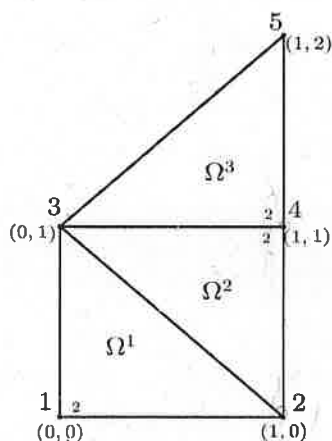


Name and surnames:

2. Consider the domain shown in the figure below, and with the elements, nodes and local and global numbering plotted there.



We want to solve the thermal problem defined by the equation

$$-\frac{\partial^2 T}{\partial x^2} - \frac{\partial^2 T}{\partial y^2} = 0$$

with boundary conditions given by:

- At the line that joints nodes 2 and 5, there is convection BC with $\beta = 3$ and $T_\infty = 30$
- $T = 100$ at the nodes 5, 3, 1 and 2.

Then, compute:

- The stiffness matrix of the first element K^1 .
- The 4th row of the global stiff matrix before applying the BC.
- The value of the coefficients for Q_{21}^2 of the local system for Ω^2 as a function of T_2 and T_4 .
- The value of the coefficients for Q_{22}^3 of the local system for Ω^3 as a function of T_4 and T_5 .
- The value of T_4 .

| Results: | |
|--|---|
| $[K^1] =$ | $\frac{1}{2} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix}$ |
| 4th row : | $\frac{1}{2} (0 \quad -1 \quad -2 \quad 4 \quad -1)$ |
| $Q_{21}^2 = a_1 T_2 + a_2 T_4 + a_3$ | coeff a_i : $a_1 = -\frac{1}{2}, \quad a_2 = -1, \quad a_3 = 45$ |
| $Q_{22}^3 = b_1 T_4 + b_2 T_5 + b_3$ | coeff b_i : $b_1 = -1, \quad b_2 = -\frac{1}{2}, \quad b_3 = 45$ |
| a_i and b_i are among the values: $-2, 2, 1, -1, 1/2, -1/2, 1/6, -1/6, 35, 40, 45, 50, 85, 90, 95, 100, 105$ | |
| $T_4 =$ | 47.5 |

(2 points)

①
Data: $T_0 = 30$, $\beta = 3$, $T = T_{1,3,5,2} = 100^\circ\text{C}$

②

i) $K^1 = \frac{1}{2} \begin{pmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{pmatrix} = K^2 = K^3$

ii) $K(4,:) = (0, K_{21}^2, K_{23}^2 + K_{21}^3, K_{22}^2 + K_{22}^3, K_{23}^3)$
 $= \frac{1}{2} (0, -1, -2, 4, -1)$

iii) $Q_{21}^2 = \int_0^{h_1^2} -\beta (T_2 \psi_{11}^2(s) + T_4 \psi_{21}^2(s) - T_\infty) \psi_{21}^2(s) ds$
 $= -\beta T_2 \int_0^{h_1^2} \psi_{11}^2(s) \psi_{21}^2(s) ds - \beta T_4 \int_0^{h_1^2} (\psi_{21}^2(s))^2 ds + \beta T_\infty \int_0^{h_1^2} \psi_{21}^2(s) ds$
 $= -\beta T_2 h_1^2 \frac{1!1!}{3!} - \beta T_4 h_1^2 \frac{2!0!}{3!} + \beta T_\infty h_1^2 \frac{1!0!}{2!}$
 $= -\beta h_1^2 \left(\frac{T_2}{6} + \frac{T_4}{3} - \frac{T_\infty}{2} \right) \Big|_{h_1^2=1} = -3 \left(\frac{T_2}{6} + \frac{T_4}{3} - 15 \right) = \boxed{-\frac{1}{2}T_2 - T_4 + 45}$

Alternatively, using the "linear flow's rule":

$$Q_{21}^2 = -\beta h_1^2 \left(\frac{T_2}{2} + \frac{1}{3} (T_4 - T_2) \right) + \beta h_1^2 \frac{T_\infty}{2} = -\beta h_1^2 \left(\frac{T_2}{6} + \frac{T_4}{3} - \frac{T_\infty}{2} \right) = -3 \left(\frac{T_2}{6} + \frac{T_4}{3} - 15 \right)$$

iv) $Q_{22}^3 = \int_0^{h_2^3} -\beta (T_4 \psi_{22}^3(s) + T_5 \psi_{32}^3(s) - T_\infty) \psi_{22}^3(s) ds$
 $= -\beta T_4 \int_0^{h_2^3} (\psi_{22}^3(s))^2 ds - \beta T_5 \int_0^{h_2^3} \psi_{32}^3(s) \psi_{22}^3(s) ds + \beta T_\infty \int_0^{h_2^3} \psi_{22}^3(s) ds$
 $= -\beta T_4 h_2^3 \frac{2!0!}{(2+0+1)!} - \beta T_5 h_2^3 \frac{1!1!}{(1+1+1)!} + \beta T_\infty h_2^3 \frac{1!0!}{(1+0+1)!}$
 $= -\beta h_2^3 \left(\frac{T_4}{3} + \frac{T_5}{6} - \frac{T_\infty}{2} \right) \Big|_{h_2^3=1} = -3 \left(\frac{T_4}{3} + \frac{T_5}{6} - 15 \right) = \boxed{-T_4 - \frac{1}{2}T_5 + 45}$

Alternatively:

$$-\beta h_2^3 \left(\frac{T_4}{2} + \frac{1}{6} (T_5 - T_4) \right) + \beta h_2^3 \frac{T_\infty}{2} = -\beta h_2^3 \left(\frac{T_4}{3} + \frac{T_5}{6} \right) + \beta h_2^3 \frac{T_\infty}{2}$$

$$= -\beta h_2^3 \left(\frac{T_4}{3} + \frac{T_5}{6} - \frac{T_\infty}{2} \right) = -3 \left(\frac{T_4}{3} + \frac{T_5}{6} - 15 \right)$$

$K_{22} T_4 =$

⑤

B.C.

Essentials: $T_2 = T_1 = T_3 = T_5 = T = 100$

Natural: $Q_4 = Q_{24}^2 + Q_{22}^3 = -\beta \left(\frac{T_2}{6} + \frac{2T_4}{3} + \frac{T_5}{6} - T_\infty \right)$
 $T_2 = T_5 = T = -\frac{\beta}{3} (T + 2T_4 - 3T_\infty)$

Reduced system:

$$K_{44} T_4 = -\beta/3 (T + 2T_4 - 3T_\infty) - K_{41} \overset{T}{T_1} - K_{42} \overset{T}{T_2} - K_{43} \overset{T}{T_3} - K_{45} \overset{T}{T_5}$$

$$= -(\beta/3 + K_{41} + K_{42} + K_{43} + K_{45}) T + \beta T_\infty - 2\beta/3 T_4$$

$$\Leftrightarrow 2T_4 = -(\beta/3 - 0 - \frac{1}{2} - 1 - \frac{1}{2}) \cdot T + \beta T_\infty - 2\beta/3 T_4$$

$$T_4 = \frac{(2 - \beta/3) T + \beta T_\infty}{2(1 + \beta/3)} = \frac{(2-1) \times 100 + 3 \times 30}{2(1+1)} = \frac{190}{4} = \frac{95}{2} = \boxed{47.5}$$

$\beta = 3$
 $T = 100$
 $T_\infty = 30$