

**Pedestal Structure and Stability in High-Performance Plasmas on  
Alcator C-Mod**

by

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*Abstract*

High-performance operation in tokamaks is characterized by the formation of a *pedestal*, a region of suppressed transport and steep gradients in density, temperature, and pressure near the plasma edge. The pedestal height is strongly correlated with overall fusion performance, as a substantial pedestal supports the elevated core pressure necessary for the desired fusion reaction rate and power density. However, stationary operation requires some relaxation of the particle transport barrier, to avoid the accumulation of impurities (e.g., helium “fusion ash,” plasma-facing surface materials) in the plasma. Moreover, the formation of the pedestal introduces an additional constraint: the steep gradients act as a source of free energy for Edge-Localized Mode (ELM) instabilities, which on ITER- or reactor-scale devices can drive large, explosive bursts of particle and energy transport leading to unacceptable levels of heat loading and erosion damage to plasma-facing materials. As such, the suppression, mitigation, or avoidance of large ELMs is the subject of much current research.

In light of this, a firm physical understanding of the pedestal structure and stability against the ELM trigger is essential for the extrapolation of high-performance regimes to large-scale operation, particularly in operating scenarios lacking large, deleterious ELMs. This thesis focuses on the *I-mode*, a novel high-performance regime pioneered on the Alcator C-Mod tokamak. I-mode is unique among high-performance regimes in that it appears to decouple energy and particle transport, reaching H-mode levels of energy confinement with the accompanying temperature pedestal while maintaining a L-mode-like density profile and particle transport. I-mode exhibits three attractive properties for a reactor regime: (1) I-mode appears to be inherently free of large ELMs, avoiding the need for externally-applied ELM control. (2) The lack of a particle transport barrier maintains the desired level of impurity flushing from the plasma, avoiding excessive radiative losses. (3) Energy confinement in I-mode presents minimal degradation with input heating power, contrary to that found in H-mode.

This thesis presents the results from a combined empirical and computational study of the pedestal on C-Mod. Analysis methods are first implemented in ELMy H-mode base cases on C-Mod – in particular, the EPED model based on the combined constraints from peeling-balloonning MHD instability and kinetic-balloonning turbulence is tested on C-Mod. Empirical results in ELMy H-mode are consistent with the physics assumptions used in EPED, with the pedestal pressure gradient constrained by  $\nabla p \sim I_p^2$  expected from the balloonning stability limit. To lowest-order approximation, ELMy H-mode pedestals are limited in  $\beta_{p,ped}$ , with the attainable beta set by shaping – within this limit, an inverse relationship between pedestal density and temperature is seen. The pedestal width is found to be described by the scaling  $\Delta_\psi = G\beta_{p,ped}^{1/2}$  expected from the KBM limit, where  $G(\nu, \epsilon, \dots)$  is a weakly varying function with  $\langle G \rangle = 0.0857$ . No systematic secondary scalings with field, gyroradius, shaping, or collisionality are observed. The EPED

model, based on these assumptions, correctly predicts the pressure pedestal width and height to within a systematic  $\sim 20\%$  uncertainty.

Empirical scalings in I-mode highlight the operational differences from conventional H-modes. The temperature and pressure pedestal exhibit a positive trend with current, similar to H-mode (although I-mode pedestal temperature typically exceeds that found in comparable H-modes) – however, the temperature and pressure respond significantly more strongly to heating power, with  $T_{e,95} \sim P_{net}/\bar{n}_e$  and  $p_{95} \sim P_{net}$ . The I-mode density profile is set largely independently of the temperature pedestal (unlike ELMy H-mode), controlled by operator fueling. Given sufficient heating power to maintain a consistent  $P_{net}/\bar{n}_e$ , temperature pedestals are matched across a range of fueling levels. This indicates a path to readier access and increased performance in I-mode, with the mode accessed at moderate density and power, after which the pedestal pressure is elevated with matched increases in fueling and heating power. Global performance metrics in I-mode are competitive with H-mode results on C-Mod, and are consistent with the weak degradation of energy confinement with heating power.

I-mode pedestals are also examined against the physics basis for the EPED model. Peeling-balloonning MHD stability is calculated using the ELITE code, finding the I-mode pedestal to be strongly stable to the MHD modes associated with the ELM trigger. Similarly, modeling of the KBM using the infinite-n ballooning mode calculated in BALOO as a surrogate for the threshold indicates that the I-mode pedestal is stable to kinetic-balloonning turbulence, consistent with the observed lack of a trend in the pedestal width with  $\beta_{p,ped}$ . This is found to be the case even in I-modes exhibiting small, transient ELM-like events. The majority of these events are triggered by the sawtooth heat pulse reaching the edge, and do not negatively perturb the temperature pedestal – it is proposed, then, that these events are not true peeling-balloonning-driven ELMs, but rather are an ionization front in the SOL driven by the sawtooth heat pulse. There are transient ELM events showing the characteristic temperature pedestal crash indicating a true ELM – the steady I-mode pedestals around these isolated events are also modeled to be P-B and KBM stable, although more detailed modeling of these events is ongoing.

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## INTRODUCTION

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The population of the earth is projected to increase substantially over the next half-century, potentially reaching as high as 10 billion globally by 2050 [1]. At the same time, any attempt to increase the quality of life of the existing population will necessarily involve increased energy consumption per capita, with a greater fraction of the earth approaching “first-world” consumption levels [2]. As such, worldwide energy consumption will likely continue to increase in the next few decades [3, 4]

This increase in energy demand occurs in parallel with increased pressure on traditional energy sources. Fossil fuels (oil, coal, and natural gas), while reliable sources of base-load power, nevertheless face issues. Oil faces increasing cost and technical difficulty in capturing dwindling available reserves, as well as the potential for serious ecological damage from accidents (e.g., the Deepwater Horizon offshore rig accident in 2010). Coal, while more readily available (an estimated 257 billion tons of recoverable reserves in the US, lasting roughly 240 years at current consumption [4, 5]), releases particulate matter into the atmosphere, with serious consequences both to the environment and to human health, as well as the greenhouse gases tied to deleterious climate change.

Renewable energy sources have a certain “green” appeal, providing power generation free of pollution and carbon emissions, and are in many cases scalable and near cost-competitive with fossil-fuel sources – however, each is subject to limitations on their implementation. Solar and wind power suffer from a large degree of variability in their output, necessitating a combination of expensive energy storage methods or (often fossil-fuel based) backup production to handle shortfalls. Hydroelectric and geothermal power are suitable for base-load power production, but are strictly limited in their implementation by geographic concerns – bluntly, there are relatively few locations where hydro or geothermal power generation is feasible, and many of these have already been developed.

Conventional – that is, fission-based – nuclear power can also supply carbon-free base-load power, with fuel reserves lasting through the next century. While nuclear power does suffer from the potential for extremely serious accidents (Fukushima, Chernobyl) it has, on a per-energy-produced basis, a remarkably good safety record. Public perception of nuclear power nevertheless hinges on the threat of serious accidents, limiting both the expansion of nuclear power to meet increasing demand and the development of safe long-term handling

of existing nuclear waste, as well as, ironically, preventing the replacement of an aging reactor fleet with newer, safer designs.

*Fusion*, the nuclear process driving stellar cores, is a potentially highly attractive option for satisfying the world's growing energy needs in an efficient, environmentally-sound manner. A fusion reactor would supply base-load power using only a small amount of an effectively inexhaustible fuel (readily available for harvesting from seawater), with no greenhouse gas emissions or high-level radioactive waste, and the physical impossibility of a major "meltdown" accident. However, fusion remains in the experimental stage, with significant technical hurdles remaining before the development of a prototype fusion power plant. This thesis will attempt to contribute to the understanding of one of these hurdles. Further reading on the development of fusion energy is available to the interested reader in several excellent references. [6, 7, 8] •

## 1.1 PLASMAS FOR FUSION

A *plasma* is a gas to which sufficient energy has been applied to strip some or all of the electrons from the nuclei of its constituent atoms. In a plasma, ions and electrons freely interact with one another through Coulomb collisions, behaving as coupled electrodynamic fluids. Plasmas of interest for fusion research are comprised of light elements (typically hydrogenic isotopes), and are at extremely high temperatures, in excess of 100 million Kelvin (10 – 20 keV). As these conditions are far in excess of the ionization energy for these elements, the plasma is dominated by collisions between its charged particles, rather than interactions with bound electron states.

### 1.1.1 *Plasma Parameters*

As the plasma is composed of free charged particles, it responds strongly to electric and magnetic fields. In the presence of a DC electric field (externally applied, or generated by an imbalance of positive and negative charge in the plasma), the plasma will rearrange itself to screen out the field. This effect breaks down at short length scales, at which there are insufficient numbers of charge carriers to rearrange and counter the field – the characteristic scale for this effect is the Debye Length, given by

$$\lambda_D = \sqrt{\frac{\epsilon_0 T}{n e^2}} \quad (1.1)$$

where  $n$  is the particle density,  $T$  is the temperature,  $e$  is the electron charge, and  $\epsilon_0$  is the vacuum permittivity. At size scales significantly larger than  $\lambda_D$ , this will enforce an approximately balanced electric

charge in the plasma, termed “quasi-neutrality”. This is reflected in the number densities of electrons and multiple ion species  $j$ , each with charge  $Z_j$ , by the relation

$$n_e = \sum_j n_j Z_j \quad (1.2)$$

In a multiple-ion species plasma, we may also define an effective ion charge

$$Z_{\text{eff}} = \frac{1}{n_e} \sum_j n_j Z_j^2 \quad (1.3)$$

The electrostatic force driving this charge redistribution induces a “ringing” oscillation in the plasma (primarily the electrons), at the characteristic plasma frequency  $\omega_p$ :

$$\omega_p = \sqrt{\frac{n e^2}{\epsilon_0 m_e}} \quad (1.4)$$

( $m_e$  is the electron mass). This natural oscillation in the plasma also has the effect of screening the vacuum EM propagation of AC electric fields varying at frequencies  $\omega < \omega_p$ .

Coulomb collisions between charged particles in the plasma tend to drive magnetically-confined plasmas into thermal equilibrium, with the velocity distribution for a species given by the Maxwellian

$$f(v) = n \left( \frac{m}{2\pi T} \right)^{3/2} \exp \left( -\frac{mv^2}{2T} \right) \quad (1.5)$$

where  $v$  is the species particle velocity. Electron-ion collisions also cause the plasma to emit a continuous spectrum of Bremsstrahlung radiation. For a plasma in thermal equilibrium, integration over the full spectrum gives for the total radiated power

$$P_{\text{Brems}} = (5.35 \times 10^{-37}) n_e^2 Z_{\text{eff}} \sqrt{T} \quad (1.6)$$

with  $n_e$  in  $\text{m}^{-3}$  and  $T$  in keV giving  $P_{\text{Brems}}$  in MW, representing a consistent source of heat loss from the plasma.

### 1.1.2 Fusion Fuels

Fusion collectively refers to the class of nuclear reactions merging lighter nuclei into a single heavier element. While fusion reactions



**Figure 1.1:** Binding energy per nucleon versus atomic mass number, with notable isotopes marked. Reactions forming nuclei with higher binding energy are exothermic – thus, fusion of elements lighter than  $^{56}\text{Fe}$  or fission of elements heavier than  $^{56}\text{Fe}$  releases energy. [9]

for elements lighter than iron are generally exothermic, as they form nuclei with greater binding energy per nucleon (see fig. 1.1), the most common and readily attainable involve isotopes of hydrogen or helium, the most promising candidates for which are shown below.



Here D and T indicate nuclei of deuterium and tritium, two heavy isotopes of hydrogen (one proton plus one and two neutrons, respectively). The volumetric fusion reaction rate  $R_f$  is given by

$$R_f = n_1 n_2 \langle \sigma v \rangle_{1,2} \quad [\text{m}^{-3} \cdot \text{s}^{-1}] \quad (1.11)$$

where  $n_1$  and  $n_2$  indicate the densities of the two fuel ions (e.g., for deuterium-tritium fuel  $n_1 n_2 = n_D n_T$ , while for pure-deuterium fuel  $n_1 n_2 = \frac{1}{2} n_D^2$  to remove double-counting of fuel ions) and  $\langle \sigma v \rangle_{1,2}$  is a rate parameter incorporating the energy-dependent reaction cross-



**Figure 1.2:** Reaction rate normalized to fuel density, expressed as the rate coefficient  $\langle \sigma v \rangle$ , for fusion fuels as a function of temperature. Notably, deuterium-tritium fusion exhibits a higher peak reaction rate, as well as reaching that peak at a lower temperature, than other fuels.

section averaged over the Maxwellian velocity distribution of the fuel ions (eq. (1.5)). In practice, the energy-dependent cross-section is empirically determined – measured rate parameters  $\langle \sigma v \rangle$  for the fuels of interest are shown in fig. 1.2.

Pure deuterium fuel (reactions shown in eqs. (1.7) and (1.8)) is attractive from a research standpoint, due to the abundance and ease of use of deuterium. Deuterium is a stable nucleus, obviating the need for radiation safety in the fuel system, and is naturally occurring in relative abundance (approximately 1/6420 of hydrogen nuclei on earth are deuterium [10]), allowing harvesting of deuterium fuel from seawater. However, pure-deuterium reactions suffer from low energy output per reaction and a significantly lower reaction rate at feasible plasma conditions compared to other fuel options (see fig. 1.2), setting high performance requirements for a putative DD-burning reactor.

The D –  ${}^3\text{He}$  reaction (eq. (1.9)) exhibits several desirable properties, namely an impressive energy yield per reaction, and the fact that the reaction produces only charged particles rather than the high-energy neutrons found in D – D and D – T reactions, which can cause significant damage to reactor materials (note, however, that a D –  ${}^3\text{He}$  plasma will also undergo neutronic D – D fusion at a meaningful rate). However, as with D – D fuel, the D –  ${}^3\text{He}$  reaction suffers from a lower reaction rate at attainable conditions, as well as

the fact that Helium-3 does not occur in economically usable quantities on Earth. While off-planet sources of Helium-3 exist (for example, a useful quantity is present in the lunar regolith [11] and in the atmospheres of some gas giants [12]), this fuel remains the subject of speculation.

The deuterium-tritium reaction (eq. (1.10)) is considered the most promising for a first-generation fusion reactor, due to its high energy output per reaction and favorable reaction cross-section – the rate parameter  $\langle\sigma v\rangle_{DT}$  reaches its peak at a lower temperature, and reaches a greater absolute level than other fusion fuels. However, D – T operation is limited both by fuel sources, and reaction products. D – T fusion produces a 14 MeV neutron, carrying 80% of the energy released by the fusion reaction, which can damage unshielded reactor materials. Moreover, while deuterium is stable and readily available, tritium is radioactive with a short half-life (roughly 12.3 years), so it is not naturally occurring in meaningful quantities on earth. A reactor will solve both of these problems with a *neutron blanket*, a neutron-absorbing structure surrounding the plasma. This provides the necessary shielding for sensitive reactor components. The heat generated in the blanket from neutron absorption will also be drawn off in a steam cycle to drive turbines, generating electricity from the reactor. Finally, seeding the blanket with lithium allows the following reactions with fusion neutrons:



the Lithium-6 reaction (eq. (1.12)) absorbs “slow” neutrons (that is, neutrons that have thermalized to the blanket temperature via collisions) to produce tritium, plus additional heat. Lithium-7 (eq. (1.13)) is an endothermic reaction, although the reaction also preserves the free neutron through the breeding reaction. Using blankets enriched with  $^6\text{Li}$ , coupled with neutron multipliers, a reactor will target an over-unity tritium breeding ratio, with  $> 1$  tritons produced per neutron entering the blanket (i.e., per tritium consumed in a fusion reaction). •

## 1.2 MAGNETIC CONFINEMENT

### 1.2.1 Basic Principles

The temperatures in excess of 100 million Kelvin necessary for fusion in a plasma are incompatible with any contact between solid reactor materials and the hot core of the plasma. Magnetic confinement relies on the strong response of the charged particles composing the plasma

**Figure 1.3:** Electron and ion gyro orbits in an applied magnetic field. Note that, due to the charge dependence in the Lorentz Force (eq. (1.14)), electrons and ions orbit in opposite directions relative to the magnetic field.



to magnetic fields, rather than a material wall, to retain the thermal pressure ( $\sim 10$  atm for a reactor) from the plasma. The response of a charged particle to electric and magnetic fields is governed by the Lorentz force,

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B}) \quad (1.14)$$

In a strong background magnetic field, the particle will move on a helical path along the field line. The  $\vec{v} \times \vec{B}$  factor in the Lorentz Force causes the particle to experience no magnetic force parallel to the field, while velocity perpendicular to the field generates a force proportional to the velocity times the magnetic field, directed perpendicular to both – thus the particle freely streams parallel to the field, but is trapped in a circular orbit perpendicular to it, termed “gyro motion”, shown in fig. 1.3. The particle will orbit at the cyclotron frequency,

$$\omega_c = \frac{qB}{m} \Rightarrow \omega_{ce} = \frac{eB}{m_e}, \quad \omega_{ci} = \frac{ZeB}{m_i} \quad (1.15)$$

for electrons and ions of charge  $Z$ , respectively (note that for brevity we indicate the magnitude of vectors as scalar variables, e.g.,  $B = |\vec{B}|$ ). A particle with velocity perpendicular to the magnetic field  $v_\perp$  (formally,  $v_\perp = |\vec{v} \times \vec{B}|/B$ ) orbits at its gyroradius,

$$\rho = \frac{v_\perp}{\omega_c} = \frac{mv_\perp}{qB} \quad (1.16)$$

For a thermalized plasma, the perpendicular velocity will, on average, be the thermal velocity  $v_t = \sqrt{2T/m}$ , thus

$$\rho = \frac{\sqrt{2mT}}{qB} \quad (1.17)$$

The introduction of a nonzero electric field drives additional motion for the particle in the form of a drift velocity – the guiding center (that is, the average point about which the orbital motion of the particle gyrates) will shift with a bulk velocity (see [6, § 8.4] for derivation)

$$\vec{v}_d = \frac{\vec{E} \times \vec{B}}{B^2} \quad (1.18)$$

independent of particle charge, mass, or energy.

This restriction of particle motion perpendicular to field lines to short length scales (at fusion-relevant temperatures and magnetic fields, the gyroradius is typically  $\sim 10^{-5}$  m for electrons and  $\sim 10^{-3}$  m for ions) compared to the size of the plasma is central to the concept of magnetic confinement. In the perpendicular direction, this scale restriction of particle motion permits a fluid treatment of the dynamics of the plasma. Further simplification of the fluid model (see [13, § 2.3] for detailed derivation) leads to the theory of *magnetohydrodynamics* (MHD), the “workhorse” model describing plasma behavior:

$$\begin{aligned} \frac{d\rho}{dt} + \rho \nabla \cdot \vec{v} &= 0 && \text{(mass continuity)} \\ \rho \frac{d\vec{v}}{dt} &= \vec{j} \times \vec{B} - \nabla p && \text{(momentum continuity)} \\ \frac{dp}{dt} &= -\gamma p \nabla \cdot \vec{v} && \text{(energy conservation)} \end{aligned} \quad (1.19)$$

where  $\rho$  is the mass density,  $\vec{v}$  is the fluid velocity,  $p$  is the pressure,  $\vec{j}$  and  $\vec{B}$  are the current density and magnetic field,  $\gamma$  is the ratio of specific heats, and  $d/dt = \partial/\partial t + \vec{v} \cdot \nabla$  is the “convective derivative.” A basic equilibrium in a confined plasma is described in MHD by the simple relation

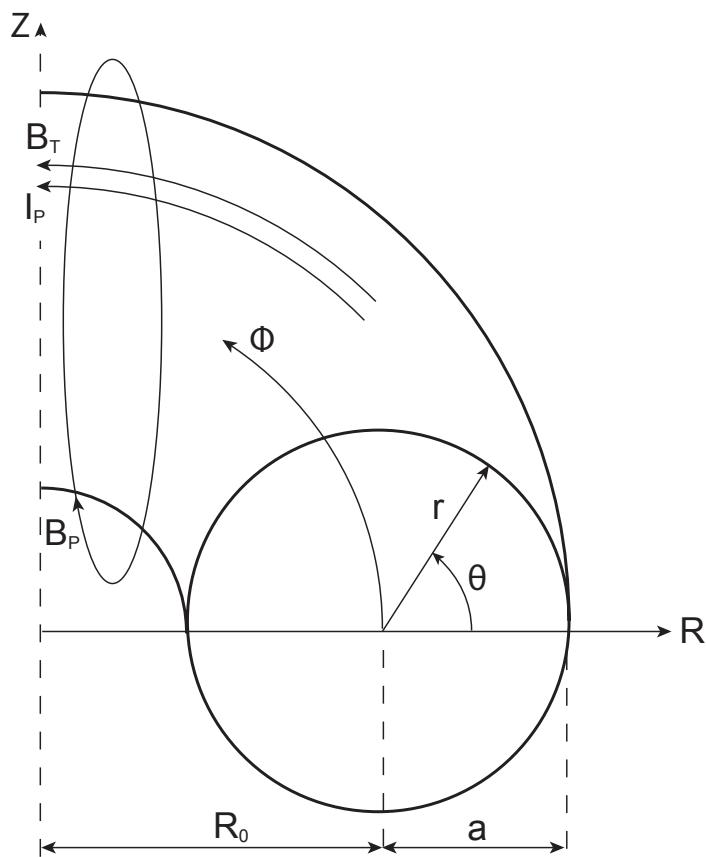
$$\nabla p = \vec{j} \times \vec{B} \quad (1.20)$$

in which the outward force due to the plasma pressure gradient is balanced by an inward force from the interplay between magnetic fields and electric currents. This interplay is readily illustrated in the simple one-dimensional case of an infinite straight cylinder of plasma – in this case, the radially-outward  $\nabla p$  force may be balanced by an axial current in the  $\hat{z}$  direction with an azimuthal  $\hat{\theta}$  magnetic field ( $z$ -pinch),

an azimuthal current and axial field ( $\theta$ -pinch), or a superposition of the two (screw pinch). However, all three of these options suffer from a lack of parallel confinement – as the magnetic field does not restrict the free-streaming parallel motion of the plasma, these linear concepts (when reduced to a physical, non-infinite size!) suffer from plasma losses at the ends of the cylinder. Despite efforts to restrict the parallel motion in a linear device (e.g., the *magnetic mirror*, which pinches the magnetic field at the cylinder ends in order to reflect the parallel motion of particles with a force due to the field gradient [14]), end losses in linear devices proved incompatible with steady-state fusion conditions. The clear solution, then, was to close the magnetic geometry such that the magnetic field lines have no ends: a *torus*.

### 1.2.2 Toroidal Configurations

**Figure 1.4:** Example geometry of a circular-cross-section tokamak plasma, describing a torus of major radius  $R_0$  and minor radius  $a$ , with poloidal coordinate  $\theta$  and toroidal coordinate  $\Phi$ . Tokamak configurations are characterized by an applied toroidal field  $B_T$  with a toroidal plasma current  $I_p$ , which in turn generates a poloidal magnetic field  $B_p$ .



An example toroidal geometry is shown above in fig. 1.4. In comparison to the previous straight cylindrical geometry, the radial coordinate is replaced by a *minor radius*  $r$ , measured from the center of the plasma column to its edge ( $r = a$ ), while the *major radius*  $R_0$  denotes the radius of the torus itself measured from its center axis (Z in fig. 1.4) to the plasma axis. The azimuthal cylindrical coordi-

nate is replaced by the poloidal coordinate  $\theta$ , wrapping immediately about the plasma column. The axial coordinate in the cylindrical system is replaced by the toroidal angle  $\Phi$  wrapping around the center axis of the torus and describing a circuit along the plasma column. As with the straight cylindrical case, the magnetic geometry may be described with toroidal and poloidal currents and magnetic fields balancing radially-outward thermal pressure.

However, introducing toroidal effects into the magnetic geometry gives rise to additional drift velocities, causing the guiding centers of particle gyro-orbits to shift (see [6, § 8.5-7]). Spatial variation in the magnetic field strength causes the  $\nabla B$  drift, given by

$$\vec{v}_{\nabla B} = \frac{v_{\perp}^2}{2\omega_c} \frac{\vec{B} \times \nabla B}{B^2} \quad (1.21)$$

while the bent toroidal magnetic field in the magnetic field causes the curvature drift,

$$\vec{v}_k = \frac{v_{\parallel}^2}{\omega_c} \frac{\vec{R}_c \times \vec{B}}{R_c^2 B} \quad (1.22)$$

where  $v_{\parallel}$  is the particle velocity parallel to the magnetic field,  $\omega_c$  is the species cyclotron frequency (eq. (1.15)), and  $\vec{R}_c$  is the radius of curvature of the field. In the case of a vacuum toroidal magnetic field, these drifts are directed vertically in the  $\hat{Z}$  direction, and are directed oppositely for electrons and ions due to the charge dependence in  $\omega_c$ . The electric field resulting from this charge separation drives a radially-outward  $\vec{E} \times \vec{B}$  drift (see eq. (1.18)), which effectively deconfines the plasma. This effect is countered by the addition of a poloidal field, which adds a helical twist to the guiding-center path to average out the separation due to particle drifts. Concepts aiming for steady-state magnetic confinement of a plasma typically rely on generating this twist, termed the *rotational transform*, to maintain stable confinement.

One of the most successful implementations of this concept for Magnetic Fusion Energy (MFE) is the *tokamak* [7] (a Russian acronym from *тороидальная камера с магнитными катушками*, *toroidalnaya kamera s magnitnymi katushkami*, “toroidal chamber with magnetic coils”). The tokamak design is characterized by a strong toroidal magnetic field (variously denoted  $B_T$  or  $B_{\Phi}$ ) applied by external coils, with a poloidal field ( $B_p$  or  $B_{\theta}$ ) primarily generated by a current (termed the *plasma current*  $I_p$ ). A schematic of the plasma and coil arrangement for a tokamak is shown in fig. 1.5. By generating the rotational transform to the magnetic field using the plasma current, the tokamak design utilizes relatively simple planar magnetic coils, avoiding the significantly more complex three-dimensional coils



**Figure 1.5:** Schematic of a tokamak configuration, showing the plasma and magnetic coils. The applied toroidal magnetic field is generated by the toroidal field coils (shown in blue). A toroidal plasma current is generated by the center transformer, in turn generating a poloidal magnetic field (shown in green). These combine to form the helical magnetic field. The plasma shape and equilibrium is adjusted with the outer poloidal field coils (gray).

used to generate the helical field in a *stellarator* (the major competing design concept [15]). However, the necessity for large ( $> 1 \text{ MA}$ ) plasma currents presents a significant engineering and physics challenge. It is straightforward to generate the plasma current through a simple transformer action from a central solenoid in the torus (depicted in fig. 1.5) – however, this AC-current-driven transformer action necessarily limits tokamaks to pulsed operation. Generation of non-inductive DC current drive [16], via RF [17, 18] or particle beams [19], is an active area of research in tokamak physics and engineering, but is outside the scope of this thesis.

Due to its regular, planar magnetic coils and continuous plasma current, tokamak equilibria are characterized by rotational symmetry (to good approximation) about the center axis of the torus (*axisymmetry*). Solutions to the MHD equilibrium force balance equation,

eq. (1.20), thus reduce to a two-dimensional equation in  $R$  and  $Z$  (as  $\partial/\partial\Phi \rightarrow 0$ ), given by the Grad-Shafranov Equation [13, 20, 21]:

$$\Delta^*\psi = -\mu_0 R^2 \frac{dp}{d\psi} - \frac{1}{2} \frac{dF^2}{d\psi} \quad (1.23)$$

where  $\Delta^*$  is a differential operator defined by

$$\Delta^* = R^2 \nabla \cdot \left( \frac{1}{R^2} \nabla \right) = R \frac{\partial}{\partial R} \left( \frac{1}{R} \frac{\partial}{\partial R} \right) + \frac{\partial^2}{\partial Z^2} \quad (1.24)$$

and  $F = RB_\phi$  encodes the toroidal field and  $p$  is the thermal pressure. The poloidal field (equivalently, the plasma current profile) is described by the poloidal magnetic flux  $\psi$ ,

$$\psi = \frac{1}{2\pi} \int \vec{B}_p \cdot d\vec{S} \quad (1.25)$$

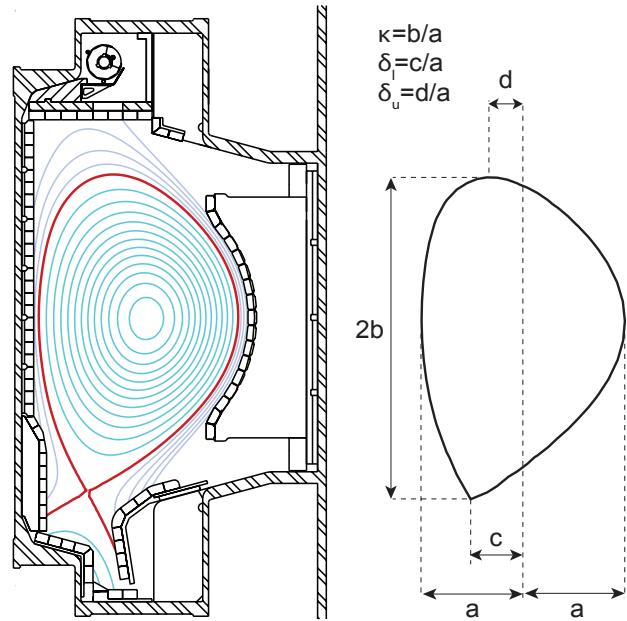
where  $\vec{S}$  is a surface with one edge along the magnetic axis. In eq. (1.23),  $\psi$  is treated as both an dependent parameter encoding the current, and as an independent variable – a consequence of Grad-Shafranov is that a number of parameters of interest, including pressure and current density, are *flux functions*, constant on a surface of constant  $\psi$ , and thus can be expressed as functions of  $\psi$  alone, e.g.  $p = p(\psi)$ . Moreover, magnetic field lines lie within surfaces of constant flux, with helical structure encoded by the flux function  $q(\psi)$ , termed the *safety factor*, given for a circular cross-section by

$$q = \frac{rB_\phi}{RB_\theta} \quad (1.26)$$

As the plasma temperature rapidly equilibrates along field lines, the temperature is also a flux function to good approximation. It is useful, then, to picture the confined plasma as a series of closed, nested surfaces of constant  $\psi$ , on which the plasma is frozen (see fig. 1.6). In practice, these contours are calculated via a numerical solution of eq. (1.23) by an equilibrium solver such as the EFIT code [22]. For flux functions (i.e., constant parameters on these flux surfaces), this explicitly removes the dependence on the poloidal angle  $\theta$  – the poloidal flux  $\psi$  is thus a useful one-dimensional abscissa derived directly from the magnetic geometry (thus independent of the physical scale of the tokamak and useful for cross-machine comparisons) for the profiles of most parameters of interest, and shall be used thus for the balance of this thesis.

Using outer poloidal field coils (shown in fig. 1.5), the tokamak operator may push the plasma into a non-circular shape, with beneficial

**Figure 1.6:** Cross-section of a plasma on the Alcator C-Mod tokamak, illustrating closed magnetic flux surfaces (light blue), the last closed flux surface (red), and surfaces with open magnetic field lines (dark blue). Definitions for plasma shaping parameters elongation  $\kappa$ , and upper and lower triangularity  $\delta_u$ ,  $\delta_l$  are shown at right.



effects on plasma performance and stability. In general, flux surfaces sufficiently far from the magnetic axis will intersect the plasma-facing wall before completing a closed loop; the magnetic boundary between closed, nested surfaces and these open surfaces is termed the *last closed flux surface* or LCFS. With sufficient shaping, the operator may generate a null point, the *X-point*, in the LCFS where the poloidal field is zero, splitting the LCFS (also called the *separatrix* in such configurations) into a minimally open surface with “legs” contacting the wall. This magnetic configuration is illustrated in fig. 1.6, along with a diagram defining the typical plasma shaping parameters: elongation  $\kappa$  and upper and lower triangularity  $\delta_u$ ,  $\delta_l$ . As the plasma diffuses outwards, it eventually crosses the LCFS and enters open flux surfaces in the *scrape-off layer* (SOL). The plasma then streams freely along these open magnetic field lines until it contacts the wall. By maintaining an X-point, the operator may steer this plasma exhaust into a section of the tokamak, the *divertor* [23, 24, 25], that is designed to handle this high heat flux and provide density control via pumping of recycled neutrals – necessary features to handle reactor-scale exhaust in a tokamak.

### 1.3 ALCATOR C-MOD

The data presented in this thesis were collected on the Alcator C-Mod tokamak [26, 27] at the MIT Plasma Science and Fusion Center. The Alcator tokamak experiments were designed as compact, high-field tokamaks. Despite its small physical size (0.67 m major radius, 0.22 m minor radius, considerably smaller than other major experiments), Al-



**Figure 1.7:** Cutaway view of the Alcator C-Mod tokamak, including cryostat and ancillary structures, illustrating the extensive support structures necessary for compact, high-field operation.



**Figure 1.8:** Cross-section of the C-Mod vacuum vessel, cryostat and diagnostic access ports, with toroidal-field and equilibrium-field magnetic coils labeled. Also shown is the plasma position in a typical LSN shape, with strike points in the lower divertor shown..

cator C-Mod plasmas are capable of approaching ITER- and reactor-relevant densities ( $> 1 \times 10^{20} \text{ m}^{-3}$ ) and pressures ( $> 1 \text{ atm}$ ).

This compact design is enabled by a very high toroidal magnetic field driven by liquid-Nitrogen-cooled copper coils, reaching as high as 8.1 T, with typical operation near 5.5 T, allowing reactor-relevant research in a small, cost-effective machine. C-Mod plasmas are primarily heated by RF heating in the ion-cyclotron range of frequencies (ICRF) [28], with up to 6 MW of heating power, with an additional  $\sim 1 \text{ MW}$  of lower-hybrid RF power used for heating and non-inductive current drive (LHCD) [29], providing exceptionally high power density in the  $\sim 1.1 \text{ m}^3$  plasma. A cutaway view of C-Mod, including support structures and the concrete “igloo” housing the cooling systems, is visible in fig. 1.7. A detailed and annotated view of the C-Mod cross-section is shown in fig. 1.8.

**Table 1.1:** Summary of Alcator C-Mod typical operating parameters.

parameter	range
major radius	0.67 m
minor radius	0.22 m
toroidal field	3 – 8.1 T
plasma current	$\leq 2 \text{ MA}$
plasma density	$\leq 5 \times 10^{20} \text{ m}^{-3}$
central temperature	$\leq 8 \text{ keV}$
plasma pressure	$\leq 2 \text{ atm}$
ICRF power	6 MW
LHCF power	1 MW

Due to their high plasma pressure and power density, C-Mod plasmas must exhaust a large heat flux, reaching levels comparable to that anticipated for ITER [30, 31, 32]. To handle this heat flux, C-Mod operates entirely with high-Z metal materials (primarily Molybdenum and Tungsten) for all plasma-facing surfaces. In addition to its high heat tolerance and low erosion rates due to plasma contact, metal walls provide relatively low retention of fuel gas at the edge – metal walls are thus the leading candidate for ITER- and reactor-scale plasma-facing components.

The presence of a full high-Z lower divertor and upper strike plate, as well as metal limiter walls, gives C-Mod great flexibility in attainable plasma shapes – plasmas may be run in a lower-single null (LSN) shape with the plasma exhaust striking the lower divertor (shown in fig. 1.8, upper-single null (USN) exhausting into the upper strike plate, or in a limited shape where the scrape-off layer directly impinges on the plasma-facing wall. •

## 1.4 CONFINEMENT & TRANSPORT

### 1.4.1 Global Confinement

The rate at which a fusion plasma “leaks” off heat is described by a characteristic time scale, the energy confinement time  $\tau_E$ . From basic power balance for the total plasma stored energy  $W_p$ ,

$$\frac{dW_p}{dt} = P_{in} - P_{out} = P_{tot} - \frac{W_p}{\tau_E} \quad (1.27)$$

where  $P_{in} = P_{tot}$  is the total input heating power, from Ohmic heating  $P_{Ohm} = I_p^2 R_{plasma}$ , RF or beam auxiliary heating power  $P_{aux}$ , or self-heating of the plasma from fusion reactions. In the case of the latter, note that as fusion neutrons are immediately lost from the plasma due to their lack of an electric charge, only the energy carried by *charged* fusion products contributes to fusion self-heating: in the case of D – T fusion we denote this as the alpha heating power  $P_\alpha = 1/5 \times P_{fusion}$  for the energy carried by the  ${}^4\text{He}$  nucleus. It is common to encapsulate these heat source and sink terms into a single “loss” power,

$$P_{loss} = P_{Ohm} + P_{aux} + P_{alpha} - \frac{dW_p}{dt} = P_{tot} - \frac{dW_p}{dt} \quad (1.28)$$

While  $P_{loss}$  is commonly used as a parameter of merit for confinement studies, it is also important to account for the radiated power  $P_{rad}$ , the heat loss due to radiative (primarily Bremsstrahlung) rather

than transport-driven effects encoded by  $W_p/\tau_E$ . This is expressed in the net power,

$$\begin{aligned} P_{\text{net}} &= P_{\text{Ohm}} + P_{\text{aux}} + P_{\text{fusion}} - P_{\text{rad}} - \frac{dW_p}{dt} \\ P_{\text{net}} &= P_{\text{loss}} - P_{\text{rad}} \end{aligned} \quad (1.29)$$

The radiative power loss is commonly difficult to consistently determine experimentally, and is only partially subject to operator control, as the radiation is due both to intrinsic impurities from plasma-facing materials and intentionally-introduced high-Z impurities for radiation control. As such,  $P_{\text{loss}}$  is by convention used for a simple relation for the experimental energy confinement time,

$$\tau_E = \frac{W_p}{P_{\text{loss}}} \quad (1.30)$$

Nevertheless an understanding of the radiated power is necessary for reactor operation. Radiated power from the core is deleterious to performance, driving decreased  $\tau_E$  at higher radiated-power fractions  $P_{\text{rad}}/P_{\text{tot}}$  [33]. Edge radiation, conversely, is essential for reactor operation to reduce the heat loads incident on the divertor, with edge radiated power fractions in excess of 50% predicted to be necessary for ITER [30]. In practice, the physics determining energy confinement are extremely complex; as such, working models for calculating  $\tau_E$  from bulk parameters typically require an empirical power-law scaling.

A closer examination of the power balance equation, eq. (1.27), reveals an important figure of merit. For a DT-burning fusion reactor, steady-state operation with plasma temperatures sustained by fusion self-heating (termed “ignition”) is highly desirable. At these conditions, the heating power is dominated by  $P_\alpha$ ; for steady-state operation ( $dW_p/dt \rightarrow 0$ ), eq. (1.27) reduces to

$$\frac{W_p}{\tau_E} = P_\alpha \quad (1.31)$$

The alpha heating power is simply the fusion reaction rate  $R_f = n_D n_T \langle \sigma v \rangle_{DT}$  times the energy carried by charged particles from a single reaction,  $E_\alpha = 1/5 \times E_{\text{fusion}} = 3.5 \text{ MeV}$ . Quasineutrality (eq. (1.2)) requires  $n_e \approx n_D + n_T$ . As the reaction rate is optimized for a 50-50 fuel mix, the alpha heating power density is given by

$$P_\alpha = \frac{1}{4} n_e^2 \langle \sigma v \rangle E_\alpha \quad (1.32)$$

The stored energy density is defined by

$$W_p = \frac{3}{2} p_{\text{thermal}} \quad (1.33)$$

with the thermal pressure in the plasma given by

$$p_{\text{thermal}} = n_e T_e + n_D T_D + n_T T_T = 2n_e T_e \quad (1.34)$$

assuming the condition above on the electron and ion densities, and assuming temperature equilibration  $T_e \approx T_D \approx T_T$ . This, then, implies  $W_p = 3n_e T_e$  (a convenient expression, as electron quantities are typically more readily measured in plasma experiments). Power balance at ignition then requires

$$\frac{3n_e T_e}{\tau_E} = \frac{1}{4} n_e^2 \langle \sigma v \rangle E_\alpha \quad (1.35)$$

thus simplifying to the Lawson Criterion [34]

$$n_e \tau_E = \frac{12 T_e}{\langle \sigma v \rangle E_\alpha} \quad (1.36)$$

Multiplying both sides by  $2T_e$  gives the “triple product,”

$$2n_e T_e \tau_E = p \tau_E = \frac{24 T_e^2}{\langle \sigma v \rangle E_\alpha} \quad (1.37)$$

an important figure of merit for a reactor, with a minimum value for ignition for D – T fusion at  $T_e \approx 15 \text{ keV}$  with a value of  $p \tau_E \approx 8.3 \text{ atm} \cdot \text{s}$  [15].

However, the maximum attainable thermal pressure in a tokamak is limited by a global MHD stability limit expressed in terms of [7, § 6.16]

$$\beta = \frac{2\mu_0 p}{B^2} \quad (1.38)$$

the ratio of thermal pressure to magnetic pressure  $B^2/2\mu_0$  (equivalently, the ratio of thermal and magnetic stored energy) – a normalization that also falls naturally out of solutions to the MHD equilibrium, eq. (1.20). Thus for a given  $B_T$  (which is by far the largest contribution to magnetic pressure in a tokamak), set by design and operational limits, there is a maximum obtainable pressure, setting a lower bound on the necessary energy confinement to reach the triple-product target for ignition.

### 1.4.2 Transport Barriers

Global improvement to energy confinement may be achieved through local modification of the transport of energy or particles out of the plasma, achieved via regions termed *transport barriers*. While the physics driving the formation of transport barriers is not entirely understood, the effect is evidently caused by sheared flows in the plasma – these break up the turbulent “eddies” driving much of the energy or particle transport through the plasma, locally reducing transport drive in the sheared region.

The effect on the transport is clearly evident from a diffusive transport model, given by

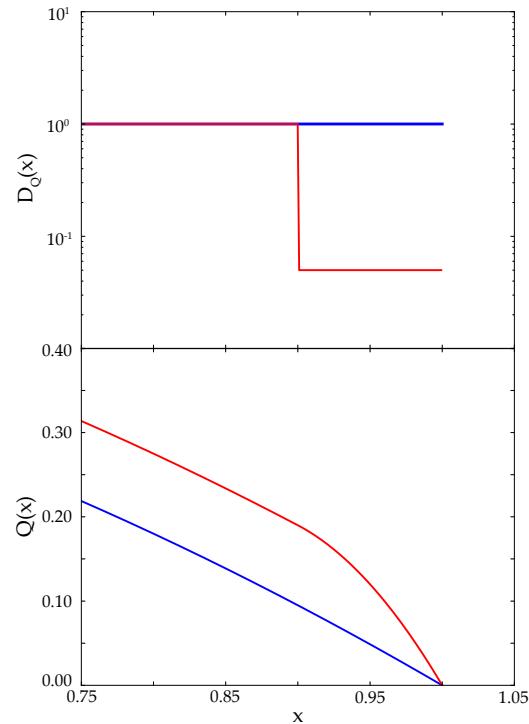
$$\frac{\partial Q}{\partial t} = \nabla \cdot (D_Q \nabla Q) + R_Q \quad (1.39)$$

for a general parameter  $Q(\vec{x}, t)$  with accompanying diffusion coefficient  $D_Q(Q, \vec{x}, t)$  and net source/sink term  $R_Q(Q, \vec{x}, t)$ . We may consider a one-dimensional “toy model” of diffusion with a simple constant source term, given in steady state by

$$\frac{d}{dx} \left( D_Q \frac{dQ}{dx} \right) + R_Q = 0 \quad (1.40)$$

The solution to this model for two sample diffusion coefficients is given in fig. 1.9. A simple constant diffusion coefficient  $D_Q$  produces a profile with weak slope, whereas an order-of-magnitude drop in  $D_Q$  near the edge (consistent with experimentally-observed values of diffusion coefficients in transport barriers) produces a region with a steep gradient in  $Q$  compared to the flat- $D_Q$  solution, despite identical source terms  $R_Q$ . Experimentally, reductions in the particle transport coefficient  $D_n$  or the heat transport coefficient  $\chi$  due to sheared flows correspond to steep-gradient regions in density or temperature, characteristic of the transport barrier.

Of particular interest is the *edge transport barrier*, also termed the *pedestal* [33, 35]. A number of high-performance tokamak regimes have been established, exploiting the formation of a pedestal to suppress transport and boost global energy confinement to levels necessary to reach the triple-product tar-



**Figure 1.9:** Diffusion coefficients and plasma profiles for a “toy model” 1D diffusion equation with a general parameter  $Q(x)$  and accompanying diffusion coefficient  $D_Q(x)$ , with constant  $D_Q$  shown in blue and  $D_Q$  reduced by a transport barrier shown in red.

get (eq. (1.37)) for an ignited plasma. The understanding of these high-performance regimes, commonly referred to as “high-confinement” or H-modes, and their extrapolation to ITER and reactor-scale devices has been a major focus of recent tokamak research.

However, the formation of the pedestal also presents challenges that must be addressed for reactor-scale operation. Increased particle confinement causes the plasma to retain impurities – particularly ionized wall materials – along with fuel ions. Low-Z impurities, particularly the  $^4\text{He}$  “fusion ash”, will slow the fusion reaction rate due to fuel dilution, while high-Z impurities drive elevated radiative losses (note the strong charge dependence for Bremsstrahlung radiation, eq. (1.6)). This ultimately leads to a *radiative collapse* [27, 33], dropping the plasma out of H-mode – thus, stationary (i. e., non-transient) operation in H-mode requires a means to regulate particle confinement and flush impurities from the plasma core.

The steep gradient in the plasma pressure generated in the pedestal has been shown to drive *Edge-Localized Modes* (ELMs) [36], instabilities that cause the pedestal and its associated steep radial gradients to periodically “crash,” expelling particles and energy into the scrape-off layer. The ELM bursts found in existing experiments provide the desired level of particle transport for stationary operation – thus ITER operation is designed considering an H-mode with ELMs as the baseline for operation [37, 38]. However, on ITER-scale devices, which will have a significantly higher ratio of thermal energy to surface area for heat exhaust compared to existing devices, the heat pulses from ELMs drive unacceptable levels of transient thermal loading and erosion damage to wall and divertor materials [39, 40]. As such, high-performance operation on ITER- or reactor-scale devices requires mitigation or elimination of large, deleterious ELMs, either through externally-applied controls or physics-based stabilization. •

## 1.5 GOALS & OUTLINE

This thesis will present results in the *I-mode*, a novel high-performance regime pioneered on Alcator C-Mod [41]. I-mode is notable for its apparent decoupling of energy and particle transport, reaching H-mode-like energy confinement while maintaining L-mode levels of particle and impurity transport, achieving the desired flushing of impurities from the plasma. This is manifested in the edge with the formation of an H-mode-like temperature pedestal without the accompanying density pedestal found in conventional H-modes. I-mode also appears to be naturally free of large ELMs, avoiding the need for complex externally-applied controls, and to exhibit highly favorable scalings of energy confinement with heating power.

A firm understanding of the structure and stability of the pedestal is essential to extend I-mode operation to larger devices. This the-

sis will describe a combined approach to the understanding of the pedestal in I-mode, using both direct observations of pedestal structure and numerical modeling of the pedestal stability against MHD triggers for large, deleterious ELMs. The applicability of I-mode to reactor operation can thereby be evaluated. The balance of this thesis is arranged as follows:

#### **CHAPTER 2: HIGH-PERFORMANCE REGIMES**

An overview of existing results in established H-mode regimes, including observed pedestal behaviors. A detailed introduction to I-mode physics and operation is also included.

#### **CHAPTER 3: PEDESTAL MODELING AND THEORY**

An introduction to the theory of the MHD and turbulent instabilities governing the pedestal and driving large ELMs, and the numerical modeling approaches used in their analysis, as well as an overview of alternate models.

#### **CHAPTER 4: ELMY H-MODES ON C-MOD**

The results of recent experiments on C-Mod testing a unified model for pedestal structure in ELMy H-mode, the approach to which is also applied to I-mode pedestals.

#### **CHAPTER 5: I-MODE PEDESTAL SCALINGS & CONFINEMENT**

New results from dedicated pedestal experiments in I-mode examining the response of pedestal structure to engineering and physics parameters, and potential extrapolations of pedestal structure and performance to larger devices. The impact on global performance and confinement is also shown.

#### **CHAPTER 6: I-MODE PEDESTAL STABILITY MODELING**

Numerical modeling results for the stability of I-mode pedestals against identified ELM triggers, and correlations to the generally observed lack of ELMs in I-mode.

#### **CHAPTER 7: CONCLUSIONS & FUTURE WORK**

A summary of the results presented in this thesis and some directions for future work.

An overview of the diagnostics used in the experiments presented here is also given in appendix A. A summary of the pedestal database used in these experiments is given in appendix B. \*



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# 2

## HIGH-PERFORMANCE REGIMES

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The development of magnetic-confinement fusion into an economical form of power generation is characterized by two seemingly contrary requirements: first, a high level of energy confinement is necessary to reach the desired level of self-heating of the plasma by fusion products, satisfying triple-product requirements (eq. (1.37)). At the same time, particle transport must be sufficient to avoid the deleterious effects of accumulated helium “fusion ash” and other impurities on fusion performance – particularly important in the case of the high-Z impurities from the metal plasma-facing walls necessary for reactor-scale devices [1, 2, 3].

A number of operating scenarios, collectively termed “high confinement” or H-modes[4, 5], satisfying these requirements have been developed. The “low confinement” or L-mode operating baseline of energy confinement is characterized through an extensive multi-machine scaling study [6] by the ITER-89 scaling,

$$\tau_{E,ITER89} = 0.048 \times \bar{n}_e^{0.1} M^{0.5} I_p^{0.85} R^{1.2} a^{0.3} \kappa^{0.5} B_T^{0.2} P_{aux}^{-0.5} \quad (2.1)$$

in which  $\bar{n}_e$  is the line-averaged density ( $10^{20} \text{ m}^{-3}$ ),  $M$  is the atomic mass (amu),  $I_p$  is the plasma current (MA),  $B_T$  is the toroidal field (T),  $R$  and  $a$  are the major and minor radii in m (see fig. 1.4),  $\kappa$  is the elongation (see fig. 1.6), and  $P_{aux}$  is the externally-applied heating power (MW). Compared to this baseline, H-modes represent a significant improvement in performance, with confinement – here represented in a normalized sense by the H-factor, i.e.,

$$H_{89} = \frac{\tau_E}{\tau_{E,ITER89}} \quad (2.2)$$

improved by roughly a factor of two compared to L-mode [7].

This improvement in confinement is due to the formation of a *pedestal*, a transport barrier (see section 1.4.2) in the outermost 5-10% of the plasma that greatly slows the transport of particles and/or energy out of the plasma, and accordingly forms a steep-gradient region in density and/or temperature at the edge. Pedestal formation is achieved through strongly sheared flows in the plasma edge, driven in part by a radial electric field (the “ $E_r$  well”) and the resulting  $\vec{E} \times \vec{B}$  flow shear in the pedestal. While this flow is difficult to model due to the short scale lengths inherent to the pedestal [8, 9], the role of edge  $E_r$  and flows has been extensively studied both from an experi-

mental [10, 11, 12, 13] and a theoretical [14, 15, 16, 17, 18] standpoint, as has the role of other edge fluctuations coupling into these flows in driving the transition into H-mode [19]. As the pedestal structure is known to set a strong constraint on the overall performance in high-confinement regimes [20], as well as determining the edge stability and heat exhaust properties of the regime, a firm understanding of the pedestal is essential for extrapolation of a high-performance regime to ITER and beyond.

This chapter provides an overview and comparison of different classes of established H-mode operation, particularly regarding their behaviors in the high energy confinement and low particle confinement required for a reactor. Additionally, observations of Edge-Localized Modes (ELMs) [21] are addressed. We then introduce the access conditions, operation, and global characteristics of *I-mode* – an alternate high-performance regime with a number of favorable characteristics for reactor operation, and the subject of the majority of this thesis.

**Table 2.1:** Typical operating parameters of tokamaks noted in this thesis, along with references to overviews of each machine. *Note:* all ITER values are projected.

Device	R/a [m]	I <sub>p</sub> [MA]	B <sub>T</sub> [T]	$\bar{n}_e$ [ $10^{19} \text{ m}^{-3}$ ]	T <sub>i0</sub> [keV]	refs.
C-Mod (USA)	0.67/0.22	$\leq 2$	3 – 8.1	$\leq 50$	$\leq 8$	[22, 23, 24]
DIII-D (USA)	1.67/0.67	1 – 3	2.2	6	5 – 10	[25, 26, 27]
ASDEX-U (GER)	1.65/0.5	$\sim 1$	3.9	7.5	2 – 3	[28, 29, 30]
JET (UK)	3.4/0.9	3 – 4	3.8	5	10 – 20	[31, 32]
JT-60U (JAP)	3.4/0.9	3 – 4	4.0	5	10 – 20	[33, 34]
JFT-2M (JAP)	1.3/0.35	0.5	2.2	5	1 – 2	[35, 36]
ITER*	6.2/2.0	15	5.3	$\leq 10$	10 – 20	[37, 38, 39]

## 2.1 ELMY H-MODE

### 2.1.1 ELMy H-Mode Operation

The first H-modes, observed in high-power experiments on ASDEX [4, 5], exhibited a prompt decrease by roughly a factor of two in both particle and energy transport [4]. The H-mode transition is marked by high edge temperatures and strong gradients – the first H-modes were observed in divertor experiments on ASDEX, as the diverted configuration allows higher edge temperatures than are attainable in limited plasmas [5]. Unlike ELM-free H-modes, however, the confinement is periodically degraded by *Edge-Localized Modes* (ELMs), intermittent “crashes” in the pedestal expelling particles and energy into the SOL, with repetition rates ranging from a few ELM cycles per second to over 100 Hz, which drives sufficient particle transport

**Figure 2.1:** Characteristic traces of a steady ELMy H-mode on Alcator C-Mod (section 2.1). Density and radiated power rise after the L-H transition, but stabilize as the periodic relaxation of the pedestal regulates and flushes impurities from the plasma. ELM bursts are visible as spikes on the edge  $D_\alpha$  signal.



**Figure 2.2:** ELMy H-mode pedestals from pedestal similarity experiments on Alcator C-Mod and DIII-D. Pedestal densities and temperatures are shown normalized to poloidal field (which accounts for differences in plasma current) such that hyperbolae in the parameter space are curves of constant poloidal beta. ELMy H-mode pedestals are, to lowest order, constrained to a curve of fixed  $\beta_{p,\text{ped}}$ .



to flush impurities from the plasma and allow stationary operation [5, 21]. The ELMY H-mode forms a strong pedestal in both density and temperature – due to profile stiffness in the core (consistent with a critical-gradient model for core transport), the pedestal supports high temperatures and pressures and good global performance [7, 40, 41]. Moreover, the ELMY H-mode is readily attainable on all major tokamak experiments at a broad range of collisionalities and operating densities, although ELMY H-modes on C-Mod require an atypical shape [42, 43]. Here we define the collisionality (normalized collision frequency) by [44],

$$\begin{aligned} \nu^* &= \frac{\nu_{\text{eff}}}{\nu_{\text{bounce}}} = \frac{qR\nu_{ei}}{\varepsilon^{3/2}\nu_{Th,e}} \\ &= (6.921 \times 10^{-18}) \frac{Rqn_e Z_{\text{eff}} \ln \Lambda_e}{\varepsilon^{3/2} T_e^2} \end{aligned} \quad (2.3)$$

with electron density  $n_e$  in  $\text{m}^{-3}$  and temperature in eV, major radius  $R$  in m, and with the Coulomb logarithm defined by  $\ln \Lambda_e = 24 - \ln(\sqrt{n_e}/T_e)$ . Typically the pedestal collisionality is calculated by evaluating  $n_e$ ,  $T_e$ , and  $q$  at the 95% flux surface. The operating density range is expressed in terms of the Greenwald density limit [45],

$$n_{Gr} = \frac{I_p}{\pi a^2} \quad f_{Gr} = \frac{\bar{n}_e}{n_{Gr}} \quad (2.4)$$

with  $I_p$  in MA and  $a$  in m yielding density in  $10^{20} \text{ m}^{-3}$ . ELMY H-mode operation is possible with Greenwald fractions ranging from  $f_{Gr} \sim 0.3 - 1.0$ , although confinement degrades as  $f_{Gr}$  approaches unity [2, 46]. As such, the ELMY H-mode is considered the baseline for ITER operation [37, 38]. Analysis of a multi-machine database [47] led to the development of the ITER98y2 H-mode confinement scaling [38],

$$\tau_{ITER98y2} = 0.0562 \times \bar{n}_e^{0.41} M^{0.19} I_p^{0.93} R^{1.39} a^{0.58} \kappa^{0.78} B_T^{0.15} P_{loss}^{-0.69} \quad (2.5)$$

$$H_{98} = \frac{\tau_E}{\tau_{E,ITER98y2}} \quad (2.6)$$

in which  $\bar{n}_e$  is the line-averaged density ( $10^{19} \text{ m}^{-3}$ ),  $M$  is the atomic mass (amu),  $I_p$  is the plasma current (MA),  $B_T$  is the toroidal field (T),  $R$  and  $a$  are the major and minor radii in m (see fig. 1.4),  $\kappa$  is the elongation (see fig. 1.6), and  $P_{loss}$  is the heating power defined in eq. (1.28) (MW). Recall from eq. (1.30) that the stored energy  $W$  trends as  $\sim P\tau_E$  – degradation in  $\tau_E$  with heating power leads to

diminishing returns in stored energy and global performance with increased heating power.

Due to the importance of pedestal structure on overall performance [20], a number of models for the pedestal width and height in ELMY H-mode have been proposed. The ELMY H-mode pedestal has been observed to be limited in pressure gradient [48, 49] – as the pedestal width on a given machine typically varies only over a small range [41, 50], this constitutes (to lowest order approximation) a limit on the attainable pedestal height. Models based on the poloidal gyroradius limits, and their expected effects on the growth rates of turbulent modes compared to the  $\vec{E} \times \vec{B}$  shearing rate, have been proposed [51, 52]. However, this has been discounted in favor of a model based on poloidal beta limits (see fig. 2.2),  $\beta_p = 2\mu_0 p / B_p^2$ , both by experiments varying density and temperature at fixed  $p_{ped}$  [53] and by isotope-mass-difference experiments [54] (both of which vary the gyroradius without varying  $\beta_{p,ped}$ ). These models are described in more detail in section 3.1.

On existing machines, ELMs provide sufficient impurity transport to allow stationary operation without seriously impacting energy confinement [55]. However, the time-averaged power load from the ELM heat pulse is consistently observed to be 20 – 30% of the input heating power [56, 57], resulting in ELM energy losses reaching 2 – 6% of the total stored energy – on ITER, this results in heat pulses as high as 20 MJ reaching the divertor plate, or transient heat loads of  $\sim 1 - 10 \text{ GW} \cdot \text{m}^{-2}$  (compared to the steady heat loading of  $\sim 5 - 10 \text{ MW} \cdot \text{m}^{-2}$ ) [58, 59]. As wall materials on ITER will be generally limited to ELM heat loads of  $\sim 10 \text{ MJ}$  per ELM [58], uncontrolled large ELM pulses can seriously exceed tolerances for ITER plasma-facing wall and divertor materials [58, 59]. Thus, avoiding or mitigating large, deleterious ELMs is essential for ITER operation.

### 2.1.2 Edge-Localized Modes & Pedestal Limits

Early phenomenological experiments on DIII-D and ASDEX [21, 40, 48] classified ELMs into three broad categories:

#### TYPE-I

Large, discrete ELMs. ELM frequency  $f_{ELM}$  rises with increasing heating power. The ELM crash is preceded by broadband electromagnetic and density fluctuations. Type-I ELMy pedestals are modeled to be at or near the ballooning stability boundary (described below).

#### TYPE-II

Smaller and faster than type-I, often termed “grassy ELMs.” No discernable  $f_{ELM}$  dependence on heating power. Found in

strongly shaped plasmas between the first and second-stable regions for ballooning MHD.

#### TYPE-III

Small ELMs,  $f_{\text{ELM}}$  decreases with increasing heating power. Exhibit a coherent magnetic precursor fluctuation before the ELM crash. Found only below a threshold pedestal temperature, typically at levels of heating power just above the L-H threshold, given by [60] (where  $\bar{n}_e$  is in  $10^{20} \text{ m}^{-3}$ ,  $B_T$  in T, and  $S$  is the plasma surface area in  $\text{m}^2$ ):

$$\begin{aligned} P_{\text{thres}} &= 0.0488 \times \bar{n}_e^{0.717} B_T^{0.803} S^{0.941} \\ S &= (2\pi)^2 a R \sqrt{\kappa} \end{aligned} \quad (2.7)$$

Early investigation of the ELMy pedestal, particularly in large type-I ELMs, associated the pedestal limit with a “ballooning” MHD instability – these MHD modes are driven unstable by strong pressure gradients in the edge, expressed in terms of the parameter  $\alpha_{\text{MHD}}$  for a general toroidal equilibrium [61],

$$\alpha_{\text{MHD}} = -\frac{2}{(2\pi)^2} \frac{\partial V}{\partial \Psi} \sqrt{\frac{V}{2\pi^2 R}} \mu_0 \frac{dp}{d\Psi} \quad (2.8)$$

This reduces to a more intuitive form for a cylindrical plasma [62],

$$\alpha_{\text{MHD}} = -\frac{2Rq^2}{B_T^2} \nabla p \quad (2.9)$$

with the  $q^2/B_T^2$  factor effectively expressing the scaling as  $\alpha_{\text{MHD}} \sim \nabla p/B_p^2$ . Type-I ELMy H-mode pedestals are typically found to be near a critical value for  $\alpha_{\text{MHD}}$  dependent on the plasma shape [53] – stronger shaping is associated with slower ELM frequencies and greater stabilization of type-I ELMs, consistent with ballooning MHD [21, 46, 49]. Due to the restricted width range for the pedestal on a given machine [41, 50], the  $\alpha_{\text{MHD}}$  limit reduces, to good approximation, to a limit on  $\beta_p$  at the pedestal top [46, 49]. For example, points at matched shaping and current across a DIII-D/C-Mod similarity experiment, shown in fig. 2.2, lie on a fixed  $n_e T_e$  line. The transition from type-I to type-III ELMs with increasing density and decreasing temperature [46], or alternately the transition from type-III ELMs just above the L-H transition to type-I ELMs with increasing heating power [48], is consistent with the transition from a resistive mode for type-III ELMs to the ideal MHD modes identified with type-I ELMs.

A simple ballooning MHD analysis, however, does not accurately capture the ELMy H-mode pedestal – parallel observations of MHD

stability in early ELMy H-modes also identified current-driven kink/peeling modes as a potential limiting instability, particularly at low collisionality [40, 48, 51]. This is particularly true in light of the *bootstrap current*, an effect by which gradients in the plasma self-generate an electric current, given by [44]

$$j_{\text{boot}} = I(\psi)p_e(\psi) \left[ \alpha \frac{dn_e}{d\psi} + \beta \frac{dT_e}{d\psi} + \gamma \frac{dT_i}{d\psi} \right] \quad (2.10)$$

where  $I(\psi) = RB_\phi$  is a flux function encoding the field,  $p_e(\psi)$  is the electron pressure, and  $\alpha$ ,  $\beta$ , and  $\gamma$  are coefficients determined by the collisionality and trapped-particle fraction, ordered  $\alpha > \beta > \gamma$ . Due to the strong density and temperature gradients in the pedestal, the local current density may be large enough for current-driven kink/peeling modes to be a concern.

MHD models built on coupled peeling and ballooning MHD modes, as well as diamagnetic effects stabilizing ballooning modes with high toroidal mode number  $n$  [40], have been developed [63, 64] and successfully capture the MHD limits of the ELMy H-mode. Moreover, turbulence studies based on the kinetic ballooning mode (KBM) [65] predict that the KBM will limit the pressure gradient and width such that the pedestal width defined in poloidal flux space scales with  $\beta_{p,\text{ped}}^{1/2}$  in a manner consistent with experimental observations,  $\Delta_{\text{ped}} \sim \beta_{p,\text{ped}}^{1/2}$  [66]. Turbulent fluctuations with an onset soon after the inter-ELM pressure pedestal gradient saturation have been observed [67], but a definitive analysis is still ongoing. A self-consistent model including both the MHD and turbulent constraints, EPED [68], has been implemented and tested in multi-machine analyses [69], including on DIII-D [70], C-Mod [71], and KSTAR [72]. The constraints of this model are discussed in detail in chapter 3.

### 2.1.3 Active ELM Control

In light of the potential deleterious effects of large ELMs on ITER-scale devices [58, 59], mitigating or preventing large type-I ELMs in H-mode is of prime concern. One engineering solution for active ELM control is the application of a *resonant magnetic perturbation* (RMP) [73, 74, 75]. Small perturbations (less than 1/1000 the magnitude of the background magnetic field), for example those driven by an  $n = 3$  coil set on DIII-D [73] or a variable  $n = 3, 4, 6$  set on MAST [76], are sufficient to completely suppress ELMs, as on DIII-D and ASDEX Upgrade, or mitigate them, as on MAST [76]. The physics mechanism underlying the RMP is unclear; it is proposed by Snyder *et al.* [70] that stochastic magnetic islands in the pedestal limit the inward growth of the pedestal such that the MHD stability boundary is not reached. In cases of ELM mitigation, Chapman *et al.* [77] propose that

modification of the edge rotation shear or 3D effects destabilize the ELM before reaching conditions for a large, deleterious ELM event. Due to its resonant nature, the RMP effect is strongly sensitive to the edge safety factor  $q$ , limiting the potential profiles possible for RMP ELM control [74].

Rather than attempting to eliminate the ELM instability, it is also possible to “smooth out” the ELM heat pulse using pellet pacing [78]. Generally, the transient ELM power  $P_{\text{ELM}} \sim f_{\text{ELM}} \Delta W_{\text{ELM}}$  is roughly fixed - thus smaller, faster ELMs expel the less energy per ELM for the same average power. By triggering smaller, faster ELMs the heat load can be smoothed to a level closer to steady-state heat loads tolerable to divertor materials, rather than large transient heat pulses. In pellet pacing, the sharp density increase locally introduced in the pedestal by the pellet triggers a high- $n$  ballooning mode, resulting in a small ELM. Experiments, e.g., on DIII-D [78], ASDEX Upgrade [79], and JET [80], including with the ITER-like metal wall [81], have demonstrated suitable ELM mitigation through pellet pacing. However, the feasibility of pellet pacing on ITER, as well as the potential for non-axisymmetric heat loading in the divertor due to the localized nature of the pellet perturbation, remain open questions.

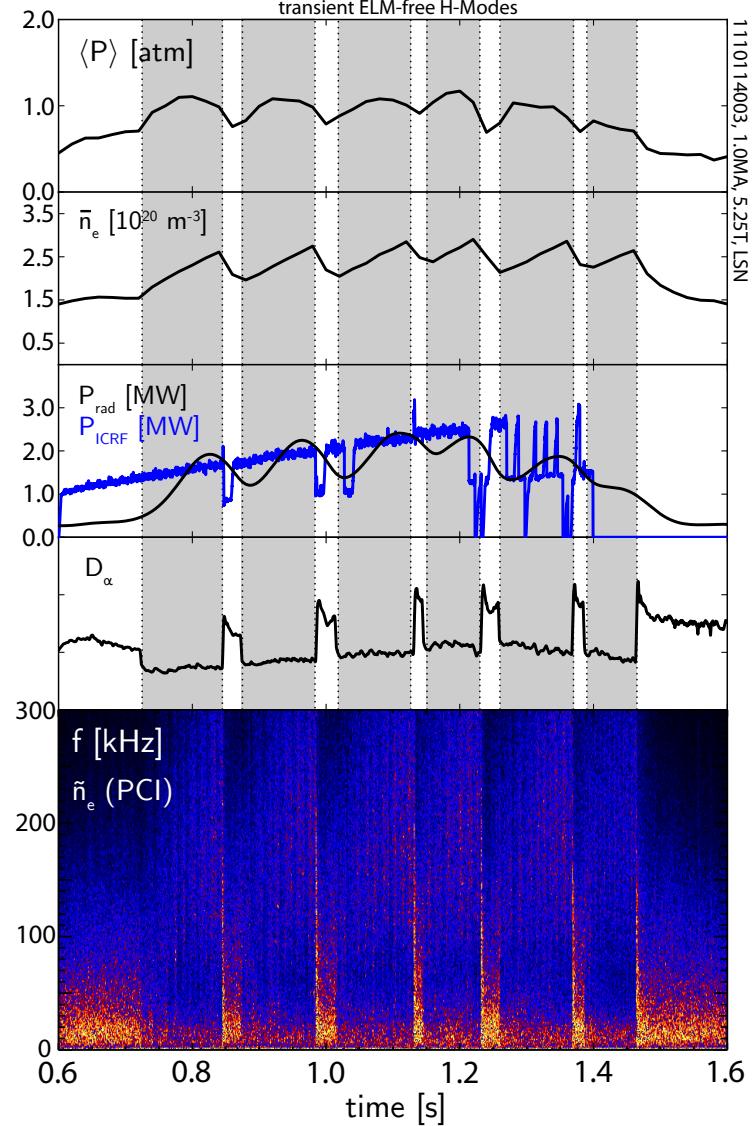
#### 2.1.4 Prospects for ELMy H-Mode

Though ELMy H-mode represents the most readily attainable high-performance regime, its applicability to ITER-scale devices hinges on the limitation, mitigation, or elimination of large ELMs and the associated heat loads on wall and divertor surfaces. ELM losses from type-I ELMs tend to be smaller for a given  $\beta_{p,\text{ped}}$  at higher density and lower temperature, ultimately transitioning to type-III ELMs [49], however these plasmas tend to exhibit lower global confinement [46]. Type-II ELMs may provide the necessary near-continuous heat exhaust, but access to the regime is narrow and highly sensitive to shaping [56]. Alternately, ELM heat loading in type-I regimes may be controlled or suppressed via engineering solutions (i.e., RMP or pellet pacing) – but these are similarly limited in availability, and are of uncertain extrapolation to ITER-scale devices and beyond. Thus, recent efforts have also placed great emphasis on high-performance regimes that are naturally free of large ELMs. •

## 2.2 ELM-FREE H-MODE

Under a broad range of conditions, the plasma may enter a transient *ELM-free H-mode*, in which an H-mode forms without exhibiting large edge-localized modes (ELMs) [21, 82]. ELM-free H-modes exhibit high levels of both energy and particle confinement ( $H_{89} \sim 2$ ), resulting in strong density and temperature pedestals [83, 84]. The

**Figure 2.3:** Characteristic traces of transient ELM-free H-modes, highlighted on the traces (section 2.2). After the L-H transition, density and thermal pressure (and therefore fusion reaction rate and stored energy) rise, while turbulent particle transport is reduced, as seen by the drop in edge  $D_\alpha$  light and suppression of turbulence (shown in the density fluctuations). However, radiated power rises due to impurity accumulation – when radiated power reaches a level comparable to total heating power, the plasma drops back into L-mode.



plasma stored energy, global pressure, and density rise monotonically after the L-H transition (shown in fig. 2.3), as does the edge pressure gradient [85]. This, however, is unsustainable – the increased particle confinement causes impurities to accumulate in the plasma, increasing the power lost to radiative effects. Above  $P_{\text{rad}}/P_{\text{in}} \sim 0.5$  confinement degrades due to cooling at the edge, and the H-mode terminates as the radiated power approaches the total heating power, an event termed the “radiative collapse” [7].

As a result, the ELM-free H-mode is an inherently transient state for the plasma – the excessive particle confinement and resulting radiative losses tend to drop the plasma back into L-mode although under certain conditions the edge pressure gradient may grow sufficiently to reach the stability boundary, terminating the H-mode with a single giant ELM [85]. As an H-L back-transition can release energy and particles on a scale in excess of even large type-I ELMs,

these transient states must be avoided similarly to uncontrolled ELMy H-modes. Moreover, the lack of a stationary “target” plasma makes achieving non-inductive current drive solutions quite difficult. This demonstrates the necessity of some form of regulation of the particle confinement in high-performance regimes to control and flush impurities from the plasma, allowing stationary operation without reaching an ELMing limit. •

### 2.3 ELM-SUPPRESSED H-MODES

In addition to H-modes exhibiting ELMs, classes of H-mode have been established capable of stationary operation with acceptable levels of particle transport (avoiding the radiative collapse and subsequent transient nature found in classical ELM-free H-modes) without exhibiting the bursty heat and particle transport driven by ELMs. Rather, the pedestal is regulated by a continuous fluctuation localized in the pedestal. The characteristics of two, the Quiescent H-mode (QH-mode) and Enhanced D<sub>α</sub> (EDA) H-mode, are presented here.

#### 2.3.1 QH-Mode

The *Quiescent H-mode* (QH-mode) was first observed on DIII-D [86, 87], and subsequently achieved on ASDEX Upgrade [88], JT-60U [89], and JET [90]. In QH-mode operation, following a brief ELM-free or ELMing phase after the L-H transition, the plasma enters a state with steady averaged density and radiated power, indicating a lack of serious impurity accumulation, despite lacking ELM-mediated transport (evident from divertor D<sub>α</sub> light, which is “quiescent” compared to the characteristic spikes driven by ELMs). Although QH-mode requires lower densities (average density reduced by roughly a factor of two from comparable ELMy H-modes) with cryopumping for density control, access is otherwise robust, with successful operation across a broad range of shaping, safety factor, current and field [86]. The regime is capable of stationary operation, with the mode sustained for most of the current flat-top on DIII-D ( $\sim 25\tau_E$ ) with very good confinement – in cases with an internal transport barrier in addition to the pedestal (termed the “Quiescent Double Barrier” or QDB regime [91, 92, 93]) a confinement metric of  $\beta_N H_{89} \sim 7$  was reached (albeit for a briefer period,  $\sim 5\tau_E$ ), compared to  $\beta_N H_{89} > 4$  found in ELMy H-modes on DIII-D [92]. Here we use the normalized pressure metric [94]

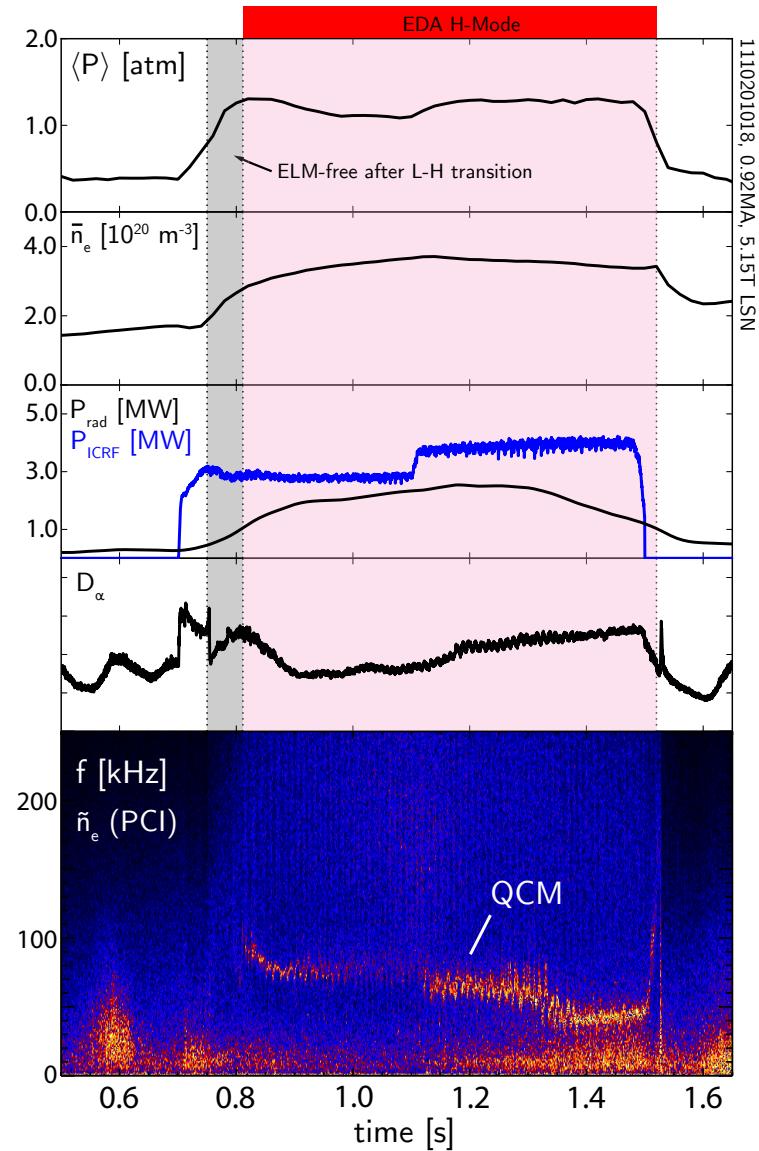
$$\beta_N = \beta \frac{a B_T}{I_p} \quad (2.11)$$

in  $\text{m} \cdot \text{T} \cdot \text{MA}^{-1}$ . Similarly competitive confinement between QH-mode and ELMy H-mode is seen on ASDEX Upgrade and JET, although the mode on JT-60U is out-performed by ELMy H-mode [95]. The pedestal density is reduced (comparable to the reduction in globally-averaged density) in QH-mode compared to ELMy H-mode, and excess fueling to the edge by gas puffing, pellet fueling, or wall outgassing destroys the QH-mode. However, pedestal temperatures are typically somewhat higher [92], thus the mode is found at ITER-relevant low collisionalities. Pedestal pressure gradients are comparable to those found in ELMy H-mode [86]. A particularly strong  $E_r$  well (2 – 3 times deeper than in comparable ELMy H-modes) is also observed in the QH-mode pedestal [93].

In place of bursty ELM transport, the pedestal in QH-mode is continuously regulated by the *Edge Harmonic Oscillation* (EHO), an MHD mode observed in density, temperature, and magnetic fluctuations [86]. The EHO is made up of distinct harmonics with toroidal mode numbers  $n \sim 1 - 10$ ; these harmonics are directly observed in the particle flux at the divertor, indicating that the EHO is responsible for density regulation in QH-mode [92]. MHD modeling approaches similar to those described in chapter 3 indicate that the EHO is a saturated peeling mode [70, 96, 97]. This is consistent with the low pedestal collisionality in the QH-mode pedestal (lower collisionalities and higher bootstrap currents tends to drive the pedestal towards the peeling side of the peeling-balloonning MHD boundary, as described in chapter 3), and with the observed localization of the EHO in the region of strongest  $E_r$  and rotation shear [91]. The saturated mode is driven by the strong rotation shear in the edge – while this typically destabilizes low- $n$  MHD modes, in the case of the EHO the magnetic component of the mode couples to the vacuum-vessel wall as the rotation spins up, providing the drag force necessary to saturate the mode at finite amplitude [98]. This prevents a rapidly-growing edge instability, thus providing the ELM suppression in QH-mode [70].

Historically, QH-mode operation has required significant neutral-beam inputs directed counter to the plasma current direction, providing the necessary rotation [86]. However, counter-current beam operation drives significant fast-ion losses into the outer wall, necessitating operation with a large outer gap to avoid wall outgassing. More recent experiments have successfully sustained QH-modes with co-current beam injection (although counter-current beams were still required for mode access) [98] and with torque from non-axisymmetric magnetic fields [99, 100]. The latter is of particular importance, as it is not expected that the NBI systems on ITER will drive sufficient torque to produce QH-mode [99]. In addition to the requirement for externally-supplied torque to maintain the mode, QH-mode suffers from accumulation of high-Z impurities – while lower-Z ions are flushed from the plasma by the EHO, high-Z impurities tend to accu-

**Figure 2.4:** Characteristic traces of an EDA H-mode on C-Mod (section 2.3.2). Following a brief ELM-free phase, the plasma density and radiated power stabilizes at a sustainable level. The edge transport barrier is regulated by the continuous QCM fluctuation at  $\sim 60 - 70$  kHz (shown in density fluctuations in the bottom panel) rather than bursty ELM transport.



mulate in the core [90, 92], which may present difficulties attaining QH-mode on metal-walled machines where high-Z impurities dominate. Nevertheless QH-mode is a potentially attractive option for a reactor regime, provided high-density operation with sufficient high-Z impurity control is attainable.

### 2.3.2 EDA H-Mode

The *Enhanced D<sub>α</sub> H-mode* (EDA H-mode) is a high-performance regime discovered and explored on the Alcator C-Mod tokamak [101, 102, 103]. Along with transient ELM-free H-modes, the EDA regime is the customary approach to H-mode operation on C-Mod, unlike other major tokamak experiments; the Type-I ELMMy H-mode commonly found on other devices requires an atypical shaping to more easily

reach the stability boundary associated with the ELM trigger on C-Mod [43]. In EDA operation, the L-H transition is followed by a rise in radiated power and density similar to an ELM-free H-mode. However, shortly thereafter the H-mode stabilizes at steady density [101], with the radiated power held at  $P_{\text{rad}}/P_{\text{in}} \sim 30\%$  [104], allowing steady operation (maintained for most of the steady current phase,  $\sim 10\tau_E$ ) and good performance, with  $H_{89} \sim 1.9$ ,  $H_{98} \sim 1$  [102]. Notably, empirical scalings in EDA H-mode (see section 3.1.1) indicate energy confinement with potentially weaker degradation of  $\tau_E$  with input heating power compared to that predicted by the ITERq8y2 scaling [103, 105, 106]. Rather than bursty ELM transport, the EDA pedestal is regulated continuously, with divertor  $D_\alpha$  signals (indicative of the particle exhaust from the plasma) recovering to near L-mode levels after an initial drop at the L-H transition. Access to EDA H-mode is strongly favored by higher collisionality,  $v_{\text{ped}}^* > 1$  (see eq. (2.3)), and edge safety factor [105, 107] and by strong shaping [107]. Although a higher collisionality is observed to be required at lower values of  $q_{95}$ , a collisionality threshold alone is insufficient to explain EDA access [105]. Instead, EDA and ELM-free H-modes are separated in a phase space of collisionality  $v^*$  and normalized pressure gradient  $\alpha_{\text{MHD}}$  (see eq. (2.8)) – however, the transition between the two regimes is soft, with the EDA smoothly appearing at higher pressure gradients and collisionalities rather than exhibiting a sharp transition [108].

While the pedestal pressure in EDA H-mode is comparable to that in ELMy H-mode, the pedestal profiles in EDA tend towards higher density and lower temperature, yielding the elevated pedestal collisionality favoring EDA access. The pedestal appears to be limited by transport effects rather than macroscopic stability – the pedestal is modeled to be stable to ideal MHD effects [43, 107], despite exhibiting a  $\nabla p \sim I_p^2$  trend expected from a ballooning instability [106]. High pedestal density results in strong ionization in the scrape-off layer and an edge that is relatively opaque to neutrals [23, 109]. As a result, the density will rise until the transport saturates – additional fueling through the edge triggers minimal response, while a density drop is countered by increased particle confinement to recover the density, resulting in pedestal and global density values set by the plasma current, with weak dependence on other engineering parameters [110].

The regulation of the pedestal in EDA H-mode is provided by the *Quasi-Coherent Mode* (QCM), a field-aligned electromagnetic fluctuation localized in the steep-gradient region of the pedestal [102, 111, 112]. The QCM is a fairly narrow-band ( $\delta f/f \sim 10\%$ ) mode strongly visible in density and magnetic fluctuations, with a centroid frequency ranging from 50 – 200 kHz and a fairly long poloidal wavenumber (equivalently, short wavelength),  $k_\theta \sim 1.5 \text{ cm}^{-1}$  [111]. QCM fluctuations are visible in the density flux to the divertor, indicating that the

QCM fluctuation drives particle transport through the EDA H-mode pedestal [23, 111]. Numerical modeling of the EDA H-mode pedestal suggests a resistive ballooning mode (the collisional analogue to the ideal ballooning MHD mode found in ELMy H-modes, described in section 3.2.1) for the QCM [108, 113]. This is consistent with experimental observations of the EDA pedestal – the requirement of high collisionality (the QCM disappears below  $\nu^* \sim 0.1$ ) suggests a resistive effect [43], while the favored high edge pressure gradient ( $\alpha_{\text{MHD}}$ ) suggests a ballooning instability. At high power and high edge pressure gradient, the QCM is replaced by small, high-frequency ELMs [107, 108, 112], potentially indicating that the pedestal is “burning through” the resistive-balloonning regulation of the pedestal and reaching the ideal MHD boundary associated with the ELM trigger.

The EDA H-mode presents another potential route to reactor-scale operation with naturally-suppressed large ELMs. The regime is robustly accessible on C-Mod using only RF heating with no external momentum sources or non-axisymmetric magnetic coils, with good confinement and acceptable levels of impurity accumulation and radiated power consistent with high performance [114]. Moreover, there is an extensive body of research studying the EDA H-mode on a machine with all-metal walls, with ITER-relevant heat flux and edge neutral behavior [23, 109], and with similar electron-ion equilibration to that expected for ITER [13]. However, the necessary collisionality near the pedestal top ( $\nu^* > 1$ ) for the QCM fluctuation is significantly higher than the collisionality targeted for the ITER pedestal,  $\nu^* < 0.1$ , based on requirements for the pedestal density and temperature ( $T_{\text{ped}} \sim 4 \text{ keV}$ ,  $n_{\text{ped}} \sim 4 \times 10^{19} \text{ m}^{-3}$ ), an apparent challenge to EDA H-mode access on ITER. •

## 2.4 I-MODE

In order for an H-mode regime to achieve stationary operation, there must be some form of relaxation of the density transport barrier – either by intermittent bursts of transport due to ELMs, or through a continuous fluctuation regulating the particle confinement (as in the EDA and QH-modes). However, each of these regimes faces some level of increased particle confinement relative to L-mode, as well as difficulties inherent in their operation – large ELMs are incompatible with reactor-scale operation due to the large pulsed heat loads on wall and divertor materials [58, 59], while alternate H-modes pose sometimes-onerous operational constraints. Recent work on Alcator C-Mod has demonstrated a novel high-confinement regime, termed the *I-mode*, which is unique in that it appears to decouple energy and particle transport, forming an H-mode-like temperature pedestal with the accompanying improvement in energy confinement, while maintain-

ing an L-mode density profile and particle transport level. I-mode exhibits several highly attractive properties for a reactor regime:

1. The lack of a particle transport barrier or density pedestal maintains the desired level of impurity flushing from the plasma, avoiding excessive radiative losses and naturally achieving stationary plasma conditions
2. I-mode appears to be generally stable against large ELMs, avoiding the excessive pulsed heat loads found in ELMs (of critical importance for ITER-scale devices) without externally-applied engineering controls
3. appears to exhibit much weaker degradation of confinement with increased heating power (*cf.* H-mode confinement, eq. (2.5))

A firm understanding of the structure and stability of the I-mode pedestal is essential for the extrapolation of I-mode operation to larger devices, and will form the balance of this thesis.

#### 2.4.1 *Access and Operation*

It has been long established that the orientation of the X-point (described in section 1.2.2) relative to the vertical particle drifts (particularly the  $\nabla B$  drift, eq. (1.21)) in the plasma column has a strong effect on plasma behavior, particularly flows in the edge [109, 115, 116, 117]. Notably, in cases where the ion  $\nabla B$  drift is directed towards the X-point, the power threshold to access conventional H-modes is reduced by roughly a factor of two [56, 118, 119] (thus for the balance of this section we refer to this configuration as the “favorable  $\nabla B$  drift direction”). In experiments in the unfavorable drift configuration (that is, ion  $\nabla B$  drift away from the X-point), however, a transitional state was observed in L-H threshold experiments in which energy confinement improved before the formation of a classical H-mode. This transient state, termed the “improved L-mode” on ASDEX [120], was later identified as a sustainable, distinct operating regime, termed I-mode, on Alcator C-Mod [13, 121, 122].

I-mode access is fairly robust, provided the appropriate drift configuration is held – this can be achieved either by running an upper-null shape, or by reversing the field (as well as the plasma current, to maintain magnetic-field helicity) and running in a standard LSN shape [123], shown in fig. 2.5. Upper-null operation allows a broader range of plasma shapes, but suffers from poorer diagnostic coverage and power handling due to the SOL flux impinging on a flat strike plate rather than the full lower divertor [123, 124]. Short I-mode periods have also been observed in the favorable-drift configuration in a modified plasma shape used for ELMMy H-mode experiments on C-Mod,

**Figure 2.5:** C-Mod cross-sections illustrating magnetic configurations suitable for I-mode access. Either upper-null operation in the normal field direction, or lower-null with field and current reversed provides ion  $\nabla B$  drift away from the X-point. This configuration is unfavorable for the H-mode threshold, but allows for easier access to I-mode.



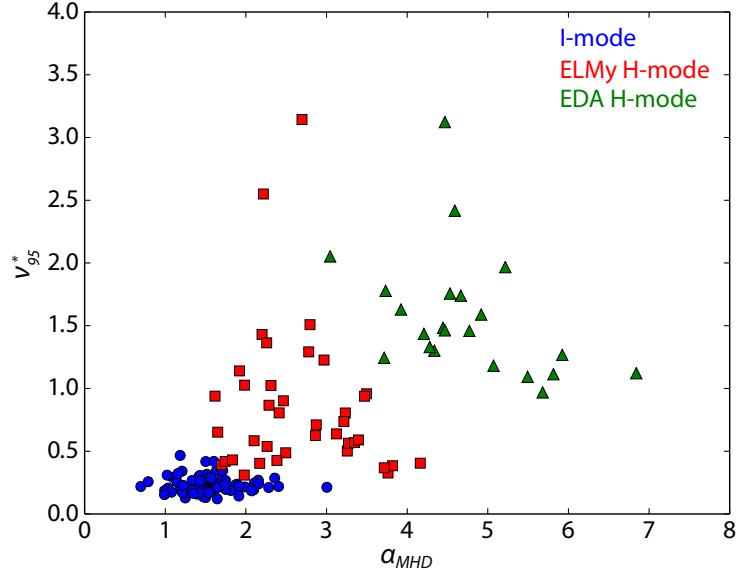
but these transitioned quickly into H-mode and will not be considered for the balance of this thesis [43, 124]. In either the forward-field USN or reversed-field LSN shape, I-mode access is favored by higher heating powers, low collisionality, and strong shaping [121]; as with all C-Mod operation, I-mode is accessible with purely RF heating, without external sources of momentum input [125]. Unlike H-modes on C-Mod, I-mode operation is also largely insensitive to wall conditions due to the low impurity confinement [123].

Initially, access to I-mode was available within a relatively narrow window in density and heating power – I-mode attempts with insufficient density were aborted by core radiation from high-Z impurities generated by interactions between fast ions and the wall, while high-density or high-power cases tended to transition into an ELM-free H-mode [121]. However, more recent experiments have greatly expanded both the available density and heating power range in I-mode, particularly by fueling into established I-modes to maintain sufficiently low density at the L-I transition [125]. As of the most recent campaign, I-modes can be sustained for the current flat-top ( $\sim 20\tau_E$ ) up to the maximum available RF heating power [123, 125].

#### 2.4.2 Global Performance & Edge Behavior

I-mode is characterized by H-mode-like normalized energy confinement ( $H_{98} \sim 1$ ) while maintaining an L-mode density profile and particle transport level. While the pedestal density is generally reduced compared to H-modes on C-Mod,  $n_{e,ped} \sim 1 \times 10^{20} \text{ m}^{-3}$ , pedestal temperatures are typically higher than H-modes at comparable power.

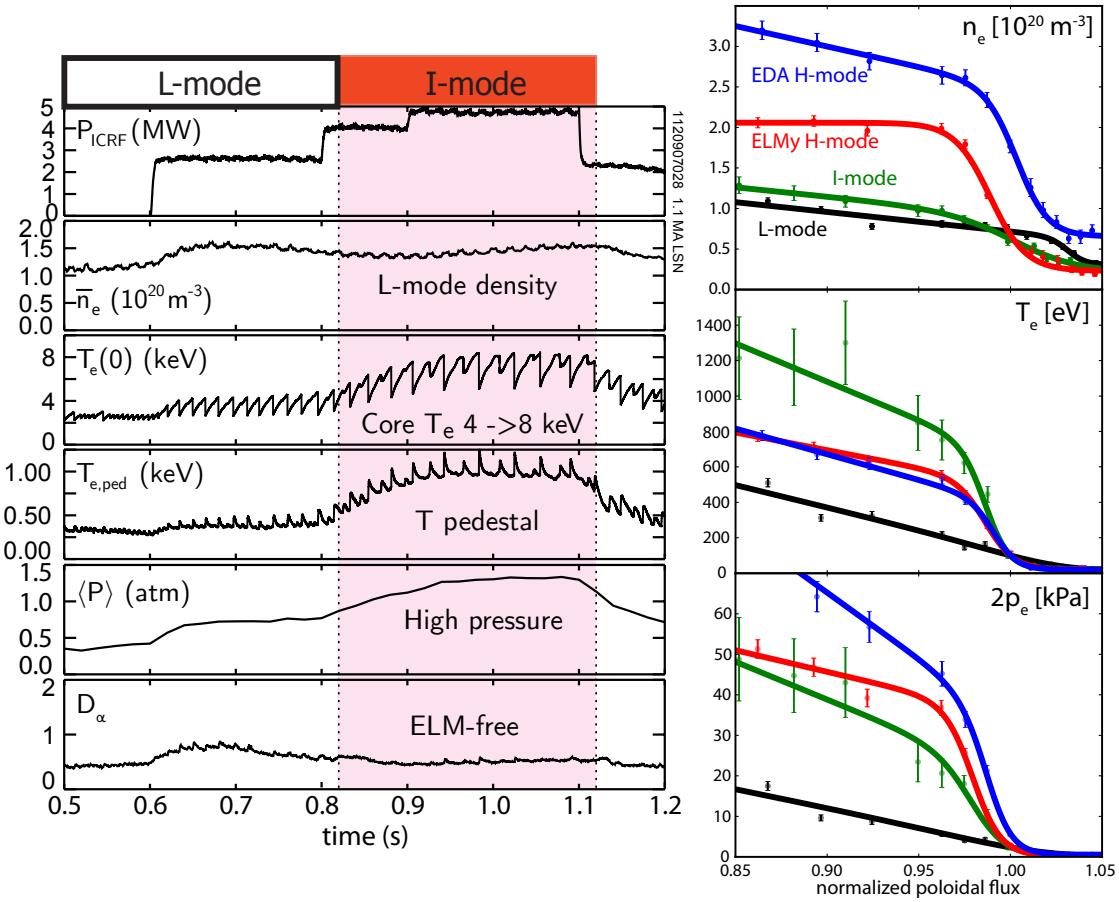
**Figure 2.6:** Customary parameter range in pedestal collisionality and normalized pressure gradient for I-mode, ELM My H-mode, and EDA H-mode. I-mode is favored by low collisionality, and exhibits the reduced  $\alpha_{MHD}$  associated with stability against ELMs.



Due to profile stiffness in the core, this results in very high core temperatures, and global-average pressures near the C-Mod H-mode record<sup>1</sup> ( $\sim 1.5$  atm in I-mode, compared to  $\sim 1.8$  atm in H-mode) [122]. Notably, scalings of stored energy against RF power in I-mode indicate only weak degradation of energy confinement with heating power, contrary to the  $\tau_E \sim P^{-0.5}$  (L-mode) or  $\tau_E \sim P^{-0.69}$  (ELM My H-mode) trends from multi-machine scalings [6, 38] – a potentially highly-favorable result for extrapolation to ITER-scale devices. Particle and impurity confinement, on the other hand, is minimal, limiting radiative losses to  $\sim 25\%$  of heating power, well below H-mode levels [121]. Impurity confinement times and accumulation are measured to be at L-mode levels on laser blow-off [126] and charge-exchange [13, 127] diagnostics. Initial studies of the I-mode threshold indicate that the mode should be accessible on ITER at reduced density ( $\sim 4 \times 10^{19} \text{ m}^{-3}$ ), then fueled after the transition up to a  $Q = 10$  scenario [24, 125]. Ready fueling control in such a scenario would be critical, as density is the primary engineering “knob” for fusion power in predominantly self-heated fusion plasmas [123].

The lack of a particle transport barrier in I-mode drives significantly different edge behavior compared to H-mode – the reduced  $\nabla n_e$  in the pedestal reduces both the overall pressure gradient and the bootstrap current drive (eq. (2.10)), which has a stabilizing effect on both ballooning and kink/peeling edge MHD modes [43]. The SOL heat flux channel in I-mode also appears to be significantly wider than in comparable H-modes [121, 125]. Energy transport suppression in I-mode appears along with the expected  $E_r$  well at the edge, which is similar in depth and  $\vec{E} \times \vec{B}$  shearing rate to some EDA H-modes, albeit weaker than that found in H-modes with the highest  $\tau_E$  [127, 128].

<sup>1</sup> and therefore the all-tokamak record thermal pressure



**Figure 2.7:** (left) Characteristic traces for a typical I-mode. At the L-I transition, the core and edge temperature rise over several sawtooth cycles (visible in the oscillations in  $T_e(0)$ ) before reaching a steady level; global confinement and pressure rise accordingly. However, the density remains at L-mode levels, and no ELMs are exhibited. (right) Edge profiles for density, temperature, and pressure in L-, I-, and H-mode. The I-mode (green) retains an density profile comparable to the L-mode (black), unlike the ELMy (red) and EDA (blue) H-modes which form a strong density pedestal. However, the I-mode forms a higher temperature pedestal than either H-mode. As a result, the I-mode reaches comparable pedestal pressures to the H-modes while retaining L-mode particle transport.

I-modes exhibit toroidal rotation levels comparable to H-mode, consistent with a  $\nabla T_e$  scaling for rotation velocity [129], which may contribute to edge shearing in I-mode [127].

Notably, the edge behavior across the L-I transition is distinct from more conventional L-H transitions. The L-H transition is rapid both in the bifurcation in measured transport (< 1 ms on C-Mod) and in pedestal development ( $\sim 20$  ms, comparable to  $\tau_E$ ) – the L-I transition, however, may exhibit a comparable bifurcation in transport (see fig. 2.9), but develops the pedestal significantly more slowly, with a steady increase in edge temperature lasting up to  $\sim 150$  ms  $\gg \tau_E$  [121, 127]. The L-I transition appears to be tied to sawtooth heat pulses reaching the edge – with each heat pulse, the edge temperature “ratchets” upward, reaching a steady I-mode over several sawtooth cycles [122, 123]. The L-I transition is seen to be more rapid at

**Figure 2.8:** Impurity confinement time  $\tau_I$  measured by laser blow-off [126] versus normalized confinement  $H_{98}$  for L-mode, I-mode, and H-mode. I-mode exhibits H-mode-like energy confinement, increased by roughly a factor of two over L-mode. However, I-mode retains L-mode levels of particle and impurity transport, readily flushing heavy impurities from the plasma. EDA H-mode exhibits strongly increased particle confinement, while transient ELM-free H-modes increase their particle confinement to the point of radiative collapse (see section 2.2)



higher levels of RF heating power and lower  $q_{95}$  [121]. Both factors are associated with larger sawtooth crashes, consistent with a transient heat pulse driving the transition [123].

#### 2.4.3 Edge Fluctuations – the Weakly-Coherent Mode

As with other high-performance regimes, the I-mode pedestal exhibits broadband suppression of turbulence at moderate frequencies ( $20 - 150$  kHz). In its place, the I-mode pedestal exhibits a broad electromagnetic fluctuation termed the *Weakly-Coherent Mode* [121]. The WCM is primarily observed as a density and magnetic fluctuation, although temperature fluctuations associated with the mode are also observed (albeit at an amplitude reduced by roughly an order of magnitude) [124, 130, 131]. Due to its prominence in the I-mode edge and similarity to the quasi-coherent mode (QCM) found in the EDA H-mode, the WCM is a prime candidate for pedestal regulation in I-mode, driving enhanced particle transport – initial observations indicate a correlation between particle flux through the LCFS and the (normalized) WCM amplitude [124], although a firm characterization of the effect of the WCM on the particle transport is ongoing.

The WCM is found at fairly long poloidal wavenumber (short wavelength),  $k_\theta \sim 1.5 \text{ cm}^{-1}$ , similar to the QCM [124]. Compared to the QCM, however, the WCM is significantly less coherent –  $\delta f/f \sim 50\%$ , compared to  $\sim 10\%$  for the QCM – and exists at a higher frequency (200 – 400 kHz) and phase velocity [122, 130]. While the radial lo-



**Figure 2.9:** Measurements of  $n_e$  fluctuations from the WCM in I-mode. (left) Reflectometer measurements in the pedestal region, showing the transition from broadband L-mode turbulence to the WCM, and subsequent fluctuation suppression as the plasma transitions into an ELM-free H-mode. Edge  $T_e$  measurements are also shown, tracking the formation of the characteristic I-mode temperature pedestal. Note the dynamics of the L-I transition – while the edge temperature increases steadily over several sawtooth periods, the turbulence suppression and formation of the WCM is more rapid, with the mode spinning up in frequency as the I-mode is established. (right) Gas-puff imaging measurements of the WCM, averaged over the I-mode. The mode is restricted in  $k$ -space to  $k_\theta \sim 1.5 \text{ cm}^{-1}$ , but is broad in frequency. Also shown is the  $k_\theta = 0$ ,  $f \sim 10 \text{ kHz}$  signal of the GAM coupled to the WCM [130].

cation and extent of the WCM has not yet been definitively determined, it has been localized within the last  $\sim 2 \text{ cm}$  of the LCFS by O-mode reflectometry [124] and gas-puff imaging [130, 132]. The onset of the WCM is immediate and contemporaneous with the turbulence suppression in the L-I transition, unlike the formation of the  $T_e$  pedestal, which typically requires several sawtooth cycles to form [132]. However, the WCM can “dither” for several sawtooth heat pulses in marginal I-modes, and typically spins up in frequency as the mode is established (contrary to the behavior observed in the QCM) [122, 132]. Notably, the WCM appears to be coupled to Geodesic Acoustic Modes (GAMs) [133] in the plasma edge. GAM dynamics have been associated with the L-H transition on other tokamaks [19, 134], but GAMs are not seen in H-modes on C-Mod – however, persistent GAMs co-existing with the mean flow in the edge are consistently seen in I-mode [130].

The nature of the WCM is, as of this writing, an open question – several candidate instabilities have been proposed, including a branch of the kinetic-ballooning mode [65] or the heavy-particle mode [135, 136], but the underlying instability in the WCM remains unknown. Experiments probing the behavior of the WCM, as well as theoretical work in understanding its underlying physics, is ongoing. ★

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# 3

## PEDESTAL MODELING AND THEORY

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While a number of high-performance regimes (described in chapter 2) have been established and are actively explored for tokamak operation, much of the physics governing these regimes is still unknown. In particular, the physics underlying the structure of the pedestal is an area of active research, due in large part to the inherent difficulty in experimentally diagnosing the pedestal plasma as it varies over short scale lengths, and in the wide variability of H-mode behaviors observed in tokamak experiments. Nevertheless confidence in the prediction of pedestal height and stability for ITER- and reactor-scale devices is essential: central temperature and pressure in the plasma are strongly sensitive to pedestal conditions due to core profile stiffness [1, 2], thus fusion power density is controlled by the pressure pedestal structure. Moreover, operation with large, uncontrolled Edge-Localized Modes (ELMs – see section 2.1) can drive transient heat loads exceeding wall material tolerances on ITER-scale devices [3, 4] – an understanding of pedestal stability against ELMs is necessary for ITER operation and beyond. This chapter provides a review of the efforts to date in theory and modeling of the pedestal, including the theoretical models considered in this thesis. •

### 3.1 EARLY MODELS

Initial efforts in understanding the pedestal took a variety of approaches, including models built from fairly simple ansatz for the physics determining the pedestal structure. Several of these approaches are detailed here. Overviews of these models may also be found in [5, 6, §2].

#### 3.1.1 *Empirical Observations*

Absent a firm understanding of the physics underlying the pedestal structure, experimental efforts have sought to characterize the pedestal in terms of simple scalings with engineering parameters. The pedestal width, in particular, presented significant difficulty in this regard, as it tends to be quite robust, varying only over a narrow range on a given machine [7] – observations on JET [8] and Alcator C-Mod [9, 10] found minimal variation of the pedestal width with plasma current or magnetic field, although a somewhat broader pedestal was observed at low current and with strong shaping on C-Mod [10, 11]. Accordingly, the measured gradients in density, temperature, and pressure

in the steepest region of the pedestal trend linearly with the corresponding value at the pedestal top [8, 10].

Multivariate dependences on engineering parameters may be explored with a reasonably general approach via power-law scalings, fitting pedestal data to scalings with no assumed underlying physics. Suttrop *et al.* [12] found for ASDEX Upgrade pedestals

$$\nabla p \sim B_T^{-0.31} P_{\text{tot}}^{0.16} \langle n_e \rangle^{-0.1} I_p^{2.1} \quad (3.1)$$

A similar approach on C-Mod using an extensive dataset of EDA H-modes [9] found

$$\begin{aligned} n_{e,\text{ped}} &\sim I_p^{0.95} n_{e,L}^{0.39} B_T^{-0.46} \\ T_{e,\text{ped}} &\sim I_p^{0.95} n_{e,L}^{-0.78} B_T^{0.80} P_{\text{net}}^{0.64} \\ p_{e,\text{ped}} &\sim I_p^{1.98} n_{e,L}^{-0.56} P_{\text{net}}^{0.48} \end{aligned} \quad (3.2)$$

(here  $n_{e,L}$  is the line-averaged L-mode target density, as pedestal density is not readily controllable in EDA H-mode). Later studies [13] in the most common range of magnetic fields, 4 – 6 T, asserted that the magnetic-field dependence was overstated in the above, although high-field ( $\sim 8$  T) studies did observe an inverse dependence of pedestal density with field [14], indicating a more complex dependence for the pedestal height than is captured in these simple models. While these empirical models perform reasonably well on their respective experimental data, a physics-based understanding of the pedestal structure is necessary to explain results on multiple machines and to confidently extrapolate to ITER-scale operation.

### 3.1.2 Neutral Penetration & the Density Pedestal

Given the proximity of the plasma pedestal to neutral gas from fueling apparatus and wall outgassing in the edge, it is logical that the density profile could depend strongly on interaction with and ionization of neutral particles in the pedestal. Based on a relatively simple particle transport model, the pedestal width is expected to scale with the characteristic neutral penetration length before ionization [6, 15]:

$$\lambda_{\text{neutral}} = \frac{v_n}{n_e \langle \sigma v \rangle_{\text{ion}}} \quad (3.3)$$

where  $v_n$  is the velocity of neutrals entering the pedestal and  $\langle \sigma v \rangle_{\text{ion}}$  is the velocity-averaged ionization rate coefficient, which is roughly constant over the temperatures of interest in the edge [6]. The neutral-penetration velocity (equivalently, the square root of the neutral kinetic energy) is set largely by molecular dissociation of neutral gas

( $\sim 1$  eV) and by charge-exchange collisions with neutrals ( $\sim 30 - 40$  eV) – over this energy range, the neutral mean free path is set by  $1/n_{e,ped}$ , with more complex models for the neutral penetration reproducing a similar dependence for the density pedestal width on  $\lambda_{neutral}$ .

However, experimental observations of the density pedestal conflict with these relatively simple predictions. Observations in similarity experiments between DIII-D, JET, and ASDEX Upgrade [16] and between DIII-D and C-Mod [17] were inconsistent with the simple model: although DIII-D data were consistent with the trends found in the model, data from JET were not, and moreover the model predicted an inconsistent scaling between the two machines for pedestal density and width. Likewise, predictions based on pedestal widths set by neutral penetration performed poorly as a predictor for pedestal height in a multi-machine scaling from AUG, DIII-D, JT-60U, and JET [18]. EDA H-modes on Alcator C-Mod show near-complete insensitivity of the density pedestal to neutral interactions – the density pedestal instead saturates to a level dictated by plasma transport (predicted best by  $n_{e,ped} \sim I_p$ ), with fueling via edge gas puffing having little effect on the density pedestal [11, 13]. This is to be expected, as then neutral mean free path in the comparatively dense SOL on C-Mod is quite short (typically on the order of a few millimeters), such that the edge is highly opaque to neutrals.

In addition to significant sensitivity to machine and discharge conditions and wall materials [16], density pedestal behavior appears to be strongly sensitive to magnetic configuration – experiments on MAST [7] found that, while the density pedestal width was poloidally constant in single-null discharges, the density pedestal is measurably broader on the outboard, low-field side in double-null discharges. These results indicate that plasma-neutral interactions in the density pedestal are quite complex, and dependent on poloidal transport behaviors and fueling asymmetries [7]. This remains an important area of research, as ITER is expected to have an edge that is highly opaque to neutrals – that is, at densities comparable to the C-Mod edge (which is observed to be opaque) and order of magnitude larger in linear size – complicating the density pedestal structure and fueling scenarios for high-density plasmas [7, 11].

### 3.1.3 Ion-Orbit Loss & Gyroradius Models

Due to the importance in the edge  $E_r$  well in pedestal formation, modeling efforts naturally turned to putative sources for the electric field to explain the pedestal. One suggested source was ion orbit loss across the last closed flux surface, in which the gyro-motion of ions near the edge intersect the SOL or the plasma-facing material surfaces (electrons are not lost due to their smaller gyroradius, reduced by the  $\sqrt{m_e/m_i}$ ). The charge imbalance induced by this particle “leak”

results in a radial electric field [19]. Assuming ion orbit losses drive the  $E_r$  well, the  $\vec{E} \times \vec{B}$  shear layer width ought to be governed by the banana orbit width, which scales as the poloidal gyroradius  $\rho_{i,pol} \sim \sqrt{T_i}/B_p$ . Accounting for the squeezing effect of the radial electric field on the banana orbit width, Shaing [20] gives for the well width

$$\Delta_{\vec{E} \times \vec{B}} \propto \sqrt{\varepsilon} \frac{\rho_{i,pol}}{\sqrt{S}}$$

$$S = \left| 1 - \frac{1}{B_p \omega_{ci,p}} \frac{dE_r}{dr} \right| \quad (3.4)$$

where  $S$  is the squeezing factor and  $\omega_{ci,p}$  is the ion cyclotron frequency evaluated with the poloidal field. The model is further refined by Itoh & Itoh [21] to include the broadening effects of viscosity shear. The predicted trend is observed in ELM-free H-modes on JT-60U [22], with  $\Delta_\rho \approx 3.3\sqrt{\varepsilon}\rho_{i,pol}$  (here  $\Delta_\rho$  is the width in real-space units mapped to the outboard-midplane minor radius); however, as the squeezing factor  $S$  is estimated to be near-unity, the measured pedestal width is broader by a factor of  $\sim 3.3$  than the  $\sim \sqrt{\varepsilon}\rho_{i,pol}$  banana width. ELMy H-modes on JT-60U exhibit a similar scaling at weak shaping, with a broader pedestal and additional safety factor dependence  $\Delta_\rho \approx 5\rho_{i,pol}q_{95}^{-0.3}$  at higher triangularity [23].

However, other predictions and experimental observations contradict these results. Depending on the calculation method of growth rate suppression by  $\vec{E} \times \vec{B}$  sheared flow, the pedestal width may scale with the gyroradius anywhere from  $\Delta \sim (\rho^*)^{1/2}$  to  $\Delta \sim \rho^*$ , where  $\rho^*$  indicates the gyroradius normalized to the plasma minor radius [16, 18]. Alternately, stabilization of drift-ballooning modes leads to a predicted dependence of  $\Delta \sim \rho_{i,pol}^{2/3}$  [24]; similarly, diamagnetic stabilization in the pedestal leads to the prediction of  $\Delta \sim I_p^2 \rho_{i,pol}^{2/3}$  [25]. Observations on DIII-D [26] found a dependence of  $\Delta/R \sim (\rho_{i,pol}/R)^{0.67}$ , while observations on ASDEX Upgrade [16, 27] found no gyroradius dependence for the pedestal width.

Distinguishing between these scalings is difficult given the diagnostic complications inherent in pedestal measurements, and the narrow range over which  $\rho_i$  or the pedestal and  $E_r$  well width vary on a given machine [7, 28]. Moreover, alternate models propose a scaling with poloidal beta at the pedestal top, rather than poloidal gyroradius, with trends of width of  $\Delta \sim \beta_{p,ped}^{0.4}$  to  $\sim \beta_{p,ped}^{0.5}$  observed on DIII-D [26, 29], JET [7], JT=60U [30], and ASDEX Upgrade [16]. Due to the strong covariance between  $\rho_{i,pol} \sim \sqrt{mT}/I_p$  and  $\sqrt{\beta_{p,ped}} \sim \sqrt{nT}/I_p$  these trends are quite difficult to separate. However, dedicated experiments to separate the two, either via pumping to vary density and temperature at fixed pressure, exploiting the density dependence in  $\beta_{p,ped}$  [26], or via isotope variation targeting the mass dependence in  $\rho_{i,pol}$  [30, 31], found the  $\beta_{p,ped}$  scaling to be the better predictor, with

a weaker secondary gyroradius dependence  $\Delta \sim \rho_{i,pol}^{0.2} \beta_{p,ped}^{0.5}$  [7, 30]. The physics underlying the  $\Delta \sim \sqrt{\beta_{p,ped}}$  scaling will be discussed in detail in section 3.3.

### 3.2 MHD STABILITY: PEELING-BALLOONING MODES

Due to the extremely rapid onset of explosive ELM instabilities, ideal MHD modes were identified early on as candidates for the ELM trigger [32, 33, 34]. In this section, we detail the development of models for the pedestal structure based on the idea that ELM instabilities represent an ultimate limit on the pedestal structure – that is, the ELM trigger sets the pedestal structure in ELMing H-mode, with the pedestal in ELM-suppressed regimes constrained at the upper bound by a transition to an ELMing phase.

The stability of a plasma may be assessed via a linear perturbation to the customary MHD equations. We consider a first-order perturbation  $\vec{\xi}$  to a plasma fluid element – typically the perturbation is considered general in spatial variables, and is taken to be a Fourier harmonic in time,  $\vec{\xi} = \vec{\xi}(\psi, \chi, \zeta) \exp(i\omega t)$  where  $\psi$  is the flux coordinate,  $\chi$  is a poloidal angle, and  $\zeta$  is a toroidal angle. Substituting into the first-order perturbation of the MHD equations, eq. (1.19), results in the simple relation (see [35, §8] for derivation)

$$\rho \frac{d^2 \vec{\xi}}{dt^2} = -\omega^2 \rho \vec{\xi} = \vec{F}(\vec{\xi}) \quad (3.5)$$

where  $\omega$  is the mode frequency,  $\rho$  is the mass density, and  $\vec{F}$  is a forcing operator given by

$$\begin{aligned} \vec{F}(\vec{\xi}) &= \frac{1}{\mu_0} (\nabla \times \vec{B}) \times \vec{Q} + \frac{1}{\mu_0} (\nabla \times \vec{Q}) \times \vec{B} + \nabla (\vec{\xi} \cdot \nabla p + \gamma p \nabla \cdot \vec{\xi}) \\ \vec{Q} &= \nabla \times (\vec{\xi} \times \vec{B}) \end{aligned} \quad (3.6)$$

with  $\vec{Q}$  for the perturbed magnetic field and  $\gamma$  for the specific heat ratio of the plasma. The usual treatment of this operator leverages the fact that  $\vec{F}$  is self-adjoint (i.e., it is its own complex conjugate) –

this permits by integration over the plasma volume  $P$  in a variational formulation

$$\begin{aligned}\omega^2 &= \frac{\delta W(\vec{\xi}^*, \vec{\xi})}{K(\vec{\xi}^*, \vec{\xi})} \\ \delta W &= -\frac{1}{2} \int_P \vec{\xi}^* \cdot \vec{F}(\vec{\xi}) d^3\vec{r} \\ K &= \frac{1}{2} \int_P \rho |\vec{\xi}|^2 d^3\vec{r}\end{aligned}\quad (3.7)$$

This formulation permits the use of the *energy principle*: if the potential energy  $\delta W$  is negative for any displacement (i.e., the perturbation drives the plasma to a more energetically-favorable state) then the mode corresponding to that displacement is unstable, captured by the fact that  $\delta W < 0$  requires an imaginary frequency  $\omega$  (and thus will have an exponentially growing mode).

This permits a conceptually straightforward means to assess mode stability. However, the formulation for  $\delta W$  is highly involved (see [35, §8.8]):

$$\begin{aligned}\delta W &= \delta W_F + \delta W_S + \delta W_V \\ \delta W_F &= \frac{1}{2} \int_P d^3\vec{r} \left[ \frac{|\vec{Q}|^2}{\mu_0} + \frac{B^2}{\mu_0} |\nabla \cdot \vec{\xi}_\perp + 2\vec{\xi}_\perp \cdot \vec{\kappa}|^2 + \gamma p |\nabla \cdot \vec{\xi}|^2 \right. \\ &\quad \left. - 2(\vec{\xi}_\perp \cdot \nabla p)(\vec{\kappa} \cdot \vec{\xi}_\perp^*) - j_\parallel (\vec{\xi}_\perp^* \times \vec{b}) \cdot \vec{Q}_\perp \right] \\ \delta W_S &= \frac{1}{2} \int_S dS |\hat{n} \cdot \vec{\xi}_\perp|^2 \hat{n} \cdot \left[ \nabla \left( p + \frac{B^2}{2\mu_0} \right) \right] \\ \delta W_V &= \frac{1}{2} \int_V d^3\vec{r} \frac{|B_1|^2}{\mu_0}\end{aligned}\quad (3.8)$$

for the fluid, surface, and vacuum energy contributions integrated over the plasma volume  $P$ , plasma surface  $S$ , and vacuum volume  $V$  respectively (in the above  $\vec{\kappa}$  is the vectorized curvature,  $\hat{n}$  is the normal vector to the plasma surface,  $\vec{b}$  is the background magnetic field unit vector, and  $B_1$  is the perturbed magnetic field in the vacuum region). The complexity of the stability problem necessitates both a firm theoretical understanding to simplify eq. (3.8) to a tractable form, and numerical approaches to efficiently calculate the stability in experimental plasmas.

### 3.2.1 Pressure-Driven Modes

Examining the fluid energy formulation  $\delta W_F$  in eq. (3.8), we see two potential sources of instability (that is, negative terms in  $\delta W$ ) – these identify the pressure gradient  $\nabla p$  and the parallel current density  $j_{\parallel}$  as potential sources of free energy to drive unstable modes. We first consider the pressure-gradient-driven modes, dubbed “ballooning modes” for their characteristic perturbation, in which the plasma tends to “bulge” outwards due to the pressure gradient. The modes tend to vary along a field line (with long parallel wavelength, although the most unstable modes have short perpendicular wavelength) such that it is concentrated in regions with the least favorable magnetic curvature, such that the increased stabilizing effect from magnetic field line bending cannot compensate for the destabilizing pressure gradient [35]. These modes were identified early on as a possible ELM trigger: early experiments in ELMy H-mode observed a limit on the pressure gradient preceding the ELM crash [36, 37], with the value of  $\nabla p$  at the limit increasing with plasma current and shaping, consistent with ballooning theory (detailed below) [27].

Early studies in ballooning modes by Connor, Hastie, and Taylor [38, 39] focused on the comparatively simple high- $n$  limit, where  $n$  is the toroidal mode number. By minimizing  $\delta W$  in terms of displacement parallel to the magnetic field and lying within the flux surface (straightforward due to the slow parallel variation of the ballooning mode), the potential energy may be expressed solely in terms of the displacement normal to the flux surface,  $\xi_{\psi}$  (here expressed for compactness as  $X = RB_p \xi_{\psi}$ ) in an expansion in powers of  $n^{-1/2}$  correct to  $O(1/n)$  by

$$\delta W = \pi \iint d\Psi d\chi \left\{ \frac{JB^2}{R^2 B_p^2} |k_{\parallel} X|^2 + \frac{R^2 B_p^2}{JB^2} \left| \frac{1}{n} \frac{\partial}{\partial \psi} (JB k_{\parallel} X) \right|^2 - \frac{2J}{B^2} \frac{dp}{d\psi} \left[ |X|^2 \frac{\partial}{\partial \psi} \left( p + \frac{B^2}{2} \right) - \frac{iF}{JB^2} \frac{\partial}{\partial \chi} \left( \frac{B^2}{2} \right) \frac{X^*}{n} \frac{\partial X}{\partial \psi} \right] \right\} \quad (3.9)$$

where  $J$  is the Jacobian, satisfying  $J d\chi = dl/B_p$  for a poloidal arc segment  $dl$ ,  $F = RB_T$  encodes the toroidal field (as in the Grad-Shafranov equation, eq. (1.23)) We define the parallel gradient operator  $k_{\parallel}$  such that

$$ik_{\parallel} = \frac{1}{JB} \left( \frac{\partial}{\partial \chi} + i n \nu \right) \quad (3.10)$$

and  $\nu = JB_T/R$  encodes the rotational transform; this requires for rational surfaces that  $n \oint \nu d\chi = 2\pi m$  for integer  $m, n$ . In eq. (3.9), the first two terms encode the stabilizing effects of magnetic field line

bending. The third term, proportional to  $(2J/B^2) dp/d\psi$ , defines the effects of the pressure gradient, which is always destabilizing, and of magnetic curvature, which is stabilizing on the inboard side and destabilizing on the outboard side – the two bracketed terms encode the effects of the components of magnetic curvature

$$\vec{\kappa} = -\vec{B} \times \left[ \vec{B} \times \nabla \left( p + \frac{B^2}{2} \right) \right] B^{-4} \quad (3.11)$$

normal to the flux surface and geodesic within the flux surface, respectively.

This is solved using the “ballooning transform” formalized in [38], which encodes the periodicity of the magnetic shear by a transform from the periodic poloidal angle  $\chi$  to an infinite, non-periodic domain  $y$  – the rapid variation in  $X$  is then contained in an exponential phase factor  $\sim \exp(-in \int v dy)$ , with the mode amplitude in a scale factor  $f(\psi, y)$  that is comparatively insensitive to  $n$ . The Euler-Lagrange equation minimizing  $\delta W$  in eq. (3.9) is satisfied by an equation of the form

$$\begin{aligned} (L + \Omega^2 M) f &= 0 \\ L &= L_0 + \frac{1}{n^{1/2}} L_1 + \frac{1}{n} L_2 + \dots \\ M &= M_0 + \frac{1}{n^{1/2}} M_1 + \frac{1}{n} M_2 + \dots \end{aligned} \quad (3.12)$$

where  $\Omega^2$  is the eigenvalue of the system and  $L, M$  are operators based on the plasma equilibrium and normalized pressure gradient  $\alpha_{MHD}$  (see eqs. (2.8) and (2.9)), with  $L$  acting as a differential operator in  $y$ . As with the expansion of the energy-principle formulation, these operators are expressed as an expansion in  $n^{-1/2}$ . To lowest order (appropriate in the  $n \rightarrow \infty$  limit) the system reduces to an eigenvalue problem for the local eigenmode characterized by  $\omega^2$  [39],  $(L_0 + \omega^2 M_0)f = 0$  – in this case, the modes are perfectly localized on their corresponding rational surfaces and decoupled from modes on other surfaces, yielding an exceedingly simple calculation, given by

$$\begin{aligned} L_0 f &= \frac{\partial}{\partial y} \left\{ \frac{1}{JR^2 B_p^2} \left[ 1 + \left( \frac{R^2 B_p^2}{B} \int^y \frac{dv}{d\psi} dy \right)^2 \right] \frac{\partial f}{\partial y} \right\} \\ &\quad + f \left\{ \frac{2J}{B^2} \frac{dp}{d\psi} \frac{\partial}{\partial \psi} \left( p + \frac{B^2}{2} \right) - \frac{F}{B^4} \frac{dp}{d\psi} \left( \int^y \frac{dv}{d\psi} dy \right) \frac{\partial B^2}{\partial y} \right\} \\ M_0 f &= \frac{J}{R^2 B_p^2} \left[ 1 + \left( \frac{R^2 B_p^2}{B} \int^y \frac{dv}{d\psi} dy \right)^2 \right] f \end{aligned}$$

(3.13)

This form is used by the BALOO code [39, 40, 41], which efficiently calculates the infinite- $n$  ballooning stability limit. Intuitively, the mode is driven by pressure gradient and stabilized by magnetic shear (variation in the field pitch angle between flux surfaces, given by  $s = d(\ln q)/dr$ ), with the attainable  $\alpha_c$  increasing with increased magnetic shear.

While the high- $n$  ballooning formalism described above has been successful for the treatment of core ballooning modes, it is insufficient to accurately model modes in the pedestal. Experimentally, the measured pressure gradient is seen to exceed the limit predicted by infinite- $n$  ballooning calculations [26, 29], indicating that stabilizing effects due to edge current density (primarily from the bootstrap effect) and diamagnetism come into play. Moreover, the assumptions used in the expansion described above break down in the edge. In the conventional theory [38, 39] described above (resulting in eqs. (3.12) and (3.13)), the mode is treated in an expansion in orders of  $n^{-1/2}$ , in which the lowest order describes a local eigenvalue  $\omega^2$  for a given flux surface, the first order  $O(n^{-1/2})$  contains the mode phase, and the second order  $O(n^{-1})$  describes the Gaussian envelope spanning  $\sim n^{1/2}$  rational flux surfaces containing the mode harmonics, as well as the correction to the “true” mode eigenvalue:  $\Omega^2 = \omega^2 + O(n^{-1})$  [42, 43]. However, the assumptions inherent in the expansion in  $n^{-1/2}$  break down in the edge due to the possibility of a steep pressure gradient out to the separatrix, and the proximity of the mode center to the plasma edge (forbidding Gaussian wave envelopes). A modification to the theory [42, 43] instead expands the energy-principle result in orders of  $n^{-1/3}$ , with the lowest order again determining a local pseudo-eigenvalue  $\omega^2$  and the first order  $O(n^{-1/3})$  defining the phase, but with the second-order expansion instead defining an Airy function envelope spanning  $\sim n^{1/3}$  rational surfaces, consistent with the edge behavior. This also provides a stabilizing  $O(n^{-2/3})$  correction to the  $n \rightarrow \infty$  theory [42]. There also remains the question of the treatment of current-driven modes, both the “peeling” mode driven by the parallel current density and the “kink” mode driven by the current gradient [44], and their effect on the edge stability, which are not included in this formalism.

### 3.2.2 Current-Driven Modes

In addition to the ballooning instability, edge kink or peeling MHD modes were proposed early on in H-mode experiments as a driver for the ELM instability [33, 45]. Whereas the ballooning modes are primarily driven by the pressure gradient, these modes are primarily driven unstable by the electric current (note the destabilizing term in

$\delta W_F$  in eq. (3.8)) in the case of the peeling mode, or by the current gradient for the kink mode [44]. These fundamentally similar instabilities – the peeling mode is strongly localized in the edge, and is driven by the rapid change in parallel current across the separatrix [42, 44]. The kink mode may be driven in the core or the edge, and tends to twist the plasma into a helix due to  $\vec{j} \times \vec{B}$  forces; the peeling mode, on the other hand, is unique to the plasma edge, and tends to peel or tear the plasma edge [43].

An extension of the analysis resulting in eq. (3.9) [39] included additional terms in  $\delta W$  accounting for the effects of current and current gradient, of the form

$$\delta W_{j_\parallel} = \pi \iint d\psi d\chi \left\{ -\frac{X^*}{n} JBk_\parallel \left( X \frac{d\sigma}{d\psi} \right) + \frac{1}{n} \left[ P^* JBk_\parallel Q + PJBk_\parallel^* Q^* \right] \right\} \quad (3.14)$$

where

$$\begin{aligned} P &= \sigma X + \frac{B_p^2}{vB^2} \frac{F}{n} \frac{\partial}{\partial \psi} (JBk_\parallel X) \\ Q &= \frac{X}{B^2} \frac{dp}{d\psi} + \frac{F^2}{vR^2 B^2} \frac{1}{n} \frac{\partial}{\partial \psi} (JBk_\parallel X) \\ \sigma &= -\frac{F}{B^2} \frac{dp}{d\psi} - \frac{dF}{d\psi} = -\frac{j_\parallel}{B} \end{aligned} \quad (3.15)$$

for parallel current density  $j_\parallel$ . An analysis in the high- $n$  limit following similar methodology to that used in ballooning modes [42] focused on the edge “peeling” modes driven by the parallel current. These modes are resonant in the vacuum on rational surfaces close to the plasma boundary – at high  $n$ , these modes are highly localized on this surface, so through an expansion about this surface Connor *et al.* [42] found for the stability criterion

$$\sqrt{1 - 4D_M} > 1 + \frac{2}{2\pi(dq/d\psi)} \oint \frac{j_\parallel B}{R^2 B_p^3} dl \quad (3.16)$$

analogous to the Mercier Criterion [46] for interchange-mode stability ( $1 - 4D_M > 0$ ), where  $D_M$  is the Mercier parameter given by

$$\begin{aligned} D_M &= -\frac{C_1}{C_2} \\ C_1 &= \frac{p'}{2\pi} \oint \frac{\partial J}{\partial \psi} d\chi - \frac{(p')^2}{2\pi} \oint \frac{J}{B_p^2} d\chi \\ &\quad + F p' \oint \frac{J}{R^2 B_p^2} d\chi \left[ \oint \frac{J B^2}{R^2 B_p^2} d\chi \right]^{-1} \left[ \frac{F p'}{2\pi} \oint \frac{J}{R^2 B_p^2} d\chi - q' \right] \quad (3.17) \\ C_2 &= 2\pi (q')^2 \left[ \oint \frac{J B^2}{R^2 B_p^2} d\chi \right]^{-1} \end{aligned}$$

It is clear from eq. (3.16) that the parallel current (on the right hand side) is destabilizing; increased pressure gradient and magnetic shear causes  $D_M$  to become more negative (deepening the “magnetic well”), stabilizing the peeling mode [47, 48]. This causes the peeling mode to destabilize below a critical value of the magnetic shear, with this value decreasing with increased pressure gradient.

**Figure 3.1:** Schematic in  $s - \alpha_{MHD}$  space of the infinite- $n$  peeling and ballooning instabilities. The ballooning instability (see section 3.2.1) is destabilized by increasing pressure gradient and stabilized by magnetic shear. A second-stable region for the ballooning mode is found at very high pressure gradient, which can be accessed by increasing the pressure gradient at low magnetic shear. The peeling instability is driven by large edge current density (equivalently, low magnetic shear), and is stabilized by increased pressure gradient.



The shared influence of pressure gradient and magnetic shear for ballooning and peeling modes is conducive to a unified picture of the stability boundaries for these modes, as shown in fig. 3.1. Ballooning instabilities are driven by pressure gradient and stabilized by magnetic shear in the first-stable region (that is, higher magnetic shear allows a steeper pressure gradient before reaching the stability boundary), while peeling modes are stabilized by pressure gradient and driven by edge current density, which is tied to the magnetic shear by the relation  $s = 2(1 - j_{||}/\langle j \rangle)$  where  $s$  is the shear and  $\langle j \rangle$  is the volume-averaged current density [38] (thus magnetic shear is

also stabilizing to peeling modes). Notably, the ballooning formalism allows for a second stable region at high pressure gradient, evident in fig. 3.1, that is accessible below a critical value for  $s$  [43, 49, 50]. This regime arises due to local effects at the outboard midplane, where the ballooning mode is most unstable – where the  $s - \alpha$  paradigm treats the flux-surface-averaged shear, it is the local shear that affects ballooning stability, with unstable modes appearing where local shear is weak or vanishing. In cases with high  $\beta$  (supported by a steep pressure gradient  $\alpha_{\text{MHD}}$ ) the Shafranov shift significantly perturbs the outboard equilibrium; when the average shear is small, this perturbation is sufficient to reverse the shear at the outboard midplane, re-stabilizing the ballooning mode and allowing second-stable access [51]. The separation of the infinite- $n$  ballooning- and peeling-unstable regions is dependent on the stabilizing effects of favorable magnetic curvature, with stronger plasma shaping (both elongation and triangularity) increasing average favorable curvature and stabilizing the modes, opening the channel in  $s - \alpha$  space for second-stable access [47].

Although the high- $n$  limit results in a highly tractable model for peeling modes, the approximation does not capture the entirety of current-driven physics in the edge. Low- $n$  kink modes can also destabilize within the pedestal due to the strongly-peaked current density profile due to the bootstrap effect, which is itself driven by the radial gradients in the profiles [47]. Moreover, multiple harmonics of the edge kink mode may couple to each other at finite  $n$  due to the broader radial extent of the mode, as well as coupling with pressure-driven ballooning modes due to the strong pressure gradient [43, 48]. Unlike the  $n \rightarrow \infty$  peeling and ballooning modes, each of which may be formulated with a simple one-dimensional calculation, treatment of the finite- $n$  coupled modes requires a more careful 2D treatment.

### 3.2.3 Coupled Modes – the ELITE Code

The high- $n$  limits for the ballooning and peeling modes (note here that we refer to all current-driven modes in the edge as “peeling,” in order to distinguish them from core kink modes) yield straightforward, one-dimensional constraints on the MHD stability of the pedestal. However, finite-larmor-radius and diamagnetic effects tend to stabilize high- $n$  modes, making this approximation relatively poor [48] – instead, the pedestal is generally limited by finite modes with toroidal wavenumbers in the range  $5 \leq n \leq 40$ . In this range, modes are radially broad enough that they are not cleanly localized on the corresponding rational surface, and may couple to other poloidal harmonics on nearby rational surfaces – this is exacerbated by the fact that the safety factor  $\sim m/n$  (for poloidal wave number  $m$ ) is divergent approaching the separatrix, such that rational surfaces become

**Figure 3.2:** Schematic in  $s - \alpha_{\text{MHD}}$  space of finite- $n$  coupled peeling-balloonning instabilities, with the infinite- $n$  decoupled results (see fig. 3.1) shown by the dashed lines. Mode coupling tends to stabilize finite- $n$  ballooning modes. However, the coupled modes can close off access to the second-stable regime; only in cases with very strong “magnetic wells” (typically achieved with extreme plasma shaping) does this access reopen.



vanishingly close together [42]. Moreover, pressure-driven ballooning and current-driven peeling modes may couple, generating modes driven by both free-energy sources, with sufficient radial extent to affect the entire pedestal region – driving the large, explosive crashes associated with type-I ELMs [52]. Treatment of these modes requires a full two-dimensional approach. Mirroring the approach shown in fig. 3.1, a schematic illustration of the results from such a 2-D calculation are shown in fig. 3.2. Although finite- $n$  effects tend to stabilize the ballooning mode (infinite- $n$  calculations for the peeling and ballooning modes are shown as the dashed lines), mode coupling tends to close off the access path to the second-stable region [43]. At higher  $n$ , the first- and second-stable regions tend to pinch together due to weakened coupling between modes, reopening access to the second-stable region; the modes also decouple more readily in a deeper “magnetic well,” expressed as  $d_M = D_M s^2 / \alpha$  to encode the effects of shaping and finite aspect ratio with deep magnetic wells and the accompanying potential for second-stable access most readily attained with strong plasma shaping [47].

We use the “Edge-Localized Instabilities in Tokamak Equilibria” or ELITE code [43, 47, 52] to calculate both the growth rate and eigenmode structure for these coupled modes. ELITE utilizes the expansion of the free energy in  $O(n^{-1})$  found in earlier studies of peeling and ballooning modes (see eqs. (3.9) and (3.14)), with an additional

boundary term for the peeling drive [52, 53], reproduced here for completeness:

$$\delta W = \pi \iint d\Psi d\chi \left\{ \frac{JB^2}{R^2 B_p^2} |k_{\parallel} X|^2 + \frac{R^2 B_p^2}{JB^2} \left| \frac{1}{n} \frac{\partial}{\partial \Psi} (JB k_{\parallel} X) \right|^2 \right. \\ - \frac{2J}{B^2} \frac{dp}{d\Psi} \left[ |X|^2 \frac{\partial}{\partial \Psi} \left( p + \frac{B^2}{2} \right) - \frac{iF}{JB^2} \frac{\partial}{\partial \chi} \left( \frac{B^2}{2} \right) \frac{X^* \partial X}{n \partial \Psi} \right] \\ - \frac{X^*}{n} JB k_{\parallel} \left( X \frac{d\sigma}{d\Psi} \right) + \frac{1}{n} \left[ PJB k_{\parallel}^* Q^* + P^* JB k_{\parallel} Q \right] \\ \left. + \frac{\partial}{\partial \Psi} \left[ \frac{\sigma}{n} X^* JB k_{\parallel} X \right] \right\} \quad (3.18)$$

with  $P$ ,  $Q$ , and  $\sigma$  as defined in eq. (3.15). Given this formulation, the methodology used in ELITE is straightforward. First, poloidal variation is encoded in a “straight field line” angle  $\omega$  [43],

$$\omega = \frac{1}{q} \int^x v \, d\chi \quad (3.19)$$

(recall that the rotational transform and safety factor  $q$  are encoded such that  $2\pi q = \oint v \, d\chi$ ). Using this, the perturbation  $X = RB_p \xi_{\psi}$  is decomposed into individual poloidal harmonics,

$$X = \sum_m u_m(\psi) e^{-im\omega} \quad (3.20)$$

where at fixed  $n$  each  $u_m$  describes the eigenmodes centered on rational surfaces determined by each  $(m, n)$  pair. It can be shown [52] that this yields the relation

$$JB k_{\parallel} X = \sum_m \left( -\frac{v}{q} \right) (m - nq) u_m(x) e^{-im\omega} \quad (3.21)$$

motivating the introduction of the radial variable  $x = m_0 - nq$ , where  $m_0$  is the poloidal mode number of an arbitrary reference rational surface. By convention, the treatment in ELITE uses  $m_0 = \text{Int}(nq_a) + 1$  for edge safety factor  $q_a$ , which constructs the first rational surface in the vacuum in a limited geometry (recall that this was the most-unstable point for high- $n$  peeling modes in section 3.2.2) – while in a divertor geometry this surface is in the plasma edge, as the safety factor is divergent approaching the separatrix due to the presence of the X-point, nevertheless the reference surface is still readily constructed using the edge safety factor. The parameter  $x$  describes spatial variation over the expected length scale for the radial extent of  $u_m$ , and is a

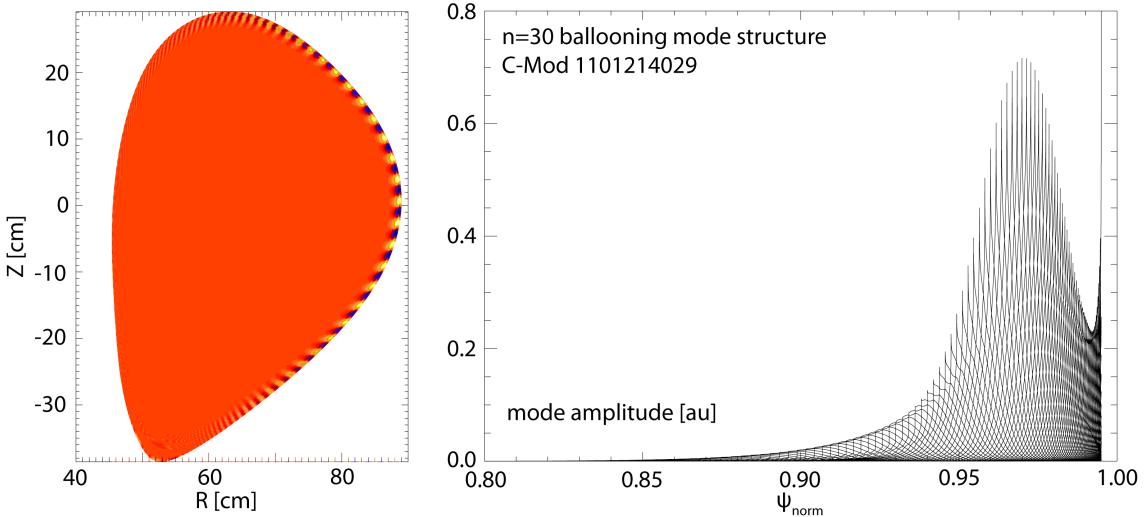
straightforward conversion from  $\psi$ . It is worth noting that ELITE does not treat the separatrix in its calculations, instead truncating the calculation at an internal surface (typically 99.5 – 99.8% of poloidal flux), which prevents a singularity in  $x$ ; although peeling modes are highly unstable at the X-point, high local collisionality prevents the omission from significantly affecting the overall result [54]. The Euler-Lagrange equations minimizing the potential energy may be expressed as a set of coupled second-order ordinary differential equations of the form [53]

$$A_{m,m'}^{(2)} \frac{d^2 u_m}{d\psi^2} + A_{m,m'}^{(1)} \frac{du_m}{d\psi} + A_{m,m'}^{(0)} u_m = 0 \quad (3.22)$$

where the coefficients  $A$  are matrix elements describing the coupling between two modes  $m$  and  $m'$  (see Wilson *et al.* [52] for definitions). Efficient computation of these eigenmodes is assisted by two simplifications: first, while the eigenmodes  $u_m$  vary on a very short length scale  $x$ , comparable to the spacing between rational surfaces, the equilibrium parameters used in the calculation of the matrix elements  $A$  vary more slowly, and can be calculated on a coarser mesh than that needed to evaluate eq. (3.22). Second, this radial localization of  $u_m$  means that only harmonics on nearby rational surfaces will strongly couple – other modes can be ignored in the computation to save time [52]. An example of the eigenmode structure for an  $n = 30$  ballooning mode is shown in fig. 3.3, with the poloidal variation of the displacement amplitude (strongest at the outboard midplane, as is typical for ballooning modes) shown at left and the radial structure of the modes shown at right.

Absent other considerations, the eigenvalue  $\gamma^2$  from this ideal MHD calculation describes both the stability of the mode, and its growth rate – positive growth rates (typically presented with a natural normalization to the Alfvén frequency  $\omega_A = v_A/R$ , with  $v_A = B/\sqrt{\mu_0 \rho}$ , arising from the system of equations) indicating an unstable mode. However, a number of studies [25, 55, 56] have noted that this treatment neglects finite-Larmor-radius and diamagnetic effects, which can have a strong stabilizing effect on modes in the pedestal. While a full treatment of the diamagnetic effects requires a fluid treatment not captured by the ideal MHD formalism, the stabilizing effect in the pedestal may be approximated by a nonzero growth-rate threshold for the instability – this is described (*cf.* [47]) by the analytic relation

$$-\gamma_{MHD}^2 = \omega(\omega - \omega_{*pi}) \quad (3.23)$$



**Figure 3.3:** Mode structure for an  $n = 30$  ballooning mode calculated by ELITE. (left) Contour plot of radial perturbations from the mode. The mode is edge-localized and strongest at the outboard midplane, consistent with an edge ballooning mode. (right) Eigenmode structure of the  $n = 30$  mode. Each peak is a poloidal harmonic localized around the rational flux surface determined by the corresponding poloidal mode number  $m$  for  $n = 30$ . The mode is strongest in the steep gradient region, but extends inward due to the comparatively high mode number (eigenmode envelope encompasses  $O(n^{1/3})$  flux surfaces). Note that, as ELITE cannot treat the separatrix, the mode calculation truncates at  $\psi_{\text{norm}} = 0.995$ .

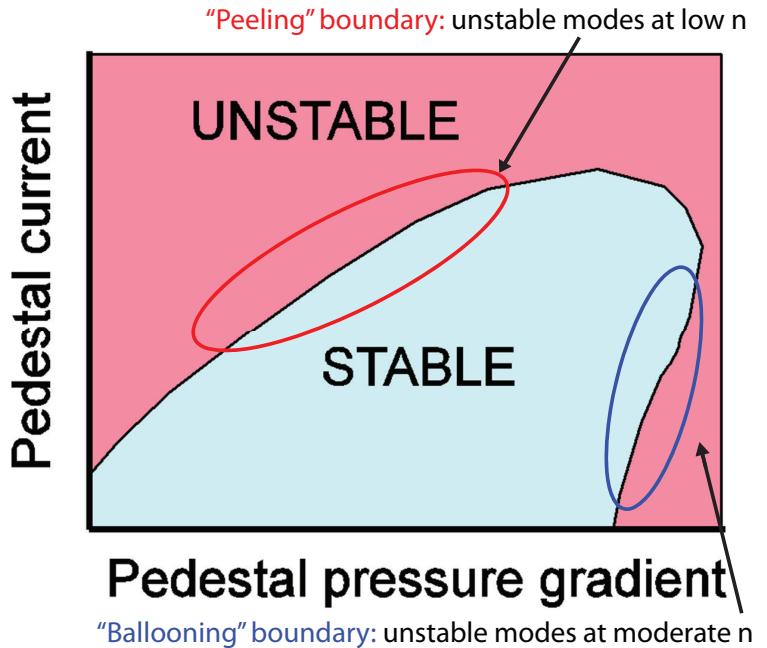
where  $\gamma_{\text{MHD}}$  is the ideal growth rate and  $\omega_{*\text{pi}}$  is the diamagnetic frequency given by [34, 55, 57].

$$\begin{aligned} \omega_{*\text{pi}} &= \tau \frac{nq \langle \nabla \psi \rangle}{\rho_0 B_0 \langle r \rangle} \frac{dp}{d\psi} \\ \tau &= \frac{1}{\omega_{Bi}\tau_A} = \frac{1}{eR_0\sqrt{M/\mu_0 n_i}} \end{aligned} \quad (3.24)$$

where angled brackets indicate a flux-surface average,  $\omega_{Bi}$  is the ion bounce frequency,  $\tau_A$  is the Alfvén time, and  $\rho_0$  is the mass density normalized to that on the magnetic axis. eq. (3.23) requires  $\gamma > \omega_{*\text{pi}}/2$  for instability; as the diamagnetic frequency is mode-number-dependent (roughly  $\omega_{*\text{pi}} \sim n\omega_A$  [48]) this provides the expected improved stabilization of higher- $n$  ballooning modes in the ELITE formalism. However, the diamagnetic frequency is expected to vary strongly on short length scales in the pedestal due to the pressure-gradient dependence [34], with the result of the peeling-balloonning stability calculation depending significantly on the treatment approach for this variation.

Sequences of ELITE calculations are capable of effectively characterizing the stability space for a pedestal – this is customarily expressed in terms of normalized pressure gradient ( $\alpha_{\text{MHD}}$ ) and normalized pedestal current ( $j_n = 2j_{||}/\langle j \rangle$ , such that  $s = 2 - j_n$ ) in place of the less-intuitive magnetic shear  $s$ , as shown in fig. 3.4. This shape is, at a glance, similar to first-stable regime in fig. 3.2 (albeit mirrored

**Figure 3.4:** Schematic of the stability space to coupled peeling-balloonning MHD modes, set by the edge pressure gradient and current density. Ballooning modes are driven by pressure gradient, while kink/peeling modes are current-driven but stabilized by pressure gradients.



along the vertical axis). However, the shape of the stability boundary is modified by the effects of collisionality on the MHD stability [57]. At low collisionality, the bootstrap current is quite high for given pedestal gradients. The enhanced edge current drives particularly unstable peeling modes, with the most unstable modes at lower  $n$ , setting the upper-left boundary of the stable region. Higher collisionality suppresses the edge current density, leaving ballooning modes the most unstable. A simplistic calculation finds that ballooning modes are consistently more unstable at higher  $n$  – however, higher- $n$  modes are strongly stabilized by diamagnetic effects [37], thus moderate  $n \sim 10 - 40$  ballooning modes limit high-collisionality pedestals [48], found at the right-side, high- $\alpha_{\text{MHD}}$  boundary. In moderate-collisionality, high-performance discharges (such that both edge pressure gradient and bootstrap current are high) coupled peeling-balloonning modes with  $n \sim 5 - 15$ , found in the “nose” of the stability boundary, limit the pedestal. These coupled modes may extend comparatively far into the plasma, leading to large, explosive ELMs on instability [52]. However, as discussed above strong shaping inhibits this mode coupling, extending the “nose” of the stability boundary to high pressure gradient and current; with extreme shaping, second-stable access may open for a broad range of  $n$ , opening the stability boundary to second-stable access [58]. In practice, the stability boundary is well-characterized by calculations spanning  $5 \leq n \leq 35$  – higher  $n$  are suppressed by diamagnetic effects, while  $n < 5$  peeling modes are difficult to distinguish from core kink modes due to their broad radial extent, and are rarely more unstable than  $n > 5$  [57].

ELITE calculations have been benchmarked against a number of other codes [54], including GATO [59], MISHKA [55, 60], MARG2D

[61, 62], and KINX [63, 64]. Notably, GATO calculations extend to lower  $n$  than are suitable in ELITE, and KINX calculations include treatment of the separatrix – however, ELITE calculations show good agreement across a broad range in toroidal mode number. ELITE has been broadly successful in capturing the limiting physics of ELMy H-mode [48], although nonlinear calculations are necessary to capture the dynamics of the ELM crash itself [65]. Moreover, other H-mode regimes are well-described by peeling-balloonning physics – the EDA H-mode [17, 66] and QH-mode [67] are modeled to be stable just below the ballooning and peeling sides of the boundary, respectively, with ELMs appearing as the pedestal crosses the ideal MHD limit. RMP ELM-suppressed H-modes are similarly calculated to be peeling-balloonning stable, with ELMs appearing as the pedestal crosses the boundary when the RMP coils are switched off [57]. The peeling-balloonning boundary is evidently a useful figure of merit in general for H-mode pedestals. •

### 3.3 KINETIC-BALLOONING TURBULENCE MODELING

Following the L-H transition, the  $\vec{E} \times \vec{B}$  flows associated with the formation of the pedestal and transition to high confinement should continue to rise, due to the strong increase in the diamagnetic term due to the pedestal [57]. However, the pedestal gradient appears to be limited, even before the onset of an ELM [7] – thus, there must be a mechanism limiting the pedestal prior to the onset of the ideal MHD instability (section 3.2). As the  $\vec{E} \times \vec{B}$  flow strongly suppresses long-wavelength turbulence, short-wavelength turbulent modes appear to be an ideal candidate. Electron-temperature-gradient (ETG) modes at short wavelengths are likely to modify the interplay between density and temperature in the pedestal, rather than limiting the total pressure [57]. Instead, recent efforts have focused on the kinetic-balloonning mode (KBM) for a constraint on the pressure pedestal.

The KBM arises from the introduction of kinetic effects in an extension of the high- $n$  ideal ballooning MHD formalism, introduced in section 3.2.1 [68]. Although the initial assumptions for each are quite different – the ideal MHD energy principle (eq. (3.9)) requires high collisionality for the coupled fluid treatment, the kinetic-energy formulation treating a collisionless plasma with trapped-particle effects results in a very similar fluid-like relation [68]. Earlier gyrokinetic studies focused on electrostatic fluctuations, of which the ion-temperature gradient (ITG) mode is dominant; however, the introduction of magnetic fluctuations both modifies ITG dynamics, and allows for the formation of the electromagnetic KBM fluctuation [69]. In regimes with high  $\beta$  or steep pressure gradients – in short, exactly the plasmas of concern for high-performance regimes – electrostatic

simplifications to gyrokinetic turbulence break down, necessitating treatment of the KBM in modeling [69, 70].

Gyrokinetic and gyrofluid simulations using the necessary electromagnetic treatment [69, 71, 72, 73] found the onset of a distinct turbulent mode at high beta, overtaking the usually-dominant ITG and trapped-electron mode (TEM) turbulence at low and moderate beta, respectively. Above this threshold in  $\beta$  (more properly, a threshold in  $\alpha_{\text{MHD}}$ ), simulations using the GYRO code [74] found that the mode onset was highly stiff – that is, the growth rate of the mode increases extremely quickly even in plasmas just above the onset threshold [73] – and is insensitive to  $\vec{E} \times \vec{B}$  shear, such that the mode drives transport levels sufficient to constrain the pedestal gradient near the critical  $\alpha_{\text{MHD}}$  [57]. Moreover, gyrofluid simulations found that the KBM is destabilized near the infinite- $n$  ideal ballooning limit – in cases with a flat temperature profile, the onset is precisely matched to the calculated MHD limit, while the inclusion of a finite temperature gradient somewhat reduced the onset  $\alpha_{\text{MHD}}$  due to ion drift resonance effects [69]. This motivates the use of more straightforward high- $n$  MHD calculations (see section 3.2.1) to calculate the KBM threshold for the purposes of this thesis, rather than complex gyrokinetic/gyrofluid simulations.

The stiff onset of the kinetic-balloonning mode, and accompanying limits to the pedestal pressure gradient, allows for a heuristic scaling for the pedestal width [57]. To good approximation, the critical gradient is simply given by  $\alpha_c \sim \beta_{p,\text{ped}}/\Delta$  for the poloidal beta at the pedestal top and the pedestal width  $\Delta$  expressed in (normalized) poloidal flux – thus we require  $\Delta \sim \beta_{p,\text{ped}}/\alpha_c$ . As with ideal MHD ballooning modes, the KBM is sensitive to magnetic shear. However, at the outboard midplane (where magnetic curvature is least favorable) the local shear is such that the critical  $\alpha_c$  increases with decreasing shear,  $\alpha_c \sim 1/s^{1/2}$ . In the pedestal, we expect the shear to trend as  $1/\langle j \rangle$ , which to lowest-order approximation is simply  $1/\beta_{p,\text{ped}}$  as the current in the pedestal is bootstrap-dominated. This implies  $\alpha_c \sim \beta_{p,\text{ped}}^{1/2}$  and therefore  $\Delta \sim \beta_{p,\text{ped}}^{1/2}$ . This trend is in accordance with experimental observations on DIII-D [26], JT-60U [30, 75], ASDEX Upgrade [16, 76] and Alcator C-Mod [77]. Moreover, the growth of the pedestal between ELMs appears to maintain a limited pressure gradient [7, 78], and pedestal fluctuations saturate early in the ELM cycle [79], consistent with the idea that KBM turbulence constrains the pedestal independent of explosive ELM-driven transport.

### 3.3.1 The Ballooning-Critical Pedestal Technique

The arguments detailed above lead to an intuitive expression for the pedestal width and height based on KBM limits,  $\Delta \sim \beta_{p,\text{ped}}^{1/2}$ . However, full quantification of the KBM constraint from first principles re-

quires a more detailed treatment. The analogous onset of the KBM to the infinite- $n$  ideal ballooning MHD mode allows a computationally-efficient approach to the turbulence threshold.

The KBM is an approximately local effect due to its short scale length – as such, no single calculated mode can describe the destabilization of the entire pedestal without a highly involved nonlocal calculation of the stability across the pedestal profile. A far more efficient and straightforward model can be developed using the “ballooning critical pedestal” (BCP) technique [80, 81], which finds the point where half of the pedestal is locally at or beyond criticality for the KBM. At fixed pedestal width, the height is incremented to increase the pressure gradient, following the same approach as the peeling-balloonning calculation. At each increment, the stability of the pedestal to high- $n$  ideal ballooning MHD modes is calculated, e.g., using the BALOO code [39, 40]. As the infinite- $n$  modes calculated by BALOO are also perfectly localized on the corresponding rational flux surfaces, the code finds unstable surfaces in the pedestal region and the width of the pedestal covered by these surfaces. When half of the pedestal width is thus unstable, the KBM threshold is said to have been reached. This approach is highly numerically efficient – as the ballooning MHD criterion reduces in the infinite- $n$  limit to a straightforward one-dimensional eigenvalue problem [39] that can be computed efficiently – and fairly robust, although it does require the unstable region of the pedestal to be well-defined and bounded (typically the “middle half” of the pedestal, where the pressure gradient is steepest). This assumption can break down at very strong shaping or low aspect ratio [81].

#### 3.4 THE EPED MODEL

In light of the importance of the pedestal structure for optimized fusion performance – both by maximizing fusion power density via the pressure pedestal height constraint on core profiles [82], and by avoiding or mitigating large, damaging ELMs [3, 4] – a predictive understanding of the pedestal is highly desirable for planned operations on ITER and beyond. Models based on peeling-balloonning MHD instability, particularly the ELITE code (section 3.2.3), have proven quite successful at capturing the limiting physics of the ELMy H-mode pedestal. However, these calculations typically rely on experimental profiles and magnetic equilibria reconstructed after the fact, and as such cannot by themselves provide predictive capability. Similarly, the constraint set by kinetic-balloonning mode (KBM) turbulence (section 3.3) corresponds well with pedestal observations in profiles with steep pressure gradients in the pedestal, but cannot by itself uniquely constrain the pedestal structure. The EPED series of mod-

els, developed by Snyder *et al.* [81], combines these two constraints into a single predictive model for the ELMy H-mode pedestal.

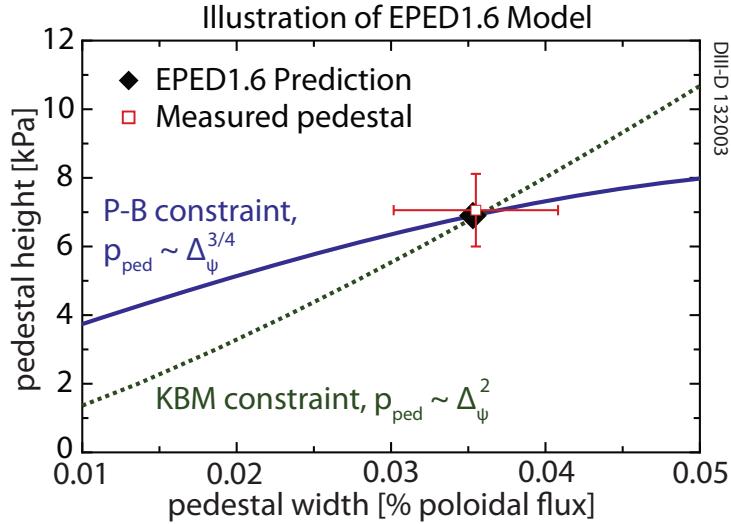
To incorporate predictive capability into the peeling-balloonning MHD stability model calculated by ELITE (section 3.2.3), the EPED model must characterize peeling-balloonning stability as accurately as possible using only parameters known prior to the plasma discharge, set by operator control; however, as discussed in section 3.2.3, the inherent nonlocality of the problem still requires two-dimensional MHD calculation. To that end, the model employs a set of model Miller equilibria [49], up/down-symmetric equilibria allowing for plasma elongation and triangularity defined with analytic plasma profiles such that the essential physics in the pedestal (namely, the pressure gradient and bootstrap current profiles) is nearly matched to experimental conditions [57]. Using this setup, the model equilibria may be defined by a small set of scalar parameters for use in ELITE: major and minor radius  $R$  and  $a$ , elongation and shaping  $\kappa, \delta$  (recall that in these up/down-symmetric equilibria  $\delta_l = \delta_u = \delta$ ), plasma current  $I_p$ , and applied field  $B_T$ , set the magnetic equilibrium when combined with the target global normalized pressure (typically the Troyon normalized  $\beta_N$  [83]). Global beta also impacts the pedestal stability via the beneficial effect of increased Shafranov shift in the core on MHD stability [67]. The EPED model additionally takes as inputs for the ELITE calculation the density at the pedestal top  $n_{e,ped}$  and the pedestal width  $\Delta$  in normalized poloidal flux (note that the density and temperature profiles are defined to have the same width) to constrain the pressure and current profiles, with the bootstrap current calculated from the density and temperature profiles from the analytic Sauter formula, eq. (2.10) [84].

The calculation of the peeling-balloonning stability boundary is straightforward – at a fixed pedestal width, the pressure pedestal height (and, accordingly, the MHD instability drives from the edge pressure gradient and current density) is increased in increments until the stability boundary is reached [57]. The interdependence between pedestal width and height is determined by repeating the calculation at a range of pedestal widths, determining a relation between the pressure pedestal width and height for a given model equilibrium. To lowest order, the MHD limit is a limit on  $\nabla p$ , leading one to expect a linear relation between the pedestal width and height. However, non-local effects on the MHD stability – in particular, the broader, lower- $n$  modes destabilized by wider pedestals leading to reduced maximum  $\alpha_{MHD}$  at wider  $\Delta$  [56] – reduces the linear dependence, leading to a rough scaling of  $p_{ped} \sim \Delta^{3/4}$  set by the peeling-balloonning stability boundary [54].

On its own, the peeling-balloonning MHD constraint defines the pedestal height as a function of width, necessitating a second constraint to allow a unique predictive solution. The Kinetic Ballooning

Mode (KBM), described in section 3.3, limits the pedestal gradient with a relation  $p_{\text{ped}} \sim \Delta^2$  (more precisely,  $\Delta \sim \beta_{p,\text{ped}}^{1/2}$ ). This constraint is sufficiently distinct from that enforced by peeling-balloon MHD that only a single nontrivial solution satisfying both exists – thereby uniquely predicting the pedestal width and height. An example of the prediction at the intersection of the P-B and KBM constraints, along with the corresponding experimental result [81], is shown in fig. 3.5.

**Figure 3.5:** Illustration of the peeling-balloon MHD and kinetic-balloon turbulent constraints used in the EPED model. The peeling-balloon constraint, calculated by ELITE, results in a trend roughly of  $p_{\text{ped}} \sim \Delta_{\psi}^{3/4}$ , while the KBM width constraint calculated via the balloon-critical pedestal (BCP) technique sets  $p_{\text{ped}} \sim \Delta_{\psi}^2$ . The unique solution to these constraints is the EPED prediction for the pedestal width and height. The prediction is here shown compared to the measured pedestal from DIII-D shot 132003 (reproduced from [81])



### 3.4.1 EPED with Semi-Empirical Width Constraint

The simplest version of the EPED series, EPED1 [57], takes advantage of the dominant scaling of the width with  $\beta_{p,\text{ped}}$  in the KBM constraint, described in section 3.3: as little secondary variation of the width beyond  $\Delta \sim \beta_{p,\text{ped}}^{1/2}$  is seen with other expected controlling parameters, e.g.,  $\nu^*$ ,  $\rho^*$  or  $\rho_{\text{pol}}^*$ ,  $n_{e,\text{ped}}$  [57] (cf. section 3.1, particularly section 3.1.3), the constraint is reduced to a single relation  $\Delta = c\beta_{p,\text{ped}}^{1/2}$  with a fitted value for  $c$ . For historical reasons based on DIII-D data, EPED1 uses  $c = 0.076$ , although a newer multi-machine fit produces  $c = 0.084$  [81].

To calculate the threshold for the peeling-balloon MHD instability, the growth rate as calculated by ELITE must be balanced against the inherent stabilizing effect of plasma diamagnetism in the pedestal, as described in section 3.2.3. The effect of diamagnetic stabilization may be approximated by a threshold in the growth rate,  $\gamma > \omega_{*\text{pi}}/2$  for the diamagnetic frequency  $\omega_{*\text{pi}}$ . In the EPED1 model  $\omega_{*\text{pi}}$  is taken to be constant across the pedestal, with a value set to the half-maximum calculated for the analytic pedestal structure used by the model equilibrium [57]. Although this is a comparatively rough approximation of the diamagnetic effect in the pedestal, it can be calculated with very high computational efficiency.

Both the KBM and P-B constraints calculated in EPED1 use significant simplifications. Nevertheless, the model is capable of producing predictions with a systematic  $\pm 15 - 20\%$  uncertainty across a range of parameters [57, 80]. The simplicity and efficiency of the calculations used allow EPED1 to be tested against very large pedestal datasets [81].

### 3.4.2 EPED with First-Principles Width Constraint

Although the bulk of the variation in the KBM-constrained pedestal width is captured by the  $\beta_{p,ped}$  scaling, it is nevertheless desirable to account for its effects on the scale factor of the trend – more properly, the weakly-varying function  $G(\nu^*, \varepsilon, \dots)$  such that  $\Delta = G\beta_{p,ped}^{1/2}$  – allowing EPED to make first-principles predictions (in that the constraint is not dependent on a scale factor set by fitted data).

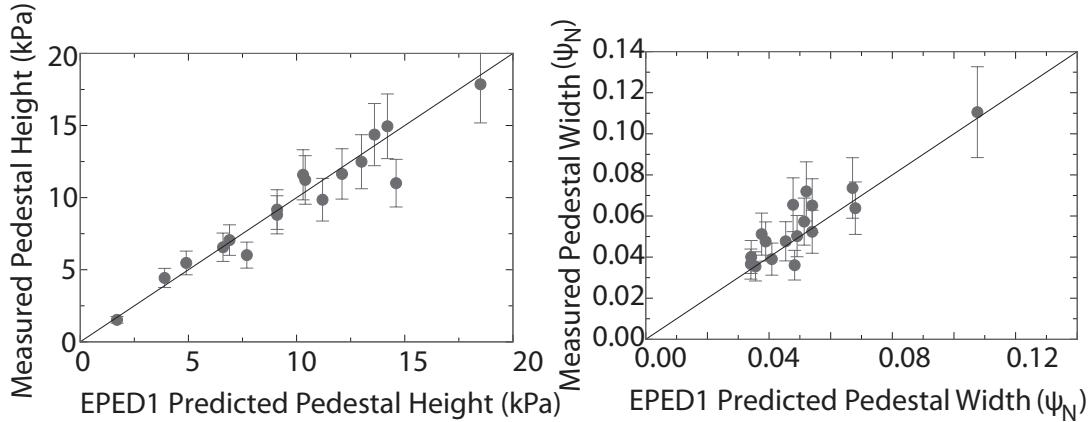
The EPED1.6 implementation [80, 81] achieves this by directly calculating the KBM constraint via the “ballooning critical pedestal” (BCP) technique, described in section 3.3.1. By performing this calculation across a range of pedestal widths and fitting the result against  $\beta_{p,ped}$ , a first-principles calculation of the KBM pedestal constraint is generated and paired with the peeling-ballooning MHD result [81]. While this approach is more computationally expensive than the fixed scaling used in EPED1, the BCP calculation allows the effects of collisionality and shaping on the KBM threshold to be properly accounted for – this manifests in a range of scale factors,  $\langle G \rangle \approx 0.07 - 0.1$ , that are comparable to the fitted result used in EPED1, but are specific to discharge characteristics.

The simple diamagnetic stabilization model used in EPED1, described above, also fails to capture important physics in the pedestal – the model assumes a constant diamagnetic frequency  $\omega_{*pi}$  for the stabilization of the peeling-ballooning modes, while in fact the diamagnetic frequency varies rapidly over the pedestal [80]. EPED1.6 replaces this with an “effective” diamagnetic frequency  $\omega_{*eff}$ , based on a fit to calculations of the diamagnetic stabilization of peeling-ballooning modes in the fluid code BOUT++ [85, 86, 87]. This provides stronger stabilization of higher- $n$  ( $n > \sim 12$ ) modes at higher collisionality than that found in the simple linear model [81, 88], a correction that is particularly necessary for the comparatively high-collisionality pedestals in ELMy H-modes on C-Mod [88].

### 3.4.3 EPED Model Implementation & ITER Predictions

The EPED model has been extensively tested on numerous machines, particularly on DIII-D [78, 81], JT-60U [54], C-Mod [89], and KSTAR [90]. The model has also been tested on NSTX [78], with limited success due to breakdown of the assumptions inherent to the KBM con-

straint at small aspect ratio [54]. Given the proximity of the pedestal to the peeling-ballooning MHD and KBM turbulence limits in most high-performance regimes, it is expected that EPED predictions are viable as a figure of merit for H-mode operation on ITER [81, 91].



**Figure 3.6:** EPED1 predictions versus measured pressure pedestal height and width on a range of DIII-D discharges [57].

Notably, EPED predictions for ITER (shown compared to results from DIII-D and C-Mod [88] in fig. 3.6) predict pedestal pressures of  $\beta_{N,ped} \sim 0.6 - 0.7$ , corresponding to  $p_{ped} \sim 90$  kPa, at a pedestal width of  $\Delta \sim 4\%$  [54, 81]. This is within a factor of  $\sim 2 - 3$  of the range of experimental results on which EPED has been tested [88, 89], and is consistent with the planned  $Q = 10$  operation on ITER assuming sufficient optimization of core and pedestal profiles [81, 91]. Although development is ongoing for the EPED model series, it has demonstrated viable predictive capability for H-mode pedestals in a variety of conditions for conventional-aspect-ratio tokamaks. ★

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# 4

## ELMY H-MODES ON C-MOD

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The ELMY H-mode [1, 2], described in section 2.1, is the most commonly accessed high-performance regime on major tokamak experiments. The bursty transport driven by ELMs provides sufficient relaxation of the particle confinement in H-mode to allow stationary operation without excessive impurity accumulation; as such, the ELMY H-mode is considered the baseline operating regime for ITER [3, 4]. However, on ITER-scale devices the pulsed heat loading associated with ELMs drives unacceptable levels of erosion and damage to plasma-facing wall and divertor materials [5, 6].

In light of the impact of large, deleterious ELMs on the ITER wall, and the profound impact of pedestal height on overall plasma performance [7, 8], a firm understanding of the physics governing the pedestal in high-performance regimes and their extrapolation to reactor-scale devices is of paramount importance to fusion research leading up to ITER operation. To that end, a Joint Research Target combining theory, experiment, and modeling efforts in the ELMY H-mode pedestal was undertaken [9, 10]. Notably, this effort saw the development of the EPED model [11, 12, 13], described in section 3.4, which predicts the pressure pedestal width and height preceding the ELM crash through a combination of constraints based on peeling-balloonning MHD instability [14, 15, 16] (section 3.2) and kinetic ballooning turbulence [17] (section 3.3). This chapter details the contributions from Alcator C-Mod to this joint effort [18] both in empirical studies of the ELMY H-mode pedestal, and in the implementation of the EPED model. C-Mod ELMY H-modes greatly expand the parameter space in which the EPED model is tested, reaching within a factor of two of the target pedestal pressure for ITER. The techniques developed in this analysis will subsequently be applied to I-mode pedestals in chapters 5 and 6.

### 4.1 ELMY H-MODE ACCESS & EXPERIMENTAL ARRANGEMENT

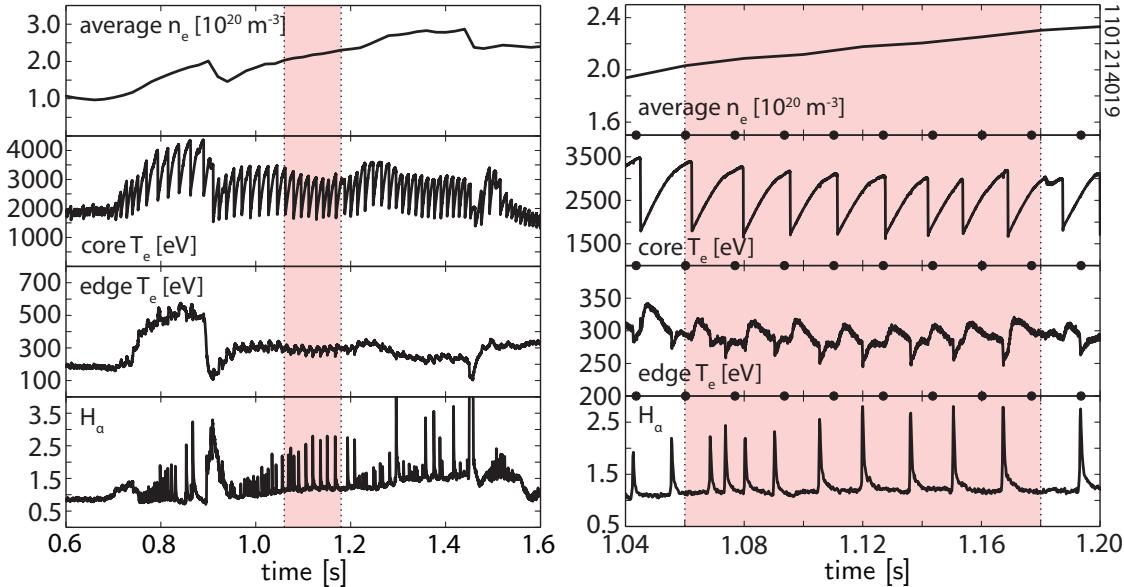
Typical H-modes on Alcator C-Mod do not exhibit the large Type-I ELMs customarily seen on other devices [20]. Instead, ELM-free H-modes tend to form at lower collisionalities, with high-density operation tending towards the continuously-regulated EDA H-mode rather than exhibiting discrete ELMs (see sections 2.2 and 2.3.2). However, by operating in a modified shape (see fig. 4.1) with low elongation,  $\kappa \sim 1.4 - 1.55$ , and low upper triangularity ( $\delta_u \sim 0.15$ ) paired with high lower triangularity ( $\delta_l > 0.75$ ) and a strike point on the diver-

**Figure 4.1:** C-Mod cross-section comparing the typical plasma shape (blue) to the altered shape favoring ELMy H-mode operation (red), developed in joint experiments with the JFT-2M tokamak [19]. ELMy H-mode access is favored by high lower triangularity and an outer strike point in the divertor slot, coupled with very low upper triangularity and elongation. This is thought to reduce the required edge pressure gradient and current to reach the peeling-ballooning boundary.



tor floor, regular ELMy H-mode operation is attainable. This comparatively weak shaping, developed in similarity experiments with the JFT-2M tokamak [21, 22], reduces the necessary pressure gradient and bootstrap current to reach the ideal peeling-ballooning MHD stability boundary (described in section 3.2), triggering the ELM. In this shape, new experiments on C-Mod [18] attained ELMy H-modes across a broad range in current (400 – 1100 kA) and field (3.5 – 8 T) with high-resolution pedestal data.

Pedestal profiles are taken with the edge Thomson scattering system, detailed in appendix A.1.2. The pedestal data is taken over steady ELMing phases (generally targeting  $< 10\%$  variation over the time window) to minimize the effects of random scatter in the data – an example of such a window, with line-averaged density  $\bar{n}_e$ , core and edge  $T_e$ , and divertor  $D_\alpha$  signal (indicative of the ELM crash), is shown in fig. 4.2, with a comparison of the individual-frame fits to the ensemble shown in fig. 4.3. Strictly, models of the pedestal struc-



**Figure 4.2:** Example ELMY H-mode window (highlighted). Phases for study are selected for steady density ( $\bar{n}_e$  shown in the top trace), temperature (ECE  $T_e$  signals shown for the core and pedestal), and ELM cycles ( $D_\alpha$  signal shown). The same modeling window is shown zoomed-in at the right. Note the strong perturbation to the edge temperature due to both the sawtooth crash and the ELM, while the interior temperature is perturbed only by the sawtooth. Thomson scattering frames are indicated by the black ticks on the axes – the ELM cycle is at a comparable frequency,  $\sim 60$  Hz, to the TS system frame rate. This presents a difficulty for selecting data masked to the “peak” of the ELM cycle, necessitating long, steady ELMing phases for study.

ture in ELMY H-mode predict the pedestal immediately preceding the ELM crash, when the pedestal is most unstable to the ELM trigger. However, ELMs on C-Mod typically cycle at 60–100 Hz, comparable to the repetition rate of the Thomson scattering system (as shown in figs. 4.2 and 4.3). This presents difficulties in resolving the pedestal with multiple frames per ELM and binning the data to the peaks of the ELM cycle. In most cases, pedestals are prepared in a single “ensemble average” utilizing all TS data in the window; in certain cases, a statistical set is also constructed using time slices during the last 20% of the ELM cycle as is typical for other machines. The results from this correction are discussed in section 4.2.

The electron density, temperature, and pressure profiles are fitted using a modified hyperbolic-tangent fit developed in [23]. In a general  $x, y$  space, the fitting function is expressed by

$$\begin{aligned}
 z &= \frac{x_0 - x}{\delta} \\
 \text{mtanh}(\alpha, z) &= \frac{(1 + \alpha z)e^z - e^{-z}}{e^z + e^{-z}} \\
 y &= \frac{h + b}{2} + \frac{h - b}{2} \text{mtanh}(\alpha, z)
 \end{aligned} \tag{4.1}$$



**Figure 4.3:** Comparison of fits for the  $n_e$ ,  $T_e$ , and  $p_e$  pedestal width and height from Thomson scattering. Individual frames of data are shown as black points, with their average shown by the black line (errorbars indicated by the dashes). The ensemble-averaged fit is shown in red. The ensemble fit captures the average behavior in a steady ELMing phase well, while suppressing the random scatter found in individual frames of TS data. For comparison, ELM crash times in the window are indicated by vertical dashed lines.

**Figure 4.4:** Example pedestal illustrating the  $\text{mtanh}$  function used for pedestal fitting (eq. (4.1)), defining the parameters: height  $h$ , baseline  $b$ , midpoint  $x_0$ , half-width  $\delta$ /full width  $\Delta$ . The inboard slope is characterized by the parameter  $\alpha$ .



where  $x_0$  is the pedestal midpoint,  $h$  and  $b$  are the height and baseline, and  $\delta$  is the half-width (we use  $\Delta = 2\delta$  as the “pedestal width”). The inboard slope is encoded by the parameter  $\alpha$ , with the multiplicative factor  $1 + \alpha z$  providing an approximately linear profile inboard from the steep-gradient region ( $z \gg 0$ ). This definition provides a smooth, continuous definition for the pedestal gradient throughout the profile, given by

$$\begin{aligned} \frac{dy}{dx} &= -\frac{h-b}{2\delta} \left[ \frac{1 + \frac{\alpha}{4} (1 + 2z + e^{2z})}{\cosh^2(z)} \right] \\ \frac{dy}{dx} &\rightarrow -\frac{h-b}{2\delta} \left( 1 + \frac{\alpha}{2} \right) \quad \text{as } x \rightarrow x_0, z \rightarrow 0 \\ \frac{dy}{dx} &\rightarrow -\frac{h-b}{2\delta} \alpha \quad \text{for } z \gg 0 \end{aligned} \tag{4.2}$$

with the peak gradient found analytically at  $x_0$  ( $z = 0$ ). Recent H-mode studies use the fitting parameter  $h$  as the figure-of-merit for the pedestal height; however, it is also common to express the pedestal height in terms of the evaluated value of the fit at the 95% poloidal flux surface. For the purposes of this document we denote the height taken from the fitting parameter  $h$  by the subscript  $\text{ped}$ , and values taken at the 95% flux surface by the subscript  $95$ .

Due to the ready availability of high-resolution electron density and temperature diagnostics, for the purposes of this section we assume equal ion and electron pressures,  $p = 2n_e T_e$  (a viable approximation on C-Mod due to the relatively low impurity content found in ELMy H-modes,  $Z_{\text{eff}} \sim 2$ , and rapid ion-electron thermal equilibration in H-mode pedestals on C-Mod [24]). All profiles are prepared using normalized poloidal flux for the abscissa, facilitating comparison to results from other machines and to the EPED model. For the



**Figure 4.5:** Comparison of the measured pedestal widths for the  $n_e$  and  $T_e$  pedestals, differentiated for the low-, standard-, and high-field H-mode cases. Pedestal widths are similar for density and temperature, although on average the density pedestal is slightly wider. The error-weighted centroid of the dataset is shown by the star.



**Figure 4.6:** Comparison of the directly-measured pressure pedestal width and the EPED width  $\Delta_\Psi$ , defined as the average of  $\Delta_{n_e}$  and  $\Delta_{T_e}$ . The widths trend quite closely to one another, although  $\Delta_\Psi$  is systematically somewhat wider.

purposes of the EPED model we also prepare an averaged width, defined by

$$\delta_\Psi = \frac{\delta_{n_e} + \delta_{T_e}}{2} \quad \Delta_\Psi = 2\delta_\Psi \quad (4.3)$$

a practice adopted in order to include in multi-machine studies devices in which the density and temperature profile measurements are generated by distinct diagnostics (rather than taking both from the Thomson scattering system, as is customary on C-Mod) and to more closely match the assumption of  $\Delta_T = \Delta_n$  used in model profiles in EPED. As the density and temperature widths are quite close (although the density pedestal is, on average, slightly wider, as shown in fig. 4.5, with an average ratio of  $\Delta_{T_e}/\Delta_{n_e} = 1.051$ ), the difference between  $\Delta_\Psi$  and the directly-measured  $\Delta_{p_e}$  is minimal – as shown in fig. 4.6, the two widths are well-correlated, with  $\Delta_\Psi$  systematically slightly wider. ●

## 4.2 ELM CYCLE SYNCHRONIZATION

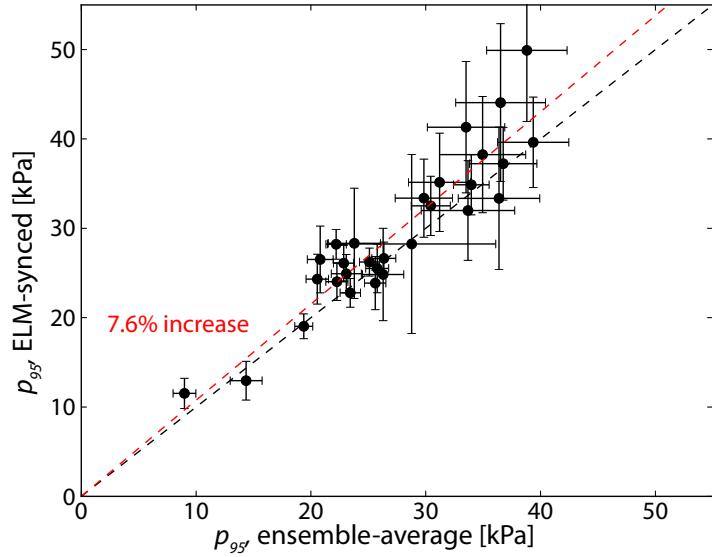
The common practice for modeling the ELMY H-mode pedestal is to take profile data immediately preceding the ELM crash (commonly, data from the last 20% of the ELM cycle), as this most closely corresponds to the pedestal profile at the stability limit associated with the ELM trigger. However, as the ELM cycle in H-mode on C-Mod is typically at a comparable repetition rate to the Thomson Scattering system (60 Hz), this practice is only possible on a subset of discharges,

with sufficiently long, steady H-mode phases, such that a sufficient number of frames in the desired time window can be found. Data prepared in this manner are denoted as “ELM-synchronized” for the purposes of this thesis.

**Figure 4.7:** Comparison of the pressure pedestal height  $p_{ped}$  between the ensemble-averaged and ELM-synchronized profiles. On average, ELM synchronization results in a 10.8% increase in measured pedestal pressure, consistent with ELM losses observed on other machines. At lower pressures, ELMs are typically small enough that the perturbation is minimal; however, the distinction becomes important for the highest-pressure ELMs on C-Mod.



**Figure 4.8:** Comparison of the pressure at the 95% flux surface,  $p_{95}$ , between the ensemble-averaged and ELM-synchronized profiles. On average, ELM synchronization results in a 7.6% increase in the measured pressure. This is consistent with the ELM perturbation to the pedestal being largely restricted to the pedestal just within the steep-gradient region, with decreasing perturbation further into the plasma from the pedestal.



A comparison between the ensemble-averaged and ELM-synchronized pressure pedestals (pedestal height  $p_{ped}$  and the pressure at the 95% flux surface  $p_{95}$ ) are shown in figs. 4.7 and 4.8. ELM synchronization finds an average 10.8% increase in the measured pressure  $p_{ped}$ , with a slightly lesser increase of 7.6% in  $p_{95}$ . This is consistent with the perturbation to the pressure pedestal by the ELM observed on other machines [5, 25]. The weaker perturbation due to the ELM crash observed at the 95% flux surface is also consistent with previous ELM observations – the ELM crash typically alters the pressure profile only

in a region just inside the steep-gradient region, with minimal perturbation to profiles in the plasma interior.

#### 4.3 ENGINEERING PARAMETER SCAN

The ELMY H-mode experiments presented here significantly expanded the parameter range available for the regime on Alcator C-Mod, including a broad scan in plasma current (400 – 1100 kA) and toroidal magnetic field (3.5, 5.4, 8.0 T), as well as a secondary scan of elongation ( $1.45 < \kappa < 1.55$ ) and collisionality ( $0.25 < \nu_{95}^* < 6$ ). This study entailed a factor of  $\sim 7$  sweep in pedestal pressure – notably, this expanded the range of pressure pedestals tested against the EPED model to within a factor of two of the target pedestal thermal pressure for ITER [12].

##### 4.3.1 $I_p$ Scan

Trends of the density, temperature, and pressure pedestal widths and heights with plasma current are shown in fig. 4.9. Previous experiments in EDA H-modes [26] demonstrated a robust linear dependence of the pedestal density on plasma current; density is less constrained by current ELMY H-mode (fig. 4.9, (b)). A weak positive trend of the pedestal temperature (fig. 4.9, (d)) is seen, but is insufficient as a unique predictor. The combined pressure pedestal ( $p = 2n_e T_e$ ) exhibits a  $p_{95} \sim I_p$  trend, with significant scatter.

The density and temperature pedestal widths individually show no systematic dependence on the plasma current. In the combined pressure pedestal width an inverse trend  $\Delta_p \sim I_p^{-1}$  is discernable, although the pressure width varies little, ranging from  $\Delta_p \sim 3 - 5\%$  of poloidal flux.

These observations imply a combined pressure gradient,  $\nabla p \sim I_p^2$ , consistent with pedestals limited by ballooning MHD instability, as described in section 3.2. However, the large degree of scatter in both the height and width – indeed, the width range at 0.7 MA and 1.0 MA span nearly the full range of widths – necessitates a more careful treatment. In general, the pressure pedestal height may be approximated well by  $p_{ped} \sim \nabla p \times \Delta_p$ . The ballooning limit is couched (*cf.* Saibene *et al.* [27]) as  $\nabla p \sim I_p^2 f_{sh}$ , where  $f_{sh}$  is a function describing the magnetic shear. Early models proposed that the pedestal width should be governed by poloidal gyroradius  $\rho_{i,pol} \sim \sqrt{T_{e,ped}}/I_p$ , as shown in fig. 4.10. However, the putative scaling of the pedestal width on  $\rho_{i,pol}$  is readily conflated with the KBM-limited trend of pedestal width with  $\beta_{p,ped}^{1/2} \sim \sqrt{n_{e,ped} T_{e,ped}}/I_p$ . Assuming a  $\beta_{p,ped}$  limit on the pedestal width, we predict  $p_{ped} \sim I_p \sqrt{n_{e,ped} T_{e,ped}}$ , shown in fig. 4.11 to be a significantly better predictor of the pedestal height.



**Figure 4.9:** Plasma current scalings of the density, temperature, and pressure pedestal widths and heights. Magnetic-field sets are differentiated by color. While the density and temperature pedestals independently show little systematic dependence of their widths on plasma current, the pressure pedestal width exhibits a  $\Delta_{ped} \sim I_p^{-1}$  trend. The  $n_e$  and  $T_e$  pedestal heights both positively trend with current, although with significant scatter – inverse trends between the two are consistent with the zero'th-order approximation of MHD-limited ELMs lying on a curve of fixed  $\beta_{p,ped}$  for a given shaping/field configuration. The pressure pedestal height shows a trend of  $p_{ped} \sim I_p$ , such that the pressure pedestal is consistent with the expected  $\nabla p \sim I_p^2$  scaling.

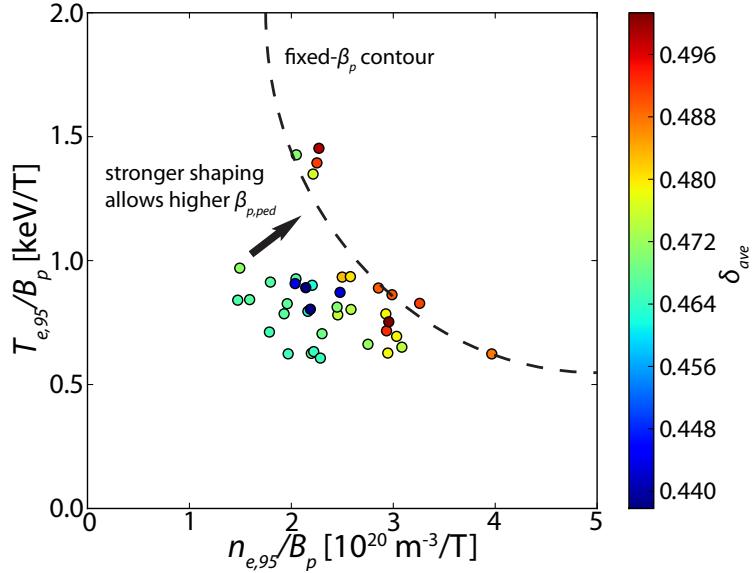


**Figure 4.10:** Pedestal pressure versus  $I_p \sqrt{T_{e,95}}$  – effectively, the  $p_{\text{ped}} \sim I_p^2 \rho_{i,\text{pol}}$  scaling predicted in [28].



**Figure 4.11:** Pedestal pressure versus  $I_p \sqrt{n_{e,95} T_{e,95}}$  – effectively, the  $p_{\text{ped}} \sim I_p^2 \sqrt{\beta_{p,\text{ped}}}$  scaling predicted for a KBM-limited pedestal.

**Figure 4.12:** Pedestal density vs. temperature normalized to poloidal field (accounting for variation in plasma current) such that hyperbolae in the parameter space are curves of fixed  $\beta_{p,\text{ped}}$ . At a given shaping, ELMY H-mode pedestals are to lowest order constrained to fixed  $\beta_{p,\text{ped}}$ , with stronger shaping allowing greater attainable  $\beta_p$ .



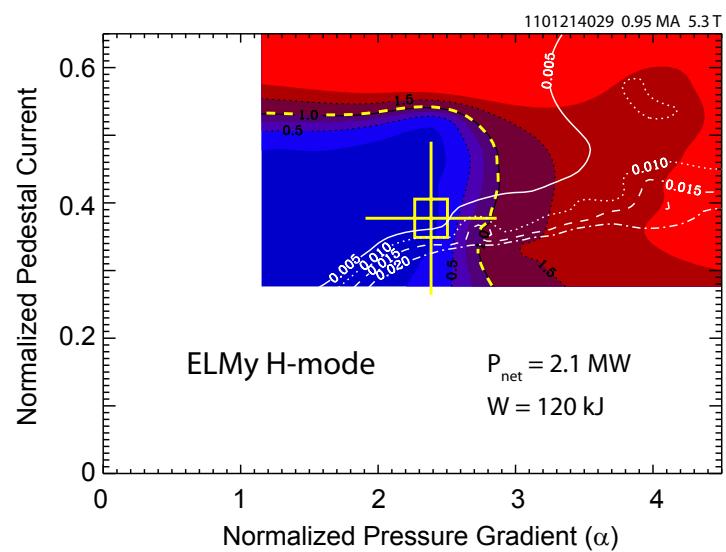
The interplay between pedestal width, height, and gradient is readily apparent in this treatment, which resolves the issues in the simplistic scaling with current alone. In the restricted shapes available for ELMY H-mode operation on C-Mod, both the pedestal width and height (specifically,  $\beta_{p,\text{ped}}$ ) vary little – broader parameter scans in pedestal width and  $\beta_p$  were achieved with shaping scans [29], due to the beneficial impact of strong plasma shaping on MHD stability, thereby improving the maximum pressure gradient, width, and height. At restricted shape, the robust width causes this scaling to reduce to  $p_{\text{ped}} \sim \nabla p \sim I_p^2$ , consistent with previous observations [30]. To lowest order, then, these ballooning-limited pedestals may be approximated to be limited in  $\beta_p$  at the pedestal top. This is shown in fig. 4.12 (see also fig. 2.2), showing the pedestal density versus temperature normalized to the poloidal field. This normalization accounts

for plasma-current differences between points, as well as rendering hyperbolae in the parameter space as contours of fixed  $\beta_{p,ped}$ . At a given shaping, ELMY H-modes lie roughly on a contour of fixed  $\beta_{p,ped}$ , with stronger shaping allowing a higher attainable poloidal beta.

#### 4.4 EPED MODEL PREDICTIONS

The EPED model, described in section 3.4, combines pedestal limits based on coupled peeling-balloonning MHD instabilities [14, 15, 16] and kinetic-balloonning mode turbulence [17]. An example of MHD and KBM calculations of the type used by EPED is shown in fig. 4.13. The red-blue contour indicates the peeling-balloonning growth rate calculated by ELITE normalized to the diamagnetic stabilization rate  $\omega_{*eff}/2$  (described in section 3.2.3), with the yellow dash indicating the stability boundary,  $\gamma/(\omega_{*eff}/2) = 1$  – in this case, the pedestal is limited by intermediate-n balloonning modes (see fig. 3.4), as is expected at the higher collisionality typically seen on C-Mod. White contours indicate the KBM stability calculated by BALOO, described in section 3.3, showing the pedestal width that is beyond the KBM threshold (the mode is considered to be triggered when half of the pedestal is thus unstable). To within error bars, the ELMY H-mode pedestal is at both the peeling-balloonning and kinetic-balloonning stability boundaries, as is expected for pedestals at the ELM threshold. Calculations of this type are shown in more detail in chapter 6.

**Figure 4.13:** Calculation of the peeling-balloonning MHD stability contour from ELITE for an ELMY H-mode pedestal on C-Mod. The red-blue contours show the peeling-balloonning growth rate with diamagnetic stabilization,  $\gamma/(\omega_{*eff}/2)$ , while white contours show the width in flux space that is unstable to the KBM. To within error bars, the pedestal lies on the peeling-balloonning boundary. The comparatively higher collisionality typical of C-Mod H-mode pedestals pushes the MHD behavior of the pedestal towards higher- $n$ , pure-balloonning modes, although moderate- $n$  coupled modes in the “nose” of the stability contour are also common.



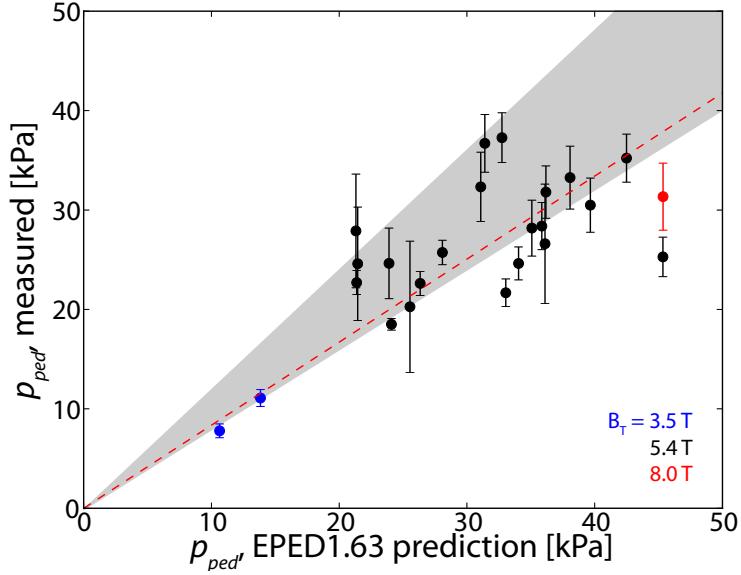
These models set two distinct constraints on the pedestal width and height, with peeling-balloonning MHD predicting  $p_{ped} \sim \Delta^{3/4}$  and kinetic-balloonning turbulence predicting  $p_{ped} \sim \Delta^2$  (see fig. 3.5). The unique intersection of these two constraints provides a predictive

value for the pedestal width and height. The most recent version of the model, EPED1.63, utilizes a modified gyrokinetic calculation compared to the standard EPED1.6 (section 3.4.2) to more accurately constrain the diamagnetic stabilization of higher- $n$  peeling-balloonning modes, necessary for the ballooning modes that typically limit the pedestal on C-Mod due to the high collisionality. A comparison between the observed and predicted pedestal parameters is presented here.

#### 4.4.1 Pedestal Height

A comparison between the pressure pedestal height predicted by EPED1.63 and the observed height is shown in fig. 4.14. While most measured pedestals lie within the  $\pm 20\%$  expected error in the EPED prediction (indicated by the grey band in fig. 4.14), the EPED model systematically over-predicts the pedestal pressure, corresponding on average ratio of measured to predicted pedestal heights of  $0.835 \pm 0.036$ , indicated by the red dashed line.

**Figure 4.14:** Pressure pedestal height predicted by EPED1.63 versus the measured (ensemble-averaged) pedestal height, color-coded by magnetic field set. The grey band indicates agreement within the  $\pm 20\%$  typical prediction accuracy for EPED. The EPED model systematically over-predicts the pedestal pressure, with an average ratio of  $0.835 \pm 0.036$  (indicated by the red dashed line).



The discrepancy between the predicted and measured pedestal heights may be attributed (at least in part) to the use of pedestal measurements averaged across the entire ELM cycle (“ensemble-averaged”). As discussed in section 4.2, models of the pedestal structure (including EPED) most closely correspond to the pedestal structure immediately preceding the ELM crash, where the pedestal is most unstable to the ELM trigger. A subset of ELMy H-modes are prepared with ELM-synchronized data, shown in fig. 4.15 with the corresponding ensemble-averaged points for comparison. The prediction accuracy is substantially improved, with an average ratio of measured to predicted pedestal heights of  $0.934 \pm 0.066$ , well within the anticipated

**Figure 4.15:** Pressure pedestal height predicted by EPED1.63 versus measured, ELM-synchronized pedestal height (red, with corresponding ensemble-average points shown in black). The grey band indicates agreement within the  $\pm 20\%$  typical prediction accuracy for EPED. ELM synchronization brings the measured pedestal height into better agreement with EPED predictions, with a correspondence of  $0.934 \pm 0.066$  (indicated by the red dash).



$\pm 20\%$  accuracy of the EPED prediction. As expected, the modification to the measured pedestal pressure by ELM synchronization is minimal at lower pedestal pressures, but becomes substantial at higher pedestal pressures ( $> 35$  kPa) as ELM losses increase proportionally with the pedestal stored energy.

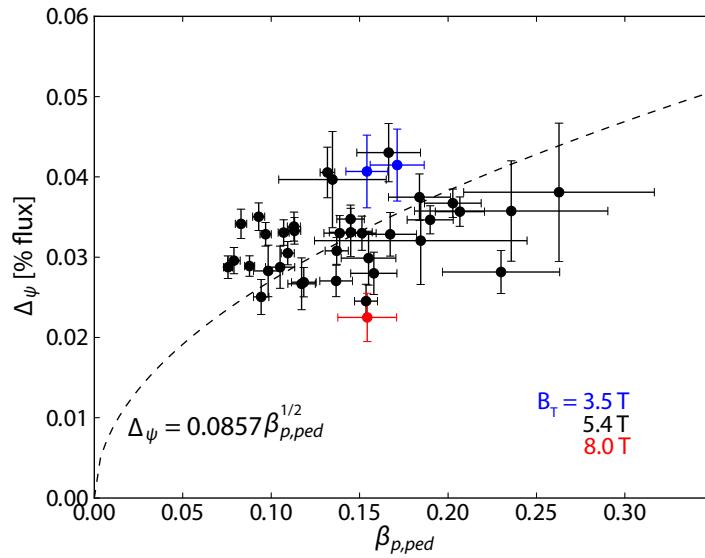
The EPED model still on average slightly over-predicts the pedestal pressure, however, although the agreement is generally within experimental uncertainty – this is potentially due to the strong sensitivity of the stability calculation to diamagnetic effects, which tend to stabilize higher- $n$  ballooning modes. As diamagnetic effects are substantial in the relatively collisional pedestal found in H-modes on C-Mod, a careful accounting of these effects is necessary for accurate prediction – use of a slightly weaker diamagnetic stabilization model brings the prediction into somewhat better agreement with C-Mod data.

#### 4.4.2 Pedestal Width

While historically a number of models for the pedestal width (see section 3.1) have been examined, the most uniformly successful has been an expected scaling of pedestal width with poloidal beta at the pedestal top ( $\beta_{p,ped}$ ), observed on several machines [9], and shown to follow from a critical-gradient limit in the edge pressure profile established by kinetic-balloonning mode (KBM) turbulence. Including magnetic shear stabilization, this takes the form  $\Delta = c\beta_{p,ped}^{1/2}$ , where  $c$  is, strictly, a weakly-varying function of a number of plasma parameters [11]. This constraint on the pedestal width and height is utilized in the EPED model, coupled with peeling-balloonning MHD stability limits to set a unique constraint on the pedestal structure at the ELM crash.

An evaluation of this scaling with ensemble-averaged data is shown in fig. 4.16, with a fitted scale factor of  $\langle c \rangle = 0.0857 \pm 0.0024$ , consistent with previously-observed scalings. The earliest versions of the EPED model used this simple constraint as the second condition on the pedestal width and height, using an experimentally-determined fixed scale factor. The newest version of the model self-consistently calculates the scale factor from gyrokinetic considerations of the KBM turbulence; however, the result is quantitatively similar. A comparison of the experimental versus the EPED1.63-predicted pedestals in  $\Delta_\psi - \beta_{p,ped}$  space is shown in fig. 4.17.

**Figure 4.16:** Ensemble-averaged EPED width  $\Delta_\psi$  (eq. (4.3)) versus  $\beta_{p,ped}$ , color-coded by field set. The expected scaling from the KBM limit,  $\Delta_\psi = c\beta_{p,ped}^{1/2}$ , is shown with a scale factor of 0.0857, consistent with observations in other experiments.



**Figure 4.17:** Comparison of EPED1.63-predicted pedestal width  $\Delta_\psi$  and height  $\beta_{p,ped}$  with the corresponding ensemble-averaged experimental points, with the KBM scaling  $\Delta_\psi = c\beta_{p,ped}^{1/2}$ . Though the EPED predictions were calculated with a self-consistent treatment of the scale factor  $c$  as a weakly-varying function of plasma parameters, the result is quantitatively similar to the simple fixed scale factor.



Application of the ELM synchronization technique does not significantly alter this result, although the pedestal pressure (i.e.,  $\beta_{p,ped}$ ) is significantly increased in the last 20% of the ELM cycle. Recent re-

**Figure 4.18:** Comparison of ensemble-averaged (black) and ELM-synchronized (Red) pedestal width and height, compared to the KBM constraint. The  $\Delta_\psi = 0.0857\beta_{p,ped}^{1/2}$  scaling found in the ensemble-averaged case is shown in black, while the minor modification of  $\Delta_\psi = 0.0896\beta_{p,ped}^{1/2}$  for the ELM-synced cases is shown in red.

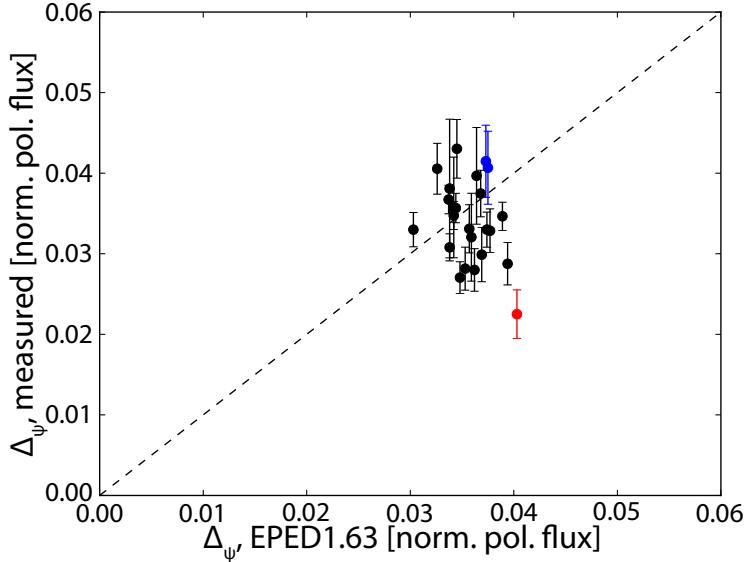


**Figure 4.19:** ELM-synchronized pedestals, with data binned by  $\beta_{p,ped}$  for clarity. The data are fitted by  $\Delta_\psi = (0.0851 \pm 0.003)\beta_{p,ped}^{1/2}$  (black), or by  $\Delta_\psi = (0.0824 \pm 0.015)\beta_{p,ped}^{0.49 \pm 0.11}$  using a more general power law.



search in the inter-ELM development of the pedestal suggests that the KBM saturates early in the ELM cycle, clamping the pedestal to the  $\beta_{p,ped}^{1/2}$  limit – the pedestal is then thought to evolve along this limit until the peeling-balloonning boundary is also reached, triggering the ELM. Observations on DIII-D [31] are consistent with this picture, and with both the pedestal width and height growing at clamped gradient prior to the ELM. Similarly, observations on C-Mod observed a fluctuation consistent with the KBM saturating early in the ELM cycle [32], although the pressure pedestal height appeared to saturate earlier in the ELM cycle [19]. Consistent with this, ELM-synchronized pedestals exhibit wider, higher pedestals on average (see also fig. 4.21 for pedestal widths), with a similar constraint imposed by the KBM compared to the ensemble-averaged result.

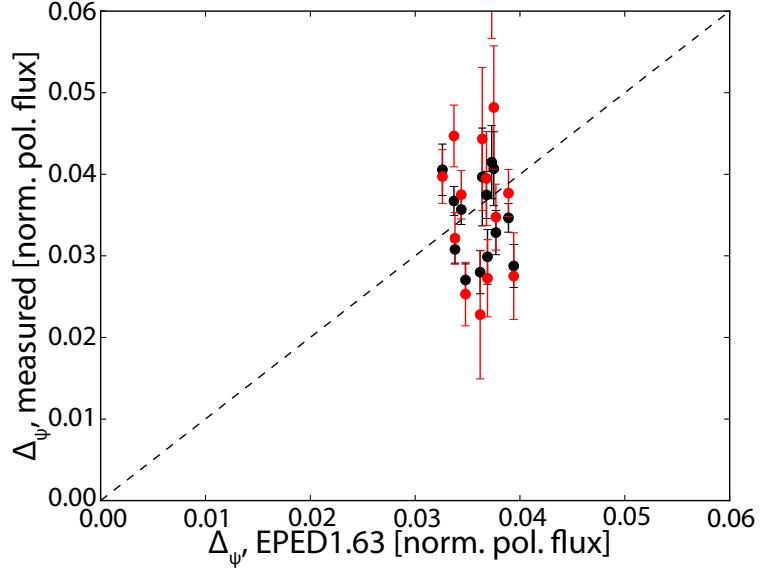
**Figure 4.20:** Measured EPED pedestal width  $\Delta_\psi = (\Delta_{n_e} + \Delta_{T_e})/2$  in ensemble-averaged pedestals versus EPED1.63-predicted pedestal widths. Magnetic-field groups are indicated by color. The dashed line indicates perfect agreement with EPED prediction. Pedestals widths are robust on C-Mod, restricted to  $\sim 2 - 5\%$  of poloidal flux. The EPED model reproduces this trait within expected prediction error.



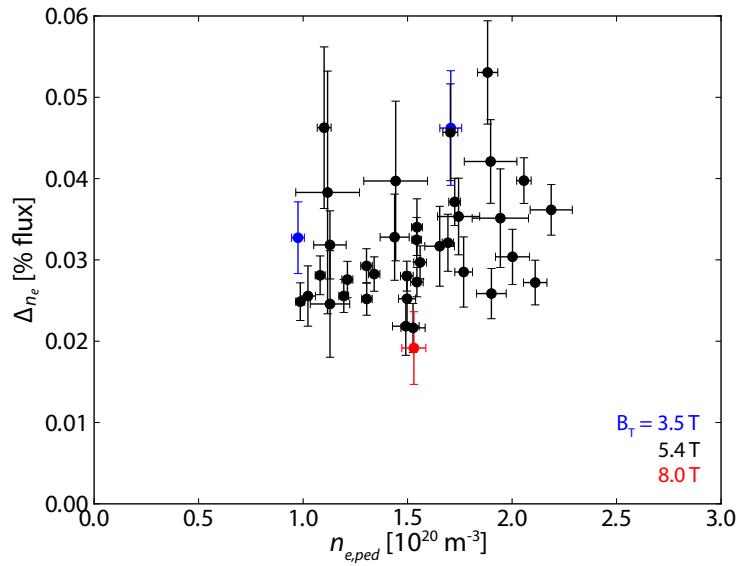
A comparison of the ensemble-averaged and ELM-synced pedestals in  $\Delta_\psi - \beta_{p,ped}$  space is shown in fig. 4.18, with the ELM-synced pedestals fitted to a scale factor  $\langle c \rangle = 0.0896 \pm 0.0034$ . The data may be clarified significantly by taking an error-weighted average within fixed bins in  $\beta_{p,ped}$  as well, shown in fig. 4.19, which tends to reduce the influence of strongly-outlying points on the fit. Again, the fit is quantitatively very similar – the data fit well to  $\Delta_\psi = c\beta_{p,ped}^{1/2}$  with  $\langle c \rangle = 0.0851 \pm 0.003$ . Alternately, we may use a more general power-law fit  $\Delta_\psi = c_1\beta_{p,ped}^{c_2}$ , with which we find  $\langle c_1 \rangle = 0.0824 \pm 0.015$  and  $\langle c_2 \rangle = 0.49 \pm 0.11$ , closely reproducing the  $\beta_{p,ped}^{1/2}$  model. The fitting results are quite consistent across these methods, demonstrating the robustness of the KBM model for the pedestal width and its insensitivity to the details of data preparation.

Prediction of the pedestal width is difficult, given the robust width of the pressure pedestal (typically 3-5% of poloidal flux space, corresponding to  $\sim 5$  mm on C-Mod). The EPED model correctly recovers this robustness (within the expected  $\pm 20\%$  prediction error), as shown in fig. 4.20. As seen in fig. 4.18, ELM-synchronized pedestals are typically somewhat wider than their ensemble-averaged counterparts, commensurate with the increased  $\beta_{p,ped}$  at the maximum of the ELM cycle while the pedestal structure is limited throughout most of the ELM cycle by KBM turbulence. A comparison of the ELM-synced pedestal widths versus EPED1.63 prediction is shown in fig. 4.21.

**Figure 4.21:** Measured pedestal width  $\Delta_\psi$  versus EPED1.63 predicted width. Ensemble-averaged points are shown in black, while corresponding ELM-synchronized points are shown in red. ELM-synced pedestals are typically somewhat wider, although still lie within the  $\pm 20\%$  expected error for EPED.



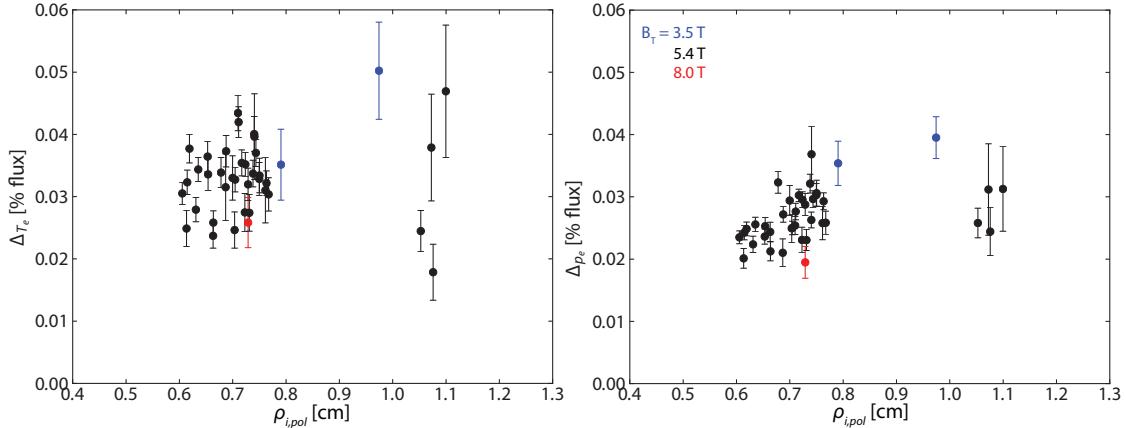
**Figure 4.22:** Density pedestal width versus pedestal density. Contrary to expectations from neutral-penetration models (see section 3.1.2), there is little systematic variation of the density pedestal width and height. This is consistent with the highly opaque SOL typical on C-Mod.



## 4.5 PEDESTAL WIDTH RESPONSE

### 4.5.1 Alternate Width Models

Early models for the pedestal width (see section 3.1) led to several easily-testable predictions – first, neutral-penetration models (section 3.1.2) predict a scaling of the density pedestal  $\Delta_{n_e} \sim 1/n_{e,ped}$ , while transport-driven models predict temperature/pressure pedestal widths limited by poloidal gyroradius, or equivalently the banana orbit width (section 3.1.3). The density pedestal width is shown against pedestal density in fig. 4.22 – while there is high scatter in the data, with both the pedestal density and measured width  $\Delta_{n_e}$  spanning more than a factor of two in variation, the densest region in the dataset shows a



**Figure 4.23:** Temperature and pressure pedestal widths versus poloidal gyroradius. The temperature pedestal width shows no systematic variation with  $\rho_{i,pol}$ . A weak trend is possible in the pressure pedestal width, comparable to the the trend of  $\Delta_p \sim \beta_{p,ped}^{1/2}$  (due to the strong covariance between  $\rho_{i,pol}$  and  $\beta_{p,ped}$ ). However, this trend is overruled in favor of a poloidal beta scaling by other observations.

weak positive trend between density pedestal width and height. This is directly contrary to the predictions from simple neutral-penetration models; however, it is consistent with previous observations in EDA H-mode [30] and with the expectations of high neutral opacity in the SOL on C-Mod, such that neutral penetration in the pedestal is reduced. The measured temperature and pressure widths  $\Delta_{T_e}$  and  $\Delta_{p_e}$  are shown against  $\rho_{i,pol}$  (the ion gyroradius evaluated with the poloidal field) in fig. 4.23. In the case of the temperature pedestal width, no systematic variation with  $\rho_{i,pol}$  is seen. A possible trend for the pressure pedestal width is seen, weaker than the  $\Delta \sim \rho_{i,pol}$  expected from ion-orbit-loss models, with comparable spread to that seen in the pressure pedestal width versus  $\beta_{p,ped}$ . However, as there is significant covariance between  $\rho_{i,pol} \sim \sqrt{T_e}/I_p$  and  $\sqrt{\beta_{p,ped}} \sim \sqrt{n_e T_e}/I_p$ , and the width scaling with  $\beta_{p,ped}$  is seen to be a superior predictor (see fig. 4.11) this model should be disregarded in favor of the  $\Delta \sim \beta_{p,ped}^{1/2}$  scaling from KBM physics. This is consistent with results from experiments designed to distinguish between  $\rho_{i,pol}$  and  $\beta_{p,ped}$  dependencies via isotope variation to exploit the mass dependence in  $\rho_{i,pol}$  [33] or pumping experiments to independently vary pedestal density and temperature at fixed pressure [29, 34].

#### 4.5.2 Normalized Pedestal Width

As detailed in section 4.4.2, the scale factor in the dominant width scaling in ELMY H-mode,  $\Delta \sim \beta_{p,ped}^{1/2}$ , is most properly a weakly varying function of plasma shaping, collisionality, and other dimensionless parameters:  $\Delta_\psi = G(\nu^*, \varepsilon, \dots) \beta_{p,ped}^{1/2}$  [12] (cf. section 3.3). These secondary dependencies in  $G$  may be examined by normalizing the

pedestal width (here we use the EPED width,  $\Delta_\psi$ , from eq. (4.3)) to the fitted scaling  $\Delta_\psi = 0.0857\beta_{p,ped}^{1/2}$  (see fig. 4.16).

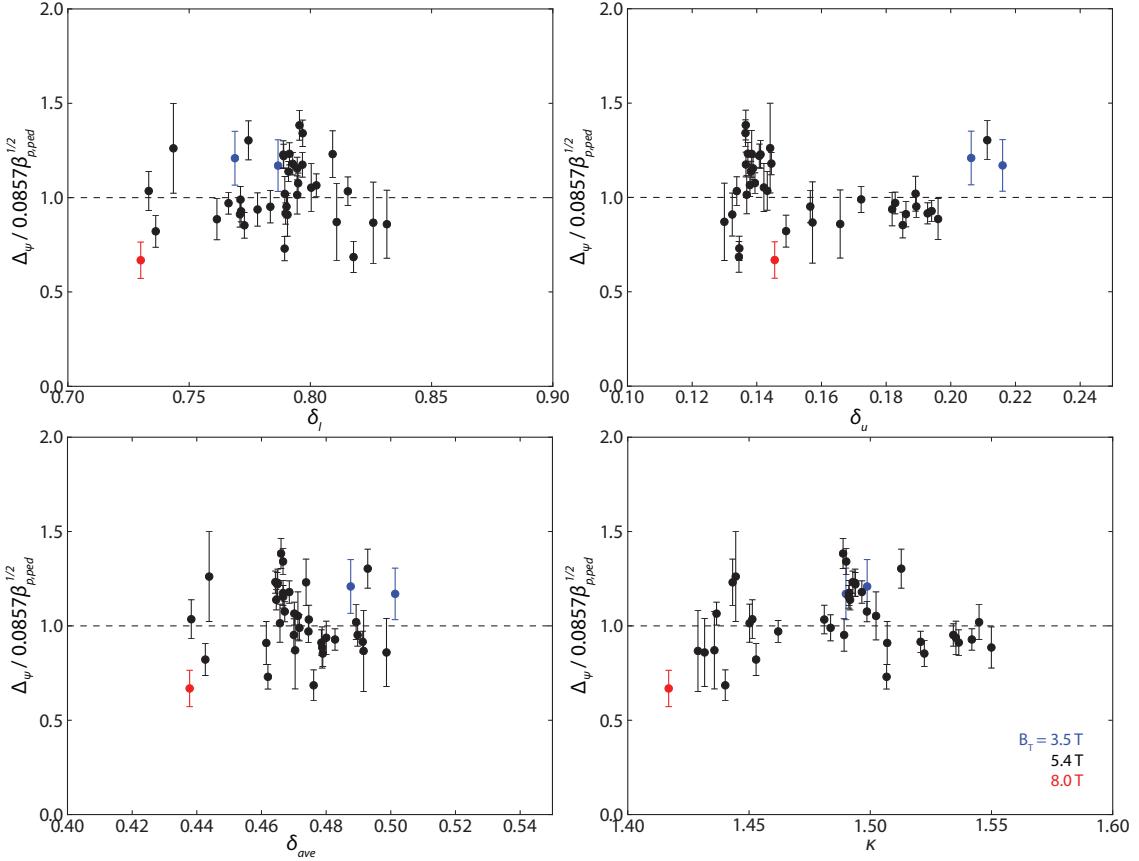
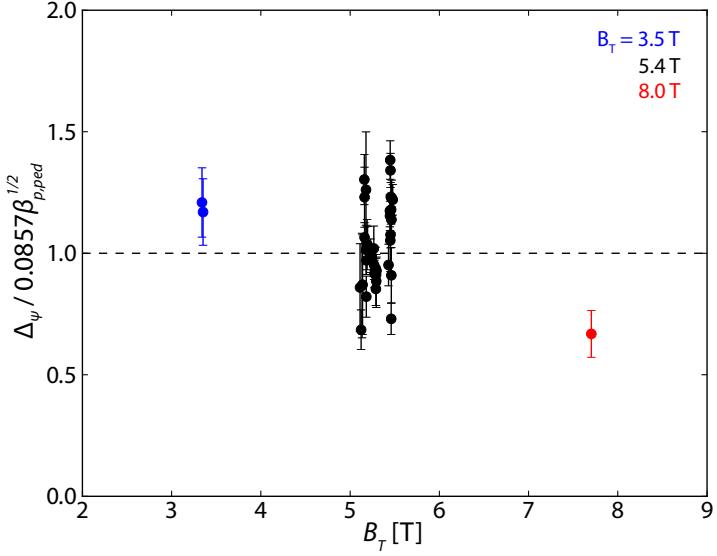
Normalized pedestal widths are shown against the range in toroidal fields in fig. 4.24. The high scatter in the normalized pedestal widths at standard field (5.4 T), along with the difficulty in attaining usable datapoints at low and high field, renders it difficult to conclusively establish a secondary scaling of the pedestal width with toroidal field. The broader pedestal at lower field is qualitatively consistent with modeling efforts [29, 35]; however, the observation of broader pedestals at low current [26] complicates this observation due to the strong co-variance between field and current in the 3.5 T range.

Similarly, normalized pedestal widths are shown against the plasma shaping parameters – upper and lower triangularity  $\delta_u$ ,  $\delta_l$ , average triangularity  $\delta_{ave} = (\delta_l + \delta_u)/2$ , and elongation  $\kappa$  – in fig. 4.25. No clear secondary dependence of the normalized pedestal width (that is, in the scale function  $G(\nu^*, \varepsilon, \dots)$ ) is seen in shaping:  $\delta_l$ ,  $\delta_{ave}$ , and  $\kappa$  exhibit no trend, while  $\delta_u$  is unclear with the broadest widths (compared to the  $\sim 0.0857\beta_{p,ped}^{1/2}$  fit) at both the low and high extremes of the range in  $\delta_u$ . Rather, the shaping dependence manifests as improved MHD stability (increasing the maximum  $\nabla p$ ), such that both the pedestal poloidal beta and width are increased along the KBM-limited curve with stronger shaping. However, as the range in shaping on C-Mod is restricted, secondary dependences of the pedestal width (that is, dependences in  $G$  independent from the  $\Delta_\psi \sim \beta_{p,ped}^{1/2}$  scaling) may go undetected here.

Pedestal collisionality  $\nu_{95}^*$  is anticipated as a controlling term in the scale function  $G$ , due to its influence on bootstrap current density and the accompanying MHD effects in the pedestal. However, across a broad range on collisionality,  $0.25 < \nu_{95}^* < 6$ , no systematic variation in the normalized pedestal width is seen (see fig. 4.26). The highest collisionality points were obtained in cold, low-field discharges, possibly conflating the elevated pedestal width (relative to the  $\sim 0.0857\beta_{p,ped}^{1/2}$  fit) with possible broadening at reduced  $B_T$ .

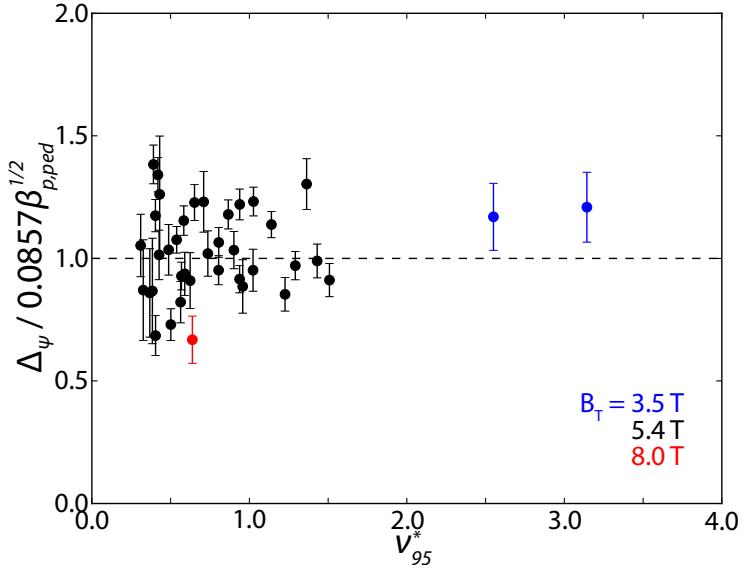
While a primary dependence of the pedestal width on the gyroradius is ruled out (see the discussion in section 4.5.1 and fig. 4.11), a secondary gyroradius dependence in addition to the  $\beta_p$  scaling is still possible – for example,  $\Delta_{ped} \sim \rho_{i,pol}^{0.2} \beta_{p,ped}^{0.5}$  found by Urano *et al.* [33]. However, when the scale function  $G$  is examined via trends of the normalized pedestal width versus normalized gyroradius  $\rho_{95}^*$ , shown in fig. 4.27, no systematic dependence is seen. Notably, the strong outlier for  $\rho^*$  – the high- $B_T$  case, shown to have a narrow pedestal compared to the expected scaling – is nevertheless within the range of normalized width for the bulk of the dataset. As such, no distinct dependence of the normalized width (equivalently,  $G(\nu^*, \varepsilon, \dots)$ ) can be discerned from the data. •

**Figure 4.24:** Scalings of the pedestal width  $\Delta_\psi$ , normalized to the dominant scaling  $\Delta_\psi = 0.0857\beta_{p,ped}^{1/2}$ , with the applied toroidal field  $B_T$ . Although the high scatter at standard  $B_T$  and the sparsity of data at low and high field makes a conclusive scaling difficult, there is some indication of an inverse relation of pedestal width with toroidal field.

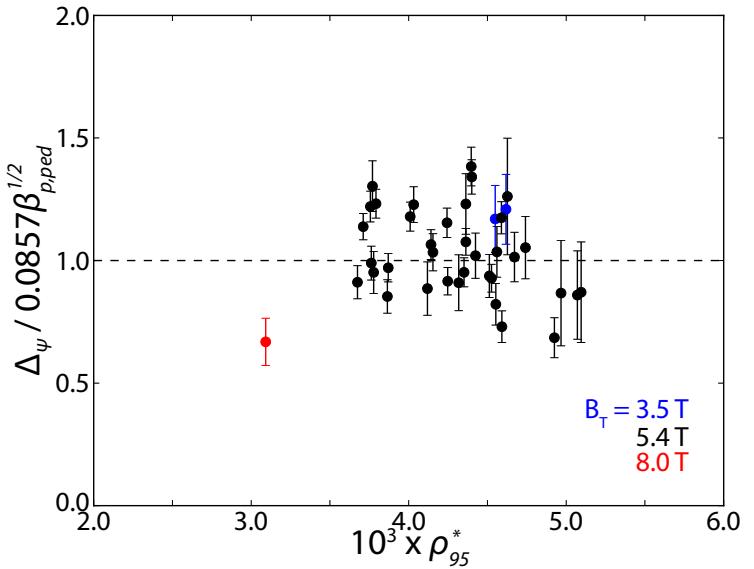


**Figure 4.25:** Scalings of the pedestal width  $\Delta_\psi$  normalized to the dominant scaling  $\Delta_\psi = 0.0857\beta_{p,ped}^{1/2}$  with plasma shaping: upper, lower, and average triangularity ( $\delta_l$ ,  $\delta_u$ ,  $\delta_{ave} = (\delta_u + \delta_l)/2$ ), and elongation  $\kappa$ . No strong trend with shaping parameters is seen – rather, the influence of plasma shaping arises in the improved MHD stability, such that both  $\beta_{p,ped}$  and  $\Delta_\psi$  increase with stronger shaping along the KBM-limited curve.

**Figure 4.26:** Scaling of the normalized pedestal width  $\Delta_\psi / 0.0857 \beta_{p,ped}^{1/2}$  versus pedestal collisionality  $\nu_{95}^*$ . Low, standard, and high-field sets are indicated in blue, black, and red respectively. No systematic variation is observed.



**Figure 4.27:** Scaling of the normalized pedestal width  $\Delta_\psi / 0.0857 \beta_{p,ped}^{1/2}$  with normalized pedestal gyroradius  $\rho_{95}^*$ . Low, standard, and high-field sets are indicated in blue, black, and red respectively. No systematic variation is seen.



#### 4.6 CONCLUSIONS

ELMy H-mode experiments on C-Mod reach the highest magnetic field and pedestal thermal pressure of any tokamak, reaching within a factor of  $\sim 2$  of the target pressure for ITER (see fig. 4.28). As part of a DOE Joint Research Target [9], these experiments tested the EPED model series [11] for ELMy H-mode pedestal width and height, greatly expanding the parameter space in which the model has been implemented [18], driving the development of the model to better handle high collisionality (through the implementation of corrections to the diamagnetic-stabilization model in EPED1.63) and magnetic field. The newest version of EPED, EPED1.63 (a minor modification to EPED1.6 to account for strong diamagnetic effects on C-

**Figure 4.28:** EPED predictions versus measured pressure pedestal heights from DIII-D and C-Mod, spanning a significant range of pedestal pressures. Notably, C-Mod pressure pedestals reach within a factor of  $\sim 2$  of the predicted ITER pedestal height. Reproduced from [19]



Mod) accurately predicts the pressure pedestal height, particularly when pedestal data is masked to time frames immediately preceding ELM crashes – a practice that, despite diagnostic difficulties on C-Mod, produces data most closely corresponding to the pedestal structure at the point of ELM instability. Although systematic prediction of the pedestal width on C-Mod is difficult due to the narrow range over which it varies, the EPED prediction for  $\Delta_\psi$  matches experimental results to within the expected  $\sim 20\%$  error.

The pedestal width is well-described by the prediction used by EPED1.6 based on the KBM,  $\Delta_\psi = G(\nu^*, \varepsilon, \dots) \beta_{p,ped}^{1/2}$ , where  $G(\nu^*, \varepsilon, \dots)$  is a weakly varying function,  $G \approx .0857$  – matching the fitted result from multiple machines [9]. Secondary scalings of the pedestal width, discerned by normalizing the pedestal width to the dominant  $\beta_{p,ped}$  dependence, with magnetic field,  $\nu^*$ ,  $\rho^*$ , and shaping parameters are minimal over the available range in the data set. Conversely, the pedestal width is not well-described by alternate models not based on the KBM-driven  $\beta_{p,ped}$  dependence: the density pedestal width does not exhibit a  $\Delta_{n_e} \sim n_{e,ped}$  trend expected from neutral-penetration models, while the temperature and pressure pedestals do not scale clearly with  $\rho_{i,pol}$ . The temperature pedestal width shows no trend with poloidal gyroradius, while the pressure pedestal does not show a trend independent of the  $\beta_{p,ped}$  scaling ( $\rho_{i,pol}$  and  $\beta_{p,ped}$  are difficult to discern from one another without careful operational control).

Examined over a broad range in plasma current, the pressure pedestal height exhibits a trend  $p_{ped} \sim I_p$ , while the pressure pedestal width trends as  $\Delta_{p_e} \sim I_p^{-1}$ , although there is significant scatter in both trends. This suggests the expected trend of  $\nabla p_{ped} \sim I_p^2$  from ballooning MHD stability. More carefully, the pedestal height is well-predicted by  $p_{ped} \sim \nabla p \times \Delta_p$  – taking  $\nabla p \sim I_p^2$  from MHD stabil-

ity and the pedestal width  $\Delta_p \sim \beta_{p,ped}^{1/2} \sim \sqrt{n_{e,ped} T_{e,ped}} / I_p$  gives  $p_{ped} \sim I_p \sqrt{n_{e,ped} T_{e,ped}}$  (see fig. 4.11), which matches the observed pressure pedestal height quite well. Due to the interplay between the gradient, width, and height of the pedestal, such a treatment is necessary to accurately capture the pedestal structure. Notably, over the restricted shaping range available on C-Mod for ELM My H-mode both  $\beta_{p,ped}$  and  $\Delta_\psi$  vary little, such that to lowest order the width is robust, with the pressure pedestal height and gradient both scaling as  $I_p^2$  (equivalently, that the pedestal is limited in attainable  $\beta_{p,ped}$ ).

The results shown in this chapter firmly establish that the pedestal in ELM My H-modes on C-Mod are limited by the physics assumed in the EPED model – namely, peeling-balloonning MHD modes and kinetic-balloonning turbulence. The ELM behavior and pedestal dynamics observed here are of the familiar kind, characteristic of type-I ELMs on larger devices. This places C-Mod on a common physics footing with other machines, and indicates that the approach used in EPED can, with reasonable confidence, be extrapolated to ITER operation. The empirical and computational tests demonstrated in this chapter may also be meaningfully applied to examine the structure and limiting physics of I-mode, shown in chapters 5 and 6. ★



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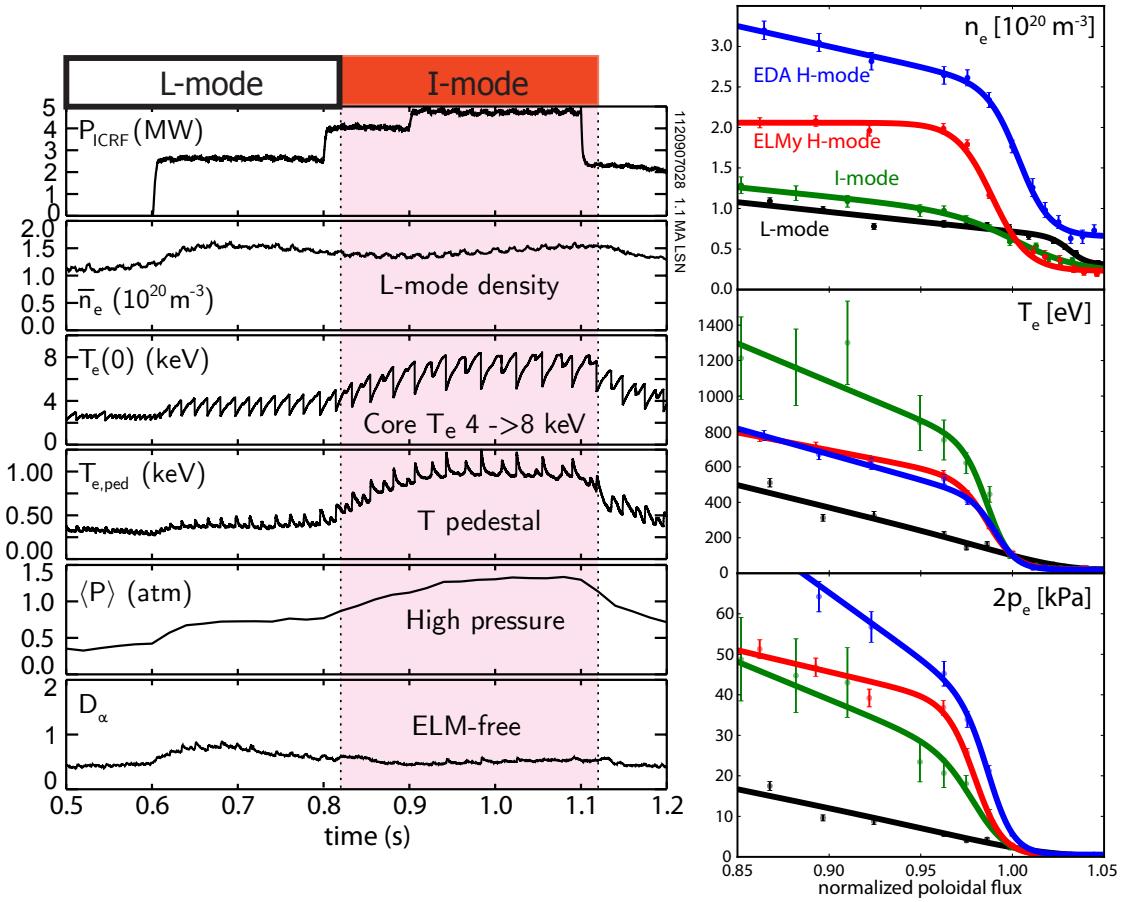
I-MODE PEDESTAL SCALINGS & CONFINEMENT

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The I-mode [1, 2, 3, 4, 5], introduced in section 2.4, is a novel high-performance regime pioneered on Alcator C-Mod. I-mode is unique in that it appears to decouple energy and particle transport, forming a steep temperature pedestal with H-mode levels of energy confinement without the accompanying density pedestal or suppression of particle transport found in conventional H-modes (see fig. 5.1). I-mode exhibits several highly attractive properties for a putative reactor regime:

1. Due to the lack of particle transport suppression (as is found in H-modes), the I-mode retains L-mode-like impurity confinement times, avoiding the accumulation of deleterious impurities in the plasma, including those from high-Z metal plasma-facing components necessary for reactor operation [6]. This enables stationary operation without the need for ELMs or continuous fluctuations in the edge to provide the necessary relaxation of the particle confinement.
2. I-mode appears to be naturally stable against large ELMs, avoiding excessive pulsed heat loading to plasma-facing components without externally-applied engineering controls (described in section 2.1.3).
3. Energy confinement in I-mode appears to exhibit little to no degradation with input heating power, in contrast to that found in ELMy H-mode ( $\tau_E \sim P^{-0.7}$  from the ITER98y2 analysis [7]), scaling quite favorably to reactor-scale devices where fusion self-heating dominates.

A firm understanding of the pedestal is essential for the extrapolation of any high-performance regime to ITER- and reactor-scale devices. The pedestal height sets a strong constraint on core temperature and pressure – and therefore overall fusion performance – both by acting as a boundary condition for the plasma profiles, and by supporting steeper core temperature gradients due to profile stiffness [8, 9]. Moreover, the pedestal structure, particularly the steep gradients in density, temperature, and/or pressure, determines stability of the plasma against large, deleterious ELMs (see section 3.2). In this chapter, we present empirical observations of the pedestal in I-mode from a recent series of dedicated experiments [10], with a focus on high-resolution pedestal profile measurements across a range of plasma parameters. Through this, we examine trends in I-mode



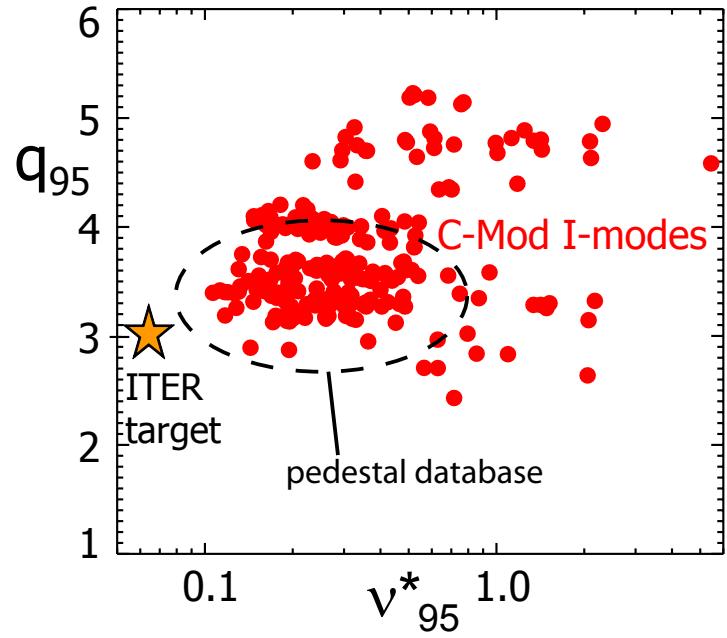
**Figure 5.1:** (left) Characteristic traces for a typical I-mode. At the L-I transition, the core and edge temperature rise over several sawtooth cycles before reaching a steady level; global confinement and pressure rise accordingly. However, the density remains at L-mode levels, and no ELMs are exhibited. (right) Edge profiles for density, temperature, and pressure in L-, I-, and H-mode. The I-mode (green) retains an density profile comparable to the L-mode (black), unlike the ELMy (red) and EDA (blue) H-modes which form a strong density pedestal. However, the I-mode forms a higher temperature pedestal than either H-mode. As a result, the I-mode reaches comparable pedestal pressures to the H-modes while retaining L-mode particle transport. (repeated from fig. 2.7)

pedestal behavior, and their impact on global behavior and performance in I-mode, and possible extrapolations to larger devices. •

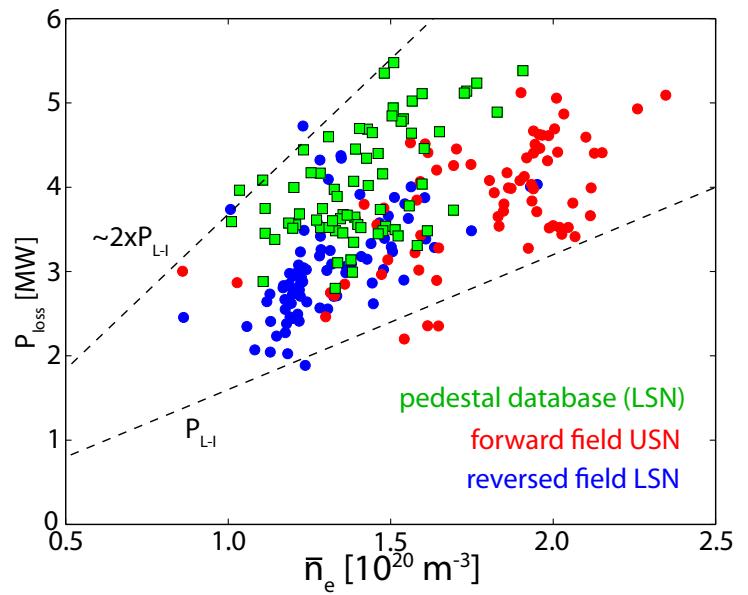
## 5.1 ACCESS AND EXPERIMENTAL SETUP

All data presented here was taken on the Alcator C-Mod tokamak, described in section 1.3. As described in section 2.4.1, I-mode access hinges primarily on operation with the ion  $\nabla B$  drift (eq. (1.21)) directed away from the primary X-point in the plasma (the “unfavorable  $\nabla B$  drift” configuration). Within this requirement, though, I-mode access is fairly robust, with steady I-modes sustained in a variety of shapes – both USN with standard field, and LSN shapes with reversed field to achieve the desired  $\nabla B$  drift direction (in the latter case, the plasma current is reversed as well to preserve field helic-

**Figure 5.2:** Range in edge collisionality  $\nu_{95}^*$  and  $q_{95}$  over which I-modes have been accessed. Notably, I-mode operation is naturally favored near ITER targets for these parameters. The subset of this data prepared with high-resolution pedestal profiles, herein termed the “pedestal database”, is also highlighted.



**Figure 5.3:** Line-averaged density and loss power range for USN and LSN I-modes, illustrating  $\sim 2 \times P_{L-I}$  range for I-mode access. USN shapes are forward-field and LSN-shapes are reversed field, such that all I-modes shown are in the unfavorable drift configuration. Data from the high-resolution pedestal database (all are LSN reversed-field) are highlighted.



ity) – and edge-current profiles, and at low-to-moderate collisionality (eq. (2.3)). The attained range in  $q_{95}$  and  $\nu_{95}^*$  is shown in fig. 5.2. I-mode has been sustained with heating power up to  $\sim 2 \times$  the L-I transition threshold power, which tends to increase approximately linearly with density (see fig. 5.3), above which the plasma typically enters an ELM-free H-mode (recall that operating with unfavorable  $\nabla B$  drift elevates the H-mode threshold power by roughly a factor of two [11, 12, 13]).

I-mode experiments in the 2012 run campaign have focused on reversed-field LSN plasmas, which exhibit the widest access window and avoid difficulties with power handling and edge diagnostics. A subset of results from these experiments have been prepared with high-resolution pedestal measurements, optimized for analysis of the I-mode pedestal structure both from an empirical standpoint and for a computational approach to the pedestal stability; these data, herein termed the “pedestal database” (parameter range highlighted in fig. 5.2) is stored in an SQL database (see appendix B) for easy access and analysis, and will be used for the bulk of the I-mode work in this thesis (chapters 5 and 6). •

## 5.2 PEDESTAL RESPONSES

To understand the physics of the I-mode pedestal, it is useful to compare the I-mode to established scalings for baseline H-modes. For the purposes of this discussion, we distinguish between the *MHD-limited* pedestals found in ELMy H-mode (see section 2.1) and the *transport-limited* pedestals in EDA H-mode (see section 2.3.2). The pedestal structure in the MHD-limited case is determined by peeling-balloonning stability, described in section 3.2 – this manifests predominantly as a limit on the pressure gradient due to the instability drive for the ballooning mode,  $\alpha_{MHD}$  (see eqs. (2.8) and (2.9)). This scales as  $\alpha_{MHD} \sim \nabla p / B_p^2$ , consistent with the observed  $\nabla p \sim I_p^2$  dependence observed in experiments [14, 15] (cf. chapter 4). To lowest-order approximation, this sets a limit on the pedestal poloidal beta, such that for a given current, field, and shaping configuration the pedestal pressure  $p \sim n_e T_e$  is fixed. Altering the density via fueling results in heating or cooling the pedestal to maintain this limit, while attempts to modify the pedestal via heating power alters the energy transport (increasing the ELM frequency  $f_{ELM} \sim P$  for large type-I ELMs [16]). In transport-limited EDA H-mode pedestals, on the other hand, the pedestal is controlled in part by the interplay between the strong particle pinch and the continuous outward particle transport driven by the QCM, such that the density tends to lock to a value set by the plasma current. Within this limit, the pedestal temperature (and therefore pressure) responds positively to increased heating power [17].

**Figure 5.4:** Pedestal temperature versus plasma current for I-mode and ELM My H-mode. I-mode temperature pedestals meet or exceed H-mode levels, and trend positively with current. The spread in  $T_{e,95}$  at a given current point is due to varying power per particle (see fig. 5.5). The highest-current I-modes exhibit temperatures below the bulk trend due to low values of  $P_{\text{net}}/\bar{n}_e$ , as these I-modes were fueled to relatively high densities.



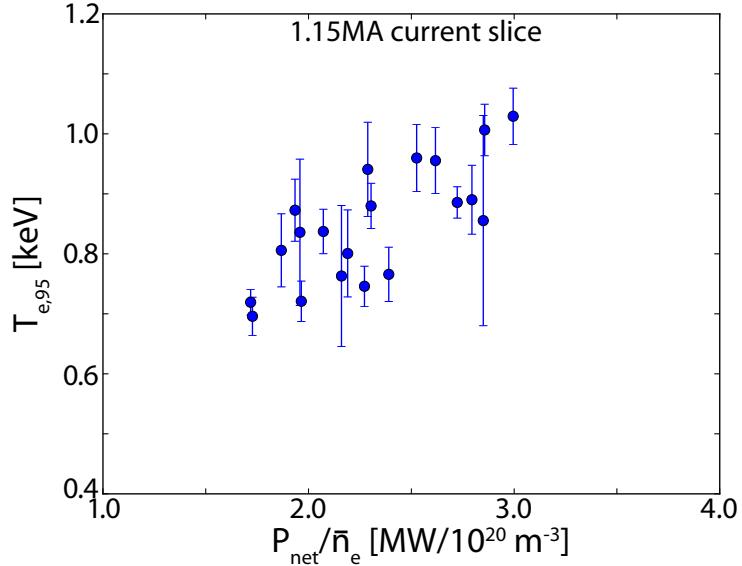
### 5.2.1 Pedestal Temperature

As the I-mode is characterized, in part, by its H-mode-like temperature pedestal and energy confinement, that is a suitable place to begin an examination of the I-mode pedestal. A scan of plasma current from 0.85 to 1.35 MA reveals a positive trend of the pedestal temperature with plasma current, shown in fig. 5.4 with ELM My H-modes for comparison. The I-mode temperature pedestal meets or exceeds the pedestal  $T_e$  found in H-modes. This is highly beneficial for global performance, as the high temperature pedestal coupled with stiff core temperature profiles supports very high (up to 8 keV) core temperatures – with moderately peaked core density profiles, this supports comparable core pressures and fusion reaction rates to H-mode despite the reduced pedestal pressure (see section 5.2.3).

There is, however, significant scatter at a given point in the  $I_p$  scan, due to variation in the input heating power. Examining a single current slice at 1.15 MA, shown in fig. 5.5, we see a strong dependence of the temperature pedestal height on the net heating power (eq. (1.29)), normalized to (line-averaged) density – effectively, the input power per particle. This same pattern is observed at other current points. The comparatively suppressed temperatures at the highest-current I-modes is a result of the higher fueling at these points, resulting in lower values of  $P_{\text{net}}/\bar{n}_e$ . I-modes in these experiments were typically fueled to densities corresponding to Greenwald fractions (eq. (2.4))  $0.15 \leq f_{Gr} \leq 0.26$ , with the highest-current points at  $f_{Gr} \sim 0.2$ , or  $1.8 \times 10^{20} \text{ m}^{-3}$ .

The temperature pedestal response in I-mode to plasma current is comparable to that seen in the density, temperature, and pressure pedestals in ELM My H-mode (*cf.* fig. 4.9), although the sensitivity of the

**Figure 5.5:** Pedestal temperature  $T_{e,95}$  vs. heating power per particle ( $P_{\text{net}}/\bar{n}_e$ ) for the 1.15 MA current slice, illustrating the approximately-linear trend in temperature at fixed current. This behavior is highly beneficial as an external control for the pedestal temperature.

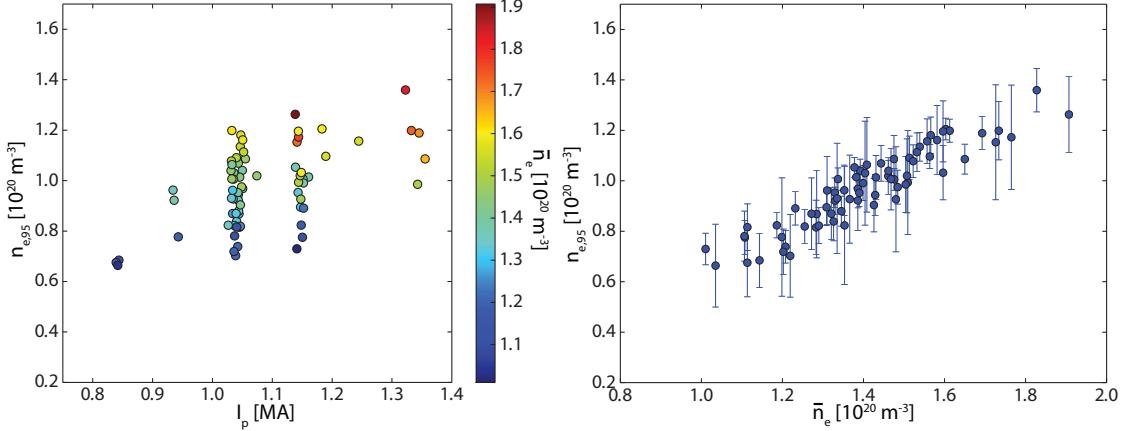


temperature pedestal in ELM My H-mode is somewhat weaker than in I-mode. The response of the temperature pedestal to heating power is notable: the temperature in ELM My H-mode pedestals is only weakly dependent on power – rather, increased heating power increases the ELM frequency and energy transport to maintain the approximately  $\beta_p$ -limited pedestal (*cf.* figs. 2.2 and 4.12). Transport-limited EDA H-mode pedestals exhibit a similar trend, given as  $T_{e,\text{ped}} \sim (P_{\text{net}}/\bar{n}_e)^{0.5 \pm 0.1}$  in [17] and  $T_{e,\text{ped}} \sim (P_{\text{net}}/\bar{n}_{e,L})^{0.7 \pm 0.1}$  in [18], with the I-mode pedestal responding at least as strongly – this suggests that I-mode pedestals are not stability-limited.

### 5.2.2 Pedestal Response to Fueling

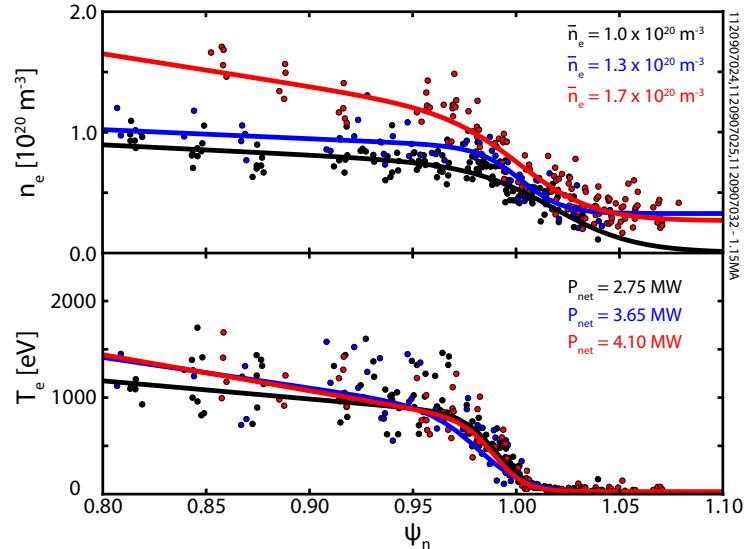
In contrast to the temperature pedestal (section 5.2.1), the edge density in I-mode exhibits markedly different behavior compared to conventional H-modes. Edge density is set primarily through operator fueling control via gas puffing, maintaining an L-mode-like density profile without the density pedestal found in H-mode. The pedestal response to fueling is shown at right in fig. 5.6. Compared to transport-limited EDA pedestals, the plasma current is insufficient as a predictor of I-mode pedestal density, with the positive trend (shown at left in fig. 5.6) due to the strong co-variance between  $I_p$  and  $\bar{n}_e$ .

Given sufficient heating power, temperature pedestals can be maintained with increased density due to the strong response of  $T_{e,95}$  to power-per-particle. Example discharges matched in current, field, and shaping are shown in fig. 5.7, spanning a range in fueling and heating power,  $\bar{n}_e = 1.0 - 1.7 \times 10^{20} \text{ m}^{-3}$ ,  $P_{\text{net}} = 2.75 - 4.10 \text{ MW}$ . Temperature pedestals are matched across all three discharges, using consistent power-per-particle  $P_{\text{net}}/\bar{n}_e = 2.4 - 2.7 \text{ MW}/10^{20} \text{ m}^{-3}$ .



**Figure 5.6:** Pedestal density as a function of current (left, colored by  $\bar{n}_e$ ) and line-averaged density (right). The pedestal density is set solely by operator fueling; in contrast the transport-limited pedestals in EDA H-mode, plasma current is a poor predictor of the pedestal density, with the trend due only to the co-variance between  $I_p$  and  $\bar{n}_e$ .

**Figure 5.7:** Density and temperature pedestals at matched current, field, and shaping, with varying fueling and heating power levels. The three discharges are fueled to  $\bar{n}_e$  of 1.0 (black), 1.3 (blue), and  $1.7 \times 10^{20} \text{ m}^{-3}$  (red) respectively, with heating powers of 2.75, 3.65, and 4.10 MW to maintain matched  $P_{\text{net}}/\bar{n}_e \sim 2.4 - 2.7$ . The constant power-per-particle maintains matched temperature pedestals across the fueling range, indicative of the independent control of pedestal  $n_e$  and  $T_e$  available in I-mode.

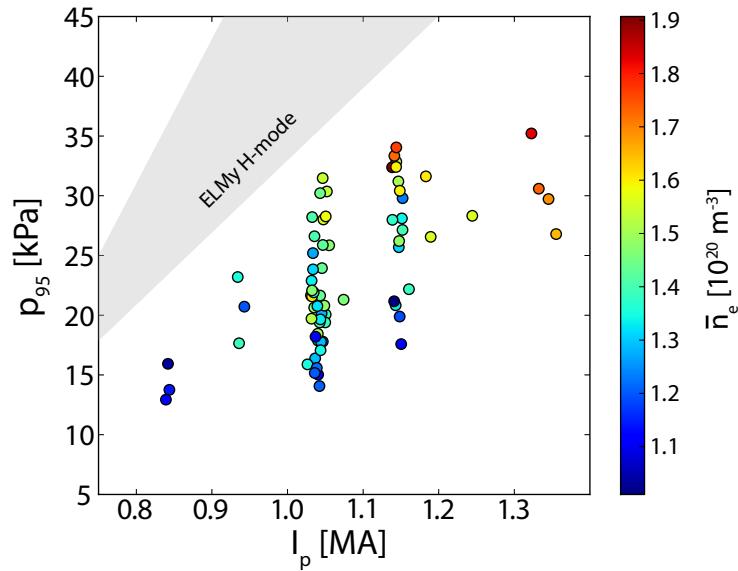


This behavior is distinct from that found in H-modes on C-Mod. ELMy H-modes at fixed current and shaping exhibit an inverse relationship between pedestal  $n_e$  and  $T_e$  due to limited pedestal  $\beta_p$ , such that increased fueling tends to cool the pedestal (although the modification of pedestal collisionality also modifies the ELM character). EDA H-modes lack the fueling control found in I-mode, instead railing the pedestal density to a value set by the plasma current, such that the outward transport and strong inward particle pinch are balanced. The largely-decoupled behavior of the density and temperature profiles in the edge in I-mode are highly desirable from an operational standpoint – fueling (done entirely via edge gas puffing on C-Mod) and heating power are separated as “knobs” for plasma and

pedestal control, granting significant operational freedom compared to the relatively-constrained H-mode pedestal behavior.

The phenomenon demonstrated in fig. 5.7 is indicative of a path to strongly improved performance in I-mode, increasing pedestal  $\beta_p$  and global confinement via matched increases in fueling and heating power, maintaining the target temperature pedestal with appropriate levels of  $P_{net}/\bar{n}_e$ . Recent experiments on C-Mod [19] have successfully applied this approach, reaching elevated density by fueling into an established I-mode in combination with increased heating power levels, reaching heating power levels that would trigger a transition to H-mode in a comparable-density L-mode. This L-mode-like density profile is also of great benefit for operation on ITER-scale devices – due to the high edge density (both observed on C-Mod, and expected for ITER) neutral penetration into the pedestal is expected to be very low. The strong inward turbulent particle pinch [20] in L-mode (and equivalently, I-mode) density profiles is highly desirable for core fueling, as neutral puffing alone is unlikely to be sufficient for core fueling on ITER.

**Figure 5.8:** Pedestal thermal pressure ( $2 \times p_{e,95}$ ) versus plasma current, colored by fueling level indicated by line-averaged density  $\bar{n}_e$ . The shaded region indicates the typical range of pedestal pressures in C-Mod ELMy H-modes. A strong, roughly  $p_{95} \sim I_p$  trend in pedestal pressure is observed. At a given current, a strong increase in pedestal pressure with fueling is also observed (note: heating power also varied in these discharges).



### 5.2.3 Pressure Pedestal Scalings and Performance

Despite lacking a density pedestal, I-mode is capable of reaching pedestal thermal pressures comparable to H-mode, while maintaining favorable behavior in its particle (particularly impurities – see fig. 2.8) transport and temperature pedestal. I-mode pedestal pressure (we use twice the electron pressure from Thomson Scattering here, consistent with  $T_i \approx T_e$  measurements in well-equilibrated pedestals on C-Mod [2] and with the relatively low impurity contribution to the pressure,  $Z_{eff} \sim 2$ ) versus plasma current is shown in fig. 5.8, with ad-

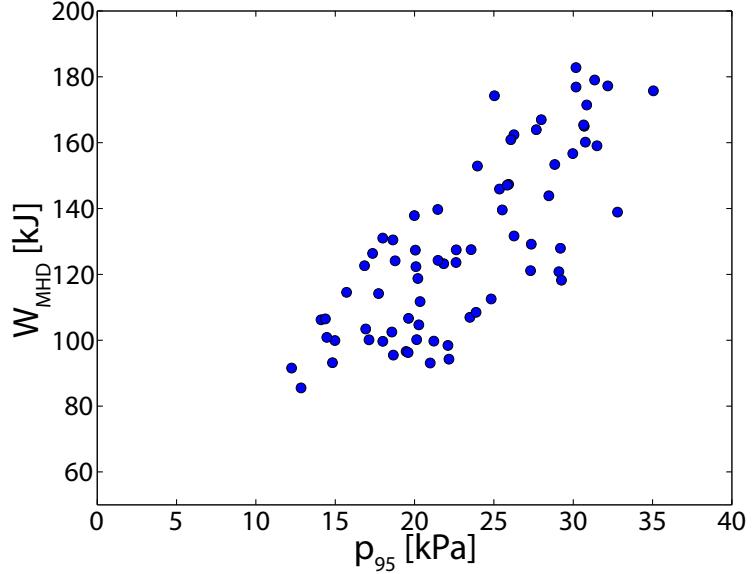
**Figure 5.9:** Pedestal pressure ( $2 \times p_{e,95}$ ) versus net heating power for the 1.15 MA current slice, illustrating the trend  $p_{95} \sim P_{\text{net}}$  at fixed current. This is consistent with the power trend in the I-mode temperature pedestal,  $T_{e,95} \sim P_{\text{net}}/\bar{n}_e$ .



ditional differentiation by fueling level indicated by color. An increase in pedestal pressure by at least  $p_{95} \sim I_p$  is observed, consistent with the scaling of the temperature pedestal  $T_e \sim I_p$ . The pedestal pressure at a given current is seen to increase strongly with increased fueling, consistent with the maintenance of the temperature pedestal with increased heating power and matched fueling, thus constant levels of  $P_{\text{net}}/\bar{n}_e$ . I-mode pedestal pressure is reduced from that typically found in H-mode (the typical range in ELMy H-mode is indicated by the shaded region in fig. 5.8). This is due to the reduced pedestal density in I-mode compared to H-mode, as the temperature pedestals found in I-mode typically meet or exceed H-mode levels. The pressure pedestal is expected to be ultimately limited by the ELM trigger – however, the independent density and temperature pedestal control should allow I-mode to approach, but not exceed, the ELMing limit.

The effect of heating power on the pressure pedestal is visible in fig. 5.9, showing the 1.15 MA current slice (see fig. 5.5 for the same). At fixed current, the pressure pedestal scales as  $p_{95} \sim P_{\text{net}}$ , consistent with the previously observed  $T_{e,95} \sim P_{\text{net}}/\bar{n}_e$  trend in the temperature pedestal as  $p_{95} \sim n_{e,95} T_{e,95}$ . This corresponds the favorable scaling of energy confinement in I-mode with heating power – plasma stored energy is set by heating power and the energy confinement time,  $W \sim P\tau_E$ , and is strongly influenced by the pedestal pressure (see fig. 5.10). Thus, the trend  $p_{95} \sim P_{\text{net}}$  is consistent with little or no degradation of  $\tau_E$  with heating power, which has been observed in global measurements of I-mode [1, 21], and is distinct from the trend  $\tau_E \sim P^{-0.7}$  found for ELMy H-modes [7]. This behavior is quite favorable when scaled to large, high-power machines, particularly in scenarios with a significant degree of fusion self-heating, where the

**Figure 5.10:** I-mode stored energy versus pedestal pressure, confirming the strong dependence of global performance on the pedestal height.



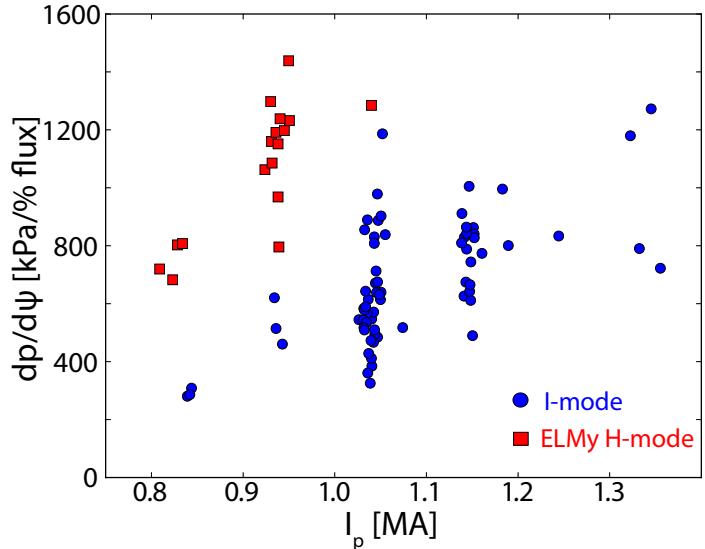
plasma pressure directly determines heating power via the fusion reaction rate ( $\sim p^2$ ).

Trends in the pressure pedestal in I-mode are also informative to its MHD stability. As shown in fig. 5.11, the peak pressure gradient (identified as the driver for ballooning MHD instabilities, described in section 3.2.1, and the trigger for large ELMs) in I-mode is consistently shallower at a given  $I_p$  than comparable ELMMy H-modes on C-Mod, due to the flat edge density profile. Moreover, the pedestal pressure gradient scales more weakly than the expected  $\nabla p \sim I_p^2$  expected from the ballooning stability boundary [22]. The intuitive conclusion from this is that I-mode is generally stable to the MHD instabilities identified with the ELM trigger – the MHD stability and ELM behavior of I-mode is explored in detail in chapter 6. •

### 5.3 PEDESTAL WIDTHS

Conventionally, H-mode pedestals are found to be constrained by critical-gradient-driven instabilities, such that the peak  $\nabla p$  is limited – therefore, the width of the transport barrier sets a constraint on the attainable pedestal height (and thus global performance). Due to the small spatial scales inherent in the pedestal, accurate measurement of the pedestal width has historically been quite difficult, although a number of theoretical models have been proposed and tested against experimental observations, e.g., [23, 24, 25]. This section explores a range of potential explanations for the observed pedestal widths in I-mode.

**Figure 5.11:** Peak pressure gradient (measured at the pedestal midpoint) versus plasma current for I-mode and ELMy H-mode. I-mode consistently exhibits a weaker pressure gradient at a given current, as well as scaling more weakly than the  $\nabla p \sim I_p^2$  expected from the ballooning MHD stability limits associated with ELMy H-mode.



### 5.3.1 Kinetic-Ballooning Limited Pedestals

The kinetic-ballooning mode (KBM), described in section 3.3, applies a constraint to the pedestal width of the form  $\Delta \sim \beta_{p,ped}^{1/2}$ , where  $\Delta$  is the pedestal width in normalized poloidal flux. This trend has been observed on several machines [15, 24, 26], including on C-Mod (see chapter 4). This constraint is used in the EPED model series, described in section 3.4. The simplest implementation of the constraint, used in EPED1 (section 3.4.1) uses a fitted coefficient,  $\Delta = 0.076\beta_{p,ped}^{1/2}$  [27]. A comparison of I-mode pedestals against this predictive line, as well as example ELMy H-modes, is shown in fig. 5.12. I-mode pedestals are wider on average than predicted by the KBM-limited ( $\sim \beta_{p,ped}^{1/2}$ ) line, and show no trend of pedestal width with poloidal beta. This suggests that the I-mode pedestal is not constrained by KBM turbulence, consistent with the relaxed pressure gradient found in I-mode – stability against the KBM is examined in more detail in section 6.2.

### 5.3.2 Local Physics Parameters

While the constraint on the pressure pedestal from kinetic-ballooning turbulence has been the most successful in capturing the limiting physics in ELMy H-modes, a number of other theories (see section 3.1) based on localized physics in the edge have been proposed, with testable trends in the pedestal width. Of particular note are models based on a trend in poloidal gyroradius, described in section 3.1.3, operating on the assumption that ion orbit loss in the plasma edge drives the radial electric field responsible for the pedestal formation – thus the size scale of the ion orbit sets the pedestal width. Some ex-

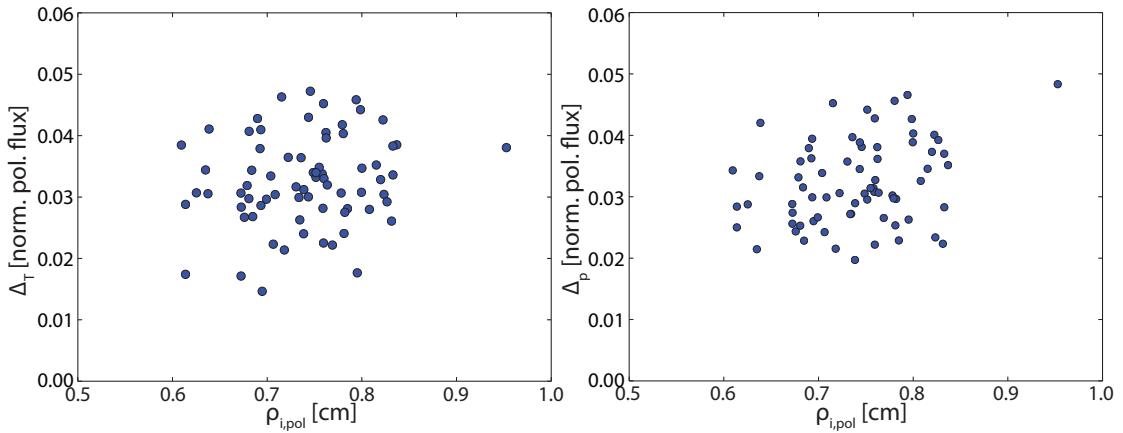
**Figure 5.12:** Pedestal width versus poloidal beta in I-mode and ELMy H-mode. ELMy H-modes lie on the  $\Delta\psi \sim \beta_{p,ped}^{1/2}$  line predicted for KBM-limited pedestals (see section 4.4.2). I-mode shows no scaling of the pedestal width with  $\beta_p$ , and exhibits pedestals consistently wider than predicted for comparable ELM-limited pedestals.



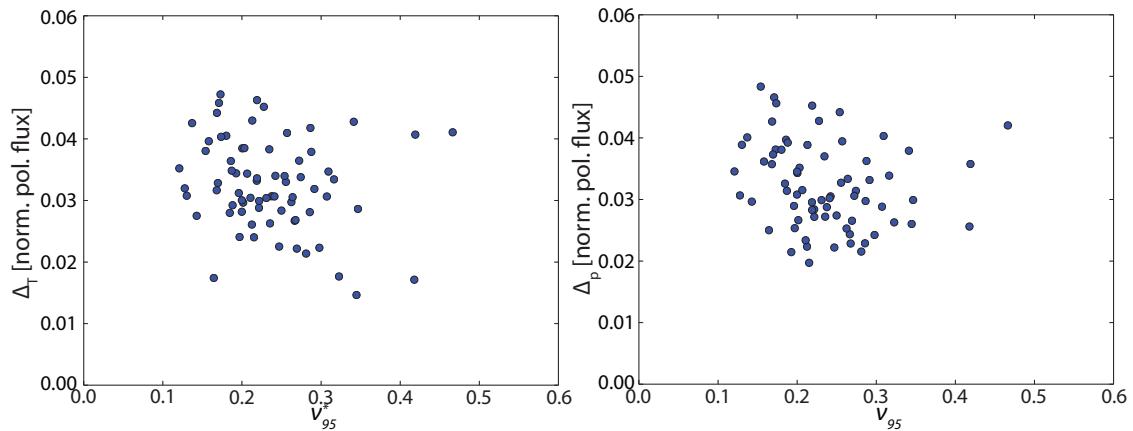
perimental observations correlate well to these predictions, although these may be largely incidental due to the strong covariance between  $\rho_{i,pol}$  and  $\beta_{p,ped}$ , and have been discounted by dedicated experiments distinguishing the two. However, as the KBM does not appear to limit the I-mode pedestal (see section 5.3.1) gyroradius scalings remain an open possibility. Electron temperature and pressure pedestal widths are shown against  $\rho_{i,pol}$  in fig. 5.13. Both pedestal widths appear quite insensitive to the gyroradius, although due to the correlation between  $T_e$  and  $I_p$  the range in  $\rho_{i,pol}$  is rather limited.

Similarly, the temperature and pressure pedestal widths are shown against pedestal collisionality  $v_{95}^*$  and edge safety factor  $q_{95}$  in fig. 5.14 and fig. 5.15, respectively. The collisionality may be expected to influence the pedestal width by controlling the bootstrap current in the edge, which enters into the peeling-balloonning MHD stability boundary (see section 3.2). The safety factor is directly tied to the magnetic shear, which is locally stabilizing to MHD modes in the edge. However, as the I-mode pedestal appears to be strongly MHD-stable, as is shown in chapter 6, these should have a minimal effect. In figs. 5.14 and 5.15, no correlation between the pedestal width and either parameter is evident.

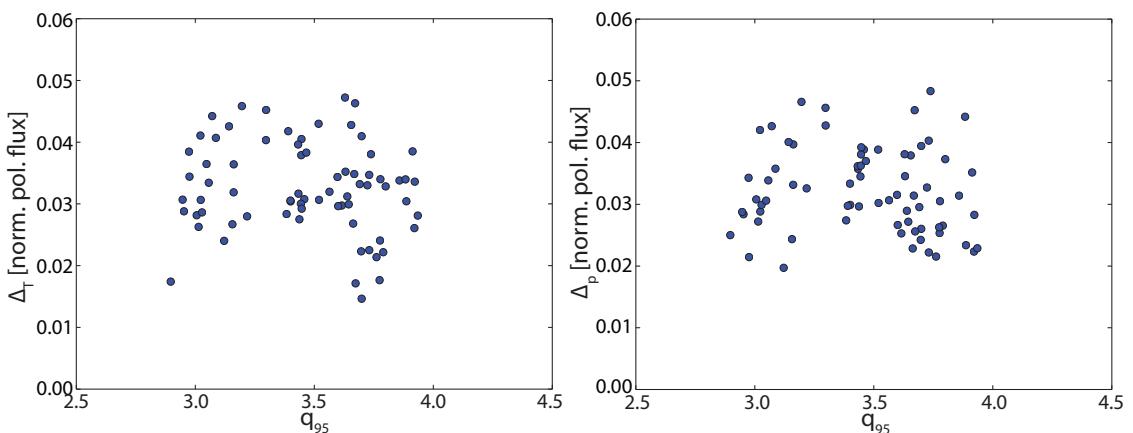
In section 5.2.1, it is shown that the temperature pedestal height is strongly dependent on  $P_{net}/\bar{n}_e$ , effectively heating power per particle (equivalently, the heat flux through the pedestal). Temperature and pressure pedestal widths are shown against power-per-particle in fig. 5.16. As with the other parameters, the pedestal width is uncorrelated with the heat flux through the pedestal.



**Figure 5.13:** Temperature (left) and pressure (right) pedestal widths versus poloidal gyroradius  $\rho_{i,\text{pol}}$ . No correlation in the pedestal width is seen, contrary to models suggesting a scaling of the sheared-flow layer and pedestal with the gyroradius.



**Figure 5.14:** Temperature (left) and pressure (right) pedestal widths versus pedestal collisionality  $\nu_{95}^*$ . No correlation is seen.

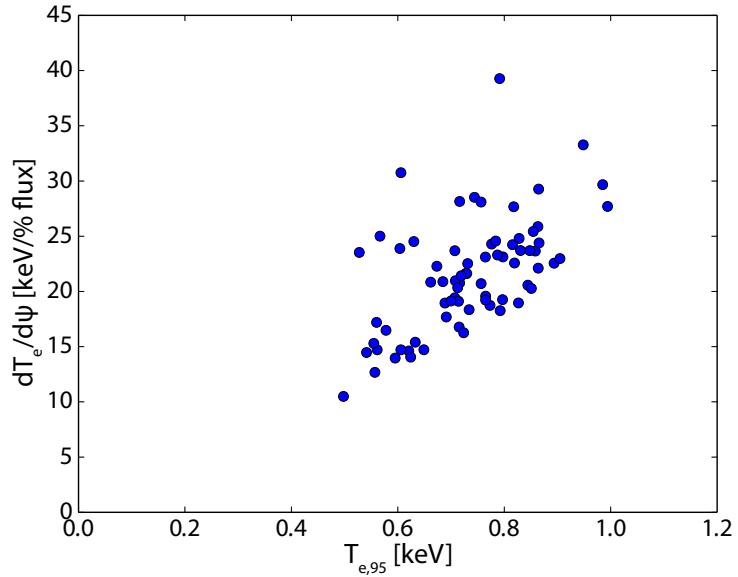


**Figure 5.15:** Temperature (left) and pressure (right) pedestal widths versus edge safety factor  $q_{95}$ . No correlation is seen.



**Figure 5.16:** Temperature (left) and pressure (right) pedestal widths versus power-per-particle,  $P_{\text{net}}/\bar{n}_e$ , i.e., the heat flux through the pedestal. No correlation is seen.

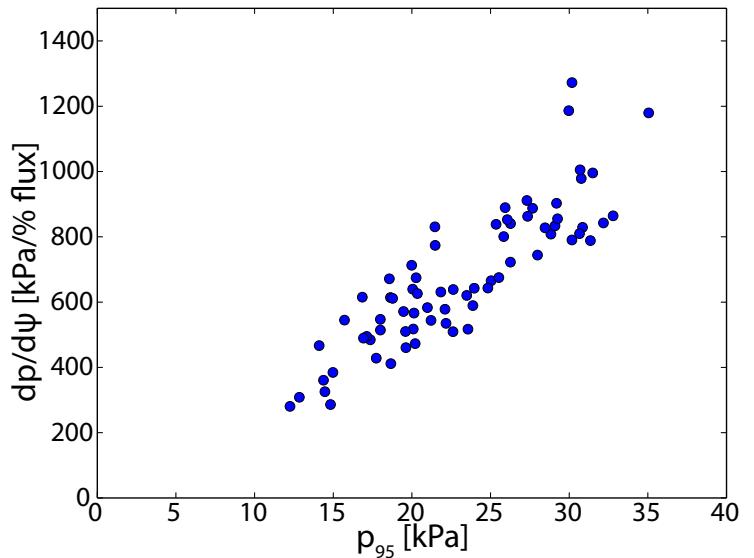
**Figure 5.17:** Peak  $\nabla T_e$  in the I-mode pedestal versus  $T_{e,95}$ . Hotter pedestals support a steeper gradient in temperature (albeit with significant scatter), consistent with a robust temperature pedestal width.



### 5.3.3 Stiff Gradient Limits

In sections 5.3.1 and 5.3.2, the I-mode pedestal width (both in temperature and pressure) is shown to be insensitive to a number of pedestal parameters. This may be examined directly by viewing the peak pedestal gradient versus its height – to lowest approximation,  $\nabla Y \sim Y/\Delta Y$  (where  $Y$  is the pedestal quantity, i.e.,  $T_e$ ,  $p_{\text{tot}}$ ). The peak gradients in temperature and pressure are shown against the corresponding 95%-flux values in fig. 5.17 and fig. 5.18, respectively. In both cases, a linear dependence of the gradient on the pedestal-top value is observed, albeit with scatter favoring higher gradients than the linear prediction in the case of the temperature. The pressure gradient is predicted quite well by its 95%-flux value. Similar behavior has been observed for the electron and ion temperatures in H-mode on AUG and DIII-D, independent of plasma shaping and evidently

**Figure 5.18:** Peak  $\nabla p$  in the I-mode pedestal versus  $p_{95}$ . There is a robust linear dependence between the pedestal gradient and height, consistent with a robust pedestal width.



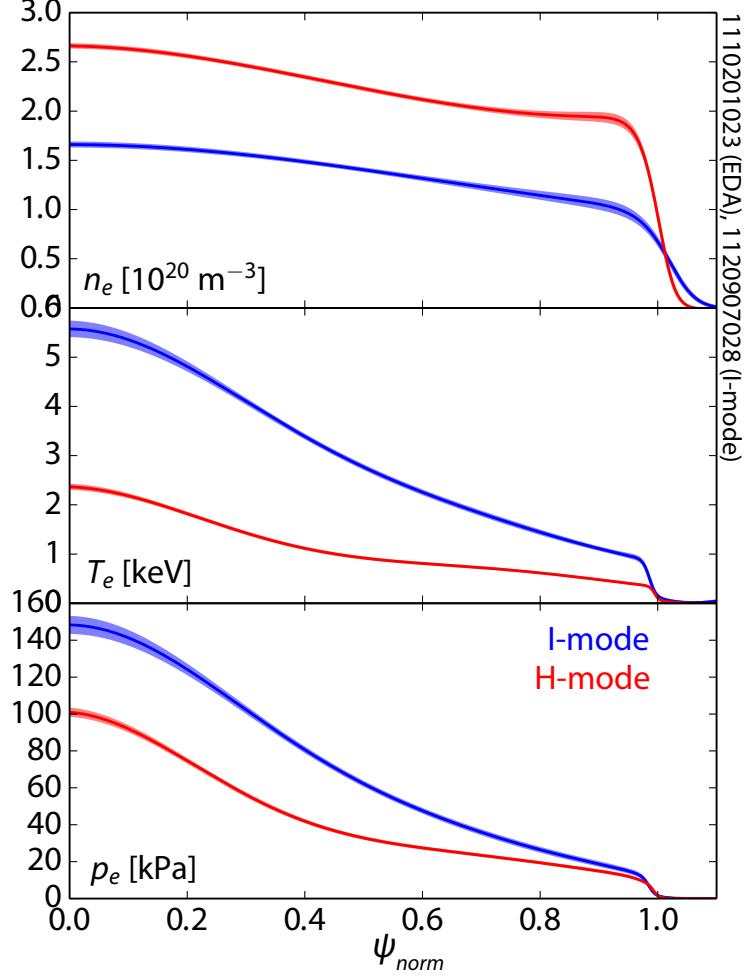
operating under a separate limit from the ideal-MHD constraint on the pressure pedestal [28]. These trends are consistent with robust pedestal widths, particularly in the pressure pedestal, in I-mode. •

#### 5.4 GLOBAL BEHAVIOR, PERFORMANCE, & CONFINEMENT

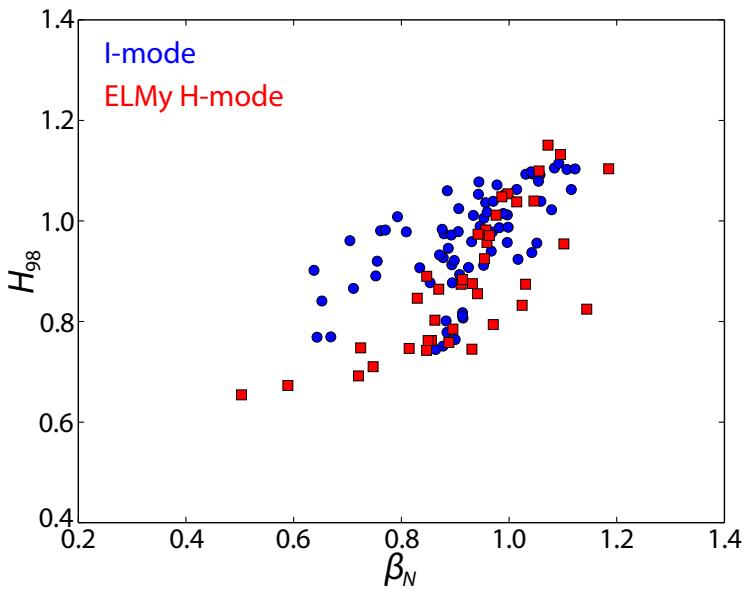
The pedestal structure of the I-mode is quite desirable for a reactor scenario – due to the strong response of the pedestal temperature to heating power, externally-applied heating power is an effective engineering control for core temperatures, and subsequently fusion reaction rates. The high pedestal temperature, coupled to stiff core temperature profiles (such that a higher temperature supports a steeper marginally-stable  $\nabla T_e$ ), supports very high core temperatures. With a moderate degree of core density peaking (with typical values of  $n_{e0}/\langle n_e \rangle \sim 1.1 - 1.3$ , comparable to H-mode [29]), this supports comparable core and volume-averaged pressures to H-mode despite the comparatively relaxed pedestal, supporting beneficial fusion conditions in the core while avoiding stability issues in the pedestal. Example density, temperature, and pressure profiles for I-mode and H-mode cases are shown in fig. 5.19, illustrating the high core pressures attainable in I-mode despite the lower pedestal and reduced density. This is reflected in fig. 5.20, showing the global-averaged normalized beta ( $\langle \beta_N \rangle = \langle \beta \rangle \alpha B_T / I_p$ ) versus the confinement metric  $H_{98}$  in I-mode and ELM My H-mode – I-mode reaches comparable levels of  $\beta_N$  while maintaining H-mode-like  $H_{98} \sim 1$  at comparable levels to ELM My H-mode, while maintaining desirable impurity confinement and ELM stability behaviors.

Energy confinement in I-mode also appears to lack strong degradation with heating power (*cf.* the  $\tau_E \sim P^{-0.7}$  degradation for H-modes,

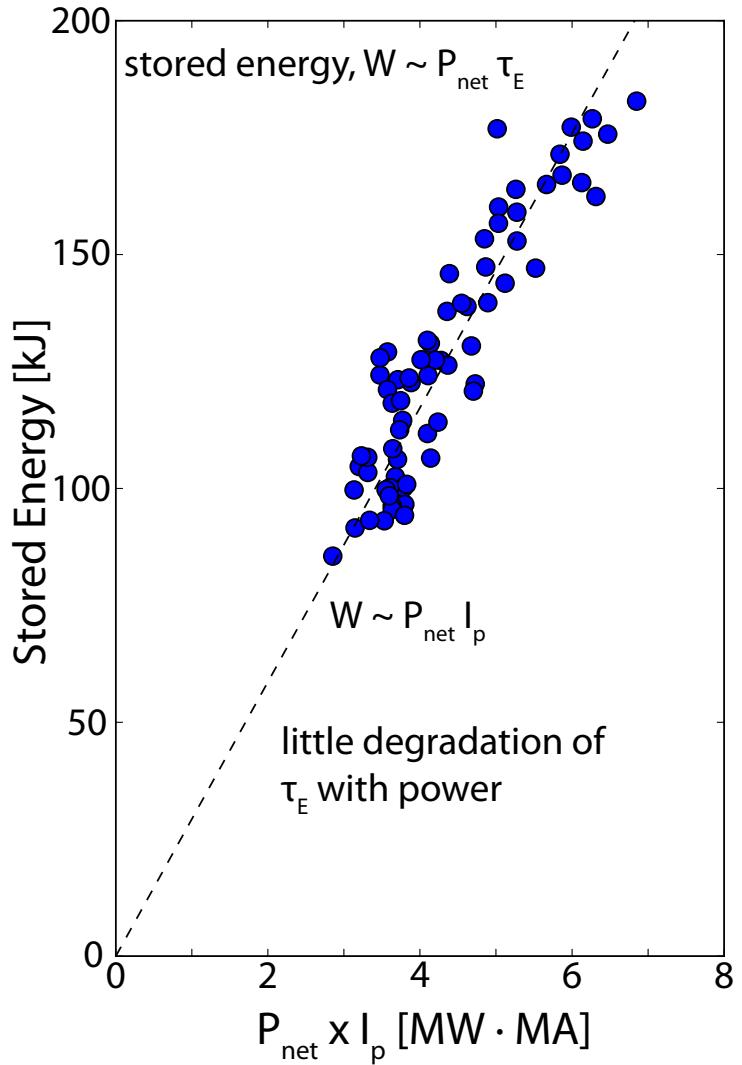
**Figure 5.19:** Profiles in density, temperature, and pressure for I-mode and EDA H-mode, with the  $\pm\sigma$  errorbars indicated by the shaded region. The H-mode case exhibits a very strong density pedestal, with a somewhat reduced temperature pedestal; the I-mode, in contrast, has a significant temperature pedestal with a relaxed density profile. While this typically results in a reduced pedestal pressure in I-mode compared to H-mode, core profile stiffness supports very high central temperatures, such that I-mode exhibits comparable or greater core and average pressure despite the relaxed pedestal.



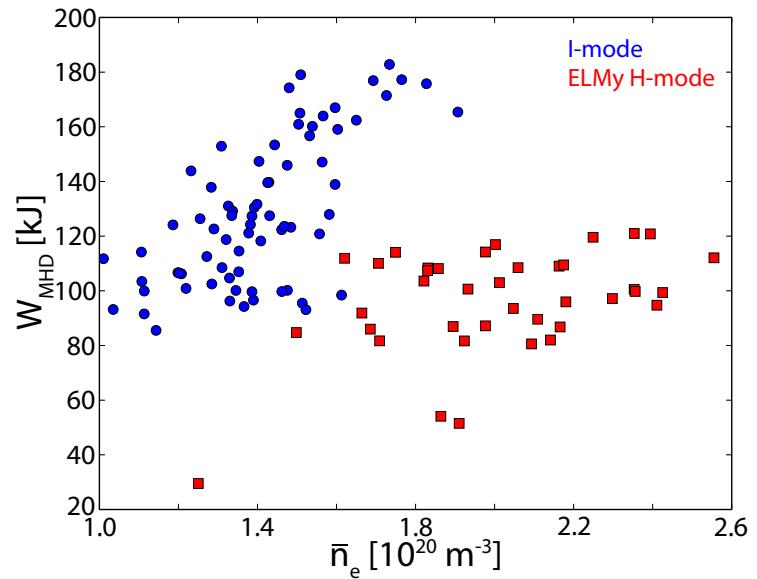
**Figure 5.20:** Global normalized  $\beta_N$  versus confinement factor  $H_{98}$  for I-mode and ELMy H-mode. Despite the relaxed pedestal pressure, I-modes reach comparable average pressures, while maintaining H-mode-like energy confinement.



**Figure 5.21:** I-mode stored energy versus the product of net heating power  $P_{\text{net}}$  and plasma current  $I_p$ . Based on the H-mode confinement scaling,  $\tau_E$  is expected to scale linearly with  $I_p$ , and to show a strong degradation with heating power:  $\tau_E \sim I_p \times P_{\text{net}}^{-0.7}$ . As the stored energy is given by  $W \sim P_{\text{net}} \tau_E$ ,  $W \sim I_p P_{\text{net}}^{0.3}$  is expected. The observed linear trend indicates little-to-no degradation of  $\tau_E$  in I-mode with heating power.



**Figure 5.22:** Plasma stored energy versus fueling, indicated by  $\bar{n}_e$  in I-mode and ELMMy H-mode. I-mode stored energy increases strongly with fueling (provided sufficient power to maintain the temperature pedestal), while ELMMy H-mode exhibits little trend with density – the global stored energy and average pressure is set by the pedestal beta, which is strongly limited in ELMMy H-mode.



as in eq. (2.5)) – a highly desirable characteristic for large devices. This may be seen intuitively in fig. 5.21. The plasma stored energy trends as  $W \sim P\tau_E$ ; from the H-mode scaling, we expect  $\tau_E \sim I_p$ . The H-mode confinement scaling, then, predicts  $W \sim I_p P_{net}^{0.3}$ . However, the stored energy in I-mode trends as  $W \sim P_{net} I_p$ , indicating that there is little or no (negative) dependence of  $\tau_E$  on heating power in I-mode. The strong dependence of the stored energy on heating power is reflected in the response of the pressure pedestal to the same, shown in fig. 5.9. The degradation of energy confinement with heating power in H-mode reflects the MHD limits on the pedestal – increased heating power raises the ELM frequency to drive enhanced energy transport, maintaining the pedestal at the MHD limit, which in turn drives the weak increase of stored energy with increased power. The lack of power degradation in I-mode, then, reflects the MHD stability of the pedestal.

Similarly, the beneficial response to fueling in the I-mode pedestal is reflected in global confinement, as the stored energy increases strongly with fueling levels (fig. 5.22) – this is particularly desirable in a burning plasma, where the alpha heating power increases with the density squared. In contrast, ELMy H-mode stored energy is largely insensitive to fueling. The stored energy and core  $\beta_N$  is instead set by the pedestal beta, which is set predominantly by plasma shape (note, however, that there is a non-negligible effect of density vs. temperature on the core pressure, with hotter, lower-density pedestals leading to higher core pressures due to stiff temperature profiles – however, these lower-collisionality pedestals tend to exhibit larger ELMs as well).

#### 5.4.1 Confinement Scaling Laws

Due to the complexity inherent in modeling global energy transport from first-principles physics, it is common to establish empirical scaling laws for energy confinement using a power-law fit to large datasets. For example, the ITER89 [30] and ITER98 [7] scalings utilized an extensive multi-machine database [31] for L-mode and H-mode confinement. In particular the ITER98y2 scaling (see eq. (2.5)) is a commonly-used baseline for high-performance regimes, particularly in terms of the normalized  $H_{98}$  (eq. (2.6)). However, as the ITER98y2 scaling was constructed predominantly with type-I ELMy H-modes (as these customarily are the highest-performance H-modes on most tokamaks), and as such implicitly includes the physics of ELM-limited pedestals. For example, the power-law fit in ITER98y2 includes a strong degradation of confinement with heating power,  $\tau_E \sim P^{-0.7}$ . This is consistent with the observed weak response of ELMing pedestals with heating power [32], with increased power instead raising the ELM frequency to maintain consistent ELM-driven heat transport.

In light of the substantially different physics of the I-mode pedestal and energy confinement compared to H-modes, it is useful to construct a power-law confinement fit using I-mode data. It is strongly emphasized that such a fit would be only preliminary, as fits using data from a single machine lack the range of parameter values needed to extrapolate to devices of different size. I-mode energy confinement times are fitted in a least-squares sense to the general form

$$\tau_{\text{I-mode}} = C I_p^{\alpha_{I_p}} B_T^{\alpha_{B_T}} \bar{n}_e^{\alpha_{n_e}} R^{\alpha_R} \varepsilon^{\alpha_\varepsilon} \kappa^{\alpha_\kappa} P_{\text{loss}}^{\alpha_P} \quad (5.1)$$

to find free exponents  $\alpha_j$  for plasma current  $I_p$  in MA, toroidal field  $B_T$  in T, line-averaged density  $\bar{n}_e$  in  $10^{20} \text{ m}^{-3}$ , major radius  $R$  in m, inverse aspect ratio  $\varepsilon$ , elongation  $\kappa$ , and loss power  $P_{\text{loss}}$  in MW (see eq. (1.28)). To extend the quantity of data and range of parameters available for this assay, the high-resolution pedestal data used in the bulk of this thesis is supplemented by older I-mode datasets containing both reversed-field LSN and forward-field USN I-mode cases. Although these data lack the high-resolution edge data necessary for pedestal structure and stability studies, they are nevertheless suitable for scalings based on global parameters. Although the net power  $P_{\text{net}}$  (see eq. (1.29)) has been demonstrated to be the more suitable parameter, rather than  $P_{\text{loss}}$  [18], these older data contain inconsistent measurements of the radiated power, necessitating the use of loss power in its stead. However, the radiated power is typically a fairly small fraction of the total power in I-mode ( $P_{\text{rad}} < 900 \text{ kW}$ ,  $P_{\text{rad}}/P_{\text{tot}} < 20\%$ ), and in any case this is consistent with previous confinement scaling studies, so the use of  $P_{\text{loss}}$  is sufficient for a first-pass examination of confinement.

Results from a number of scaling studies are shown in table 5.1, containing the values and standard deviations for each exponent value, the scale factor  $C$ , and the  $r^2$  coefficient of determination. We begin with the full parameter list used in the ITER98y2 scaling, shown as fit #1 in table 5.1, with results shown in fig. 5.23. However, it is immediately obvious that the size scalings, dependent on major radius  $R$  and inverse aspect ratio  $\varepsilon$ , are not properly captured (denoted by the extreme errorbars on these parameters). This is to be expected – absent meaningful variation in  $R$  and  $\varepsilon$  in the dataset (which requires multiple machines to produce) these parameters are not well-constrained, and result #1 is over-fitted.

For simplicity, we reduce our consideration to an effective single-machine scaling, omitting these parameters (indicated by blank entries in table 5.1). Under this fit, shown as #2 in table 5.1, the power applied to the elongation  $\kappa$  is elevated compared to that expected from the ITER98y2 scaling, with the relatively large deviation expected from the somewhat restricted range of shapes found in these stud-

**Table 5.1:** Parameters for power-law scalings of the I-mode energy confinement time  $\tau_E$ , along with  $r^2$  coefficients of determination for the fit. Blank entries indicate parameters that were omitted from that fit. Note that fit #5 utilized a fixed  $R^2\sqrt{\epsilon}$  size dependence rather than taking the size to be a free fitting parameter. Parameters are in the given units:  $I_p$  in MA,  $B_T$  in T,  $\bar{n}_e$  in  $10^{20} \text{ m}^{-3}$ ,  $R$  in m, and  $P_{\text{loss}}$  in MW. Elongation  $\kappa$  and aspect ratio  $\epsilon$  are dimensionless.

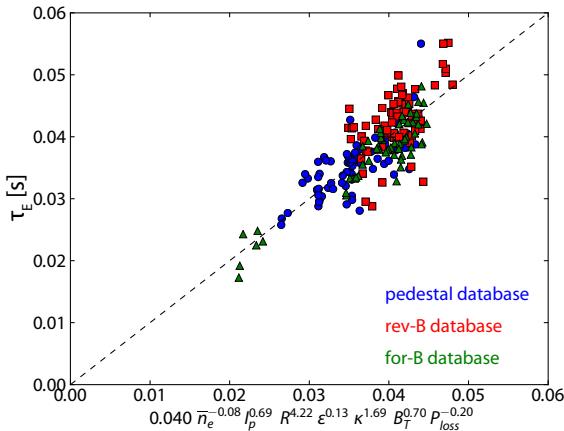
	#1	#2	#3	#4	#5
C	$0.040 \pm 0.066$	$0.007 \pm 0.002$	$0.014 \pm 0.002$	$0.014 \pm 0.002$	$0.056 \pm 0.008$
$I_p$	$0.686 \pm 0.074$	$0.696 \pm 0.073$	$0.685 \pm 0.076$	$0.692 \pm 0.073$	$0.676 \pm 0.077$
$B_T$	$0.698 \pm 0.075$	$0.697 \pm 0.071$	$0.768 \pm 0.072$	$0.773 \pm 0.071$	$0.767 \pm 0.072$
$\bar{n}_e$	$-0.077 \pm 0.055$	$-0.050 \pm 0.048$	$0.017 \pm 0.048$		$0.006 \pm 0.048$
R	$4.219 \pm 4.623$				$2^*$
$\epsilon$	$0.127 \pm 1.144$				$0.5^*$
$\kappa$	$1.686 \pm 0.398$	$1.501 \pm 0.350$			
$P_{\text{loss}}$	$-0.197 \pm 0.048$	$-0.220 \pm 0.043$	$-0.286 \pm 0.042$	$-0.281 \pm 0.039$	$-0.275 \pm 0.042$
$r^2$	0.713	0.711	0.685	0.684	0.683

ies. Omitting this fitting parameter results in a minimum-complexity fit,

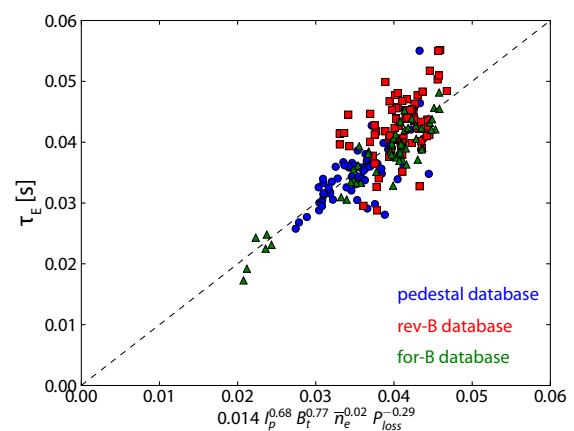
$$\tau_{\text{I-mode}} = 0.014 \times I_p^{0.685} B_T^{0.768} \bar{n}_e^{0.017} P_{\text{loss}}^{-0.286} \quad (5.2)$$

with a coefficient of determination of  $r^2 = 0.685$  (also shown as #3 in table 5.1). The correspondence between experimental  $\tau_E$  and the modeled confinement time is shown in fig. 5.24. The density dependence in  $\tau_E$  is quite weak, and may be omitted (fit #4) with minimal alteration to the result; however, this may not capture effects on the transport at higher Greenwald fraction, and requires additional experiments. Both fits capture the weak degradation of  $\tau_E$  with input power, compared to standard L- or H-mode, consistent with observations of the pedestal and global stored energy. The strong dependence of  $\tau_E$  on current is similar to that expected for H-modes, while the  $B_T$  dependence is stronger; notably, the H-mode threshold power is strongly dependent on magnetic field (see eq. (2.7)), this may reflect the fact that I-modes are bounded above by the transition to H-mode, allowing higher confinement and more aggressive pedestals at stronger  $B_T$  simply by suppressing the I-H transition.

As an illustrative exercise, we restore a fixed size dependence of the form  $R^2\sqrt{\epsilon}$  (as is found in ITER98y2) to the fit, shown as #5 in table 5.1, with the correspondence to experimental  $\tau_E$  shown in fig. 5.25. This enables extrapolation of the result to larger devices, with example predictions for DIII-D, ASDEX Upgrade, JET, and ITER shown in fig. 5.26. Due to the weakened power degradation ( $\tau_E \sim P^{-0.28}$ ), I-mode operation on ITER (in the putative  $Q = 10$  scenario with



**Figure 5.23:** Power-law fit for I-mode energy confinement time  $\tau_E$ , fitted using the full ITER98y2 parameter set (fit #1 in table 5.1). Both the high-resolution pedestal database and older reversed-field LSN and forward-field USN I-mode databases are used. While the fit is generally good, lack of variation in certain parameters – particularly the size parameters  $R$  and  $\varepsilon$  (as expected for a single-machine scaling), and elongation  $\kappa$  mean that the true variation with these parameters is not accurately captured. However, the expected weak degradation of  $\tau_E$  with heating power is captured.



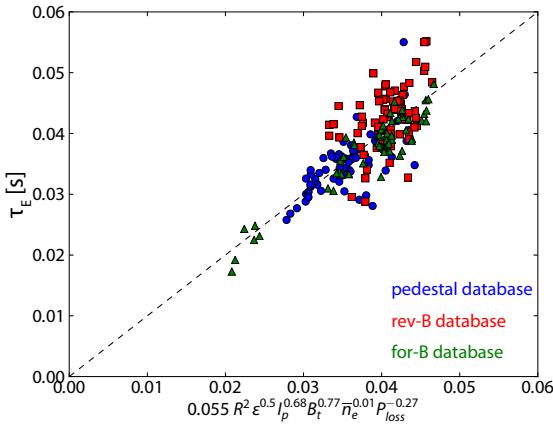
**Figure 5.24:** Power-law fit for I-mode energy confinement time  $\tau_E$ , fitted with the size parameters  $R$  and  $\varepsilon$ , and elongation  $\kappa$  excluded due to the lack of variation in these variables in the available data (fit #3 in table 5.1). Both the high-resolution pedestal database and older reversed-field LSN and forward-field USN I-mode databases are used. This represents the minimum-complexity fit for I-modes on C-Mod, capturing the essential dependences on current, field, and fueling, and notably the weak degradation of confinement with heating power.

100 MW of alpha heating) projects to a  $\sim 8$  s energy confinement time, well in excess of the expected  $\tau_E \sim 2.5$  s for H-mode.

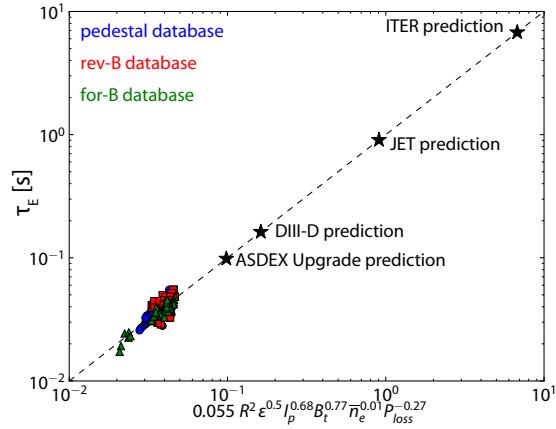
Again, we emphasize that single-machine scalings are of limited reliability for extrapolative purposes. However, this illustrates the potential gains in performance in the application of I-mode to larger devices, while correctly capturing the observed physics in I-mode (e.g., the degradation in  $\tau_E$  is, to within uncertainty, consistent with the observed strong dependence of the stored energy and pedestal pressure on heating power). However, it is notable that preliminary results in I-mode experiments on ASDEX Upgrade observed energy confinement times in the range of 0.07 – 0.1 s, consistent with the predictions of the I-mode model in the corresponding parameter range, although detailed analysis of these shots has not been performed. •

## 5.5 SUMMARY & DISCUSSION

Due to the strong influence of the pedestal structure on global confinement and performance, as well as on stability against large ELM events, a firm understanding of the pedestal is essential for the extrapolation of I-mode operation to larger devices. Empirical observations of the I-mode pedestal and global performance provide an intuitive picture of I-mode pedestal structure and stability in comparison to conventional high-confinement regimes (particularly the canonical



**Figure 5.25:** Power-law fit to I-mode energy confinement time  $\tau_E$ , with the ansatz of an  $R^2\sqrt{\varepsilon}$  size scaling fixed (fit #5 in table 5.1). Both the high-resolution pedestal database and older reversed-field LSN and forward-field USN I-mode databases are used. Note the expected weak degradation of  $\tau_E$  with heating power.



**Figure 5.26:** Modeled energy confinement time  $\tau_E$  with the fixed  $R^2\sqrt{\varepsilon}$  size scaling (fit #5 in table 5.1), extrapolated to DIII-D, ASDEX Upgrade, JET, and ITER. Modeled energy confinement times are competitive with H-modes, both the measured  $\tau_E$  for existing machines and the expected ITER98y2 prediction for ITER H-modes.

type-I ELMy H-mode), consistent with beneficial H-mode-like behaviors in energy confinement modified by the enhanced particle transport in I-mode.

The pedestal temperature is found to scale strongly with plasma current,  $T_{e,95} \sim I_p$ , comparable to that found in H-mode (*cf.* the results in chapter 4). Notably, the I-mode temperature pedestal height is found to scale strongly with heating power per particle,  $T_{e,95} \sim P_{net}/\bar{n}_e$ , in contrast to the minimal positive effect of heating power on the temperature pedestal in ELMy H-mode (note that the temperature pedestal in transport-limited EDA H-modes exhibit a positive trend with heating power somewhat weaker than in I-mode). Similarly, the pressure pedestal height scales strongly with heating power,  $p_{95} \sim n_{e,95} T_{e,95} \sim P_{net}$ , significantly more strongly than in H-mode. In contrast, the density profile is set externally by operator fueling control independent of physics limits, due to the L-mode-like particle confinement – a highly desirable result for fueling scenarios on ITER. Given sufficient power to maintain a given value of  $P_{net}/\bar{n}_e$ , temperature pedestals are matched across a range of fueling levels (fig. 5.7). Heating power and fueling are thus two largely-independent “knobs” for operator control of pedestal profiles, in contrast to both ELMy H-modes (which exhibit an inverse relationship between density and temperature due to the limit on  $\beta_{p,ped}$  imposed by MHD stability) and EDA H-modes (in which the pedestal density is locked to a value set by the current due to the interplay between particle-pinch and transport effects).

The pedestal width in I-mode does not appear to trend strongly with any of the examined physics parameters. No dependence on

$\beta_{p,ped}$  is seen, suggesting that the I-mode pedestal is not limited by KBM turbulence; moreover, the I-mode pedestal is consistently wider than predicted from the KBM width constraint used in the EPED model for ELMy H-mode. Similarly, no width dependence is seen on the poloidal gyroradius, collisionality, safety factor/magnetic shear, or heat flux through the pedestal. Both the temperature and pressure pedestal width appear to be robust across the observed range in I-mode pedestals, such that the peak gradient in each is linearly dependent on the pedestal-top value. However, it should be noted that the pressure gradient is consistently shallower than that found in H-mode due to the flat density profile, and does not exhibit the trend with plasma current expected for an MHD-limited pedestal, consistent with the observed lack of ELMs.

Although the I-mode exhibits a more relaxed pressure pedestal than found in H-mode, the comparatively higher temperature pedestal supports steep core temperature profiles, reaching significant core and average pressure provided a moderate degree of density peaking. Thus, I-mode is capable of reaching competitive levels of global confinement (both in terms of averaged pressure,  $\beta_N$ , and normalized confinement time  $H_{98} \sim 1$ ) with H-mode, while the relaxed pedestal provides beneficial stability and particle-confinement properties. It should be noted that the strongly reactive region of the plasma for fusion events (where  $\langle \sigma v \rangle \sim T_i^2$ , or  $R_{fusion} \sim p^2$ ) is largely restricted to where the plasma temperature is greater than  $\sim 4$  keV – thus, the steep core temperature profiles also maximizes the fusing volume in the plasma core in I-mode. The strong response of the pedestal to fueling (provided sufficient power) is reflected in the strong increase of stored energy with fueling, in contrast to the limited range of global stored energy set by the limited pedestal poloidal beta in ELMy H-mode. Global stored energy reflects the weak degradation of confinement with heating power, trending as  $W \sim P_{net} I_p$ . An examination of I-mode energy confinement under a power-law fit of the form used in the ITER89 and ITER98 L-mode and H-mode confinement scalings is consistent with this behavior, capturing the expected positive trend with current with a strong positive dependence on the magnetic field with weak degradation with heating power ( $\tau_E \sim P^{-\alpha}$ , with  $0.2 < \alpha < 0.3$ ). Such behavior would extrapolate to a confinement time well in excess of the expected H-mode level for an ITER-scale device.

The pedestal (and subsequent global) behavior in I-mode is highly desirable for a high-performance regime – in particular, the decoupled response to fueling and heating power provides a path to strongly increased performance, in which matched increases in density and power into an established I-mode step up the pedestal pressure, allowing the I-mode to exceed conditions which, if targeted as a starting point rather than reached in an established I-mode, would typi-

cally trigger a transition to H-mode. This behavior is also beneficial for I-mode access on ITER – initial analysis [33] indicates that the external heating power on ITER should be sufficient for I-mode access at reduced ( $\sim 4 \times 10^{19} \text{ m}^{-3}$ ) density, after which increased fueling ( $\sim 5 \times 10^{19} \text{ m}^{-3}$ ) and heating power (including alpha heating) should be sufficient to reach  $Q = 10$  operation within operational limits. Note that the ITER simulation in [33] assumed a trend of  $\tau_E \sim P^{-0.3}$  or  $W \sim P^{0.7}$  and moderate density peaking, consistent with observations of the density profile in I-mode and with the observed and modeled confinement degradation with heating power presented here.  $\star$

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# 6

## I-MODE PEDESTAL STABILITY MODELING

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Large, uncontrolled Edge-Localized Modes (ELMs – see section 2.1) in ITER-scale operation are expected to drive unacceptable levels of pulsed heat loading and erosion damage to plasma-facing materials [1, 2]. As such, avoiding or mitigating large ELMs is a major focus of research in high-performance regimes: approaches include active ELM control in H-mode (section 2.1.3) and inherently ELM-suppressed regimes (section 2.3). To these we add the I-mode (section 2.4), which appears to be naturally stable against large, deleterious ELMs in addition to its other beneficial properties (see chapter 5).

Confidence in plans for high-performance operation on ITER- and reactor-scale devices requires a predictive model for the pedestal structure and stability, to optimize fusion performance and ELM control or avoidance. Recent cooperative efforts among theory, modeling, and experiment [3] have resulted in such a model for ELMy H-modes, termed EPED [4, 5], detailed in section 3.4. The EPED model combines constraints from peeling-balloonning MHD stability (section 3.2) [6, 7, 8] and kinetic-balloonning turbulence (section 3.3) [9, 10, 11]. The EPED model has been used to successfully predict the pedestal in ELMy H-mode on a number of machines, including DIII-D [4, 5], JT-60U [4], C-Mod [12], and KSTAR [13], as well as in QH-mode [14]; small/no-ELM regimes (EDA H-mode, type-II and type-III ELMy H-modes) have been shown to be stable against the drive identified in the EPED model [4].

In this chapter, we test the underlying physics assumptions from EPED in I-mode, examining the stability of the I-mode pedestal against peeling-balloonning MHD and kinetic-balloonning turbulence [15]. This is compared to the observed lack of large ELMs in I-mode, with a goal of examining the parameter space in which stationary ELM-free operation with I-mode is possible. We also examine the stability and edge behavior of cases in which small, intermittent ELM-like events are observed in I-mode operation. •

### 6.1 MHD STABILITY – ELITE

The triggering of large ELMs in H-mode has been identified with the interaction between pressure-driven ballooning and current-driven edge kink/peeling MHD instabilities (the latter is typically referred to as a “peeling” mode to distinguish it from similarly current-driven core kink modes) in the pedestal [6, 7, 8]. Numerical studies of these instabilities using the ELITE code [6, 16], detailed in section 3.2.3,

have proven quite successful in capturing the physics of the ELM trigger.

### 6.1.1 ELITE Implementation

At its simplest, a single pass in ELITE calculates the growth rate of the peeling-balloonning instability at fixed toroidal mode number  $n$  for a given plasma profile (to wit, the pressure gradient and current density in the pedestal) and equilibrium [17]. This requires a reconstructed magnetic equilibrium with sufficiently high point density to capture the rapid variation in flux surfaces near the edge – all results in this chapter were prepared using high-resolution EFIT [18] reconstructions constrained by kinetic profiles – and high-resolution diagnostics to generate accurate profile measurements in the pedestal. To fully capture the physics of the pedestal, however, it is beneficial to visualize the pedestal relative to the full stability boundary (see fig. 3.4 for a schematic illustration), typically expressed in terms of the pressure-gradient and current-density drive terms.

Beginning from the experimental result, the profiles are scaled at fixed pedestal width, such that the pressure pedestal height or peak current density (with the current calculated by the Sauter formulation [19]) is increased or decreased relative to the original by a scalar factor, after which a self-consistent EFIT reconstruction is attempted. This effectively fills in a grid in  $\alpha_{\text{MHD}} - j$  space (a practice termed *varyped*). Horizontal slices represent a scaling of the pressure pedestal height (and therefore gradient) at fixed current, and vertical slices represent a scaling of the current density at fixed  $\nabla p$ . While ELITE does not explicitly distinguish between density and temperature profiles, these slices implicitly vary density and temperature relative to each other. For example, horizontal slices increase both density and temperature at roughly fixed  $n_e/T_e^2$ , such that collisionality is fixed, while vertical slices decrease pedestal density and increase temperature to preserve the pedestal pressure while decreasing collisionality, thereby increasing the bootstrap current (note that these trends are inexact, as the *varyped* process attempts to generate self-consistent equilibria after scaling the pedestals in this fashion, which tends to skew the grid slightly). Note that the practice described in section 3.4 of increasing pressure (and pressure gradient) at fixed width to find the maximum ELM-stable pressure as a function of width is essentially a diagonal slice through the  $\alpha_{\text{MHD}} - j$  grid: only the pressure profile is explicitly scaled, with the bootstrap current allowed to self-consistently vary, and will increase with increasing  $\nabla p$ . At each point in the  $\alpha_{\text{MHD}} - j$  grid, ELITE is run for a range of mode numbers (here  $5 \leq n \leq 35$ ) to find the most unstable mode and its growth rate; this is normalized to diamagnetic stabilization effects by the threshold for instability onset,  $\gamma_{\text{MHD}} > \omega_{*\text{eff}}/2$ , where  $\omega_{*\text{eff}}$  is the effective diamagnetic frequency



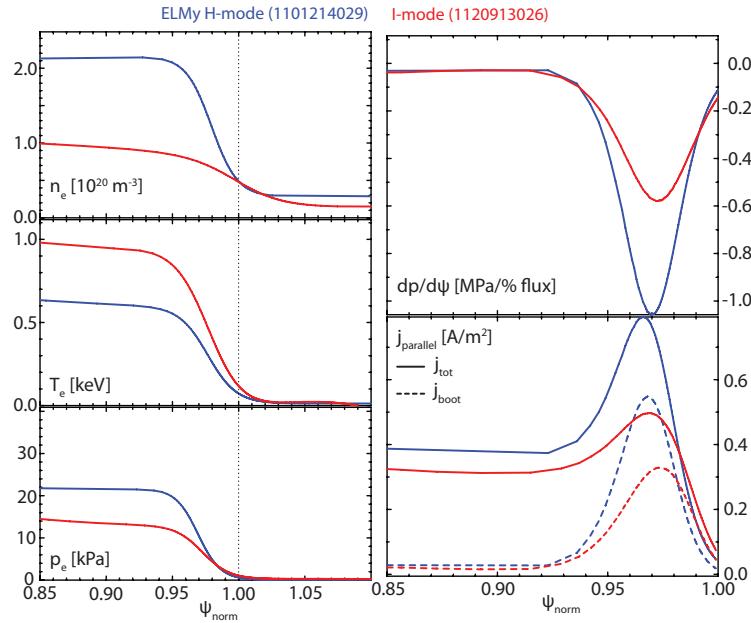
**Figure 6.1:** MHD stability contour for a high-current (1.3 MA), high-performance I-mode generated by the ELITE code. The experimental measurement is shown by the crosshair, with the stability boundary indicated by the yellow dashed line. Parameters for the modeled phase of the discharge are shown below. The I-mode pedestal is observed to be far from both the peeling and ballooning MHD stability boundaries.

accounting for variation in the pedestal, as implemented in EPED1.6 (see section 3.4.2).

### 6.1.2 I-Mode ELITE Calculations

An ELITE calculation for the I-mode pedestal is shown in fig. 6.1, along with parameters (line-averaged density, core and edge  $T_e$ , global-average pressure, and  $H_\alpha$  emission) for the modeled phase of the discharge. The I-mode pedestal parameters, indicated by the yellow crosshair, are far from both the peeling and ballooning MHD stability boundaries calculated by ELITE (indicated by the yellow dashed line, marking the  $\gamma/(\omega_{\text{eff}}/2) = 1$  contour) – compare this with the ELMMy H-mode calculation shown in fig. 4.13. This is consistent with the observed lack of large ELMs, even in higher-performance I-modes (both in the normalized sense, with  $H_{98} = 1.02$  and  $\beta_N = 1.0$ , and in absolute terms,  $W_{\text{MHD}} = 177 \text{ kJ}$  in the case in fig. 6.1, compared to  $W \sim 100 - 120 \text{ kJ}$  in ELMMy H-mode and  $W \sim 150 - 190 \text{ kJ}$  in EDA H-mode).

**Figure 6.2:** Pedestal profiles in I-mode and ELMMy H-mode. Due to the steep density gradient in the pedestal, the H-mode exhibits significant pressure gradient and edge current density, which drive the peeling-ballooning MHD instability associated with the ELM trigger. Despite this, the high edge temperature in I-mode allows it to reach an appreciable pedestal pressure.

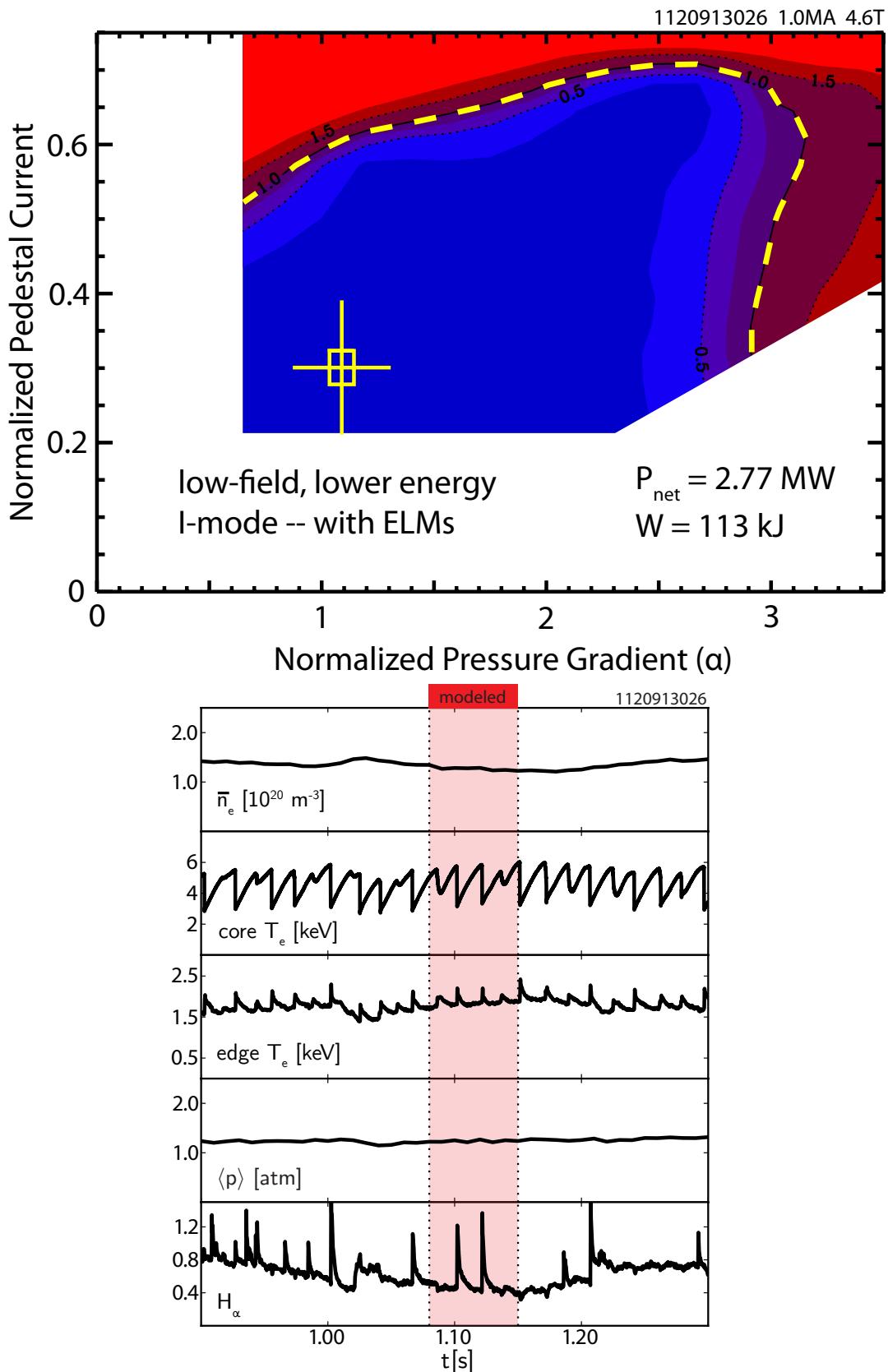


The calculated MHD stability is intuitively understood from the I-mode pedestal profile: while the I-mode reaches comparable pedestal pressures to H-mode, the pressure is due largely to the strong temperature pedestal, with a relaxed density profile and broader pedestal width than comparable- $\beta_p$  H-modes. This reduces the total pressure gradient (and thus the ballooning MHD drive), as well as the local bootstrap current (set largely by the density gradient) and peeling drive. A comparison of the pedestal profiles, with pressure gradient and edge current density, between I-mode and H-mode is shown in fig. 6.2. However, due to the strong interplay between the pressure

gradient and bootstrap current (which is reduced by the lack of a density pedestal, but enhanced by the naturally low collisionality in I-mode), the full computational approach in ELITE is necessary to accurately characterize the pedestal stability.

Although I-mode is free of the regular, large ELMs typical of (type-I) ELM<sub>My</sub> H-mode, under certain conditions – particularly reduced toroidal field and plasma current – small (< 1% drop in stored energy) intermittent ELM-like events are occasionally observed in I-mode. However, when examined in ELITE (fig. 6.3) these cases are found to still be far from the peeling-balloonning boundary. These intermittent events occur in conjunction to sawtooth heat pulses reaching the edge, visible on the fast ECE  $T_e$  signal, indicating that the events are potentially triggered by transient modification of the pedestal by the heat pulse – however, these events are not consistently triggered on each sawtooth crash under similar conditions. More study is required on this front, with initial results shown in section 6.3.

Examination of the I-mode pedestal is also illuminating from the perspective of MHD stability. To lowest order approximation, MHD-limited pedestals, as are found in ELM<sub>My</sub> H-mode, are limited in the attainable poloidal beta at the pedestal top (a limit arising from the limit on  $\alpha_{MHD}$  from ballooning instability coupled with the weakly-varying pedestal width on a given tokamak – *cf.* section 2.1.2). This is illustrated in fig. 6.4(a), showing the pedestal density and temperature normalized to poloidal field (accounting for variation in plasma current). Due to the normalization to  $B_p$ , hyperbolae in the parameter space are curves of constant pedestal  $\beta_p$ . ELM<sub>My</sub> H-mode data lie on such a curve (note that, since the  $\beta_p$  limit is shaping-dependent, only ELM<sub>My</sub> H-mode cases with approximately matched shape are shown on the single hyperbolic curve), with the expected inverse relationship between pedestal density and temperature. I-mode pedestal density and temperature, on the other hand, are uncorrelated, consistent with the pedestal not being limited by MHD stability constraints. I-mode pedestal pressure, similarly normalized, is shown against normalized pedestal density in fig. 6.4(b). Where MHD-limited pedestals would show a flat trend due to the limit on poloidal beta, I-mode  $\beta_p$  instead exhibits a linear trend with density. This is consistent with the strong response of pedestal performance with increased fueling (described in chapter 5, particularly section 5.2.2) provided sufficient heating power to maintain the pedestal. The slope of this trend is a line of constant  $T_{e,95}/B_p$ , consistent with the observed  $T_e \sim I_p$  as well (see section 5.2.1). This trend in the normalized pressure is in addition to the response of pedestal pressure with heating power, as shown in fig. 6.5. The temperature response to heating power is encoded in setting the slope of the fixed  $T_{e,95}/B_p$  line, reflecting the higher temperatures at fixed current with increased  $P_{net}/\bar{n}_e$ .

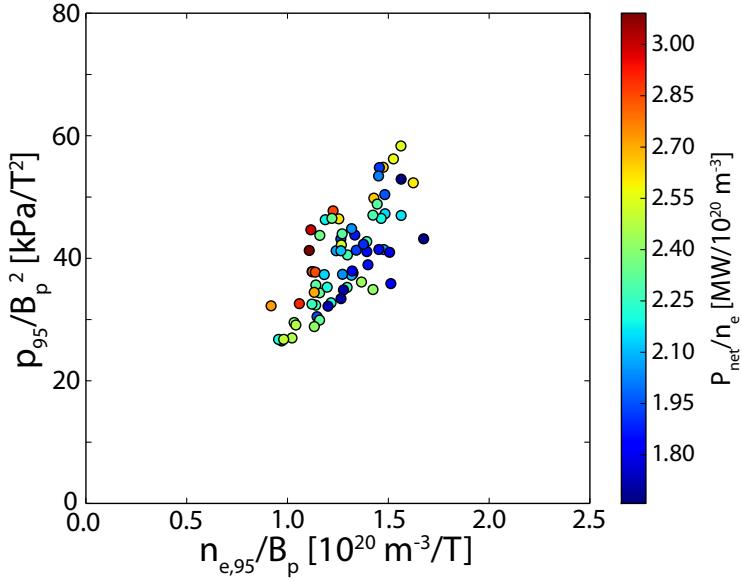


**Figure 6.3:** MHD stability contour for a low-field (4.6 T), lower-energy I-mode generated by the ELITE code. The experimental measurement is shown by the crosshair, with the stability boundary indicated by the yellow dashed line. Parameters for the modeled phase of the discharge are shown below. This case exhibited small, intermittent ELM-like events, but is still calculated to be peeling-balloonning stable for profiles averaged over the time window.



**Figure 6.4:** Pedestal temperature (left) and pressure (right) versus pedestal density. Parameters are normalized to the edge poloidal field – this accounts for plasma-current variation in the datapoints, as well as allowing a natural representation of MHD boundaries. (a) Pedestal temperature vs. density for I-mode and ELMy H-mode. Due to the poloidal-field normalization, hyperbolae in the parameter space are curves of constant  $\beta_{p,ped}$ . ELMy H-modes lie, to lowest-order approximation, on a  $\beta_{p,ped}$ -limited curve (indicated by the dashed line) with the expected inverse relationship between density and temperature; I-mode  $n_e$  and  $T_e$ , however, are uncorrelated. (b) Pedestal pressure normalized to poloidal field pressure versus normalized density in I-mode. Pedestal poloidal beta trends linearly with (normalized) density, rather than lying on the  $\beta_{p,ped}$ -limited line expected for MHD-limited pedestals, consistent with the strong response of the I-mode pedestal to fueling (see section 5.2.2). I-mode data lie on a line of constant  $T_e/B_p$ , consistent with the observed  $T_{e,ped} \sim I_p$  seen in section 5.2.1.

**Figure 6.5:** Pedestal pressure normalized to poloidal field pressure versus normalized density in I-mode (cf. fig. 6.4(b)). Points are color-coded by power-per-particle, which sets the pedestal temperature – differing values of  $P_{net}/\bar{n}_e$  set the slope of the fixed  $T_e/B_p$  line. The increase in normalized pressure, then, is not solely due to increased power, but rather indicates a positive response with fueling.





**Figure 6.6:** Infinite- $n$  ballooning MHD results calculated by BALOO, overlaid on the ELITE results for the same case (see fig. 6.1). The Infinite- $n$  ballooning threshold is taken as a surrogate for the onset of KBM turbulence. Due to the local nature of the infinite- $n$  constraint, BALOO calculates the width in flux space that is locally ballooning-critical – when this reaches half of the pedestal width, the KBM is assumed to be triggered. This case is near the KBM-predicted pedestal width  $\Delta_{\text{EPED}}$ , but is nevertheless modeled to be KBM-stable (for  $\Delta_\psi \sim 0.02$ , the half-width threshold is the white dotted contour labeled 0.01).

## 6.2 KINETIC-BALLOONING MODE STABILITY

Edge turbulence in I-mode is characterized by the strong reduction of mid-frequency turbulence corresponding to the reduced energy transport after the L-I transition. Instead, the I-mode exhibits a broad higher-frequency (200–400 kHz) fluctuation, the *Weakly-Coherent Mode* [20, 21, 22] (see section 2.4.3). Due to its prominence in the I-mode edge and qualitative similarity to the Quasi-Coherent Mode (QCM) in EDA H-mode [23] (see section 2.3.2), the WCM is thought to play a role in regulating the I-mode pedestal, particularly by driving enhanced particle flux [24]. While the WCM is fairly well-characterized experimentally, the underlying physics of the mode remain an open question. From the standpoint of both turbulence characterization and ELM stability, the kinetic-ballooning mode (KBM) is a valuable starting point for comparing the WCM to the turbulent behavior in more conventional H-modes.



**Figure 6.7:** Infinite- $n$  ballooning MHD results calculated by BALOO, overlaid on the ELITE results for the same case (see fig. 6.3). This case exhibited sawtooth-triggered ELM-like events. This case is substantially wider than the KBM-predicted pedestal width  $\Delta_{EPED}$ , and is modeled to be strongly KBM-stable – in fact, the BALOO assay could not calculate enough ballooning-unstable rational surfaces to draw the contour for the BCP-predicted threshold of 0.02.

Computational modeling of the KBM is possible using infinite- $n$  ideal ballooning MHD as a surrogate for the turbulence threshold [4, 10, 11] (see section 3.3). The localized constraint from the KBM (and perfectly-localized infinite- $n$  ideal MHD) is applied to the entire pedestal via the “ballooning-critical pedestal” technique, described in section 3.3.1, in which the KBM threshold is identified as the point at which half of the pedestal (typically the “middle half” where the pressure gradient is steepest) is locally at or beyond criticality to the MHD surrogate. This is calculated using the BALOO code [25, 26]; at each point in the *varyped* grid, the number of rational surfaces that are unstable to infinite- $n$  ballooning modes and subsequently the width in poloidal flux space covered by these surfaces is calculated, drawing contours of pedestal half-width corresponding to the KBM threshold.

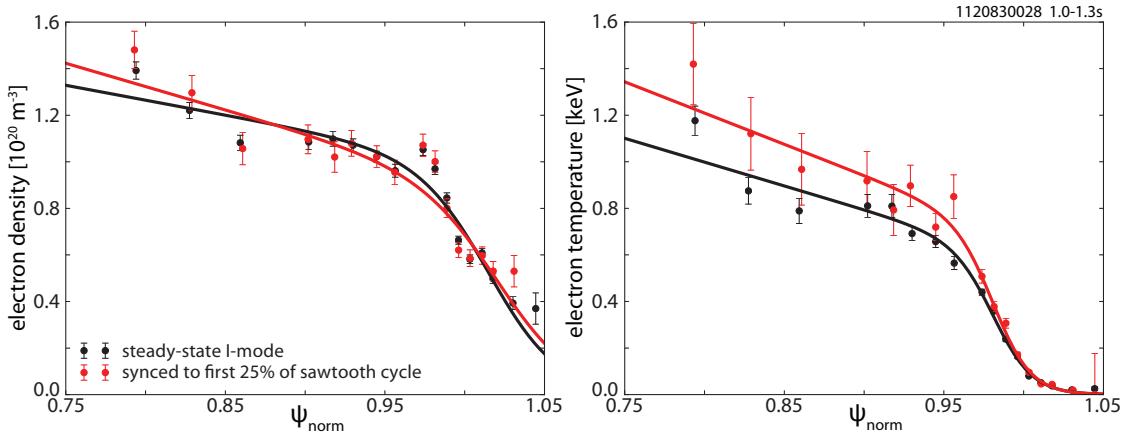
I-mode pedestals exhibit little trend in width (in poloidal flux space) with pedestal poloidal beta (see fig. 5.12), as would be expected for pedestals limited by KBM turbulence. We may compare cases spanning the range in pedestal width  $\Delta_\psi$  against the KBM-limited prediction for the width,  $\Delta_\psi = 0.076\beta_{p,ped}^{1/2}$ , from EPED1 (see section 3.4.1),

herein termed  $\Delta_{\text{EPED}}$ . A representative case near the EPED1 prediction line is shown in fig. 6.6 (overlaid on the ELITE result for the same case, fig. 6.1). For  $\Delta_\psi = .021$ , the expected KBM threshold based on the BCP half-width calculation is the 0.01 contour – the pedestal is calculated to be stable compared to this threshold. The representative case far from the EPED1 prediction line is shown in fig. 6.7 (overlaid on the ELITE result for the same case, fig. 6.3). At  $\Delta_\psi = 0.04$ , the expected KBM threshold is the 0.02 contour – however, the BALOO assay could not calculate enough ballooning-unstable rational surfaces to even draw this contour. Suffice to say that the pedestal is far from the KBM onset threshold as calculated from infinite-n MHD. Notably, the former case ( $\Delta_\psi \sim \Delta_{\text{EPED}}$ ) was a relatively high-performance case, and did not exhibit ELM-like events, while the latter ( $\Delta_\psi \gg \Delta_{\text{EPED}}$ ) exhibited ELM-like events. The indication from both experimental observation (namely, the lack of dependence of the pedestal width on  $\beta_{p,\text{ped}}$ ) and computational modeling, then, is that the KBM is not responsible for limiting the pedestal in I-mode. •

### 6.3 INTERMITTENT ELMs IN I-MODE

Given the importance of controlling or avoiding large ELMs on ITER- and reactor-scale devices, a firm understanding of the physics underlying the ELM trigger is essential for planned ITER operation. While I-mode is typically observed to be naturally free of large, damaging ELMs, there are nevertheless a minority of cases – twelve time windows comprised of ten unique shots, out of 72 windows (52 unique shots) total in the pedestal database – under certain conditions (particularly, reduced current and toroidal field) in which small, intermittent ELMs or ELM-like events are observed. It is to these cases that we now turn our attention.

ELMs in I-mode are generally observed to be small (< 1% perturbation to the stored energy), and are sporadic, rather than occurring in a regular cycle as in the conventional type-I ELMy H-mode. The majority events occur shortly following the sawtooth heat pulse reaching the edge (26 sawtooth-triggered events in the studied windows, compared to 10 off of the sawtooth), based on timing from fast ECE  $T_e$  measurements in the pedestal. This indicates a possible trigger for the event due to transient modification of the pedestal structure. An example case of this is shown in fig. 6.8. The sawtooth heat pulse does not perturb the density profile, but drives a significant transient increase in the temperature pedestal (data masked to the first 25% of the sawtooth cycle after the heat pulse reaches the edge shown in red). Calculations in ELITE and BALOO for this case are shown in fig. 6.9 for both the time-averaged pedestal profile, and the masked data to the sawtooth cycle. While the sawtooth synchronization does



**Figure 6.8:** Profiles of  $n_e$  and  $T_e$  in the I-mode pedestal, with the full ensemble-averaged data (black) compared to data masked to the first 25% of the sawtooth cycle following the heat pulse reaching the edge. The sawtooth does not meaningfully perturb the density profile, but triggers a measurable transient increase in the temperature pedestal.



**Figure 6.9:** Peeling-ballooning MHD stability calculated by ELITE and KBM thresholds calculated by BALOO for an I-mode case, comparing the time-averaged data against pedestal profiles prepared with data masking to the first 25% of the sawtooth cycle following the heat pulse reaching the edge (see fig. 6.8). Note that, to directly compare two separately-calculated equilibria, we replace the  $\alpha_{\text{MHD}}$  and  $j_{\parallel}$  axes with stability metrics arising from peeling and ballooning MHD. While the sawtooth heat pulse does measurably perturb the pedestal in stability space, it is insufficient to reach either the peeling-ballooning or KBM threshold.

drive a measurable perturbation to the pedestal in stability space – the effect is predominantly in the pressure gradient, rather than the current density, due to the weaker effect of the temperature gradient on the bootstrap current – the effect is insufficient to reach either the peeling-balloonning MHD or the KBM turbulence threshold (although the perturbed point nears the KBM threshold within errorbars, indicating that the KBM may still be a factor). Note that, in order to compare two separately-computed equilibria, we use alternate axes in fig. 6.9: rather than directly using  $\alpha_{\text{MHD}}$  and the (normalized) edge current density, the parameter space is presented in terms of ballooning and kink-peeling stability parameters,  $\beta_N/\Delta^{3/4}$  and  $j_{\max}\Delta^{1/4}$ . The first encapsulates the  $p_{\text{ped}} \sim \Delta^{3/4}$  trend expected from ballooning stability, when accounting for the nonlocal effects – at broader  $\Delta$ , wider low- $n$  modes destabilize more easily, reducing the maximum  $\alpha_{\text{MHD}}$ , as described in section 3.2 – and current stabilization. The second accounts for the trend in the total current,  $\int j d\psi \sim \Delta^{3/4}$  from the  $p_{\text{ped}} \sim \Delta^{3/4}$  trend from ballooning stability, with the total edge bootstrap current set by the pedestal pressure; however, the maximum current density and total pedestal current may be related by  $\int j d\psi \sim j_{\max}\Delta \rightarrow j_{\max} \sim 1/\Delta^{1/4}$ , thus the current-driven kink/peeling stability may be expressed in terms of the normalized  $j_{\max}\Delta^{1/4}$ .

In light of the observed stability of I-mode to peeling-balloonning MHD – even in cases where the perturbation of the putative sawtooth



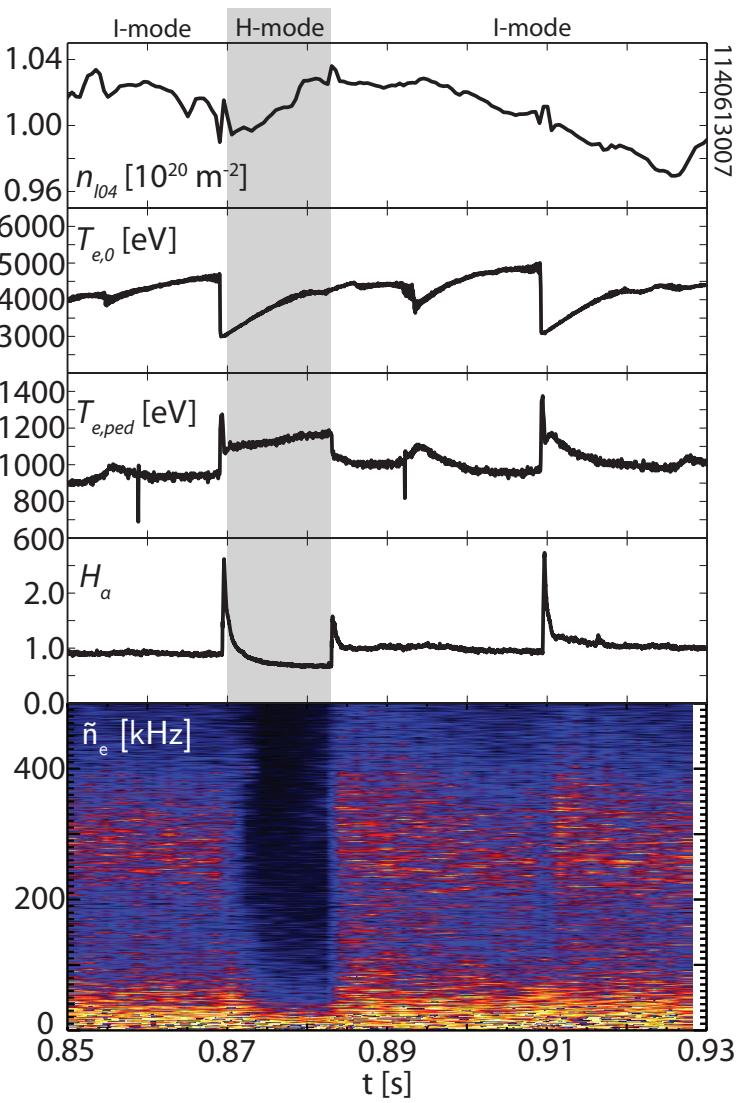
**Figure 6.10:** Traces of  $n_{104}$ , core and edge ( $r/a \sim 0.98$ )  $T_e$ , and  $H_\alpha$  for ELMMy H-mode (left) and I-mode (right). ELMs in H-mode (visible on the  $H_\alpha$  trace) are independent of the sawtooth cycle, and drive perturbations to the edge temperature and line-integrated density, as both energy and particles are expelled from the plasma by the ELM crash. This is particularly clear on the edge temperature, which exhibits a clear increase with the sawtooth heat pulse and a separate crash with the ELM. I-mode, in contrast, exhibits ELMs (or ELM-like events) that are tied to sawtooth heat pulses reaching the edge, as visible on the ECE  $T_e$  signal. No visible crash in edge temperature is visible following the ELM, nor is there a significant perturbation to the density.

trigger is accounted for – it is worthwhile to examine the behavior of the ELMs in I-mode compared to those found in more conventional H-modes. Traces from a type-I ELMy H-mode and an I-mode are shown in fig. 6.10. The ELMy case (left) exhibits behavior typical of a type-I ELM cycle: discrete, regular ELMs (visible on the  $H_{\alpha}$  trace), with crashes in edge temperature as the ELM expels energy and particles into the SOL. The effects of the sawteeth are distinct from the ELM, with a spike and subsequent relaxation in edge temperature from the heat pulse visible on the edge ECE  $T_e$  separate from the sharp temperature-pedestal crash due to the ELM. The sporadic sawtooth-triggered events in I-mode (right), despite a similar trace in  $H_{\alpha}$ , do not exhibit the characteristic crash in edge temperature associated with an ELM – rather, only the spike in  $T_e$  from the sawtooth heat pulse is visible, followed by a relaxation to the steady pedestal temperature.

The distinction between the two edge perturbations is visible in a single case, shown in fig. 6.11. The sawtooth heat pulse at 0.87 s triggers an I-H transition, indicated by the reduction in  $H_{\alpha}$  light following the pulse from the sawtooth, and the sudden reduction in turbulence visible in the  $\tilde{n}_e$  spectrogram (both destroying the WCM fluctuation at  $\sim 300$  kHz, and further reducing the mid-frequency broadband turbulence). Such a transition is not unheard-of – recall that the L-I transition is tied to sawtooth heat pulses as well. This H-mode terminates with a non-sawtooth-triggered ELM at 0.885 s, with the customary crash in edge temperature and  $H_{\alpha}$  spike. After the H-mode terminates, the plasma reverts to I-mode, with a further sawtooth-triggered event at 0.91 s. Although there does appear to be some  $T_e$  reduction due to the ELM, it is insufficient to outweigh the  $T_e$  spike from the sawtooth heat pulse.

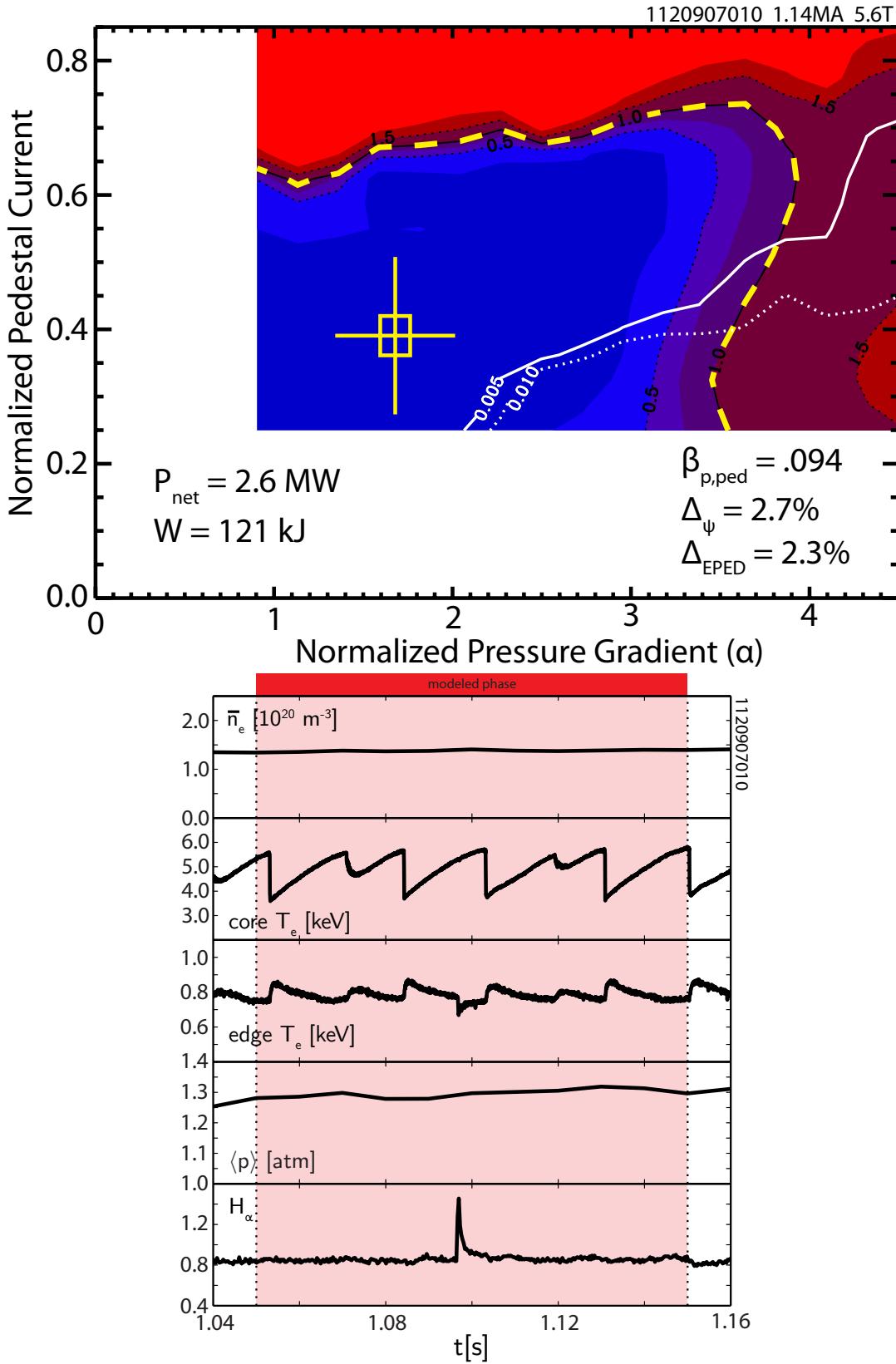
Given that these majority cases (shown in fig. 6.10 at right) do not exhibit the expected temperature pedestal crash and are MHD-stable, it is apparent that these cases are not instability-triggered ELMs at all, but rather are a distinct, and far more benign, phenomenon. For clarity, we will call these “sawtooth  $H_{\alpha}$  spikes” (indeed, this seems to be the only distinguishing factor for these edge events!). A plausible explanation is that the sawtooth does not trigger an instability in the edge, but instead propagates into the scrape-off layer. The heat pulse then creates a propagating ionization front as it encounters the cold plasma and neutral gas in the SOL. The burst of  $H_{\alpha}$  light and subsequent exponential decay is due to this sudden pulse energizing neutrals in the edge. Fundamentally, the  $H_{\alpha}$  spike from a conventional ELM is driven by the same cause – a sudden influx of particles and energy into the SOL, as well as a similar ionization front in the neutrals in the far SOL. However, the underlying phenomenon of these events is not entirely clear – even under comparable conditions, the spikes are not consistently triggered by similarly-sized sawtooth

**Figure 6.11:** Traces of  $n_{104}$ , core and edge  $T_e$ , and  $H_\alpha$  for an I-mode exhibiting ELM-like events. The sawtooth heat pulse at  $\sim 0.87$  s triggers an I-H transition, indicated by the drop in  $H_\alpha$  and suppression of turbulence visible on the  $\tilde{n}_e$  plot. This H-mode terminates with a non-sawtooth-triggered ELM with visible edge temperature crash and density perturbation, dropping back into I-mode. The I-mode phase also exhibits sawtooth-triggered ELM-like events with minimal density perturbation or temperature crash.



heat pulses. The edge behavior of these cases is therefore a subject of continuing investigation.

In addition to the sawtooth-triggered  $H_\alpha$  spike events described above, a minority of edge  $H_\alpha$  events do exhibit the characteristic temperature crash of an ELM, and are not in all cases triggered by a sawtooth (although some of these cases may be compound ELMs following a sawtooth-triggered event). Peeling-ballooning and KBM stability analysis of such a case is presented in fig. 6.12. In this case, a single ELM is visible at 1.1 s, independent of the sawtooth cycle – rather, the characteristic crash is visible in the edge temperature after relaxation of the temperature from the sawtooth heat pulse (note, however, that the ELM does not significantly perturb the stored energy/global-averaged pressure). When modeled in ELITE and BALOO, however, the steady I-mode phase around the ELM is nevertheless found to be well into the stable region both for infinite- $n$  ballooning modes and finite- $n$  coupled peeling-ballooning modes. While it is possible that a



**Figure 6.12:** MHD stability contour for I-mode generated by the ELITE code, with results from the infinite- $n$  BALOO calculation overlaid. The experimental measurement is shown by the crosshair, with the stability boundary indicated by the yellow dashed line. Parameters for the modeled phase of the discharge are shown below. This case exhibited a solitary ELM not triggered by the sawtooth heat pulse, with the characteristic edge temperature crash of a canonical ELM. However, the I-mode phase around the ELM is calculated to be peeling-balloonning stable and below the KBM threshold.

transient effect not captured by the profiles used for the stability calculation drove the pedestal near the classical ELM stability boundary in this case, the stationary state for the plasma is evidently stable to the expected ELM triggers.

#### 6.4 SUMMARY & DISCUSSION

Models for the trigger of large, deleterious ELMs based on coupled peeling-balloonning MHD instabilities [6, 7, 8, 16] and kinetic-balloonning turbulence [9, 10, 11] have been particularly successful in capturing the physics underlying the ELMy H-mode pedestal. This approach is applied to the I-mode pedestal. The majority of I-mode cases are naturally free of ELMs, and are modeled to be strongly stable both to coupled peeling-balloonning MHD modes and to KBM turbulence (calculated by way of the infinite-n ideal-balloonning MHD surrogate). Under certain conditions, particularly reduced plasma current and magnetic field, the I-mode exhibits small, intermittent ELM-like events. The majority of these cases are evidently tied to the sawtooth heat pulse reaching the plasma edge, and lack the characteristic edge temperature crash expected due to the expulsion of energy and particles by the ELM. This, coupled with the computed stability of these pedestals (even when the data are treated to account for the transient modification of the temperature pedestal by the sawtooth), suggests that the phenomenon is distinct from a traditional type-I ELM, with the measured spike in  $H_\alpha$  light (customarily indicative of an ELM) possibly driven by an ionization front in the SOL from the sawtooth heat pulse propagation, rather than an explosive edge instability. A minority of ELM events in I-mode exhibit the characteristic  $T_e$  crash, including some events that are not evidently triggered by the sawtooth heat pulse. The steady I-mode phases around these events, however, are also modeled to be stable, indicating a transient event not captured by these models driving the ELM instability.

This assay into the computed stability of I-mode is consistent with the observed absence of large, deleterious type-I ELMs in I-mode. This stability is self-enforcing, from the fundamental nature of the I-mode pedestal – the pressure pedestal is set largely by the strong temperature pedestal, with the flat density profile suppressing both the pressure gradient and the bootstrap current drive. For minority of I-mode cases exhibiting apparent ELMs, most cases are evidently not “true” instability-driven ELMs, but are rather a benign sawtooth-triggered  $H_\alpha$  spike. In the minority of edge events, an edge temperature crash is present, indicating an ELM; however, these crashes are small (< 1% perturbation to stored energy), with the temperature crash in sawtooth-triggered cases insufficient to overcome the positive effect of the heat pulse on the edge temperature. Moreover, these I-mode cases exhibiting ELMs are typically the *lower* performance

cases, with less aggressive fueling and heating power, reaching lower pedestal beta.

It is worth noting that more conventional “ELM-suppressed” regimes (e.g., RMP-suppressed H-modes, QH-mode) also can still present ELMs, with the suppression resulting in smaller, less dangerous ELMs rather than completely removing them. While some ELM behavior is evidently endemic to high-performance pedestals, this behavior is limited in I-mode to small, intermittent events – the existing I-mode parameter space is naturally stable against large (type-I) ELMs, as desired for a putative reactor regime. \*



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## CONCLUSIONS & FUTURE WORK

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The work described in this thesis has contributed to the study of the pedestal in high-performance regimes – as the pedestal sets a strict constraint on the core pressure and fusion power density, as well as determining the stability against large, deleterious Edge-Localized Modes (ELMs), a firm understanding of the physics entailed in the structure and stability of the pedestal is essential to the development of operating scenarios for ITER- and reactor-scale devices. To this end, this thesis details a combined approach using both empirical observations and theoretical/computational models to understand the governing physics of the pedestal.

These analysis methods are developed first for ELM<sub>y</sub> H-mode experiments on Alcator C-Mod – as this is the most broadly-accessible and well-understood high-performance regime on most tokamak devices (see chapter 2), ELM<sub>y</sub> H-mode is considered the baseline for high-confinement operation on ITER [1]. However, large, uncontrolled ELMs can drive pulsed heat loading and erosion damage in excess of the material tolerances of plasma-facing components. Understanding the limits placed on the pedestal by ELM stability, then, is of critical importance for planned operation on ITER. The work presented in this thesis (see also [2]) was undertaken as a contribution to a joint research effort across several machines [3] to develop a predictive model for the ELM<sub>y</sub> H-mode pedestal.

The empirical and computational analyses developed for ELM<sub>y</sub> H-mode are also applied in this thesis to the I-mode [4], a novel high-confinement regime developed on Alcator C-Mod, with a number of highly desirable characteristics for reactor operation. I-mode is notable in that it decouples energy and particle transport, forming an H-mode-like temperature pedestal with high energy confinement while maintaining an L-mode-like density profile with low particle confinement and favorably rapid transport of impurities from the plasma. Moreover, the energy confinement in I-mode appears to degrade significantly more weakly than H-mode. The work in this thesis (see also [5]) focuses on characterizing the I-mode pedestal in terms of its structure and impact on global performance – and therefore implications for operation on larger devices – and its inherent avoidance of the instabilities associated with the ELM trigger. •

### 7.1 CONTRIBUTIONS TO ELMY H-MODE PHYSICS

ELMy H-mode experiments on C-Mod, described in chapter 4, significantly expand the parameter range of investigation: C-Mod operation reaches the highest thermal pressure of any tokamak, up to within a factor of  $\sim 2$  of the target pedestal pressure for ITER, as well as reaching the highest magnetic field at 8 T. These experiments also entailed a significant scan in plasma current (400 – 1100 kA) and field (3.5 – 8 T), representing a broad parameter range well outside of the explored operational space on other devices, at ITER-like conditions in several respects (e.g., field, density, pressure).

The observed behavior in the pedestal are consistent with limits based in peeling-balloonning MHD instability and kinetic-balloonning turbulence (described in section 3.2 and section 3.3, respectively). Over the scan in plasma current (see section 4.3), the pressure pedestal height exhibits a trend of  $p_{\text{ped}} \sim I_p$ , while the pressure pedestal width scales as  $\Delta_{p_e} \sim I_p^{-1}$ . Within this trend, the density and temperature pedestal widths individually exhibit no systematic trend with the plasma current, while the density and temperature pedestal heights both exhibit a weakly-positive trend with current. This behavior is consistent with the expected  $\nabla p \sim I_p^2$  constraint expected from the balloonning MHD stability limit; however, there is significant scatter, which may be corrected with a more refined analysis accounting for the pedestal width. The attainable poloidal beta at the pedestal top is set largely by plasma shaping – this is consistent with the balloonning MHD limit, constrained in terms of  $\alpha_{\text{MHD}} \sim d\beta_p/d\psi$ , which over the fairly restricted pedestal width sets (to zero'th order approximation) a limit on  $\beta_{p,\text{ped}}$ , with the attainable beta increasing with shaping due its stabilizing effect on the MHD mode.

The pedestal width is seen to scale as  $\Delta \sim \beta_{p,\text{ped}}^{1/2}$ , as expected from KBM turbulence (*cf.* section 4.4.2, particularly fig. 4.19). Alternate width models (section 4.5.1) are largely discounted – the density pedestal width does not exhibit the inverse dependence on the pedestal density expected from neutral-penetration models, while the temperature pedestal exhibits no dependence on the poloidal gyroradius, in contrast to predictions based on ion-orbit loss influence on the  $\vec{E} \times \vec{B}$  sheared flow. The pressure pedestal width variation with poloidal gyroradius is explained by the strong co-variance between  $\rho_{i,\text{pol}}$  and  $\beta_{p,\text{ped}}$ . The scatter in the pedestal height versus plasma current is corrected by accounting for this variation in width. Taking the pedestal height to scale as  $p_{\text{ped}} \sim \nabla p \times \Delta_p$ , the pedestal height is predicted well by the combination of the balloonning MHD limit and the width scaling above,  $p_{\text{ped}} \sim I_p^2 \beta_{p,\text{ped}}^{1/2} \sim I_p \sqrt{n_{e,\text{ped}} T_{e,\text{ped}}}$ . To lowest-order approximation, both the pedestal width and poloidal beta are robust, with both  $\nabla p$  and  $p_{\text{ped}}$  varying as  $I_p^2$  – the inclusion

of the beta scaling accounts for much of the dependence in ELM-limited pedestals on shaping.

Strictly, the KBM model allows for secondary variation on shaping and collisionality on the mode threshold, taking the form  $\Delta = G(\nu^*, \epsilon, \dots) \beta_{p,ped}^{1/2}$  where  $G$  is a weakly-varying function (taken to be constant in the simplest model). The scale function is fitted to an average value  $\langle G \rangle = 0.0857$ , with no systematic dependence of the width on field, collisionality, shaping, or toroidal gyroradius observed (section 4.5.2).

ELMy H-mode pedestals are also tested against results from the EPED model [6], described in section 3.4, which operates based on self-consistent calculations of the peeling-balloonning MHD and KBM turbulence limits. Notably, EPED bases its calculations only on engineering target parameters, such that it may be used predictively, rather than relying on reconstructed experimental data. EPED predictions (see section 4.4) for the pressure pedestal width and height match the observed results to within the  $\sim 20\%$  systematic uncertainty of the model, with the best correspondence between prediction and experiment when the observed data is treated to only use time frames immediately preceding the ELM crash, when the pedestal structure most closely matches the point of instability. Notably, the application of the EPED model to C-Mod has motivated development of the model to treat higher collisionalities and densities than typically found on other machines.

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## 7.2 CONTRIBUTIONS TO I-MODE PHYSICS

I-mode exhibits a number of highly-desirable behaviors for reactor-scale operation – the formation of a hot, H-mode like temperature pedestal provides good energy confinement at ITER-relevant collisionality, while the absence of a density pedestal prevents the accumulation of impurities in the plasma, a particularly important trait for machines operating with large heat fluxes onto high-Z metal plasma-facing components (as is the case on C-Mod, and as expected for ITER). Moreover, I-mode appears to lack large ELMs, avoiding the large pulsed heat loads anticipated for uncontrolled ELMy H-modes on ITER without the need for active engineering solutions for ELM mitigation or suppression. The work presented in this thesis draws on a dedicated series of experiments across a range of plasma current, density, and heating power, prepared with high-quality pedestal profile data. This provides a large dataset for empirical observations of pedestal structure, with the goal of improving the understanding of I-mode performance and the potential for extrapolation to higher performance. These high-grade profiles are also useful for a detailed computational approach to the stability of the I-mode pedestal in terms of the instabilities identified with the ELM trigger, applying

the stability-analysis techniques used in section 7.1 and chapter 4 for ELM<sub>y</sub> H-mode.

### 7.2.1 Empirical Observations

Empirical observations of the I-mode pedestal structure and its impact on global performance, described in chapter 5, are illuminating in terms of the observed global behavior in I-mode.

The temperature pedestal (section 5.2.1) in I-mode exhibits some H-mode-like behavior, although the response to heating power is significantly modified. The pedestal temperature scales roughly as  $T_e \sim I_p$ , albeit with significant scatter at a given current point due to variations in heating power. This is consistent with the observed behavior in ELM<sub>y</sub> H-mode (recall that both density and temperature in ELM<sub>y</sub> H-mode are positively correlated with current, consistent with the zero'th order limit on  $\beta_{p,ped}$  at consistent shaping). Notably, the I-mode pedestal temperature meets or exceeds that found in ELM<sub>y</sub> H-mode at comparable current – a highly beneficial trait for global performance, as high temperature pedestals support steep core temperature gradients and high core temperature and pressure (and therefore fusion power density). At fixed current, the pedestal temperature exhibits a strong trend with heating power per particle,  $T_{e,95} \sim P_{net}/\bar{n}_e$ . This is distinct from the behavior in ELM<sub>y</sub> H-mode, for which the temperature responds only weakly to heating power (rather, elevated power tends to increase ELM-driven heat transport to maintain the pedestal limit). EDA H-modes, which are not constrained by the strong ELMing MHD limit, exhibit a positive trend of pedestal temperature with  $P_{net}/\bar{n}_e$ , although the sensitivity is weaker than in I-mode.

In contrast, the density profile in I-mode (section 5.2.2) exhibits markedly different behavior compared to H-mode. The edge density in I-mode is set primarily by operator fueling (via gas puffing on C-Mod), maintaining an L-mode-like profile without a strong pedestal. Moreover, the density profile is set largely independently of the temperature pedestal – given sufficient power to maintain a consistent  $P_{net}/\bar{n}_e$ , the temperature pedestal can be matched across a range of fueling levels (see fig. 5.7). This contrasts strongly with observed H-mode behavior – in MHD-limited pedestals the density and temperature exhibit an inverse relationship to maintain the lowest-order  $\beta_p$  limit, with the pedestal beta set by shaping, with the interplay between density and temperature instead playing a role in the ELM dynamics. Transport-limited pedestals exhibit a similar response to heating power, but lack the ready control of the density profile, with the pedestal density instead forced by the interplay between transport and the inward particle pinch. The L-mode-like density profile in I-mode is highly desirable for ITER scenarios, as the inward turbulent

particle pinch is necessary to sufficiently fuel the core in plasmas with high edge neutral opacity (as is found on C-Mod, and as expected for ITER).

Despite the lack of a density pedestal, the I-mode pedestal (section 5.2.3) reaches competitive levels of thermal pressure compared to H-mode, while maintaining the beneficial behavior in density and temperature. Consistent with the positive trend in temperature with plasma current, the pedestal pressure scales as  $p_{95} \sim I_p$ , with additional scatter at each current point due to heating power and fueling levels (particularly, the pressure trends strongly with  $\bar{n}_e$ , visible in fig. 5.8). The trend  $T_{e,95} \sim P_{net}/\bar{n}_e$  implies  $p_{95} \sim P_{net}$ , as is observed at fixed current. This is indicative of the weaker degradation of confinement with heating power, and is a significantly stronger response than is observed in H-mode. It should be noted, however, that the pressure pedestal is typically relaxed compared to that in comparable H-modes, exhibiting a  $\nabla p$  less than that found in H-mode, and scaling more weakly than the  $\nabla p \sim I_p^2$  expected from MHD stability.

The temperature and pressure pedestal width (see section 5.3) in I-mode appears to be quite robust, such that the peak temperature and pressure gradients trend linearly with their pedestal-top values. In particular, the pressure pedestal width exhibits no systematic dependence on poloidal beta, as expected for pedestals limited by kinetic ballooning turbulence (described in section 7.1); The pedestal is also systematically wider than predicted by the EPED1-like width scaling. Similarly, the width exhibits no systematic trend with poloidal gyroradius, collisionality, magnetic shear, or heat flux through the pedestal.

As the pedestal sets a strong constraint on global performance,  $p_{ped} \sim W_{MHD}$  (fig. 5.10), this dataset is also suitable for explorations of the global behavior in I-mode (see section 5.4). Although the I-mode pressure pedestal is more relaxed than H-mode, the high pedestal temperature, combined with stiff temperature profiles in the plasma interior, supports very high core temperatures, which provides comparable core and average pressure to H-mode provided moderate density peaking, as well as comparable normalized energy confinement (see figs. 5.19 and 5.20). Global stored energy reflects the strong response of the pedestal to heating power and fueling – stored energy scales linearly with  $P_{net}I_p$ , consistent with weak degradation of  $\tau_E$  with heating power, as well as increasing strongly with fueling, contrary to ELMy H-mode. I-mode energy confinement is examined under a power-law fit, following the form of the ITER89 and ITER98 scalings for L- and H-mode (see section 5.4.1). A simplified single-machine parameter fit reliably captures I-mode confinement over the (admittedly somewhat restricted) parameter range captures the beneficial effects of current and field on confinement, as well as the weak degradation with heating power. As an illustrative exercise, this scaling (modified with an ITER98-like machine size dependence, which

is not captured in the single-machine fit) is applied to DIII-D, ASDEX Upgrade, JET, and ITER, demonstrating the potential of I-mode operation on larger devices, with a predicted  $\tau_E$  for ITER of  $\sim 8$  s, well in excess of that expected from ITER98y2. The degradation of  $\tau_E$  with power, and plasma response to fueling, is consistent with ITER simulations supporting a method for I-mode access and approach to a  $Q = 10$  scenario on ITER [7].

### 7.2.2 Stability Modeling

The predictive computational model utilized in chapter 4, based on coupled peeling-balloonning MHD instabilities and kinetic-balloonning turbulence, are applied to the I-mode pedestal in chapter 6 with an eye towards the observed lack of large, deleterious ELMs in the regime. Peeling-balloonning MHD stability is calculated using the ELITE code, described in section 3.2.3, while the kinetic-balloonning threshold is found using an infinite-n balloonning MHD analogue calculated by BALOO (section 3.2.1).

The majority of I-mode cases are naturally free of ELMs – these cases are modeled to be strongly stable to peeling-balloonning MHD modes. This is intuitively consistent with the I-mode pedestal structure, in which the relaxed density profile reduces both the total pressure gradient (which was observed to be more relaxed than in ELMy H-mode) and the bootstrap current drive, stabilizing both peeling and balloonning modes. Similarly, these cases are modeled to be below the KBM threshold (recall that the pedestal width in I-mode is observed to lack the scaling with  $\beta_{p,ped}$  expected for pedestals at the KBM limit). The pedestal parameter space in density and temperature is consistent with the calculated stability – density and temperature (normalized to poloidal field) are found to be uncorrelated, rather than exhibiting the inverse relation expected from the peeling-balloonning limit, while the pedestal poloidal beta increases linearly with normalized current, indicative of the strongly beneficial effect of fueling on pedestal and global performance.

A minority of I-mode cases, particularly at reduced current and magnetic field, have been seen to exhibit small, intermittent ELM-like events. These events may be broken into three categories. The majority of the events are observed to be timed with the sawtooth heat pulse reaching the pedestal, and do not appear to negatively perturb the pedestal (evidenced by the lack of a crash on the edge temperature visible on the ECE signal). A minority of events, however, do appear to perturb the temperature pedestal; moreover, cases both triggered by the sawtooth heat pulse and independent of the sawtooth cycle are observed. The former, sawtooth-triggered case has also been examined for peeling-balloonning MHD and KBM stability, and is found to also be stable. The transient modification of the tem-

perature pedestal by the sawtooth heat pulse is accounted for (see fig. 6.9), and is seen to modify the pedestal in stability space, but is insufficient to reach the stability boundary. This suggests that these cases are not edge-instability-triggered ELMs of the usual type, but rather a benign sawtooth-driven  $H_\alpha$  spike, possibly driven by an ionization front in the edge neutrals from the sawtooth heat pulse without negatively perturbing the pedestal. The latter case, despite exhibiting the expected edge behavior for the ELM, is modeled (for the stationary I-mode pedestal surrounding the ELM event) to be peeling-balloonning stable, shown in fig. 6.12, indicating transient events may be triggering the ELM instability (for which the sawtooth is an obvious candidate). Work in quantifying the ELMs (or ELM-like events) in I-mode is ongoing, and cases with ELMs that do exhibit pedestal temperature perturbations have not been thoroughly examined for peeling-balloonning stability immediately at the ELM crash itself. •

### 7.3 FUTURE WORK

The development and understanding of high-performance regimes which avoid large, deleterious ELMs – either via physics solutions, in which the pedestal self-regulates such that the ELM boundary is not reached, or via engineering solutions, which externally apply means to suppress or mitigate ELMs – is of crucial importance to the planning and development of operations on ITER and beyond. Research on Alcator C-Mod has contributed greatly to this endeavor, and presents a number of potential avenues for continued research.

#### 7.3.1 *ELMy H-mode*

The ELMy H-mode continues to be a valuable research path, as it is the most common shared operational regime among tokamak experiments and is considered the baseline scenario for ITER operation (although this expectation is modified by the growing necessity of control or mitigation of large type-I ELMs). The EPED model series continues to be developed to assess this regime, as well as related regimes near the ELMing limit (e.g., QH-mode, RMP-controlled H-modes). C-Mod is an excellent test bed for this model, as it regularly operates well outside the common parameter range of other major tokamaks in terms of collisionality, field, and density, while reaching several ITER-relevant values. In particular, the strong sensitivity of higher-collisionality pedestals on C-Mod to diamagnetic effects is necessary to test more detailed calculations of the diamagnetic stabilization threshold used in ELITE. Proposed implementations of the EPED model operating on more generalized tokamak equilibria, rather than the up/down-symmetric Miller equilibria currently used, could also be benchmarked against previous EPED predictions on C-Mod, as

the experimental shape used is quite different from the model equilibrium (indeed, the accuracy of EPED calculations is remarkable given the discrepancy between model and experimental equilibria!).

### 7.3.2 *I-mode*

The desirable properties found in I-mode – good (low) impurity confinement, high core temperature with density control, lack of large, deleterious ELMs, and lack of strong degradation in energy confinement with heating power – have attracted significant interest in the fusion research community. Nevertheless, there is considerable research still necessary to develop I-mode into a readily-accessible regime in the high-performance “toolkit” for tokamak operation. These topics are currently high-priority research areas on C-Mod, with experiments planned on other machines as well.

While the work presented in this thesis forms a reasonable basis for the understanding of the stationary pedestal structure in I-mode, transient events and fluctuations – that is to say, ELMs and the weakly-coherent mode (WCM) fluctuation – may be further examined in detail. The observed ELM behavior in I-mode are quite complex: the distinction between triggering mechanisms (i.e., triggered by the sawtooth heat pulse versus spontaneous ELMs) and temperature pedestal perturbation (or lack thereof) suggests that multiple distinct phenomena may be in play, while the relative scarcity of transient ELM events in I-mode make a statistical approach difficult. This requires thorough and carefully-diagnosed experiments in I-mode, focusing on the parameter range known to trigger these events (particularly, low toroidal field), with edge and divertor diagnostics to carefully characterize the ELM dynamics. Further modeling efforts are also possible on this front – while peeling-balloonning analysis of ELMing I-mode cases indicates that the stationary pedestal structure was stable (see fig. 6.12), this analysis included substantial non-ELMing periods, leaving transient pedestal instabilities as a possibility. A more careful treatment of the KBM is also possible, accounting for the reduction of the critical gradient from the ideal-MHD result by ion-drift-resonance effects in steep temperature profiles; significant modification to the KBM threshold is seen even at  $\eta_i = L_{T_i}/L_{n_i} = 2$  (a reasonable value in H-mode) [8], such that I-mode pedestals with  $\eta_i \sim 10$  [4] may exhibit a KBM threshold significantly different from the ideal-balloonning surrogate.

Given its apparent role in regulating the density profile in I-mode, a clear understanding of the WCM is desirable. Planned experiments in the upcoming run campaign on C-Mod will explore the WCM fluctuation amplitude, radial extent, and localization in the pedestal. This data can be integrated into the existing “pedestal database” structure used in this thesis for ready analysis in terms of pedestal profiles and

engineering parameters. Modeling of the WCM in gyrokinetic and fluid codes (e.g., GYRO, BOUT++) is also planned.

Although I-mode operation has demonstrated good performance on C-Mod, its density is still restricted below that found in H-modes. In a burning plasma, heating power is set by the fusion reaction rate, proportional to  $n_e^2$  – as such, I-mode operation with increased operational window in density is an ongoing effort on C-Mod. The results presented in this thesis are promising in this regard, as the application of matched increases in fueling in heating power (such that the temperature pedestal is maintained with consistent  $P_{net}/\bar{n}_e$ ) strongly increase the pedestal pressure and global beta/stored energy, while maintaining the beneficial relaxed edge density gradient. The question remains whether large-scale (e.g., high-performance targets on ITER) can reach the necessary  $P_{net}/\bar{n}_e$  to sustain the target temperature pedestal, necessitating further study for pedestal optimization. The impact of increased fueling on pedestal stability will also be examined – while initial observations indicate that the density gradient remains relaxed at higher fueling levels (raising the SOL density apace with the pedestal density, rather than developing a density pedestal), the impact of increased fueling on the pressure gradient and bootstrap current drives may ultimately pose a peeling-balloonning MHD limit on the I-mode pedestal. On the other hand, the elevated SOL density is beneficial for power handling and divertor detachment; this, coupled with the relatively broad SOL heat-flux channel observed in I-mode, may well add divertor power handling to the list of benefits to I-mode operation.

Finally, research into I-mode access on existing larger devices is still in the initial stages – while I-mode experiments have been carried out on DIII-D and ASDEX Upgrade (with some I-mode-like features observed on JET as well) the regime has not been firmly established outside of C-Mod. Due to the significant differences in parameter space (magnetic field, size, and density, as well as edge neutral behavior on carbon-walled devices) between C-Mod and other major tokamak experiments, the window for I-mode access on other devices is not well understood despite the relative ease of access on C-Mod. Further experiments better characterizing the L-I and I-H thresholds on C-Mod, as well as a firm understanding of the edge fluctuation behavior (described above), are necessary to solidify I-mode access on existing tokamak experiments and projection to ITER operation. \*



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# A

## DIAGNOSTICS

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The dedicated pedestal experiments, both in I-mode and ELMy H-mode, presented here required an extensive suite of diagnostics to characterize pedestal behavior. Broadly, these diagnostics may be broken down into three categories:

### THOMSON SCATTERING

Details the edge Thomson scattering diagnostic, from which the high-resolution profile data used for the bulk of this thesis was gathered.

### FAST DIAGNOSTICS

Details the Electron-Cyclotron Emission (ECE) diagnostics used to track sawtooth crashes and ELM events in the plasma edge.

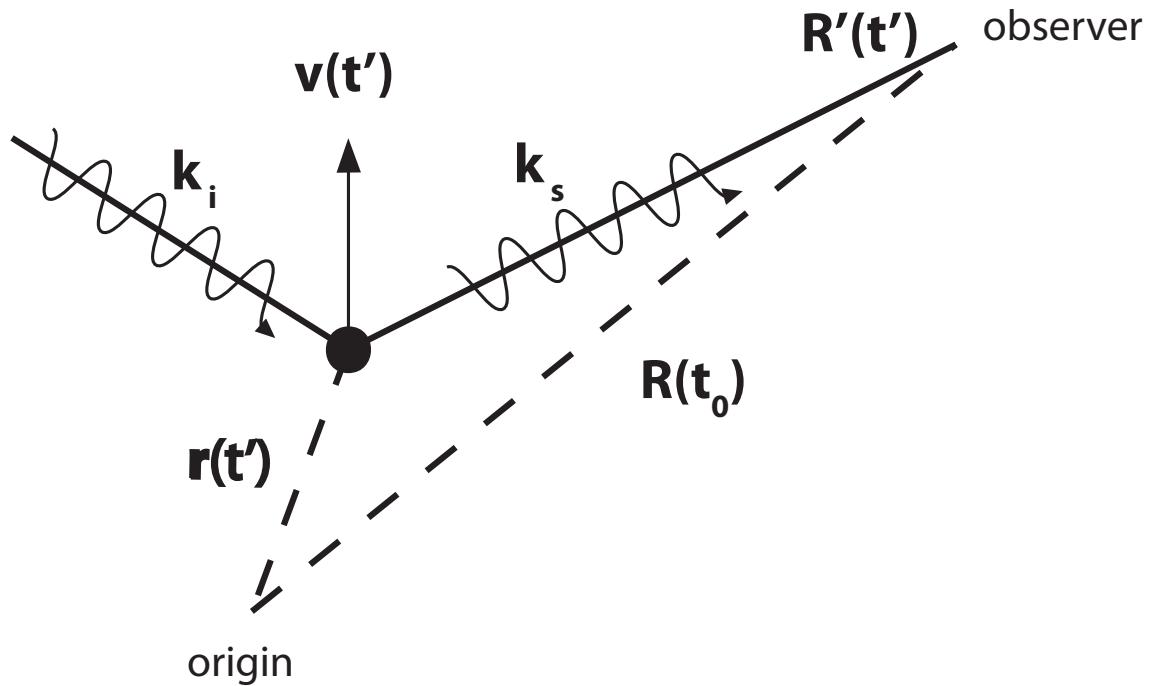
### FLUCTUATION DIAGNOSTICS

Details Reflectometry, used to characterize the mid-frequency fluctuations localized in I-mode pedestals.

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#### A.1 THOMSON SCATTERING

Due to the steep gradients in density, temperature, and pressure found in the pedestal, accurate characterization of plasma profiles in this region requires diagnostics capable of very fine spatial resolution. Measurements based on the Thomson scattering [1] of laser light off of electrons in the plasma provides the high-resolution pedestal profiles used in this thesis: Thomson scattering is a near-direct measurement of electron temperature and density, independent of bulk plasma parameters (i.e., it is unaffected by the cutoffs or reflections found in other diagnostics, and produces no significant perturbation to the plasma). Measurement via Thomson scattering produces an effective “snapshot” of the plasma parameters at each measurement point, with spatial resolution limited only by collection optics geometry, and time resolution limited by repetition rate on the lasers. Despite significant technical difficulties – for example, the high-powered lasers and sensitive collection optics needed to capture the weak scattered light and the necessity for careful calibration of density measurements – Thomson scattering diagnostics remain a versatile and powerful tool for plasma pedestal measurement, and provided the bulk of the profile data used in this thesis.



**Figure A.1:** Coordinate system considered for Thomson scattering, with the incident wave of wavenumber  $\vec{k}_i$  incident on a particle at  $\vec{r}(t')$  for retarded time  $t'$ . The scattered wave  $\vec{k}_s$  is drawn to an observer at  $\vec{R}'(t')$ .

### A.1.1 Principles of Thomson Scattering

An intuitive picture of the Thomson scattering phenomenon may be obtained by the consideration of a stationary, free electron with an EM wave impinging on it. The particle will be accelerated by the wave (approximately sinusoidally for E-field-dominated acceleration at nonrelativistic speeds), causing it to radiate. Any motion of the electron will cause Doppler shifting in the scattered radiation – motion relative to the incident wave shifts the incident frequency  $\omega_i$ , at which the particle oscillates, while motion relative to an observer shifts the scattered wave. This geometry for general positions of the particle and observer is given in fig. A.1.

The scattered electric field from a generally-accelerated electron moving at  $\vec{\beta} = \vec{v}/c$  is given from the Lienard-Wiechert potentials [2, §7],

$$\vec{E}_s = \frac{-e}{4\pi\epsilon_0} \left[ \frac{1}{\kappa^3 R c} \hat{s} \times \left( (\hat{s} \times \vec{\beta}) \times \dot{\beta} \right) \right]_{t'} \quad (\text{A.1})$$

$$\kappa = 1 = \frac{\vec{R}' \cdot \vec{v}}{R' c} = 1 - \hat{s} \cdot \vec{\beta}, \quad t' = t - \frac{R'}{c}$$

where  $\hat{s}$  indicates the unit vector along the scattering direction,  $\vec{R} = R\hat{s}$  is the vector to the observer,  $\kappa$  is a relativistic scale factor, and  $t'$  is

the relativistic retarded time. The apostrophe indicates a parameter evaluated at the retarded time, i.e.,  $R' = R(t')$ ; the bracketed term in eq. (A.1) likewise is evaluated at  $t'$ . The scattered power per solid angle is given by

$$\begin{aligned}\frac{dP_s}{d\Omega} &= R^2 \vec{S} \cdot \hat{s} = R^2 \frac{1}{\mu_0} (\vec{E} \times \vec{B}) \cdot \hat{s} \\ &= R^2 \epsilon_0 c (\vec{E}_s \times (\hat{s} \times \vec{E}_s)) \cdot \hat{s} = R^2 c \epsilon_0 |\vec{E}_s|^2\end{aligned}\quad (\text{A.2})$$

Relativistically, the electron motion (which in turn sets the field determined by eq. (A.1)) is given by

$$\dot{\beta} = \frac{d}{dt} (\gamma m_e \vec{v}) = -e (\vec{E}_i + \vec{v} \times \vec{B}_i) \quad (\text{A.3})$$

where  $\gamma = (1 - \beta^2)^{-1/2}$  is a relativistic scale factor. Thus

$$m_e \gamma \dot{\beta} + \gamma^3 m_e \beta (\vec{\beta} \cdot \dot{\beta}) = -e \left( \frac{\vec{E}_i}{c} + \vec{\beta} \times \vec{B}_i \right) \quad (\text{A.4})$$

Dotting  $\vec{\beta}$  into this and substituting,

$$\dot{\beta} = -\frac{e}{m_e \gamma} \left( \frac{\vec{E}_i}{c} - \frac{\vec{\beta} \cdot \vec{E}_i}{c} \vec{\beta} + \vec{\beta} \times \vec{B}_i \right) \quad (\text{A.5})$$

The general relativistic solution to eqs. (A.1) and (A.2) with the above is rather intractible, although full relativistic treatments have been undertaken [3, 4, 5, 6]. However, the radiated field may be simplified substantially in the nonrelativistic limit – in the limit of  $\beta \ll 1$ , the acceleration is simply

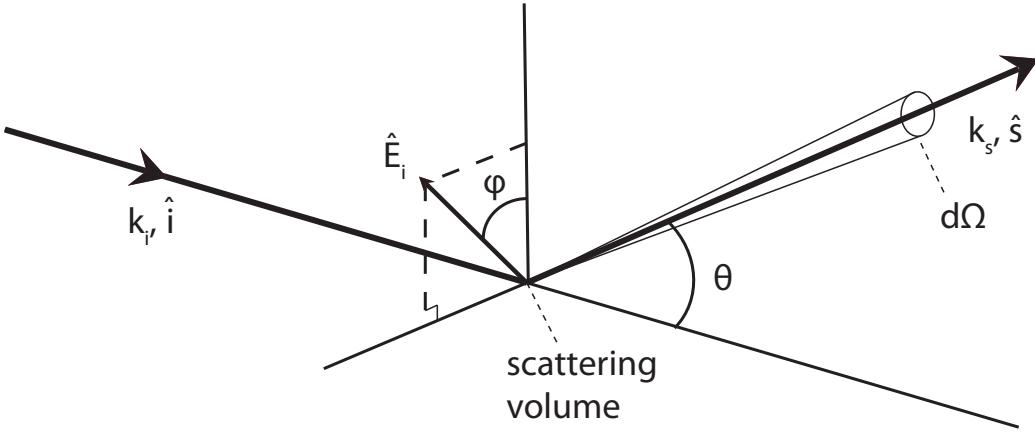
$$\dot{\beta} = -\frac{e}{m_e c} \vec{E}_i \quad (\text{A.6})$$

and the scattered field is

$$\vec{E}_s = \frac{e^2}{4\pi\epsilon_0 m_e c^2} \left[ \left[ \frac{1}{R} \hat{s} \times (\hat{s} \times \vec{E}_i) \right] \right]_{t'}, \quad (\text{A.7})$$

Recalling the classical electron radius,

$$r_e = \frac{e^2}{4\pi\epsilon_0 m_e c^2} \quad (\text{A.8})$$



**Figure A.2:** Definitions of the angular dependences in the Thomson scattering geometry: namely, the angle  $\theta$  between the incident wave direction  $\hat{i}$  and scattering direction  $\hat{s}$ , and the polarization angle  $\phi$  of the incident electric field  $\hat{E}_i$  with respect to the projection of  $\hat{s}$  into the polarization plane.

the radiated power is given by

$$\frac{dP_s}{d\Omega} = r_e^2 c \epsilon_0 E_{i0}^2 \llbracket \hat{s} \times (\hat{s} \times \hat{E}_i) \rrbracket^2 \cos^2(\vec{k}_i \cdot \vec{r}' - \omega_i t') \quad (\text{A.9})$$

separating the magnitude, direction, and phase (evaluated at  $t'$ ) of the incident field.

We may first consider the scattering direction dependence,

$$\llbracket \hat{s} \times (\hat{s} \times \hat{E}_i) \rrbracket_{t'}^2 \quad (\text{A.10})$$

Defining the angular geometry as in fig. A.2 for the scattering angle  $\theta$  between the incident wave direction  $\hat{i}$  and scattering direction  $\hat{s}$ , and the polarization angle  $\phi$  (defined between  $\hat{E}_i$  and the projection of  $\hat{s}$  into the polarization plane), this reduces to (cf. [1, §1.7])

$$\llbracket \hat{s} \times (\hat{s} \times \hat{E}_i) \rrbracket^2 = 1 - \sin^2 \theta \cos^2 \phi \quad (\text{A.11})$$

Since the incident power flux is given by

$$S_i = c \epsilon_0 E_{i0}^2 \cos^2(\vec{k}_i \cdot \vec{r}' - \omega_i t') \quad (\text{A.12})$$

We may separate the incident flux and scattering by

$$\frac{dP}{d\Omega} = S_i \frac{d\sigma_t}{d\Omega} \Rightarrow \frac{d\sigma_t}{d\Omega} = r_e^2 [1 - \sin^2 \theta \cos^2 \phi] \quad (\text{A.13})$$

defining a scattering cross-section  $\sigma_t$ . Integrating over  $d\Omega$ ,

$$\sigma_t = \frac{8\pi}{3} r_e^2 = 6.65 \times 10^{-29} \text{ m}^2 \quad (\text{A.14})$$

The extremely small cross-section for Thomson scattering necessitates high-powered lasers and sensitive collection optics – for example, the fraction of photons scattered from a segment along the laser beam path of length  $L$  with electron density  $n_e$  is given simply by  $L n_e \sigma_t$ . For  $L = 1 \text{ mm}$  and  $n_e = 1 \times 10^{20} \text{ m}^{-3}$ , Thomson scattering faces an attenuation factor on the order of  $\sim 10^{-11}$  to the incident photon count from the laser.

The phase of the scattered wave is determined by a retarded-time evaluation of the incident phase,  $\vec{k}_i \cdot \vec{r}(t') - \omega_i t'$ . Substituting  $\vec{r}(t') = \vec{r}_0 + \vec{v}t'$ , and assuming  $R(t') \approx R(t_0)$  (which holds for observers far from the scattering volume,  $R \gg r$ ) we may rewrite the retarded time as

$$t' = \frac{1}{1 - \hat{s} \cdot \vec{\beta}} \left( 1 - \frac{R}{c} + \frac{\hat{s} \cdot \vec{r}_0}{c} \right) \quad (\text{A.15})$$

Substituting, the phase argument becomes

$$k_i \frac{1 - \hat{i} \cdot \vec{\beta}}{1 - \hat{s} \cdot \vec{\beta}} R - \omega_i \frac{1 - \hat{i} \cdot \vec{\beta}}{1 - \hat{s} \cdot \vec{\beta}} t - k_i \frac{1 - \hat{i} \cdot \vec{\beta}}{1 - \hat{s} \cdot \vec{\beta}} \hat{s} \cdot \vec{r}_0 + \vec{k}_i \cdot \vec{r}_0 \quad (\text{A.16})$$

where  $\hat{i}$  is the incident wave propagation direction. We have naturally arrived at the Doppler-shifted frequency,

$$\begin{aligned} \omega_s &= \frac{1 - \hat{i} \cdot \vec{\beta}}{1 - \hat{s} \cdot \vec{\beta}} \omega_i \\ \vec{k}_s &= k_i \frac{1 - \hat{i} \cdot \vec{\beta}}{1 - \hat{s} \cdot \vec{\beta}} \hat{s} = \frac{\omega_s}{c} \hat{s} \end{aligned} \quad (\text{A.17})$$

so the phase is

$$\vec{k}_i \cdot \vec{r}' - \omega_i t' = k_s R - \omega_s t + (\vec{k}_s - \vec{k}_i) \cdot \vec{r}_0 \quad (\text{A.18})$$

Alternately, we may define

$$\begin{aligned} \vec{k} &= \vec{k}_s - \vec{k}_i \\ \omega &= \omega_s - \omega_i = \vec{k} \cdot \vec{v} \end{aligned} \quad (\text{A.19})$$

We may establish the frequency spectrum of the scattered radiation by taking the Fourier transform of the scattered field,

$$\vec{E}_s(\omega_s) = \int \vec{E}_s(t) e^{i\omega_s t} dt \quad (\text{A.20})$$

At retarded time,  $dt = \kappa' dt'$ , and

$$\vec{E}_s(\omega_s) = \frac{r_e}{R'} \int \kappa' \Pi \cdot \vec{E}_i(\vec{r}', t') e^{-\omega_s (t' + \frac{R'}{c} - \frac{\hat{s} \cdot \vec{r}'}{c})} dt' \quad (\text{A.21})$$

Here, for generality we use the polarization tensor  $\Pi$ , which includes relativistic effects – in the nonrelativistic limit  $\Pi = \hat{s}\hat{s} - \mathbf{I}$  such that  $\Pi \cdot \vec{E}_i = \hat{s} \times (\hat{s} \times \vec{E}_i)$ . Using  $\vec{E}_i(\vec{r}, t) = \vec{E}_{i0} \exp(i(\vec{k}_i \cdot \vec{r} - \omega_i t))$  and eq. (A.19),

$$\vec{E}_s(\omega_s) = \frac{r_e}{R'} e^{ik_s R'} \int \kappa' (\Pi \cdot \hat{E}_i) E_{i0} e^{i(\omega t' - \vec{k} \cdot \vec{r}')} dt' \quad (\text{A.22})$$

Integrating and substituting  $\omega_s = 2\pi\nu_s$ ,

$$\vec{E}_s(\nu_s) = \frac{r_e}{R'} e^{ik_s R} 2\pi \kappa (\Pi \cdot \vec{E}_{i0}) \delta(\vec{k} \cdot \vec{v} - \omega) \quad (\text{A.23})$$

We may thus construct the scattered power per solid angle per unit frequency

$$\frac{d^2 P}{d\Omega d\nu_s} = r_e^2 |\Pi \cdot \hat{E}_i|^2 (c\epsilon_0 E_{i0}^2) \delta \left( \nu_s - \frac{1 - \hat{i} \cdot \vec{\beta}}{1 - \hat{s} \cdot \vec{\beta}} \nu_i \right) \quad (\text{A.24})$$

So we have established the scattered power spectrum in solid angle and frequency of a single electron as a function of scattering direction (encoded in  $\Pi \cdot \hat{E}_i$ ) and incident laser energy (in the incident Poynting flux  $\langle S_i \rangle = c\epsilon_0 E_{i0}^2$ ). The scattered spectrum locked to a single frequency by the Dirac delta function, forcing the scattered spectrum to radiate strictly at the Doppler-shifted frequency set by the electron motion.

To consider the spectrum from a population of electrons, we must consider the interactions between nearby electrons. On length scales comparable to the electron Debye length  $\lambda_{De}$  (eq. (1.1)), electrons in the plasma screen out incident electric fields – this organized motion leads to interference in the scattered radiation, referred to as *collective*

or *coherent scattering*. The full solution for the scattered spectrum (see [1, §3]) may be expanded in a series in the factor

$$\alpha = \frac{1}{k\lambda_{De}} \quad (\text{A.25})$$

Coherent effects are negligible in the limit of  $\alpha \ll 1$ , at which the scattering is said to be *incoherent* or *noncollective* – the radiation from a population of electrons is simply the sum of each individual contribution. For the effective scattering wavevector,  $\vec{k} = \vec{k}_s - \vec{k}_i$  (eq. (A.19)),

$$\begin{aligned} |\vec{k}| &= \sqrt{k_s^2 + k_i^2 - 2k_s k_i \cos \theta} \\ &\approx \sqrt{2} k_i \sqrt{1 - \cos \theta} = \sqrt{2} k_i \sqrt{2 \sin^2 \left( \frac{\theta}{2} \right)} \end{aligned} \quad (\text{A.26})$$

assuming  $k_s \approx k_i$ . Thus the noncollective requirement reduces to

$$\frac{1}{2k_i \sin(\theta/2)\lambda_{De}} \ll 1 \Rightarrow \frac{\lambda_i}{\lambda_{De}} \ll 4\pi \sin \left( \frac{\theta}{2} \right) \quad (\text{A.27})$$

This condition is readily satisfied at near-perpendicular scattering ( $\theta \approx 90^\circ$ , where the scattering amplitude is maximized) and with laser wavelengths much smaller than the Debye length ( $\lambda_{De} \sim 10 - 100 \mu\text{m}$  at tokamak conditions, compared to the  $\lambda_i \sim 1 \mu\text{m}$  IR lasers commonly used for Thomson scattering photon sources).

Thus, the incoherent scattered spectrum is simply the sum of contributions from each electron in the scattering volume – the spectrum from a population described by the distribution function  $f_e(\vec{r}, \vec{v})$  is

$$\frac{d^2P}{d\Omega dv_s} = 2\pi r_e^2 \int_V \langle S_i \rangle \int |\Pi \cdot \hat{E}_i|^2 f_e(\vec{r}, \vec{v}) \kappa^2 \delta(\vec{k} \cdot \vec{v} - \omega) d^3v d^3r \quad (\text{A.28})$$

For small scattering volumes, the electron distribution function is approximately uniform in space. In the nonrelativistic limit,  $\Pi \cdot \hat{E}_i$  is independent of velocity, thus the spatial contribution may be separated out:

$$\int_V \langle S_i \rangle |\Pi \cdot \hat{E}_i|^2 d^3r \quad (\text{A.29})$$

encoding the incident photon flux (from the Poynting vector of the laser) and the scattering direction dependence. The velocity integral (noting  $\kappa \approx 1$  in the nonrelativistic case) is

$$\int f(\vec{v}) \delta(\vec{k} \cdot \vec{v} - \omega) d^3\vec{v} \quad (\text{A.30})$$

Splitting the velocity into components parallel and perpendicular to  $\vec{k}$ ,  $\vec{v}_\perp$ ,  $\vec{v}_k$ , this is

$$\int f(\vec{v}_\perp, \vec{v}_k) \delta(kv_k - \omega) d^2\vec{v}_\perp dv_k = \int f_k(v_k) \delta(kv_k - \omega) dv_k \quad (\text{A.31})$$

utilizing the normalization required for  $f(\vec{v})$  to solve the integrals over  $\vec{v}_\perp$ . For a Maxwellian (eq. (1.5)) the distribution along the effective wavevector  $\vec{k}$  is

$$f_k(v_k) = n_e \frac{1}{v_t \sqrt{\pi}} e^{-v_k^2/v_t^2} \quad (\text{A.32})$$

thus the above is solvable,

$$\int f_k(v_k) \delta(kv_k - \omega) dv_k = \frac{1}{k} f_k \left( \frac{\omega}{k} \right) \quad (\text{A.33})$$

Substituting into eq. (A.28),

$$\begin{aligned} \frac{d^2P}{d\Omega dv_s} &= 2\pi r_e^2 \left[ \int_V \langle S_i \rangle |\hat{s} \times (\hat{s} \times \hat{E}_i)|^2 d^3\vec{r} \right] \times \\ &\quad \frac{1}{\sqrt{\pi k}} \frac{n_e}{v_t} \exp \left( -\frac{\omega^2}{k^2 v_t^2} \right) \end{aligned} \quad (\text{A.34})$$

Substituting  $k \approx 2k_i \sin(\theta/2) = (4\pi/\lambda_i) \sin(\theta/2)$ , the exponent is

$$-\frac{(\omega_s - \omega_i)^2}{4 \frac{4\pi^2}{\lambda_i^2} \sin^2(\theta/2) v_t^2} \approx -\frac{c^2 (\lambda_s - \lambda_i)^2}{4 \lambda_i^2 v_t^2 \sin^2(\theta/2)} \quad (\text{A.35})$$

Converting from a frequency to a wavelength spectrum, and assuming the scattering volume to be sufficiently small that the scattering angle and incident Poynting flux are uniform (thus  $\int \langle S_i \rangle d^3\vec{r} =$

**Figure A.3:** Spectral functions normalized to density and laser power, evaluated at  $\theta = \phi = \pi/2$ . The spectrum spreads farther from the laser line at higher temperature, as well as blue-shifting due to relativistic effects.



$\langle S_i \rangle AL = P_i L$  for laser cross-section  $A$ , scattering volume  $L$ , and laser power  $P_i$ ) the nonrelativistic scattering spectrum is

$$\frac{d^2P}{d\Omega d\lambda_s} = P_i r_e^2 n_e L |\hat{s} \times (\hat{s} \times \hat{E}_i)|^2 S(T_e, \theta, \lambda_s)$$

$$S(T_e, \theta, \lambda_s) = \frac{1}{2\sqrt{\pi} \sin(\theta/2)} \frac{c}{\lambda_i v_t} \exp\left(-\frac{c^2(\lambda_s - \lambda_i)^2}{4v_t^2 \lambda_i^2 \sin^2(\theta/2)}\right) \quad (\text{A.36})$$

This expression is a Maxwellian centered at  $\lambda = \lambda_i$  with a spread determined by the electron temperature  $T_e$  (manifesting in the thermal velocity  $v_t$ ) and the scattering angle  $\theta$ . Recalling the angle  $\phi$  defined between the incident polarization  $\hat{E}_i$  and the scattering direction  $\hat{s}$  (see fig. A.2),  $|\hat{s} \times (\hat{s} \times \hat{E}_i)|^2 = \sin^2 \phi$  is maximized for scattering perpendicular to the incident laser polarization.

This analysis breaks down for relativistic electron populations. However, relativistic effects (see [1, §9]) may be expressed as a polynomial correction to eq. (A.36),

$$S_{\text{rel}}(T_e, \theta, \lambda_s) = S(T_e, \theta, \lambda_s) \left[ 1 - \frac{3.5(\lambda_s - \lambda_i)}{\lambda_i} + \frac{c^2(\lambda_s - \lambda_i)^3}{4v_t^2 \lambda_i^2 \sin^2(\theta/2)} \right] \quad (\text{A.37})$$

The relativistic correction breaks the symmetry of the Maxwellian spectrum, introducing a net blue shift to the spectrum. Physically, this is due to “relativistic headlighting,” in which the radiation from an accelerating relativistic particle is biased forward of its motion – The radiated power is stronger from particles moving toward the observer

(thus with a blue Doppler shift to their emissions). The spectral form factor  $S(T_e, \theta, \lambda_s)$  is shown in figure fig. A.3, illustrating the width dependence of the spectrum on the electron temperature and the blue shifting evident in the spectrum even at relatively low plasma temperatures.

Examination of eqs. (A.36) and (A.37) readily illustrates the method for extracting  $n_e$  and  $T_e$  measurements from the Thomson scattering spectrum – the spread of the spectrum of scattered radiation is directly tied to the electron temperature, while the integrated amplitude gives electron density (as the total scattered power is linearly proportional to  $n_e$ ). Assumptions regarding the Maxwellian distribution of the electrons allows accurate measurement of the electron profile with relatively simple hardware, detailed in the next section.

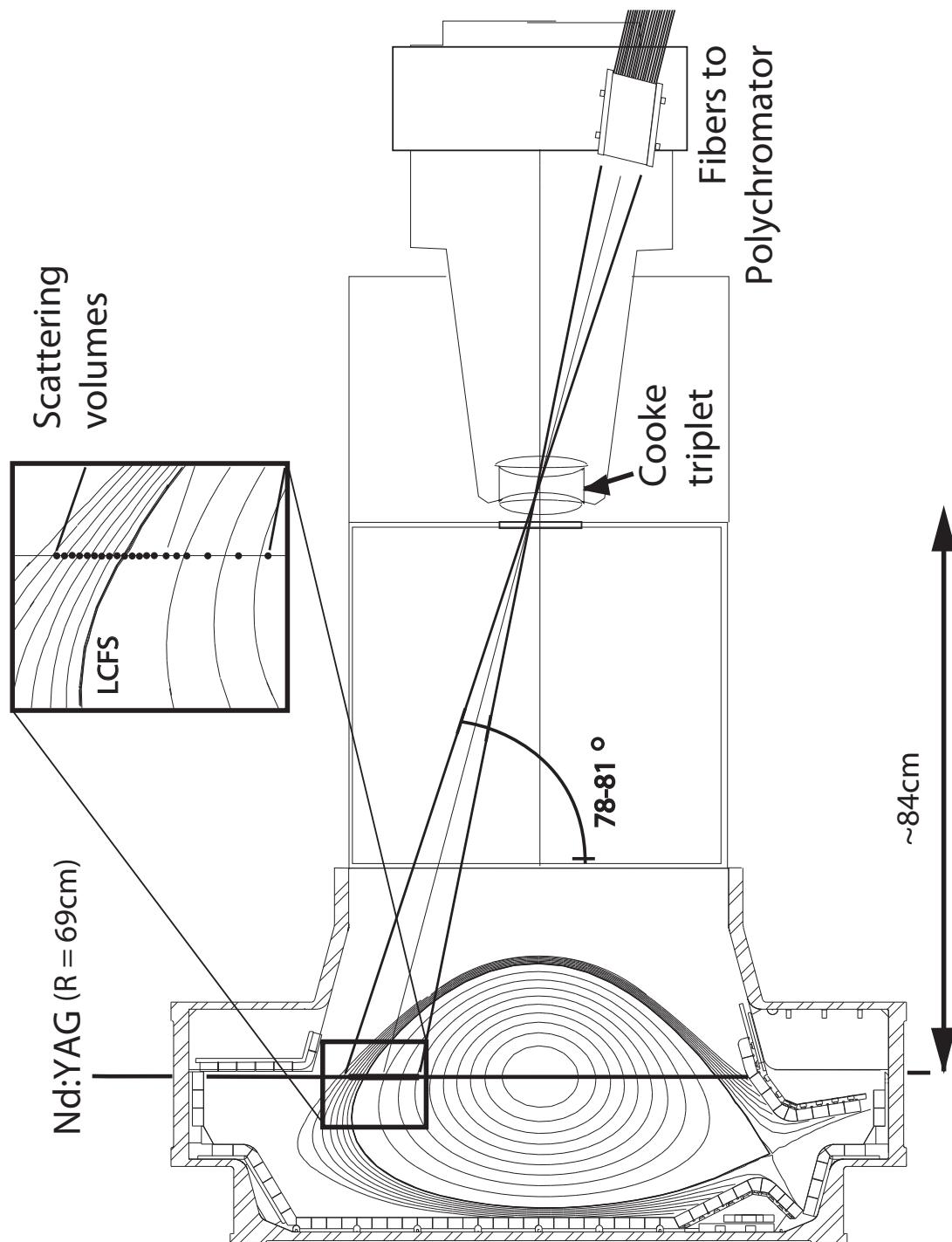
### A.1.2 Edge Thomson Scattering on C-Mod

High-resolution density and temperature measurements on C-Mod are achieved with the core [7, 8] and edge [9, 10, 11] Thomson Scattering systems. While extracting density and temperature from the general Thomson-scattered spectrum (eq. (A.28)) for an arbitrary electron distribution  $f_e(\vec{r}, \vec{v})$  is intractible, the spectrum for a thermal electron distribution is well-characterized (see eqs. (A.36) and (A.37)) and can be measured with a relatively simple system.

Both the core and edge TS systems measure light scattered from a pair of neodymium-doped yttrium-aluminum garnet (Nd:YAG) lasers with  $\lambda_i = 1064 \text{ nm}$  fired vertically through the plasma at  $R \sim 69 \text{ cm}$  such that it passes roughly through the magnetic axis. The lasers are each fired at 50 Hz  $180^\circ$  out of phase, such that the pair produce one hundred  $\sim 5 \text{ ns}$  pulses per second, taking effective “snapshots” of the plasma profile. Each pulse provides  $\sim 1 \text{ J}$  of laser energy, corresponding to roughly  $5 \times 10^{18}$  photons per laser pulse, ensuring sufficient collected photons even after the significant attenuation inherent in Thomson scattering. Focusing optics mounted at the vertical entrance port constrict the beam to a  $\sim 2 \text{ mm}$  width through the plasma.

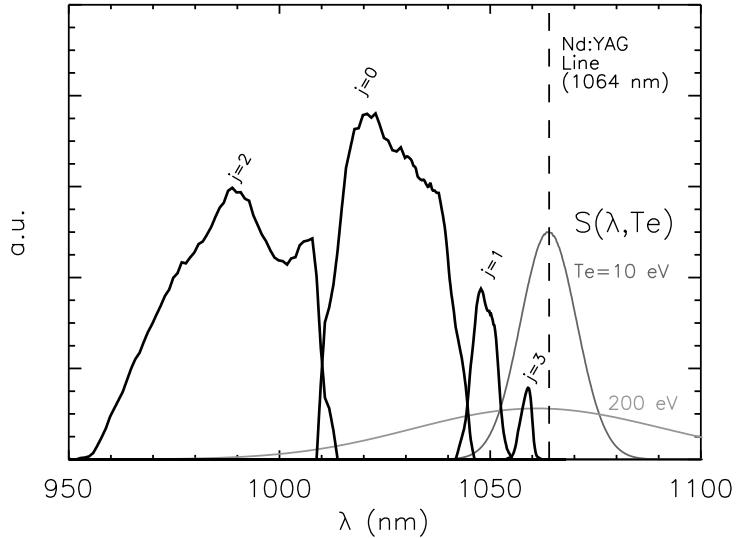
The scattered photons are focused through a Cooke triplet with 1:2 demagnification mounted at an outboard-midplane access port onto an array of fiber-optic collectors mounted on an actuated plate (see fig. A.4). Dedicated edge-viewing fibers are mounted in an adjustable block at the base of the plate, viewing the upper plasma at a scattering angle of  $\theta \sim 80^\circ$ . While the  $\sim 1 \text{ cm}$  spot size of the core fibers is sufficient to resolve the core plasma profile, the small radial extent of the pedestal on C-Mod necessitates the millimeter resolution provided by the edge fibers.

The edge collection fibers deliver the scattered light to a filter polychromator array with 25 available spatial channels divided into four spectral bands. The spectral bandpasses, shown in fig. A.5, are de-



**Figure A.4:** Layout of collection optics for the core and edge Thomson scattering diagnostics on Alcator C-Mod. Two Nd:YAG lasers are fired vertically through the plasma near the magnetic axis, with the scattered light focused through a Cooke triplet at the outboard midplane onto an array of fiber optics. The positions of the high-resolution edge scattering volumes are highlighted in the inset.

**Figure A.5:** Normalized spectral response functions of the edge TS polychromator bandpasses, compared to characteristic scattered spectra at 10 eV and 200 eV.



signed such that the laser line is excluded from the captured light (reducing noise from reflected laser light incident on the fibers) while covering the expected spread in the scattered spectrum across a range of temperatures. Extracting  $n_e$  and  $T_e$  for each spatial channel is conceptually straightforward – the total signal in all spectral channels is analogous to the integrated area under the scattered spectrum (and thus  $n_e$ ), while the relative signal strengths between spectral channels is set by the spread in the spectrum (thus  $T_e$ ). For temperatures below  $\sim 50$  eV (with the true lower bound dependent on the local density), the scattered spectrum is largely restricted to the  $j = 3$  channel, setting a lower bound on the temperature measurement. Similarly, for  $T_e \gtrsim 800$  eV the spectral response in  $j = 1$  and  $j = 3$  is flat, limiting the effectiveness of those spectral bandpasses in constraining the temperature measurement.

Although the  $n_e$  and  $T_e$  measurements from Thomson scattering require careful calibration and sensitive IR optics, the edge TS system provides reliable high-resolution profile measurements across a range of parameters found in the C-Mod edge. Further details on the edge TS hardware, calibration, and data analysis procedures is available in [11, §3].

## A.2 FAST DIAGNOSTICS

In addition to the high spatial resolution necessary to diagnose the pedestal profile – provided by the edge Thomson Scattering system – a suite of diagnostics with high time resolution is desirable to capture rapid variations in plasma parameters near the pedestal. For our purposes, we focus on the electron-cyclotron emission (ECE) and  $H_\alpha$  emission diagnostics. ECE provides fast measurement of local elec-

tron temperature, useful to track the impact of transient events like ELM crashes or sawtooth heat pulses on the pedestal temperature.  $H_\alpha$  line emission in the plasma edge provides a measurement of density expelled into the plasma exhaust, marking both the particle transport changes during high-confinement modes and transient density bursts into the SOL during ELM crashes.

### A.2.1 Electron-Cyclotron Emission

Electron-cyclotron emission, or ECE [2, §5.2], arises from the radiation driven by gyro motion of electrons in a magnetized plasma. Relativistically, the electron motion is described by

$$\frac{d}{dt}(\gamma m_e \vec{v}) = -e(\vec{v} \times \vec{B}) \quad (\text{A.38})$$

resulting in gyro-motion at the (relativistic) cyclotron frequency

$$\omega_c = \frac{eB}{\gamma m_e} \quad (\text{A.39})$$

While it is conceptually straightforward to substitute this motion into the Lienard-Wiechert potentials, eq. (A.1), the complexity of the motion results in a rather intractible general form for the radiation even for a single electron, requiring an infinite sum of Bessel functions to characterize the harmonics of the radiation. Fortunately, ECE systems may exploit the trait that electrons undergoing gyro-motion will also *absorb* radiation at the same frequency as their emitted radiation. Over a given path  $s$  through the plasma, the absorption is governed by the absorption coefficient  $\alpha(\nu)$  (fractional absorption per unit path length), with which the radiated intensity  $I(\nu)$  is given by

$$\frac{dI}{ds} = j(\nu) - I\alpha(\nu) \quad (\text{A.40})$$

where  $j(\nu)$  is the frequency-dependence emissivity. For two points  $s_1$ ,  $s_2$  along a path, this is solved by

$$I(s_2) = I(s_1)e^{\tau_1 - \tau_2} + \int_{s_1}^{s_2} j(\nu)e^{\tau - \tau_2} ds \quad (\text{A.41})$$

$$\tau \equiv \int_s \alpha(\nu) ds$$

for the optical depth  $\tau$ . When the optical depth for a given path  $\tau_{21} \equiv \tau_2 - \tau_1$  satisfies  $\tau_{21} \gg 1$ , the plasma within the path absorbs all

radiation incident upon it – it may then be treated as optically black, with the radiation given by the blackbody intensity

$$I(\nu) = \frac{\nu^2}{c^2} \frac{h\nu}{e^{h\nu/T} - 1} \approx \frac{\nu^2 T}{c^2} \quad (\text{A.42})$$

with the approximation holding for  $h\nu \ll T$ . In a broad range of tokamak plasma conditions, the first few harmonics will be optically thick, meaning that the intensity of those harmonics is a direct, straightforward measurement of the electron temperature.

This analysis must be modified somewhat to account for a spatially-varying magnetic field (for example, the  $B_T \sim 1/R$  variation in a tokamak). Fortunately, for a given frequency  $\nu_0$  the emission is only strong close to the position of exact resonance. Through this resonance layer at location  $s_0$ , the optical depth for a given harmonic  $m$  is given by

$$\tau_m = \frac{\alpha_m(s_0)}{m |d\omega_c/ds|} \quad (\text{A.43})$$

with the emission given by

$$I(\nu_0) = \frac{\nu_0^2 T(s_0)}{c^2} (1 - e^{-\tau_m}) \quad (\text{A.44})$$

Thus electron-cyclotron emission in a tokamak allows easy measurement of electron temperature. By observing emission within a given frequency band, the measurement may be localized to a resonance layer, the location of which is calculated by the known magnetic field variation  $d\omega_c/ds$ .

High time resolution ECE measurements are provided by a suite of diagnostics on C-Mod. Two grating polychromator systems (GPCs) view the plasma from the outboard midplane with coverage through the radial plasma profile on the high-field and low-field sides, though the spatial channel locations depend on the magnetic field and wavelength settings of the gratings [12]. The original nine-channel system, (GPC1) was originally developed for the MTX tokamak [13]. This is complemented by a second system, GPC2 [14], which adds 19 spatial channels at the midplane. These systems provide good frequency resolution,  $\Delta f/f < 1\%$ , with 10  $\mu\text{s}$  time resolution and  $\sim 10 \text{ eV}$  noise levels for the signal. However, due to geometric effects and frequency broadening, the system is only capable of  $\sim 1 \text{ cm}$  spatial resolution [12]. An additional heterodyne ECE system developed by the Fusion Research Center for C-Mod [15, 16], is capable of higher spatial and temporal resolution measurements – the off-midplane viewing angle, when mapped to the outboard midplane, provides  $\sim 4 \text{ mm}$  radial resolution, with  $\sim 100 \text{ ns}$  time resolution, capable of resolving local

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temperature fluctuations with low noise levels.

The spatial resolution provided by these systems is more than sufficient to resolve core  $T_e$  profiles, and has historically been used for temperature pedestal measurements by sweeping the toroidal field (and therefore channel position) in otherwise steady plasmas [17]. However, the spatial resolution of the system is not, on its own, sufficient to resolve the sub-centimeter pedestal on C-Mod. Rather, ECE measurements from channels near the pedestal top are utilized in this thesis to track rapid perturbations to the pedestal temperature from sawtooth heat pulses or ELM crashes. These perturbations occur at frequencies typically in the range of 10 – 100 kHz, comparable to the framerate of the Thomson Scattering system, such that TS datapoints are effectively randomized in their timing relative to the perturbation cycle. ECE data is used to prepare specialized profiles, with TS datapoints masked for a particular phase of the perturbation cycle.

### A.3 FLUCTUATION DIAGNOSTICS

A firm understanding of plasma fluctuations is necessary to characterize high-performance regimes. Turbulent fluctuations drive enhanced transport of energy and particles out of the plasma, and it is the suppression of these fluctuations, particularly in the plasma edge, that defines high-performance operation. Conversely, beneficial fluctuations regulate the pedestal to allow stationary ELM-free operation (e.g., in EDA H-mode, QH-mode, and I-mode). Thus, an extensive suite of diagnostics to measure global and local fluctuation levels are maintained on C-Mod. One of these, the O-mode reflectometer system, is a standard tool for I-mode identification and characterization, and is detailed here.

#### A.3.1 Reflectometry

As plasmas are composed of freely-interacting charged particles, electromagnetic waves interact quite strongly with the plasma. The dispersion relation for a wave of frequency  $\omega$  and wavevector  $\vec{k}$  (alternately, refractive index  $\vec{N} = \vec{k}c/\omega$ ) is characterized (in the cold plasma approximation) by the Appleton-Hartree formula [2, §4],

$$N^2 = 1 - \frac{X(1-X)}{1-X - \frac{1}{2}Y^2 \sin \theta \pm \left[ \left( \frac{1}{2}Y^2 \sin^2 \theta \right)^2 + (1-X)^2 Y^2 \cos^2 \theta \right]^{1/2}} \quad (\text{A.45})$$

where  $X = \omega_p^2/\omega^2$ ,  $Y = \omega_c/\omega$ , and  $\theta$  is the angle between  $\vec{k}$  and the background magnetic field  $\vec{B}_0$ . For waves propagating perpendicular to the field ( $\theta = \pi/2$ ), this reduces to two solutions:

$$\begin{aligned} N^2 &= 1 - X \\ N^2 &= 1 - \frac{X(1-X)}{1-X-Y^2} \end{aligned} \quad (\text{A.46})$$

which are called the *ordinary* or *O-mode*, and *extraordinary* or *X-mode* respectively. We primarily consider the O-mode propagation. Recall that the plasma frequency  $\omega_p$  characterizes a natural “ringing” rate at which the plasma rearranges itself in response to a changing electric field – this screens out electromagnetic waves with frequencies  $\omega < \omega_p$ . As the wave propagates inward from the edge the plasma density increases, such that  $X \rightarrow 1$ . Above this point, the *cutoff*, the wave is evanescent with imaginary  $N$  and will reflect from the cutoff layer. The cutoff density  $n_c$  is trivially obtained from the above,

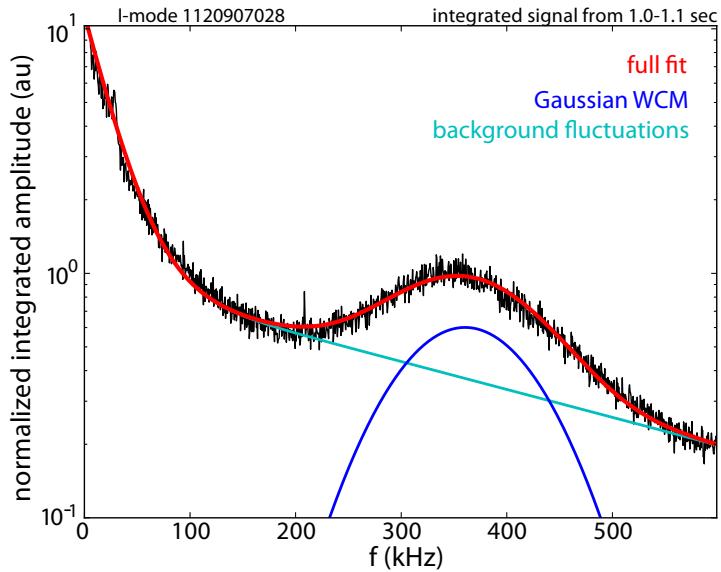
$$n_c = \frac{m_e \epsilon_0}{e^2} \omega^2 = \left( \frac{f}{89.8} \right)^2 \quad (\text{A.47})$$

where  $n_c$  is in  $10^{20} \text{ m}^{-3}$  and  $f$  is in GHz. Measurement of the reflected wave yields a wealth of information about the density profile – simple phase-delay measurements at a variety of frequencies produce a non-perturbative measurement of the density profile, as for each input frequency the density at the cutoff layer (the location of which is derived from the phase delay) must be equal to  $n_c(f)$ .

The phase delay of the reflectometer signal is quite sensitive to density fluctuations – thus, reflectometry was identified early on as a possible means to characterize the local turbulence. To this end, an O-mode reflectometer system (described in [18, §2.2]) was implemented on C-Mod, and subsequently upgraded from the initial amplitude-modulated implementation to a fully base-band system optimized for fluctuations measurements [19]. The system is designed with a low-frequency component spanning  $50 - 110$  GHz, corresponding to a cutoff density range of  $0.31 - 1.5 \times 10^{20} \text{ m}^{-3}$ , with additional 132 and 140 GHz modules bringing the maximum observable baseline density to  $2.4 \times 10^{20} \text{ m}^{-3}$ . A 2-megasample/second digitization rate and tuned  $\sim 500$  MHz spectral width allow confident measurement of highly-localized, fairly high-frequency fluctuations in the pedestal, ideal for measurement of QCM and WCM fluctuations.

Over steady I-mode phases, the fluctuation amplitude  $\zeta(f)$ , expressing the local fluctuation intensity as a function of frequency, may be time-integrated (see fig. 2.9 for such a phase) to easily extract the frequency dependence of turbulent fluctuations tied to specific mode structures (for example, the QCM in EDA H-mode or the WCM in

**Figure A.6:** Time-integrated fluctuation intensity for a steady I-mode phase, fitted as a function of frequency to the form in eq. (A.48). The Gaussian fit to the WCM is shown in blue, with the exponentially dropoff in background fluctuations is shown in teal. The full fit is shown in red.



I-mode). I-mode fluctuation data may be fitted to the form developed in [18, §3],

$$\zeta(f) = Ae^{-f/f_1} + Be^{-f/f_2} + Ce^{-(f-f_{WCM})^2/w^2} \quad (\text{A.48})$$

in which the background fluctuations are characterized by a pair of exponentially-decaying functions, and the WCM is taken to be a Gaussian centered at  $f_{WCM}$  with width  $w$ . Such a fit is shown for an I-mode case in fig. A.6. This allows a common definition for the mode amplitude, centroid frequency, and spectral broadening  $\Delta f/f$ . However, as the reflectometer does not have a consistent amplitude calibration between shots, no absolute mode amplitude data may be obtained. Characterization of the WCM frequency and amplitude response is the subject of ongoing research. \*



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# B

## HIGH-RESOLUTION PEDESTAL DATABASE

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For the work presented in this thesis, a subset of recent I-mode experiments on Alcator C-mod was prepared with high-resolution pedestal data. These data are stored in an SQL database under the C-Mod “logbook” system. Use of an SQL table enables easy cross-platform access to pedestal data in a format ideal for data mining, and allows for easy extensibility for additional experiments. The database stores time phases in which plasma parameters (e.g., temperature, stored energy, density, heating power) are steady – usable phases last at least  $\sim 100$  ms ( $\sim 10$  TS frames), over which data is averaged (described in section 4.1). For each phase, the SQL database stores a variety of physics and engineering parameters, and scalar fitting parameters from high-resolution pedestal fits (defined using the  $mtanh$  function, eq. (4.1)). The fits are defined in normalized poloidal flux space (denoted  $\psi_n$  in the units below). The table also stores analogous data from H-modes (EDA and ELM<sub>y</sub>), as well as ELM-synchronized data from the ELM<sub>y</sub> H-mode experiments in chapter 4, for direct comparison to I-mode. A parameter list for the SQL database is shown in table B.1. Parameters are organized as follows:

### KEY PARAMETERS

The set of these keys is sufficient to uniquely identify an entry in the database.

### PHASE FLAGS

Searchable flags for the phase type, specifiers for the pedestal profile MDS tree.

### MEASURED PARAMETERS

Plasma measurements apart from the pedestal profiles.

### EFIT PARAMETERS

Calculated parameters from the EFIT reconstruction.

### HEATING POWER, STORED ENERGY, AND CONFINEMENT

Stored values for power source and sink terms, stored energy, and energy confinement (both dimensional and normalized).

### PEDESTAL PROFILES

Fitting parameters and calculated values from the high-resolution pedestal profiles in electron density, temperature, and pressure.

### WCM FLUCTUATIONS

I-mode-specific parameters storing fitted values from WCM fluctuation measurements.

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**Table B.1:** SQL database parameters, with datatype, units, and description. These parameters store data from the EFIT reconstruction and global metrics, as well as parameters for the pedestal fits.

<i>SQL database key parameters</i>			
<i>column</i>	<i>type</i>	<i>units</i>	<i>description</i>
SHOT	long		C-Mod shot number
TA	long	ms	start time of phase
TB	long	ms	end time of phase
MODE	string		type of phase in window, e.g., 'IMODE', 'ELMY', 'EDA', 'LMODE', 'ELMBIN'
<i>time window flags</i>			
ELMS	int		binary flag, = 1 for ELMs in phase
LH	int		binary flag, = 1 for LHCD in phase
WCM	int		binary flag, = 1 for WCM fluctuation in phase (I-mode only)
TREE_PATH	string		path to branch in pedestal-profile MDS tree
TREE_SHOT	long		shot number flagged in pedestal-profile MDS tree, used to differentiate sub-branches of a single shot
SEED_SPC	string		gas seeding species (Ne, N, Ar) - None for no gas seeding
<i>measured parameters</i>			
NLo4	float	$\text{m}^{-2}$	line-integrated density from TCI
NLo4_ERR	float	$\text{m}^{-2}$	error in NLo4
NEBAR	float	$\text{m}^{-3}$	line-averaged density from TCI
NEBAR_ERR	float	$\text{m}^{-3}$	error in NEBAR
ECE_To	float	eV	core electron temperature from ECE

<i>column</i>	<i>type</i>	<i>units</i>	<i>description</i>
ECE_TPED	float	eV	pedestal electron temperature from ECE (channel nearest 95% flux surface)
NEo	float	$m^{-3}$	core density from TS
NEo_ERR	float	$m^{-3}$	error in NEo
TEo	float	eV	core temperature from TS
TEo_ERR	float	eV	error in TEo
NUSTAR	float		pedestal collisionality at 95% flux surface
RHOSTAR	float		pedestal normalized gyroradius at 95% flux surface
ZEFF	float		average effective charge
ZEFF_ERR	float		error in ZEFF measurement
<i>EFIT parameters</i>			
KAPPA	float		plasma elongation $\kappa$ (see fig. 1.6)
KAPPA_ERR	float		error in KAPPA
DELTA_U	float		plasma upper triangularity (see fig. 1.6)
DELTA_U_ERR	float		error in DELTA_U
DELTA_L	float		plasma lower triangularity (see fig. 1.6)
DELTA_L_ERR	float		error in DELTA_L
IP	float	MA	plasma current
IP_ERR	float	MA	error in IP
DIDT	float	$MA \cdot s^{-1}$	change in plasma current $dI_p/dt$
DIDT_ERR	float	$MA \cdot s^{-1}$	error in DIDT
BT	float	T	axial toroidal field
BT_ERR	float	T	error in BT
BP	float	T	flux-surface averaged edge poloidal field
BP_ERR	float	T	error in BP

<i>column</i>	<i>type</i>	<i>units</i>	<i>description</i>
Qo	float		axial safety factor $q_0$
Qo_ERR	float		error in Qo
Q95	float		edge safety factor $q_{95}$
Q95_ERR	float		error in Q95
R	float	cm	major radius
A	float	cm	outboard-midplane minor radius
SSEP	float	cm	X-point position: $\sim 1$ is USN, $\sim -1$ is LSN, 40 is limited
BETAT	float		global toroidal beta, $\langle \beta_t \rangle$
BETAP	float		global poloidal beta, $\langle \beta_p \rangle$
BETAN	float	$m \cdot T \cdot MA^{-1}$	global normalized beta, $\beta_N = \langle \beta \rangle / (I_p/aB_t)$
TAU_MHD	float	s	MHD energy confinement time, $\tau_E$
TAU_MHD_ERR	float	s	error in TAU_MHD
<i>heating power, stored energy, &amp; confinement</i>			
PLASMA_W	float	J	plasma stored energy
PLASMA_W_ERR	float	J	error in PLASMA_W
DWDT	float	MW	change in stored energy, $dW_{plasma}/dt$
DWDT_ERR	float	MW	error in DWDT
P_ICRF	float	MW	absorbed ICRF heating power
P_ICRF_ERR	float	MW	error in P_ICRF
P_OHM	float	MW	Ohmic heating power
P_OHM_ERR	float	MW	error in P_OHM
P_LH	float	MW	absorbed lower-hybrid heating power
P_LH_ERR	float	MW	error in P_LH
P_RAD	float	MW	radiated power from bolometry
P_RAD_ERR	float	MW	error in P_RAD
P_SOL	float	MW	net power through SOL, eq. (1.29)
P_SOL_ERR	float	MW	error in P_SOL

<i>column</i>	<i>type</i>	<i>units</i>	<i>description</i>
P_THRES	float	MW	H-mode threshold power, eq. (2.7)
P_THRES_ERR	float	MW	error in P_THRES
H	float		ITER98y2 H-mode confinement scaling, $H_{98} = \tau_E / \tau_{98y2}$
H_ERR	float		error in H
H89	float		ITER89 L-mode confinement scaling, $H_{89} = \tau_E / \tau_{89}$
H89_ERR	float		error in H89
<i>parameters for high-resolution pedestal profiles</i>			
NEPED_H	float	$m^{-3}$	density pedestal height
NEPED_H_ERR	float	$m^{-3}$	error in NEPED_H
NEPED_B	float	$m^{-3}$	density pedestal baseline
NEPED_B_ERR	float	$m^{-3}$	error in NEPED_B
NEPED_D	float	$\psi_n$	density pedestal half-width
NEPED_D_ERR	float	$\psi_n$	error in NEPED_D
NEPED_Ro	float	$\psi_n$	density pedestal midpoint
NEPED_Ro_ERR	float	$\psi_n$	error in NEPED_Ro
NEPED_ALPHA	float		density pedestal inboard-slope parameter
NEPED_ALPHA_ERR	float		error in NEPED_ALPHA
NEPED_HEIGHT	float	$m^{-3}$	density at NEPED_Ro - NEPED_D
NEPED_GRAD	float	$m^{-3} \cdot \psi_n^{-1}$	peak density pedestal gradient (pedestal midpoint)
NEPED_GRAD_ERR	float	$m^{-3} \cdot \psi_n^{-1}$	error in NEPED_GRAD
NEPED_LGRAD	float	$\psi_n$	peak density pedestal gradient scale length
NEPED_LGRAD_ERR	float	$\psi_n$	error in NEPED_LGRAD
NEPED_95	float	$m^{-3}$	density at 95% flux surface
NEPED_95_ERR	float	$m^{-3}$	error in NEPED_95
TEPED_H	float	eV	temperature pedestal height

<i>column</i>	<i>type</i>	<i>units</i>	<i>description</i>
TEPED_H_ERR	float	eV	error in TEPED_H
TEPED_B	float	eV	temperature pedestal baseline
TEPED_B_ERR	float	eV	error in TEPED_B
TEPED_D	float	$\psi_n$	temperature pedestal half-width
TEPED_D_ERR	float	$\psi_n$	error in TEPED_D
TEPED_Ro	float	$\psi_n$	temperature pedestal midpoint
TEPED_Ro_ERR	float	$\psi_n$	error in TEPED_Ro
TEPED_ALPHA	float		temperature pedestal inboard-slope parameter
TEPED_ALPHA_ERR	float		error in TEPED_ALPHA
TEPED_HEIGHT	float	eV	temperature at TEPED_Ro - TEPED_D
TEPED_GRAD	float	$eV \cdot \psi_n^{-1}$	peak temperature pedestal gradient (pedestal midpoint)
TEPED_GRAD_ERR	float	$eV \cdot \psi_n^{-1}$	error in TEPED_GRAD
TEPED_LGRAD	float	$\psi_n$	peak temperature pedestal gradient scale length
TEPED_LGRAD_ERR	float	$\psi_n$	error in TEPED_LGRAD
TEPED_95	float	eV	temperature at 95% flux surface
TEPED_95_ERR	float	eV	error in TEPED_95
PEPED_H	float	$m^{-3} \cdot eV$	pressure pedestal height
PEPED_H_ERR	float	$m^{-3} \cdot eV$	error in PEPED_H
PEPED_B	float	$m^{-3} \cdot eV$	pressure pedestal baseline
PEPED_B_ERR	float	$m^{-3} \cdot eV$	error in PEPED_B
PEPED_D	float	$\psi_n$	pressure pedestal half-width
PEPED_D_ERR	float	$\psi_n$	error in PEPED_D
PEPED_Ro	float	$\psi_n$	pressure pedestal midpoint
PEPED_Ro_ERR	float	$\psi_n$	error in PEPED_Ro
PEPED_ALPHA	float		pressure pedestal inboard-slope parameter
PEPED_ALPHA_ERR	float		error in PEPED_ALPHA
PEPED_HEIGHT	float	$m^{-3} \cdot eV$	pressure at PEPED_Ro - PEPED_D

<i>column</i>	<i>type</i>	<i>units</i>	<i>description</i>
PEPED_GRAD	float	$m^{-3} \cdot eV \cdot \psi_n^{-1}$	peak pressure pedestal gradient (pedestal midpoint)
PEPED_GRAD_ERR	float	$m^{-3} \cdot eV \cdot \psi_n^{-1}$	error in PEPED_GRAD
PEPED_LGRAD	float	$\psi_n$	peak pressure pedestal gradient scale length
PEPED_LGRAD_ERR	float	$\psi_n$	error in PEPED_LGRAD
PEPED_95	float	$m^{-3} \cdot eV$	pressure at 95% flux surface
PEPED_95_ERR	float	$m^{-3} \cdot eV$	error in PEPED_95
ALPHA	float		peak normalized pressure gradient $\alpha_{MHD}$
ALPHA_ERR	float		error in ALPHA
PROF_SHIFT	float	$\psi_n$	radial shift (in norm. poloidal flux) in TS profiles to satisfy power balance through SOL
EPED_WID	float	$\psi_n$	EPED-predicted pedestal width in normalized poloidal flux
EPED_P	float	kPa	EPED-predicted pressure pedestal height

*WCM fluctuation measurements*

WCM_AMP	float		normalized peak amplitude of WCM from reflectometry
WCM_FREQ	float	kHz	centroid frequency of WCM from reflectometry
WCM_WID	float	kHz	spectral width of WCM determined by $\pm\sigma$ of Gaussian fit on reflectometry
WCM_AMP_PCI	float		normalized peak amplitude of WCM from PCI
WCM_FREQ_PCI	float	kHz	centroid frequency of WCM from PCI
WCM_WID_PCI	float	kHz	spectral width of WCM determined by $\pm\sigma$ of Gaussian fit on PCI



## COLOPHON

This document was typeset using `classicthesis` developed by André Miede (although aspects were changed to comply with the MIT thesis standards and the author's personal preferences). The style was inspired by Robert Bringhurst's seminal book on typography "*The Elements of Typographic Style*". `classicthesis` is available for both L<sup>A</sup>T<sub>E</sub>X and LyX:

<http://code.google.com/p/classicthesis/>

*Final Version* as of August 18, 2014 (`classicthesis` version 4.1).

Hermann Zapf's *Palatino* and *Euler* type faces (Type 1 PostScript fonts *URW Palladio L* and *FPL*) are used. The "typewriter" text is typeset in *FPL*, originally developed by Bitstream, Inc. as "Bitstream Vera". (Type 1 PostScript fonts were made available by Malte Rosenau and Ulrich Dirr.)