

# Pedestal Structure and Stability in High-Performance Plasmas on Alcator C-Mod

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# Thank you to...

- The thesis committee: JW Hughes, DG Whyte, AE White, JP Freidberg
- The I-mode crew: AE Hubbard, JL Terry, I Cziegler, A Dominguez, SG Baek, C Theiler, RM Churchill, ML Reinke, JE Rice...
- Physops: R Granetz, S Shiraiwa, S Wolfe, S Wukitch...
- C-Mod operations, engineering, researchers and techs
- PSFC grad students, past and present
- Family and friends
- the audience!

# Outline

## ■ Context & Motivation

- ▶ High-performance regimes
- ▶ Pedestal physics
- ▶ Introduction to I-mode

## ■ Pedestal Modeling & Theory:

- ▶ Peeling-balloonning MHD stability
- ▶ Kinetic-balloonning mode turbulence

## ■ ELMy H-Mode Physics<sup>1</sup>

- ▶ EPED Modeling on C-Mod

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<sup>1</sup>JR Walk *et al.*, Nuclear Fusion 52 (2012)

# Outline

## ■ I-Mode Pedestals & Global Performance<sup>2,3</sup>

- ▶ Pedestal response to fueling, heating power
- ▶ Pedestal widths and gradients
- ▶ Global performance and confinement scalings

## ■ I-Mode Pedestal Stability

- ▶ P-B MHD, KBM modeling
- ▶ ELM characterization

## ■ Summary, Future Work, & Questions

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<sup>2</sup>JR Walk *et al.*, *Physics of Plasmas* **21** (2014)

<sup>3</sup>Invited talk, APS-DPP Nov. 2013

## The problem...

By default (“L-mode”), rapid transport of energy and particles from plasma driven by turbulence

- and energy transport gets *worse* with more heating power!
- need very strong magnetic field and/or large machine size to overcome poor plasma performance

L-mode likely not suitable for (economical) power plant development.

## The solution?

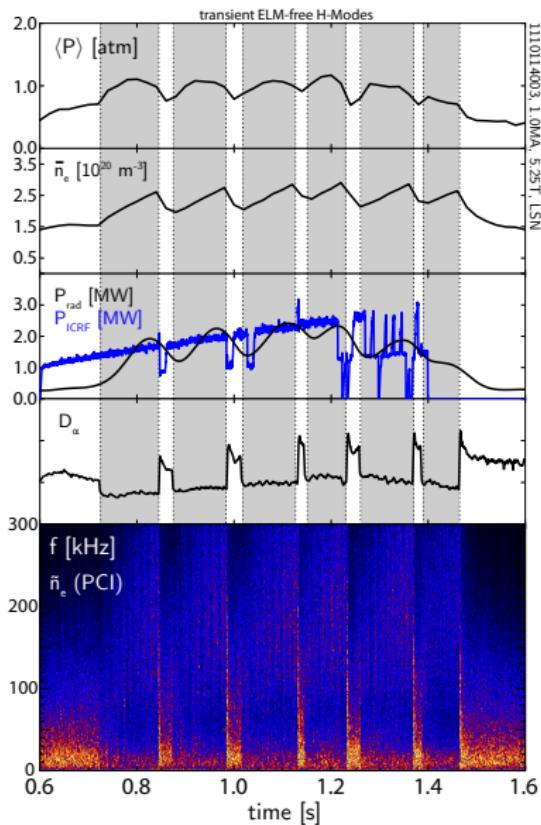
Under right conditions, plasma forms “transport barrier” in edge, with steep gradients in density and temperature – the *pedestal*  
→ plasma transitions to “high-confinement” or H-mode

- immediate factor of  $\sim 2$  increase in energy confinement
- pedestal supports higher core pressures = fusion power density

pedestal height sets strong constraint on global performance

## ...But this has problems of its own

- increased particle confinement  
= plasma retains impurities as well as fuel ions
- radiated power ( $\sim Z^2$  for a given impurity species) increases, overcomes heating power  $\rightarrow$  plasma drops back into L-mode
- inherently transient state

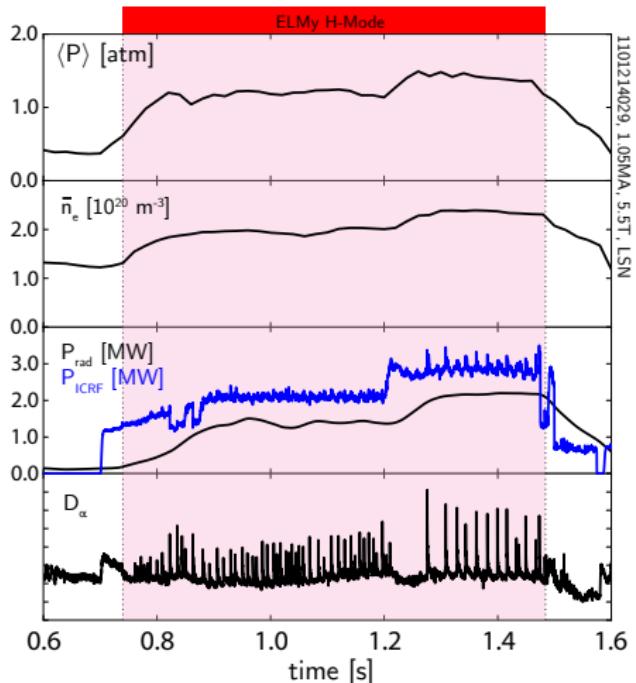


so, we need:

- high energy confinement
- low particle confinement (low enough, at least)
- ... and that's it, right?

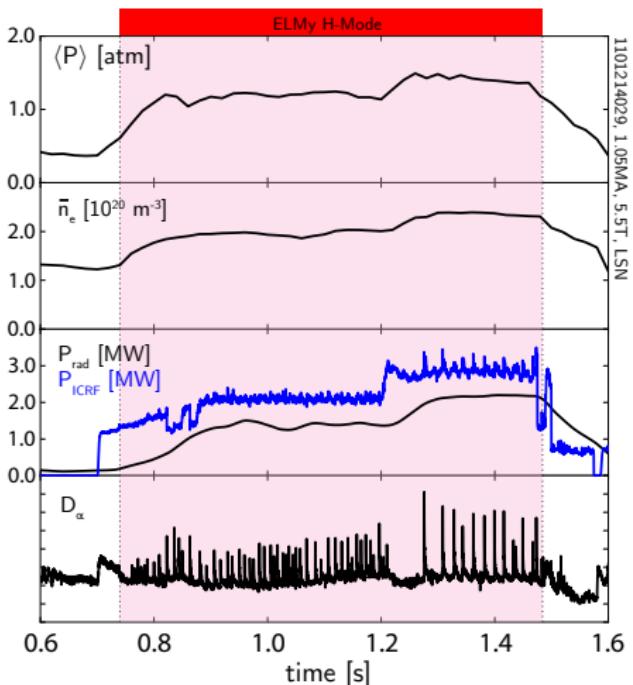
# The solution? (part II)

- Edge-Localized Modes (ELMs)
  - instabilities that relax the pedestal, drive bursts of energy, particle transport, enough to prevent impurity accumulation



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- Edge-Localized Modes (ELMs)
  - instabilities that relax the pedestal, drive bursts of energy, particle transport, enough to prevent impurity accumulation
- large ELMs drive pulsed heat loads in excess of plasma-facing material tolerances



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- avoid, mitigate, or suppress large ELMs



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  - ▶ engineering solutions:  
pellet pacing, resonant magnetic perturbations

so, we need:

- high energy confinement
- low particle confinement (low enough, at least)
- avoid, mitigate, or suppress large ELMs
  - ▶ engineering solutions:  
pellet pacing, resonant magnetic perturbations
  - ▶ physics solutions:  
pedestal regulation by fluctuations below ELM limit

## The solution? (part III)

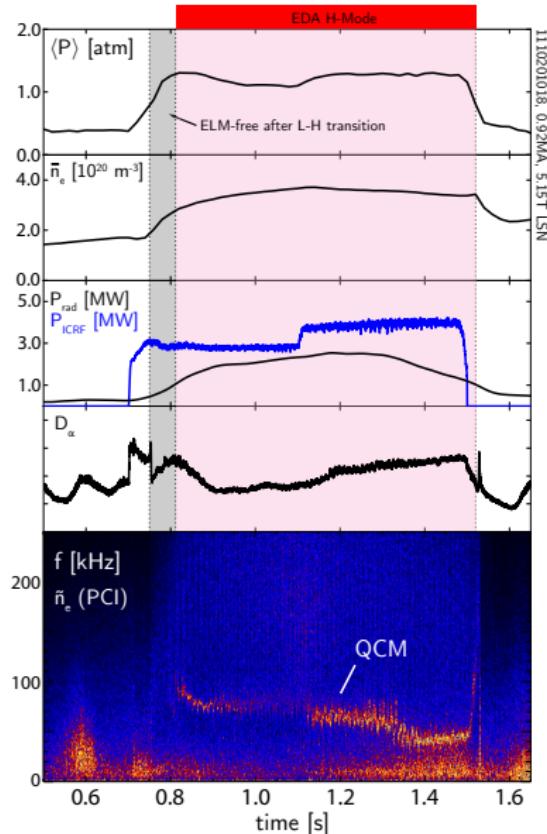
A number of fluctuation-regulated regimes have been observed:

- EDA H-mode  
Quasi-Coherent Mode (QCM) – C-Mod, AUG(?)
- Quiescent H-mode  
Edge Harmonic Oscillator (EHO) – DIII-D, JET, AUG
- High-Recycling Steady H-mode  
edge MHD fluctuations – JFT-2M
- type-II, -III ELMy H-modes  
small, rapid ELMs – various devices

generally capable of stationary high performance without large ELMs

# EDA H-mode (on C-Mod and elsewhere)

- pedestal regulated by continuous edge fluctuation (QCM), rather than bursts of ELM transport
- steady density,  $P_{rad} \rightarrow$  stationary operation possible with good performance

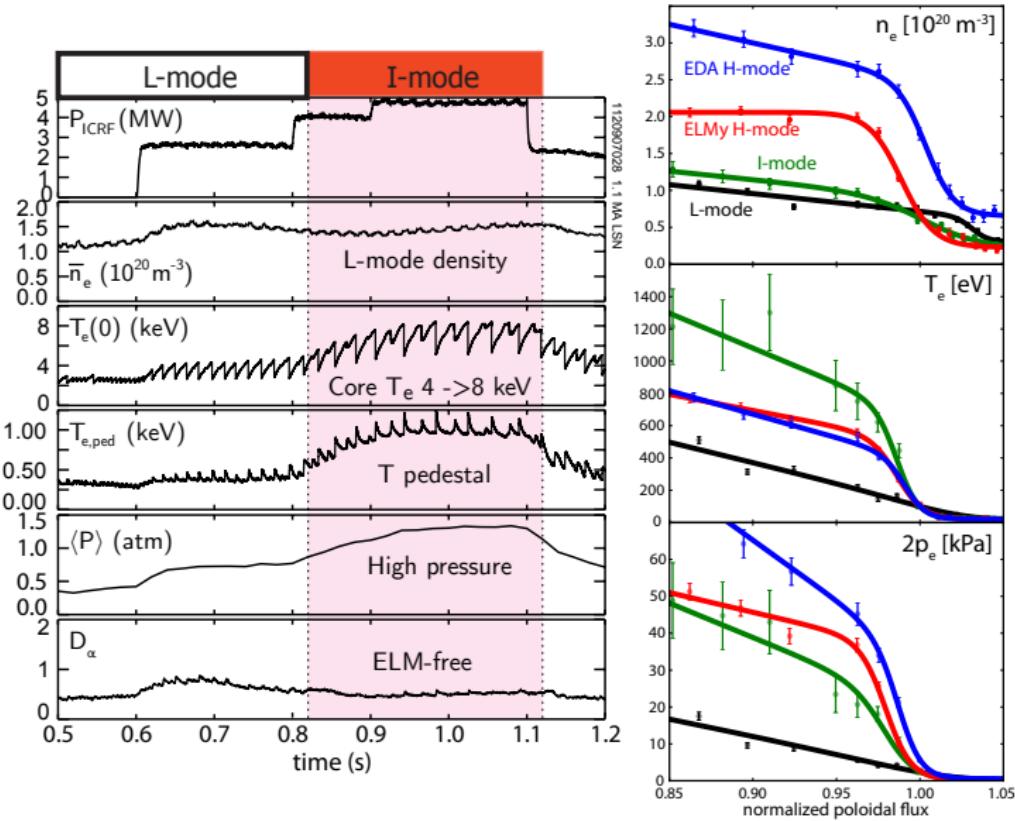


## But each of these has drawbacks

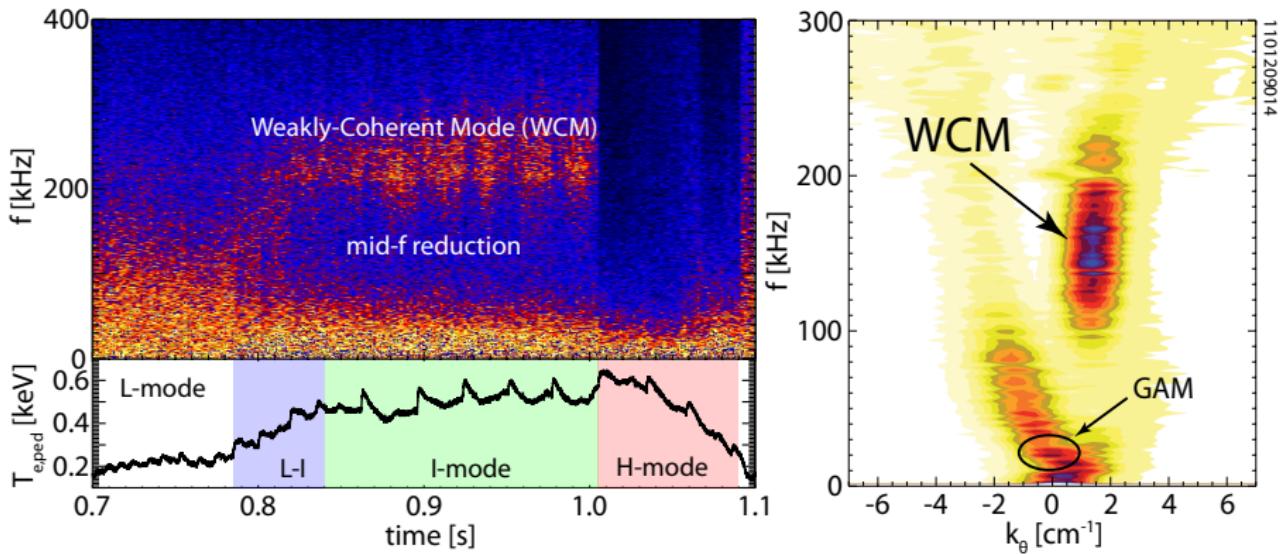
- engineering requirements, e.g. high beam torque for QH-mode
- access limits: high collisionality for EDA, shaping for type-II ELMs

Can we do better?

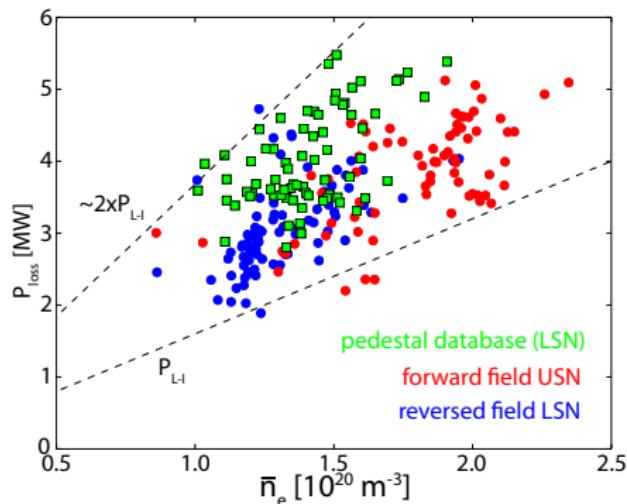
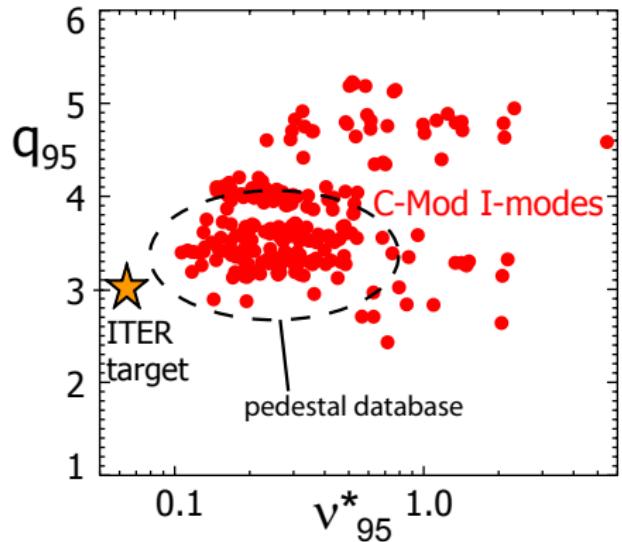
# A challenger appears: the I-mode



# I-mode pedestal regulated by Weakly-Coherent Mode (WCM)



# Robust I-mode access on C-Mod



- I-mode accessed over range of edge current profiles, low-mid collisionalities
- “Unfavorable”  $\nabla B$  orientation (ion  $\nabla B$  drift away from primary X-point) – forward-field upper-null or reversed-field lower-null operation
- Sustain mode with heating power up to  $\sim 2\times$  above L-I threshold

last intro slide here

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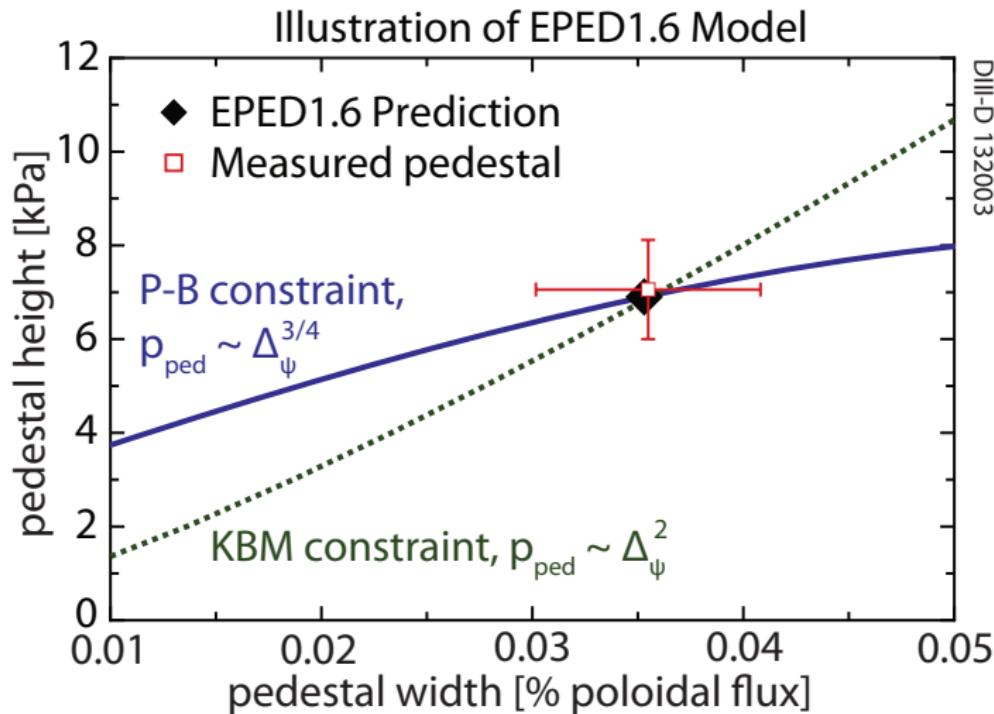
- ▶ EPED Modeling on C-Mod

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<sup>1</sup>JR Walk *et al.*, *Nuclear Fusion* 52 (2012)

how much detail here for modeling, vs in extra slides?

# Predictive Model for ELM My H-modes – EPED<sup>4</sup>



<sup>4</sup>PB Snyder *et al.*, Nuclear Fusion **51** (2011)

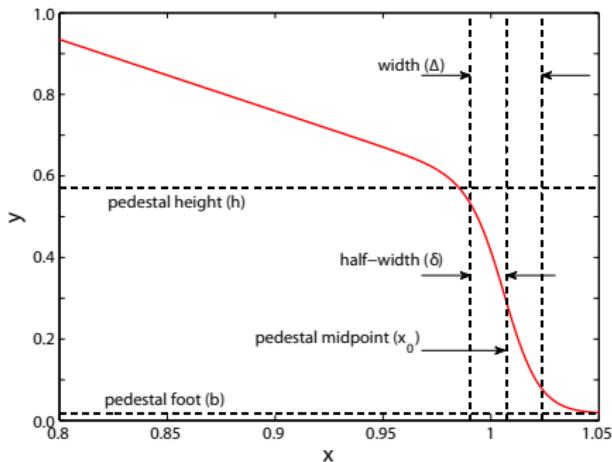
# Pedestal Structure Definitions

pedestals fitted by

$$z = \frac{x_0 - x}{\delta}$$

$$mtanh(\alpha, z) = \frac{(1 + \alpha z)e^z - e^{-z}}{e^z + e^{-z}}$$

$$y = \frac{h + b}{2} + \frac{h - b}{2} mtanh(\alpha, z)$$



rigorous definition for pedestal width  $\Delta = 2\delta$ , continuous and differentiable throughout pedestal profile

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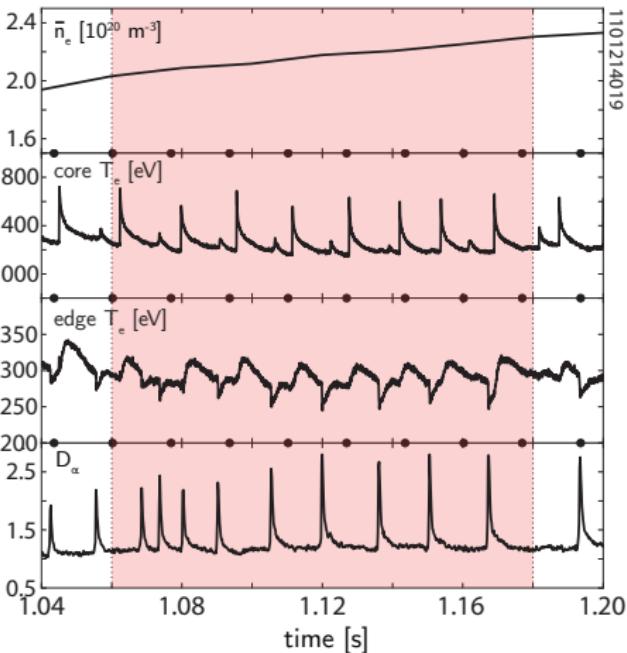
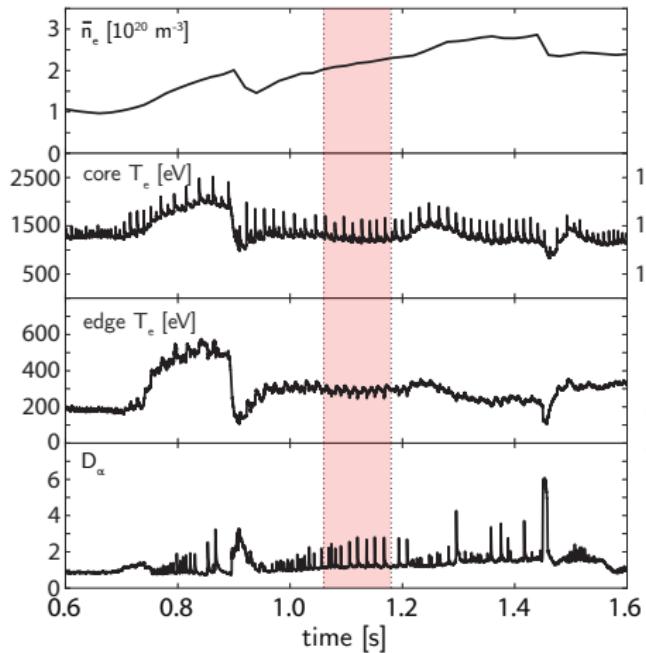
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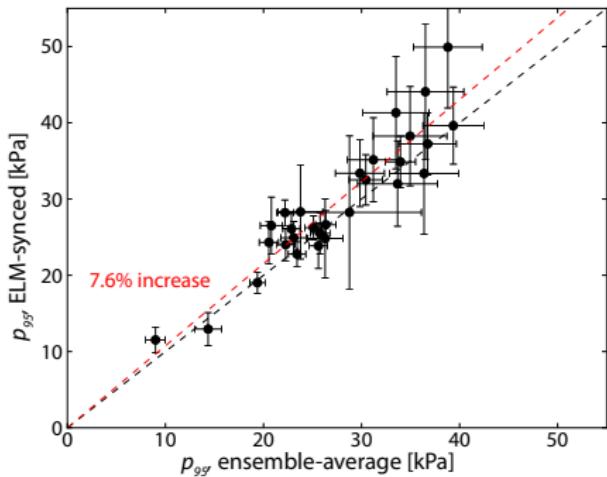
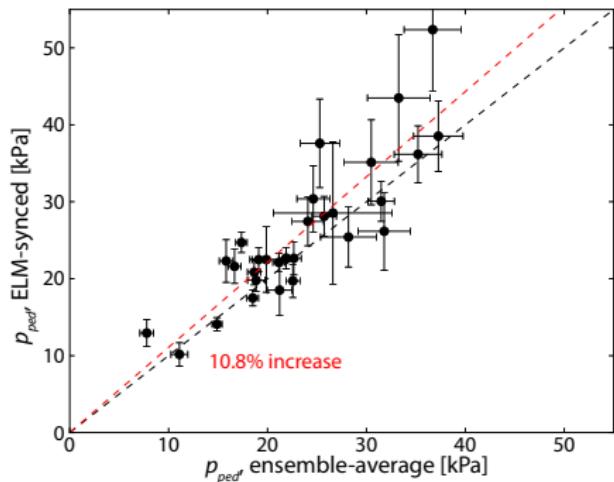
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# Target steady ELMy phases for study

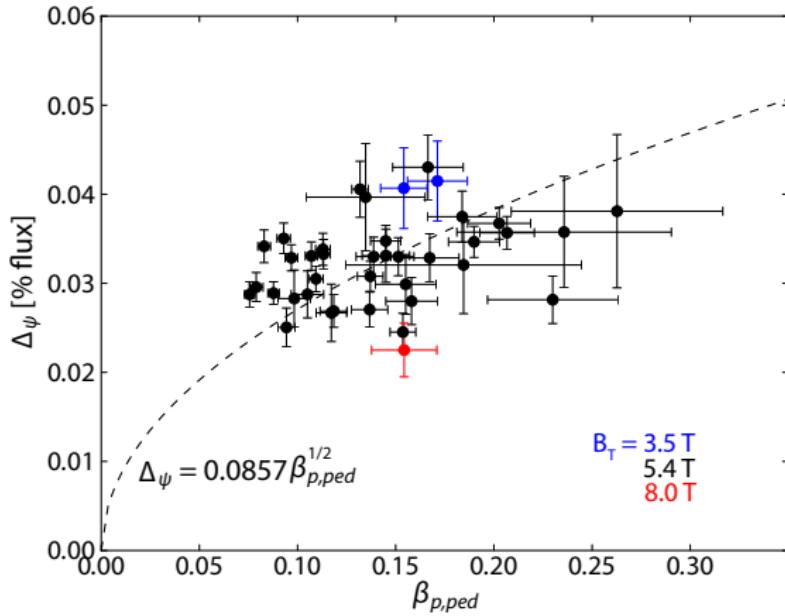


# ELM cycle binning necessary to capture pedestal limit



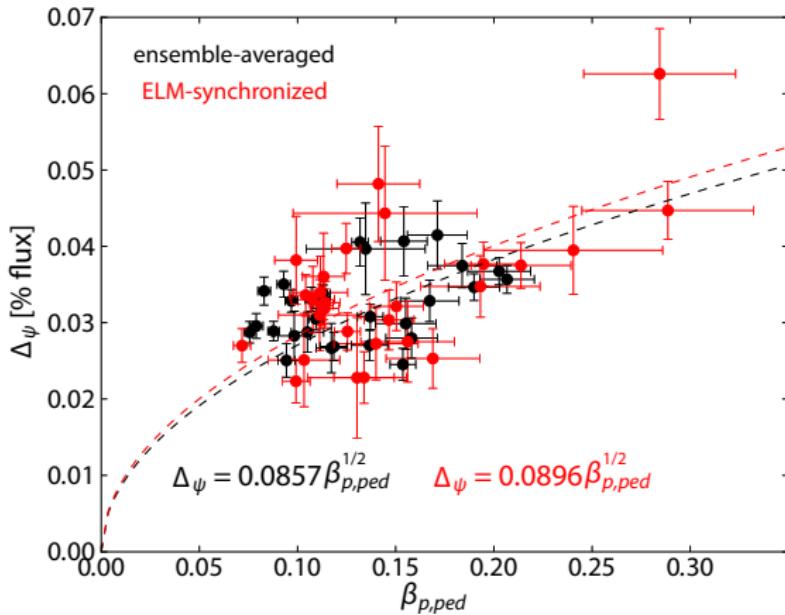
Take profile data immediately preceding ELM crash (typically last 20% of ELM cycle) for pedestal structure at point of instability – necessary, but difficult given ELM frequency on C-Mod (subset of data prepared thus).

# Pedestal width described well by KBM limit



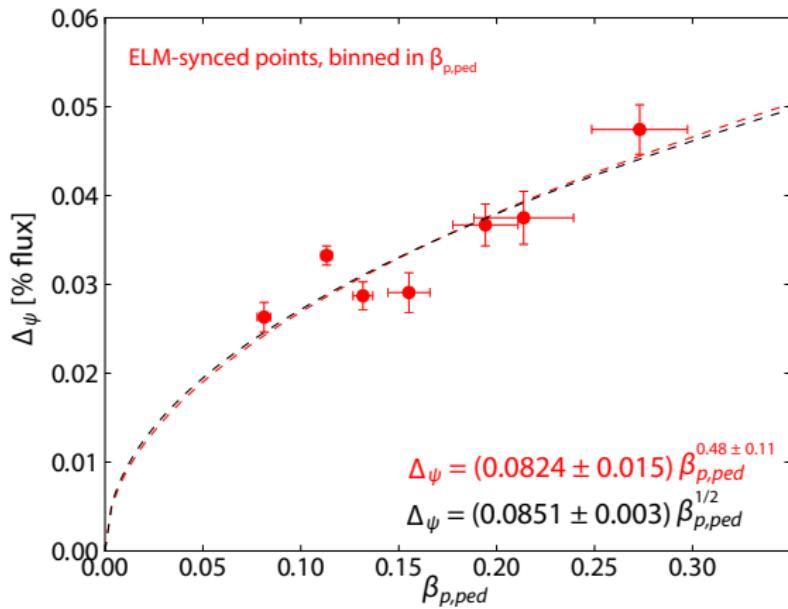
KBM limit predicts width  $\Delta_\psi = G(\nu^*, \varepsilon, \dots) \beta_{p,ped}^{1/2}$

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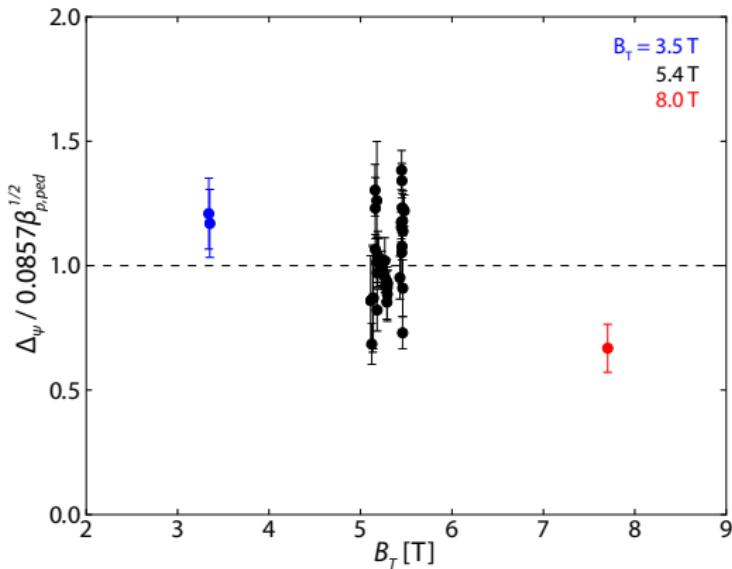
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## Minimal dependence of width on other parameters

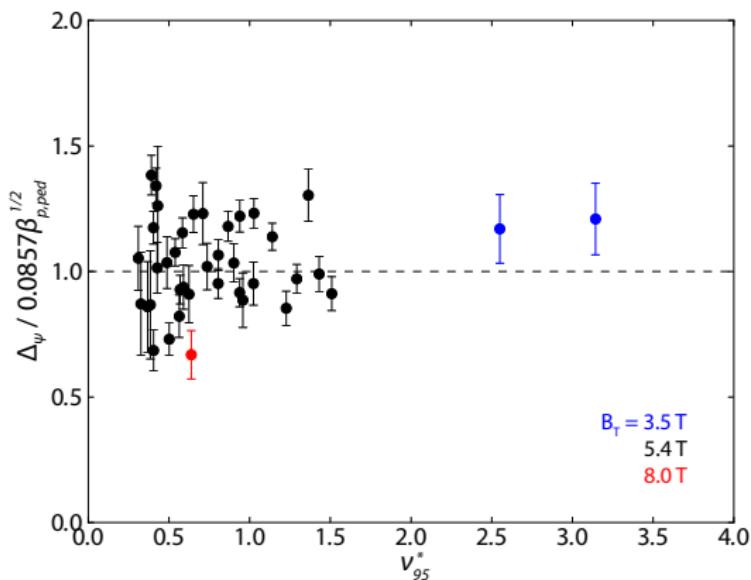
Secondary dependences via pedestal width normalized to  $\beta_{p,ped}^{1/2}$  scaling



- broader pedestal at low field qualitatively  $\sim$  some modeling efforts, but within spread at standard field, strong covariance with current
- no variation with collisionality, despite effects on edge current  $\rightarrow$  magnetic shear
- no variation with gyroradius (expected as dependence in  $G$ )

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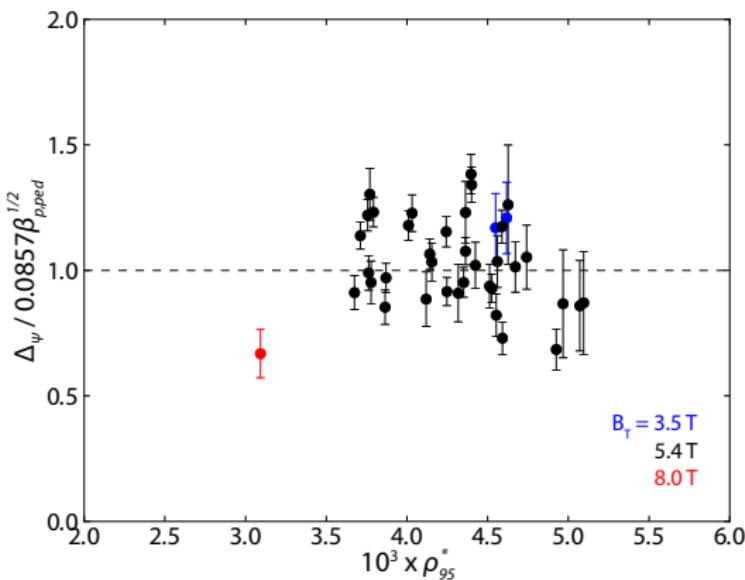
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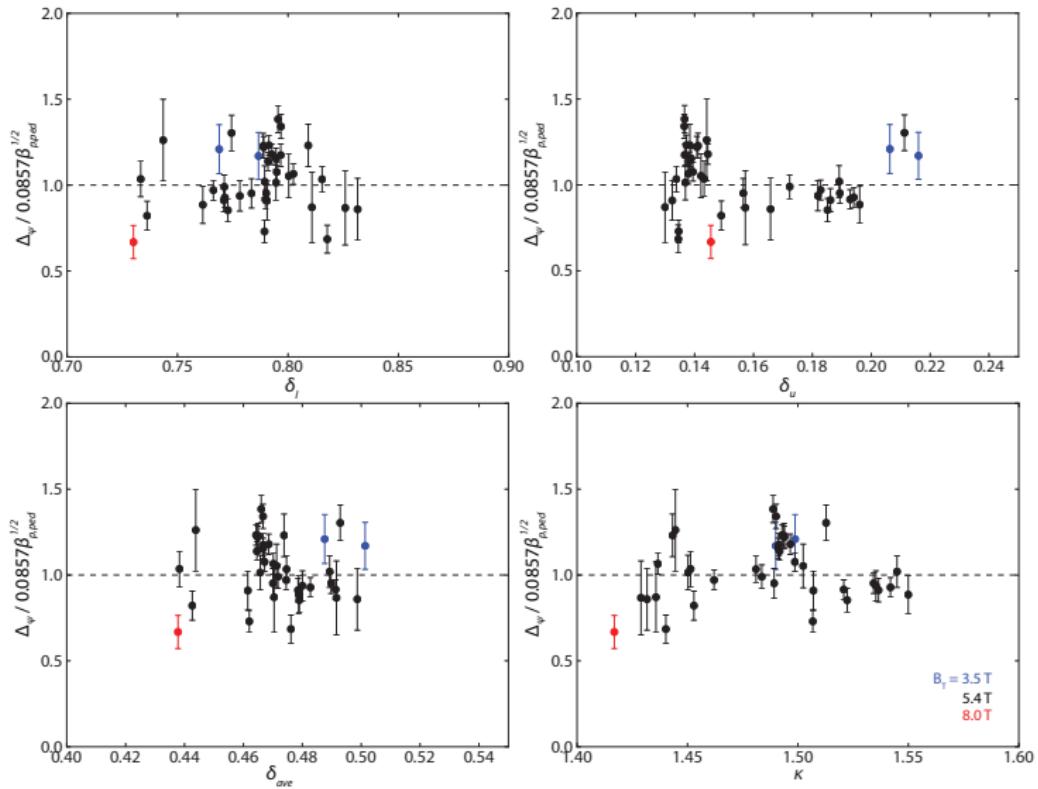
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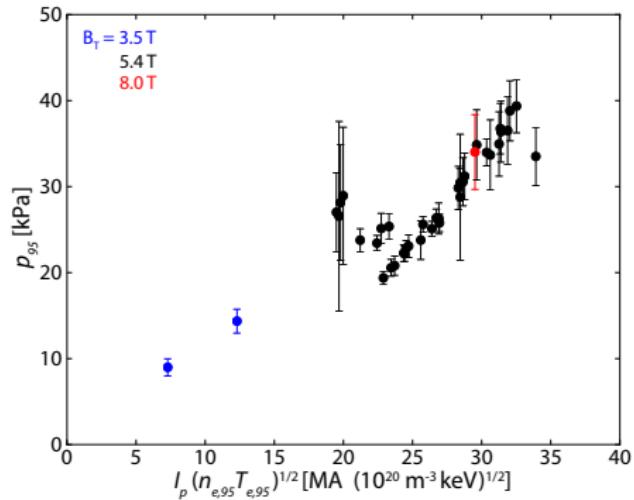
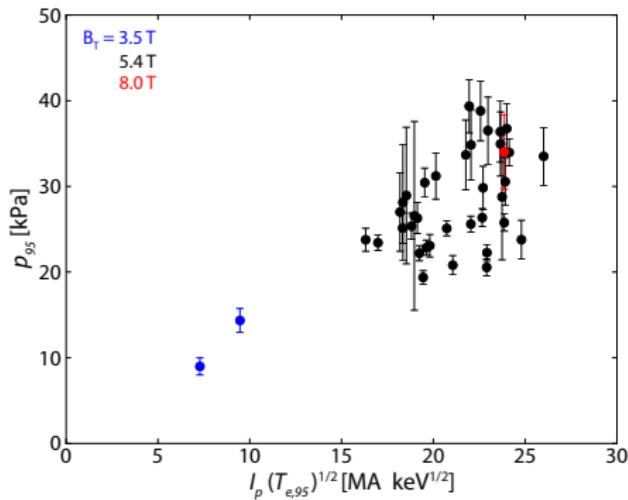


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# Minimal dependence of normalized width on shaping

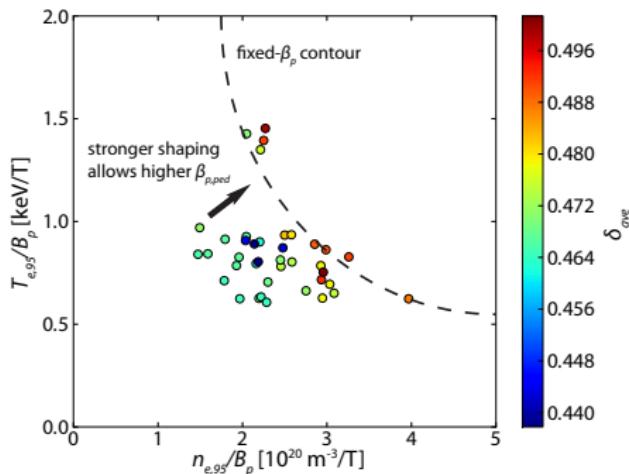
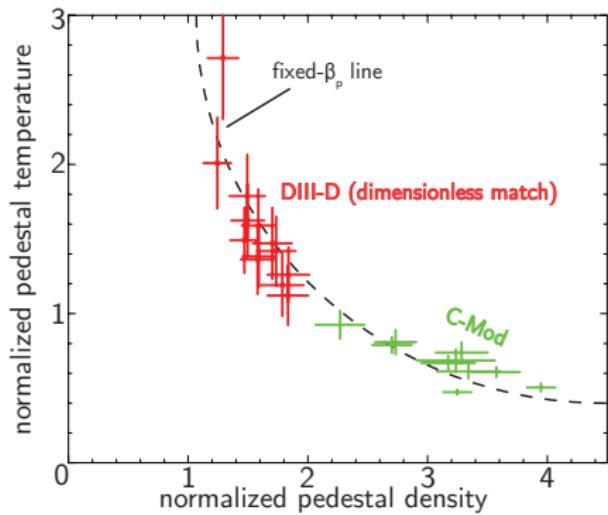


# Pedestal height predicted by ballooning $\nabla p$ limit

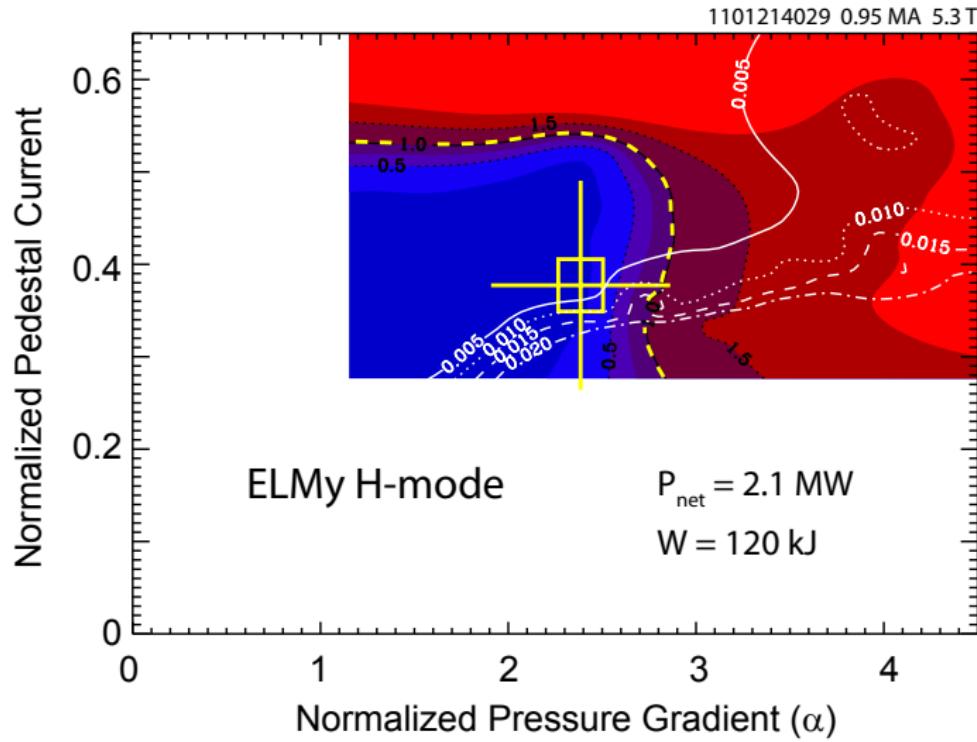


Pedestal height  $p_{ped} \sim \nabla p \times \Delta_p \rightarrow \sim I_p^2 \Delta_p$  from ballooning MHD  
predicted well by  $\Delta_p \sim \sqrt{\beta_{p,ped}}$ , less so by  $\Delta_p \sim \rho_{i,pol}$

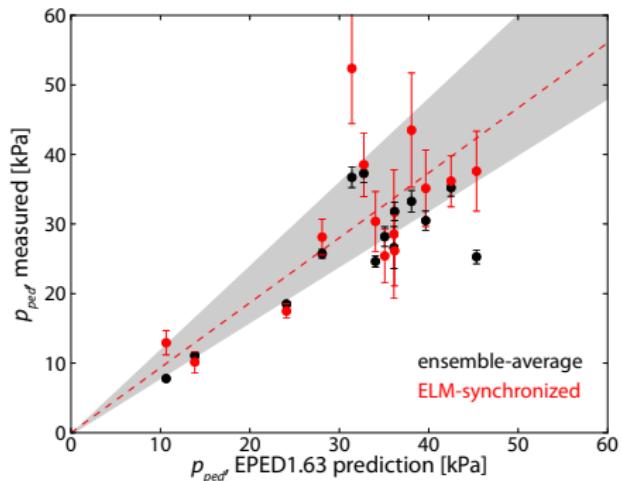
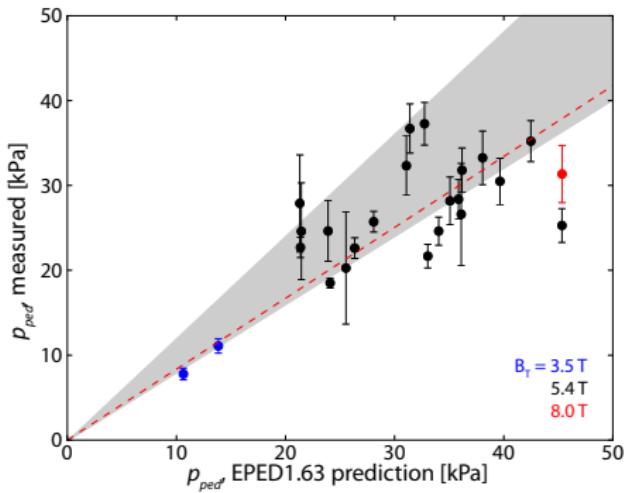
# Robust width, gradient limit = attainable $\beta_{p,ped}$ limited in ELM My H-mode



# Computational modeling of P-B MHD, KBM captures ELMy pedestal

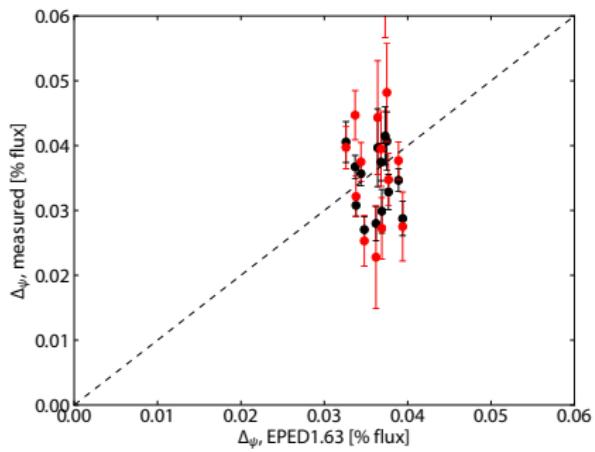
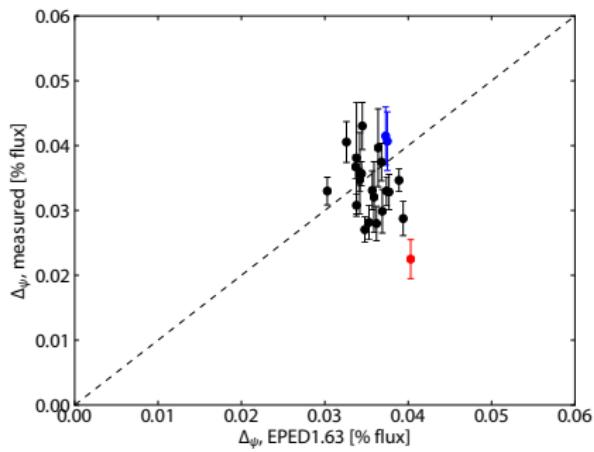


# EPED predicts pedestal height for ELM-binned pedestals



measured to predicted ratio of  $0.835 \pm 0.036$  for ensemble-averaged data,  $0.934 \pm 0.066$  for ELM-synced pedestals, well within expected  $\pm 20\%$  accuracy for EPED predictions

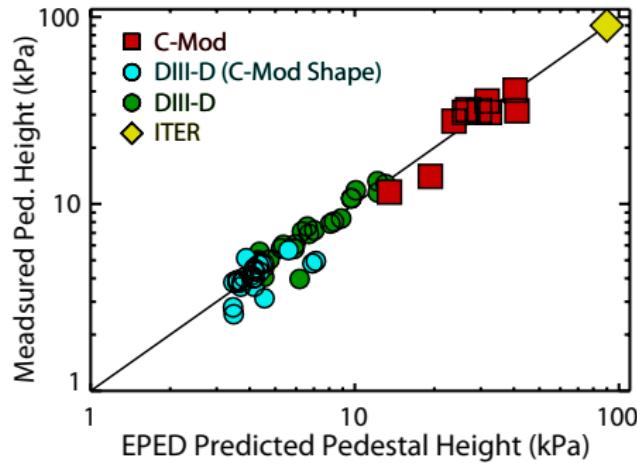
# Width varies over narrow range, hard to predict



Pedestal width varies little over range of 3 – 5% of poloidal flux, difficult to extract trend – EPED reproduces robust width to within  $\pm 20\%$  uncertainty

# Experiments expand parameter space tested in EPED<sup>5</sup>

- reach highest field (8 T), highest thermal pressure, within factor of  $\sim 2$  of ITER pedestal target
- C-Mod contribution to multi-machine Joint Research Target, motivates development of EPED to higher collisionality, density
- reliable physics-based understanding of H-mode pedestal limits



<sup>5</sup>RJ Groebner et al., Nuclear Fusion 53 (2013)

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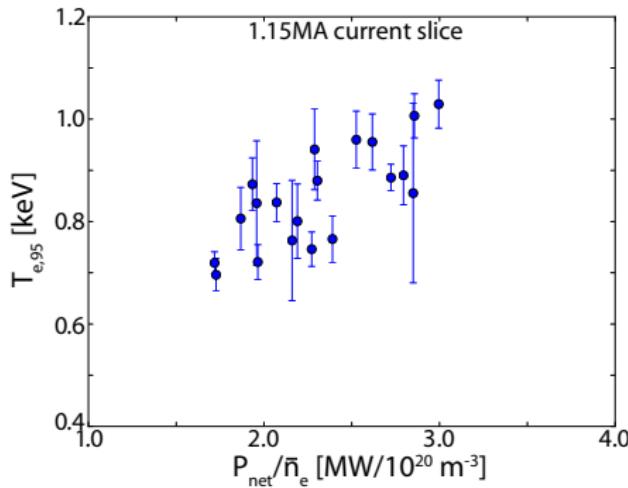
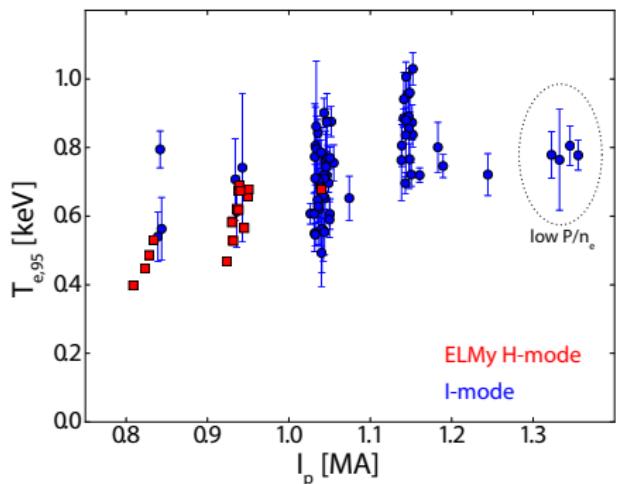
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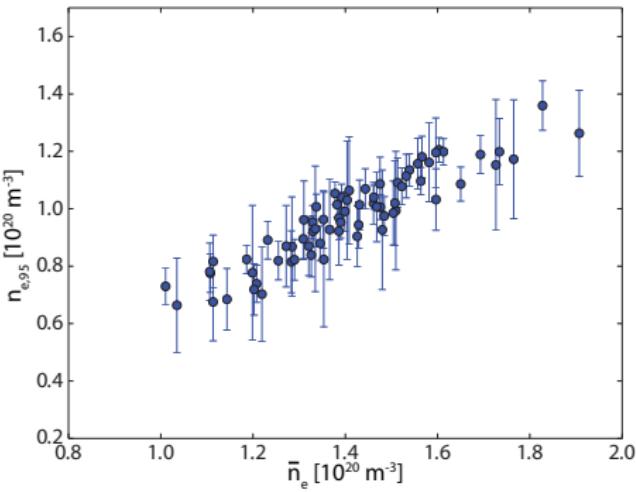
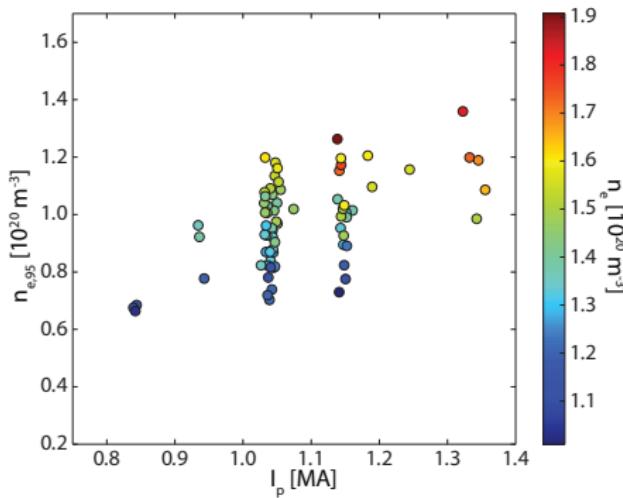
motivate I-mode discussion here

# Temperature pedestal H-mode-like, set by plasma current, heating power



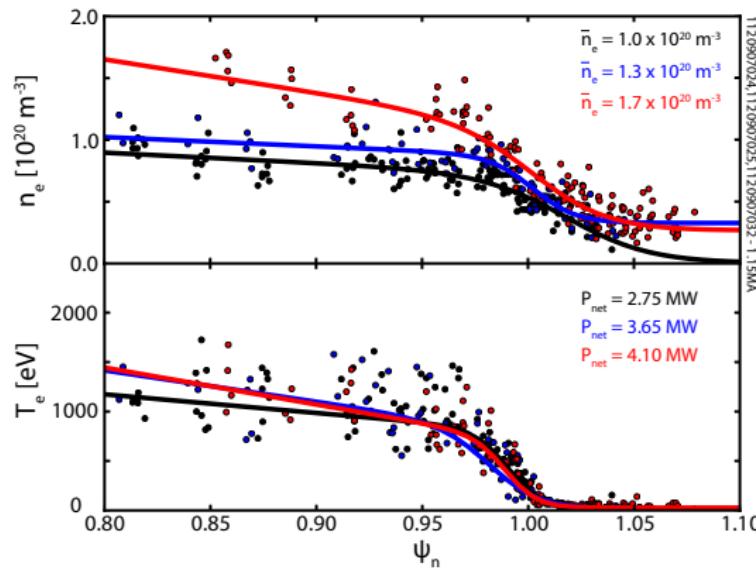
- pedestal  $T_e$  shows positive trending  $T_e \sim I_p$ , spread at given current due to heating power
- input power strongly affects pedestal temperature as with EDA H-mode – more properly, **power per particle sets pedestal temperature** at fixed current

In contrast, density set by operator fueling,  
with L-mode-like profile



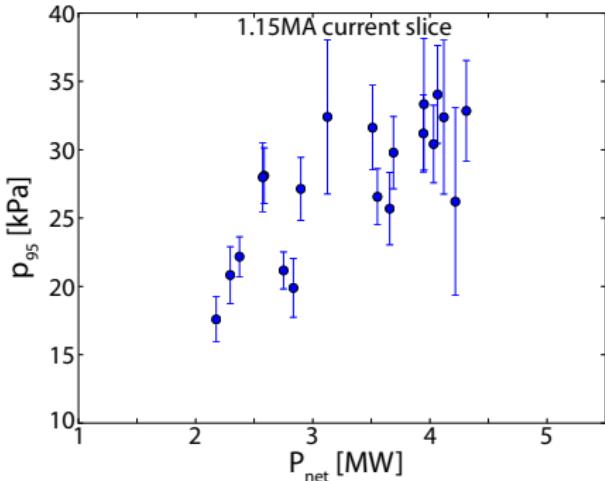
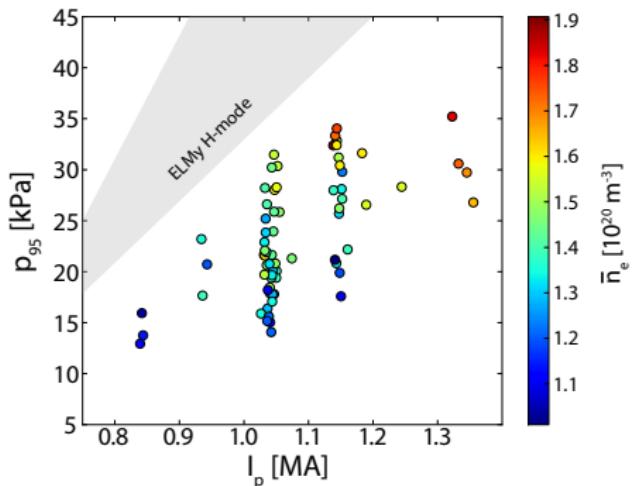
Plasma current a poor predictor of pedestal density, in contrast to  
transport-limited EDA H-modes – easy density control

# Pedestal density separately controlled from temperature, independent of MHD limits



- with sufficient power to maintain  $P_{\text{net}}/\bar{n}_e$ , temperature pedestal matched across range of fueling
- Contrasts to MHD-limited pedestals (fixed  $\beta_{p,ped} \rightarrow$  limit on  $n_e T_e$ ) – path to strongly increase pedestal beta

# I-mode pedestal pressure scales with current, heating power, fueling, competitive to H-mode



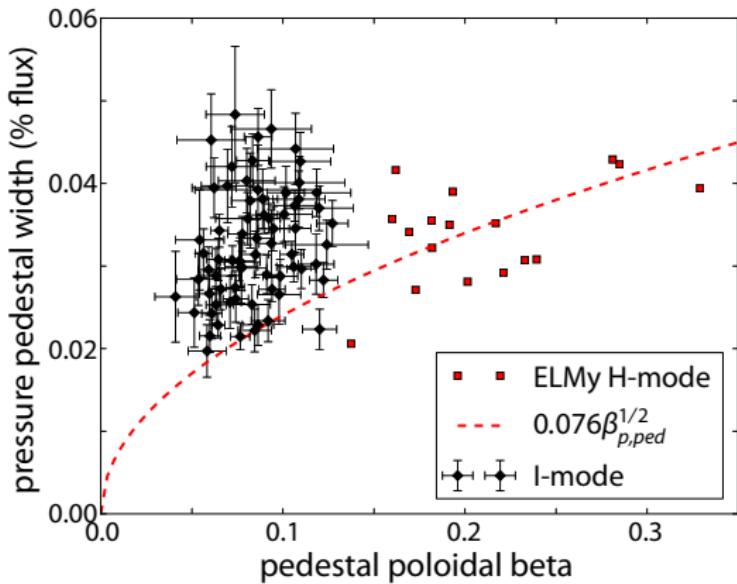
- Pedestal pressure increases at least as  $p_{ped} \sim I_p$ , due to increased  $T_e \sim I_p$  and more fueling (fixed  $f_{Gr}$ ) at higher current
- Pedestal pressure at fixed current  $\sim P_{net}$  (consistent with  $T_e \sim P/n_e$ ), corresponds to favorable scaling of energy confinement with heating power
- Fueling (with sufficient power to maintain temperature pedestal) strongly increases pedestal pressure

# What does this get us?

## Pedestal widths & gradients

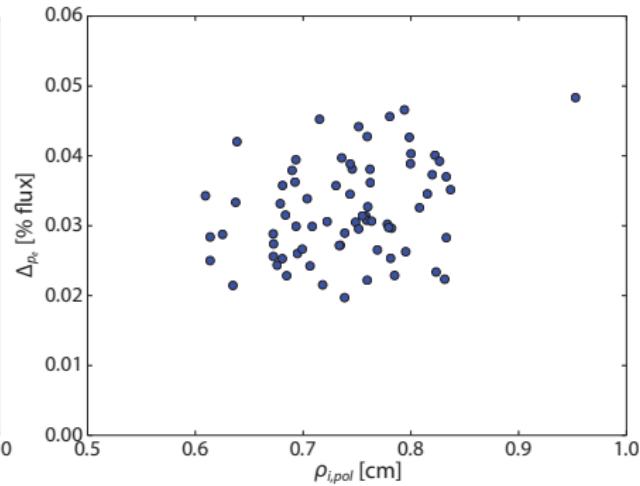
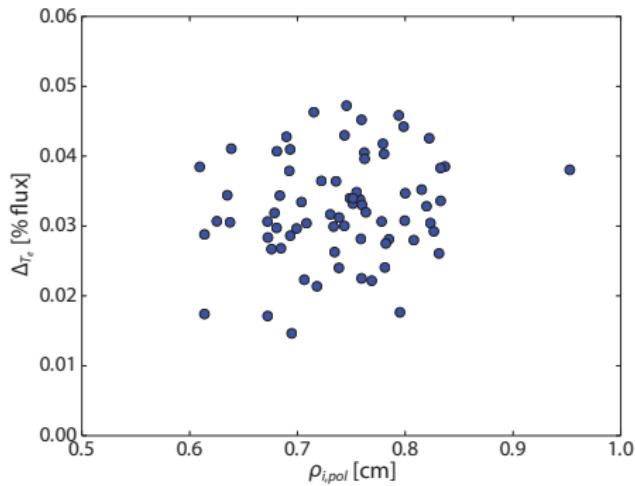
- pedestal structure typically constrained by gradient limits → need to understand pedestal width to predict height, performance
- small spatial scales → accurate measurement historically difficult

# Pedestal width uncorrelated with $\beta_{p,ped}$ , contrary to KBM limit



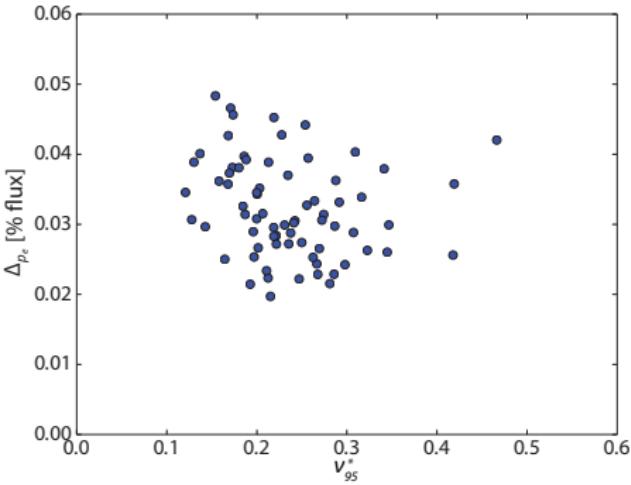
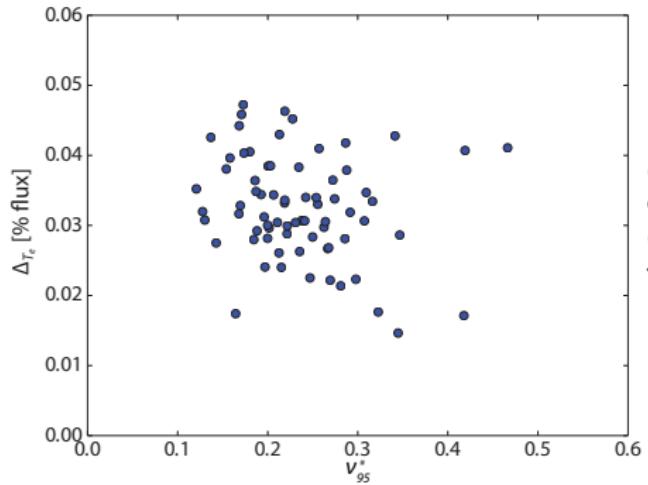
- I-mode pedestal width shows no trend with  $\beta_{p,ped}$ , consistently broader than predicted by EPED1-like KBM limit  $\Delta_\psi = 0.076\beta_{p,ped}^{1/2}$
- intuitively, pedestal  $\nabla p$  insufficient to drive ballooning-like instabilities

# I-mode temperature, pressure pedestal widths uncorrelated with physics parameters



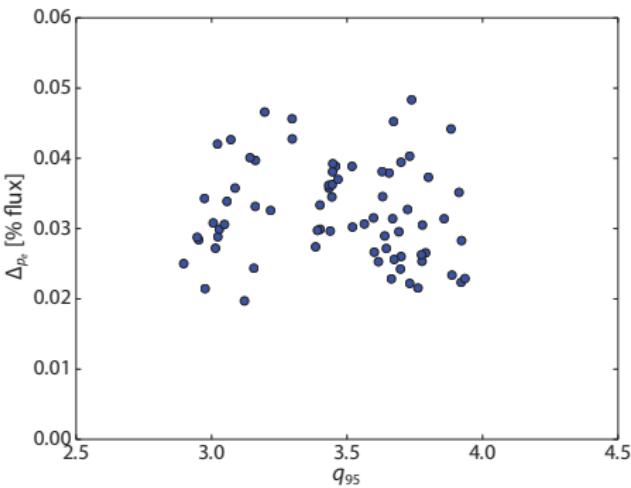
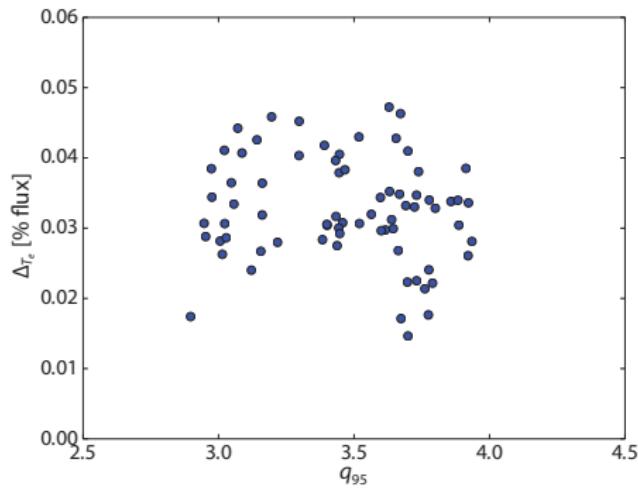
$\rho_{i,pol} \rightarrow$  ion-orbit-loss models for  $E_r$  well width

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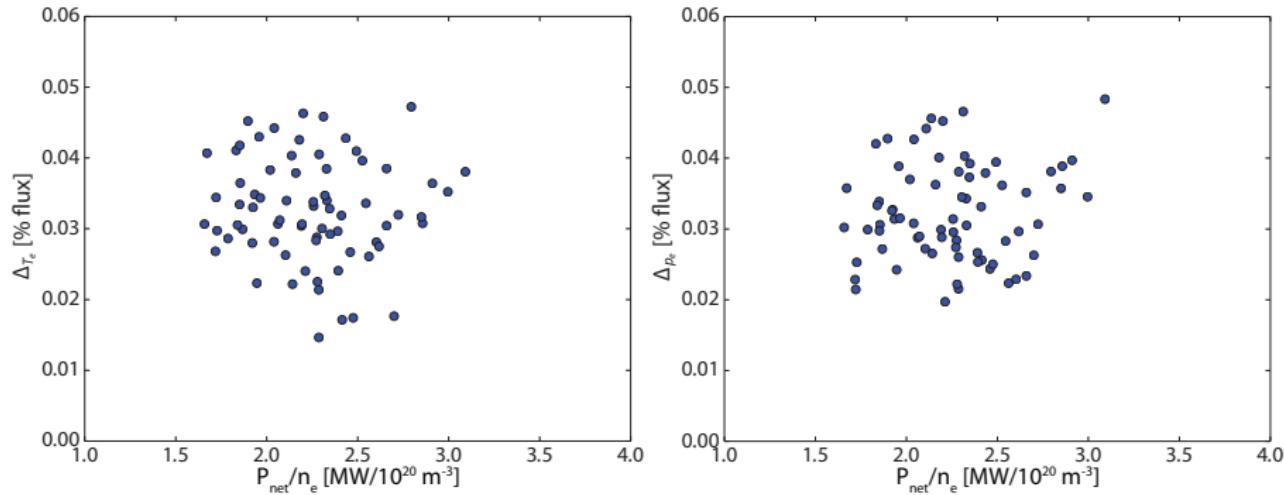
edge collisionality → bootstrap current instability drive

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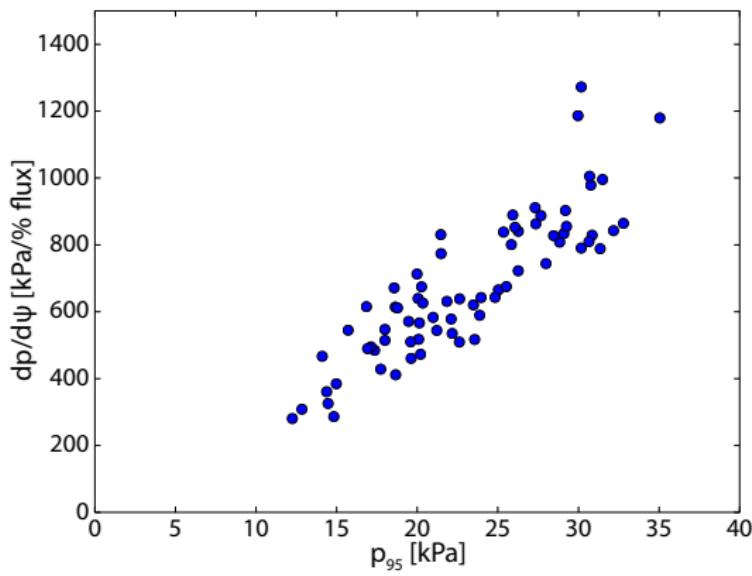
edge safety factor → magnetic shear, ballooning stabilization

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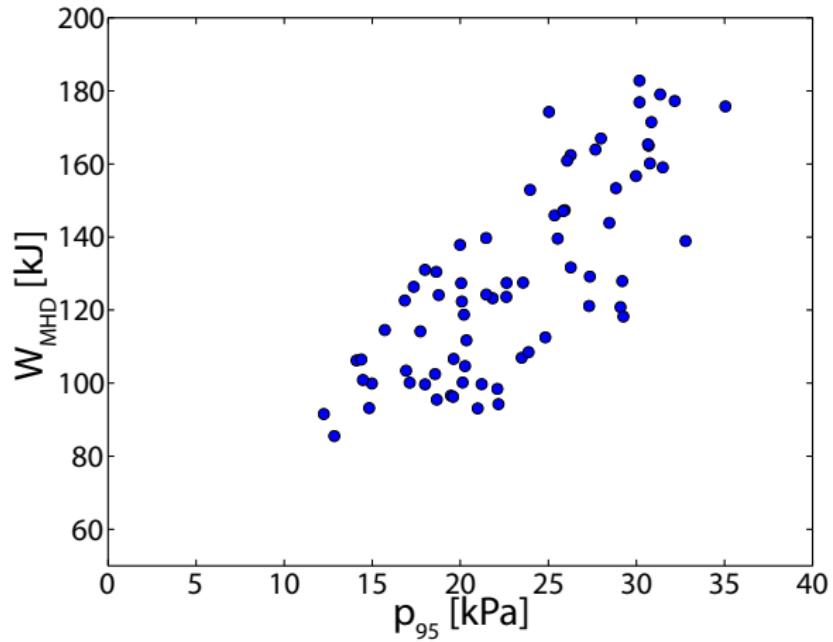
heating power per particle → heat flux through temperature pedestal

# I-mode pressure pedestal width robust across dataset

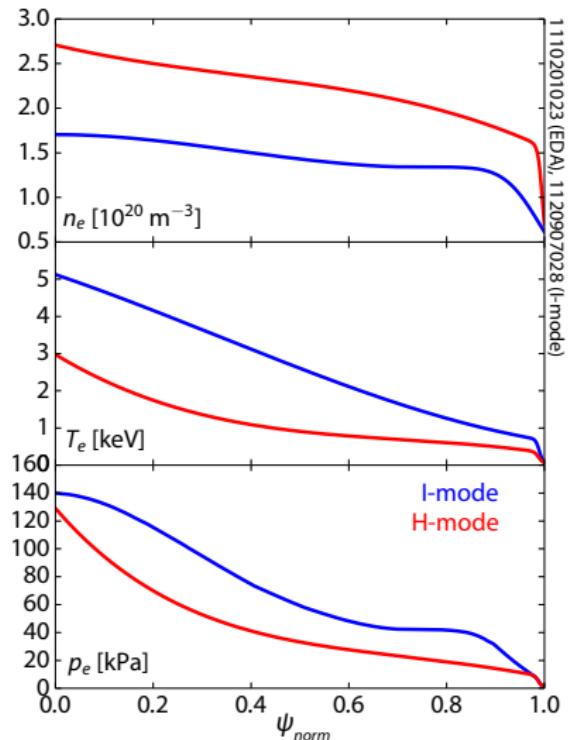


- width robust across dataset,  $\nabla p \sim p_{95}$
- suggests with increasing pressure, ballooning  $\nabla p$  boundary could be exceeded → ELMs
- independent density, temperature profile control = approach, but not exceed, limit

# Pedestal impacts core, global performance

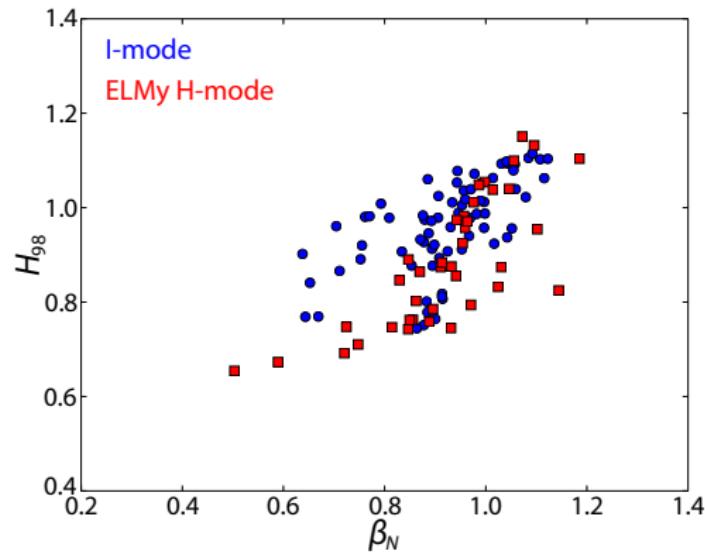
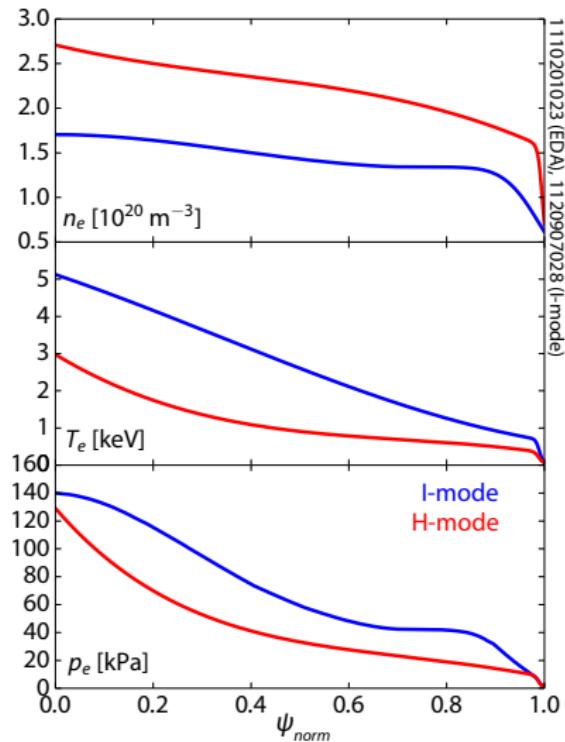


# Strong temperature pedestal supports high core temperature, pressure



- stiff ( $R/L_{T_e} \sim \text{fixed}$ ) temperature profiles  $\rightarrow$  higher  $T_{ped}$  supports greatly increased core temperatures
- provided moderated density peaking ( $n_{e,0}/\langle n_e \rangle \sim 1.1 - 1.3$  in I-mode), reaches comparable core, vol-average pressure despite relaxed  $p_{ped}$
- fusion-reactive plasma where  $T_e > 4 \text{ keV}$ , high  $T_{ped}$  maximizes fusing volume

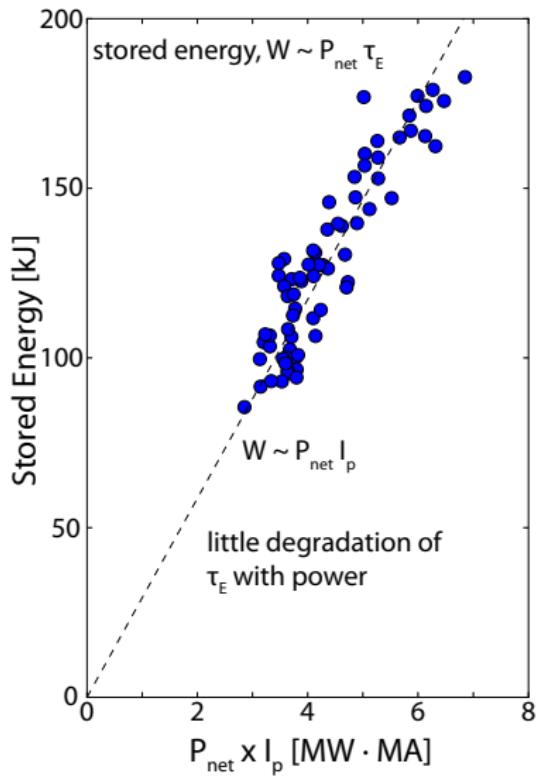
# Strong temperature pedestal supports high core temperature, pressure



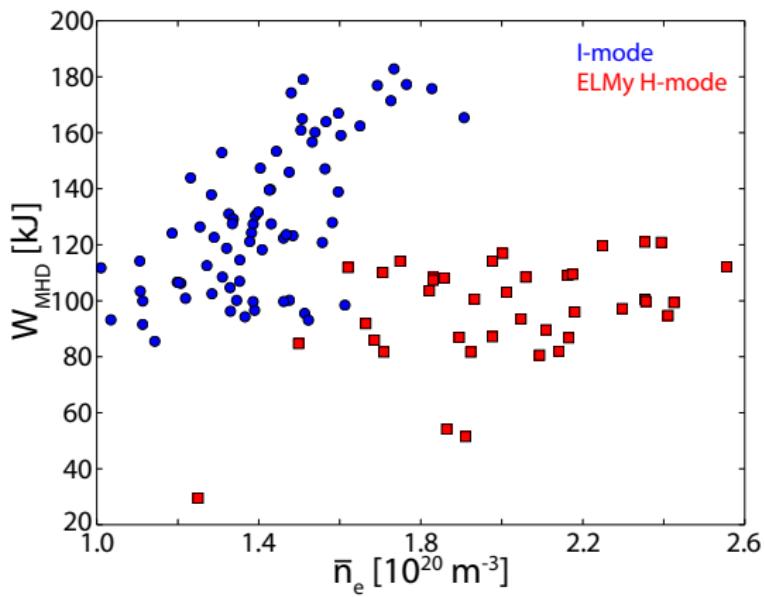
→ same  $\langle \beta_N \rangle$ , normalized confinement to ELMy H-mode

# Energy confinement lacks degradation with heating power

- Stored energy  $W \sim P\tau_E$
- for H-mode, expect  $\tau_E \sim I_p$ , with power degradation  $\tau_E \sim P^{-0.7}$  thus  $W \sim I_p P^{0.3}$
- I-mode stored energy  $W \sim I_p P_{net} \rightarrow$  little/no degradation of  $\tau_E$  with heating power
- reflects lack of MHD limit on pedestal



## ...As well as with fueling



- I-mode stored energy set by pedestal pressure, responding strongly to fueling
- ELMy H-mode stored energy set by pedestal  $\beta_p$ , limited by MHD constraint – mainly increase pedestal  $\beta_p$  with stronger shaping, flat relation with fueling

## First pass at an I-mode confinement scaling

Following practice in ITER89,ITER98 scalings, express I-mode energy confinement as a power law of the form

$$\tau_E = C I_p^{\alpha_{Ip}} B_T^{\alpha_{BT}} \bar{n}_e^{\alpha_{ne}} R^{\alpha_R} \varepsilon^{\alpha_\varepsilon} \kappa^{\alpha_\kappa} P_{loss}^{\alpha_P}$$

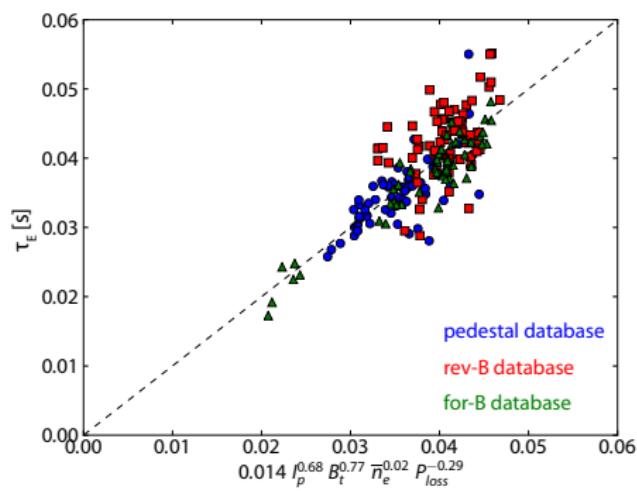
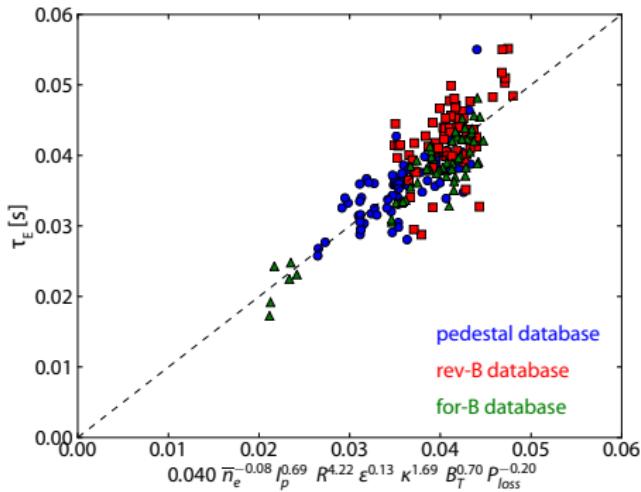
Using high-res pedestal database plus older forward- and reversed-field datasets for expanded parameter range

## Reduced fitting parameter set captures I-mode physics

	(a)	(b)	(c)
$C$	$0.040 \pm 0.066$	$0.014 \pm 0.002$	$0.056 \pm 0.008$
$I_p$	$0.686 \pm 0.074$	$0.685 \pm 0.076$	$0.676 \pm 0.077$
$B_T$	$0.698 \pm 0.075$	$0.768 \pm 0.072$	$0.767 \pm 0.072$
$\bar{n}_e$	$-0.077 \pm 0.055$	$0.017 \pm 0.048$	$0.006 \pm 0.048$
$R$	$4.219 \pm 4.623$		$2^*$
$\varepsilon$	$0.127 \pm 1.144$		$0.5^*$
$\kappa$	$1.686 \pm 0.398$		
$P_{loss}$	$-0.197 \pm 0.048$	$-0.286 \pm 0.042$	$-0.275 \pm 0.042$
$r^2$	0.713	0.685	0.683

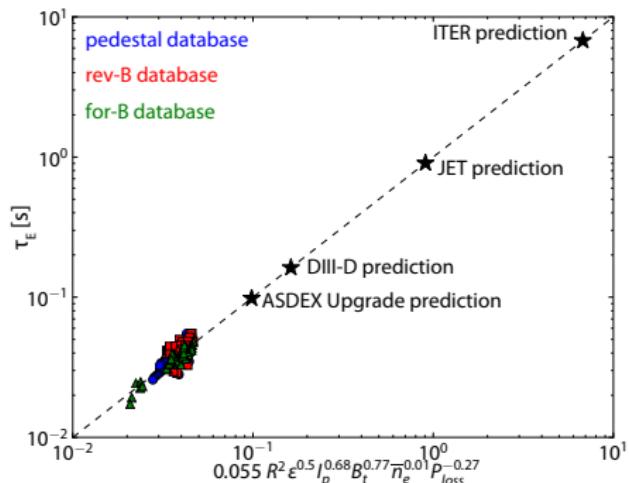
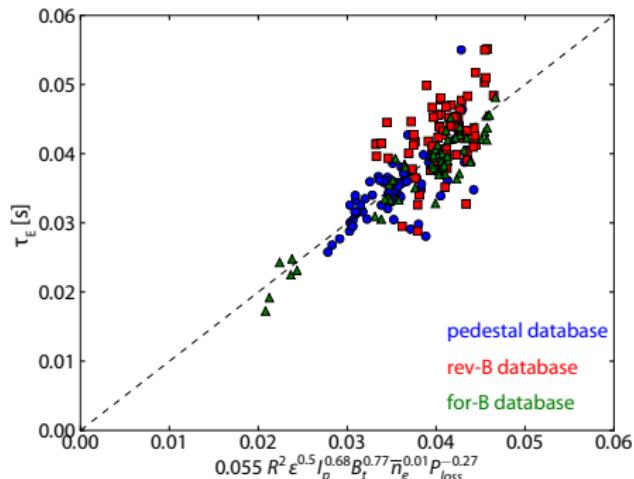
poor fitting in  $R$ ,  $\varepsilon$ ,  $\kappa$  due to restricted range in dataset

# Reduced fitting parameter set captures I-Mode physics



Both fits capture weak degradation of  $\tau_E$  with heating power, strong response to current, field

# Thought experiment: apply ITER98-like size dependence to I-mode scaling, extrapolate to larger machines?



Apply fixed  $R^2 \sqrt{\epsilon}$  size scaling – does not impact C-Mod data fit.  
Weak degradation  $\tau_E \sim P_{loss}^{-0.27}$  extrapolates highly favorably to large devices –  $\tau_E \sim 8$  s for ITER!

## I-mode behavior beneficial for global performance, confinement

- high temperature pedestal supports steep core  $\nabla T$ , comparable pressure and confinement despite relaxed pedestal
- stored energy responds strongly to heating power, fueling, consistent with pedestal response
  - ▶ good news: in burning plasma, alpha heating power  $\sim n_e^2$

## First-pass confinement scaling laws consistent with observed behaviors

- single-machine scaling captures strong response to current, field, weak degradation with heating power ( $\tau_E \sim P^{-\alpha}$ ,  $\alpha < 0.3$ )
  - ▶ consistent with assumptions in ITER simulations leading to  $Q = 10$  scenario<sup>6</sup>
- extrapolates to  $\tau_E \sim 8\text{ s}$  for ITER(!)

<sup>6</sup>DG Whyte, APS-DPP Nov. 2011

# Outline

## ■ I-Mode Pedestals & Global Performance<sup>2,3</sup>

- ▶ Pedestal response to fueling, heating power
- ▶ Pedestal widths and gradients
- ▶ Global performance and confinement scalings

## ■ I-Mode Pedestal Stability

- ▶ P-B MHD, KBM modeling
- ▶ ELM characterization

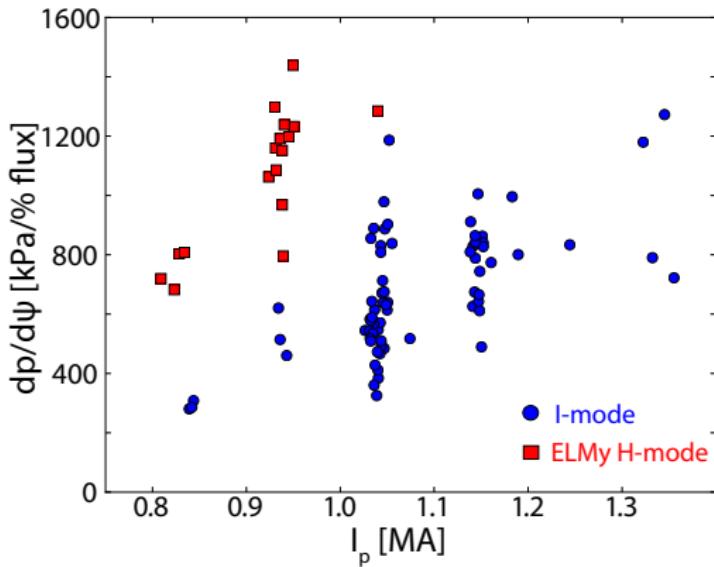
## ■ Summary, Future Work, & Questions

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<sup>2</sup>JR Walk *et al.*, *Physics of Plasmas* 21 (2014)

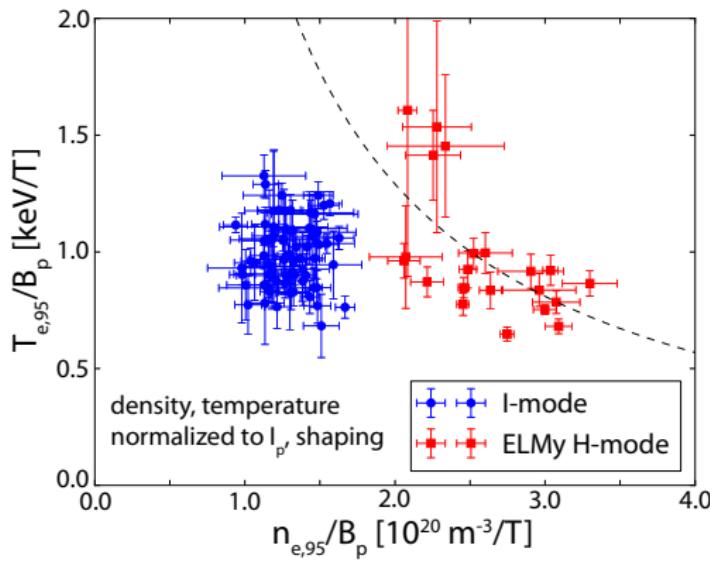
<sup>3</sup>Invited talk, APS-DPP Nov. 2013

# Pedestal pressure gradient suggests MHD stability, headroom for performance improvement



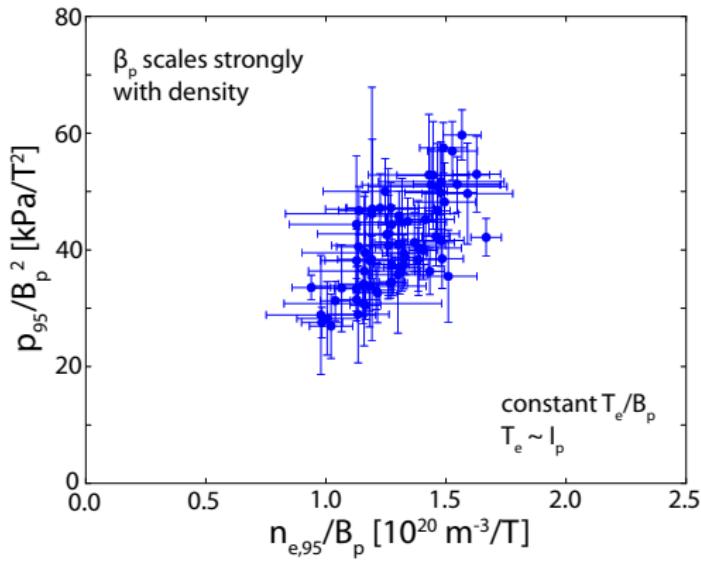
- Pedestal  $\nabla p$  shallower at given  $I_p$  than ELMy H-mode due to lack of density pedestal
- Gradients scale more weakly than  $\nabla p \propto I_p^2$  from ballooning MHD (critical-gradient) stability boundary

# I-mode pedestal scalings consistent with stability against peeling-balloonning MHD



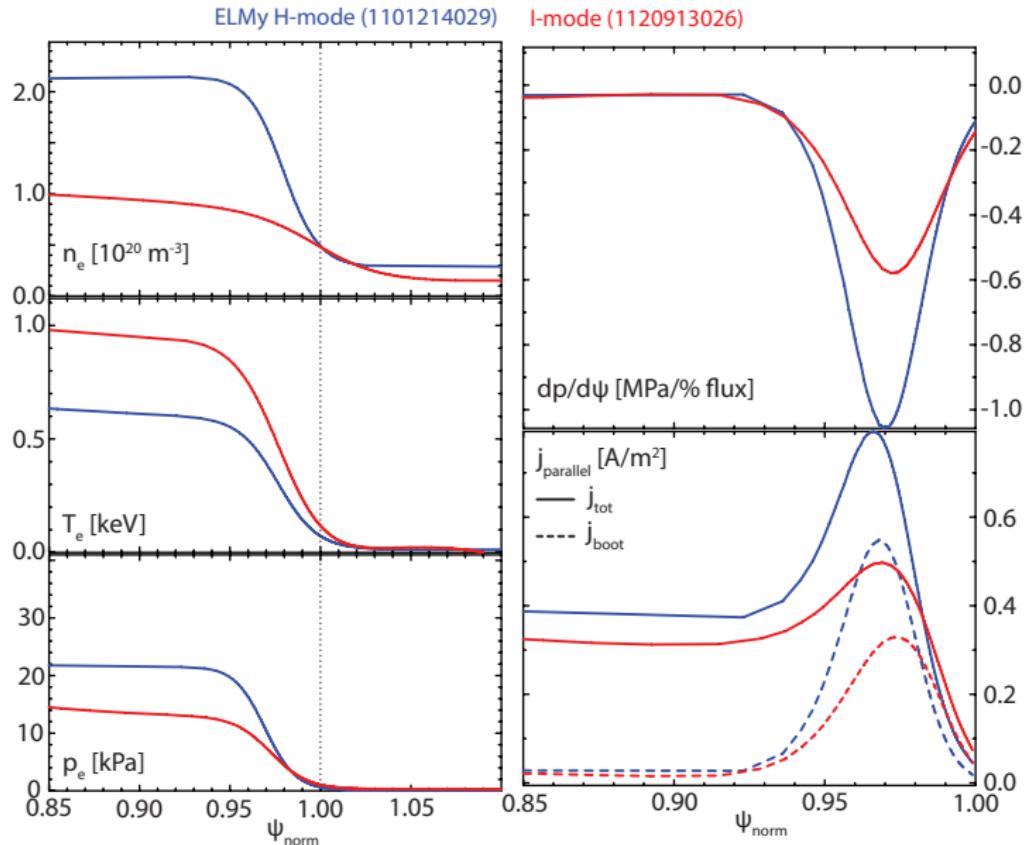
- ballooning stability, to lowest order, limits pedestal  $\beta_p$  in ELMy H-mode; I-mode  $n_e$ ,  $T_e$  independent, rather than fixed  $n_e T_e$
- Pedestal  $\beta_p$  scaling with density consistent with constant  $T_{e,95}/B_p \rightarrow T_e \sim I_p$ , rather than  $T_e \sim 1/n_e$

# I-mode pedestal scalings consistent with stability against peeling-balloonning MHD

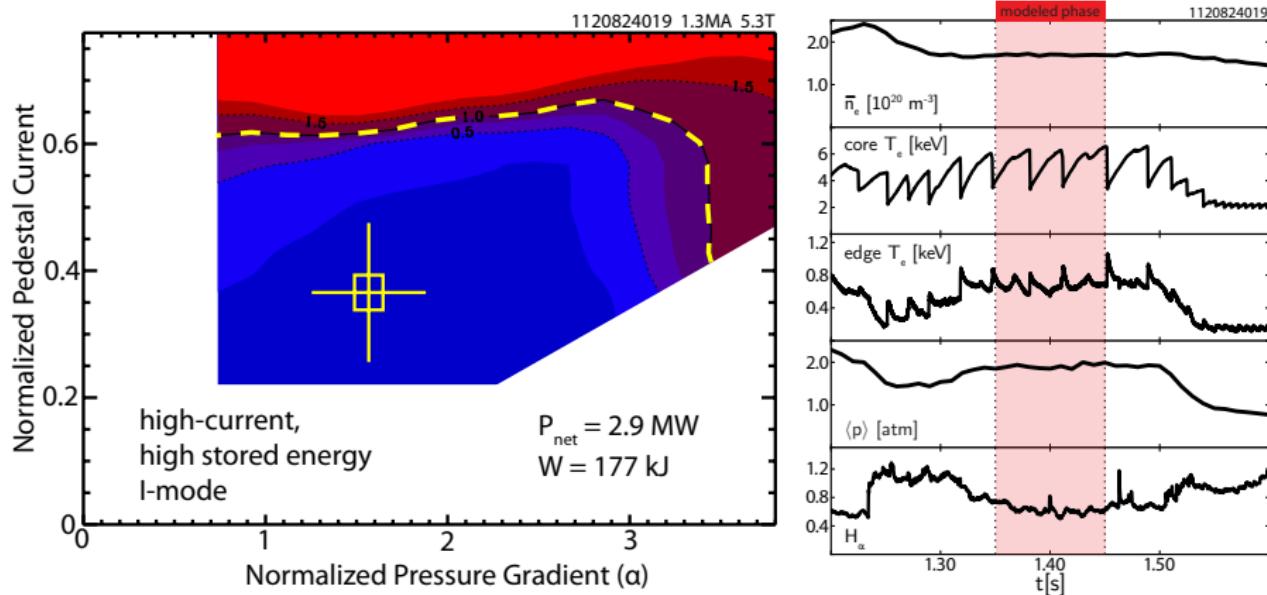


- ballooning stability, to lowest order, limits pedestal  $\beta_p$  in ELM My H-mode; I-mode  $n_e$ ,  $T_e$  independent, rather than fixed  $n_e T_e$
- Pedestal  $\beta_p$  scaling with density consistent with constant  $T_{e,95}/B_p \rightarrow T_e \sim I_p$ , rather than  $T_e \sim 1/n_e$

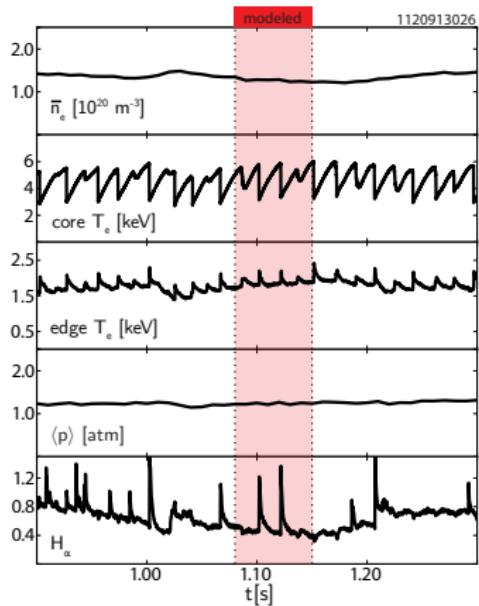
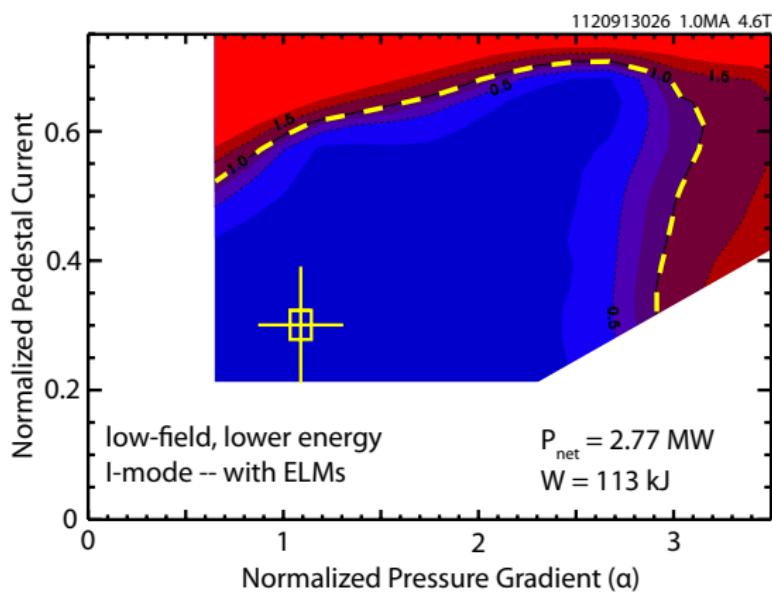
# Stability is self-enforcing for I-mode pedestals



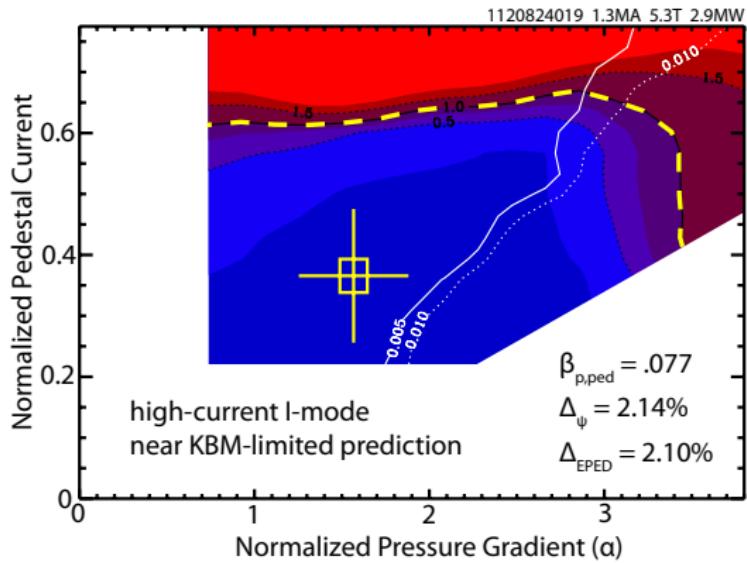
# I-mode pedestal strongly stable against peeling-balloonning MHD, KBM turbulence



# Including in low-field, low-energy cases exhibiting apparent ELMs

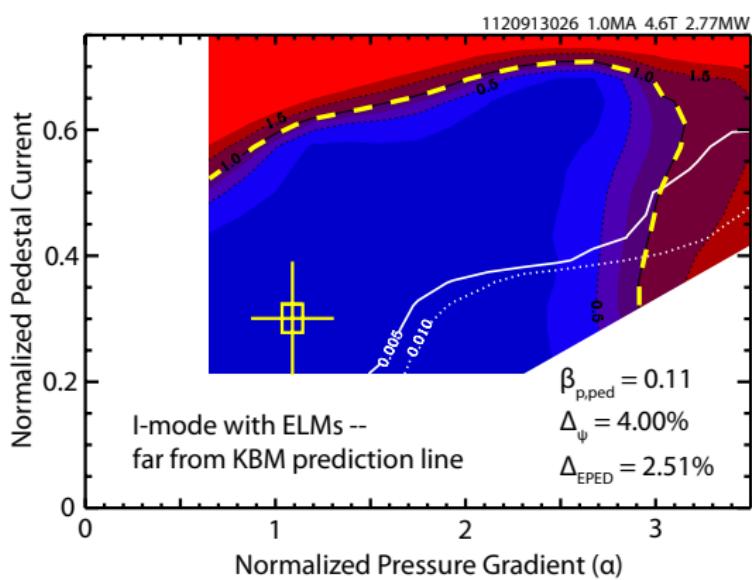


# I-mode pedestal modeled to be below KBM threshold as well, including cases with ELMs



- KBM-limited (EPED1) prediction for width,  $\Delta_{EPED} = 0.076\beta_{p,ped}^{1/2}$
- BALOO calculates width of pedestal locally beyond threshold – mode onset when half of pedestal is unstable
- I-mode cases spanning width range modeled below threshold

# I-mode pedestal modeled to be below KBM threshold as well, including cases with ELMs



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- BALOO calculates width of pedestal locally beyond threshold – mode onset when half of pedestal is unstable
- I-mode cases spanning width range modeled below threshold

## EPED physics assumptions alone are not capturing all observed edge behavior in I-mode

I-mode pedestal is stable against identified ELM triggers – however, in minority of cases (12 time windows / 10 unique shots, out of dataset of 72 time windows / 52 shots), particularly at low field ( $\sim 4.6$  T) exhibit small, intermittent events that appear to be ELMs.

→ need to more carefully characterize these events!

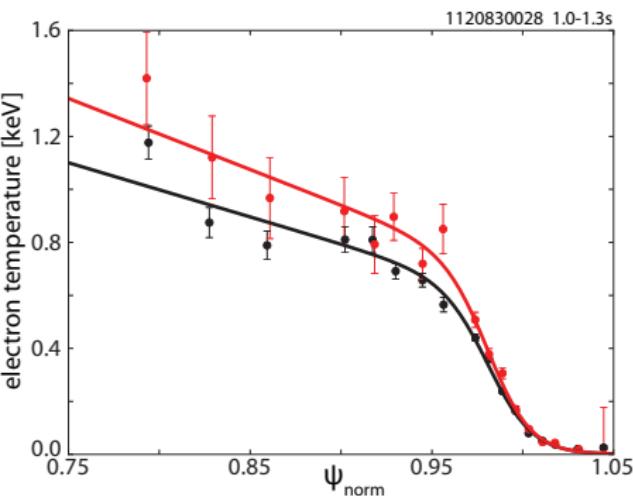
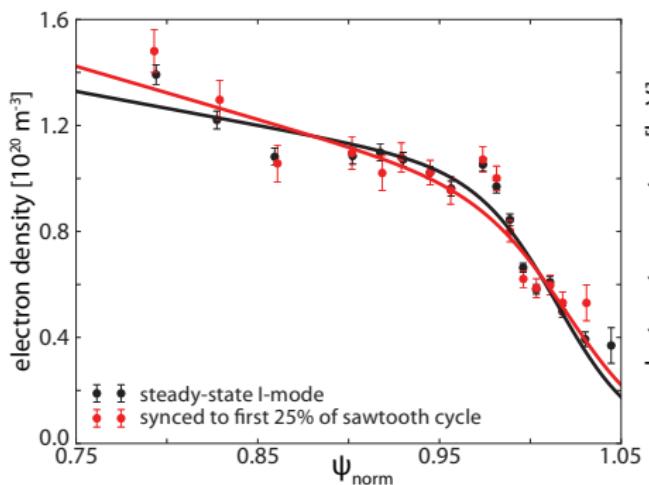
# What is an ELM?

ELMs denoted by:

- burst of ionization in edge → spike in  $H_\alpha$  light
- “explosive” crash in pedestal, both temperature and pressure
- unstable fluctuation leading up to ELM (P-B MHD instability, magnetic precursors, turbulent fluctuations...)

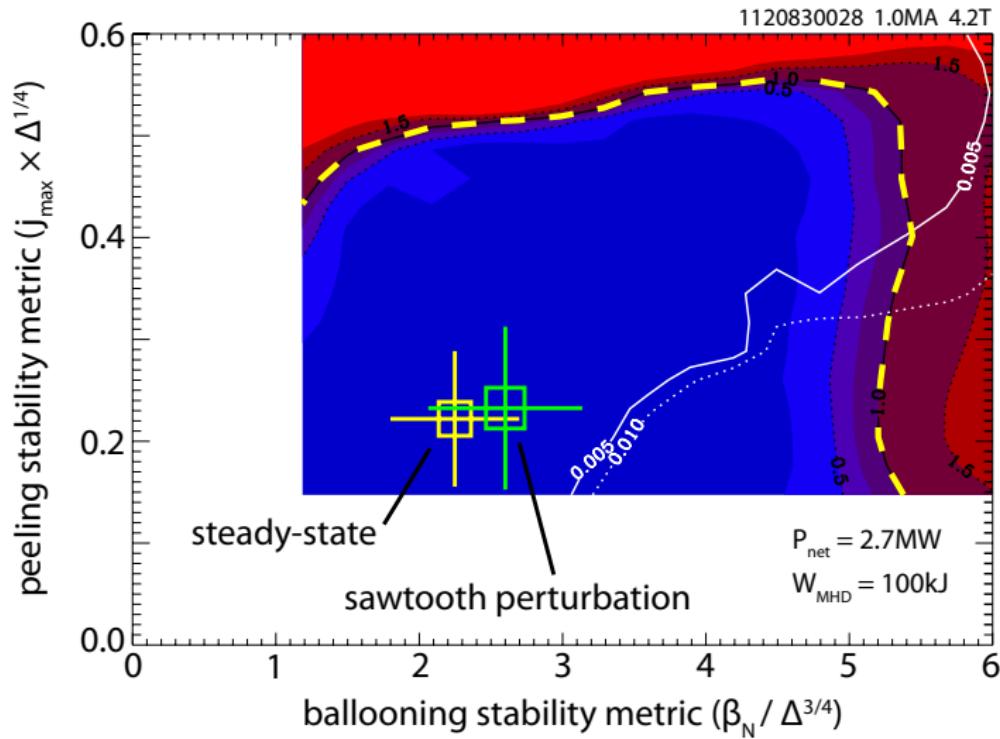
observations of ELMs in I-mode based on  $H_\alpha$  spikes, in most cases ( $\sim 70\%$ ) tied to the sawtooth heat pulse reaching the edge – good place to begin!

# Sawtooth heat pulse modifies temperature pedestal, little impact on density profile

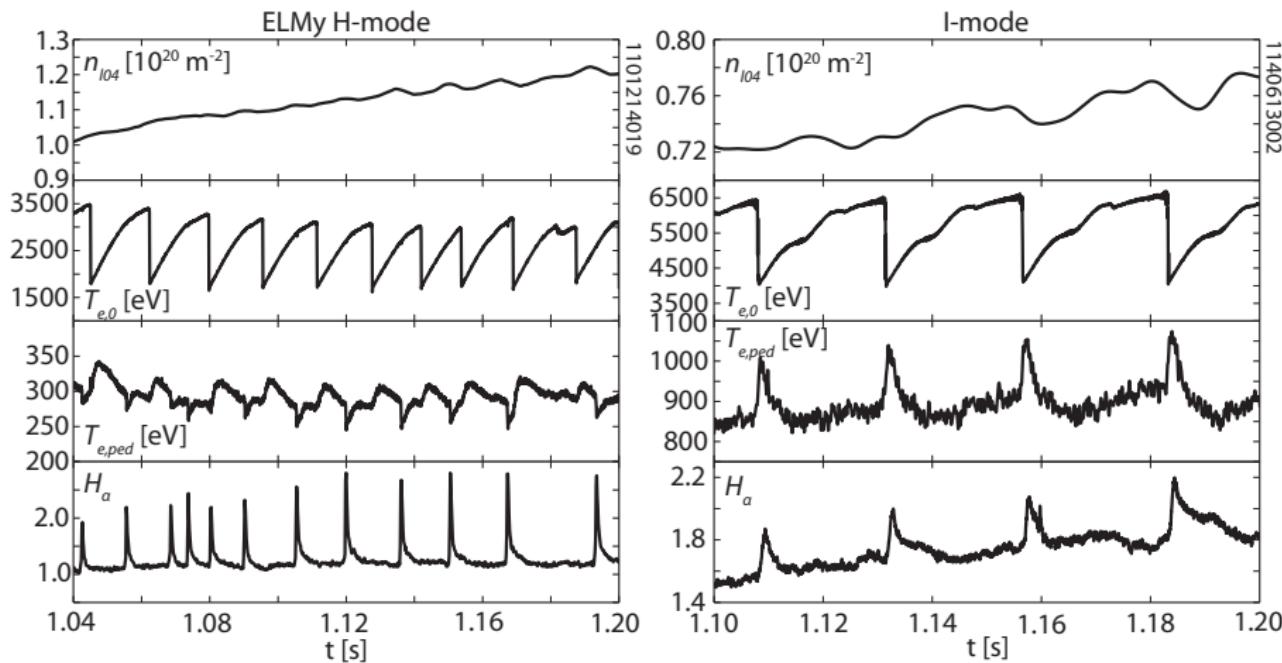


prepare data by masking TS frames to first 25% of sawtooth cycle  
(immediately following heat pulse reaching edge) – similar to  
ELM-binning technique used for ELMy H-mode

Sawtooth measurably perturbs pedestal in stability space, but insufficient to reach ELM threshold



I-mode sawtooth  $H_\alpha$  events (mostly) do not exhibit characteristic temperature crash expected for ELMs



## These events do not appear to be ELMs

Given the lack of a temperature pedestal crash and the computed stability against known ELM triggers, these events appear to not be instability-driven ELMs at all – best described simply as “sawtooth-driven  $H_\alpha$  bursts.”

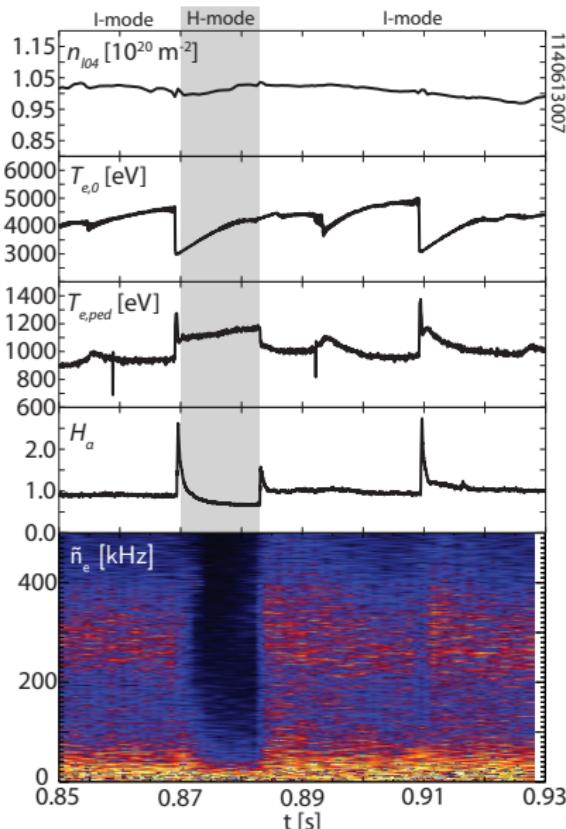
possible explanations:

- ionization front impacting neutrals in SOL?
- density transport effect from sawtooth interaction with WCM?

which raise questions:

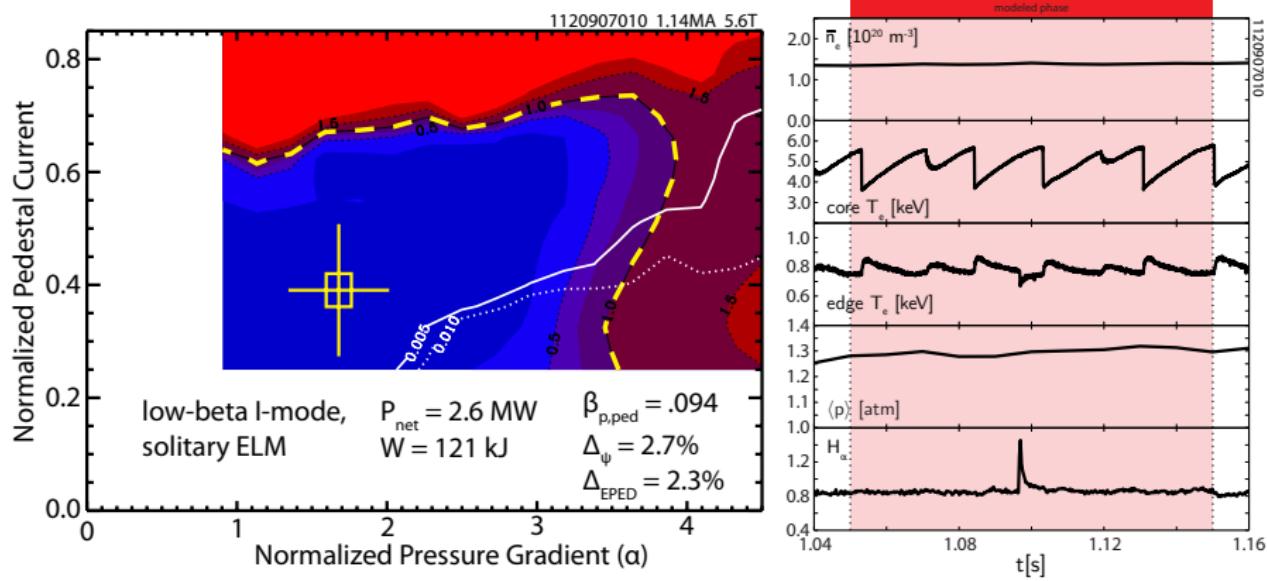
- why are these sometimes triggered – field, shaping, density effects?
- under comparable conditions, why are  $H_\alpha$  spikes inconsistently triggered by similarly-sized sawteeth?

# Minority of $H_\alpha$ spikes do appear to be ELMs, however



- Few events (10 out of 37 total events) do exhibit observable drop in edge  $T_e$  with spike, are not necessarily triggered by sawteeth
- suggests these are “true” ELMs – but perturbation is still small, < 1% stored energy drop,  $T_e$  crash on sawtooth-triggered ELMs insufficient to overcome  $T_e$  increase from heat pulse

# Stationary pedestal structure around intermittent ELMs still stable to P-B MHD, KBM threshold



- $H_{\alpha}$  spikes (putative ELMs) in minority of I-mode cases (12 out of 72 time windows)
- Majority ( $\sim 70\%$ , 27/37) of identified events do not appear to be ELMs at all, consistent with computed stability and observed pedestal behavior – rather, are benign  $H_{\alpha}$  pulses triggered by sawteeth
- a few do exhibit ELM behavior, not necessarily triggered on sawteeth – but these are rare, small
  - ▶ stationary pedestal structure still stable – transient modifications to hit stability boundary?

# Outline

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<sup>2</sup>JR Walk *et al.*, *Physics of Plasmas* 21 (2014)

<sup>3</sup>Invited talk, APS-DPP Nov. 2013

# ELMy H-mode

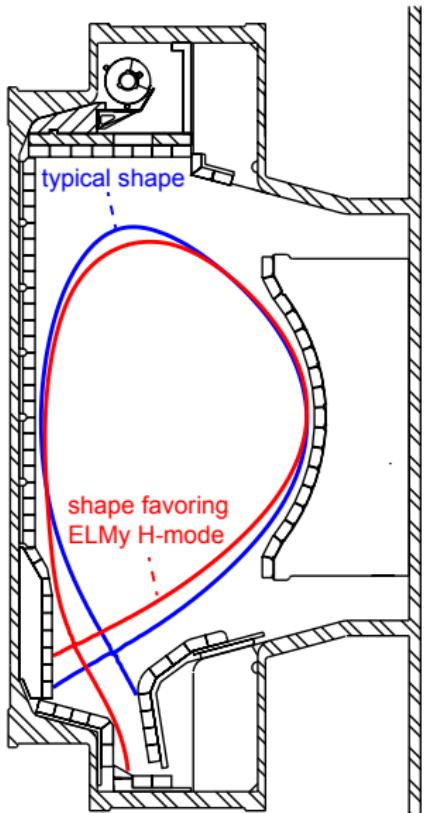
# I-mode pedestals & performance

# I-mode stability & ELM characterization

# Supplemental Slides



# Plasma shaping in C-Mod operation

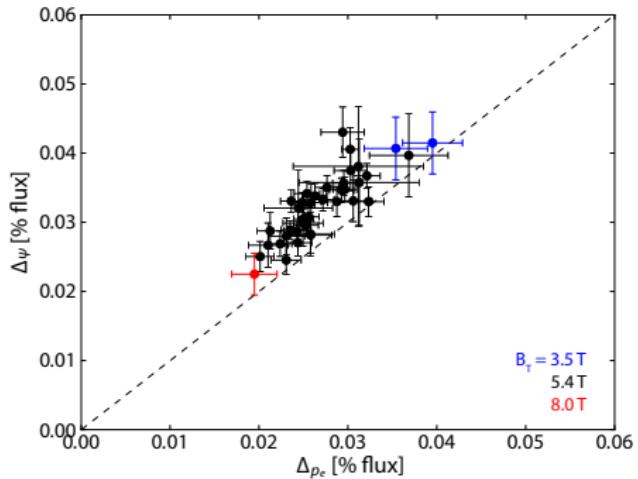
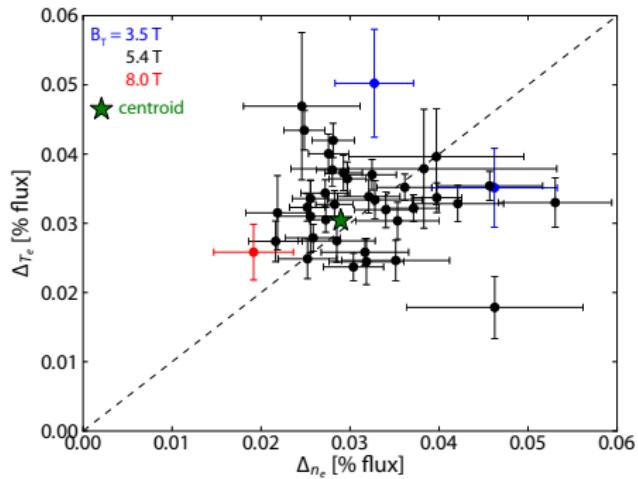


- I-mode operates at typical shaping for C-Mod plasmas (with reversed  $I_p$ ,  $B_T$  for unfavorable  $\nabla B$  drift)
- ELM My H-mode on C-Mod requires special shaping with low elongation, upper triangularity, high lower triangularity – in normal shaping in forward field, reach ELM-free H-mode (low  $\nu^*$ ) or EDA H-mode (high  $\nu^*$ )

# ELMy H-mode

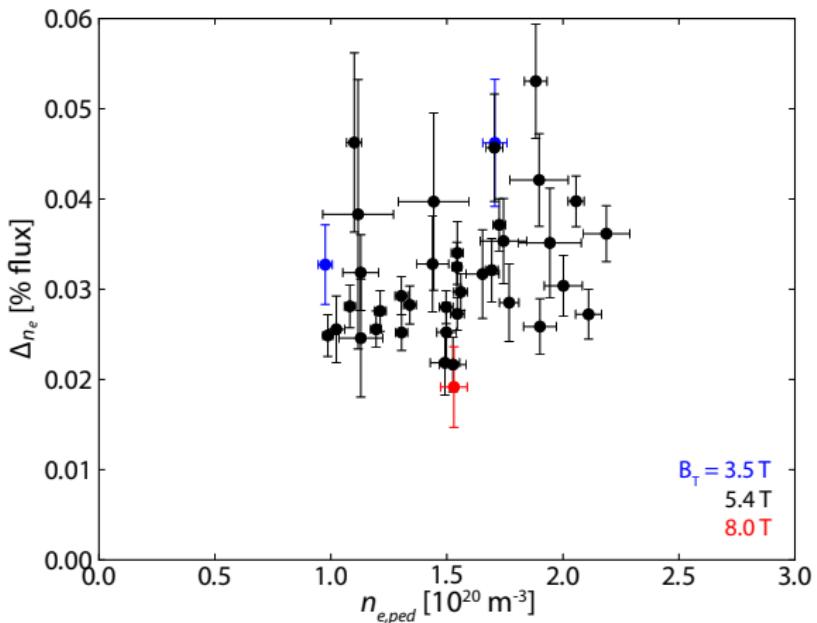


# Density, temperature, and pressure widths in ELMy H-mode



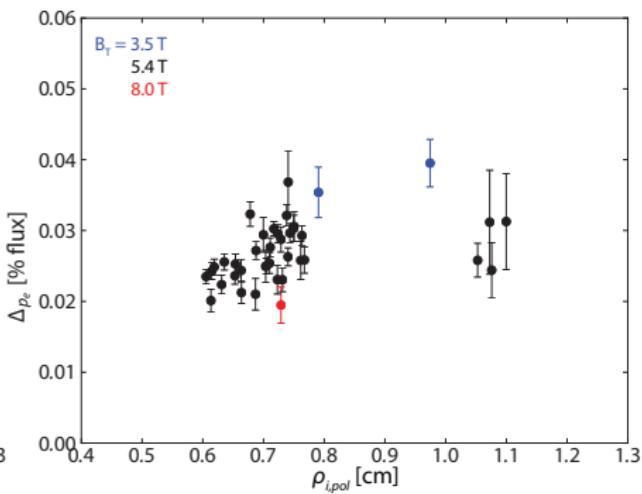
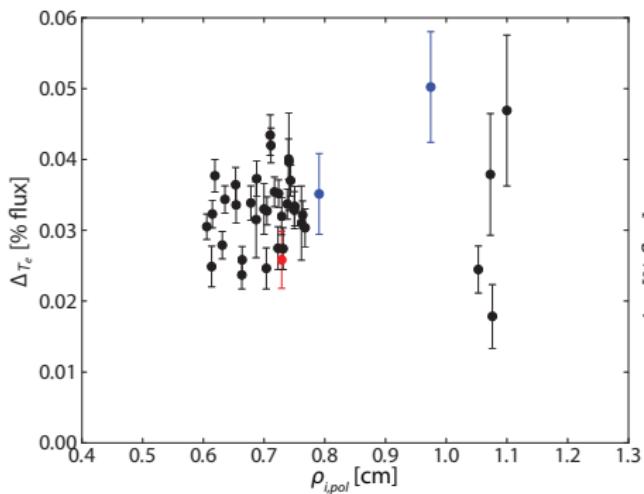
$$\Delta_\psi = (\Delta n_e + \Delta T_e)/2, \text{ tracks with directly-measured } \Delta p_e$$

# Density pedestal width in ELM My H-mode inconsistent with neutral-penetration model



as expected from high-density, neutral-opaque SOL on C-Mod

# Temperature, pressure pedestal widths not well-described by gyroradius scaling



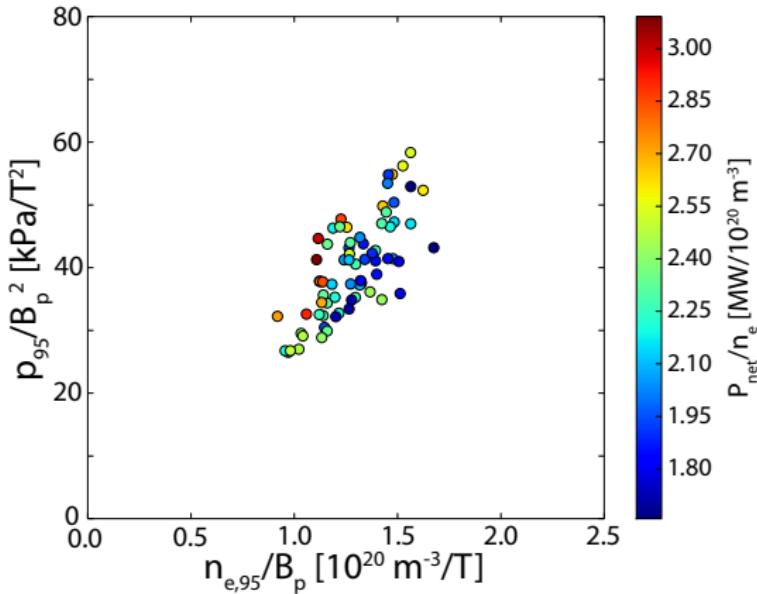
$T_e$  pedestal width uncorrelated;  $p_e$  pedestal width trend due to covariance between  $\rho_{i,pol} \sim \sqrt{T_{e,ped}}/I_p$  and  $\sqrt{\beta_{p,ped}} \sim \sqrt{n_{e,ped} T_{e,ped}}/I_p$

# I-mode pedestals



## $\beta_{p,95}$ scaling with norm. density in addition to heating-power response

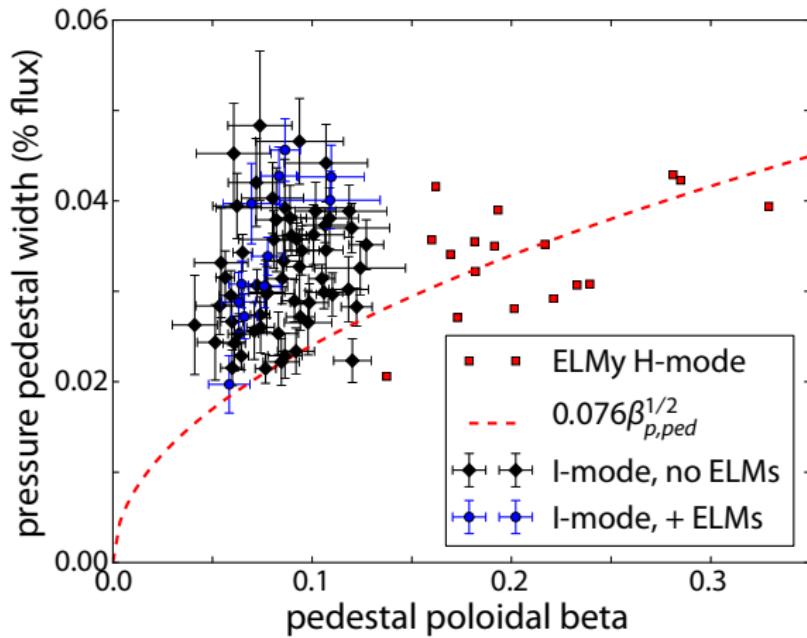
- $P_{net}/\bar{n}_e$  sets slope of  $T_e/B_p$  line – response of pedestal temperature at fixed current
- pressure responds to fueling, provided sufficient power to maintain the pedestal



# I-mode stability & ELM characterization



I-modes exhibiting edge  $H_\alpha$  spikes / ELMs typically at lower  $\beta_p$  range



# MHD stability analysis



$$\vec{Q} = \nabla \times (\vec{\xi} \times \vec{B})$$

$$\delta W = \delta W_F + \delta W_S + \delta W_V$$

$$\begin{aligned}\delta W_F = & \frac{1}{2} \int_P d^3\vec{r} \left[ \frac{|\vec{Q}|^2}{\mu_0} + \frac{B^2}{\mu_0} \left| \nabla \cdot \vec{\xi}_\perp + 2\vec{\xi}_\perp \cdot \vec{\kappa} \right|^2 + \gamma p \left| \nabla \cdot \vec{\xi} \right|^2 \right. \\ & \left. - 2 \left( \vec{\xi}_\perp \cdot \nabla p \right) \left( \vec{\kappa} \cdot \vec{\xi}_\perp^* \right) - j_{||} \left( \vec{\xi}_\perp^* \times \vec{b} \right) \cdot \vec{Q}_\perp \right]\end{aligned}$$

$$\delta W_S = \frac{1}{2} \int_S dS \left| \hat{n} \cdot \vec{\xi}_\perp \right|^2 \hat{n} \cdot \left[ \nabla \left( p + \frac{B^2}{2\mu_0} \right) \right]$$

$$\delta W_V = \frac{1}{2} \int_V d^3\vec{r} \frac{|B_1|^2}{\mu_0}$$

$$X = RB_p \xi_\psi$$

$$ik_{\parallel} = \frac{1}{JB} \left( \frac{\partial}{\partial \chi} + i n \nu \right) \quad \quad \nu = JB_T / R$$

$$P = \sigma X + \frac{B_p^2}{\nu B^2} \frac{F}{n} \frac{\partial}{\partial \psi} (JBk_{\parallel} X)$$

$$Q = \frac{X}{B^2} \frac{dp}{d\psi} + \frac{F^2}{\nu R^2 B^2} \frac{1}{n} \frac{\partial}{\partial \psi} (JBk_{\parallel} X)$$

$$\sigma = - \frac{F}{B^2} \frac{dp}{d\psi} - \frac{dF}{d\psi} = - \frac{j_{\parallel}}{B}$$

$$\begin{aligned}
\delta W = \pi \iint d\psi d\chi & \left\{ \frac{JB^2}{R^2 B_p^2} |k_{\parallel} X|^2 + \frac{R^2 B_p^2}{JB^2} \left| \frac{1}{n} \frac{\partial}{\partial \psi} (JBk_{\parallel} X) \right|^2 \right. \\
& - \frac{2J}{B^2} \frac{dp}{d\psi} \left[ |X|^2 \frac{\partial}{\partial \psi} \left( p + \frac{B^2}{2} \right) - \frac{iF}{JB^2} \frac{\partial}{\partial \chi} \left( \frac{B^2}{2} \right) \frac{X^* \partial X}{n \partial \psi} \right] \\
& - \frac{X^*}{n} JBk_{\parallel} \left( X \frac{d\sigma}{d\psi} \right) + \frac{1}{n} [PJBk_{\parallel}^* Q^* + P^* JBk_{\parallel} Q] \\
& \left. + \frac{\partial}{\partial \psi} \left[ \frac{\sigma}{n} X^* JBk_{\parallel} X \right] \right\}
\end{aligned}$$

magnetic line bending: stabilizing

$$\delta W = \pi \iint d\psi d\chi \left\{ \frac{JB^2}{R^2 B_p^2} |k_{\parallel} X|^2 + \frac{R^2 B_p^2}{JB^2} \left| \frac{1}{n} \frac{\partial}{\partial \psi} (JB k_{\parallel} X) \right|^2 \right\}$$

ballooning  
drive

$$- \frac{2J}{B^2} \frac{dp}{d\psi} \left[ |X|^2 \frac{\partial}{\partial \psi} \left( p + \frac{B^2}{2} \right) - \frac{iF}{JB^2} \frac{\partial}{\partial \chi} \left( \frac{B^2}{2} \right) \frac{X^* \partial X}{n \partial \psi} \right]$$

kink  
drive

$$- \frac{X^*}{n} JB k_{\parallel} \left( X \frac{d\sigma}{d\psi} \right) + \frac{1}{n} [ P J B k_{\parallel}^* Q^* + P^* J B k_{\parallel} Q ] \\ + \frac{\partial}{\partial \psi} \left[ \frac{\sigma}{n} X^* J B k_{\parallel} X \right] \} \quad \begin{array}{l} \text{magnetic curvature: stabilizing inboard,} \\ \text{destabilizing outboard} \end{array}$$

surface term: peeling drive

ELITE solves this for given  $n$  by encoding the poloidal angle  $\chi$  in a straight-line coordinate via the “ballooning transform,”

$$\omega = \frac{1}{q} \int^{\chi} \nu \, d\chi$$

(note  $2\pi q = \oint \nu \, d\chi$ ) and decomposing the displacement  $X$  into poloidal harmonics

$$X = \sum_m u_m(\psi) e^{-im\omega}$$

centered on the  $(m, n)$  rational surface. Define a “fast” radial variable

$$x = m_0 - nq$$
$$m_0 = \text{Int}(nq_a) + 1$$

readily convertible between  $x$  and  $\psi$ .

Euler-Lagrange equation minimizing the energy may be expressed in this harmonic expansion by a set of coupled equations<sup>7</sup>

$$A_{m,m'}^{(2)} \frac{d^2 u_m}{d\psi^2} + A_{m,m'}^{(1)} \frac{du_m}{d\psi} + A_{m,m'}^{(0)} u_m = 0$$

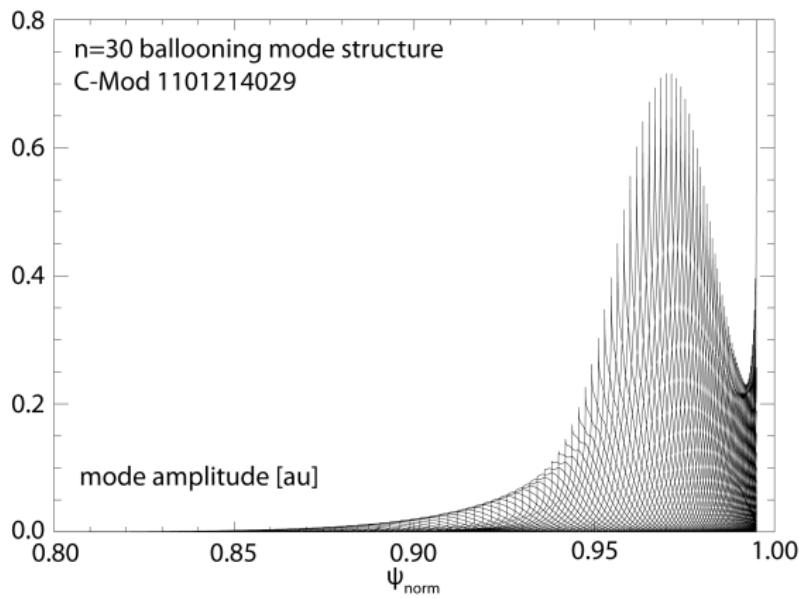
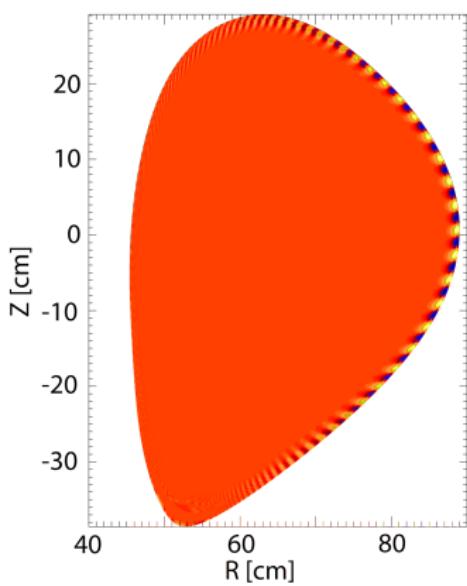
describing coupling between harmonics  $m, m'$ , with matrix elements  $A$  calculated from the equilibrium describing the mode amplitudes. Features:

- $u_m$  varies rapidly ( $\sim x$ , comparable to spacing between rational surfaces), needs fine mesh;  $A$  set by equilibrium parameters, varies more slowly, can be calculated on coarse mesh for numerical efficiency
- modes only couple to few nearest neighbors, so most  $A_{m,m'}$  may be ignored
- can quickly calculate “fictitious eigenvalue” for stable/unstable determination, or true eigenvalue  $\gamma^2$  for mode growth rate when inertial terms included (modifications to matrix elements  $A$ )

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<sup>7</sup>HR Wilson et al., *Physics of Plasmas* **9** (2002)

# ELITE radial, poloidal mode structure for $n = 30$ ballooning mode



BALOO solves simplified version of ballooning energy formulation, in the  $n \rightarrow \infty$  limit: reduces to 1-D eigenvalue equation,

$$(L_0 + \omega^2 M_0)f = 0$$

$$X = f(\psi, y)e^{-in \int \nu dy}$$

for displacement  $X$  and ballooning-transformed angle  $y$ , given by

$$L_0 f = \frac{\partial}{\partial y} \left\{ \frac{1}{JR^2 B_p^2} \left[ 1 + \left( \frac{R^2 B_p^2}{B} \int^y \frac{d\nu}{d\psi} dy \right)^2 \right] \frac{\partial f}{\partial y} \right\}$$

$$+ f \left\{ \frac{2J}{B^2} \frac{dp}{d\psi} \frac{\partial}{\partial \psi} \left( p + \frac{B^2}{2} \right) - \frac{F}{B^4} \frac{dp}{d\psi} \left( \int^y \frac{d\nu}{d\psi} dy \right) \frac{\partial B^2}{\partial y} \right\}$$

$$M_0 f = \frac{J}{R^2 B_p^2} \left[ 1 + \left( \frac{R^2 B_p^2}{B} \int^y \frac{d\nu}{d\psi} dy \right)^2 \right] f$$