Performance-Portable Implicit Scale-Resolving Compressible Flow Using libCEED

SIAM CSE 2023

James Wright, Jed Brown, Kenneth Jansen, Leila Ghaffari February 27, 2023

Ann and H.J. Smead Department of Aerospace Engineering Sciences



Outline

- 1. libCEED Overview
- 2. Compressible Fluid Equations in libCEED
- 3. Viscous Outflow Boundary Conditions
- 4. Efficient Implicit Timestepping



libCEED Overview



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- Geared toward high-order finite element discretizations



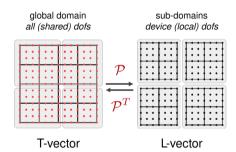
$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$

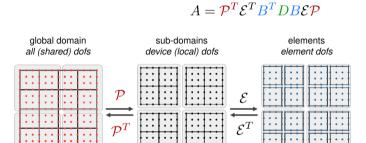
global domain all (shared) dofs



T-vector

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$



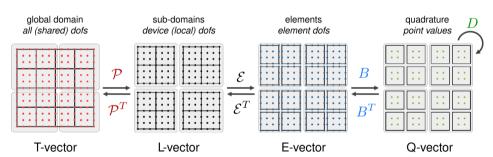


L-vector

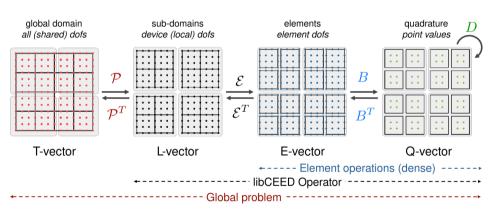
E-vector

T-vector

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$



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Compressible Fluid Equations in libCEED

Compressible Navier-Stokes

$$\mathbf{A_0}\mathbf{Y}_{.t} + \mathbf{F}_{i.i}(\mathbf{Y}) - S(\mathbf{Y}) = 0$$

for

$$\mathbf{A_0} \underbrace{\begin{bmatrix} p \\ u_i \\ T \end{bmatrix}}_{\mathbf{Y}} = \begin{bmatrix} \rho \\ \rho u_i \\ \rho e \end{bmatrix}, \quad \mathbf{F}_i(\mathbf{Y}) = \underbrace{\begin{pmatrix} \rho u_i \\ \rho u_i u_j + p \delta_{ij} \\ (\rho e + p) u_i \end{pmatrix}}_{\mathbf{F}_i^{\text{adv}}} + \underbrace{\begin{pmatrix} 0 \\ -\sigma_{ij} \\ -\rho u_j \sigma_{ij} - kT_{,i} \end{pmatrix}}_{\mathbf{F}_i^{\text{diff}}}, \quad S(\mathbf{Y}) = -\begin{pmatrix} 0 \\ \rho \mathbf{g} \\ 0 \end{pmatrix}$$

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Find $\boldsymbol{Y} \in \mathcal{S}^h$, $\forall \boldsymbol{v} \in \mathcal{V}^h$

$$\int_{\Omega} \boldsymbol{v} \cdot \left(\boldsymbol{A_0} \boldsymbol{Y}_{,t} - \boldsymbol{S}(\boldsymbol{Y}) \right) \, \mathrm{d}\Omega + \int_{\Omega} \boldsymbol{v} \cdot \boldsymbol{F}_{i,i}(\boldsymbol{Y}) \, \, \mathrm{d}\Omega$$

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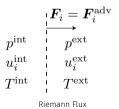
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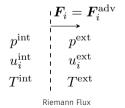
$$\Rightarrow \quad \mathcal{P}^{T} \mathcal{E}^{T} B^{T} G B \mathcal{E} \mathcal{P} \begin{bmatrix} \mathbf{Y}_{,t} \\ \mathbf{Y} \end{bmatrix} = 0$$



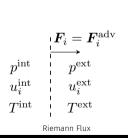
· Riemann Flux BCs everywhere is ideal

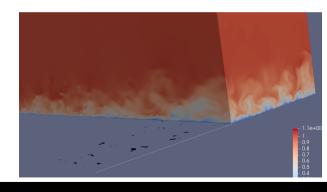


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- · Riemann Flux BCs everywhere is ideal
- \cdot Velocity not known *a priori* \longrightarrow traditional Riemann BCs not applicable
- Weak-pressure prescription ill-posed for recirculation

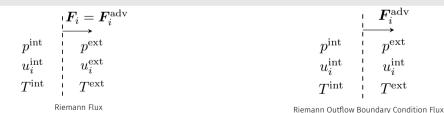




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Solution

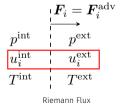
· Calculate F_i^{adv} via Riemann solver, setting $u_i^{\text{ext}} = u_i^{\text{int}}$

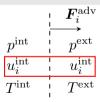


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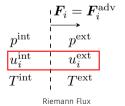


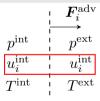
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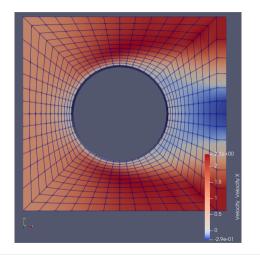
- · Calculate F_i^{adv} via Riemann solver, setting $u_i^{\text{ext}} = u_i^{\text{int}}$
- · Calculate F_i^{diff} from solution, then $F_i = F_i^{\text{adv}} + F_i^{\text{diff}}$





Riemann Outflow Boundary Condition Flux

Viscous Outflow Boundary Conditions Demonstration



- · Cylinder in cross flow torture test
- · Stable for significant outflow recirculation
- \cdot Only p and T set at boundary

Efficient Implicit Timestepping

Implicit timestepping requires solving:

$$\frac{\mathrm{d}\mathcal{G}(\boldsymbol{Y}_{,t},\boldsymbol{Y})}{\mathrm{d}\boldsymbol{Y}}\Delta\boldsymbol{Y} = -\mathcal{G}(\boldsymbol{Y}_{,t},\boldsymbol{Y})$$

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- · Krylov solvers form solution basis from $\operatorname{span}\left\{\left[\frac{\mathrm{d}\mathcal{G}(\boldsymbol{Y}_{\!,t},\boldsymbol{Y})}{\mathrm{d}\boldsymbol{Y}}\right]^n\Delta\boldsymbol{Y}\right\}_{n=0}$

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Bottom Line

Cost of $\frac{\mathrm{d}\mathcal{G}(Y_{,t},Y)}{\mathrm{d}Y}\Delta Y$ dominates implicit timestepping cost



Jacobian Matrix-Vector Multiply Options

How to compute $\frac{\mathrm{d}\mathcal{G}(\pmb{Y}_{\!,t},\pmb{Y})}{\mathrm{d}\pmb{Y}}\Delta\pmb{Y}$?

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- Store $\frac{\mathrm{d}\mathcal{G}}{\mathrm{d}\mathbf{Y}}$ directly (sparse matrix representation)
 - · Pros: Opens up preconditioning options
 - · Cons: Is large, expensive to store

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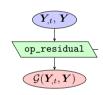
- Store $\frac{d\mathcal{G}}{d\mathbf{v}}$ directly (sparse matrix representation)
 - · Pros: Opens up preconditioning options
 - · Cons: Is large, expensive to store
- Finite difference matrix-free approximation:

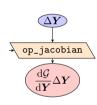
$$\frac{\mathrm{d}\mathcal{G}(\boldsymbol{Y}_{,t},\boldsymbol{Y})}{\mathrm{d}\boldsymbol{Y}}\Delta\boldsymbol{Y}\approx\frac{\mathcal{G}(\boldsymbol{Y}_{,t},\boldsymbol{Y}+\epsilon\Delta\boldsymbol{Y})-\mathcal{G}(\boldsymbol{Y}_{,t},\boldsymbol{Y})}{\epsilon}$$

- · Pros: Just need a residual evaluation, cheap (in programming and computation)
- Cons: Accuracy limited to $\sqrt{\epsilon_{\text{machine}}}$, preconditiong require partial assembly

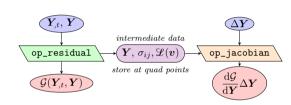
$$\frac{\mathrm{d}\mathcal{G}}{\mathrm{d}\boldsymbol{Y}}\Delta\boldsymbol{Y} = \frac{\mathrm{d}}{\mathrm{d}\boldsymbol{Y}} \left[\mathcal{P}^T \mathcal{E}^T B^T G B \mathcal{E} \mathcal{P} \right] \Delta \boldsymbol{Y}$$
$$= \left[\mathcal{P}^T \mathcal{E}^T B^T \frac{\mathrm{d}G}{\mathrm{d}\boldsymbol{Y}} B \mathcal{E} \mathcal{P} \right] \Delta \boldsymbol{Y}$$

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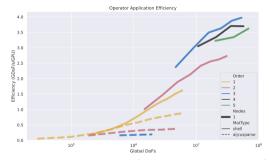
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$$\downarrow \text{op_residual} \qquad \downarrow \boldsymbol{Y}, \sigma_{ij}, \mathcal{L}(\boldsymbol{v}) \qquad \downarrow \text{op_jacobian} \\
\downarrow \boldsymbol{g}(\boldsymbol{Y}_{,t}, \boldsymbol{Y}) \qquad \qquad \downarrow \boldsymbol{g}(\boldsymbol{Y}_{,t}, \boldsymbol{Y}) \qquad \qquad \downarrow \boldsymbol{g}(\boldsymbol{Y}_{,t}, \boldsymbol{Y}) \qquad \downarrow \boldsymbol{g}(\boldsymbol{Y}_{,t}, \boldsymbol{Y}) \qquad \qquad \boldsymbol{g}(\boldsymbol{Y}_{,t}, \boldsymbol{Y}) \qquad \qquad \boldsymbol{g}(\boldsymbol{Y}_{,t}, \boldsymbol{Y}) \qquad \boldsymbol{g}(\boldsymbol{Y}_{,t},$$

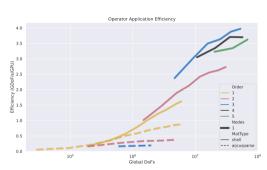
- Pros: Exact Jacobian matrix-vector product (potentially faster convergence)
- · Cons: Preconditioning requires partial assembly

Performance Exact Matrix-Free Jacobian via CeedOperator

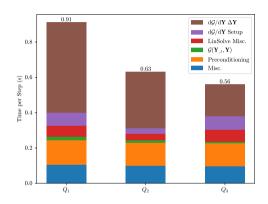


Matrix-Free Application Comparison (Reproduced from Brown et al. 2022). Not from fluids code, but representative of libCEED matrix-free

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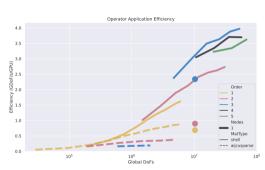


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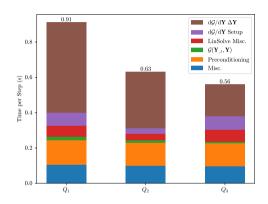


Fluids performance, DoFs fixed. Run on ALCE's Polaris on two nodes (8 x NVIDIA A100)

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Support and References

This work was supported by.... Add in sponsor support (ALCF, FastMATH DOE, ECP, etc)

