

Performance-Portable Implicit Scale-Resolving Compressible Flow Using libCEED

SIAM CSE 2023

James Wright

February 27, 2023

Ann and H.J. Smead Department of Aerospace Engineering Sciences



Smead Aerospace
UNIVERSITY OF COLORADO **BOULDER**

1. What is libCEED?
2. libCEED Overview
3. Fluid Simulations with libCEED
4. Accuracy and Performance of High-Order Scale-Resolving Simulations



What is libCEED?



What is libCEED?

- C library for element-based discretizations



What is libCEED?

- C library for element-based discretizations
 - Bindings for Fortran, Rust, Python, and Julia available



What is libCEED?

- C library for element-based discretizations
 - Bindings for Fortran, Rust, Python, and Julia available
- Designed for matrix-free operator evaluation



What is libCEED?

- C library for element-based discretizations
 - Bindings for Fortran, Rust, Python, and Julia available
- Designed for matrix-free operator evaluation
- Portable to different hardware via computational backends



What is libCEED?

- C library for element-based discretizations
 - Bindings for Fortran, Rust, Python, and Julia available
- Designed for matrix-free operator evaluation
- Portable to different hardware via computational backends
 - Code that runs on CPU also runs on GPU without changes



What is libCEED?

- C library for element-based discretizations
 - Bindings for Fortran, Rust, Python, and Julia available
- Designed for matrix-free operator evaluation
- Portable to different hardware via computational backends
 - Code that runs on CPU also runs on GPU without changes
 - Computational backend selectable at runtime, using runtime compilation



What is libCEED?

- C library for element-based discretizations
 - Bindings for Fortran, Rust, Python, and Julia available
- Designed for matrix-free operator evaluation
- Portable to different hardware via computational backends
 - Code that runs on CPU also runs on GPU without changes
 - Computational backend selectable at runtime, using runtime compilation
- Geared toward high-order element discretizations



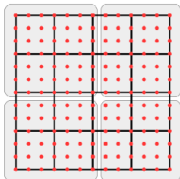
libCEED Overview



Finite Element Operator Decomposition

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$

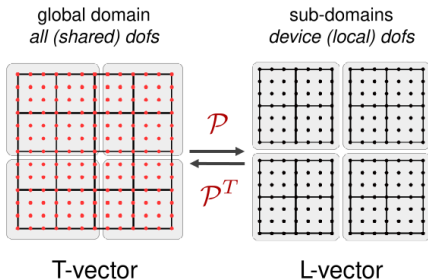
global domain
all (shared) dofs



T-vector

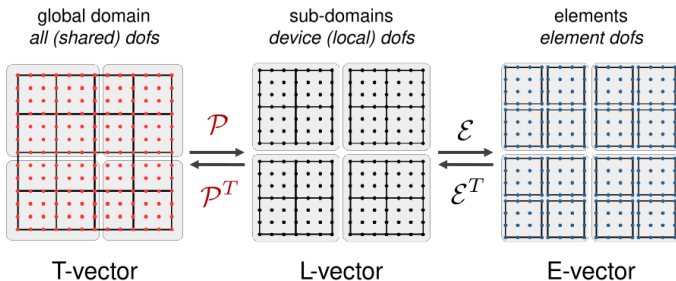
Finite Element Operator Decomposition

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$



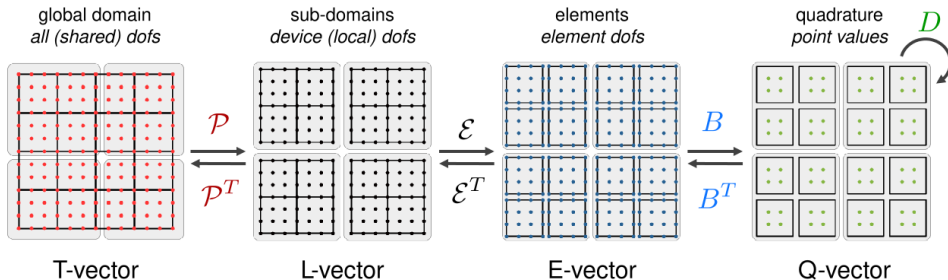
Finite Element Operator Decomposition

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$



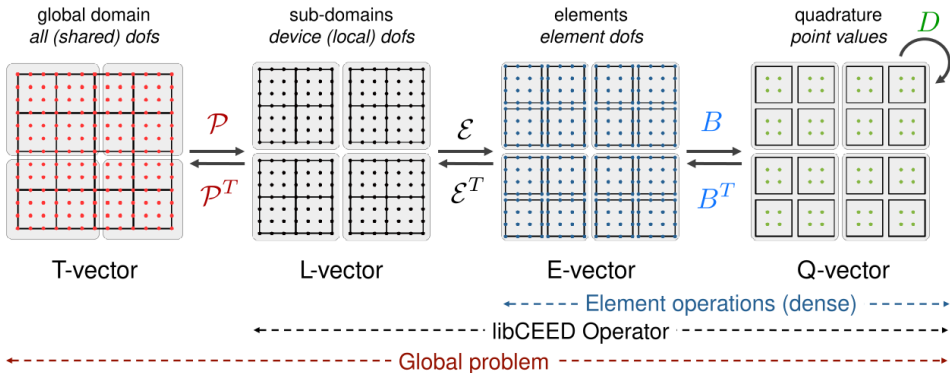
Finite Element Operator Decomposition

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$



Finite Element Operator Decomposition

$$A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$$



Fluid Simulations with libCEED



$$\mathbf{U}_{,t} + \mathbf{F}_{i,i}(\mathbf{U}) - S(\mathbf{U}) = 0$$

for

$$\mathbf{U} = \begin{bmatrix} \rho \\ \rho u_i \\ E \equiv \rho e \end{bmatrix}, \quad \mathbf{F}_i(\mathbf{U}) = \underbrace{\begin{pmatrix} \rho u_i \\ \rho u_i u_j + p \delta_{ij} \\ (\rho e + p) u_i \end{pmatrix}}_{\mathbf{F}_i^{\text{adv}}} + \underbrace{\begin{pmatrix} 0 \\ -\sigma_{ij} \\ -\rho u_i \sigma_{ij} - k T_{,i} \end{pmatrix}}_{\mathbf{F}_i^{\text{diff}}}, \quad S(\mathbf{U}) = - \begin{pmatrix} 0 \\ \rho \mathbf{g} \\ 0 \end{pmatrix}$$

convert to primitive variable formulation

Compressible Navier-Stokes for FEM

Find $\mathbf{U} \in \mathcal{S}^h$

$$\begin{aligned} \int_{\Omega} \mathbf{v} \cdot (\mathbf{U}_{,t} - \mathbf{S}(\mathbf{U})) \, d\Omega - \int_{\Omega} \mathbf{v}_{,i} \cdot \mathbf{F}_i(\mathbf{U}) \, d\Omega \\ + \int_{\partial\Omega} \mathbf{v} \cdot \mathbf{F}_i(\mathbf{U}) \cdot \hat{\mathbf{n}} \, d\partial\Omega \end{aligned}$$



Compressible Navier-Stokes for FEM

Find $\mathbf{U} \in \mathcal{S}^h$

$$\begin{aligned} \int_{\Omega} \mathbf{v} \cdot (\mathbf{U}_{,t} - \mathbf{S}(\mathbf{U})) \, d\Omega - \int_{\Omega} \mathbf{v}_{,i} \cdot \mathbf{F}_i(\mathbf{U}) \, d\Omega \\ + \int_{\partial\Omega} \mathbf{v} \cdot \mathbf{F}_i(\mathbf{U}) \cdot \hat{\mathbf{n}} \, d\partial\Omega \\ + \underbrace{\int_{\Omega} \mathcal{P}(\mathbf{v})^T (\mathbf{U}_{,t} + \mathbf{F}_{i,i}(\mathbf{U}) - \mathbf{S}(\mathbf{U})) \, d\Omega}_{\text{SUPG}} = 0, \quad \forall \mathbf{v} \in \mathcal{V}^h \end{aligned}$$



Compressible Navier-Stokes for FEM

Find $\mathbf{U} \in \mathcal{S}^h$

$$\begin{aligned} \int_{\Omega} \mathbf{v} \cdot (\mathbf{U}_{,t} - \mathbf{S}(\mathbf{U})) \, d\Omega - \int_{\Omega} \mathbf{v}_{,i} \cdot \mathbf{F}_i(\mathbf{U}) \, d\Omega \\ + \int_{\partial\Omega} \mathbf{v} \cdot \mathbf{F}_i(\mathbf{U}) \cdot \hat{\mathbf{n}} \, d\partial\Omega \\ + \underbrace{\int_{\Omega} \mathcal{P}(\mathbf{v})^T (\mathbf{U}_{,t} + \mathbf{F}_{i,i}(\mathbf{U}) - \mathbf{S}(\mathbf{U})) \, d\Omega}_{\text{SUPG}} = 0, \quad \forall \mathbf{v} \in \mathcal{V}^h \end{aligned}$$

Further simplified into residual form:

$$\mathcal{G}(\mathbf{U}_{,t}, \mathbf{U}) = 0$$



Compressible Navier-Stokes for FEM

Find $\mathbf{U} \in \mathcal{S}^h$

$$\begin{aligned} \int_{\Omega} \mathbf{v} \cdot (\mathbf{U}_{,t} - \mathbf{S}(\mathbf{U})) \, d\Omega - \int_{\Omega} \mathbf{v}_{,i} \cdot \mathbf{F}_i(\mathbf{U}) \, d\Omega \\ + \int_{\partial\Omega} \mathbf{v} \cdot \mathbf{F}_i(\mathbf{U}) \cdot \hat{\mathbf{n}} \, d\partial\Omega \\ + \underbrace{\int_{\Omega} \mathcal{P}(\mathbf{v})^T (\mathbf{U}_{,t} + \mathbf{F}_{i,i}(\mathbf{U}) - \mathbf{S}(\mathbf{U})) \, d\Omega}_{\text{SUPG}} = 0, \quad \forall \mathbf{v} \in \mathcal{V}^h \end{aligned}$$

Further simplified into residual form:

$$\begin{aligned} \mathcal{G}(\mathbf{U}_{,t}, \mathbf{U}) &= 0 \\ \Rightarrow \quad \mathcal{P}^T \mathcal{E}^T \mathbf{B}^T \mathbf{G} \mathbf{B} \mathcal{E} \mathcal{P} &= 0 \end{aligned}$$



Implicit Timestepping

Implicit timestepping requires solving:

$$\frac{d\mathcal{G}(U,t,U)}{dU} \Delta U = \mathcal{G}(U,t,U)$$



Implicit Timestepping

Implicit timestepping requires solving:

$$\frac{d\mathcal{G}(\mathbf{U}, t, \mathbf{U})}{d\mathbf{U}} \Delta \mathbf{U} = \mathcal{G}(\mathbf{U}, t, \mathbf{U})$$

- Store $\frac{d\mathcal{G}}{d\mathbf{U}}$ directly
 - Pros: Opens up preconditioning options
 - Cons: Is large, expensive to store



Implicit Timestepping

Implicit timestepping requires solving:

$$\frac{d\mathcal{G}(\mathbf{U}_t, \mathbf{U})}{d\mathbf{U}} \Delta \mathbf{U} = \mathcal{G}(\mathbf{U}_t, \mathbf{U})$$

- Store $\frac{d\mathcal{G}}{d\mathbf{U}}$ directly
 - Pros: Opens up preconditioning options
 - Cons: Is large, expensive to store
- Finite difference matrix-free approximation:

$$\frac{d\mathcal{G}(\mathbf{U}_t, \mathbf{U})}{d\mathbf{U}} \Delta \mathbf{U} \approx \frac{\mathcal{G}(\mathbf{U}_t, \mathbf{U} + \epsilon \Delta \mathbf{U}) - \mathcal{G}(\mathbf{U}_t, \mathbf{U})}{\epsilon}$$

- Pros: Just need a residual evaluation, cheap (in programming and computation)
- Cons: Approximation, accuracy limited to $\sqrt{\epsilon_{\text{machine}}}$



Exact Matrix-Free Jacobian

$$\frac{d\mathcal{G}}{d\mathbf{U}} \Delta\mathbf{U} = \frac{d}{d\mathbf{U}} [\mathcal{G}(\mathbf{U}, t, \mathbf{U})] \Delta\mathbf{U}$$



$$\begin{aligned}\frac{d\mathcal{G}}{d\mathbf{U}}\Delta\mathbf{U} &= \frac{d}{d\mathbf{U}} [\mathcal{G}(\mathbf{U}, t, \mathbf{U})] \Delta\mathbf{U} \\ &= \frac{d}{d\mathbf{U}} \left[\mathcal{P}^T \mathcal{E}^T \mathbf{B}^T \mathbf{G} \mathbf{B} \mathcal{E} \mathcal{P} \right] \Delta\mathbf{U}\end{aligned}$$

Exact Matrix-Free Jacobian

$$\begin{aligned}\frac{d\mathcal{G}}{d\mathbf{U}}\Delta\mathbf{U} &= \frac{d}{d\mathbf{U}} [\mathcal{G}(\mathbf{U},t,\mathbf{U})] \Delta\mathbf{U} \\ &= \frac{d}{d\mathbf{U}} \left[\mathcal{P}^T \mathcal{E}^T \mathbf{B}^T \mathbf{G} \mathbf{B} \mathcal{E} \mathcal{P} \right] \Delta\mathbf{U} \\ &= \left[\mathcal{P}^T \mathcal{E}^T \mathbf{B}^T \frac{d\mathbf{G}}{d\mathbf{U}} \mathbf{B} \mathcal{E} \mathcal{P} \right] \Delta\mathbf{U}\end{aligned}$$



$$\begin{aligned}\frac{d\mathcal{G}}{d\mathbf{U}}\Delta\mathbf{U} &= \frac{d}{d\mathbf{U}} [\mathcal{G}(\mathbf{U}_t, \mathbf{U})] \Delta\mathbf{U} \\ &= \frac{d}{d\mathbf{U}} \left[\mathcal{P}^T \mathcal{E}^T \mathbf{B}^T \mathbf{G} \mathbf{B} \mathcal{E} \mathcal{P} \right] \Delta\mathbf{U} \\ &= \left[\mathcal{P}^T \mathcal{E}^T \mathbf{B}^T \frac{d\mathbf{G}}{d\mathbf{U}} \mathbf{B} \mathcal{E} \mathcal{P} \right] \Delta\mathbf{U}\end{aligned}$$

- Store intermediary data at quadrature points to improve efficiency (“taping”)
 - We store \mathbf{U} , viscous stress, and stabilization perturbation ($\mathcal{P}(\mathbf{v})$)
- Pros: Exact Jacobian matrix-vector product (potentially faster convergence)
- Cons: More expensive than residual evaluation (but not by too much)



- PETSc used for handling everything libCEED doesn't
 - $\mathcal{P}, \mathcal{P}^T$ (Partition global-to-local operations)
 - Time integration, linear, non-linear equation solving
 - Strong boundary conditions



- PETSc used for handling everything libCEED doesn't
 - $\mathcal{P}, \mathcal{P}^T$ (Partition global-to-local operations)
 - Time integration, linear, non-linear equation solving
 - Strong boundary conditions
- PETSc calls a libCEED operator when it needs the residual evaluation



- PETSc used for handling everything libCEED doesn't
 - $\mathcal{P}, \mathcal{P}^T$ (Partition global-to-local operations)
 - Time integration, linear, non-linear equation solving
 - Strong boundary conditions
- PETSc calls a libCEED operator when it needs the residual evaluation
- libCEED Operator based on user-implemented **CeedQFunctions** (\mathcal{D})
 - Use different **CeedQFunctions** for volume vs boundary integrals
 - Combined into a single **CeedOperator** to represent $\mathcal{G}(\mathbf{U}_t, \mathbf{U})$



Time Step Loop

1. PETSc gets $\mathbf{U}^L = \mathcal{P}\mathbf{U}^G$ from current solution



Time Step Loop

1. PETSc gets $\mathbf{U}^L = \mathcal{P}\mathbf{U}^G$ from current solution
2. PETSc calls libCEED to get $\mathbf{G}^L = \underbrace{\boldsymbol{\varepsilon}^T \mathbf{B}^T \mathbf{D} \mathbf{B} \boldsymbol{\varepsilon}}_L \mathbf{U}^L$



Time Step Loop

1. PETSc gets $\mathbf{U}^L = \mathcal{P}\mathbf{U}^G$ from current solution
2. PETSc calls libCEED to get $\mathbf{G}^L = \underbrace{\boldsymbol{\varepsilon}^T \mathbf{B}^T \mathbf{D} \mathbf{B} \boldsymbol{\varepsilon}}_L \mathbf{U}^L$
3. PETSc gets $\mathbf{G}^G = \mathcal{P}^T \mathbf{G}^L$



Time Step Loop

1. PETSc gets $\mathbf{U}^L = \mathcal{P}\mathbf{U}^G$ from current solution
2. PETSc calls libCEED to get $\mathbf{G}^L = \underbrace{\boldsymbol{\varepsilon}^T \mathbf{B}^T \mathbf{D} \mathbf{B} \boldsymbol{\varepsilon}}_L \mathbf{U}^L$
3. PETSc gets $\mathbf{G}^G = \mathcal{P}^T \mathbf{G}^L$
4. PETSc uses \mathbf{G}^G to compute new solution value



Time Step Loop

1. PETSc gets $\mathbf{U}^L = \mathcal{P}\mathbf{U}^G$ from current solution
2. PETSc calls libCEED to get $\mathbf{G}^L = \underbrace{\boldsymbol{\varepsilon}^T \mathbf{B}^T \mathbf{D} \mathbf{B} \boldsymbol{\varepsilon}}_L \mathbf{U}^L$
3. PETSc gets $\mathbf{G}^G = \mathcal{P}^T \mathbf{G}^L$
4. PETSc uses \mathbf{G}^G to compute new solution value ...or whatever else it wants



Accuracy and Performance of High-Order Scale-Resolving Simulations



Flat Plate Boundary Layer, Zero Pressure Gradient

Problem Description:

- $Re_\theta \approx 970$ boundary layer at inflow, $M \approx 0.1$
- Synthetic turbulence generation (STG) used for inflow structures
- Internal damping layer (IDL) used in STG development region to prevent pressure wave growth
- **asdf**
- Domain size of $\{27 \times 24 \times 4\}\delta_0$



- Test 3 different order elements, Q_1, Q_2, Q_3 tensor-product hexes
- Maintain *DOF resolution* (DOFs per physical length)
- DOF resolution for streamwise and spanwise was $\Delta x^+ = 30$ and $\Delta z^+ = 12$
 - For Q_1 , this is about half the resolution required for DNS resolution



This work was supported by.... Add in sponsor support (DOE, ECP, etc)

