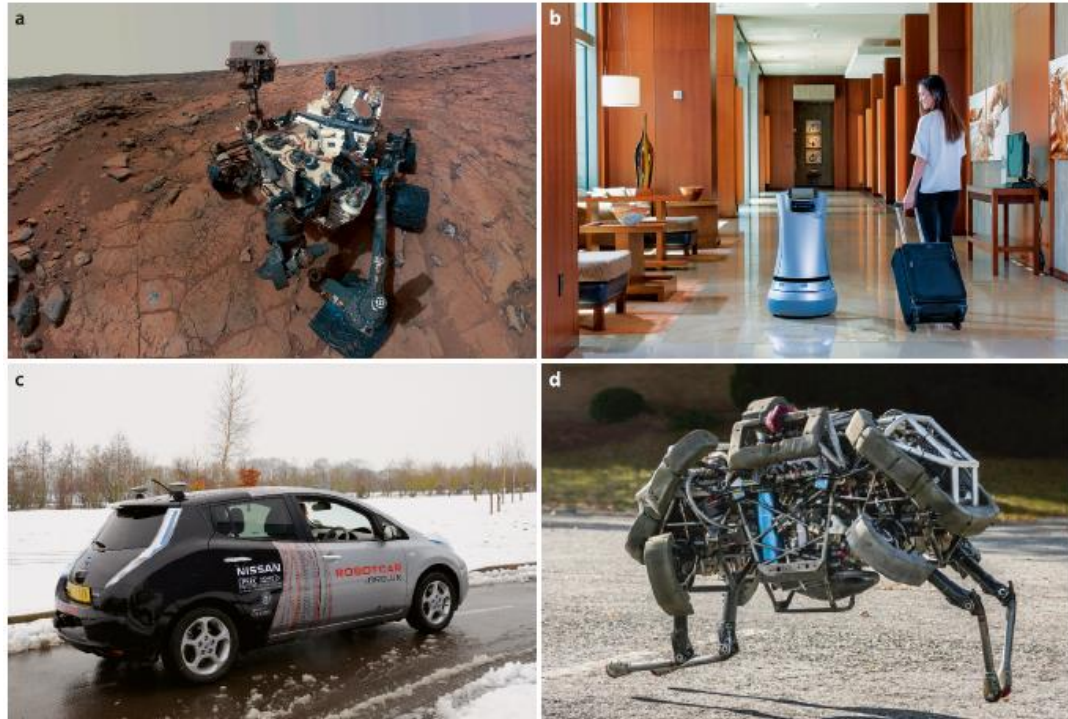


ME 397- ASBR

Week 4-Lecture 2



a Curiosity NASA/JPLCaltech; **b** Savioke Relay; **c** self driving car, Oxford Univ.;
d Cheetah legged robot, Boston Dynamics

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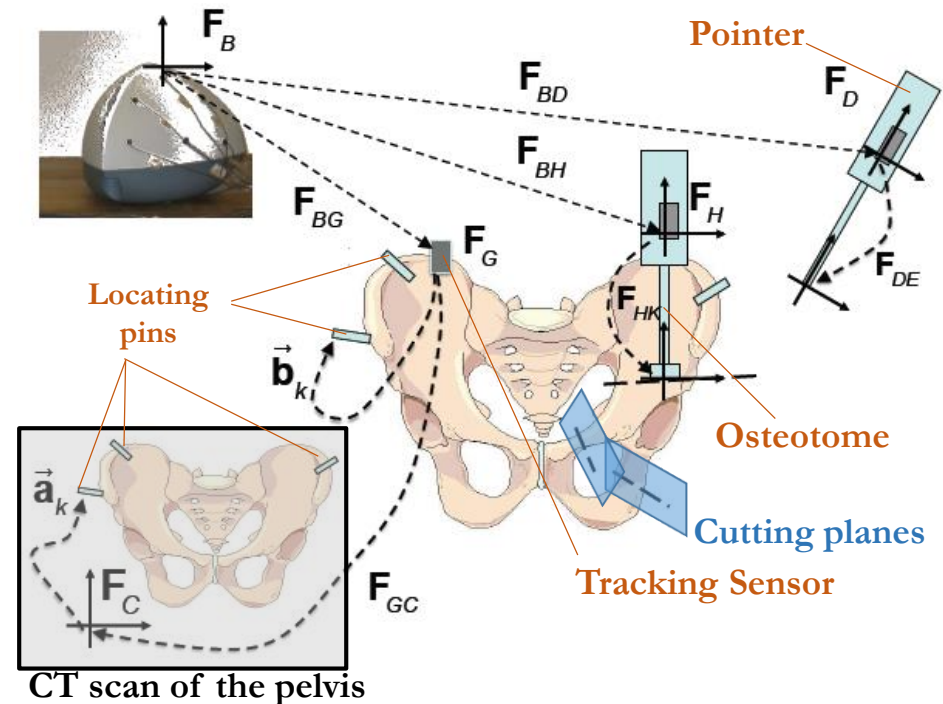
The University of Texas at Austin
Mechanical Engineering
Cockrell School of Engineering

Spring 2022

Example: Computer-Assisted Osteotomy

Consider the pelvic osteotomy situation illustrated in the figure. Here we assume that a **three locating pins** have been inserted into the patient's pelvis, and that a CT scan of the pelvis with the pins inserted has been produced. The patient has been placed onto the operating table.

- A magnetic navigation system (here, the Northern Digital Aurora) is present in the room.
- **Two surgical tools** are available:
 - ✓ A probe/pointer device
 - ✓ An osteotome (essentially a fancy chisel) that will be used to cut the pelvis.



<https://www.youtube.com/watch?v=N8rfMzU4siQ>

- 6 DOF Aurora tracking sensors have been attached to the **handle of each tool** and an additional 6 DOF sensor has been **affixed rigidly to the pelvis**. The Aurora is capable of determining the position and orientation of each sensor relative to the Aurora base unit.
- Let $\mathbf{p}_{tip} = \mathbf{p}_{GE}$ be the position of the tip of the pointer tool relative to the reference marker coordinate system \mathbf{F}_G .
- Give a formula for computing \mathbf{p}_{tip} , based on the available tracking system measurements

$$\mathbf{F}_{Bx} = (\mathbf{R}_{Bx} \mathbf{p}_{Bx})$$

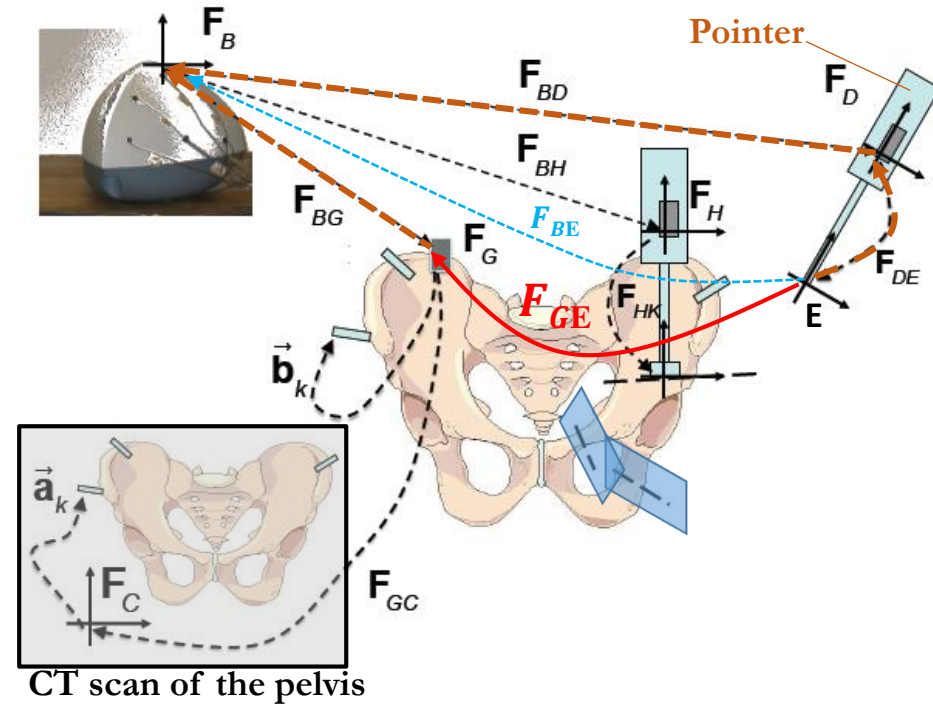
Example is from the Computer Integrated Surgery course, Russell H. Taylor, JHU

Example: Computer-Assisted Osteotomy

$$\begin{matrix} F_{BG} & F_{GE} \\ F_{BG} & F_{GE} \end{matrix} = \begin{matrix} F_{BD} & F_{DE} \\ F_{BD} & F_{DE} \end{matrix}$$

$$\Rightarrow F_{GE} = F_{BG}^{-1} F_{BD} F_{DE}$$

\mathbf{p}_{GE} is the last column of F_{GE}



Example is from the Computer Integrated Surgery course, Russell H. Taylor, JHU

Angular Velocities

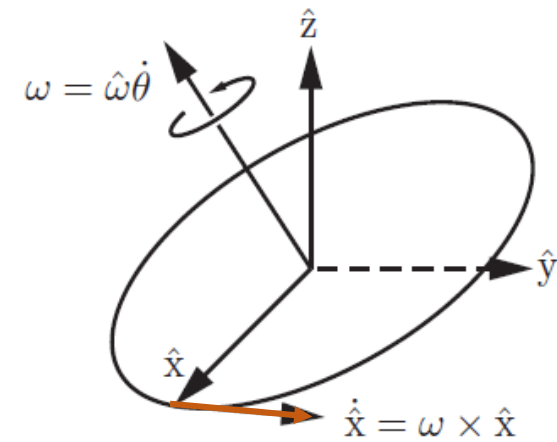
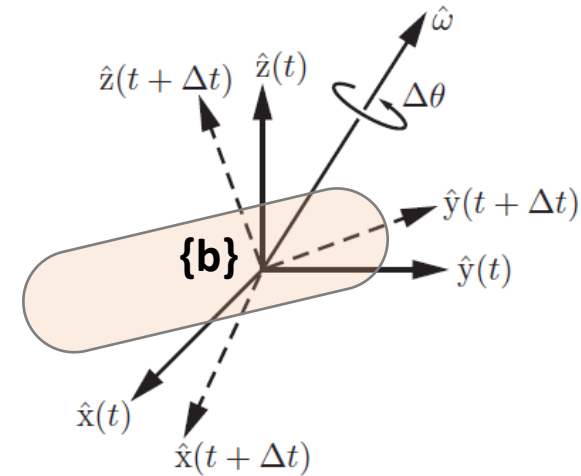
- Suppose that a **body frame** with **unit** axes $\{\hat{x}, \hat{y}, \hat{z}\}$ is attached to a **rotating body**.
- If we examine the body frame at times t and $t+\Delta t$, the **change in frame orientation** can be described as a rotation of angle $\Delta\theta$ about some unit axis $\hat{\omega}$ passing through the origin.
- The axis $\hat{\omega}$ is coordinate-free; it is not yet represented in any particular reference frame.
- As t approaches zero, the ratio $\Delta\theta/\Delta t$ becomes the **rate of rotation $\dot{\theta}$** , and $\hat{\omega}$ is the instantaneous axis of rotation. Hence, **angular velocity** \mathbf{w} is:

$$\mathbf{w} = \hat{\omega} \dot{\theta}.$$

- We can then calculate **linear velocities** as:

$$\begin{aligned}\dot{\hat{x}} &= \mathbf{w} \times \hat{x}, \\ \dot{\hat{y}} &= \mathbf{w} \times \hat{y}, \\ \dot{\hat{z}} &= \mathbf{w} \times \hat{z}.\end{aligned}$$

- To express these equations in coordinates, we have to choose a reference frame in which to represent \mathbf{w} typically the **fixed frame $\{s\}$ or the body frame $\{b\}$.**



Fixed-Frame Angular Velocities

- Let $R(t)$ be the rotation matrix describing the **orientation of the body frame with respect to the fixed frame $\{s\}$** at time t and $\dot{R}(t)$ is its time rate of change.

- Let $R(t) = [\hat{x}(t); \hat{y}(t); \hat{z}(t)]$ where \hat{r}_i is the representation of the corresponding **body frame axis** in the fixed frame $\{s\}$.

- At a specific time t , let $\omega_s \in \mathbb{R}^3$ be the angular velocity ω expressed in **fixed-frame** then we have:

$$\dot{r}_i = \omega_s \times r_i, \quad i = 1, 2, 3.$$

OR $\dot{R} = [\omega_s \times r_1 \quad \omega_s \times r_2 \quad \omega_s \times r_3]$

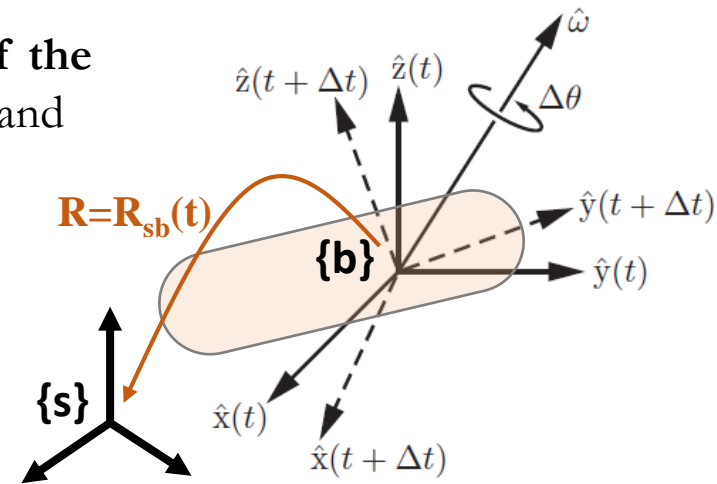
- We can rewrite $\omega_s \times r_i$ as $[\omega_s]R$, where $[\omega_s]$ is a 3×3 **skewsymmetric** matrix representation of $\omega_s \in \mathbb{R}^3$. Hence:

Skew-Symmetric angular **velocity of ω** represented in the **fixed frame**

$$[\omega_s]R = \dot{R}$$

$$[\omega_s] = \dot{R}R^{-1}$$

Time rate of change of the **orientation of the body frame with respect to the fixed frame $\{s\}$**



$$w = \hat{w}\dot{\theta}.$$

$$[x] = \begin{bmatrix} 0 & -x_3 & x_2 \\ x_3 & 0 & -x_1 \\ -x_2 & x_1 & 0 \end{bmatrix}$$

$$a \times b = (a)^\wedge b.$$

Body-Frame Angular Velocities

- Let ω_s and ω_b be two different **vector representations** of the same angular velocity w expressed in the **fixed and body-frame** coordinates, respectively. Hence: $\omega_s = R_{sb}\omega_b$.

➔
$$\omega_b = R_{sb}^{-1}\omega_s = R^{-1}\omega_s = R^T\omega_s$$

- Let us now use the **skew-symmetric operator** $[\cdot]$ to rewrite this equation in a matrix format:

$$R[\omega]R^T = [R\omega]$$

Given any $\omega \in \mathbb{R}^3$ and $R \in SO(3)$

$$[\omega_s] = \dot{R}R^{-1}$$

$$RR^T = R^T R = I.$$

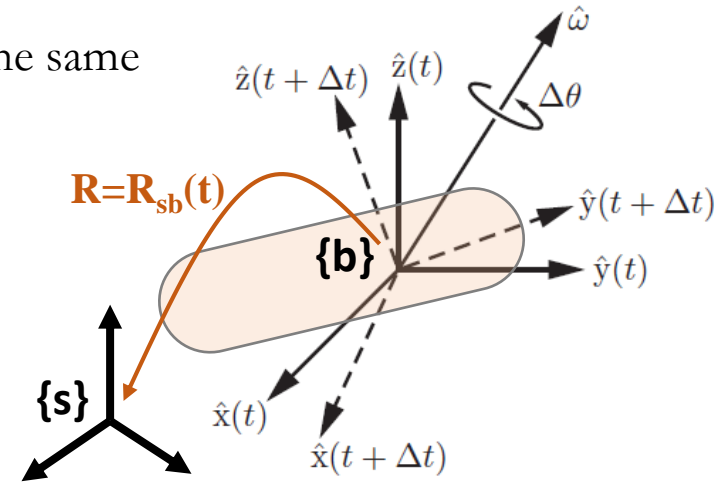
Skew-Symmetric angular velocity of ω represented in the **body frame**

$$\begin{aligned} [\omega_b] &= [R^T\omega_s] \\ &= R^T[\omega_s]R \end{aligned}$$

$$= R^T(\dot{R}R^T)R$$

$$[\omega_b] = R^T\dot{R} = R^{-1}\dot{R}.$$

Time rate of change of the **orientation of the body frame** with respect to the fixed frame $\{s\}$



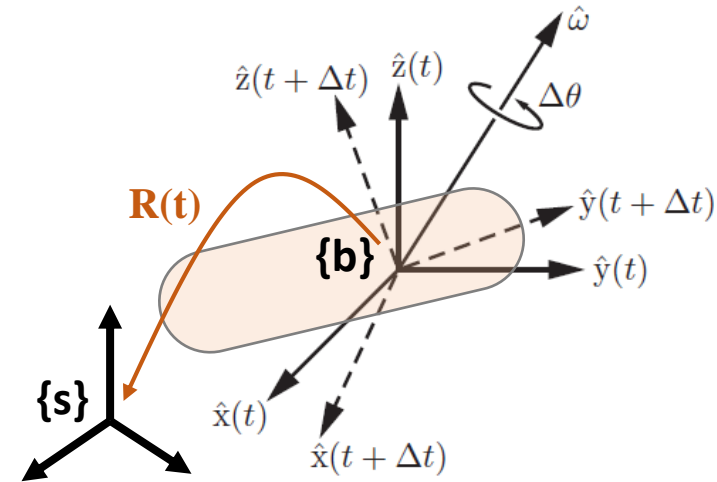
$$[\omega_s]R = \dot{R}.$$

$$[x] = \begin{bmatrix} 0 & -x_3 & x_2 \\ x_3 & 0 & -x_1 \\ -x_2 & x_1 & 0 \end{bmatrix}$$

Angular Velocities

- Let $R(t)$ denote the orientation of the rotating frame as seen from the fixed frame. Denote by \mathbf{w} the angular velocity of the rotating frame. Then

$$\begin{aligned}\dot{R}R^{-1} &= [\omega_s], \\ R^{-1}\dot{R} &= [\omega_b],\end{aligned}$$



where $\omega_s \in \mathbb{R}^3$ is the **fixed-frame vector** representation of \mathbf{w} and $[\omega_s] \in \mathfrak{so}(3)$ is its 3×3 matrix representation, and where $\omega_b \in \mathbb{R}^3$ is the **body-frame vector** representation of \mathbf{w} and $[\omega_b] \in \mathfrak{so}(3)$ is its 3×3 matrix representation.

- It is important to note that the **fixed-frame angular velocity** ω_s **does not depend** on the choice of body frame.
- **Similarly**, the body-frame angular velocity ω_b **does not depend on** the choice of fixed frame.
- An angular velocity expressed in an **arbitrary frame {d}** can be represented in another **frame {c}** if we know the rotation that takes {c} to {d}:

$$\omega_c = R_{cd}\omega_d.$$

Twists

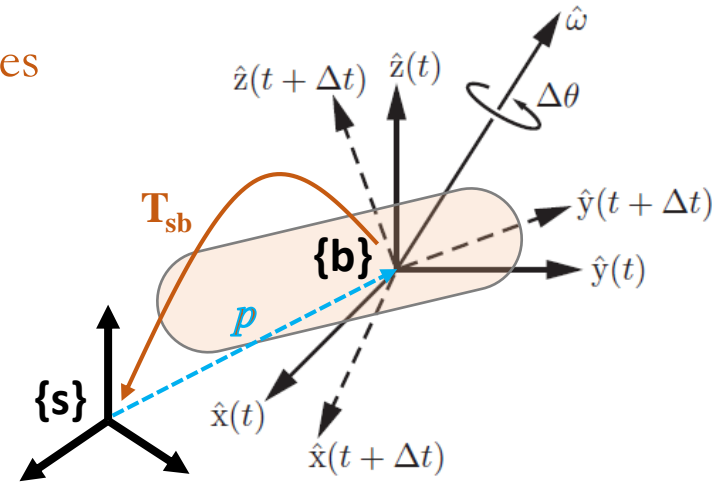
- We now consider **both the linear and angular velocities** of a moving frame. Let

$$T_{sb}(t) = T(t) = \begin{bmatrix} R(t) & p(t) \\ 0 & 1 \end{bmatrix}$$

- Let us pre-multiply \dot{T} by T^{-1} :

$$\begin{aligned} T^{-1} \dot{T} &= \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{R} & \dot{p} \\ 0 & 0 \end{bmatrix} \\ &= \begin{bmatrix} R^T \dot{R} & R^T \dot{p} \\ 0 & 0 \end{bmatrix} \\ &= \begin{bmatrix} [\omega_b] & v_b \\ 0 & 0 \end{bmatrix}. \end{aligned}$$

$v_b = R^T \dot{p}$ is the **linear velocity of the origin of {b}** expressed in {b}.



- $T^{-1} \dot{T}$ represents the **linear and angular velocities** of the moving frame relative to the stationary frame {b} currently aligned with the moving frame (i.e., **current body frame**).

Body Twist

- We define the **spatial velocity in the body frame**, or simply the **body twist** \mathcal{V}_b as:

$$\mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} \in \mathbb{R}^6$$

- As it is convenient to have a **skew-symmetric matrix** representation of an **angular velocity vector**, it is convenient to have a **matrix representation of a twist** as:

$$T^{-1}\dot{T} = [\mathcal{V}_b] = \begin{bmatrix} [\omega_b] & v_b \\ 0 & 0 \end{bmatrix} \in se(3). \quad [x] = \begin{bmatrix} 0 & -x_3 & x_2 \\ x_3 & 0 & -x_1 \\ -x_2 & x_1 & 0 \end{bmatrix}$$

where $[\omega] \in so(3)$ and $v_b \in \mathbb{R}^3$.

- The set of all **4×4 matrices** of **this form** is called **se(3)**.
- **se(3)** comprises the **matrix representations** of the twists associated with the rigid-body configurations **SE(3)**.

Spatial Twist

- let us now evaluate $\dot{T}T^{-1}$:

$$\begin{aligned}\dot{T}T^{-1} &= \begin{bmatrix} \dot{R} & \dot{p} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} \dot{R}R^T & \dot{p} - \dot{R}R^T p \\ 0 & 0 \end{bmatrix} \\ &= \begin{bmatrix} [\omega_s] & v_s \\ 0 & 0 \end{bmatrix}.\end{aligned}$$

$$\begin{aligned}\dot{R}R^{-1} &= [\omega_s] \\ R^{-1}\dot{R} &= [\omega_b]\end{aligned}$$

where $[\omega_s] \in \mathfrak{so}(3)$ and $v_s \in \mathbb{R}^3$.

- We can assemble ω_s and v_s into a **six-dimensional twist**:

$$\mathcal{V}_s = \begin{bmatrix} \omega_s \\ v_s \end{bmatrix} \in \mathbb{R}^6, \quad [\mathcal{V}_s] = \begin{bmatrix} [\omega_s] & v_s \\ 0 & 0 \end{bmatrix} = \dot{T}T^{-1} \in \mathfrak{se}(3)$$

- We call v_s the **spatial velocity in the space frame**, or simply the **spatial twist**.
- We can obtain v_b from v_s as follows:

$$\begin{aligned}[\mathcal{V}_b] &= T^{-1} \dot{T} \\ &= T^{-1} [\mathcal{V}_s] T.\end{aligned} \quad [\mathcal{V}_s] = T [\mathcal{V}_b] T^{-1}$$

Adjoint Representation

$$[\mathcal{V}_s] = T [\mathcal{V}_b] T^{-1} \Rightarrow [\mathcal{V}_s] = \begin{bmatrix} R[\omega_b]R^T & -R[\omega_b]R^T p + Rv_b \\ 0 & 0 \end{bmatrix}$$

$R[\omega]R^T = [R\omega]$
 $[\omega]p = -[p]\omega$ for $p, \omega \in \mathbb{R}^3$

$$\underbrace{\begin{bmatrix} \omega_s \\ v_s \end{bmatrix}}_{\mathcal{V}_s} = \underbrace{\begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix}}_{[\text{Ad}_T]} \underbrace{\begin{bmatrix} \omega_b \\ v_b \end{bmatrix}}_{\mathcal{V}_b}$$

Math tricks to factor out the ω_b

- Given $T = (R; p) \in \text{SE}(3)$, its **adjoint** representation $[\text{Ad}_T]$ is

$$[\text{Ad}_T] = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$

- For any $\mathcal{V} \in \mathbb{R}^6$, the adjoint map associated with T is

$$\mathcal{V}' = [\text{Ad}_T]\mathcal{V} \equiv \mathcal{V}' = \text{Ad}_T(\mathcal{V})$$

- In terms of the matrix form $[\mathcal{V}] \in \text{se}(3)$ of $\mathcal{V} \in \mathbb{R}^6$: $[\mathcal{V}'] = T[\mathcal{V}]T^{-1}$

Adjoint Properties

➤ Let $T_1, T_2 \in \text{SE}(3)$ and $\mathbf{v} = (\boldsymbol{\omega}; v)$ and $[\text{Ad}_T] = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \in \mathbb{R}^{6 \times 6}$ then,

$$\text{Ad}_{T_1}(\text{Ad}_{T_2}(\mathcal{V})) = \text{Ad}_{T_1 T_2}(\mathcal{V}) \quad \text{or} \quad [\text{Ad}_{T_1}][\text{Ad}_{T_2}]\mathcal{V} = [\text{Ad}_{T_1 T_2}]\mathcal{V}.$$

➤ Also, for any $T \in \text{SE}(3)$ the following holds:

$$[\text{Ad}_T]^{-1} = [\text{Ad}_{T^{-1}}]$$

Proof: Choosing $T_1 = \mathbf{T}^{-1}$ and $T_2 = \mathbf{T}$,

$$\text{Ad}_{T^{-1}}(\text{Ad}_T(\mathcal{V})) = \text{Ad}_{T^{-1}T}(\mathcal{V}) = \text{Ad}_I(\mathcal{V}) = \mathcal{V}.$$

$$[\text{Ad}_{T_1}][\text{Ad}_{T_2}]\mathcal{V} = [\text{Ad}_{T_1 T_2}]\mathcal{V}.$$

Summary of Twist Results

Given a fixed (space) frame $\{s\}$, a body frame $\{b\}$, and a differentiable $T_{sb}(t) \in SE(3)$

1. Matrix representation of the **body twist**

$$T_{sb}(t) = \begin{bmatrix} R(t) & p(t) \\ 0 & 1 \end{bmatrix}$$

$$T_{sb}^{-1} \dot{T}_{sb} = [\mathcal{V}_b] = \begin{bmatrix} [\omega_b] & v_b \\ 0 & 0 \end{bmatrix} \in se(3)$$

2. Matrix representation of the **spatial twist**

$$\dot{T}_{sb} T_{sb}^{-1} = [\mathcal{V}_s] = \begin{bmatrix} [\omega_s] & v_s \\ 0 & 0 \end{bmatrix} \in se(3)$$

3. The twists \mathcal{V}_s and \mathcal{V}_b are related by

$$\begin{aligned} \mathcal{V}_s &= \begin{bmatrix} \omega_s \\ v_s \end{bmatrix} = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} = [\text{Ad}_{T_{sb}}] \mathcal{V}_b, \\ \mathcal{V}_b &= \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} = \begin{bmatrix} R^T & 0 \\ -R^T[p] & R^T \end{bmatrix} \begin{bmatrix} \omega_s \\ v_s \end{bmatrix} = [\text{Ad}_{T_{bs}}] \mathcal{V}_s. \end{aligned}$$

4. For any two frames $\{c\}$ and $\{d\}$, a twist represented as \mathcal{V}_c in $\{c\}$ is related to its representation \mathcal{V}_d in $\{d\}$ by:

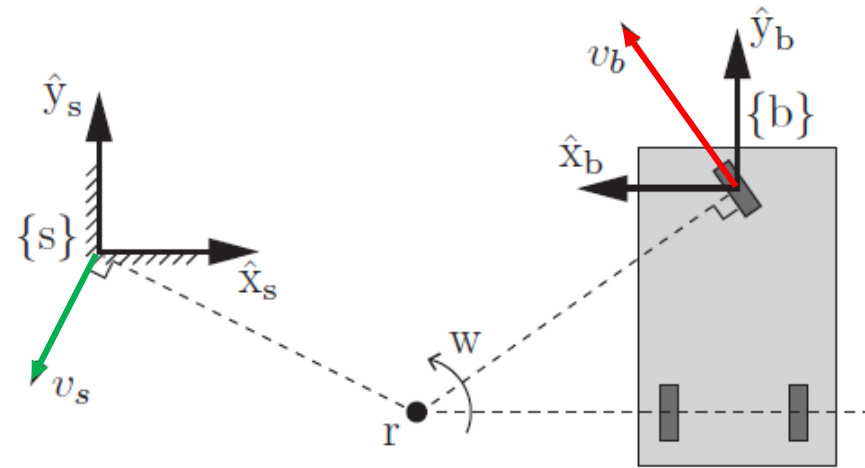
$$\mathcal{V}_c = [\text{Ad}_{T_{cd}}] \mathcal{V}_d, \quad \mathcal{V}_d = [\text{Ad}_{T_{dc}}] \mathcal{V}_c$$

Example

Figure shows a top view of a car, with a single steerable front wheel, driving on a plane. The $\hat{\mathbf{z}}_b$ -axis of the body frame $\{b\}$ is **into the page** and the $\hat{\mathbf{z}}_s$ -axis of the fixed frame $\{s\}$ is **out of the page**.

- The angle of the front wheel of the car causes the car's motion to be a **pure angular velocity $w = 2 \text{ rad/s}$** about an axis out of the page at the **point \mathbf{r}** in the plane.

If $\mathbf{r}_s = (2; -1; 0)$ or $\mathbf{r}_b = (2; -1.4; 0)$, **calculate twists \mathbf{v}_s and \mathbf{v}_b** and verify them using **corresponding adjoints**.



Example

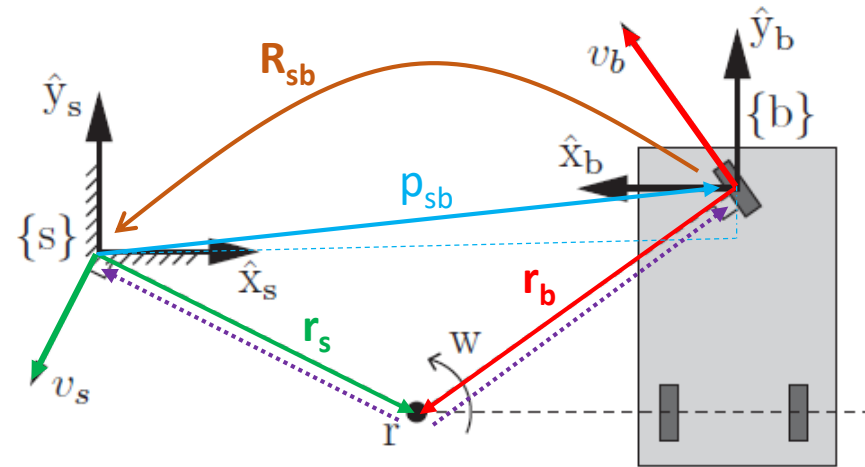
$$\mathbf{r}_s = (2; -1; 0)$$

$$\mathbf{r}_b = (2; -1.4; 0)$$

$$\boldsymbol{\omega}_s = (0; 0; 2)$$

$$\boldsymbol{\omega}_b = (0; 0; -2)$$

$$T_{sb} = \begin{bmatrix} R_{sb} & p_{sb} \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \hat{x}_b & \hat{y}_b & \hat{z}_b & \\ -1 & 0 & 0 & 4 \\ 0 & 1 & 0 & 0.4 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



From the figure we get:

$$\mathbf{v}_s = \boldsymbol{\omega}_s \times (-\mathbf{r}_s) = \mathbf{r}_s \times \boldsymbol{\omega}_s = (-2, -4, 0),$$

$$\mathbf{v}_b = \boldsymbol{\omega}_b \times (-\mathbf{r}_b) = \mathbf{r}_b \times \boldsymbol{\omega}_b = (2.8, 4, 0),$$

$$\mathcal{V}_s = \begin{bmatrix} \boldsymbol{\omega}_s \\ \mathbf{v}_s \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 2 \\ -2 \\ -4 \\ 0 \end{bmatrix}, \quad \mathcal{V}_b = \begin{bmatrix} \boldsymbol{\omega}_b \\ \mathbf{v}_b \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ -2 \\ 2.8 \\ 4 \\ 0 \end{bmatrix}$$

$$\mathcal{V}_s = \begin{bmatrix} \boldsymbol{\omega}_s \\ \mathbf{v}_s \end{bmatrix} = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \begin{bmatrix} \boldsymbol{\omega}_b \\ \mathbf{v}_b \end{bmatrix} = [\text{Ad}_{T_{sb}}] \mathcal{V}_b$$

$$[x] = \begin{bmatrix} 0 & -x_3 & x_2 \\ x_3 & 0 & -x_1 \\ -x_2 & x_1 & 0 \end{bmatrix}$$

$[p]$ is the **skew-symmetric matrix** representation of **vector** p_{sb}

References

- Murray, R.M., Li, Z., Sastry, S.S., “*A Mathematical Introduction to Robotic Manipulation.*”, **Chapter 2.**
- Corke, Peter. “Robotics, vision and control: fundamental algorithms in MATLAB®” second, completely revised. Vol. 118. Springer, 2017, **Chapter 2.**
- Lynch and Park, “*Modern Robotics,*” Cambridge U. Press, 2017, **Chapter 3.**