

Toward Wi-Fi Halow Signal Coverage Modeling in Collapsed Structures

Muhammad Faizan Khan^{ID}, Guojun Wang^{ID}, Member, IEEE, Md Zakirul Alam Bhuiyan^{ID}, Senior Member, IEEE, and Kun Yang^{ID}

Abstract—With the emerging concept of Wi-Fi radio as sensors, we are witnessing more device-free sensing applications. But we observe that most of the existing works of these applications are meant for simple indoor layout and are not adequate for complex cases, e.g., collapsed structures. In this article, we explore the feasibility of Wi-Fi Halow signals for the collapsed scenario as it can boost rescue efforts. To achieve this, we aim at two prime objectives of this article. First, we model debris constituent of common collapsed scenario materials, such as concrete, brick, glass, and lumber by conducting a field survey of an earthquake-affected area. After that, we consider signal propagation models for better coverage in this debris model by employing two methods. The first method is an integrated TOPSIS and Shannon entropy-based on a bijective soft set, which provides us an approximation tool to select the best Wi-Fi Halow signal coverage in debris. The second method composes two modified wireless signal propagation models, which are transmitter-receiver (TR) and Wi-Fi radar, respectively. We perform extensive simulations and figure out that low power transmission using Wi-Fi radar can yield better coverage, which is also verified by the Shannon entropy method.

Index Terms—Collapsed structure, coverage, IoT, path loss, rescue, soft set, Wi-Fi Halow.

I. INTRODUCTION

WITH the realization of leveraging Wi-Fi radio as sensors, the research community is paying more attention to device-free sensing applications [1], as these are being considered the future of IoT, where widget free sensing will be more imminent. But, there are certain areas such as human rescue from collapsed structures, where wireless signal penetration is very weak. So, there is dire need to investigate low-powered wireless signals that may also provide sensing

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Muhammad Faizan Khan and Guojun Wang are with the School of Computer Science, Guangzhou University, Guangzhou 510006, China (e-mail: csgjwang@gzhu.edu.cn).

Md Zakirul Alam Bhuiyan is with the Department of Computer and Information Sciences, Fordham University, New York, NY 10458 USA, and also with the School of Computer Science, Guangzhou University, Guangzhou 510006, China.

Kun Yang is with the School of Computer Science and Electronic Engineering, University of Essex, Colchester CO4 3SQ, U.K.

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for possible human detection under debris. This is entirely in line with the concept of IoT deployment by paving the way for ubiquitous disaster management. In this article, we consider Wi-Fi Halow, which is a low-powered Wi-Fi standard primarily designed for IoTs to address the weak signal coverage issue in collapsed structures.

A. Prior Work

Wireless signal coverage in the complex indoor layout has been extensively studied within the domain of indoor wireless communication. We observe through studies [2], [3] that attenuations, fading, higher path losses, scattering, etc., adversely affect the wireless signals in indoor environments. It becomes even worse for the case of a collapsed indoor structure, where roofs, walls, partitions, and doors turn into multilayered debris. So, wireless signal penetration through debris seems almost impossible. But, we do need to study the wireless signals for these collapsed structures as it may lead to the post-disaster rescue.

It has been observed that structural collapses are widespread everywhere in the world, which, unfortunately, results in the loss of precious human lives. Although there are some techniques available in the literature to boost the rescue efforts which have been manual by large till today. These solutions are based on cameras [4], [5], robots [6], sensors [7], and radars [8]. We have an observation that the most promising one is the radar-based technique among all others, which recognizes the micro-signatures [9] and phase change from echo at low frequency [10], [11]. But these techniques are by large susceptible to noises and also very much expensive, which limits their applications as most of the developing nations cannot utilize these methods, where major collapses occur due to poor infrastructure and low engineering standards. So, there is a dire need to find an alternative solution that should be both ubiquitous and cost effective.

Recently, Wi-Fi radios are being leveraged as sensors for various indoor IoT applications. These signals have sensing capability because of channel state information (CSI) [12] that encompasses this information of the desired event from the surroundings within the channel. Some of the most prominent Wi-Fi signal applications are: WiGest [13], CSI-based indoor localization [14], WiFi-ID [15], WiHear [16], Mo-sleep [17], breathing detection [18], WiKey [19], WiDraw [20], RT-Fall [21], security [12], [22], and privacy [23], [24] to name a few. We envision that Wi-Fi signals used as sensing modality

can lead to a ubiquitous and cost-effective rescue solution as it can benefit from breathing detection and localization research. However, the main challenge in this area is the weak signal strength having a low CSI, which can be used for extracting any valuable information. In some cases, there is no coverage of Wi-Fi signals under debris due to the multilayered obstacle scenario that causes attenuations, fading, higher path losses, scattering, etc. Therefore, there is a dire need to investigate the Wi-Fi signal penetration and to increase the signal strength under debris because it may lead to a device-free post-disaster rescue, which will be quite cost effective and ubiquitous as well. Based on this motivation, we focus our research on the coverage aspect of low-frequency Wi-Fi signals that may open new dimensions in rescue solutions.

There are two fundamental challenges to Wi-Fi signals for adequate coverage in collapsed structures, which are path loss models and various Wi-Fi standards. We observe that most of the existing radar sensing techniques operate at low frequencies as high-frequency signals face more attenuations, improper reflections, fading, and scattering from debris. There are some research studies like [25] and [26] dealing with various frequencies ranging from 50 MHz to 2.4 GHz for complex structures, which convince us that low-frequency wireless signals can penetrate better in collapsed structures. But none of these works explicitly dealt with Wi-Fi radios as sensors. Similarly, path loss modeling has been widely studied, such as [2], [3], and [27]–[29], but unfortunately, these works do not analyze the path losses for the collapsed structure case. To the best of our knowledge, all the existing studies related to path loss models consider source and destination at two different locations, which limit coverage of wireless signals in debris as damping, attenuations, and fading come into effect. So, there is a dire need to study new methods for wireless path losses in collapsed structures. Recently, there is work by Khan *et al.* [30]–[33], where they tried to investigate the subject matter and suggested that Wi-Fi Halow [34], which is low power and low-frequency standard from Wi-Fi Alliance, is best suited for adequate coverage in collapsed structures in comparison with other Wi-Fi standards. The current study is an extension of ongoing research by having a more in-depth analysis of path losses with a proper comparison based on strong theoretical and conceptual methodology. We also have an observation that research on structural health monitoring like [35]–[37] can provide a breakthrough on coverage computation of wireless signals in complex environments.

The prime objective of this article is to study the in-depth feasibility of Wi-Fi Halow signals for debris scenarios as [31] states that low frequency is the optimal solution for coverage in collapsed structures. Low frequencies result in higher wavelength, which ensures better diffraction of the beam. It can also excite delocalized electrons in a metal that allows penetration of low-frequency signals better than higher ones. It is also evident from [34] that Wi-Fi Halow has been designed primarily for IoT. This concept perfectly justifies our idea of low power and the ubiquitous post-disaster rescue solution. Moreover, the purpose of this article is to exploit the sensing capability of Wi-Fi signals for possible breathing detection rather than data communication due to the complex nature of the debris. Therefore, we focus on the coverage aspect of

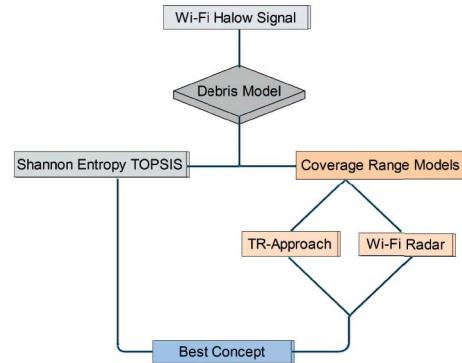


Fig. 1. Coverage concept.

Wi-Fi Halow signals, which may turn into a rescue solution soon in the future.

B. Contribution and Organization

The prime objective of this article is to study the Wi-Fi Halow signal coverage in a collapsed structure. We consider two main goals of this article to address coverage adequately. First, we need to develop a debris structural model which should be based on a real field survey to provide a sound basis. To achieve this, we conducted a field survey of an earthquake area of China that resulted in a loss of more than 68 000 people. We studied the causes of structural collapses, kind of structural materials and impact of the earthquake, and developed a layered debris model constituent of concrete, brick, glass, and lumber to map ruins into theoretical replicas. After that, we define the problem through echo modeling based on the Doppler radar principle. To address the coverage of Wi-Fi Halow from the echo and debris model, we consider two methodologies, as shown in Fig. 1, which are Shannon entropy TOPSIS based on bijective soft set [38] from the theoretical aspect and coverage range models from wireless signal propagation theory. Shannon entropy TOPSIS method provides a mathematical proof on conceptual understandings of wireless signals in collapsed structures, whereas coverage models properly employ two modified path loss methods for signal losses and attenuations. These methods are transmitter-receiver (TR) and Wi-Fi radar, respectively. The difference between both methods is the placement of the receiver, which in the TR-approach is at a separate place than the transmitter, whereas in the Wi-Fi radar technique, its same device. Finally, we compare the results from both radio models with the Shannon entropy TOPSIS method to figure out the best possible concept for adequate coverage of the Wi-Fi Halow signal in collapsed structures.

The major contributions of this article as follows.

- 1) We explore the feasibility of Wi-Fi Halow signals for adequate coverage in the complex indoor layout such as collapsed structures. There can be multiple causes of structural collapses, such as earthquakes, tsunamis, terrorism, etc. So, to address the nature of the debris, we conducted a field survey of an earthquake-affected area as soil mechanics, structural materials, environment, and area economics matters a lot.

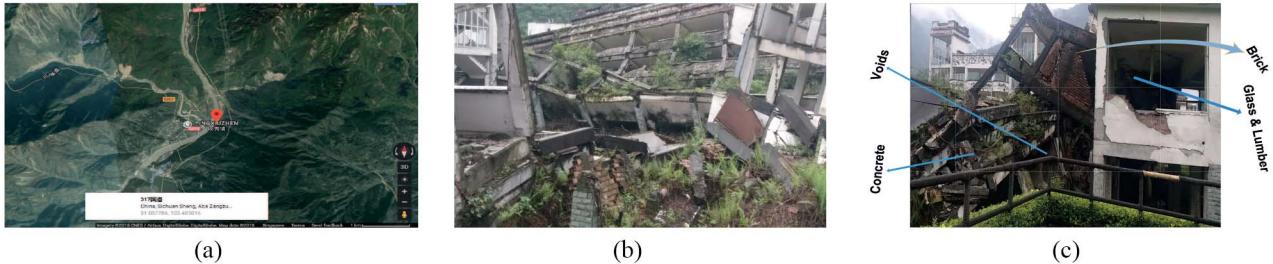


Fig. 2. Earthquake survey site: Yingxiu town, Wenchuan County, China. (a) Location of Yingxiu town. (b) Xuankou middle school. (c) Collapsed materials.

- 2) We define our coverage problem through Wi-Fi Halow signal and echo modeling based on the debris model developed from a real field survey. These models provide an in-depth investigation of structural materials and signal propagation mechanism. We envision that wireless signals will be reflected after striking with objects quite similar to the Doppler radar method.
- 3) We formulate two methodologies to address the Wi-Fi Halow signal coverage from debris and echo models. First, we present Shannon entropy TOPSIS based on a bijective soft set technique to visualize the wireless signal propagation in debris conceptually. It is based on the selection of proper attributes to provide better coverage using preferential values from radio specialists. After that, we present two coverage range methods, which are TR and Wi-Fi radar, respectively. These both methods have been modified from existing path loss techniques and radar range equation to address the coverage in collapsed structures.
- 4) Finally, we validate our signal propagation models through proper simulations while considering signal intensities, threshold, modulation schemes, debris layers, and Wi-Fi Halow frequency for two countries, i.e., China and USA. Furthermore, we compare these results with conceptual results obtained from the Shannon entropy TOPSIS method. We conclude that Wi-Fi Halow signals with low power and the low frequency with a smaller modulation scheme at minimum layered debris yield better coverage results. This inference completely justifies the basic concept of Wi-Fi Halow, which was primarily designed for IoTs, and our results also suggest that low power Wi-Fi Halow signals can probably provide us better coverage. So, we envision to expect IoT-based post-disaster rescue solutions around the world in the future.

The remainder of this article is organized as follows. We discuss problem formulation in Section II. We present two methodologies, i.e., Shannon entropy TOPSIS and coverage range methods in Sections III and IV. The simulations results have been provided in Section V. After that, we briefly analyze both methods in Section VI along with contributions and limitations in comparison with the existing literature. Finally, Section VII concludes this article with future directions.

II. PROBLEM FORMULATION

This section provides the foundation of our study. First, we provide a brief analysis of the nature of the collapsed

structure through a field survey of an earthquake affected area of southwestern China. Then, we investigate the core reasons along with a study of structural materials. Furthermore, we transform the field survey into a debris model and discuss Wi-Fi Halow signal behavior in this multiobstructed scenario. Finally, we come up with the echo model, which provides a proper problem formulation.

A. Collapsed Structure Measurement

The first goal of this article is to find a possible collapsed structure because it may lead to proper debris modeling that can further assist in coverage computation. We observed there are multiple causes of collapsed environments, such as earthquakes, tsunamis, terrorist activities, fire incidents, or structural failures. But in this research, we have considered an earthquake as a leading source of structural collapse as the majority of the active fault lines exist mostly in developing countries, where construction standards are not followed adequately due to the weak economy. To cope with this, we conducted a field survey of an earthquake hit area of Sichuan, which is the southwestern province of China. The main reason to select this site was the construction standards as rural areas did not fully comply with building codes, whereas urban areas have been planned according to standards.

The epic center of the earthquake was Yingxiu,¹ a small town in southern Wenchuan county within Sichuan province. It is located at latitude and longitude of $31^{\circ}03'32''N$ and $103^{\circ}29'41''E$ respectively, as shown in Fig. 2(a). Most of the adjoining rural areas of Wenchuan were destroyed by a devastating earthquake that hit China with a moment magnitude of 7.9 on May 12, 2008.² Government sources put the casualties' number to more than 68 000. We conducted an in-depth investigation from the ruins of Xuankou middle school, as shown in Fig. 2(b) located in the town of Yingxiu. We observed that structural collapse was caused by poor building construction with concrete, brick, glass, and lumber, as shown in Fig. 2(c). This collapse also caused voids, where there was a possibility of humans. Therefore, a proper study containing reasons for structural failure can lead to better rescue. Our analysis showed that the columns were not reliable, and also the steel binding in the core basement did not meet construction codes. Even the beam was not up to the mark and collapsed with the first shock. In short, construction materials with poor standards were the primary source of collapse. So, in this article, we

¹<https://en.wikipedia.org/wiki/Yingxiu>

²<https://earthquake.usgs.gov/earthquakes/eventpage/usg000g650#executive>

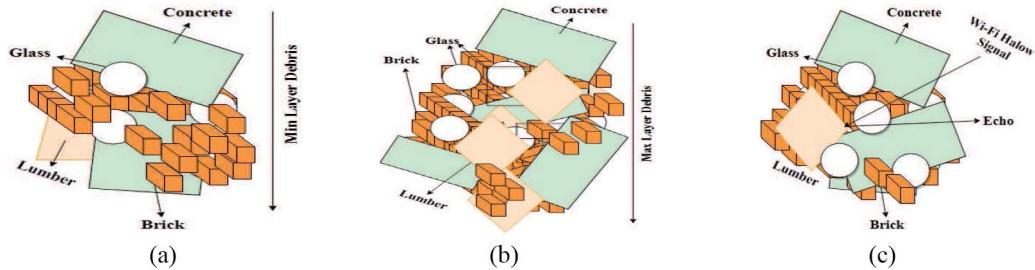


Fig. 3. Earthquake survey site with echo and layered models. (a) Minimum layers. (b) Maximum layers. (c) Wi-Fi Halow echo.

focus our research on Wi-Fi Halow signal penetration through these construction materials that are commonly used in all developing countries.

B. Debris Model

Let us map our field survey from Fig. 2(c) to theory through a debris model. It is a fact that the selection of adequate debris is pivotal for coverage computation in collapsed structures. This is evident from the debris that structures after collapse turn up into multiple objects laying over each other. Furthermore, there can be various materials in this debris as well, but we have only considered brick, concrete, glass, and lumber to address both structural complexities and to simplify the problem as shown in Fig. 2(c).

Let us dive into further depth of this debris model. The geometry of debris is also a significant factor that classifies it into horizontal and vertical directions. We consider it as layered debris where multiple objects laying over each other defines the depth and width of debris. The extent of debris is considered through vertical layers, and our layered model primarily focuses on this. We further classify these vertical layers into minimum and maximum layered model, as seen in Fig. 3(a) and (b). The reason for this classification is to figure out the maximum possible coverage of the Wi-Fi Halow signal. It is quite evident that the signal will damp after penetration through various materials, but we need to find the maximum depth that can provide us some coverage.

C. Wi-Fi Halow Echo Model

Let us consider the Wi-Fi Halow signal behavior in the above-developed debris model, as shown in Fig. 2(c). Collapsed structures are far complex than typical indoor scenarios primarily because of the multilayered debris formed from halls, walls, doors, etc. So, it becomes very much difficult for the wireless signal to penetrate and reflect from debris. Most of the time, there is a chance of signal damping because of various fading phenomena. But, there is still a need for in-depth investigation for Wi-Fi signals as it may turn into a post-disaster rescue solution.

To simplify the coverage computation, we consider a Wi-Fi Halow echo model, as shown in Fig. 3(c). We assume that wireless signals follow the Doppler radar principle. There is a stream of wireless pulses penetrating debris, which will either be reflected or damped. Our goal is to get a proper echo, which may provide us suitable CSI. Although we may get

signal coverage with very low sensitivity, i.e., -100 dBm, those reflections will be very weak, and we cannot extract CSI from the received signal. So, there is a need for a strong echo signal. To achieve this, echo signals should be above the predefined threshold (PDT). We only consider signals from reflected from debris, while other signals are assumed to be noise.

In a nutshell, our main objective is to have better coverage for Wi-Fi Halow signal from collapsed structures as these face higher attenuation in debris. So, there is a need to formulate methods based on echo and debris models that may assist in comprehending and computing the Wi-Fi signals.

III. SHANNON ENTROPY TOPSIS

In this section, we employ a conceptual model using Shannon entropy TOPSIS based on a bijective soft set to select the best Wi-Fi signal attributes for coverage in collapsed structures. But, before going into the detail of the conceptual model, we first discuss the motivation behind employing this technique from operational research to computer science. After that, we provide some preliminary definitions followed by the method and its operation to the debris model.

We know that decision making from multicriteria attributes is one the biggest challenge in operational research, and researchers have been proposing new methods to have effective decisions. A significant contribution was soft sets, which were introduced by Molodtsov [39], and followed by a study [40], that proposed a bijective soft set. Furthermore, [41] extended soft sets to intuitionistic fuzzy soft sets. These studies suggest that soft sets are handy for decision making and to deal with uncertainties. Now, our problem also needs some conceptual level decision making before specifically proposing wireless propagation models, because Wi-Fi signal penetration in collapsed structures is entirely uncertain. We cannot randomly decide some wireless propagation methods. There is a need to consult the literature and radio specialists to realize the afore-discussed field survey in the context of Wi-Fi Halow signals. Therefore, we need to conceptually analyze the problem and make trustworthy decisions that may help us to employ path loss models effectively. Motivated by study [38], [42], which is based on Shannon entropy weights, we apply this approach for Wi-Fi Halow signals as it covers both wireless aspect and theoretical bijective soft set as shown in Fig. 4.

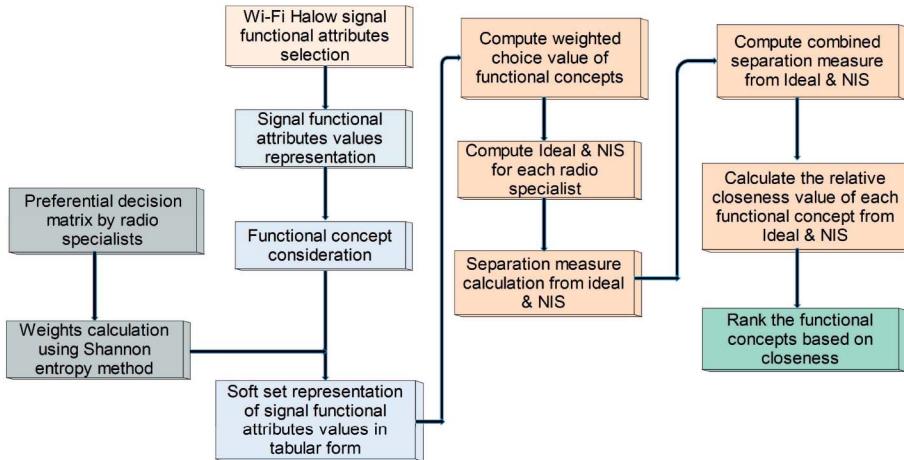


Fig. 4. Proposed functional concept methodology.

A. Preliminary Definitions

Let us consider the fundamental operation and definition of soft sets as it would make subsequent sections more understandable.

1) *Soft Set*: Suppose we have set of parameters and universal set as S and U , respectively. Let $P(U)$ be the power set of U , and X is a subset of S as $X \subset S$. Then, a pair (F, X) is known as a soft set over U , where mapping function F is given by $F : X \rightarrow P(U)$ [43].

2) *Bijective Soft Set*: Let (F, S) be a soft set over universal set U and S as a nonempty set of parameters. Then, (F, S) is known as bijective soft set [40] if the following conditions are met.

- 1) $\bigcup_{\beta \in S} F(\beta) = U$.
- 2) For any two parameters; $\beta_i, \beta_j, \beta_j \in S, \beta_i = \beta_j, F(\beta_i) \cap F(\beta_j) = \emptyset$.

B. Method

Input: Set of Wi-Fi Halow signal functional requirements.

Output: Best Wi-Fi Halow coverage concept.

- 1) Identify the Wi-Fi Halow signal functional attributes (SFAs) which matters the most for debris scenario. After that, assign possible conceptual values to these attributes by following the standard communication standards and represent it in a set form.
- 2) Generate functional concepts for the signal from attribute values that are most suited for coverage in collapsed structures and discard others. These concepts provide a theoretical understanding of Wi-Fi signal penetration in debris.
- 3) Represent attributes values in both soft set and bijective soft set form to proceed for decision making.
- 4) Capture the Wi-Fi Halow signal preferences for radio specialists on the abstract level and form the preferential decision matrix as $\mathcal{PDM} = [p_{ij}]_{a \times b}$, where $i = 1, \dots, a$ and $j = 1, \dots, b$; p_{ij} imply the preferences values. Here, “a” and “b” represent number of radio specialists and total signal attribute values, respectively.

- 5) Calculate the projection value (pv), entropy (\mathfrak{Ent}), divergence (\mathfrak{Div}), and weight (\mathfrak{Wgt}) of each signal attribute value γ_{ij} from [44] as

$$pv_{ij} = \frac{p_{ij}}{\sum_{i=1}^a p_{ij}}, \quad \mathfrak{Ent} = -\kappa \sum_{i=1}^a pv_{ij} \ln(pv_{ij})$$

where κ is a constant implied as, $\kappa = (\ln(a))^{-1}$, then

$$\mathfrak{Div} = 1 - (\mathfrak{Ent}), \quad \mathfrak{Wgt}(\gamma_{ij}) = \sum_{\kappa=1}^n \frac{\mathfrak{Div}_j}{\mathfrak{Div}_{\kappa}}.$$

- 6) Capture the requirements from radio specialists \mathcal{RSR} that may provide better coverage for Wi-Fi Halow signal.
- 7) Represent the Shannon entropy weights in soft set tabular form and compute weighted choice value WCV for each radio preference scheme through respective attributes and functional concepts as $WCV_{ik} = \sum_j \mathfrak{Div}_{ij}$, where $\mathfrak{Div}_{ij} = \mathfrak{Wgt}(\gamma_{ij}) \times q_{ij}$. Here, q_{ij} is obtained from signal functional concepts.
- 8) Determine ideal (IS) and nonideal solution (NIS) as γ_i^* and $\check{\gamma}_i$ for each radio specialist using TOPSIS as

$$\gamma_i^* = \text{Max}(WCV_{ik}); \quad \check{\gamma}_i = \text{Min}(WCV_{ik}).$$

- 9) Calculate the separation measure ($\Delta_{ik}^*, \Delta_{ik}^{\check{}}$) of each functional concept from the IS and NIS using n-dimensional Euclidean distance for each radio specialist by the following relation; $\Delta_{ik}^* = (\gamma_{ij} - \gamma_i^*)^2, \Delta_{ik}^{\check{}} = (\gamma_{ij} - \check{\gamma}_i)^2$. Then combined separation measure ($\Delta_k^*, \Delta_k^{\check{}}$) for each functional concept will be computed as

$$\Delta_k^* = \sqrt{\sum_{i=1}^{i=m} \Delta_{ik}^*}, \quad \Delta_k^{\check{}} = \sqrt{\sum_{i=1}^{i=m} \Delta_{ik}^{\check{}}}.$$

- 10) Determine the analogous closeness of each signal functional concept $\mathcal{F}\zeta_k$ to IS, which is provided as

$$\zeta_k^* = \frac{\Delta_k^{\check{}}}{\Delta_k^* + \Delta_k^{\check{}}}.$$

The most closer measure to the concept will be the best coverage of Wi-Fi Halow signals in the collapsed structures.

TABLE I
PREFERENTIAL DECISION MATRIX

	γ_{11}	γ_{12}	γ_{13}	γ_{21}	γ_{22}	γ_{23}	γ_{31}	γ_{32}	γ_{33}	γ_{41}	γ_{42}	γ_{43}	γ_{51}	γ_{52}
\mathcal{RS}_1	0.1	0.4	0.8	0.6	0.4	0.1	0.8	0.6	0.1	0.8	0.6	0.4	0.8	0.4
\mathcal{RS}_2	0.4	0.8	0.6	0.4	0.6	0.8	0.6	0.4	0.4	0.4	0.4	0.1	0.4	0.6
\mathcal{RS}_3	0.8	0.6	0.1	0.1	0.8	0.6	0.4	0.4	0.1	0.6	0.4	0.1	0.1	0.8

TABLE II
PROJECTION, ENTROPY, DIVERGENCE, WEIGHT

	γ_{11}	γ_{12}	γ_{13}	γ_{21}	γ_{22}	γ_{23}	γ_{31}	γ_{32}	γ_{33}	γ_{41}	γ_{42}	γ_{43}	γ_{51}	γ_{52}
\mathcal{PRS}_1	0.0769	0.2222	0.5333	0.5455	0.2222	0.0667	0.4444	0.4286	0.1667	0.4444	0.4286	0.6667	0.6154	0.2222
\mathcal{PRS}_2	0.3077	0.4444	0.4	0.3636	0.3333	0.5333	0.3333	0.2857	0.6667	0.2222	0.2857	0.1667	0.3077	0.3333
\mathcal{PRS}_3	0.6154	0.3333	0.0667	0.0909	0.4444	0.4	0.2222	0.2857	0.1667	0.3333	0.2857	0.1667	0.0769	0.4444
\mathfrak{Ent}	0.7817	0.9656	0.8031	0.8342	0.9656	0.8031	0.9656	0.9821	0.7897	0.9656	0.9821	0.7897	0.7817	0.9656
\mathfrak{Div}	0.2183	0.0344	0.1969	0.1658	0.0344	0.1969	0.0344	0.0179	0.2103	0.0344	0.0179	0.2103	0.2183	0.0344
\mathfrak{Wgt}	0.1344	0.0213	0.1212	0.1021	0.0213	0.1212	0.0213	0.0110	0.1295	0.0213	0.0110	0.1295	0.1344	0.0213

C. Operation

We can apply the Shannon entropy TOPSIS method based on bijective soft set to our Wi-Fi Halow coverage problem as follows.

- 1) Wi-Fi Halow coverage requirements can be defined by five SFAs to form a SFA set as per 1: $\mathcal{SFAs} = [\mathcal{SFA}_1, \mathcal{SFA}_2, \mathcal{SFA}_3, \mathcal{SFA}_4, \mathcal{SFA}_5]$, where these attributies represent the following. $\mathcal{SFA}_1 = \text{Power}$, $\mathcal{SFA}_2 = \text{MDS threshold}$, $\mathcal{SFA}_3 = \text{Coverage}$, $\mathcal{SFA}_4 = \text{Echo reception probability}$, $\mathcal{SFA}_5 = \text{Debris layers}$. Furthermore, there is a need to assign values to these SFAs according to standard regulatory bodies. We denote these values with γ as follows:

$$\begin{aligned}\mathcal{SFA}_1 &= \{\gamma_{11}, \gamma_{12}, \gamma_{13}\} = \{\text{High, Medium, Low}\} \\ \mathcal{SFA}_2 &= \{\gamma_{21}, \gamma_{22}, \gamma_{23}\} = \{\text{V. Good, Good, Poor}\} \\ \mathcal{SFA}_3 &= \{\gamma_{31}, \gamma_{32}, \gamma_{23}\} \\ &= \{\text{V. Good, Acceptable, Low}\} \\ \mathcal{SFA}_4 &= \{\gamma_{41}, \gamma_{42}, \gamma_{43}\} \\ &= \{\text{V. Good, Acceptable, Low}\} \\ \mathcal{SFA}_5 &= \{\gamma_{51}, \gamma_{52}\} = \{\text{Maximum, Minimum}\}.\end{aligned}$$

- 2) We generate five Wi-Fi Halow functional concepts as per 2) by forming an appropriate combination from SFAs which can be provided in a universal set given as

$$\bigcup = \mathcal{F}\zeta_1 + \mathcal{F}\zeta_2 + \mathcal{F}\zeta_3 + \mathcal{F}\zeta_4 + \mathcal{F}\zeta_5.$$

We present these functional concepts as sets below

$$\begin{aligned}\mathcal{F}\zeta_1 &= \{\gamma_{11}, \gamma_{21}, \gamma_{33}, \gamma_{43}, \gamma_{52}\} \\ \mathcal{F}\zeta_2 &= \{\gamma_{11}, \gamma_{23}, \gamma_{33}, \gamma_{43}, \gamma_{52}\} \\ \mathcal{F}\zeta_3 &= \{\gamma_{12}, \gamma_{22}, \gamma_{32}, \gamma_{43}, \gamma_{52}\} \\ \mathcal{F}\zeta_4 &= \{\gamma_{13}, \gamma_{21}, \gamma_{32}, \gamma_{42}, \gamma_{51}\} \\ \mathcal{F}\zeta_5 &= \{\gamma_{13}, \gamma_{21}, \gamma_{31}, \gamma_{41}, \gamma_{51}\}.\end{aligned}$$

- 3) Soft sets which may provide us an indirect representation of desired signal specification from $\mathcal{F}\zeta$ can be given as

follows:

$$\begin{aligned}\{\mathcal{SS}_1, \mathcal{SFA}_1\} &= \{\mathcal{SS}_1(\gamma_{11}), \mathcal{SS}_1(\gamma_{12}), \mathcal{SS}_1(\gamma_{13})\} \\ \{\mathcal{SS}_2, \mathcal{SFA}_2\} &= \{\mathcal{SS}_2(\gamma_{21}), \mathcal{SS}_2(\gamma_{22}), \mathcal{SS}_2(\gamma_{23})\} \\ \{\mathcal{SS}_3, \mathcal{SFA}_3\} &= \{\mathcal{SS}_3(\gamma_{31}), \mathcal{SS}_3(\gamma_{32}), \mathcal{SS}_3(\gamma_{33})\} \\ \{\mathcal{SS}_4, \mathcal{SFA}_4\} &= \{\mathcal{SS}_4(\gamma_{41}), \mathcal{SS}_4(\gamma_{42}), \mathcal{SS}_4(\gamma_{43})\} \\ \{\mathcal{SS}_5, \mathcal{SFA}_5\} &= \{\{\mathcal{SS}_5(\gamma_{51}), \mathcal{SS}_5(\gamma_{52})\}\}.\end{aligned}$$

Furthermore, bijective soft sets as per 3) can be given as

$$\begin{aligned}\mathcal{SS}_1(\gamma_{11}) &= \{\mathcal{F}\zeta_1, \mathcal{F}\zeta_2\}; \mathcal{SS}_1(\gamma_{12}) = \{\mathcal{F}\zeta_3\} \\ \mathcal{SS}_1(\gamma_{13}) &= \{\mathcal{F}\zeta_4, \mathcal{F}\zeta_5\}; \mathcal{SS}_2(\gamma_{21}) = \{\mathcal{F}\zeta_1, \mathcal{F}\zeta_4, \mathcal{F}\zeta_5\} \\ \mathcal{SS}_2(\gamma_{22}) &= \{\mathcal{F}\zeta_3\}; \mathcal{SS}_2(\gamma_{23}) = \{\mathcal{F}\zeta_2\} \\ \mathcal{SS}_3(\gamma_{31}) &= \{\mathcal{F}\zeta_5\}; \mathcal{SS}_3(\gamma_{32}) = \{\mathcal{F}\zeta_3, \mathcal{F}\zeta_4\} \\ \mathcal{SS}_3(\gamma_{33}) &= \{\mathcal{F}\zeta_1, \mathcal{F}\zeta_2\}; \mathcal{SS}_4(\gamma_{41}) = \{\mathcal{F}\zeta_5\} \\ \mathcal{SS}_4(\gamma_{42}) &= \{\mathcal{F}\zeta_4\}; \mathcal{SS}_4(\gamma_{43}) = \{\mathcal{F}\zeta_1, \mathcal{F}\zeta_2, \mathcal{F}\zeta_3\} \\ \mathcal{SS}_5(\gamma_{51}) &= \{\mathcal{F}\zeta_4, \mathcal{F}\zeta_5\}; \mathcal{SS}_5(\gamma_{52}) = \{\mathcal{F}\zeta_1, \mathcal{F}\zeta_3, \mathcal{F}\zeta_3\}.\end{aligned}$$

These relations satisfy the both conditions of bijective soft set. Let us consider $(\mathcal{SS}_1, \mathcal{SFA}_1)$ as an example, union of all the soft sets of $(\mathcal{SS}, \mathcal{SFA}_2)$ marks concept sources, which is universal set U or $\bigcup_{\gamma_{ij} \in \mathcal{SFA}_1} \mathcal{SS}(\gamma_{ij}) = U$. Furthermore, considering any of two SFA values, $\gamma_{11}, \gamma_{12} \in \mathcal{SFA}_1$, $\gamma_{11} \neq \gamma_{12}$, $\mathcal{SS}_1(\gamma_{11}) \cap \mathcal{SS}_1(\gamma_{12}) = \emptyset$.

- 4) Let us capture the preference values as per 4) to introduce Shannon weights and represent it as \mathcal{PDM} . Radio specialists assign preference values as shown in Table I, where, Low = 0.1; Medium = 0.4; High = 0.6; and Very high = 0.8.
- 5) Projection value (\mathfrak{pv}), entropy (\mathfrak{Ent}), divergence (\mathfrak{Div}), and weight (\mathfrak{Wgt}) of each signal attribute value γ_{ij} computed as per 5) can be realized in Table II.
- 6) After computing Shannon weights, we obtain abstract requirements from radio specialists \mathcal{RSR} for Wi-Fi Halow signal coverage in collapsed structures as

$$\begin{aligned}\mathcal{RSR}_1 &= \{\gamma_{13}, \gamma_{21}, \gamma_{31}, \gamma_{41}, \gamma_{51}\} \\ \mathcal{RSR}_2 &= \{\gamma_{12}, \gamma_{23}, \gamma_{31}, \gamma_{41}, \gamma_{52}\} \\ \mathcal{RSR}_3 &= \{\gamma_{11}, \gamma_{22}, \gamma_{32}, \gamma_{41}, \gamma_{52}\}.\end{aligned}$$

TABLE III
SOFT SET REPRESENTATION OF RS_1

	γ_{13}	γ_{21}	γ_{31}	γ_{41}	γ_{51}	WCV
$\mathcal{F}\zeta_1$	0	1	0	0	0	0.1021
$\mathcal{F}\zeta_2$	0	0	0	0	0	0
$\mathcal{F}\zeta_3$	0	0	0	0	0	0
$\mathcal{F}\zeta_4$	1	1	0	0	1	0.3577
$\mathcal{F}\zeta_5$	1	1	1	1	1	0.4004
\mathfrak{W}_{gt}	0.1212	0.1021	0.0213	0.0213	0.1344	

TABLE IV
SOFT SET REPRESENTATION OF RS_2

	γ_{12}	γ_{23}	γ_{31}	γ_{41}	γ_{52}	WCV
$\mathcal{F}\zeta_1$	0	0	0	0	1	0.0213
$\mathcal{F}\zeta_2$	0	1	0	0	1	0.1425
$\mathcal{F}\zeta_3$	1	0	0	0	1	0.0427
$\mathcal{F}\zeta_4$	0	0	0	0	0	0
$\mathcal{F}\zeta_5$	0	0	1	1	0	0.0427
\mathfrak{W}_{gt}	0.0213	0.1212	0.0213	0.0213	0.0213	

TABLE V
SOFT SET REPRESENTATION OF RS_3

	γ_{11}	γ_{21}	γ_{32}	γ_{41}	γ_{52}	WCV
$\mathcal{F}\zeta_1$	1	0	0	0	1	0.1557
$\mathcal{F}\zeta_2$	1	0	0	0	1	0.1557
$\mathcal{F}\zeta_3$	0	1	1	0	1	0.05373
$\mathcal{F}\zeta_4$	0	0	1	0	1	0.0111
$\mathcal{F}\zeta_5$	0	0	0	0	1	0.0213
\mathfrak{W}_{gt}	0.1344	0.0213	0.0111	0.0213	0.0213	

TABLE VI
IDEAL AND NIS FOR EACH RS

Radio	Specialists	$\mathbb{JS}(\gamma_i^*)$	NIS(γ_i^*)
RS_1		0.40038	0
RS_2		0.14254	0
RS_3		0.15574	0.01105

- 7) Subsequent tabular soft set representation along with WCV of each γ_{ij} for respective radio specialists \mathcal{RS} can be visualized through Tables III–V.
- 8) After that, we compute IS and NIS for all \mathcal{RS} s using 8, a key point in TOPSIS and envisage it in Table VI.
- 9) Corresponding separation measures of each \mathcal{RS} from IS and NIS computed as per 9 can be shown in Table VII, whereas combined separation measure based on signal functional concepts $\mathcal{F}\zeta_k$ and aforecomputed separation measures is presented in Table VIII.
- 10) Finally, we calculate the relative closeness of each $\mathcal{F}\zeta_k$ toward IS as in Table IX and rank the best result. We get ζ_5 as our signal functional concept. $\mathcal{F}\zeta_5$ is given as

$$\mathcal{F}\zeta_5 = \{\gamma_{13}, \gamma_{21}, \gamma_{31}, \gamma_{41}, \gamma_{51}\}.$$

Relative values of SFA for $\mathcal{F}\zeta_5$ are

$$\begin{aligned} \zeta_5 = & \text{Low, Poor, V.Good, Good} \\ & \times \text{V.Good, Maximum}. \end{aligned}$$

Finally, let us analyze the achieved signal functional concept as it may lead to a better solution. We observe from ζ_5 that low power, poor minimum detectable signal (MDS) threshold, very good coverage, good echo reception probability, and higher debris layer is the best

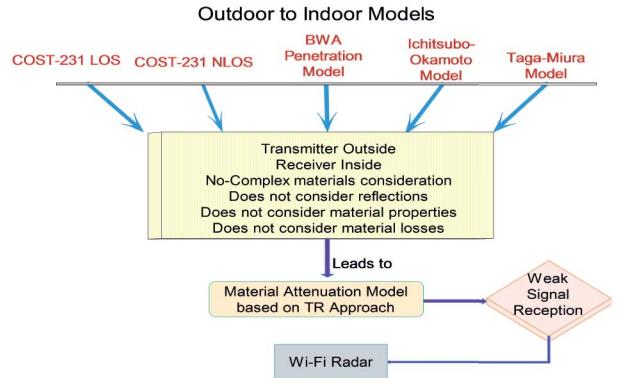


Fig. 5. Path to coverage range methods.

case to study the coverage of Wi-Fi Halow in collapsed structures. But, there can be an argument that radio specialists can directly give their opinions, and there is no need to apply the Shannon entropy method. The answer to this argument is that varied opinions of radio specialists cannot be trusted directly as it is multicriteria decision-making problem. It also needs cross-verification from the wireless communication theory and multiple opinion assessment to reach proper concept. So, Shanon entropy TOPSIS based on the bijective soft set method ensures trustworthy conceptual analysis from multicriteria coverage problem.

IV. COVERAGE RANGE METHODS

In this section, let us study wireless signal propagation methods that may provide us better coverage. First, we discuss the problem geometry from debris and echo models. After that, we employ TR and Wi-Fi radar techniques that may provide us better echo having proper CSI.

A. Problem Geometry

Let us revisit the echo model adopted in Fig. 3(c). We observe that the Wi-Fi transmitter usually radiates signals to possibly every direction. But to map the model for collapsed structure, we only assume the directional pattern of antenna focused on debris to avoid signals reflected from undesired resources and consider as noises. We also assume that a Wi-Fi device is placed outside of rubble with no other radio device in the vicinity. This placement provides us an understanding that Wi-Fi signal penetration through our debris model will comprise two parts, as shown in Fig. 6(a). These are free space and debris paths. It can be seen that wireless signals will travel about 1 m in free space before penetrating debris. After that, it faces many attenuations, fading, and damping from noisy and cluttered environments inside the debris model. A simplified relation from Fig. 6(a) can be given as follows:

$$PL = PL_{\text{free-space}} + PL_{\text{debris}}. \quad (1)$$

We can compute free-space path loss as

$$\begin{aligned} PL_{\text{free-space}} = & 20 \log_{10}(d) + 20 \log_{10}(f) \\ & + \log_{10}\left(\frac{4\pi}{c}\right) - AGains \end{aligned} \quad (2)$$

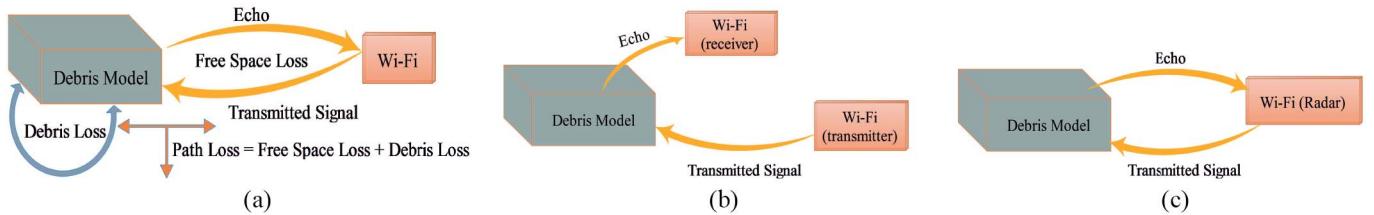


Fig. 6. Illustration of coverage range methods. (a) Path loss in collapsed structure (b) TR-approach. (c) Wi-Fi radar.

TABLE VII
SEPERATION MEASURE OF RS_1 , RS_2 , RS_3 FROM IS AND NIS

Functional Concepts	$\Delta_{1\kappa}^*$	$\Delta_{1\kappa}^\circ$	$\Delta_{2\kappa}^*$	$\Delta_{2\kappa}^\circ$	$\Delta_{3\kappa}^*$	$\Delta_{3\kappa}^\circ$
$\mathcal{F}\zeta_1$	0.089709	0.01042441	0.01468944	$4.553956E^{-4}$	0	0.0209351961
$\mathcal{F}\zeta_2$	0.1603041	0	0	0.0203176516	0	0.0209351961
$\mathcal{F}\zeta_3$	0.1603041	0	$9.97201E^{-3}$	$1.82158E^{-3}$	0.014060401	$1.8215824E^{-3}$
$\mathcal{F}\zeta_4$	$1.82158E^{-3}$	0.12794929	0.0203176516	0	0.0209351961	0
$\mathcal{F}\zeta_5$	0	0.1603041	$9.97201E^{-3}$	$1.82158E^{-3}$	0.01806336	$1.058841E^{-4}$

TABLE VIII
COMBINED SEPERATION MEASURE

Functional Concepts	Δ_κ^*	Δ_κ°
$\mathcal{F}\zeta_1$	0.3219632588	0.1783676027
$\mathcal{F}\zeta_2$	0.4003799446	0.2031079705
$\mathcal{F}\zeta_3$	0.4250672301	0.06035861496
$\mathcal{F}\zeta_4$	0.2075437971	0.3577
$\mathcal{F}\zeta_5$	0.1674531606	0.402779726

TABLE IX
RELATIVE CLOSENESS OF $\mathcal{F}\zeta$

Functional Concepts	ζ_κ^*
$\mathcal{F}\zeta_1$	0.3564993022
$\mathcal{F}\zeta_2$	0.3365570929
$\mathcal{F}\zeta_3$	0.1243415767
$\mathcal{F}\zeta_4$	0.6328242819
$\mathcal{F}\zeta_5$	0.7063425058

where d and f denote free-space distance and frequency, respectively. AGains represents the corresponding antenna gains for a Wi-Fi device. Now the only remaining term is PL_{debris} .

Debris Path Loss: To study debris path loss, we need to consider attenuations, which are caused by reflections, scattering, multipath, diffraction, and fading. Furthermore, fading will be both slow and fast, but to explicitly study attenuation and fading phenomena for collapsed structure, we need another research, and it cannot be covered in this article. So, we only use the existing literature for attenuations and introduce the term, X_G that comprises every probable path loss encountered to Wi-Fi signal and is given as follows:

$$PL_{debris} = X_G = x * AF(Br) + y * AF(Con) + z * AF(Gls) + k * AF(Lum) \quad (3)$$

where x , y , z , and k stands for the number of layers for our materials. AF is an attenuation factor induced by a single layer of concrete, glass, brick, and lumber, respectively. The thickness of structural elements will also characterize the ramification of layers, and AF values alter correspondingly.

Outdoor to Indoor Models: Wi-Fi Halow signal coverage problem in the debris model has resemblance with outdoor to indoor signal penetration scenario. So, we need to look into existing path loss models that only deals with building penetration loss from outdoor to indoor, as shown in Fig. 5. These methods are COST-231 LOS, COST-231 NLOS, broadband wireless access (BWA) model, Ichitsubo–Okamoto, and Taga–Miura model using the identification of path passing through wall openings which have been discussed in [29]. We observe that all outdoor to indoor models consider the receiver to be inside the building, which is contrary to our approach where the receiver should be outside of debris. Second, these methods do not adequately consider attenuations caused by materials that adversely affect Wi-Fi signals in collapsed structures. So, this triggers us to modify the existing models with the materials attenuation approach, which leads to TR and Wi-Fi radar techniques based on the probability of signal strength.

CSI Consideration: This article aims to investigate the coverage of Wi-Fi Halow signal that may be utilized for breathing detection in the future. It is mainly possible due to CSI encompassed in the echo received from the debris model. The echo signal will also contain clutter and noises in the CSI that may yield untrustworthy breathing detection. So, there is a need to consider CSI with robust breathing information for both coverage range methods. To achieve this, the echo signal should be above or equal to PDT, as discussed earlier in the echo model.

B. TR-Approach

In this technique, we make use of a “PL-Collapsed” from our work [30] with an extension to a more complex structure. We adopt this method to study existing outdoor to indoor path loss methods [29] for coverage in collapsed structures, as mentioned earlier in Fig. 5. We observe that even Wi-Fi sensing applications discussed before employ the same propagation models. To the best of our knowledge, all these techniques do not consider the receiver to be placed outside, although

there is one commonality that both transmitters and receivers at two different locations. Although, this mode also does not work well in collapsed structures, yet we still need to study the modified TR-approach for possible coverage as it can pave the way for new techniques. So, let us revisit the echo signal for the TR approach as shown in Fig. 6(b), where transmitter and receiver are placed at two distinct positions. To realize the Wi-Fi signal penetration in the debris model, we consider the link budget equation as

$$P_r = G_t + G_r + P_t - PL \quad (4)$$

where G and P represent the antenna gains and power for transceivers. PL defines the path losses incurred to Wi-Fi signal in both free space and debris. Let us compute path loss which is mainly dependent on the distance covered in debris and can be represented in the log as

$$PL = PL_{\text{free-space}} + 10 * \alpha * \log_{10} \left(\frac{d}{d_0} \right) + X_g \quad (5)$$

where $PL(d_0)$ is path loss for first 1 m d_0 . But this is only calculated for outside of debris as after penetrating the collapsed structure, there is no free space. α is path loss exponent having values ranging from 2 to 6 depending on the nature of the environment. We consider it 5, so dealing with complex structures while excluding metallic materials. Finally, we can incorporate attenuations of multiple layers of our debris through X_g .

CSI Consideration for TR Approach: To achieve an echo having substantial CSI, we consider a MDS. We envisage that echo should be equal or above than MDS with the probability of acceptable error rate $MDS(P_e)$ and can be given as

$$2P_{tx} + G_{tx} + G_{rx} - PL \geq MDS(P_e). \quad (6)$$

C. Wi-Fi Radar

In this method, we employ the Wi-Fi radar technique to complex structures, as shown in Fig. 6(c). In this technique, transmitter and receiver are considered to be at the same location quite similar to radar. We are confident that it will yield better results than the traditional TR-approach by reducing clutter and noise. We envision that all the existing studies do not study the Wi-Fi radar path loss model for debris scenarios except [33], which is work of authors, where they discussed it for simple structures without comparison with the TR-approach. Let us revisit Wi-Fi radar for our debris model as discussed in Section II-B. Under normal circumstances, it depends on cross-sectional area, signal intensities, antenna gains, and distance between target and transmitter. It can be given as follows:

$$P_r = P_t G_t G_r \left(\frac{c^2 \sigma}{(4\pi)^3 f^2 R^4} \right) \quad (7)$$

where P_t , P_r , G_t , and G_r represents power and gains of Wi-Fi radar transceiver. σ is cross-sectional area, which we consider as debris area while f and R symbolizes the frequency and range correspondingly. After this, the received signal at the input of Wi-Fi radar will be

$$\left\{ \begin{array}{l} \text{WiFi Signal received} \\ \text{at WiFi Radar} \end{array} \right\} = \frac{P_t G_t \lambda^2 4\pi \sigma}{(4\pi R)^2 \lambda^2} \times \frac{G_r \lambda^2}{(4\pi R)^2}. \quad (8)$$

TABLE X
SIMULATION PARAMETERS

Parameter	Values
Operational Frequencies	(902, 779)MHz
Transmission Power	(30, 24, 23, 13, 10) dBm
Antenna Gains	(6, 12, 13, 23, 26) dBi
Radar Cross Section	$4m^2$
Debris Type	Concrete, Brick, Glass, Lumber
Attenuation of Concrete 8"	23dB at 902 MHz
Attenuation of Brick 10.5"	7dB at 902 MHz
Attenuation of Glass (13mm)	2dB at 902 MHz
Attenuation of Lumber (76mm)	2.8dB at 902 MHz
Minimum Debris Layers	10 ($4b+2c+2g+2l$)
	13 ($5b+3c+2g+3l$)
Maximum Debris Layers	18 ($8b+3c+3g+4l$)
	22 ($10b+4c+4g+4l$)
Modulation Type	256QAM, 64QAM, 16QAM
Channel BW at 256QAM	1MHz
Channel BW at 64QAM	1MHz
Channel BW at 16QAM	16MHz
MDS Threshold at 256QAM	-70dBm
MDS Threshold at 64QAM	-77dBm, -78dBm
MDS Threshold at 16QAM	-71dBm, -75dBm
Path Loss Exponent	5

Although, a detailed derivation of Wi-Fi radar range is provided in the Appendix, yet the reduction of (8) to log form after doing some mathematics can be given as follows:

$$P_R = G_T + G_R + G_\sigma + P_T - 2\beta_1 \quad (9)$$

where β_1 and G_σ represents free-space path losses and target gain, respectively. Now, we need to incorporate the debris losses and clutter faced by Wi-Fi Halow because of multilayered scenario from (3) in (9), and then we reconvert log form to normal scale given as

$$\text{WiFi Radar Range} = R = \sqrt[4]{\frac{P_t G_t G_r}{P_r} \left(\frac{\lambda^2 \sigma}{(4\pi)^3} \right) \frac{1}{X_g}}. \quad (10)$$

After getting a complete relation of coverage from (10), we can take (10) to log form again for final range calculation as provided in VII. We consider σ in (10) as debris area under observation whereas P_r is the MDS which can provide us desired echo.

CSI Consideration for Wi-Fi Radar: To achieve an echo having desired CSI for Wi-Fi radar, we consider signal-to-noise ratio (SNR). We envision that received echo should have SNR above or equal to a PDT as $\text{SNR} \geq \text{SNR}_T$.

V. NUMERICAL RESULTS

In this section, we present our simulation method and the numerical results for evaluation. We simulated Wi-Fi Halow for vital signal attributes. Finally, we compare these results to select the best radio propagation method for better coverage in a collapsed structure.

A. Method

To achieve substantial results, there is an immense need to select the simulation parameters shown in Table X accurately. We have performed simulations in MATLAB 18a.

Let us discuss the reasons for the selection of these simulation parameters. We considered two operating frequencies for

TABLE XI
WI-FI HALOW SIGNAL COVERAGE AT 902 MHz

Transmit Power dBm	Max Antenna dBi	Range in Collapsed Structure (m)													
		QAM 256(R =5/6)(MS=-70dBm)				QAM 16(R =3/4)(MS=-71dBm)				QAM 16(R =1/2)(MS=-75dBm)					
		T-R		Wi-Fi Radar		T-R		Wi-Fi Radar		T-R		Wi-Fi Radar			
		Mn 10	Mx 18	Mn 10	Max 18	Mn 10	Mx 18	Mn 10	Mx 18	Mn 10	Mx 18	Mn 10	Mx 18		
30 24 23	6 12 13	0.7519 1.7224 1.9776	0.0506 0.1159 0.1331	4.4289 6.2560 6.6267	0.1518 0.2144 0.2271	0.7873 1.8036 2.0708	0.0530 0.1214 0.1394	4.6913 6.6267 7.0193	0.1518 0.2144 0.2271	0.9465 2.1684 2.4897	0.0637 0.1459 0.1675	5.9060 8.3425 8.8368	0.1518 0.2144 0.2271		
		QAM64(R =3/4)(MS=-78dBm)				QAM64(R =5/6)(MS=-77dBm)									
		13 10	23 26	7.8730 11.9163	0.5298 0.8019	11.7840 14.0054	0.4039 0.4801	11.3799 17.2242	0.7658 1.1592	18.6764 22.1970	0.4039 0.4801	10.8678 16.4490	0.7314 1.1070	17.6317 20.9553	0.4039 0.4801
		QAM 16(R =3/4)(MS=-71dBm)				QAM 16(R =1/2)(MS=-75dBm)									
30 24 23	6 12 13	0.1660 0.3803 0.4367	0.0084 0.0192 0.0221	0.6703 0.9469 1.0030	0.0161 0.0227 0.0241	0.1738 0.3982 0.4572	0.0088 0.0201 0.0231	0.7101 1.0030 1.0624	0.0161 0.0227 0.0241	0.2090 0.4788 0.5497	0.0106 0.0242 0.0278	0.8939 1.2627 1.3357	0.0161 0.0227 0.0241		
		QAM64(R =3/4)(MS=-78dBm)				QAM64(R =5/6)(MS=-77dBm)									
		13 10	23 26	1.7384 2.6311	0.0879 0.1331	1.7836 2.1198	0.0428 0.0509	2.5127 3.8031	0.1271 0.1924	2.8268 3.3597	0.0428 0.0509	2.3996 3.6320	0.1214 0.1837	2.6687 3.1717	0.0428 0.0509

TABLE XII
WI-FI HALOW SIGNAL COVERAGE AT 779 MHz

Transmit Power dBm	Max Antenna dBi	Range in Collapsed Structure (m)													
		QAM 256(R =5/6)(MS=-70dBm)				QAM 16(R =3/4)(MS=-71dBm)				QAM 16(R =1/2)(MS=-75dBm)					
		T-R		Wi-Fi Radar		T-R		Wi-Fi Radar		T-R		Wi-Fi Radar			
		Mn 10	Mx 18	Mn 10	Max 18	Mn 10	Mx 18	Mn 10	Mx 18	Mn 10	Mx 18	Mn 10	Mx 18		
30 24 23	6 12 13	0.7973 1.8264 2.0970	0.0537 0.1229 0.1411	4.7657 6.7318 7.0306	0.1634 0.2307 0.2444	0.8348 1.9125 2.1959	0.0562 0.1287 0.1478	5.0481 7.1306 7.5532	0.1634 0.2307 0.2444	1.0037 2.2994 2.6400	0.0675 0.1547 0.1777	6.3552 8.9769 9.5089	0.1634 0.2307 0.2444		
		QAM64(R =3/4)(MS=-78dBm)				QAM64(R =5/6)(MS=-77dBm)									
		13 10	23 26	8.3485 12.6359	0.5618 0.8504	12.6803 15.0705	0.4346 0.5166	12.0672 18.2645	0.8121 1.2292	20.0969 23.8852	0.4346 0.5166	11.5241 17.4425	0.7755 1.1738	18.9727 22.5491	0.4346 0.5166
		QAM 16(R =3/4)(MS=-71dBm)				QAM 16(R =1/2)(MS=-75dBm)									
30 24 23	6 12 13	0.1760 0.4033 0.4630	0.0089 0.0204 0.0234	0.7213 1.0189 1.0793	0.0173 0.0244 0.0259	0.1843 0.4223 0.4849	0.0093 0.0214 0.0245	0.7641 1.0793 1.1432	0.0173 0.0244 0.0259	0.2216 0.5077 0.5829	0.0112 0.0257 0.0295	0.9619 1.3587 1.4392	0.0173 0.0244 0.0259		
		QAM64(R =3/4)(MS=-78dBm)				QAM64(R =5/6)(MS=-77dBm)									
		13 10	23 26	1.8433 2.7900	0.0932 0.1411	1.9192 2.2810	0.0460 0.0547	2.6645 4.0328	0.1348 0.2040	3.0418 3.6152	0.0460 0.0547	2.5445 3.8513	0.1287 0.1948	2.8716 3.4129	0.0460 0.0547

Wi-Fi Halow, i.e., China (779 MHz) and the U.S. (902 MHz), as given in [34] and [45], which are regulated by IEEE Task Group³ [45], [46]. We selected China and U.S. standards due to our field survey and for its worldwide acceptance. Now, both countries have their power consideration for Wi-Fi Halow spectrum limits as in [45]. Similarly, variance in other

parameters, such as signal intensities and antenna gains is regulated with Federal Communications Commission (FCC)⁴ para 17.245 rules for point to multipoint (PTMP).⁵

Next, we discuss the selection of debris types. We considered concrete, brick, glass, and lumber for our simulations because these were the primary structural materials found

⁴<https://www.fcc.gov/tags/radio-rules>

⁵<https://www.air802.com/fcc-rules-and-regulations.html>

in the field survey. These materials have different thickness levels, but to simplify the results, we only considered brick 10.5'', concrete 8'', lumber(76 mm), and glass(13 mm). The depth of these materials defines the complexity of collapsed structures. We employ the attenuations caused by single layers of under considered materials from Digi⁶ and U.S. National Institute of Standards and Technology (NIST).⁷ We also selected the debris layers with minimum as (10, 13) and maximum as (18, 22) to properly compute the Wi-Fi Halow signal penetration through debris model.

Finally, we discuss the MDS threshold, which is very important to receive an echo signal having significant CSI. We have taken the MDS threshold from [34], [46], [47] ranging from -70 to -78 dBm at different rates depending on three QAM types (256, 64, 16) with 1-MHz channel bandwidth for QAM 256 and QAM64, and 16-MHz channel for QAM 16, correspondingly. We cannot choose 1-MHz channel bandwidth for 16QAM because the required MDS will be more than -80 dBm as per [47], which is not feasible for collapsed sensing purposes. The best case is to have a higher MDS threshold, preferably between -70 to -80 dBm for reasonable CSI. Higher QAM ensures better data rate, but also cause noise and interference. On the contrary, lower QAM reflects less noise, but in our case, selecting lower QAM means weak SNR, which is not much suitable for Wi-Fi. Furthermore, minimum channel bandwidth such as 1 MHz provides more coverage than the 16-MHz channel. That is why we have chosen both high and low QAM scenarios with different channel bandwidths to have a better knowledge of Wi-Fi Halow signals. Moreover, path loss exponent is taken as 5 to consider the complex debris layout.

B. Results

We conducted simulations on the criteria as mentioned earlier by mapping field survey to theory. We present simulations results in Tables XI and XII. These results show coverage level at varied debris types across antenna and intensity for Wi-Fi Halow frequencies. Both frequency cases have been tested for overall 240 times to have a better inference. Let us compare the coverage results in subsequent sections. For convenience, we have presented TR and Wi-Fi radar methods as 1 and 2 in the graphical results.

1) Range With Respect to Debris Type: We classify debris into two types for the layered model. We consider type 1 as ($\text{MinLayer} = 10$, $\text{MaxLayer} = 18$) followed by type 2 as ($\text{MinLayer} = 10$, $\text{MaxLayer} = 18$) and perform simulations for 902 MHz and 779 MHz. A comparison is as follows.

a) 902 MHz: We compare the results for types 1 and 2 debris from Table XI and plot them as individual value plot in Figs. 7 and 8. It can be observed from the results that type 1 debris can provide more coverage than the other one. Let us revisit Table XI for the 10-dBm power case; we can see that range for type 1 min layer is 11.916 m for TR and 14.0054 m for the Wi-Fi Radar, respectively; whereas, for type 2 min layer, the range at TR is 2.63 and 2.1198 m. These results show

⁶<http://ftp1.digi.com/support/images/XST-AN005a-IndoorPathLoss.pdf>

⁷<http://www.ciwellspring.org/shielding.html>

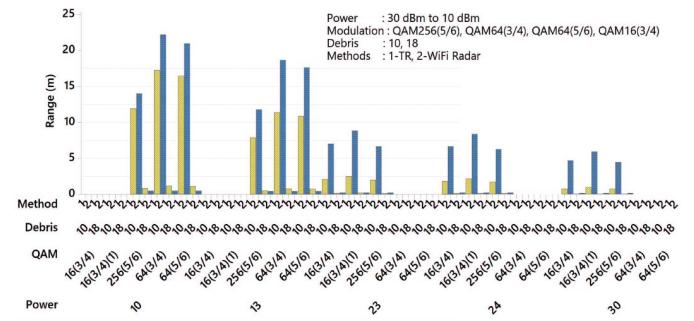


Fig. 7. Range in type 1 debris (902 MHz).

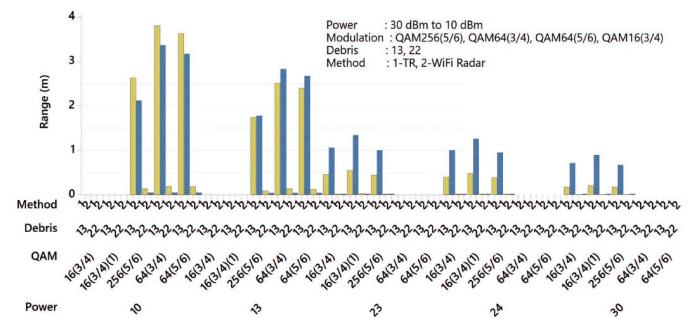


Fig. 8. Range in type 2 debris (902 MHz).

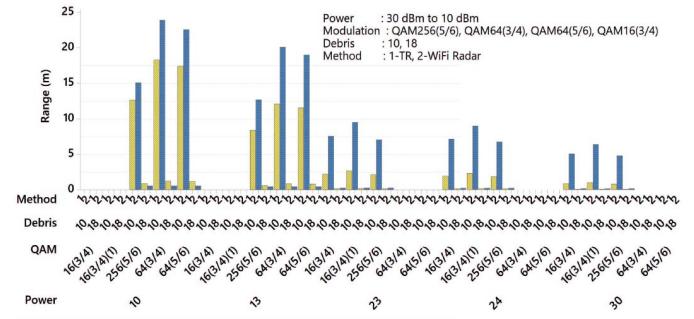


Fig. 9. Range in type 1 debris (779 MHz).

that low-layered debris using the Wi-Fi radar method provides better coverage rather than TR. However, in heavy layered debris, TR performs relatively better, but TR is not a practical method as it does not consider echo properly, and coverage margin is not much significant. Moreover, this sharp decline in coverage is due to the added debris layers that cause attenuations, fading, scattering, and related challenges. Besides, we also observe increased signal coverage for lower QAM. Let us consider QAM 256 and QAM 64 for the 10 dBm power case for type 2 max layer scenario as an example. The coverage at QAM 256 using the TR is 0.1411 m and 0.0547 m for the Wi-Fi Radar, respectively. However, the range at QAM 64 for the same parameters is 0.2040 and 0.0547 m while using TR and Wi-Fi radar techniques correspondingly. This behavior is the same across all other power and QAM values. In conclusion, we observe that increasing debris layers reduces coverage.

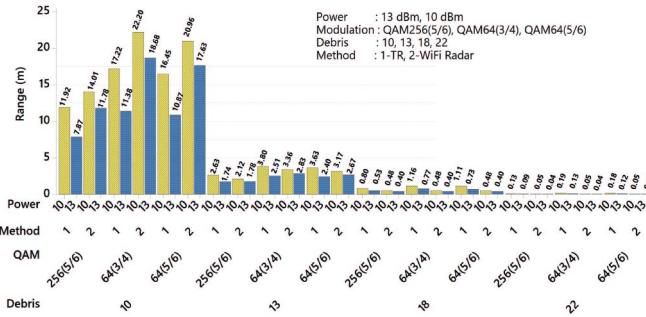


Fig. 10. Range in type 2 debris (779 MHz).

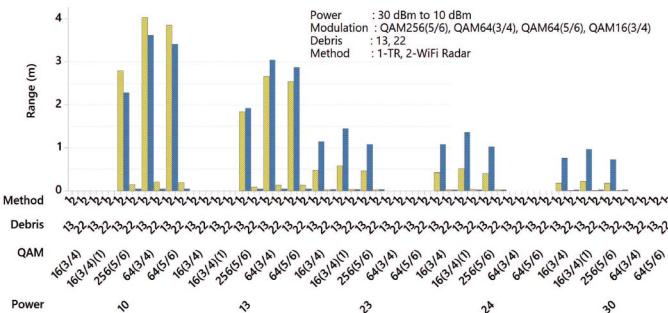


Fig. 11. Range at low power with all debris cases (902 MHz).

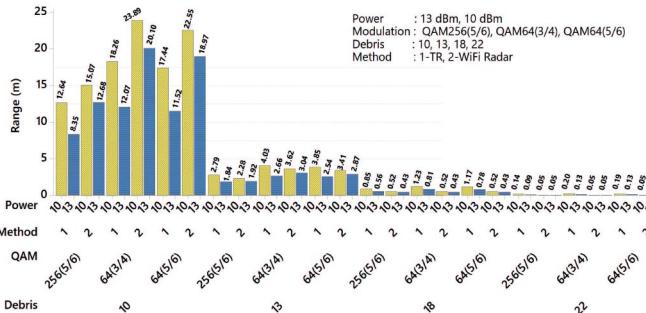


Fig. 12. Range at low power with all debris cases (779 MHz).

b) **779 MHz:** Similarly, we compare the results at 779 MHz for type 1 and 2 debris from Table XII and plot them as individual value plot in Figs. 9 and 10. We get a similar trend to that of 902 MHz. Now, again, looking into Table XII for the 10-dBm power case as an example, we can observe that range for type 1 min layer is 12.63 m while using TR and 15.0705 m for the Wi-Fi Radar, respectively; whereas, for type 2-min layer, the range is 2.79 m at TR and 2.2810 m. This behavior is the same across all other power and QAM values. Quite similar to 902 MHz, we observe that increasing debris layers reduces coverage. But we observe that 779 MHz has slightly better coverage than 902 MHz.

2) **Range With Respect to Low Power:** We observe from Section V-B1 that low power Wi-Fi Halow yields better results. Let us revisit Table XI to verify the range at low and high power. We take type 1 debris with min layer using Wi-Fi radar method as an example. It can be observed that the signal

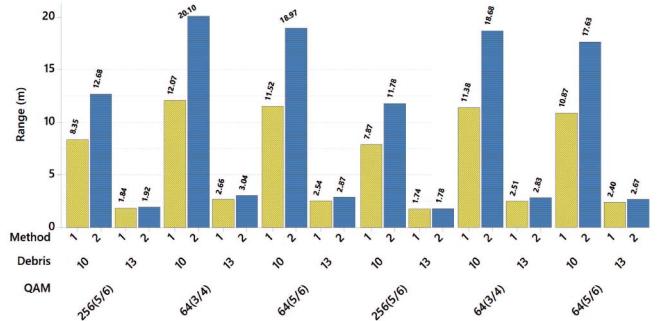


Fig. 13. Frequency wise range for lower debris at 13 dBm.

range at 30-dBm power is 4.428 and 14.0054 m at 10 dBm, respectively. This trend is the same across all debris cases, QAM values, and both propagation methods. Therefore, let us focus on lower power values, i.e., 13 and 10 dBm for both 902 and 779 MHz as plotted in Figs. 11 and 12. It can be observed that 10 dBm with the Wi-Fi radar method performs better than 13 dBm, e.g., at the 902-MHz range at 13 dBm with QAM 256 and min layer 10 is 11.78 m using Wi-Fi radar whereas, it is 14.0054 m at 10 dBm. There is the same trend as 779 MHz. We also observe a decreasing trend of coverage with the increase in debris layers. Let us consider coverage at 779 MHz with 13-min layer, the Wi-Fi radar, and 10-dBm power; it is 0.0547 m. On the contrary, it is 0.0547 m with the same parameters except for change of debris layers to 22. So, we can rightly say that Wi-Fi Halow is serving our purpose of low-power Wi-Fi sensing solution.

3) **Range With Respect to Frequency:** Let us further investigate the low power penetration into debris with a comparison of both frequencies at lower debris layers. We observed from Section V-B2 that lower debris layers can yield better results; so, we envisaged that higher debris layers could not provide better coverage. We plot a frequency-wise comparison for 13-dBm and 10 dBm in Figs. 13 and 14, respectively. Let us consider the 10-dBm plot, where maximum coverage with 10-layered debris employing Wi-Fi radar method at 779 MHz has coverage of 23.89 m, whereas it is 22.20 m for 902 MHz. By making a comparison of all results, we figure out that Chinese (779 MHz) provides better results than the U.S. (902 MHz). The main reason for the low frequency to have better coverage is higher wavelength, which ensures better diffraction of the beam.

4) **Range With Respect to Method:** Finally, we compare the Wi-Fi signal propagation methods. We employed two techniques, i.e., TR approach and Wi-Fi radar in this article. To have a comparison, let us consider Fig. 14. The maximum coverage range at 10-layered debris for 779 MHz at QAM 64 is 23.89 m through the Wi-Fi radar approach; however, it is 18.26 with a TR approach. From this, we figure out Wi-Fi radar, which is a modified form of conventional Doppler radar provides us better coverage. However, if we compare the results at 13-layered debris for same 779 MHz and QAM64, the coverage is 4.03 and 3.6 m for TR and Wi-Fi Radar techniques, respectively. Here, we observe the opposite trend for signal

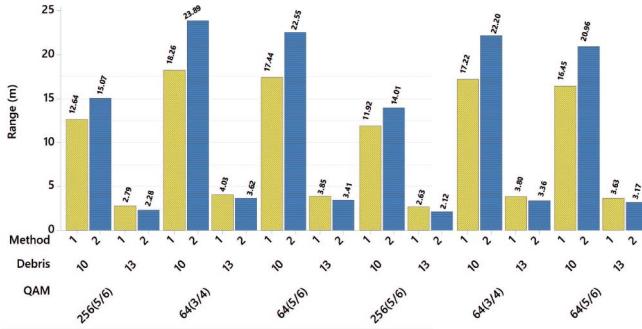


Fig. 14. Frequency wise range for lower debris at 10 dBm.

coverage while considering heavy debris layers. This analysis provides us an understanding that the TR method is not a practical method as coverage should drastically be lower if there is heavy debris; however, this trend does not happen. On the contrary, Wi-Fi Radar ensures better coverage at fewer debris scenarios and receives weak signals for complex scenarios, which is true in real-world environments. If we compare these methods across both Tables XI and XII, we get the same trend providing us immense insight into the application of Wi-Fi radar.

VI. PERFORMANCE ANALYSIS

In this section, we briefly analyze our study. First, we deliberate the complexity of the problem in the context of existing literature. Then, we present signal propagation methods from both the conceptual and signal levels. Finally, we discuss the importance, applications, implications, and limitations of this article.

Let us analyze the complexity of the problem. We observe that collapsed structures turn into complex indoor layout having multilayered obstacles where signal penetration becomes very poor. That is why there are no successful post-disaster rescue solutions available, in spite of the IoT era. Although, there are some rescue techniques, out of which radar sensing [8] is the most promising one, yet it is not well-suited for rescue, except providing a strong motivation for the wireless signal application. Another reason for the need for this article is that most of the existing studies, as discussed in Section I-A are expensive and cannot be deployed in developing countries. So, this motivated us to investigate this subject using Wi-Fi radios as sensors in [30]–[33] to initiate a new dimension of research, which is quite ubiquitous and cost effective, and availability is also ensured with the growing Internet market.

Let us discuss the methods to study the coverage of Wi-Fi Halow in collapsed structures. We presented signal propagation models both at the conceptual and communication level by employing the Shannon entropy TOPSIS and coverage range methods, respectively. TOPSIS using the Shannon entropy based on the bijective soft set was introduced by [48] for multicriteria decision making problems. We applied this method to select the best coverage concept from available intensities, gains, thresholds, debris nature, and CSI consideration.

Similarly, coverage range methods are further classified into the TR approach and Wi-Fi radar, which we earlier introduced separately in [30] and [33] for regular debris. We take the range of Wi-Fi signals as the main objective for evaluation because it gives us insight into future rescue solutions while employing IoT.

Now, let us discuss the best coverage concept for the Wi-Fi Halow signal. The Shannon entropy method in Section III provides us immense insight about conceptual coverage where functional concept \mathcal{F}_5 was considered as the most optimal solution. \mathcal{F}_5 represents low power, weak MDS threshold, higher echo reception probability, and better debris types. Now, we need to compare this functional concept with simulation results of coverage range methods. After an in-depth analysis of Section V, we observe that Wi-Fi radar with low power can yield almost the same results to the conceptual level model with a minor difference of debris complexity. Although there can be an argument on the coverage of both TR and Wi-Fi radar, yet echo reception probability of later is better because in the TR approach, received signal only need to be reflected, but it does not ensure the same Wi-Fi device. So, there is a probability of more noises for the TR approach.

Finally, we discuss the possible applications of this article. We observe that Wi-Fi sensing application for breathing detection in [18] along with [14] can provide us better results for rescue if signal strength can be increased using our Wi-Fi radar technique that may give us better CSI. To the best of our understandings, all the Wi-Fi sensing applications do not employ the Wi-Fi radar method, which lacks their practical consideration for collapsed structures. So, we envision that our study can provide a breakthrough to the scientific community to investigate more about Wi-Fi Halow signals in a collapsed structure. It is because of low frequency, low power, ubiquitous, and cost effectiveness of Wi-Fi Halow, which is primarily designed for IoTs. This article of ours justifies that wireless signals can have better coverage using low power and low frequency. So, we can rightly say that further research in this domain will lead us to the ubiquitous post-disaster rescue, which will be available in developing countries as well hence truly serving humanity.

Limitations: Like every other work, this article has some limitations. The first and the most important one is a lack of practical implementation of Wi-Fi Halow signals to collapsed structures. It is due to the primitive nature of this article, as we cannot deploy the solution without having proper simulations and conceptual models based on a strong theoretical background. So, our work emphasizes the theoretical aspect of the problem. However, we conducted a field survey to have practical consideration of theory. Another limitation of this article is that we did not discuss fading models and just used attenuation factors for materials from NIST. The reason for this limitation is quite similar that we cannot deal with these issues in simulations directly. So, the best way is to use the practical results of standard bodies. However, there is a dire need to study signal attenuations, fading, and related challenges in a separate study before the practical deployment of

such technique. Based on these observations, we are hopeful that this article will trigger further research in IoTs-based rescue solutions.

VII. CONCLUSION

In this article, we studied the feasibility of Wi-Fi Halow for adequate coverage in collapsed structures. To achieve this, we conducted a field survey of an earthquake site to realize debris as a multiobstacle layered indoor layout that needs better signal penetration. After that, we presented signal propagation methods both at a conceptual level and signal communication, as well. The first method is based on a bijective soft set with an integrated approach of Shannon entropy TOPSIS, which provides results with strong mathematical foundations. Furthermore, the TR approach and Wi-Fi radar techniques present the communication of signals in the debris model to realize the collapsed structure and give us probable coverage. Finally, we conclude that the Wi-Fi radar method is the most suited technique as the TR approach can face more attenuations, and also it does not seem practical for the collapsed environment. We envision that the Wi-Fi Halow with Wi-Fi radar method can trigger more research in this post-disaster rescue.

APPENDIX

PROOF OF THE WI-FI RADAR RANGE EQUATION

$$P_r = \frac{P_t G_t G_r \lambda^2 \sigma}{(4\pi)^3 R^4}. \quad (11)$$

Since $\lambda = (c/f)$, (11) can be modified as

$$P_r = P_t G_t G_r \left(\frac{c^2 \sigma}{(4\pi)^3 f^2 R^4} \right)$$

$$\left\{ \begin{array}{l} \text{Signal Received} \\ \text{at Debris} \end{array} \right\} = \frac{P_t G_t G_r \lambda^2}{(4\pi R)^2}.$$

Since $G_r = (4\pi \sigma / \lambda^2)$, signal reflected from debris will be

$$\left\{ \begin{array}{l} \text{Signal Reflected} \\ \text{from Debris} \end{array} \right\} = \frac{P_t G_t \lambda^2 4\pi \sigma}{(4\pi R)^2 \lambda^2} \quad \text{then}$$

$$\left\{ \begin{array}{l} \text{Received Signal} \\ \text{at WiFi Radar} \end{array} \right\} = \frac{P_t G_t \lambda^2 4\pi \sigma}{(4\pi R)^2 \lambda^2} \times \frac{G_r \lambda^2}{(4\pi R)^2}. \quad (12)$$

Let us reduce above equation in to log form as

$$P_R = P_T + G_T + G_R + 20 \log \left(\frac{\lambda}{4\pi R} \right) + 10 \log \left(\frac{4\pi \sigma}{\lambda^2} \right)$$

$$+ 20 \log \left(\frac{\lambda}{4\pi R} \right)$$

$$P_R = P_T + G_T + G_R + G_\sigma - 2\beta_1 \quad (13)$$

where $\beta_1 = 20 \log(4\pi f R / c)$ and $G_\sigma = 10 \log(4\pi \sigma / \lambda^2)$

$$PL = PL_{\text{free-space}} + PL_{\text{debris}} \quad (14)$$

$$PL_{\text{debris}} = X_G = l * AF(Br) + m * AF(Con)$$

$$+ o * AF(Gls) + p * AF(Lum) \quad (15)$$

$$P_R = P_T + G_T + G_R + G_\sigma - 2\beta_1 - X_G. \quad (16)$$

To compute coverage, we need to reconvert log form and employ (12) which provides us range in power form

$$R^4 = \frac{P_t G_t G_r}{P_r} \left(\frac{\lambda^2}{4\pi} \right) \left(\frac{4\pi \sigma}{\lambda^2} \right) \left(\frac{\lambda^2}{4\pi} \right) \frac{1}{X_g}. \quad (17)$$

Finally, by rearranging the above equation for range, we get

$$\text{WiFi Radar Range} = R = \sqrt[4]{\frac{P_t G_t G_r}{P_r} \left(\frac{\lambda^2 \sigma}{(4\pi)^3} \right) \frac{1}{X_g}}. \quad (18)$$

Equation (18) in log form can be given as follows:

$$10 \log R \cong \frac{1}{4} [P_T + G_T + G_R + 10 \log \sigma - P_R - 20 \log f$$

$$- 30 \log(4\pi) + 20 \log(c) - X_G]. \quad (19)$$

Let us consider $K_1 = 20 \log[4\pi/c]$, so (19) will yield the following relation:

$$10 \log R \cong \frac{1}{4} [P_T + G_T + G_R + 10 \log \sigma - P_R - X_G$$

$$- 20 \log f - K_1 - 10.99 \text{ dB}]. \quad (20)$$

Finally, Wi-Fi radar range through log form can be computed as

$$\text{WiFi Radar Range} = R = 10^{\frac{Q_{\text{dB}}}{10}}. \quad (21)$$

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Muhammad Faizan Khan received the B.Sc. degree in information and communication system engineering from the National University of Science and Technology, Islamabad, Pakistan, and the Master of Engineering degree in communication and information systems from the Huazhong University of Science and Technology, Wuhan, China. He is currently pursuing the Ph.D. degree in computer science and cyber engineering with Guangzhou University, Guangzhou, China.

He worked as a Lecturer with the University of South Asia, Lahore, Pakistan.



Guojun Wang (Member, IEEE) received the B.Sc. degree in geophysics, the M.Sc. degree in computer science, and the Ph.D. degree in computer science from Central South University, Changsha, China, in 1992, 1996, and 2002, respectively.

He is currently a Pearl River Scholarship Distinguished Professor and the Vice Dean of the School of Computer Science and Cyber Engineering, Guangzhou University, Guangzhou, China, where he is also the Director of Institute of Computer Networks. He was a Professor with Central South University, Changsha; the Visiting Scholar with Temple University, Philadelphia, PA, USA, and Florida Atlantic University, Boca Raton, FL, USA; the Visiting Researcher with the University of Aizu, Aizuwakamatsu, Japan; and the Research Fellow with the Hong Kong Polytechnic University, Hong Kong. His research interests include artificial intelligence, big data, cloud computing, and cyberspace security.

Prof. Wang is a Distinguished Member of CCF, and a member of ACM and IEICE.



Kun Yang received the Ph.D. degree from the Department of Electronic and Electrical Engineering, University College London (UCL), London, U.K.

He worked with UCL on several European Union (EU) research projects for several years. He is currently a Chair Professor with the School of Computer Science and Electronic Engineering, University of Essex, leading the Network Convergence Laboratory, U.K. He manages research projects funded by various sources, such as U.K. EPSRC, EU FP7/H2020, and industries. He has published over 150 journal papers and filed ten patents. His main research interests include wireless networks and communications, IoT networking, data and energy integrated networks, and mobile edge computing.

Dr. Yang serves on the editorial boards for both IEEE and non-IEEE journals. He has been a fellow of IET since 2009.



Md Zakirul Alam Bhuiyan (Senior Member, IEEE) received the Ph.D. degree from Central South University, Changsha, China, in 2013.

He is currently an Assistant Professor with the Department of Computer and Information Sciences, Fordham University, New York, NY, USA, where he is the Founding Director of Fordham Dependable and Secure System Laboratory (DependSys). He worked as an Assistant Professor with the Temple University, Philadelphia, PA, USA. He is also a Visiting Professor with Guangzhou University, Guangzhou, China. His research focuses on dependability, cybersecurity, big data, and cyber physical systems. His work in these areas published in top-tier venues, including the IEEE TRANSACTIONS ON COMPUTERS, the IEEE TRANSACTIONS ON PARALLEL AND DISTRIBUTED SYSTEMS, the IEEE TRANSACTIONS ON DEPENDABLE AND SECURE COMPUTING, the IEEE TRANSACTIONS ON INDUSTRIAL INFORMATICS, *IEEE Communications Magazine*, the IEEE INTERNET OF THINGS JOURNAL, the ACM Transactions on Sensor Networks, the ACM Transactions on Autonomous and Adaptive Systems, Computer Science, Information Sciences, and the Journal of Network and Computer Applications.

Dr. Bhuiyan has served as the Guest/Associate Editor for the IEEE TRANSACTIONS ON BIG DATA, the ACM TRANSACTIONS ON CYBER-PHYSICAL SYSTEMS, the IEEE INTERNET OF THINGS JOURNAL, *Information Sciences*, *Future Generation Computer Systems*, and the *Journal of Network and Computer Applications*. He has also served as an Organizer, the General Chair, the Program Chair, the Workshop Chair, and a TPC Member of various international conferences including IEEE INFOCOM. He is a member of ACM.