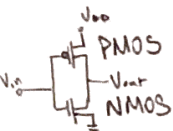


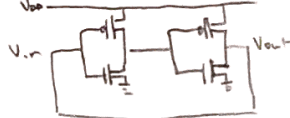
# ① RC Circuits

Inverter: logical block output inverse,  $0 \leftrightarrow 1$ 

Oscillator: device oscillates between 0 and 1



CMOS Inverter



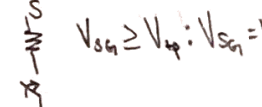
Ring Oscillator

$V_{in}$	$V_{out}$	NMOS	PMOS
$V_{DD}$	0	on	off
0	$V_{DD}$	off	on

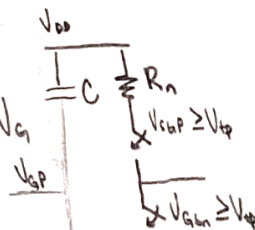
DPMOS Transistor



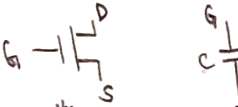
Resistor-Switch Model



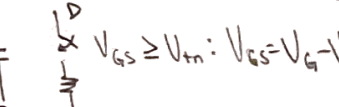
$$V_{GS} \geq V_{th}: V_{S1} = V_S - V_{GS}$$



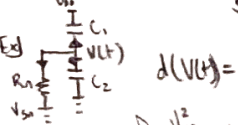
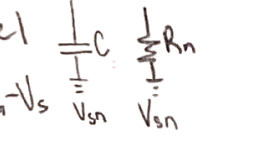
NMOS Transistor



Resistor-Switch Model



$$V_{GS} \geq V_{th}: V_{GS} = V_G - V_S$$



$$d(V_{out}) = \frac{V(t)}{R_n(C_1 + C_2)}$$

$$P = \frac{V_{DD}^2}{R_n} \text{ when } V_{in} = V_{DD}, \text{ or } 0$$

$$V(t) = C_0 e^{-\frac{t}{RC}}: \text{Charging}$$

$$V(t) = V_{DD}(-e^{-\frac{t}{RC}} + 1): \text{Discharging}$$

## ② Input

$$\frac{d}{dt} V(t) = \lambda v(t) + \lambda u(t)$$

$$V(t) = V_0 e^{\lambda t} + \lambda \int_0^t u(\theta) e^{\lambda(t-\theta)} d\theta$$

## ③ Vector Differential Equations

$$A \vec{v}_\lambda = \lambda \vec{v}_\lambda \quad \vec{v}_\lambda \neq 0 \text{ eigenvector} \quad \det(A - \lambda I_n) = 0$$

$$\vec{x}(t) \xrightarrow{A \cdot VAV^{-1}} \frac{d}{dt} \vec{x}(t)$$

$$\vec{v}(t) \xrightarrow{V^{-1}} \frac{d}{dt} \vec{v}(t)$$

$$\vec{v}(t) \xrightarrow{\Lambda = VAV^{-1}} \frac{d}{dt} \vec{v}(t)$$

$$\Lambda = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \quad V = \begin{bmatrix} \vec{v}_1 & \vec{v}_2 \\ 1 & 1 \end{bmatrix}$$

$$\frac{d}{dt} \begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix} = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix}$$

$$\det(\lambda I - A) \Rightarrow \lambda_1, \lambda_2, \vec{v}_1, \vec{v}_2$$

$$V = [\vec{v}_1, \vec{v}_2] \quad \Lambda = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}$$

$$\vec{x} = V^{-1} \vec{v} \quad \frac{d}{dt} \vec{x}(t) = V^{-1} \frac{d}{dt} \vec{v}(t)$$

$$\frac{d}{dt} V^{-1} \vec{x}(t) = V^{-1} V A V^{-1} \vec{x} \Rightarrow \frac{d}{dt} \vec{x}(t) = \Lambda \vec{x}(t)$$

$$\vec{x}[1] = K_1 e^{\lambda_1 t} \quad \vec{x}[2] = K_2 e^{\lambda_2 t}$$

$$\begin{bmatrix} \vec{x}[1](0) \\ \vec{x}[2](0) \end{bmatrix} = V^{-1} \begin{bmatrix} v_1(0) \\ v_2(0) \end{bmatrix}$$

$$\vec{x} = V \vec{v}$$

$$\frac{d}{dt} \vec{x}(t) = A \vec{x} + \vec{b} \Rightarrow A \hat{x} = A \vec{c} + \vec{b} \Rightarrow \frac{d}{dt} \hat{x} = A \hat{x}$$

$$\vec{v} = \hat{A}^{-1} (\hat{A} \vec{v} + \vec{b}) = \begin{bmatrix} K_1 \\ K_2 \end{bmatrix}$$

$$\vec{v} = \hat{A}^{-1} (\hat{A} \vec{v} - \vec{b}) = \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

Inductors: Stores energy in magnetic field  $[H]$ 

$$V(t) = L \frac{dI(t)}{dt}$$

Series:  $L_1 + L_2$ Parallel:  $\frac{L_1 L_2}{L_1 + L_2}$ 

prod sum

## ④ Complex Mms

$$j = \sqrt{-1} \quad z = a + jb$$

Conjugate:  $\bar{z} = a - jb$ 

$$|z| = \sqrt{a^2 + b^2}$$

$$z = |z| e^{j\theta} = |z| (\cos \theta + j \sin \theta)$$

$$\sin \theta = \frac{e^{j\theta} - e^{-j\theta}}{2j}$$

$$\text{rotation matrix: } \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} = \begin{bmatrix} a & -b \\ b & a \end{bmatrix}$$

$$\cos \theta = \frac{e^{j\theta} + e^{-j\theta}}{2}$$

## ④ Phasors

$$V(t) = V_0 \cos(\omega t + \phi_0)$$

$$i(t) = I_0 \cos(\omega t + \phi_i)$$

 $V_0, I_0$ : amplitude $\omega$ : angular frequency $\phi$ : phase shift

$$\omega = 2\pi f \quad \text{cycles/sec}$$

$$f = \frac{1}{T} \quad \text{period}$$

$$\cos(\theta) = \frac{1}{2} (e^{j\theta} + e^{-j\theta})$$

$$V(t) = V_0 \cos(\omega t + \phi) = \text{Re}(V_0 e^{j(\omega t + \phi)}) = \text{Re}(V_0 e^{j\phi} e^{j\omega t})$$

Phasor: not time dependent  $\vec{V} = V_0 e^{j\phi}$ 

$$V_0 \cos(\omega t + \phi) = \frac{1}{2} (\vec{V} e^{j\omega t} + \vec{V}^* e^{-j\omega t})$$

$$\sin(t + \frac{\pi}{2}) = \cos(t)$$

Impedance: depend on  $j\omega$   $Z = \frac{\vec{V}}{\vec{I}}$ 

$$\text{Resistor: } Z_R = R$$

$$\text{Capacitor: } Z_C = \frac{1}{j\omega C}$$

$$\text{Inductor: } Z_L = j\omega L$$

Transfer function:

$$H(j\omega) = \frac{V_{out}(\omega)}{V_{in}(\omega)}$$

KCL works for phasors

 $\omega$  is constant throughout

## ⑤ Circuit Filters

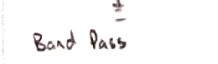
$$H(\omega) = |H(\omega)| e^{j\phi} \quad \text{magnitude of transfer func}$$

- Express sinusoidal input as phasors (coefficient of  $e^{j\omega t}$ )
- Solve output  $V/I$  phasors as func of input phasor
- Determine transfer func

Look at magnitude/phase shift of transfer func at input freq



$$H(\omega) = \frac{Z_2}{Z_1 + Z_2}$$



$$H(\omega) = \frac{1}{1 + j\omega/\omega_c}$$

$$H(\omega) = \frac{j\omega/\omega_c}{1 + j\omega/\omega_c}$$



$$H(\omega) = 1$$

$$H(\omega) = 1$$

Unity Gain Buffer to access output voltage of filter w/o drawing current, prevent second loading first

Make current draw low by increasing impedance

$$f_{cutoff} = \frac{1}{2\pi RC}$$

Bode Plots:

log-log plot (Magnitude  $H(\omega)$ ) Phase of  $H(\omega)$  angle-log plot

$$\frac{d}{dt} x(t) = \lambda x(t)$$

$$x(t) = x(0)e^{\lambda t}$$

$$\frac{d}{dt} x(t) = \lambda x(t) + \alpha$$

$$x(t) = x(0)e^{\lambda t} + \frac{\alpha}{\lambda}(e^{\lambda t} - 1)$$

$$\frac{d}{dt} x(t) = \lambda x(t) + u(t)$$

$$x(t) = x(0)e^{\lambda t} + \int_0^t u(\tau)e^{\lambda(t-\tau)} d\tau$$

Change of variables  $\tilde{V}_{out} = V_{out} - V_{in}$

$\omega_c$ : cutoff freq

$$\omega_c \text{ st } |H(\omega_c)| = \frac{1}{\sqrt{2}} |H(\omega_c)_{max}| \quad \left| \frac{1}{RC} \text{ or } \frac{R}{L} \right|$$

If transfer functions in series w/ unity gain buffers, we can multiply transfer fncs

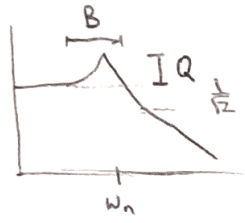
### Resonance

$\lambda \rightarrow$  real = decay "envelop"  
 $\lambda \rightarrow$  imaginary = oscillation

Impedance - generalized resistance  $[Z]$   $Z = R + jX$   
 Resistance Reactance

$\xi = \frac{1}{2} \frac{R}{\sqrt{L/C}}$  "damping ratio"

$$Q = \frac{1}{2\xi}$$



$$\text{Bandwidth } B = \frac{\omega_n}{Q} = 2\omega_n \xi$$

Resonance frequency:  $\frac{1}{\sqrt{LC}}$  when impedances of inductor and capacitor are equal

For differential equation  $\frac{d^2}{dt^2} x(t) + a \frac{d}{dt} x(t) + b x(t) = 0$

$$\lambda^2 + a\lambda + b = 0 \quad \lambda = \frac{-a \pm \sqrt{a^2 - 4b}}{2}$$

1) Critically damped:  $a^2 - 4b = 0$

2) Undamped:  $a$  is 0

3) Underdamped:  $a^2 - 4b < 0$

4) Overdamped:  $a^2 - 4b > 0$

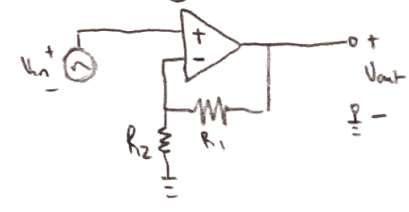
repeated eigenvalue, real  
 eigenvalues purely imaginary  
 eigenvalues complex, real and imag  
 eigenvalues purely real

### Circuits

Unity Gain Buffer:  $\frac{V_{out}}{V_{in}} = 1$



Non-Inverting Amplifier:  $V_{out} = V_{in} (1 + \frac{R_1}{R_2})$



$$i(0) = N = 0 = j\omega L = 0$$

Inductors = short circuit

Capacitors = open circuit

NMOS  $\rightarrow \frac{1}{H}$

PMOS  $\rightarrow \frac{1}{H}$

High = 1	1
Low = 0	0

High = 1	0
Low = 0	1

$$\cos(x) = \sin(x + \frac{\pi}{2})$$

$$\sin(x) = \cos(x - \frac{\pi}{2})$$

### Phasors

1) Adopt cosine reference (time domain)

2) Transfer to phasor domain

$$\begin{aligned} i &\rightarrow \tilde{I} & L &\rightarrow Z_L = j\omega L \\ v &\rightarrow \tilde{V} & C &\rightarrow Z_C = \frac{1}{j\omega C} \\ R &\rightarrow Z_R = R \end{aligned}$$

3) Cast Equations in phasor form

4) Solve for unknown

5) Transform back to Time domain

$$\begin{aligned} i &= \text{Re}[\tilde{I}e^{j\omega t}] \\ &= I \cos(\omega t - 105^\circ) \end{aligned}$$

### Units

$m = 10^{-3}$	$k = 10^3$
$\mu = 10^{-6}$	$M = 10^6$
$n = 10^{-9}$	$G = 10^9$
$p = 10^{-12}$	$T = 10^{12}$

6A State Space Models

State variables: internal variable representing state of a dynamic system

State vector: vector of state variables

State model: vector differential equation of vector

General form State Equations:  $n$  states and  $m$  inputs

$$\frac{d}{dt} \vec{x}(t) = f(\vec{x}(t), \vec{u}(t)) \quad \text{where } \vec{x} = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}, \vec{u} = \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_m \end{bmatrix}$$

$$\text{linear: } \frac{d}{dt} \vec{x}(t) = A \vec{x}(t) + B \vec{u}(t) \quad A \in \mathbb{R}^{n \times n} \quad B \in \mathbb{R}^{n \times m}$$

Equilibrium State: for all  $t \geq t_0$ , remains at  $\vec{x}^*$

$$\frac{d}{dt} \vec{x}(t) = f(\vec{x}^*) = 0, \quad \vec{x}(t) = \vec{x}^* \quad t \geq t_0$$

6B Equilibrium & Linearization

Linear if:  
1) Scaling  $f(ax) = af(x)$   
2) Additivity  $f(x+y) = f(x) + f(y)$

Linear systems w/ inputs @ equilibrium: constant  $\vec{u}$

$$A \vec{x} + B \vec{u} = 0$$

Linearization: approx nonlinear system

$$\text{Taylor: } f(x) \approx f(x^*) + \nabla f(x)|_{x=x^*} (x - x^*)$$

Jacobian:  $\nabla f(\vec{x}) = \begin{bmatrix} \frac{\partial f_1(x_1, x_2, \dots, x_n)}{\partial x_1} & \frac{\partial f_1(x_1, x_2, \dots, x_n)}{\partial x_2} & \dots & \frac{\partial f_1(x_1, x_2, \dots, x_n)}{\partial x_n} \\ \frac{\partial f_2(x_1, x_2, \dots, x_n)}{\partial x_1} & \frac{\partial f_2(x_1, x_2, \dots, x_n)}{\partial x_2} & \dots & \frac{\partial f_2(x_1, x_2, \dots, x_n)}{\partial x_n} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial f_n(x_1, x_2, \dots, x_n)}{\partial x_1} & \frac{\partial f_n(x_1, x_2, \dots, x_n)}{\partial x_2} & \dots & \frac{\partial f_n(x_1, x_2, \dots, x_n)}{\partial x_n} \end{bmatrix}$

$\vec{x}^*$  is equilibrium

$$\frac{d}{dt} \vec{x}(t) = f(\vec{x}(t)) \quad f(\vec{x}^*) = 0 \quad \tilde{x}(t) := \vec{x}(t) - \vec{x}^*$$

$$A \equiv \nabla f(\vec{x})|_{\vec{x}=\vec{x}^*} \quad \frac{d}{dt} \tilde{x}(t) \approx A \tilde{x}(t)$$

7A Linearization & Discrete-Time Systems

Linearizing systems w/ inputs: equilibrium  $\vec{x}^*$  and  $\vec{u}^*$   $f(\vec{x}^*, \vec{u}^*) = 0$

$$\frac{d}{dt} \vec{x}(t) = f(\vec{x}(t), \vec{u}(t)) \quad \vec{x}(t) := \vec{x}(t) - \vec{x}^* \quad \vec{u}(t) := \vec{u}(t) - \vec{u}^*$$

2) Find  $\nabla_x f(\vec{x}, \vec{u})$  and  $\nabla_u f(\vec{x}, \vec{u})$  set

$$A := \nabla_x f(\vec{x}, \vec{u})|_{\vec{x}=\vec{x}^*, \vec{u}=\vec{u}^*} \quad B := \nabla_u f(\vec{x}, \vec{u})|_{\vec{x}=\vec{x}^*, \vec{u}=\vec{u}^*}$$

3) Linearization:  $\frac{d}{dt} \tilde{x}(t) \approx A \tilde{x}(t) + B \tilde{u}(t)$

Discrete Time System: evolves w/ difference equation

$$\tilde{x}[t+1] = A \tilde{x}[t] + B \tilde{u}[t]$$

7B Discretization

Changing State Variables: transform to  $\tilde{z}$

$$1) \tilde{z} := T \tilde{x}$$

$$2) A_{\tilde{z}} = T A T^{-1} \quad B_{\tilde{z}} = T B$$

$$3) \frac{d}{dt} \tilde{z}(t) = A_{\tilde{z}} \tilde{z}(t) + B_{\tilde{z}} \tilde{u}(t)$$

$$x(kT+T) - x(kT) = \int_{kT}^{kT+T} \dot{x}(s) ds$$

Digital Control: continuous vs. discrete

input is sampled every  $T$  units time  $\vec{x}(0), \vec{x}(T), \vec{x}(2T)$

$$\vec{x}_d[k] := \vec{x}(kT)$$

$$\vec{u}(t) = \vec{u}_d[k] + t \in [kT, (k+1)T]$$

cont  $\rightarrow$  Discrete



Discrete  $\rightarrow$  Continuous



Discretization w/ single state single input

$$x_1(k+1) = A_d x_1(k) + B_d u_d(k)$$

$$\frac{d}{dt} x(t) = \lambda x(t) + b u(t)$$

$$x_1(k+1) = \lambda_d x_1(k) + b_d u_d(k)$$

$$\text{where } \lambda_d = e^{\lambda T} \quad b_d = b \int_0^T e^{\lambda s} ds = \begin{cases} bT & \text{if } \lambda = 0 \\ \frac{b(e^{\lambda T} - 1)}{\lambda} & \text{if } \lambda \neq 0 \end{cases}$$

8A Controllability

$$\text{let } A = \begin{bmatrix} \lambda_1 & & \\ & \ddots & \\ & & \lambda_n \end{bmatrix} \quad B = \begin{bmatrix} b_1 \\ \vdots \\ b_n \end{bmatrix} \quad \text{let } A_d = \begin{bmatrix} e^{\lambda_1 T} & & \\ & \ddots & \\ & & e^{\lambda_n T} \end{bmatrix} \quad B_d = \begin{bmatrix} \int_0^T e^{\lambda_1 s} ds b_1 \\ \vdots \\ \int_0^T e^{\lambda_n s} ds b_n \end{bmatrix}$$

Using  $\tilde{z} = V^{-1} \vec{x}$  where  $V$  is eigenvectors

$$\tilde{z}[k+1] = A_d \tilde{z}[k] + B_d V^{-1} B u_d[k]$$

$$\tilde{x}_d[k] = V \tilde{z}_d[k]$$

$$\tilde{x}_d[k+1] = V A_d V^{-1} \tilde{x}_d[k] + V B_d V^{-1} B u_d[k]$$

Controllability

$$\vec{x}(t) = A^t \vec{x}(0) + [B \quad AB \quad \dots \quad A^{t-1}B \quad A^{t-2}B \quad \dots \quad A^0B] \begin{bmatrix} \vec{u}(t-1) \\ \vec{u}(t-2) \\ \vdots \\ \vec{u}(1) \\ \vec{u}(0) \end{bmatrix}$$

If there exists  $t$  and input sequence  $\vec{u}(0), \vec{u}(1), \dots, \vec{u}(t-1)$  such that  $\vec{x}(t) = \vec{x}_{\text{target}}$  then it is controllable

$$\text{Controllability} \Leftrightarrow \text{span} \{ \vec{b}, A\vec{b}, \dots, A^{n-1}\vec{b}, A^{n-2}\vec{b}, \dots, A^0\vec{b} \} = \mathbb{R}^n$$

8B System Identification

$y \in \mathbb{R}^1$  measurements  $\rightarrow \hat{y} = D \hat{p} + \tilde{e}$   $\leftarrow$  measurement error  $m \times n$   
 $k$ th matrix  $\leftarrow$  unknown parameters  $m > n$

Given:  $x(t+1) = \lambda x(t) + b u(t) + e(t)$

Scalar:  $\begin{bmatrix} x(0) \\ x(1) \\ \vdots \\ x(L-1) \end{bmatrix} \begin{bmatrix} 1 \\ \lambda \\ \vdots \\ \lambda^{L-1} \end{bmatrix} + \begin{bmatrix} b \\ b\lambda \\ \vdots \\ b\lambda^{L-1} \end{bmatrix} \begin{bmatrix} u(0) \\ u(1) \\ \vdots \\ u(L-1) \end{bmatrix} = \begin{bmatrix} x(1) \\ x(2) \\ \vdots \\ x(L) \end{bmatrix}$

vector:  $\tilde{x}(k) = \tilde{x}(k-1)^T A^T + \tilde{u}(k-1)^T B^T + \tilde{e}(k-1)^T$

$$\begin{bmatrix} \tilde{x}(0)^T \\ \tilde{x}(1)^T \\ \vdots \\ \tilde{x}(L-1)^T \end{bmatrix} \begin{bmatrix} A^T \\ A^T B^T \\ \vdots \\ A^T B^T \end{bmatrix} + \begin{bmatrix} \tilde{e}(0)^T \\ \tilde{e}(1)^T \\ \vdots \\ \tilde{e}(L-1)^T \end{bmatrix} = \begin{bmatrix} \tilde{x}(1)^T \\ \tilde{x}(2)^T \\ \vdots \\ \tilde{x}(L)^T \end{bmatrix}$$

$$\tilde{P} = (D^T D)^{-1} D^T \tilde{y}$$

9A Singular Value Decomposition (SVD)

SVD separates rank  $r$  matrix  $A \in \mathbb{R}^{m \times n}$  into sum of  $r$  rank 1

Find  $D$  orthonormal vectors  $\vec{v}_1, \dots, \vec{v}_r \in \mathbb{R}^n$

2) orthonormal vectors  $\vec{v}_1, \dots, \vec{v}_r \in \mathbb{R}^n$

3) real positive numbers  $\sigma_1, \dots, \sigma_r$   $\sigma_1 \geq \sigma_2 \geq \dots \geq \sigma_r > 0$

$$A = \sigma_1 \vec{v}_1 \vec{v}_1^T + \sigma_2 \vec{v}_2 \vec{v}_2^T + \dots + \sigma_r \vec{v}_r \vec{v}_r^T$$

Orthonormal: columns  $a_i$  are

1) Orthogonal,  $\langle a_i, a_j \rangle = 0 \quad i \neq j$



## 9B Finding SVD

Using  $A^T A$

- 1) Find eigenvalues of  $A^T A$ ,  $\lambda_1 \geq \lambda_2 \geq \dots \geq \lambda_r > 0$ ,  $(A - \lambda I) = 0$
- 2) Find orthonormal eigenvectors  $\vec{v}_i$ , (plug in  $(A - \lambda I)$  matrix and find where  $= \vec{0}$ )  
 $A^T A \vec{v}_i = \lambda_i \vec{v}_i$
- 3) Let  $\sigma_i = \sqrt{\lambda_i}$ , get  $\vec{u}_i$   
 $\vec{u}_i = \frac{1}{\sigma_i} A \vec{v}_i$   $i = 1, \dots, r$

Using  $A A^T$

- 1) Find eigen values of  $A A^T$
- 2) Find orthonormal eigenvectors  $\vec{u}_i$   
 $A A^T \vec{u}_i = \lambda_i \vec{u}_i$
- 3) Let  $\sigma_i = \sqrt{\lambda_i}$  get  $\vec{v}_i$   
 $\vec{v}_i = \frac{1}{\sigma_i} A^T \vec{u}_i$   $U^T U = I$   
 $V^T V = I$

## 11A SVD Cont.

min:  $A = U \Sigma V^T$

$\begin{bmatrix} \vec{u}_1 & \dots & \vec{u}_r & \dots & \vec{u}_m \end{bmatrix}_{m \times m}$ 
 $\Sigma = \begin{bmatrix} \sigma_1 & 0 & 0 \\ & \ddots & \\ 0 & \sigma_r & 0 \\ 0 & \dots & 0 \end{bmatrix}_{m \times n}$ 
 $\begin{bmatrix} \vec{v}_1 & \dots & \vec{v}_r & \dots & \vec{v}_n \end{bmatrix}_{n \times n}$

$\forall U$  and  $V$  must be orthonormal so append orthonormal basis if needed

Geometric Interpretation:

$A\vec{x}$  composition of

- 1)  $V^T \vec{x}$ : reorients  $\vec{x}$  w/o changing length
  - 2)  $\Sigma V^T \vec{x}$ : stretches along axis w/ singular value
  - 3)  $U \Sigma V^T \vec{x}$ : reorients vector w/o changing length
- if  $\|\vec{x}\| = 1$  then  $\|A\vec{x}\| \leq \sigma_1$ , for  $\vec{x} = \vec{v}_1$ ,  $\|A\vec{x}\| = \sigma_1$

Symmetric Matrices:  $Q = Q^T$  (Spectral Theorem)

Symmetric Matrix has real eigenvalues, real orthonormal eigenvectors

- real eigen values
- real orthonormal eigenvectors
- diagonalizable ( $A = V \Lambda V^T$ )

Rank-Nullity Theorem:

For  $A = n \times m$

$$\text{rank}(A) + \text{Null}(A) = m$$

$$(AB)^T = B^T A^T$$

If  $Q$  can be written as  $Q = R^T R$  for some  $R$ , eigenvalues are nonnegative

## General

- Stable if eigenvalue  $< 1$
- Plugging into  $x$  with  $\theta$  iter  $\begin{bmatrix} \cos(\theta) \\ \sin(\theta) \end{bmatrix}$  gives eigenvectors
- inverse of orthogonal matrix is same as transpose

## Controllability

To reach  $x(n)$ :

$$\begin{bmatrix} u(n-1) \\ \vdots \\ u(0) \end{bmatrix} = \begin{bmatrix} \vec{b} & A\vec{b} & \dots & A^{n-1}\vec{b} \end{bmatrix}^{-1} \vec{x}(n)$$

11B Applications of SVD

Least Squares with SVD

tall matrix  $m \times n$ ,  $m > n$ 

$$A = U \begin{bmatrix} S \\ 0_{(m-n) \times n} \end{bmatrix} V^T$$

$$y = Ax + \tilde{e}$$

$$\hat{x} = VS^{-1}U^T y$$

Minimum Norm Solution

wide matrix  $m \times n$ ,  $m < n$ Many choices for  $\hat{x}$  so we want to choose shortest length

$$A = U \begin{bmatrix} S & 0_{m \times (n-m)} \end{bmatrix} V^T \quad \hat{y} = Ax = USV^T \hat{x}$$

$$\hat{x} = VS^{-1}U^T \hat{y}$$

$$V = \begin{bmatrix} v_1 & v_2 \\ 1 & 1 \end{bmatrix} \quad V^T = \begin{bmatrix} -v_1 & -v_2 \\ -v_1 & -v_2 \end{bmatrix}$$

Principal Component Analysis (PCA)

finds most informative directions in a data set

1) From each measurement subtract avg  $A \in \mathbb{R}^{m \times n}$ 2) "covariance matrix":  $\frac{1}{m-1} A^T A$  :  $n \times n$  matrixEigenvalues of matrix are singular values of  $A$  except for scaling factor  $m-1$ Orthogonal eigenvectors correspond to  $\vec{v}_1, \vec{v}_2, \dots, \vec{v}_n$  of SVD

Eigen vectors corresponding to largest singular values are principle components and identify dominant directions

12A Min Energy / Stability

Use min norm

have

$$\begin{bmatrix} \text{Purser} \\ 0 \end{bmatrix} = \underbrace{\begin{bmatrix} \vec{0} & A\vec{0} & \dots & A^{k-1}\vec{0} \end{bmatrix}}_{C_k} \begin{bmatrix} u_k(k-1) \\ u_k(k-2) \\ \vdots \\ u_k(0) \end{bmatrix}$$

to get desired state in  $k$  time steps

$$\begin{bmatrix} u(k-1) \\ u(k-2) \\ \vdots \\ u(0) \end{bmatrix} = \underbrace{C_k^T (C_k C_k^T)^{-1}}_F \begin{bmatrix} \text{Purser} \\ 0 \end{bmatrix}$$

Controllability matrix target state vector

Stability of Linear State Models

System:  $x(t+1) = Ax(t) + bu(t)$ 

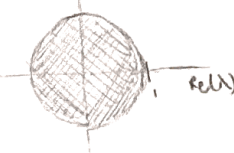
$$x(t) = A^t x(0) + A^{t-1} bu(0) + A^{t-2} bu(1) + \dots + bu(t-1)$$

$$x(t) = A^t x(0) + \sum_{k=0}^{t-1} A^{t-1-k} bu(k)$$

Stability: Stable:  $x(t)$  is bounded for any initial and bounded inputUnstable: can find initial and bounded input st  $|x(t)| \rightarrow \infty$  as  $t \rightarrow \infty$  $|A| > 1$ : unstable -  $|A|^t$  grows unbounded  $|A|^t |x(0)| \rightarrow \infty$  $|A| < 1$ : Stable -  $|\sum_{k=0}^{t-1} A^{t-1-k} bu(k)| \leq |b| M \sum_{k=0}^{t-1} |A|^k \rightarrow \frac{1}{1-|A|}$  $|A| = 1$ : "marginal stability" - if  $b=0$ :  $|A^t x(0)| \rightarrow |x(0)|$  else  $b \neq 0$  unbounded

Vector Case

$$x(t+1) = Ax(t) + Bu(t) \quad \hat{x}(t) = A^t x(0) + \sum_{k=0}^{t-1} A^{t-1-k} Bu(k)$$

 $|A_i| < 1$  for all eigenvalues: stable $|A_i| > 1$  for at least one eigenvalue: unstablecontrollable  $\Rightarrow$  stabilizablestabilizable  $\nRightarrow$  controllable12B StabilityDiscrete  $z$ -planeStable:  $|A| < 1$ 

Transient Behavior

Oscillates if has imaginary

grows unbounded if outside stability zone

converges if inside stability zone

$$x(t) = e^{At} x(0) + \int_0^t e^{A(t-s)} u(s) ds$$

Continuous  $s$ -planeStable:  $\text{Re}\{\lambda\} < 0$ 13A State Feedback Control

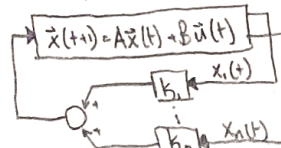
$$\hat{x}(t+1) = A\hat{x}(t) + B\hat{u}(t) \quad \text{choose } \hat{u} = K\hat{x}$$

$$\text{then } \hat{x}(t+1) = (A+BK)\hat{x}(t)$$

Choose  $K$  so all eigenvalues inside unit circle

Closed Loop Control

Can shape transients (well damped conv)



Open Loop Control

Sensitive to disturbances

 $u(0), u(1), \dots$ 

$$\hat{x}(t+1) = A\hat{x}(t) + B\hat{u}(t)$$

1) Find  $A+BK$ 

$$\begin{bmatrix} a_{11} + b_1 k_1 & a_{12} + b_1 k_2 \\ a_{21} + b_2 k_1 & a_{22} + b_2 k_2 \end{bmatrix} \quad BK = \begin{bmatrix} b_1 & b_2 \end{bmatrix} \begin{bmatrix} k_1 \\ k_2 \end{bmatrix}$$

2) Find eigenvalues/equation

$$\lambda_1 = 1+k_1, \quad \lambda_2 = 2$$

$$\lambda^2 - (\lambda_1 + \lambda_2)\lambda + \lambda_1 \lambda_2$$

3) Solve for values of  $k$  / or declare unstable $|\lambda_2| > 1$  unstable13B Feedback, Controller Canonical Form

Controller Canonical Form

$$A_c = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 0 & 1 \\ a_1 & a_2 & \dots & a_{n-1} & a_n \end{bmatrix} \quad B_c = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

$$\det(\lambda I - A) = \lambda^n - a_n \lambda^{n-1} - a_{n-1} \lambda^{n-2} - \dots - a_1$$

$$\det(\lambda I - (A_c + B_c K)) = \lambda^n - (a_n + k_n) \lambda^{n-1} - (a_{n-1} + k_{n-1}) \lambda^{n-2} - \dots - (a_1 + k_1)$$

Can tune each  $k$  value by the coefficient of polynomial to reach any set of eigenvaluesIf system is controllable, can assign eigenvalues of  $A+BK$  with choices of  $K$ 

-CCF has eigenvalues on bottom row

## 14A Upper Triangularization

- $N \times N$  matrix is diagonalizable (values only in diagonal) if it has  $n$  linearly independent eigenvectors, distinct eigenvalues
- Any square matrix can be upper triangular
- Upper triangular matrix has eigenvalues along diagonal

## Gram-Schmidt Process

Algo takes linearly independent vectors  $\{s_1, \dots, s_n\}$  and generates an orthonormal set of vectors  $\{q_1, \dots, q_n\}$  that span same space

1) Find unit vector  $\vec{q}_1$   $\text{span}(\{q_1\}) = \text{span}(\{s_1\})$

$$\vec{q}_1 = \frac{\vec{s}_1}{\|\vec{s}_1\|}$$

2) Find  $\vec{q}_2$

- ① Span same
- ② orthogonal
- ③ normal

$$z_2 = \vec{s}_2 - \alpha \vec{q}_1 \quad ①$$

get orthogonal vector with OMP

$$\text{proj}_{\vec{q}_1} \vec{s}_2 = \vec{q}_1 \vec{q}_1^T \vec{s}_2 \vec{q}_1 \quad ② \quad \vec{z}_2 = \vec{s}_2 - \vec{q}_1 \vec{q}_1^T \vec{s}_2 \vec{q}_1$$

$$③ \quad \vec{q}_2 = \frac{\vec{z}_2}{\|\vec{z}_2\|}$$

Algo

$$\vec{q}_1 = \frac{\vec{s}_1}{\|\vec{s}_1\|}$$

for  $i=2 \rightarrow n$ :

$$\vec{z}_i = \vec{s}_i - \sum_{j=1}^{i-1} (\vec{s}_i^T \vec{q}_j) \vec{q}_j$$

$$\vec{q}_i = \frac{\vec{z}_i}{\|\vec{z}_i\|}$$

## Conceptual

PCA: How to approx higher dimension data into lower dimension essence. First Principle Component is which 1D line best approx, by projecting data points onto it

SVD: Decompose  $A$  into sum of rank 1 matrices  
ith rank 1 matrix formed from taking outer product of normalized column vectors  $\vec{u}_i$  and normalized row vectors  $\vec{v}_i^T$  scaled by  $\sigma_i$ .  
Adding each matrix for singular value on top of each other

Phasors: By converting to phasor domain, you take snapshot of time domain, solve it relative to snapshot and phasor extends to all phases so you can convert back to time domain, and result will describe solution