Advanced Dynamics & Automatic Control

Root Locus

Dr. Mitch Pryor

THE UNIVERSITY OF TEXAS AT AUSTIN

Lesson Objective

- Understand how Root Locus can be a useful tool for understanding controllers in the frequency domain (using an illustrative example)
- Find the value of a parameter of interest which makes a system go from a stable to unstable response.

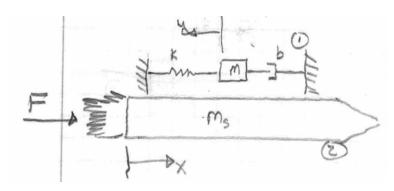
Recall our awesome rocket sled...



http://www.sandia.gov/vqsec/SON-ST.html

Rocket Sled, Review

Find the open loop transfer function T(s) for a rocket sled.



$$m\frac{d^2(x+y)}{dt^2} + b\frac{dy}{dt} + ky = 0$$
 (1)

$$M_s \frac{d^2 y}{dt^2} = F(t)$$
 (2)

Plug (2) into (1)

$$\frac{d^2y}{dt^2} + \frac{b}{m}\frac{dy}{dt} + \frac{k}{m}y = -\frac{F(t)}{M_s}$$

Let,
$$Q(s) = -\frac{F(t)}{M_s}$$

$$s^{2}Y(s) + 3sY(s) + 2Y(s) = Q(s)$$

$$T(s) = \frac{output}{input} = \frac{Y(s)}{Q(s)} = \frac{1}{s^2 + 3s + 2}$$

Recall, T(s) is the ratio of the output/input for a system given all initial conditions are zero.

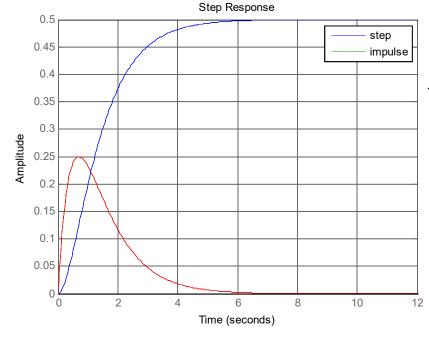
Rocket Sled

$$T(s) = \frac{1}{s^2 + 3s + 2}$$

```
num = [1]
den = [ 1 3 2 ]

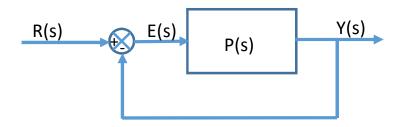
sys = tf( num, den )

hold on;
impulse(sys, 'r')
step(sys, 'b')
legend('step', 'impulse');
```



Our open loop zero frequency gain is 0.5 since our reference input was 1.

Rocket Sled with Unity Feedback



$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{P(s)}{1 + P(s)}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{1}{s^2 + 3s + 2}}{1 + \frac{1}{s^2 + 3s + 2}}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{1}{s^2 + 3s + 2}}{1 + \frac{1}{s^2 + 3s + 2}} \frac{s^2 + 3s + 2}{s^2 + 3s + 2}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{1}{s^2 + 3s + 2 + 1}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{1}{s^2 + 3s + 3}$$

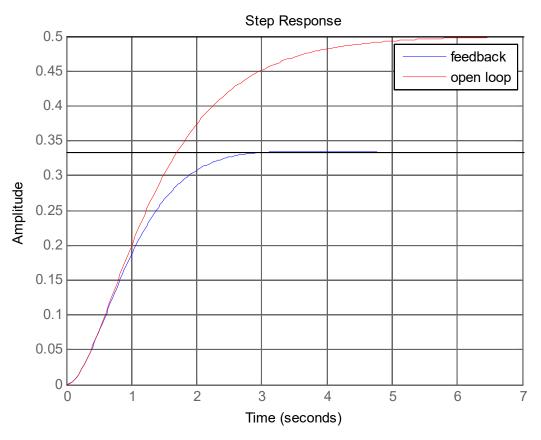
Rocket Sled with Feedback

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{1}{s^2 + 3s + 3}$$

```
clear all;
num = [1];
den = [ 1 3 2 ];
numfb = [ 1 ];
denfb = [ 1 3 2+1 ];

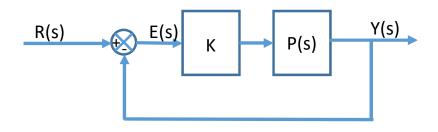
sys = tf( num, den );
sysfb = tf( numfb, denfb );

hold on; grid on;
step( sysfb, 'b' );
step( sys, 'r' );
legend('feedback', 'open loop');
```



Simple unity feedback didn't really help, and the zero frequency gain is lower.

Rocket Sled with Amplified Feedback



$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{K P(s)}{1 + K P(s)}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{K}{s^2 + 3s + 2}}{1 + \frac{K}{s^2 + 3s + 2}}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{K}{s^2 + 3s + 2}}{1 + \frac{K}{s^2 + 3s + 2}} \frac{s^2 + 3s + 2}{s^2 + 3s + 2}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{K}{s^2 + 3s + 2 + K}$$

What is the zero frequency gain as the gain approaches infinity?

Are there practical limits to what the maximum gain can be?

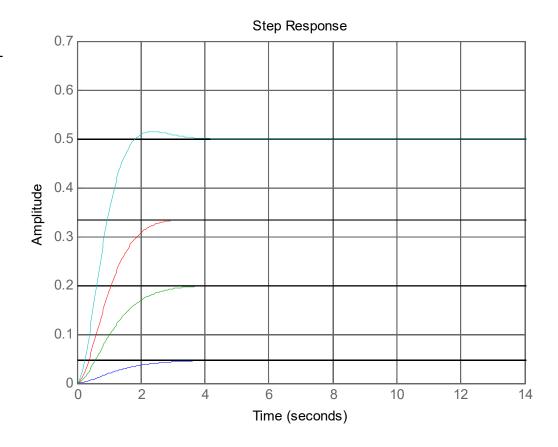
Robot sled with amplified feedback

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{K}{s^2 + 3s + 2 + K}$$

```
clear all;

K = [ .1 .5 1 2 ];

for i=1:length(K)
    numfb = [ K(i) ];
    denfb = [ 1 3 2+K(i) ];
    sysfb = tf( numfb, denfb );
    hold on;
    step( sysfb );
end
hold off; grid on;
```

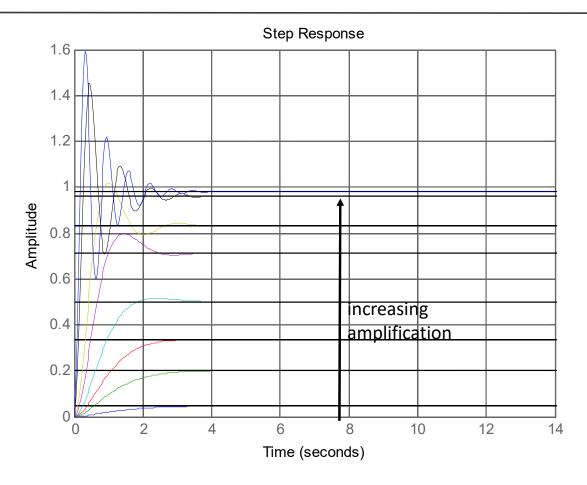


Robot sled with amplified feedback

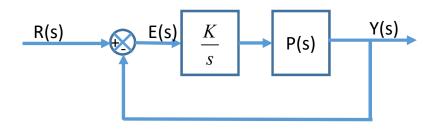
$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{K}{s^2 + 3s + 2 + K}$$

```
clear all;
K = [ .1 .5 1 2 5 10 50 100 ];

for i=1:length(K)
    numfb = [ K(i) ];
    denfb = [ 1 3 2+K(i) ];
    sysfb = tf( numfb, denfb );
    hold on;
    step( sysfb );
end
hold off; grid on;
```



Recall that integrators eliminate steady-state error



$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{K}{s}P(s)}{1 + \frac{K}{s}P(s)}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{K}{s^3 + 3s^2 + 2s}}{1 + \frac{K}{s^3 + 3s^2 + 2s}}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{\frac{K}{s^3 + 3s^2 + 2s}}{1 + \frac{K}{s^3 + 3s^2 + 2s}} \frac{s^3 + 3s^2 + 2s}{s^3 + 3s^2 + 2s}$$

$$T_{cl}(s) = \frac{Y(s)}{R(s)} = \frac{K}{s^3 + 3s^2 + 2s + K}$$

What is the zero frequency gain as the gain approaches infinity?

More simply, what is the zero frequency gain?

Now amplify the feedback

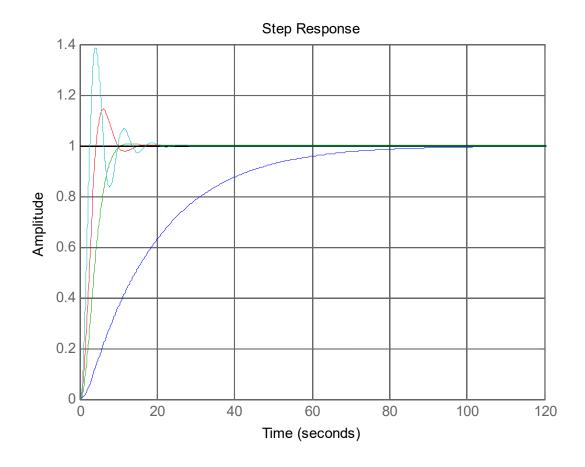
$$T_{OL}(s) = \frac{1}{s(s^2 + 3s + 2)}$$

$$T_{CL}(s) = \frac{K}{s^3 + 3s^2 + 2s + K}$$

```
clear all;

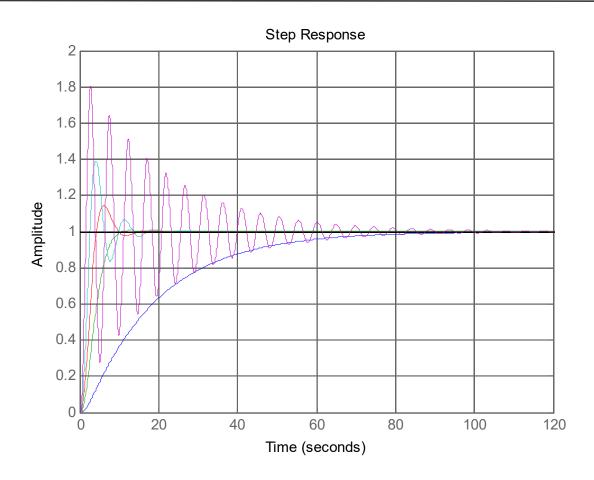
K = [ .1 .5 1 2 ];

for i=1:length(K)
    numfb = [ K(i) ];
    denfb = [ 1 3 2 K(i) ];
    sysfb = tf( numfb, denfb );
    hold on;
    step( sysfb );
end
hold off; grid on;
```



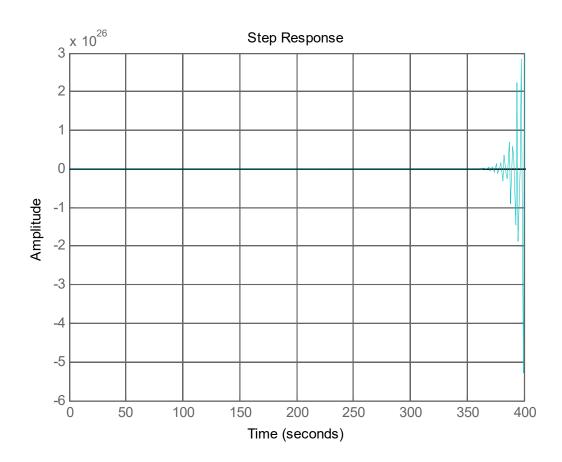
Really amplify the feedback

```
clear all;
K = [ .1 .5 1 2 5 ];
for i=1:length(K)
    numfb = [ K(i) ];
    denfb = [ 1 3 2 K(i) ];
    sysfb = tf( numfb, denfb );
    hold on;
    step( sysfb );
end
hold off; grid on;
```

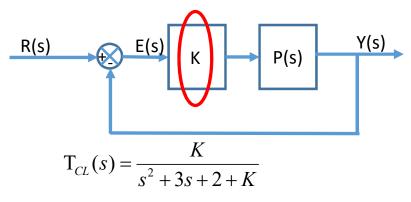


Really, REALLY amplify the feedback

```
clear all;
K = [ .1 .5 1 2 5 10 ];
for i=1:length(K)
   numfb = [ K(i) ];
   denfb = [ 1 3 2 K(i) ];
   sysfb = tf( numfb, denfb );
   hold on;
   step( sysfb );
end
hold off; grid on;
```



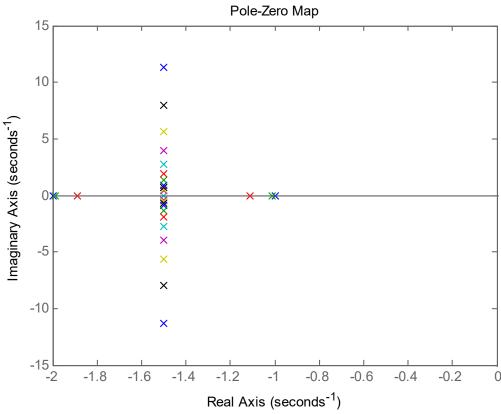
Poles for different gains



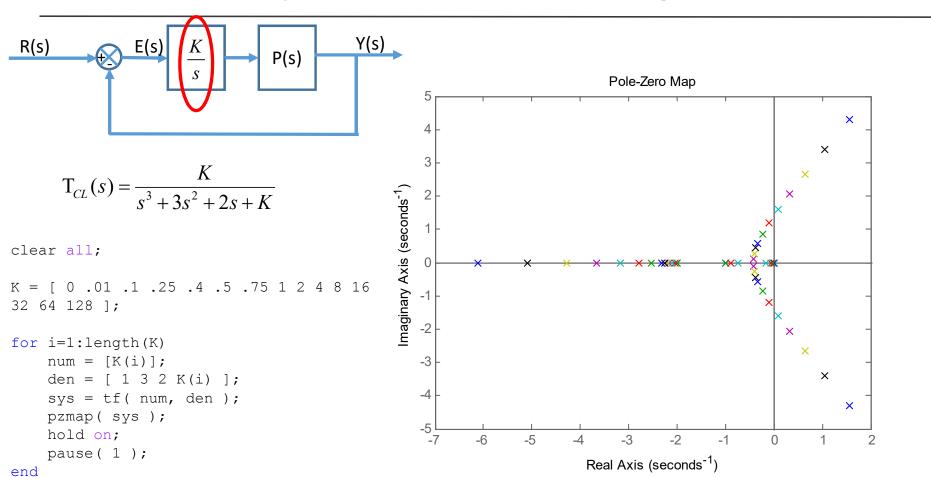
```
clear all;

K = [ 0 .01 .1 .25 .4 .5 .75 1 2 4 8 16
32 64 128 ];

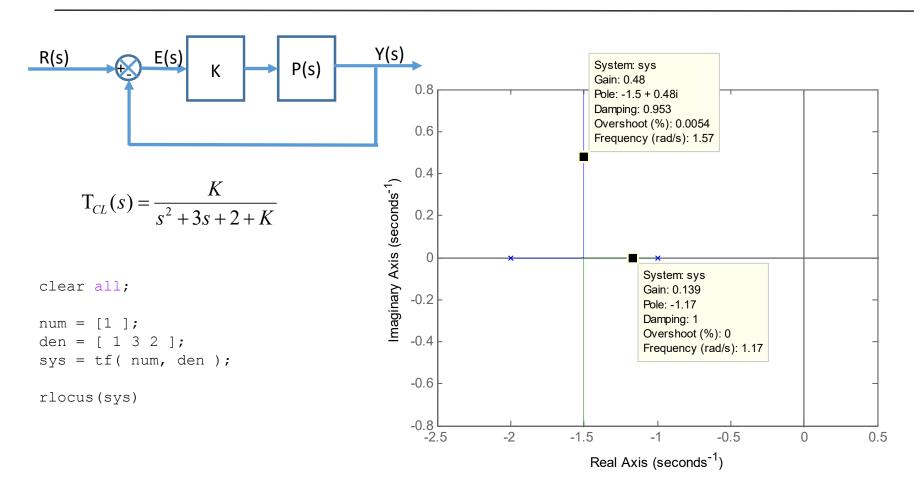
for i=1:length(K)
   num = [K(i)];
   den = [ 1 3 2+K(i) ];
   sys = tf( num, den );
   pzmap( sys );
   hold on;
   pause( 1 );
end
```



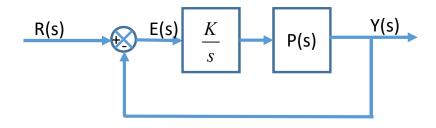
And in the system with the integrator...



Example: Root Locus

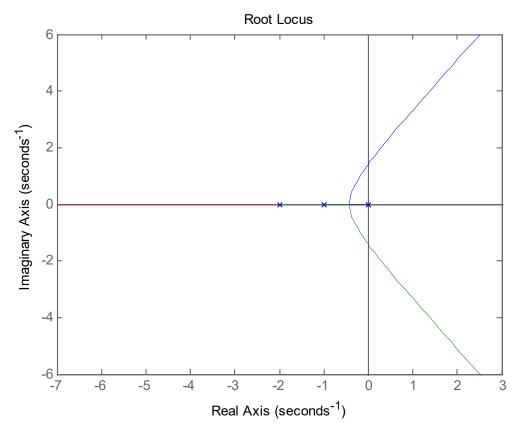


Example: Root Locus



$$T_{CL}(s) = \frac{K}{s^3 + 3s^2 + 2s + K}$$

```
clear all;
num = [1 ];
den = [ 1 3 2 0 ];
sys = tf( num, den );
rlocus(sys)
```



Root Locus relates Gains, Poles & Zeros

$$G(s) = C(sI - A)^{-1}B + D = \frac{\text{num}(s)}{\text{den}(s)} = K \frac{\text{num'}(s)}{\text{den'}(s)}$$

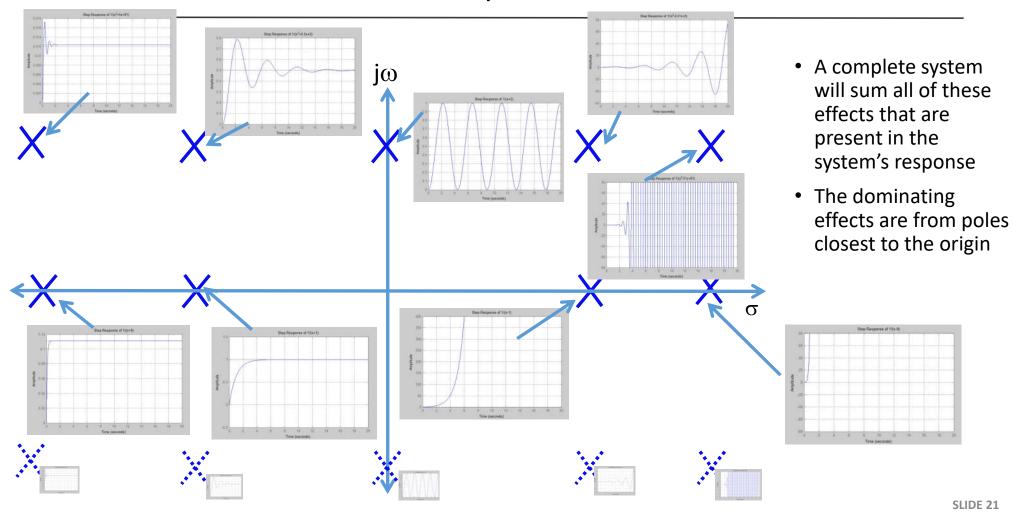
- Denominator roots are the system "poles"
 - Poles associated with the modes of the system
 - and the eigenvalues from state-space representation
- Numerator roots are the system "zeros"
 - Zeros counteract the effect of a pole at a given location
- The variable s is a complex number $(0+j\omega)$ for sinusoidal input
- The value of G(0) is the zero frequency or steady state gain of the system

$$G(0) = D - CA^{-1}B = \frac{y_o}{u_o} = \frac{b_1 0^m + b_2 0^{m-1} + \dots + b_m}{a_1 0^n + a_2 0^{n-1} + \dots + a_n} = \frac{b_m}{a_n}$$

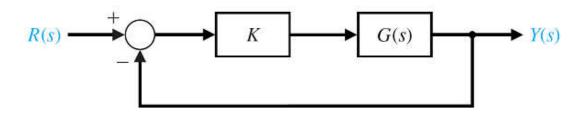
Using Root Locus

- We can use the block diagrams to design simple (and eventually complex) controllers for systems modeled in the Laplace domain.
- In many cases, the parameter we need to quantify is an amp gain that determines the response and stability of the feedback system.
 - But it can be tedious to find this gain value via trial and error.
- Root Locus is a plot of the systems transfer function on a complex plane,
 - We can manual plot the root locus by incrementally increasing the parameter of interest
 - MATLAB has several functions (rlocus, rlocfind, rltool, zpk, pzmap, pzplot, etc.) to find (or help find) the Root Locus
 - We have a step by step procedure to find it more intuitively by hand
- We can quickly examine the impact of adding zeros or poles to the system as a control strategy.

Root Locus Factor Responses



The root locus plot



- The root locus plots system response as a function of positive real values of K.
- With unity negative feedback, the closed loop transfer function is

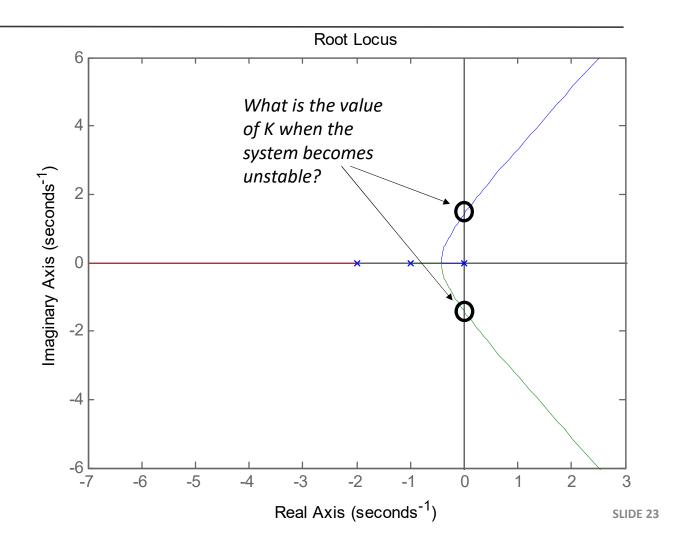
$$\frac{Output(s)}{Input(s)} = \frac{KG(s)}{1 + KG(s)} = \frac{K\frac{N_G(s)}{D_G(s)}}{1 + K\frac{N_G(s)}{D_G(s)}} = \frac{KN_G(s)}{D_G(s) + KN_G(s)}$$

- The characteristic equation is $\Delta(s) = 1 + KG(s) = D_G(s) + KN_G(s)$
- MATLAB makes the rlocus relatively easy to find
 - rlocus, rlocfind, rltool, zpk, pzmap, pzplot, etc.
- It is (relatively) easy and useful to sketch the Root Locus.

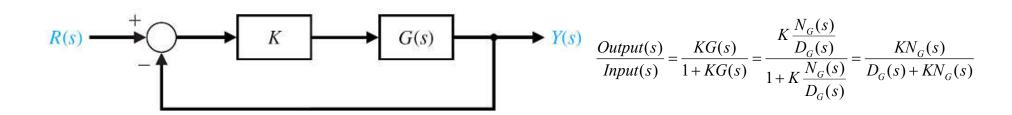
...But first...

```
T_{CL}(s) = \frac{K}{s^3 + 3s^2 + 2s + K}
```

```
clear all;
num = [1 ];
den = [ 1 3 2 0 ];
sys = tf( num, den );
rlocus(sys)
```



Necessary but NOT sufficient



- The Characteristic Equation (CE) is $\Delta(s) = 1 + KG(s) = D_G(s) + KN_G(s)$
- It is necessary but not sufficient for all the coefficients of the CE to be nonzero and the same sign

Definitely unstable

$$\Delta(s) = s^5 + 4s^4 - s^3 + 3s^2 + s + 1$$

$$\Delta(s) = s^5 + 4s^4 + s^3 + 3s^2 + s + 1$$

Possibly stable

$$\Delta(s) = s^5 + 4s^4 + s^3 + 3s^2 + s + 1$$

Hurwitz Criteria (necessary & sufficient)

$$\Delta(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_2 s^2 + a_1 s + a_0$$

Is defined using the following set of determinants:

$$\mathbf{D}_1 = \left| a_{n-1} \right|$$

$$\mathbf{D}_2 = \begin{bmatrix} a_{n-1} & a_n \\ a_{n-3} & a_{n-2} \end{bmatrix}$$

$$\mathbf{D}_{3} = \begin{bmatrix} a_{n-1} & a_{n} & 0 \\ a_{n-3} & a_{n-2} & a_{n-1} \\ a_{n-5} & a_{n-4} & a_{n-3} \end{bmatrix}$$

Or more generally

$$\mathbf{D}_{n-1} = \begin{bmatrix} a_{n-1} & a_n & \cdots & 0 \\ a_{n-3} & a_{n-2} & \cdots & \vdots \\ \vdots & \vdots & \cdots & \vdots \\ \vdots & \vdots & \cdots & \vdots \\ 0 & 0 & \cdots & a_0 \end{bmatrix}$$

:

Note: the transpose of a matrix has the same determinant. So some books/sites set up the matrices using differently, but all should give the same result.

Hurwitz Criteria, cont'd

$$\Delta(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_2 s^2 + a_1 s + a_0$$

All Hurwitz determinants must be positive for a system to be stable. This criterion is both sufficient and necessary.

Quick example:

R(s) E(s)
$$\frac{s+40}{s(s+10)}$$
 Y(s)
$$\frac{K}{s+20}$$

$$T_{cl}(s) = \frac{\frac{s+40}{s(s+10)}}{1 + \frac{K(s+40)}{s(s+10)(s+20)}}$$

$$\Delta(s) = s(s+10)(s+20) + K(s+40)$$
$$= s^3 + 30s^2 + (200 + K)s + 40K$$

Hurwitz Criteria, cont'd

$$\Delta(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_2 s^2 + a_1 s + a_0$$

Quick example cont'd
$$\Delta(s) = s^3 + 30s^2 + (200 + K)s + 40K$$

Necessary but not sufficient: 200 + K > 0

Necessary AND sufficient: $\mathbf{D}_1 = |a_{n-1}| = 30$ >0 so always true.

$$\mathbf{D}_{2} = \begin{bmatrix} a_{n-1} & a_{n} \\ a_{n-3} & a_{n-2} \end{bmatrix} = \begin{bmatrix} a_{2} & a_{3} \\ a_{1} & a_{0} \end{bmatrix} = \begin{bmatrix} 30 & 1 \\ 40K & 200 + K \end{bmatrix}$$

Therefore:

$$6000 + 30K - 40K > 0$$
$$600 > K$$

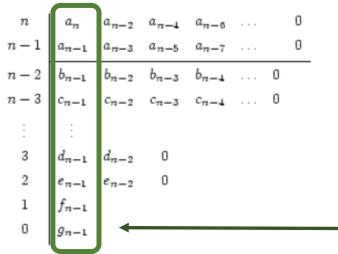
Thus the system is stable for all 0<*K*<600.

At this gain, at least one pole resides in the right hand plane of the Root Locus.

Routh Criterion

$$\Delta(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_2 s^2 + a_1 s + a_0$$

The Routh Schema contains n+1 rows organized in the following manner...



System is stable *if and only if* all elements in the first column of the Routh schema are positive.

Where the values of the third row and beyond are found using...

$$b_{n-1} = \frac{a_{n-1}a_{n-2} - a_n a_{n-3}}{a_{n-1}} \qquad c_{n-1} = \frac{b_{n-1}a_{n-3} - a_{n-1}b_{n-2}}{b_{n-1}}$$

$$b_{n-2} = \frac{a_{n-1}a_{n-4} - a_n a_{n-5}}{a_{n-1}} \qquad c_{n-2} = \frac{b_{n-1}a_{n-5} - a_{n-1}b_{n-3}}{b_{n-1}}$$

$$b_{n-3} = \frac{a_{n-1}a_{n-6} - a_n a_{n-7}}{a_{n-1}} \qquad c_{n-3} = \frac{b_{n-1}a_{n-7} - a_{n-1}b_{n-4}}{b_{n-1}}$$

$$c_{n-1} = \frac{b_{n-1}a_{n-3} - a_{n-1}b_{n-2}}{b_{n-1}}$$

$$f_{n-1} = \frac{e_{n-1}d_{n-2} - d_{n-1}e_{n-2}}{e_{n-1}}$$

$$c_{n-2} = \frac{b_{n-1}a_{n-5} - a_{n-1}b_{n-3}}{b_{n-1}} \dots$$

$$g_{n-1} = e_{n-2}$$

Most dynamical systems are not an extremely high order...

Routh Criterion, cont'd

Let's do a quick example

$$\Delta(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_2 s^2 + a_1 s + a_0$$

= $s^3 + 2s^2 + 4s + 9$

Where the values of the third row and beyond are found using...

$$n = 3$$
: 1 4
 $n = 2$: 2 9
 $n = 1$: -0.5 0
 $n = 0$: 9 0

Note $b_{n-2}=b_1$ is zero since there is not a_{n-4} or a_{n-5}

Note $c_{n-2} = c_1$ is zero since there is no b_{n-1} or b_{n-3}

The system is unstable since not all elements in the first column have the same sign. $c_{n-3} = \frac{b_{n-1}a_{n-7} - a_{n-1}b_{n-4}}{b_{n-1}}$

$$b_{n-1} = \frac{a_{n-1}a_{n-2} - a_na_{n-3}}{a_{n-1}}$$

$$b_{n-2} = \frac{a_{n-1}a_{n-4} - a_na_{n-5}}{a_{n-1}}$$

$$b_{n-3} = \frac{a_{n-1}a_{n-6} - a_na_{n-7}}{a_{n-1}}$$

$$c_{n-1} = \frac{b_{n-1}a_{n-3} - a_{n-1}b_{n-2}}{b_{n-1}}$$

$$c_{n-2} = \frac{b_{n-1}a_{n-5} - a_{n-1}b_{n-3}}{b_{n-1}}$$

$$c_{n-3} = \frac{b_{n-1}a_{n-7} - a_{n-1}b_{n-3}}{b_{n-1}}$$

Routh Criterion, cont'd

Let's do an example with a parameter of interest:

$$\Delta(s) = a_n s^n + a_{n-1} s^{n-1} + \dots + a_2 s^2 + a_1 s + a_0$$

= $s^3 + 2s^2 + (5+K)s + 3K$

Where the values of the third row and beyond are found using...

$$n = 3$$
: 1 5 + K
 $n = 2$: 2 3 K
 $n = 1$: 5 - 2 K 0

$$n = 0$$
: $3K$ 0

Note $b_{n-2}=b_1$ is zero since there is not a_{n-4} or a_{n-5}

Note $c_{n-2} = c_1$ is zero since there is no b_{n-1} or b_{n-3}

The system is only stable if 0<K<2.5!

$$b_{n-1} = \frac{a_{n-1}a_{n-2} - a_na_{n-3}}{a_{n-1}}$$

$$b_{n-2} = \frac{a_{n-1}a_{n-4} - a_na_{n-5}}{a_{n-1}}$$

$$b_{n-3} = \frac{a_{n-1}a_{n-6} - a_na_{n-7}}{a_{n-1}}$$

: .

$$c_{n-1} = \frac{b_{n-1}a_{n-3} - a_{n-1}b_{n-2}}{b_{n-1}}$$

$$c_{n-2} = \frac{b_{n-1}a_{n-5} - a_{n-1}b_{n-3}}{b_{n-1}}$$

$$c_{n-3} = \frac{b_{n-1}a_{n-7} - a_{n-1}b_{n-4}}{b_{n-1}}$$

Summary

- The Root locus can tell us a lot about the performance of a system over the range of a parameter of interest including a controller gain.
- A critical value is one where the system goes from stable to unstable.
 - MATLAB's rlocus(sys) function produces an interactive plot
 - The Hurwitz and Routh Criteria provide some analytical methods to determine this critical value.
 - Gonna leave the theory related to Hurwitz numbers for another course (or you can productively procrastinate with a little Googling...)
- Coming up! How to create the Root Locus by hand!
 - Learn more about the impact of poles and zeros (even from a proposed controller)