

HW#3 - Joseph Speed

1)



$$F_{\text{drag}} = -Kv$$

$$K > 0$$

m_i = initial mass, m_0 = final mass (no fuel)
 u = speed of fuel

$$F = ma = \text{thrust} - \text{drag}$$

$$\frac{(m_i - m_0)}{K} \propto \frac{1}{\alpha}$$

$$ma = u \frac{dm}{dt} - Kv$$

$$F = \frac{dp}{dt} \Rightarrow F dt = dp \Rightarrow dp = (p(t+dt) - p(t))$$

$$p(t+dt) = (m_i - dm)(v_0 + dv) + dm(v_0 - u)$$

$$p(t) = m_i v_0$$

2 small things each other

$$dp = m_i v_0 + m_i dv - dm v_0 - dm dv + dm v_0 - dm u - m_i v_0$$

$$F dt = m dv - dm u$$

$$-Kv dt = m dv - dm u \Rightarrow dm u = m dv + Kv dt$$

$$\Rightarrow m u = m v + Kv \Rightarrow m v = u m - Kv$$

$$dM = -dm$$

$$g) \dot{M} = -\alpha \Rightarrow \dot{m} = \alpha$$

$$M \dot{v} = u \alpha - Kv \Rightarrow M \frac{dv}{dt} = u \alpha - Kv \Rightarrow \frac{M dv}{u \alpha - Kv} = dt$$

$$m_i - m_0 = \alpha t; \text{ + need to go to when fuel is all used up } t_0 = \frac{m_i - m_0}{\alpha}$$

$$M = m_i - \alpha t \leftarrow M \text{ is a function of time}$$

$$\frac{M dv}{u \alpha - Kv} = dt \Rightarrow \int_0^{v_0} \frac{M dv}{u \alpha - Kv} = \int_0^{t_0} dt \Rightarrow \frac{1}{K} \left[\ln(u \alpha - Kv) \right]_0^{v_0} = t_0$$

$$= \frac{1}{\alpha} \left[\ln(m_i - \alpha t) \right]_0^{t_0} \Rightarrow \frac{1}{\alpha} \left(\ln(m_i - \alpha t_0) - \ln(m_i - 0) \right)$$

(2) Dimensional analysis for $\left(\frac{K}{\alpha}\right)$

(1) need to use v_0, v_0 & t_0, t_0 for units derived in $\ln(\dots)$

HW 3 - cont

$$\begin{aligned} 1a) \quad \frac{1}{K} (\alpha x - b v_0 - 1) &= \frac{1}{\alpha} (\ln(mi - m_i + m_0) - \ln(mi)) \\ &= \frac{1}{K} (\ln(\alpha x - b v_0) - 1) = \frac{1}{\alpha} \ln\left(\frac{m_0}{mi}\right) \Rightarrow \frac{\alpha}{K} \ln(\alpha x - b v_0) - \frac{1}{K} = \ln\left(\frac{m_0}{mi}\right) \\ \Rightarrow (\alpha x - b v_0)^{\frac{\alpha}{K}} e^{\frac{1}{K}} &= \frac{m_0}{mi} \Rightarrow (\alpha x - b v_0)^{\frac{\alpha}{K}} = \frac{m_0}{mi} e^{-\frac{1}{K}} \end{aligned}$$

$$Mi = \alpha x - b v, \quad M = mi - \alpha t, \quad \alpha t_0 = mi - m_0 \Rightarrow t_0 = \frac{mi - m_0}{\alpha}$$

$$(mi - \alpha t) \frac{dv}{dt} = \alpha x - b v \Rightarrow (mi - \alpha t) dv = (\alpha x - b v) dt$$

$$\Rightarrow \frac{dv}{(\alpha x - b v)} = \frac{dt}{(mi - \alpha t)} \Rightarrow \int_{v_0}^{v_g} \frac{dv}{(\alpha x - b v)} = \int_{t_0}^{t_g} \frac{dt}{mi - \alpha t}$$

$$\Rightarrow \frac{-1}{b} (\ln(\alpha x - b v_g) - \ln(\alpha x - b v_0)) = \frac{-1}{\alpha} (\ln(mi - \alpha t_g) - \ln(mi - \alpha t_0))$$

$$\Rightarrow \ln\left(\frac{\alpha x - b v_g}{\alpha x - b v_0}\right) = \frac{K}{\alpha} \ln\left(\frac{mi - \alpha t_g}{mi - \alpha t_0}\right) \Rightarrow \ln\left(\frac{\alpha x - b v_g}{\alpha x - b v_0}\right) = \ln\left(\frac{mi - \alpha t_g}{mi - \alpha t_0}\right)^{\left(\frac{K}{\alpha}\right)}$$

$$\Rightarrow \frac{\alpha x - b v_g}{\alpha x - b v_0} = \left(\frac{mi - \alpha t_g}{mi - \alpha t_0}\right)^{\left(\frac{K}{\alpha}\right)} \quad \text{plugging in initial conditions}$$

$$\Rightarrow \frac{\alpha x - b v_g}{\alpha x} = \left(\frac{mi - \alpha \left(\frac{mi - m_0}{\alpha}\right)}{mi}\right)^{\left(\frac{K}{\alpha}\right)} \Rightarrow 1 - \frac{b v_g}{\alpha x} = \left(\frac{mi - mi + m_0}{mi}\right)^{\left(\frac{K}{\alpha}\right)}$$

$$\Rightarrow 1 - \frac{b v_g}{\alpha x} = \left(\frac{m_0}{mi}\right)^{\left(\frac{K}{\alpha}\right)} \Rightarrow \alpha x - b v_g = \alpha x \left(\frac{m_0}{mi}\right)^{\left(\frac{K}{\alpha}\right)}$$

$$\Rightarrow \alpha x - \alpha x \left(\frac{m_0}{mi}\right)^{\left(\frac{K}{\alpha}\right)} = b v_g \Rightarrow v_g = \frac{\alpha x}{b} - \frac{\alpha x}{b} \left(\frac{m_0}{mi}\right)^{\left(\frac{K}{\alpha}\right)}$$

$$\Rightarrow v_g = \frac{\alpha x}{b} \left(1 - \left(\frac{m_0}{mi}\right)^{\left(\frac{K}{\alpha}\right)}\right) \quad \leftarrow \text{dimensional work}$$

HW#3

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$$c) v_g = \frac{u\alpha}{k} \left(1 - \left(\frac{m_0}{m_i} \right)^{\left(\frac{k}{\alpha} \right)} \right) \quad \frac{m}{\alpha} \cdot \frac{k_0}{\alpha} / \frac{k_0}{\alpha} \left(1 - \left(\frac{k_0}{k_0} \right)^{\left(\frac{k_0}{\alpha} / \frac{k_0}{\alpha} \right)} \right)$$

units work out & makes physical sense,

$\uparrow \alpha$, faster : $\uparrow k$, slower

- $\frac{m_0}{m_i}$ tells ratio of how much fuel we can use & this to the exponent $\left(\frac{k}{\alpha} \right)$ & subtracted from 1 means the higher k is, the slower we go $\left(1 - \left(\frac{m_0}{m_i} \right)^{\frac{k}{\alpha}} \right)$ means we'll have a lower total which makes sense
- increasing α means higher end total $\left(1 - \frac{m_0}{m_i} \left(\frac{k}{\alpha} \right) \right)$ & this makes sense etc the faster we burn fuel, the less time drag has to act

$$d) \text{ match eq 6 } : v = v_0 - u \ln \left(\frac{m}{m_0} \right), \text{ use Taylor approx of } \ln(x)$$

Taylor expansion of A^x about $x=0$

$$\text{Derivative of } A^x = A^x \ln A$$

$$f(x) \approx 1 + f'(x)x + \dots \quad A^x \approx 1 + A^x \ln(A)x + \dots$$

$$\therefore \left(\frac{m_0}{m_i} \right)^{\left(\frac{k}{\alpha} \right)} \approx 1 + \left(\frac{m_0}{m_i} \right)^{\left(\frac{k}{\alpha} \right)} \ln \left(\frac{m_0}{m_i} \right) \left(\frac{k}{\alpha} \right) + \dots$$

Plugging in

$$v_g = \frac{u\alpha}{k} \left(1 - \left(1 + \left(\frac{m_0}{m_i} \right)^{\left(\frac{k}{\alpha} \right)} \ln \left(\frac{m_0}{m_i} \right) \left(\frac{k}{\alpha} \right) \right) \right) \quad \text{since } \frac{k}{\alpha} \approx 0, \left(\frac{m_0}{m_i} \right)^{\left(\frac{k}{\alpha} \right)} \approx 1$$

$$\Rightarrow v_g = \frac{u\alpha}{k} \left(1 - \left(1 + \ln \left(\frac{m_0}{m_i} \right) \left(\frac{k}{\alpha} \right) \right) \right) \Rightarrow v_g = \frac{u\alpha}{k} \left(\frac{k}{\alpha} \ln \left(\frac{m_0}{m_i} \right) \right)$$

$$\Rightarrow v_g = u \ln \left(\frac{m_0}{m_i} \right)$$

$$+kx = m_i - m_f \quad \alpha = \frac{m_i \cdot m_f}{t_0}$$

$$\Rightarrow v_g = -u \ln \left(\frac{m_i}{m_0} \right)$$

HW#3

1a) $v_0 = -u \ln\left(\frac{m}{m_0}\right)$ make equal to $v = v_0 - u \ln\left(\frac{m}{m_0}\right)$

or us, $v_0 = 0$ & $m = m_0$, so $v = -u \ln\left(\frac{m}{m_0}\right)$

in this case $v_0 = v = -u \ln\left(\frac{m}{m_0}\right)$

these equations are the same in this situation

2) generally $v = v_0 - u \ln\left(\frac{m}{m_0}\right)$

v_0 reduces to this because the force equation is

eq 4/5 $\rightarrow m\dot{v} = u\dot{m} \Rightarrow m \frac{dv}{dt} = u \frac{dm}{dt} \Rightarrow m dv = u dm$
- Kr force

$\Rightarrow dv = \frac{u dm}{m} \Rightarrow \int_{v_0}^{v_0} dv = u \int_{m_0}^{m_0} \frac{dm}{m} \Rightarrow v_0 - v_0 = u \ln\left(\frac{m}{m_0}\right)$

$\Rightarrow v_0 = v_0 + u \ln\left(\frac{m}{m_0}\right) \Rightarrow v_0 = v_0 - u \ln\left(\frac{m_0}{m}\right)$

if b is small, then the $(-bv)$ term drops out in the original equation & then it simplifies down to eq 6

b/a also ≈ 0 if $b \ll a$, so the old expression is still valid

HW 163

b) $F(x, y, z) = -a(x^M i + y^N j + z^P k)$ $\vec{F} = -a \vec{\nabla} f$ $U = -af$

a) $F(x, y, z)$ conservative if

$$\frac{\partial M}{\partial y} = \frac{\partial N}{\partial x} \quad \frac{\partial N}{\partial z} = \frac{\partial P}{\partial y} \quad \frac{\partial M}{\partial z} = \frac{\partial P}{\partial x}$$

$$\frac{\partial M}{\partial y} = 0 = \frac{\partial N}{\partial x} \quad \frac{\partial N}{\partial z} = 0 = \frac{\partial P}{\partial y} \quad \frac{\partial M}{\partial z} = 0 = \frac{\partial P}{\partial x}$$

$$F_x = -ax \Rightarrow f_x = \int x dx = \frac{x^2}{2} + g(y, z) + C$$

$$F_y = -ay \Rightarrow f_y = \int y dy = \frac{y^2}{2} + g(x, z) + C$$

$$F_z = -az \Rightarrow f_z = \int z dz = \frac{z^2}{2} + g(x, y) + C$$

$$f = f_x + f_y + f_z = \frac{x^2}{2} + y^2 + \frac{z^2}{2} + C$$

$$\text{Potential function } U = -a\left(\frac{x^2}{2} + y^2 + \frac{z^2}{2}\right) + C$$

A 3-D spring w/ different spring constants in each direction would give the potential function

HW #3

30) $F(x, y, z) = (-y, x, 0)$

$\frac{\partial F_x}{\partial y} = -1 \neq \frac{\partial F_y}{\partial x} = 1$ Fails test, is not conservative

4) $F(x, y, z) = (2xz^3 + 2axy^3, 2ayz^3 + 2ay^4 + 3ax^2y^2 + 3ay^4, 3ax^2y^2 + 3ay^3z^2)$

$\frac{\partial F_x}{\partial y} = 6axy^2 = \frac{\partial F_y}{\partial x}, \frac{\partial F_x}{\partial z} = 6xz^2 = \frac{\partial F_z}{\partial x}, \frac{\partial F_y}{\partial z} = 6ayz^2 = \frac{\partial F_z}{\partial y}$

$\vec{F}(x, y, z) = -a \vec{\nabla} f(x, y, z) \quad U = a f(x, y, z)$

$F_x = 2xz^3 + 2axy^3 \Rightarrow a_x = \int (2xz^3 + 2xy^3) dx = x^2z^3 + x^2y^3 + g(y, z) + C$

$F_y = 2ayz^3 + 2ay^4 + 3ax^2y^2 + 3ay^4 \Rightarrow a_y = \int (2yz^3 + 3x^2y^2 + 5y^4) dy$
 $= y^2z^3 + x^2y^3 + y^5 + g(x, z) + C$

$F_z = 3ax^2y^2 + 3ay^3z^2 \Rightarrow a_z = \int (3x^2y^2 + 3y^3z^2) dz = x^2y^3 + y^3z^3 + g(x, y) + C$

$a = (a_x \cup a_y \cup a_z) + C = x^2y^3 + x^2y^3 + y^2z^3 + y^5 + C$

$U = a(x^2y^3 + x^2y^3 + y^5 + y^2z^3 + y^3) + C$

? do we need a constant

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1) $\vec{F}(\vec{r}) = (Ay^2, By^3, 2Axy)$

$\vec{F} = -\vec{\nabla} U$

a) $\frac{\partial F_x}{\partial y} = 0 = \frac{\partial F_z}{\partial x}, \frac{\partial F_x}{\partial y} = 2Ay = \frac{\partial F_z}{\partial x}, \frac{\partial F_y}{\partial z} = 0 = \frac{\partial F_z}{\partial y} \checkmark \text{ conservative}$

$F_x = Ay^2, \phi_x = A \int y^2 dx \Rightarrow Ax y^2 + g(y, z) + C$

$F_y = By^3, \phi_y = B \int y^3 dy \Rightarrow B y^4/4 + g(x, z) + C$

$F_z = 2Axy, \phi_z = 2A \int xy dz \Rightarrow Axy^2 + g(x, y) + C$

$U = \phi_x \cup \phi_y \cup \phi_z = Ax y^2 + B \frac{y^4}{4} + C = 0$

2) $\vec{F} = m\vec{a} = m\vec{v}' = m \frac{d\vec{v}}{dt}$

$m d\vec{v} = \vec{F} dt \Rightarrow m \int_{\vec{v}_0}^{\vec{v}_t} d\vec{v} = \int_0^t (Ay^2, By^3, 2Axy) dt$

$\Rightarrow m(\vec{v}_t - \vec{v}_0) = (Ay^2 t, By^3 t, 2Axy t)$

$\Rightarrow \vec{v}_t = \vec{v}_0 + (Ay^2 t, By^3 t, 2Axy t) / m$

@ $\hat{r} = -\hat{i} + 2\hat{j} + \hat{k}$

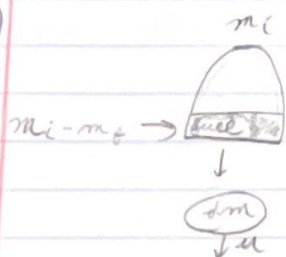
$\Rightarrow \vec{v}_t = \vec{v}_0 + (At, 8Bt, -2At) / m$

$\Rightarrow |\vec{v}_t| = \sqrt{v_0^2 + \frac{A^2 t^2}{m^2} + 64 \frac{B^2 t^2}{m^2} + 4 \frac{A^2 t^2}{m^2}} = \sqrt{v_0^2 + \frac{5A^2 t^2 + 64B^2 t^2}{m^2}}$

$|\vec{v}_t| = \sqrt{v_0^2 + \frac{t^2}{m^2} (5A^2 + 64B^2)}$

HW #3

2)



$\downarrow \theta/6 = \theta_c \quad \theta = -9.21$

$$a) \cancel{m \dot{x}} = u \cancel{m \dot{x}} - m g_e \Rightarrow m \frac{dx}{dt} = u \frac{dm}{dt} - m g_e \Rightarrow m dx = u dm - m g_e dt$$

~~$\frac{dr}{dt} = 0$ etc v doesn't change $dv = 0$~~

$$\Rightarrow u dm = \rho g_e dt \Rightarrow \int_{m_i}^{m_f} u dm = g_e \int_0^{t_f} m dt$$

$$F = ma = \mu m - mg \Rightarrow a = \frac{\mu m}{m} - g, a = 0 \text{ want to stay still}$$

$$g_e = \frac{u}{m} \frac{dm}{dt} \Rightarrow g_e dt = \frac{u}{m} dm \Rightarrow g_e \int_0^T dt = u \int_{m_i}^{m_f} \frac{1}{m} dm$$

$$\Rightarrow q_e t_e = u (\ln(m_0) - \ln(m_i)) \Rightarrow q_e t_e = u \ln\left(\frac{m_0}{m_i}\right) \Rightarrow t_e = \frac{u}{q_e} \ln\left(\frac{m_0}{m_i}\right)$$

$$t_0 = \frac{u}{g} \ln\left(\frac{m_B}{m_i}\right)$$

units make sense & $\left[\frac{m}{s} / \frac{m}{s^2} = s \right]$ & the last must

② the ent, the more fuel is used the greater the mag of en, but it is negative. However ρ_c is negative, so they cancel out to give a $t_0 > 0$

$$c) t_0 = \frac{1500}{g} \ln\left(\frac{2}{3}\right) = \frac{1500 \text{ m/s}^2}{-1.635 \text{ m/s}^2} \cdot -0.40546 = 371.99 \text{ s}$$

$$t_g = 371.99 \text{ s}$$

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s)



$$d) F = \frac{dp}{dt} \Rightarrow F dt = dp \Rightarrow dp = (p_f - p_i)$$

$$\Rightarrow p_f = (m_0 + \sigma dt)(v_0 + dv) = m_0 v_0 + v_0 \sigma dt + m dv = \sigma dt dv$$

$$p_i = m_0 v_0$$

$$dp = v_0 \sigma dt + m dv$$

etc

$$\Rightarrow F = 0, \text{ on ice so no friction } \& \quad \Sigma F_y = 0$$

$$\Rightarrow 0 = v_0 \sigma dt + m dv \Rightarrow m dv = -v_0 \sigma dt \Rightarrow m \int_{v_0}^{v_f} dv = -v_0 \sigma \int_0^{t_f} dt$$

$$\Rightarrow m_0 (v_f - v_0) = -v_0 \sigma t_f \Rightarrow \boxed{v_f = v_0 - \frac{v_0 \sigma t_f}{m_0}}$$

$$e) m \dot{v} dt = dp = (p_f - p_i)$$

$$p_f = m(v + dv) + dm(v - u) = mv + m dv + v dm - u dm$$

$$p_i = m v$$

$$dp = m dv + v dm - u dm$$

$$\Rightarrow 0 = m dv + v dm - u dm \Rightarrow m dv = u dm - v dm \Rightarrow m dv = (u - v) dm$$

$$\Rightarrow \frac{m}{u - v} dv = dm \Rightarrow \int_{v_0}^{v_f} \frac{m}{u - v} dv = \int_{m_0}^{m_f} dm \Rightarrow \int_{v_0}^{v_f} \frac{m_0}{u - v} dv = \sigma \int_0^{t_f} dt$$

$$\Rightarrow -m_0 (\ln(u - v_f) - \ln(u - v_0)) = \sigma t_f \Rightarrow \ln\left(\frac{u - v_f}{u - v_0}\right) = -\frac{\sigma t_f}{m_0}$$

$$\Rightarrow \frac{u - v_f}{u - v_0} = e^{-\frac{\sigma t_f}{m_0}} \Rightarrow u - v_f = (u - v_0) e^{-\frac{\sigma t_f}{m_0}} \Rightarrow v_f = u - (u - v_0) \exp\left(-\frac{\sigma t_f}{m_0}\right)$$

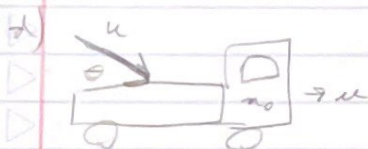
$$\boxed{v_f = u - (u - v_0) \exp\left(-\frac{\sigma t_f}{m_0}\right)} \quad v_f = u - \frac{(u - v_0)}{\exp\left(\frac{\sigma t_f}{m_0}\right)}$$

HW#3

5c) your slings have at least dm in the bucket, so



If the car is traveling at speed u already, once it gets another dm inside the pump, the speed slows to $P/(m_0 + dm)$ because momentum is conserved. Then once it ejects the dm , the speed goes to u again (P/m_0).



$$F dt = dp = (P_f - P_i)$$

$$P_f = (m_0 + \sigma dt)(v_0 + dv)$$

$$P_i = (m_0 v_0) + (u \sigma dt)$$

$$P_f = m_0 v_0 + m_0 dv + \sigma v_0 dt + \sigma dt dv$$

$$P_i = m_0 v_0 + u \sigma dt$$

$$dP = m_0 dv + \sigma v_0 dt - u \sigma dt$$

$$F = m \ddot{x} \Rightarrow \int \ddot{x} dt = \dot{x} \Rightarrow 0 = m_0 dv + \sigma v_0 dt - u \sigma dt$$

$$\Rightarrow -m_0 dv = \sigma (v_0 - u) dt \Rightarrow -m_0 \int_{v_0}^{v_f} dv = \sigma \int_0^{t_g} (v_0 - u) dt$$

$$\Rightarrow v_0 - v_f = \frac{\sigma}{m_0} \int_0^{t_g} (v_0 - u) dt \Rightarrow v_f = v_0 - \frac{\sigma (v_0 - u) t_g}{m_0}$$

$$v_f = v_0 - \frac{\sigma t_g (v_0 - u)}{m_0}$$

$$v_f = v_0 - \frac{\sigma t_g}{m_0} (v_0 - u)$$

If the component of u in the direction the truck is moving, is greater than the speed of the truck, it will help