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# Chapter 1

## Calorimeter R&D

### 1.1 Glass RPC SDHCAL

#### 1.1.1 Introduction

Hadronic calorimeter (HCAL) plays an essential role in PFA-based experiments as those proposed for the ILC. It allows to separate the deposits of charged and neutral hadrons and to precisely measure the energy of the neutrals. The contribution of the neutrals to the jet energy, around 10% on average, fluctuates in a wide range from event to event, and the accuracy of the measurement is the dominant contribution to the particle flow resolution for jet energies up to about 100 GeV. For higher energies, the performance is dominated by confusion, and both topological pattern recognition and energy information are important for correct track-cluster assignment. High-granularity hadronic calorimeter is thus needed to achieve excellent jet energy resolution. HCAL proposed for both projects of ILC (ILD and SiD), are sampling calorimeters with steel as absorber and scintillator tiles or gaseous devices with embedded electronics for the active part. The steel was chosen due to its rigidity which allows to build self-supporting structure without auxiliary supports (dead regions). Moreover, the moderate ratio of hadronic interaction length ( $\lambda_I = 17$  cm) to electromagnetic radiation length ( $X_0 = 1.8$  cm) of iron, allows a fine longitudinal sampling in terms of  $X_0$  with a reasonable number of layers in  $\lambda_I$ , thus keeping the detector volume and readout channel count small. This fine sampling is beneficial both for the measurement of the sizable electromagnetic energy part in hadronic showers as for the topological resolution of shower substructure, needed for particle separation. For the ILD project we propose gaseous detectors for the HCAL active layers: The Resistive Plate Chamber (RPC). This is motivated by the excellent efficiency and very good homogeneity the gaseous detectors could provide. Another important advantage of gaseous detectors is the possibility to have very fine lateral segmentation. Indeed, in contrast to scintillator tiles, the lateral segmentation of gaseous devices is determined by the electronics readout used to read them. Active layer thickness is also of importance for what concerns the ILC hadronic calorimeter to be placed inside the magnetic field. Highly efficient gaseous detectors can indeed be built with

a thickness of less than 3 mm. To obtain excellent resolution of hadronic shower energy measurement using a binary readout, a lateral segmentation of few millimeters is needed. This however leads to a huge number of electronics hardly affordable for the future ILC hadronic calorimeters.  $1 \times 1 \text{ cm}^2$  cells were found to be a good compromise that still provides very good resolution at moderate energies. However, simulation studies show that saturation effects are expected to show up at higher energies ( $> 50 \text{ GeV}$ ). This happens when many particles cross one cell in the center of the hadronic shower. To reduce these effects, the choice of multi-threshold electronics (Semi-Digital) readout was envisaged to improve on the energy resolution by exploiting the particle density in more appropriate way. High-granularity calorimeters imply however a huge number of electronics channels to operate them. This has two important consequences. The first is the power consumption and the resulting increase of temperature which affects the behavior of the active layers. The other consequence is the number of service cables needed to power, read out these channels. These two aspects can deteriorate the performance of the HCAL and destroy the principle of PFA if they are not addressed properly. The R&D pursued by the SDHCAL-GRPC groups has succeeded to pass almost all the technical hurdles of the PFA-based HCAL. The SDHCAL-GRPC groups have succeeded to build the first technological prototype of these new-generation calorimeters with 48 active layers of GRPC,  $1 \text{ m}^2$  each. The prototype validates the concept of high-granularity gaseous detector and permits to study the energy resolution of hadrons one can obtain with such calorimeter.

### 1.1.2 Readout Electronics

The readout electronics of the two Semi-Digital HCAL (SDHCAL) projects were developed in common. An ASIC called HARDROC was first developed to read out the G\_RPC detectors proposed for the ILD project. To solve the problem of connections related to the high number of electronics channels, the option of a detector embedded electronics using the DAISY chain scheme was chosen and Printed Circuit Board (PCB) were conceived for the readout of large detectors G\_RPC.

#### Front-end ASIC

The HARDROC chip (HR) implements a multi-threshold readout which integrates the functionalities of amplification, shaping, digitization, internal triggering and local storage of the data. Each of its 64 channels consists of a fast low impedance current preamplifier with 8-bit variable gain (in the  $[0, 2]$  range) followed by 3 fast shapers (15 ns shaping time). A low offset discriminator is present on each path and the three corresponding thresholds establish the multi-level readout. The thresholds are set using three integrated 10-bit Digital to Analog Converters (DAC). The outputs of the three discriminators are then encoded 3-to-2 bit and stored in an internal digital memory latched by a trigger event. A trigger is generated when one of the lowest level discriminators is fired but can also be configured on the other thresholds. A frame consists of the 64 encoded discriminator outputs, plus a 24-bit time-stamp and a chip identifier is stored after a trigger is received. Noisy channels could be easily masked via the configuration parameters control. In order to avoid fake trig-

gers produced by noisy channels, the output of each dis- criminator can be switched off from the trigger generator logic via the configuration parameters control (Slow Control hereafter) commands. The response of all the channels can be calibrated by injecting an analog signal through an integrated  $2 \pm 0.02$  pF input test capacitor; this is a useful tool to make the response of the different channels as uniform as possible [1748-0221-6-02-P02001]. The ASIC contains a 127-frame long digital memory. This allows to work in a triggerless mode and keep all the data accumulated during the bench crossing. Once the memory is full the acquisition is stopped, the readout is performed and the ASIC can start acquisition again. The Gray-coded time-stamp is derived from an external 5 MHz clock. An essential feature of the HR is the possibility to be operated in the power-pulsing mode (PP) that consists of switching off almost all power-consumption functionalities in between the bench crossings (BC) of the ILC electron beams. With the ILC duty cycle of one 1 ms of BC every 200 ms, this mode allows a reduction factor of more than 100 of power consumption. Thanks to this reduction, the temperature increase of the HCAL is moderate and only simple cooling system is needed to operate it efficiently.

### Active Sensor Units

To read out the  $1\text{ m}^2$  detector of the SDHCAL, an electronic board with the same size is needed. This electronic board is an important piece in the present design. It hosts both the pick-up pads and the ASICs in addition to the connections linking the pads to the ASICs and those among the different ASICs. To ensure good transmission qualities and low cross-talk, 8-layer Printed Circuit Board (PCB) is designed. Feasibility constraints, make the tasks of circuit production, components soldering, testing and handling of the assemblies, exceedingly difficult in the case of a single board of one square meter. The solution of dividing that circuit into 6 smaller but more manageable PCB was adopted. Each of these small ASUs hosts 24 chips to read out  $48 \times 32$  pads of  $1\text{ cm}^2$  each. This dressed PCB is dubbed Active Sensor Unit (ASU). The base pattern connecting 64 pads arranged in a  $8 \times 8$  matrix to the ASIC's pins is shown in Figure 1.1. This is identical to the one used in the ASUs of the small GRPC chambers described in reference [1748-0221-6-02-P02001]. The routing of each input signal from its own pad up to chip pin has been carefully optimized to reduce the cross-talk. All input signals are laid out in the same analog signal layer which is sandwiched between two GND layers. The routing of digital signals was kept well separated from the vias connecting signals from one layer to another. In the case of the GRPC related ASU, the HARDROC base pattern is replicated  $4 \times 6$  times in the  $33.33\text{ cm} \times 50\text{ cm}$  board. 4 1.6 mm diameter holes are present on the four angles of a PCB to be used for fixation purposes as will be explained later. The rooting was conceived so two of the ASUs can be associated to form one slab hosting 48 ASICs. Each slab is then connected to one Detector InterFace board (DIF). The connection between the DIF and the slab as well as the connection of the two ASUs is performed thanks to tiny connectors allowing the different clocks, signals as well as the power to circulate between the two ASUs. Three slabs are then assembled to form the required electronics board. To ensure the same electric reference level for the six ASUs, the GND layer of the six ASUs is connected thanks to a copper gasket on all the common sides. Similar schemes could be

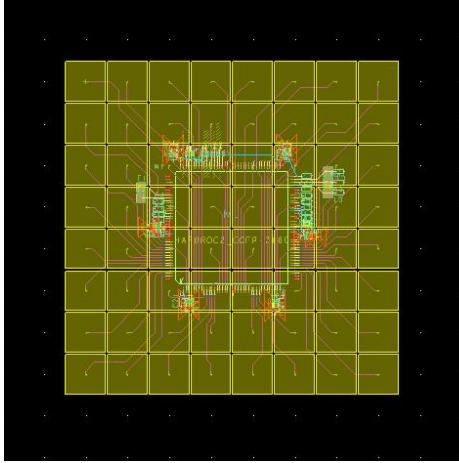


Figure 1.1: Pads connection to the ASIC pins

proposed for GRPC detectors with larger size.

### **Front-end and back-end boards**

The interface between the ASUs and the data acquisition system (DAQ) is realised by the detector interface board called DIF. The main elements of the DIF is an FPGA and USB, HDMI and SAMTEC connectors. It manages the control signals (e.g. clock, busy/ready, external/internal trigger, power-pulsing) and supply power to the ASICs and also performs the readout of the ASIC memories. DIFs are read out by other FPGA-based boards called Data Concentrator Cards (DCC). They can be connected up to 9 DIFs through HDMI links and are controlled by a synchronous DCC (or SDCC). The SDCC can connects to up to 9 DCCs to which it distributes the clock and the commands. It is also connected to the computer network for the user to control the DAQ. In the case of Micromegas ASUs, a small additional board called inter-DIF is used between the DIF and ASU to provide the high voltage to the meshes and drift electrode.

### **Acquisition Software**

To exploit the data collected by the SDHCAL detectors an acquisition software was developed. This software is organized in three parts. The first one allows to access the hardware devices (DIF, SDCC) through an FTDI chip associated to each of these devices. It transmits the configurations parameters to ASICs through these devices and collect the data as well. The second part is the configuration data base. It gives the possibility to store and retrieve all parameters needed by the DAQ system. The database itself is hosted on an Oracle server at CC IN2P3 (Villeurbanne, France). To interface this SQL database with the DAQ software and to allow users to insert and query data without knowledge of SQL, a C++ library has been written. A special care

was taken to allow to download the parameters associated to a given parameters of the prototype (roughly 550000 parameters) in few seconds. The third part concerns the data collection. Data from different DIFs may be readout at a different times but will have the same Bench Crossing IDentifier (BCID) for a given trigger. The logical way to keep synchronicity is to store in a BCID indexed map the buffers of all read DIFs but it requires to manage memory allocation, access and cleaning. This was achieved thanks to the abilities offered by recent Linux kernels to use file based shared memory. In addition, whenever several computers are involved in the data taking, as it is the case for the SDHCAL prototype, a communication framework is needed. The CMS data acquisition XDAQ framework was chosen. This provides communication tools with both binary and XML, an XML description of the computer and software architecture, a web-server implementation of all data acquisition application and a scalable event builder. A monitoring system was also developed to have an online follow-up of the acquisition during data collection.

### 1.1.3 GRPC-SDHCAL for ILD

#### Detector Development

The structure of GRPC proposed as an active layer of the HCAL proposed for ILD is shown in Figure 1.2. It is made out of two glass plates of 0.7 mm and 1.1 mm thickness. The thinner is used to form the anode while the thicker forms the cathode. Ceramic balls of 1.2 mm diameter are used as spacers between the glass plates. The balls are glued on only one of the glass plates. In addition to those balls, 13 cylindrical fiber-glass buttons of 4 mm diameter are also used. Contrary to the ceramic balls the buttons are glued to both plates ensuring thus a robust structure. Special spacers (ceramic balls) were used to maintain uniform gas gap of 1.2 mm. Their number and distribution were optimized to reduce the noise and dead zones (0.1%). The distance between the spacers (10 cm) was fixed so that the deviation of the gap distance between the two plates under the glass weight and the electric force does not exceed 45 microns. The choice of these spacers rather than fishing lines was intended to reduce the dead zones (0.1%). It was also aimed at reducing the noise contribution observed along the fishing lines in standard GRPC chambers. The gas volume is closed by a 1.2 mm thick and 3 mm wide glass-fiber frame glued on both glass plates. The glue used for both the frame and the spacers was chosen for its chemical passivity and long term performance. The resistive coating on the glass plates which is used to apply the high voltage and thus to create the electric field in the gas volume was found to play important role in the pad multiplicity associated to a mip [1748-0221-6-02-P02001]. To find the best coating for GRPC chambers many products were tested. Finally, a new product based on two components was chosen. By changing the two components ratio one can obtain the needed surface resistivity. Commercial products like Licron<sup>TM</sup> and Statguard<sup>TM</sup> which are used for Electro-Static Discharge (ESD) applications were tried and few 1 m<sup>2</sup> chambers were built using those products and intensively tested. Both products failed to satisfy our application either for long term stability under the high voltage (Licron using those products) or due to the impossibility to obtain the surface uniformity needed for our application.

(Statguard using those products). Eventually, two products were identified, both of which are based on colloids containing graphite. Both can be applied using the silk screen print method, which ensures very uniform surface quality. One of these products is a single component paint with a dry surface resistivity of  $1 - 10 \text{ M}\Omega/\text{cm}$ . The second product comes as two components which must be mixed by the user. The surface resistivity may be adjusted over a wide range by changing the mix ratio. Both products require baking at around  $170^\circ\text{C}$  to attain a stable surface resistivity. One product based on colloids containing graphite was finally selected. The product can be applied using the silk screen print method, which ensures very uniform surface quality. In addition, the product is made of two components and it was found that by changing the mix ratio the surface resistivity may be adjusted over a wide range. The measured surface resistivity at various points over a  $1 \text{ m}^2$  glass coated with the previous paint showed a mean value of  $1.2 \text{ M}\Omega/\text{cm}$  and a ratio of the maximum to minimum values of less than 2. A study was also made of the repeatability of the surface resistivity between different mix batches. It was found that surface resistivity in the range  $0.5 - 2 \text{ M}\Omega/\text{cm}$  could be reliably reproduced. For  $1 \text{ m}^2$  GRPCs the painting is applied on the whole glass plate except for 3 mm from the edges. This distance, corresponding to the frame width, was optimized so the dead zone of the detector is reduced while external sparks due to the presence of the metallic cassette in the vicinity is completely eliminated. Another important aspect of this development concerns the gas circulation within the GRPC taking into account that for ILD SDHCAL gas outlets should all be on one side. A genuine system was proposed. It is based on channeling the gas along one side of the chamber and releasing it into the main gas volume at regular intervals. A similar system is used to collect the gas on the opposite side. A finite element model has been established to check the gas distribution [**Bedjidian2010120**]. The simulation confirms that the gas speed is reasonably uniform over most of the chamber area. In order to improve on the gas distribution in large chambers taking into account the requirement that both gas outlets should be on the same side of the detector to satisfy all possible mechanical structures proposed for ILD hadronic calorimeter, new schemes were studied. The one we finally adopted allows us to improve the gas distribution by channeling the gas along one side of the chamber and releasing it into the main gas volume at regular intervals thanks to 1.2 mm diameter PEEK<sup>TM</sup>tubes fixed 2 cm from the chamber side. A similar system is used to collect the gas at the other side of the chamber. A finite element model has been established to check the gas distribution [**Bedjidian2010120**]. The simulation confirms that the gas speed is reasonably uniform over most of the chamber area. as can be seen in Figure 1.3. The GRPC and its associated electronics are housed in a special cassette which protects the chamber and ensures that the readout board is in intimate contact with the anode glass. The cassette is a thin box consisting of 2.5 mm thick stainless steel plates separated by 6 mm wide stainless steel spacers. Its plates are also a part of the absorber. The electronics board is assembled thanks to a polycarbonate spacer which is also used to fill the gaps between the readout chips and to improve the overall rigidity of the detector. The electronics board is fixed on the small plate of the cassette. Thanks to tiny screws and the new set is fixed on the other plate which hosts the detector and the spacers. The whole width of the cassette is 11 mm with only 6 of them corresponding to the sensitive medium including the

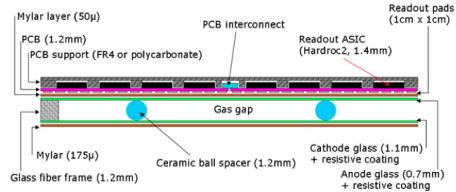


Figure 1.2: Cross-section through a  $1\text{ m}^2$  chamber

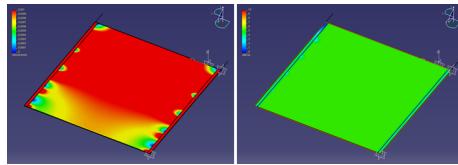


Figure 1.3: Left: gas speed profile in the range 0-1 mm/s. Right: Least mean age profile in the range 0-10 s

GRPC detector and the readout electronics.

### Prototype

A technological prototype corresponding to the SDHCAL option proposed in the ILC LOI was built. 48 cassettes as the one described above were built. They fulfilled a stringent quality control. It is worth mentioning that 10500 HR ASICs were produced and tested using a dedicated robot for this purpose. The yield was found to be higher than 92%. The ASICs were then fixed on the PCBs to make a  $1\text{ m}^2$  and itself fixed on the cassette cover once successfully tested. The cassettes were inserted in a self-supporting mechanical structure that was conceived and built in collaboration with the Spanish group of CIEMAT. The structure is made of Stainless Steel plates of 1.5 cm each. The plates were machined to have an excellent flatness and well controlled thickness. The flatness of the plates was measured using a laser-based interferometer system. It was found that the flatness of the plates are less than 500 microns. This results guarantees that for the SDHCAL V structure proposed for ILD, a tolerance of less than 1 mm is achievable.

The first cassettes were extensively tested using a cosmic-rays bench and later particles beam at CERN. Both the efficiency and the multiplicity of the GRPC cassettes were studied. These studies showed high efficiency and good homogeneity and validated the cassette concept. The prototype construction lasted less than 6 months. A commissioning test at CERN in 2011 allowed to understand the whole system behavior. More precisely a problem related to the acquisition system of the more than 430000 channels was found and fixed. In parallel a single cassette was tested in a magnetic field of 3 Tesla (H2 line at CERN) applying the power-pulsed mode. The TB results indicated clearly that the use of the power-pulsed mode in such a magnetic field is possible. The behavior of the detector (efficiency, multiplicity..) was found to

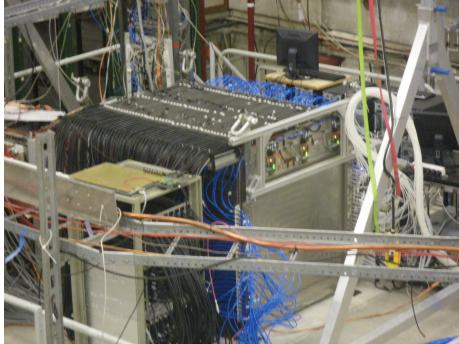


Figure 1.4: Cross-section through a  $1\text{ m}^2$  chamber

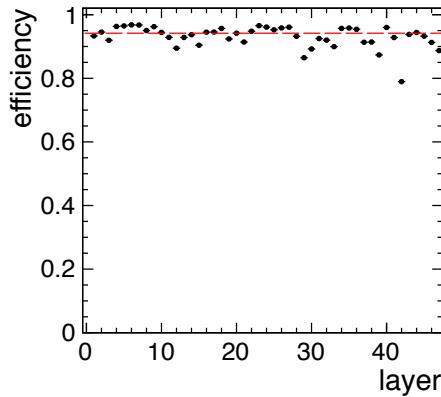


Figure 1.5: Efficiency of the GRPC prototype

be similar to those obtained in the absence of both the magnetic field and the power-pulsed mode (Figures 1.5 and 1.6).

In April 2012 the prototype was exposed to pion, muon, electron beams of both the PS and the SPS of CERN (Figure 1.4). Power-pulsed mode was applied to the whole prototype using the beam cycle structure (0.3 ms time duration for the PS beam and 9 s for the SPS beam every 45 s). A basic water-based cooling system was used to keep under control the temperature increase particularly in the case of the SPS where the consumption reduction is only 5 (to compare with a factor of more than 100 in the ILC case). An acquisition mode a l'ILC was operated. The data were collected continuously in a triggerless mode. The DAQ stops when the memory of one ASIC is full. Data are then transferred to a storage station and then the acquisition starts again. Figures 1.5 and 1.6 shows the efficiency and pad multiplicity of the prototype GRPC chambers measured using the muon beam. The SDHCAL prototype results obtained with a minimum data treatment (no grain correction) show clearly that excellent linearity and good resolution could be achieved on large energy scale as can

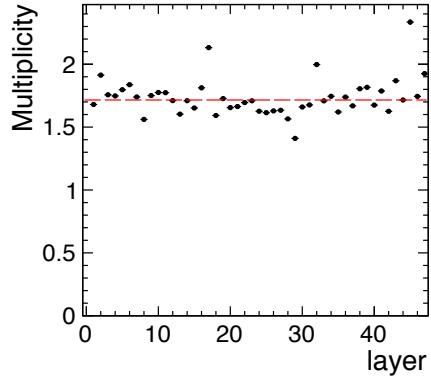


Figure 1.6: Pad multiplicity of the GRPC prototype

be shown in Figures 1.7 and 1.8. Useless to mention that the high granularity of the SDHCAL allows one to study thoroughly the hadronic showers topology and to improve on the energy resolution by, among others, separating the electromagnetic and the hadronic contribution. The separation between close-by showers will also get big benefit thanks to the high granularity on the one hand and to the very clean detector response ( $< 1 \text{ Hz/cm}^2$ ) on the other hand. These two points are being worked and recent results confirm this. The quality of data obtained during three weeks of data taking validates completely the SDHCAL concept as proposed in the LOI. This is especially encouraging since no gain correction was applied to the electronics channels to equalize their response. However a gain correction mode is elaborated and tested during the TB. It will be applied in the future to assess the effect of such correction on the energy resolution.

#### 1.1.4 ILD Preparation

The expertise acquired with the construction and the commissioning of the technological prototype and the obtained results were used to implement a realistic simulation of the ILD HCAL. Physics channels such as the ttH were studied using the SDHCAL option and results were found identical to those obtained with the scintillator tile option despite the fact that the jet energy reconstruction code was optimized for the latter. In addition, the French groups participated actively in the HCAL part of the ILC TDR (ILD part) by proposing a genuine mechanical structure for the hadronic calorimeter (called V-structure). The V structure was conceived to eliminate the projective holes and cracks so none of the particles produced close to the detector centre could escape detection. The V structure has additional advantages. It eliminates in principle the space between the barrel and the Endcaps avoiding the shower deformation which results not only because of this space but also of the different cables and services needed in CMS-like mechanical structures. In this structure the different services such as the gas tubes, data collection and electric cables of both the barrel and the Endcaps are taken out from the outer radius side. Detailed studies

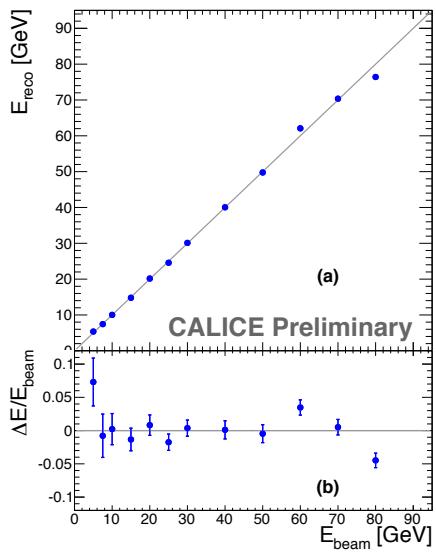


Figure 1.7: (a) : Mean reconstructed energy for pion showers and (b) : relative deviation of the pion mean reconstructed energy with respect to the beam energy

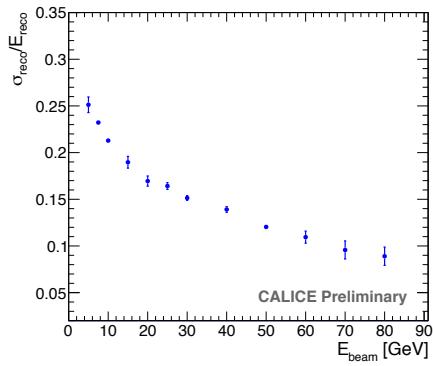


Figure 1.8:  $\frac{\sigma_{\text{reco}}}{E_{\text{reco}}}$  of the reconstructed pion energy  $E_{\text{reco}}$  as a function of the beam energy.

have shown that the deformation of this structure is extremely low and its robustness was verified experimentally with the SDHCAL technological prototype built with a self-supporting structure respecting the spirit of the V one. Services and Integration issues were also worked out. Besides, realistic costing was performed, based on the prototype experience.

### **1.1.5 Recent Milestones**

### **1.1.6 Engineering Challenges**

### **1.1.7 Detector R&D plans for the coming years**

Large G<sub>R</sub>PC of 1 m<sup>2</sup> were developed and built for the technological prototype. However, larger G<sub>R</sub>PC are needed in the future DHCAL with the largest one being 290 × 91 cm<sup>2</sup>. These large chambers with gas inlet and outlet on one side need a dedicated study to guarantee a uniform gas gap everywhere notwithstanding the angle of the plate. It is necessary also to ensure an efficient gas distribution as it was done for the 1 m<sup>2</sup> chambers. The readout of such chambers needs also to be as efficient as the one of the technological prototype 1 m<sup>2</sup>. An upgrade of the HR ASIC allowing larger dynamic range was conceived, produced and is currently tested. The new ASIC allows to be directly addressed and easily bypassed in case of failure. Although we do not expect major difficulties to achieve these purposes, we intend to start soon the R&D to completely validate the feasibility of the SDHCAL with the V mechanical structure. In addition to the previous challenges we need to improve on the interface boards (DIF) needed to control the ASICs synchronization and data transfer. Indeed, the space left between the active layer of one module and the cryostat is only 5 cm. This means that the DIF components should be optimized to cope with the volume availability.

### **1.1.8 Applications Outside of Linear Colliders**

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