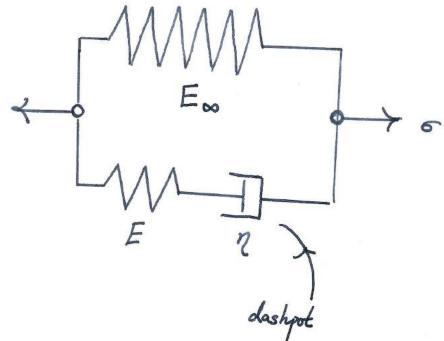
## Viscoelasticity

Standard Solid Model:



a: inelastic strain in the dashpot.

ov: Viscous stress in the dashpot.

linear elastic
$$\begin{cases}
V = \eta \frac{\partial}{\partial t} \alpha(t) \\
Viscosity
\end{cases}$$

$$6 = E_{\infty} \varepsilon + 6^{V}$$
total strain

$$6^{v} = E(\mathcal{E} - \infty)$$

C strain can be additively decomposed.

$$\Rightarrow 6 = (E_{so} + E) E - E \alpha \qquad \Rightarrow \text{constitution}$$

$$E_{o} : \text{ initial modulus}$$
and  $(G^{V} =) \quad \mathcal{T} \alpha = E(E - \alpha)$ 

$$\Rightarrow \alpha + \frac{E}{\mathcal{T}} \alpha = \frac{E}{\mathcal{T}} E$$

$$\Rightarrow \alpha + \frac{1}{\mathcal{T}} \alpha = \frac{1}{\mathcal{T}} E \qquad \mathcal{T} := \frac{n}{E} \text{ relaxation time}$$

$$\Rightarrow \frac{\partial}{\partial t} (e k p(\frac{t}{\mathcal{T}}) \alpha) = \frac{1}{\mathcal{T}} E e k p(\frac{t}{\mathcal{T}})$$

$$\Rightarrow \alpha(t) = \frac{1}{\mathcal{T}} \int_{-\infty}^{t} e k p(-\frac{t-s}{\mathcal{T}}) E(s) ds$$

$$= E(t) - \int_{-\infty}^{t} e k p(-\frac{t-s}{\mathcal{T}}) E(s) ds$$

$$= \int_{-\infty}^{t} \left[ E_{so} + E e k p(-\frac{t-s}{\mathcal{T}}) E(s) ds \right]$$

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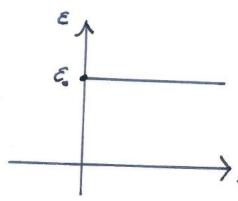
Relaxation test.
$$\mathcal{E}(t) = H(t) \mathcal{E}_{0} = \begin{cases} 0 & \text{if } t \neq 0 \\ \mathcal{E}_{0} & \text{if } t \neq 0 \end{cases}$$

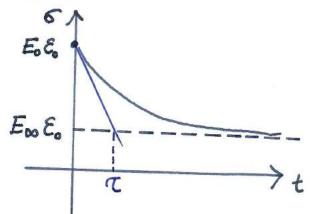
$$\Rightarrow 6(t) = \int_{-\infty}^{t} G(t-s) \mathcal{E}_{o} \ \delta(s) \ ds = G(t) \mathcal{E}_{o} \ t>0$$

= 
$$\left[E_{\infty} + E \exp(-\frac{t}{\pi})\right] \varepsilon$$
.

$$\dot{G}(t) = -\frac{E}{\tau} \exp(-\frac{t}{\tau}) \mathcal{E}_{o}$$

$$\dot{G}(0) = -\frac{E}{\tau} \mathcal{E}_0$$





Generalization \_\_\_\_ multiple Maxwell elements in paraller

$$G' = \sum_{i=1}^{N} E_i \left( \varepsilon - \alpha_i \right)$$

$$\Rightarrow 6 = E_0 e - \sum_{i=1}^{N} E_i \alpha_i$$

$$\Rightarrow E_0 = E_{10} + \sum_{i=1}^{N} E_i$$

$$q_i \alpha_i = E_i (\varepsilon - \alpha_i)$$

$$\Rightarrow \alpha_i + \frac{\alpha_i}{\tau_i} = \frac{\varepsilon}{\tau_i}$$

$$t_{--10} \alpha_i = 0$$

$$\alpha_i(t) = \sum_{i=1}^{N} E_i \exp(-\frac{t-s}{\tau_i}) \dot{\varepsilon}(s) ds$$

$$\Rightarrow 6 = \int_{-\infty}^{t} \left[ E_{10} + \sum_{i=1}^{N} E_i \exp(-\frac{t-s}{\tau_i}) \right] \dot{\varepsilon}(s) ds$$

$$G(t-s)$$

$$E_{10}$$

$$G(t-s)$$

Stored energy: 
$$\psi(\mathcal{E}, \alpha) = \frac{1}{2} E_{\infty} \mathcal{E}^{2} + \frac{1}{2} \sum_{i=1}^{N} E_{i} (\mathcal{E} - \alpha_{i})^{2}$$

vector of  $(\alpha_{1}, ..., \alpha_{N})^{T}$ .

Recall that Clausius-Plank inequality gives

$$\psi_{i\varepsilon} = E_{\infty}\varepsilon + \sum_{i=1}^{N} E_{i}(\varepsilon - \alpha_{i}) = 6$$

$$\Rightarrow \mathcal{D} = \sum_{i=1}^{N} G_{i}^{v} \dot{\alpha}_{i} = \sum_{i=1}^{N} \eta_{i} \left( \dot{\alpha}_{i} \right)^{2} \geq 0$$

due to the constitutive model for the dashpot. (inelasticity) Characterization of equilibrium response.

Under a preserbed strain/stress, the device reaches equilibrium if no further changes in the dashpots take place.

or. 
$$|\alpha_i| = 0$$
 for  $i = 1, \dots, N$ .
$$|\alpha_i| = 0$$

or.  $|e_i| = 0$  for  $i = 1, \dots, N$  (i.e. the force vanishes)

$$\Rightarrow \dot{\alpha}_{i} + \frac{\alpha_{i}}{\tau_{i}} = \frac{\varepsilon}{\tau_{i}} \Rightarrow \dot{\alpha}_{i} = \varepsilon \quad \text{in equilibrium}$$

 $\Rightarrow$   $6 \mid_{q} = E_{\infty} \varepsilon$ .

Remarks: the variable  $f_i = -\frac{\partial \psi}{\partial \alpha_i} = E_i(E - \alpha_i) = G_i^V$ is often used in place of  $\alpha_i$ , in a lot works.