

A NEW UNIVERSAL AC POWER PROTECTION APPROACH

WHITE PAPER



Bourns® IsoMOV™ Hybrid Protectors



Bourns® SinglFuse™ SMD Fuses



Bourns® TBU® High-Speed Protectors (HSPs)



Bourns® TiSP® Thyristor Surge Protectors

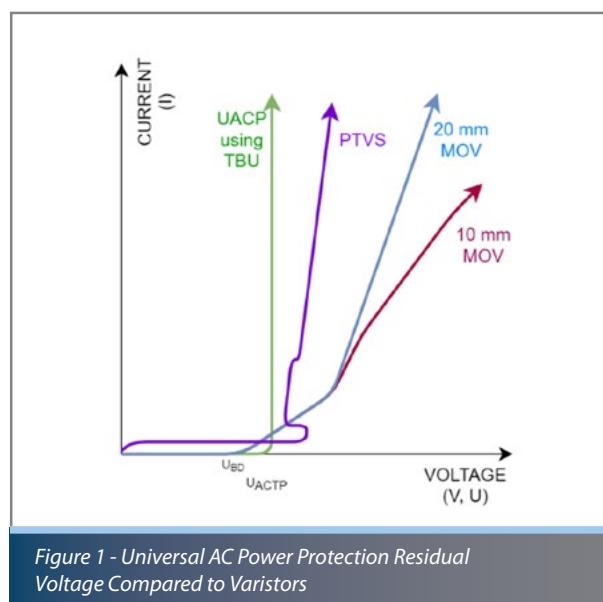


INTRODUCTION

Lightning surges and power disturbances on AC mains can have a detrimental effect on a wide range of electronic equipment. The damage caused by overvoltage and overcurrent events can result in costly down time and repair costs and contribute to low customer confidence in the manufacturer.

What is needed is a new approach to AC power input protection that gives developers the option to integrate a robust, on-demand protection circuit. Using this type of protection methodology offers minimal interference during an application's normal operation, which can reduce component degradation over time to help extend the equipment's lifespan.

This white paper introduces a coordinated circuit protection methodology that employs a new hybrid protector. It presents the special features delivered in a new universal AC power protection solution and covers Bourns lab tests on simulated AC line swells and lightning. Multiple application examples are provided that highlight how the new level of protection can be achieved to help maximize reliability and reduce downtime.



Comparing the residual voltage of the universal AC power protection with 14 mm and 20 mm MOVs shows that the voltage does not increase with current as it does with the varistors.

This comes about by carefully coordinating a group of circuit protection components so that each component protects the ones next to it.



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FEATURE REQUIREMENTS FOR UNIVERSAL AC POWER PROTECTION

Current safety standards and regulatory codes specify protection schemes to help mitigate the failure effects surges can have for the user and on associated connected equipment (i.e., fuses). This new approach provides protection in excess of existing standards and regulations and gives developers the option to integrate a robust, on-demand protection circuit that offers minimal interference during normal operations without degrading its components (i.e., blown fuses), and one that helps extend the equipment's lifetime.

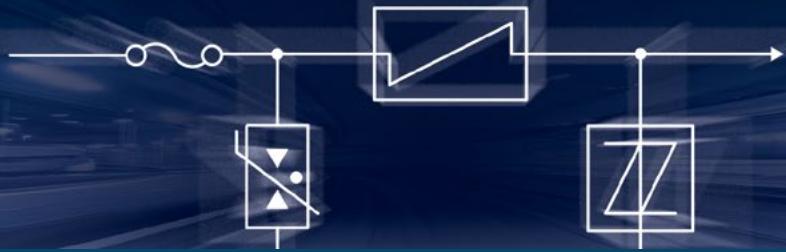
Currently, there is no overcurrent and overvoltage protection solution that exists that can deliver universal power to help equipment designers meet safety requirements. This requires a solution that offers absolute maximum voltage protection, regardless of the intensity of the surge input, in order to reduce design margin requirements and the associated costs of downstream circuit components. The ideal circuit protection approach needs to automatically reset every half cycle to provide continuous protection when needed. For universal AC power protection, the optimal surge protector would also have to limit power let-through to prevent fires in case of component failure or damage.

To meet these requirements, Bourns has engineered innovative primary protection devices like GMOV™, IsoMOV™, and high energy varistors (MOVs). The Bourns IsoMOV™ is a coordinated self-protecting device. The **Bourns® IsoMOV™** device is designed to be a coordinated self-protecting solution working in conjunction with **Bourns® SinglFuse™ SMD fuse**, **TBU® high-speed protector (HSP)** and **TISP® thyristor surge protector** components. Ideal for mission-critical applications where failure is not acceptable or service is difficult, this coordinated approach conditions AC power delivered in certain harsh environments to protect equipment from voltage spikes, swells or overvoltages. The protection scheme that employs the Bourns primary protection components help to increase reliability, improve system up-time and contribute to reduced lifecycle costs and warranty issues.

This paper describes a robust multi-stage circuit protection solution that:

- Survives lightning surges
- Tolerates voltage swells without damage
- Provides overcurrent limiting capability in the event of internal faults
- Is a wide-range permanent protection solution





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PROTECTION CIRCUIT OPERATIONAL BASICS

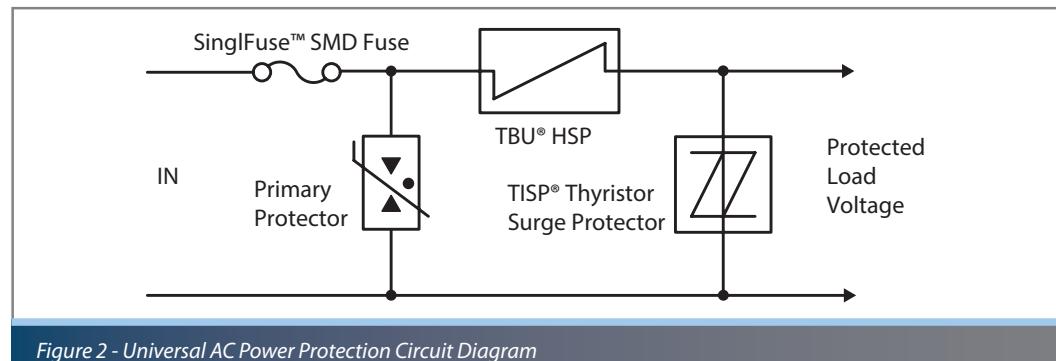


Figure 2 - Universal AC Power Protection Circuit Diagram

Figure 2 shows a basic schematic of the protection circuit. Line power is applied at the left-side port and the protected equipment is connected to the right-side port. The operation of the circuit is best described moving from right to left – starting with the TISP® device.

The TISP® device shown is a thyristor that is triggered if the voltage across the protected load should exceed its breakdown voltage rating. Important in selecting a TISP® device is its breakdown voltage, which is key in preventing damage caused by excessive voltage in the protected circuit. This allows precise selection of the maximum voltage necessary to protect the specified circuit.

The following lists the series of steps in the universal AC power protection scheme:

1. If a voltage event should trip the TISP® device, it will short out the AC line. The excessive current drawn will trip the Bourns® TBU® high-speed protector (HSP) device into its blocking state. When the TBU® HSP blocks the excessive current, the protected load and TISP® device are essentially disconnected from the AC line, protecting both from damage.
2. As the TBU® HSP blocks the current, the input voltage may continue to rise until the primary protector, such as the Bourns varistors (MOVs), GMOV™, and IsoMOV™ hybrid protector, trips and limits the voltage below the TBU® HSP's maximum blocking voltage rating.
3. Should the voltage continue to rise until the current through the primary protector exceeds its surge rating, the Bourns® SinglFuse™ device will open and permanently disconnect the circuit from the AC line.

Secondarily, if the protected load attempts to draw in excess of the TBU® HSP's trip current, the device will go into the blocking state and the circuit will behave as before (Steps 2 and 3).

When the AC input voltage crosses zero, the circuit resets to the initial state and can either resume normal operation (typical for a lightning surge) or be tripped again on the next half cycle (typical for a voltage swell).





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AC LINE VOLTAGE SWELL RESPONSE

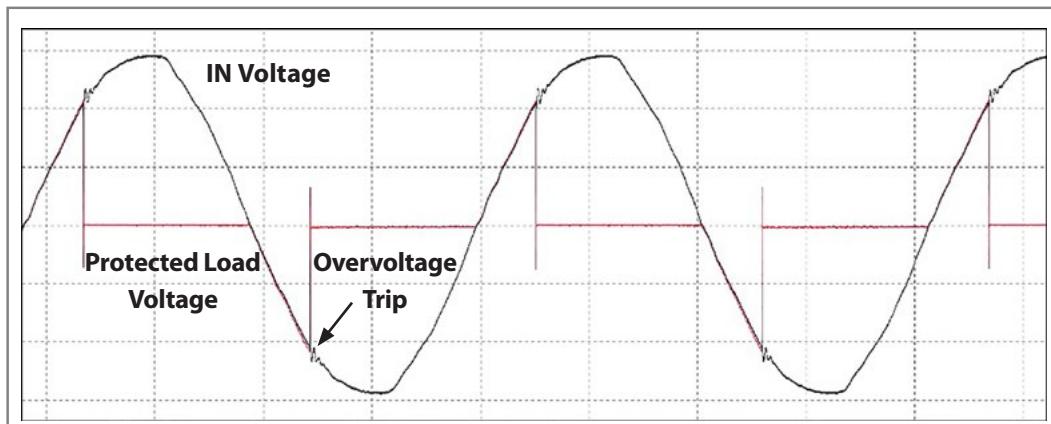


Figure 3- Illustration of Universal AC Power Protection Operation with AC Line Voltage Swell

Figure 3 shows the response of the circuit to an AC line voltage swell. The TISP® device employed activates at about 220 V – a typical value selected for nominal 120 VAC power lines. The swell voltage applied is set to about 200 VAC. As shown above, the input and output voltages track until the TISP® protector fires, at which time the load voltage drops to zero for the remainder of each half-cycle.

Later we will show that protected switched-mode power supplies (SMPS) loads we tested continued to operate during these voltage swells.





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LIGHTNING TRANSIENT RESPONSE

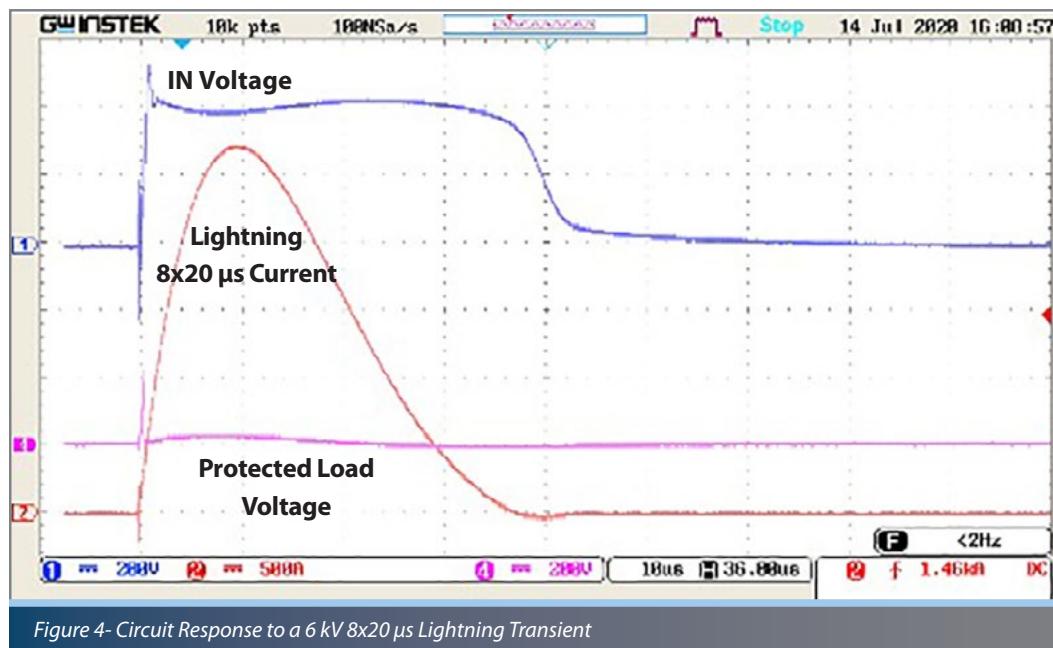


Figure 4 illustrates the response of the circuit to an IEC 61000-4-5 simulated lightning pulse of 6000 V with an 8x20 μ s waveshape. Such lightning surges last only about 50 μ s. Switching transients and other impulse-like line noise are typically even shorter in duration. It should be noted that these particular tests were not performed on an AC line. In real-world applications, the TBU® HSP, once put into the blocking state by lightning or some other transient, will continue in its blocking state until the next power line zero crossing.

The oscilloscope in Figure 4 shows that the IN voltage is clamped at about 400 V by the Bourns primary protection device. The generator sources the current from a capacitor charged to 6000 V. The driving voltage for the current is then 6000 V minus 400 V or 5600 V. Since the generator has a characteristic impedance of 2 Ohms, the peak current of about 2800 A is the expected value.





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LIGHTNING TRANSIENT RESPONSE (Continued)

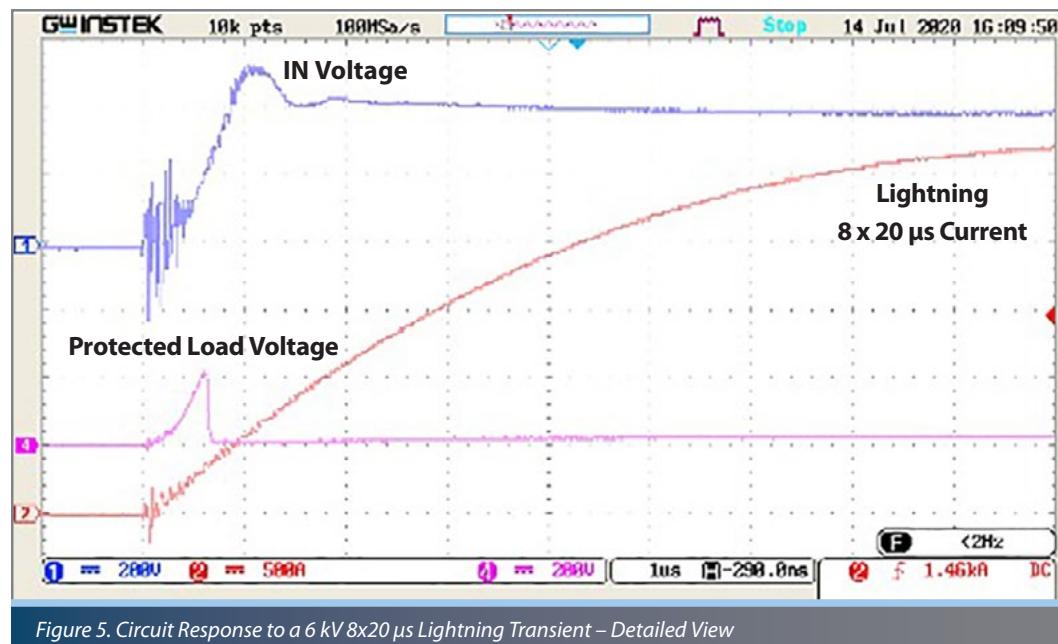
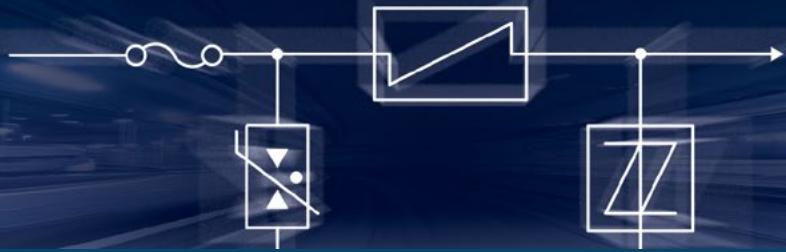


Figure 5 displays the same waveform of Figure 4, but with a timescale of 1 μ s/div, which translates to a 10X view of the details of the lightning transient response. The waveform in Channel 4 shows the response of the TISP® device to the overvoltage event. Some ringing is evident in these measurements. The ringing in Channel 1 is largely caused by the switching action of the surge generator interacting with the high voltage scope probe. Note that ringing is not evident in Channel 4 (at the protected load). Also some of the ringing that appears in Channel 1 is a reaction by the transformer driving the AC voltage when the TBU® HSP suddenly switches to its blocking state.

The key takeaway from this test is that in the face of a rather severe lightning event, the peak voltage experienced by the protected load is only about 230 V.





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APPLICATION: STREETLIGHT VOLTAGE SWELL

A 150 W LED streetlight luminaire (LEDMyPlace.com #719034339818) with a switch mode power controller and dimming function is set to a power level of about 50 watts.

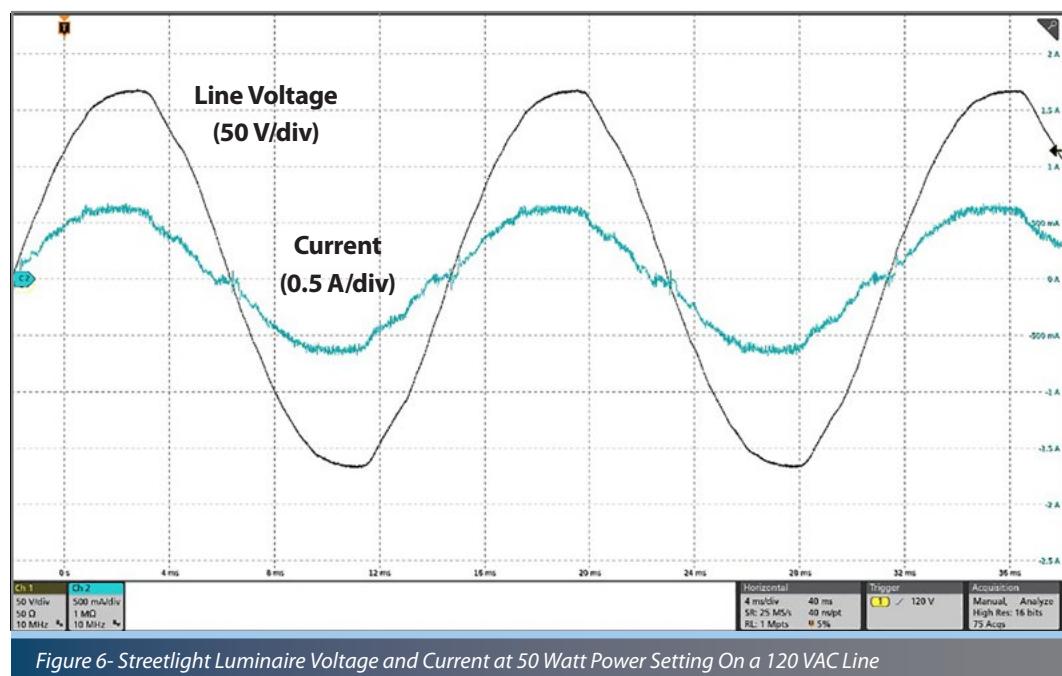
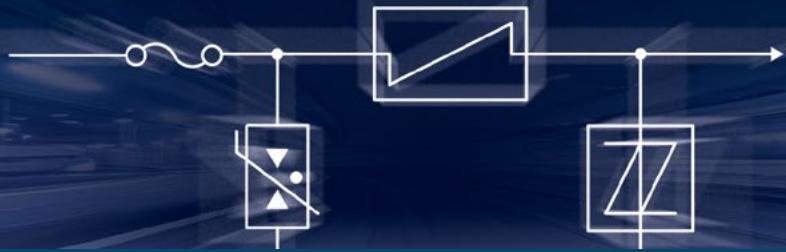


Figure 6 shows the voltage and current waveforms from a 120 VAC mains AC supply. The luminaire current is nearly sinusoidal with little power drawn between the current zero crossing and the voltage zero crossing. The load appears slightly capacitive in nature. The peak current draw is approximately 600 mA.





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APPLICATION: STREETLIGHT VOLTAGE SWELL (Continued)



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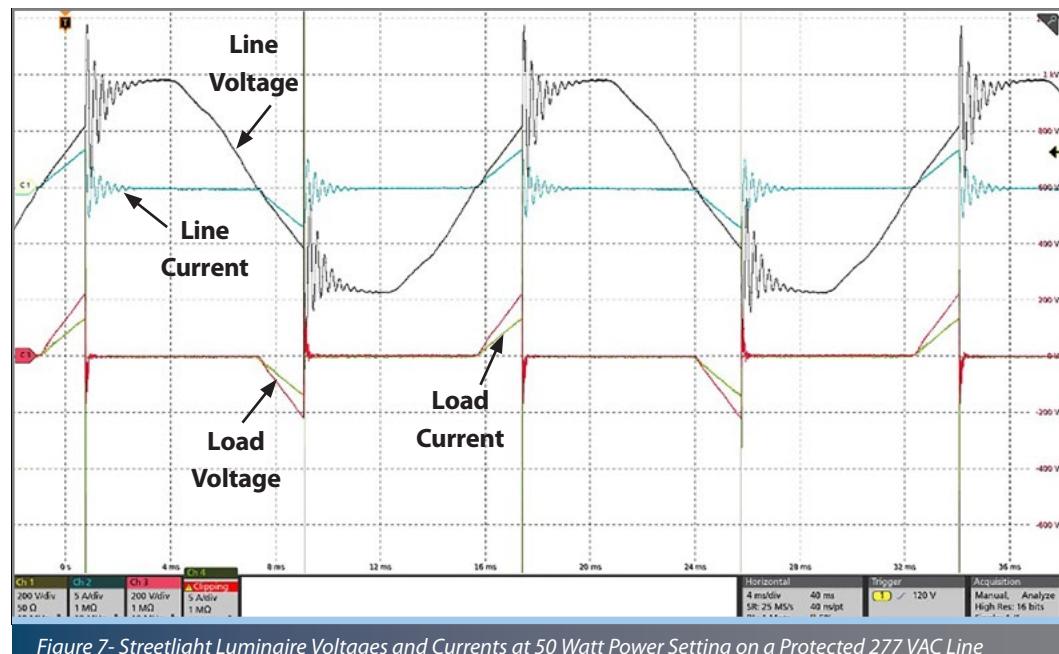
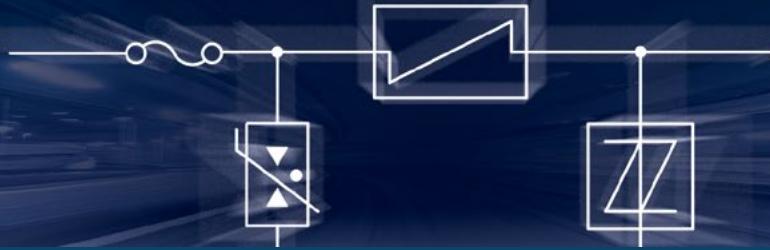


Figure 7 shows the luminaire at the same power setting driven at 277 VAC with the protection circuit in place (using the same approximately 220 V TISP® device). The power to the luminaire can be seen to be cut off at about 210 V. When tested in the Bourns lab, some ringing on the AC line was evident when the lab power transformer inductance reacts with the sudden current blocking action from the TBU® HSP.

Note that the luminaire drew large currents (the 0 to 3 A ramp) before the TISP® device triggered. At the TBU® HSP trigger point on each peak of each half-cycle, it drew about 600 W! As previously noted, under normal line conditions the luminaire drew about 600 mA peak on a near sinusoidal wave.

In this test, the luminaire light output appeared to be unaffected by the voltage swell.





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APPLICATION: COMPUTER POWER SUPPLY

A common laptop computer power supply rated at 64 watts output with 90 to 240 VAC input is operated with a resistive load drawing 43 watts.

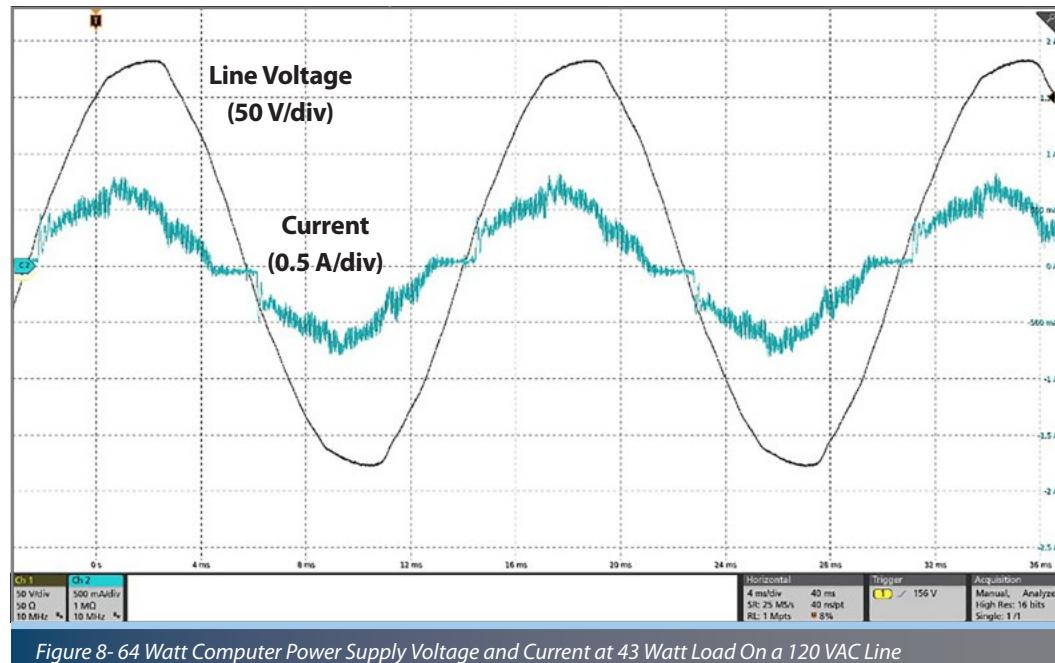
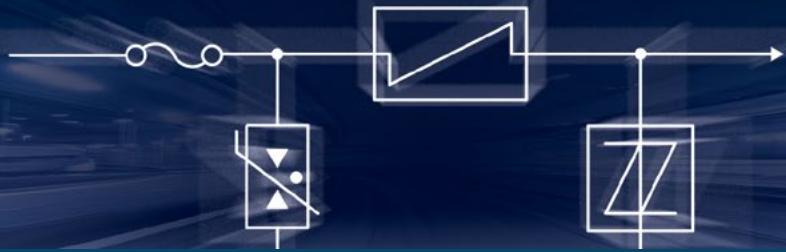


Figure 8 illustrates the voltage and current waveforms from a 120 VAC mains AC supply. The power supply current is nearly sinusoidal with a dropout between the current zero crossing and the voltage zero crossing. The load appears slightly capacitive in nature. The peak current draw is about 700 mA.





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APPLICATION: COMPUTER POWER SUPPLY (Continued)

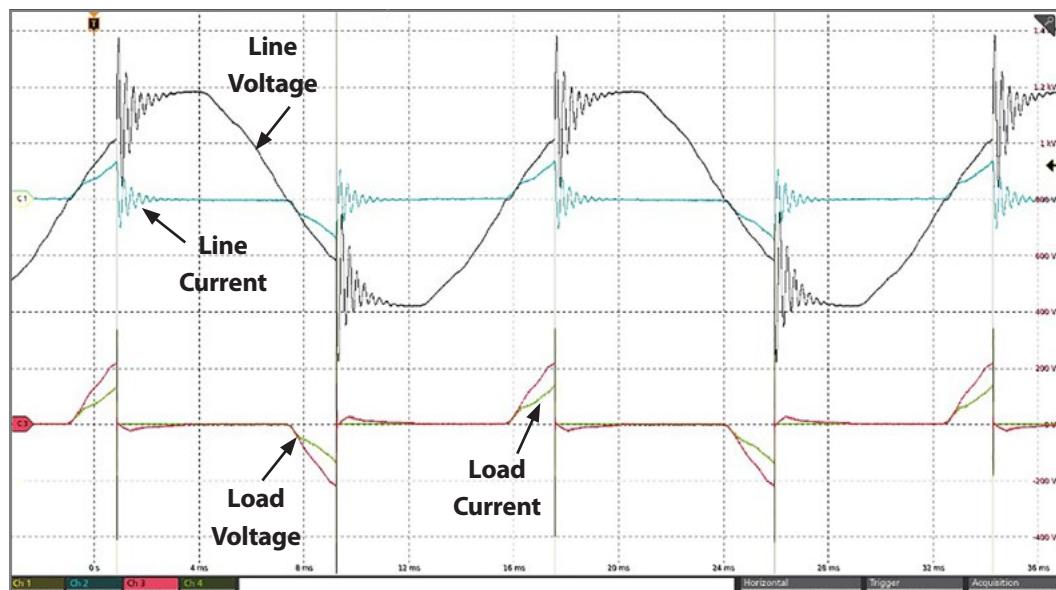


Figure 9 shows the computer power supply with the same 43 watt load driven at 277 VAC with the protection circuit in place (using the same 220 V TISP® device). During the test in the Bourns lab, the voltage to the power supply can be seen to be cut off at about 210 V. Ringing on the AC line was evident again as the lab power transformer inductance reacts with the sudden current blocking action from the TBU® HSP.

Note that in the Bourns test, the power supply drew large currents (the 0 to 3 A ramp) before the TISP® device triggered. At the TBU® HSP trigger point on each peak of each half-cycle, it drew about 600 W! And as previously noted under normal line conditions, the power supply drew 700 mA peak on a near sinusoidal wave which is controlled by the current blocking action of the TBU® HSP.

The power supply operation appeared to unaffected otherwise by the voltage swell.





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TBU® HSP RESISTANCE AND EFFICIENCY TRADEOFFS

In the active AC protector circuit, the TBU® HSP is in series resistance. For prototype purposes, the Bourns lab setup used four Bourns® TBU-CA085-500-WH devices in parallel. Each of these has a nominal trip current of 750 mA, a resistance of 10.7 ohms and a standoff voltage of 850 V. This yields a composite device of about 3 A trip current and 2.7 ohms of resistance.

There is a natural tradeoff in the protection circuit between cost and additional value provided by a TBU® HSP's resistance. The trip current is of little concern provided it is enough to support the inrush and operating currents of the protected load. When the TISP® device is triggered, the available short-circuit current from the AC line will instantly trip the TBU® HSP.

The resistance of the TBU® HSP can cause continuous power losses as seen in Figures 10 and 11. Note that the higher peak currents encountered in the clipping "protection mode" will tend to cause more loss compared with the near sinusoidal currents experienced in normal operation.

The design engineer is then faced with finding an acceptable balance of cost and efficiency.

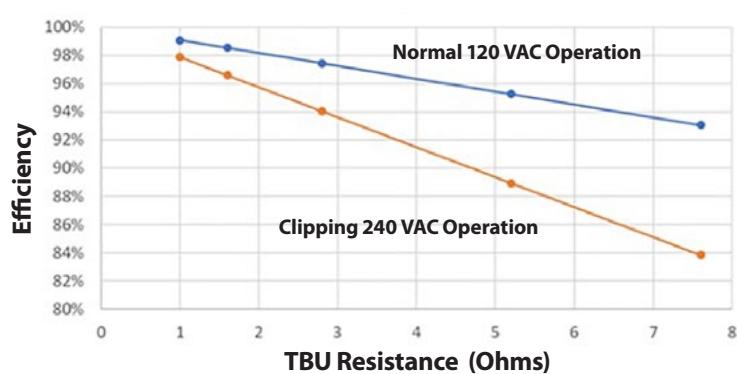


Figure 10 - AC Protector Efficiency for the Streetlight Luminaire at 50 Watts

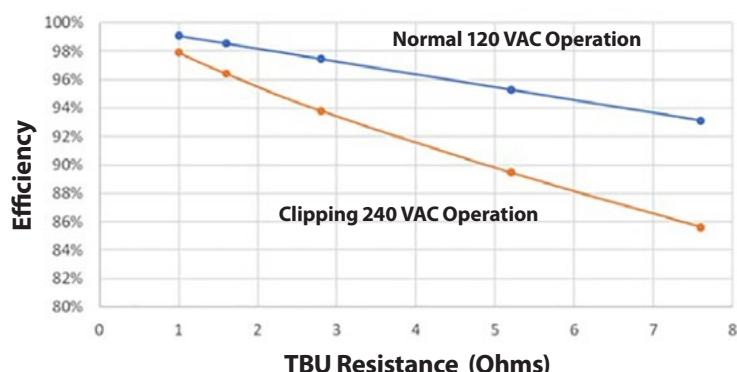


Figure 11 - AC Protector Efficiency for the Computer Power Supply Loaded to 43 Watts





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ADDITIONAL AC MAINS DESIGN CONSIDERATIONS

Up to this point we have only looked at the operation of the UACP circuit using 120 V mains. The UACP concept, however, is applicable to other AC mains voltages as well. Following the process outlined below – whereby the primary protector and TISP® devices change to accommodate the different voltages – can lead to a successful application of the UACP circuitry for alternative AC mains voltages.

To design the appropriate UACP protection circuit, designers should consider the following:

1. For the TISP® device selection:

- The V_{BO} must be below the protected circuit's maximum input voltage.
- Tolerances and temperature variations must be also considered.
- The power dissipation of the TISP® device is typically minuscule and not critical.

2. For the TBU® HSP device selection:

- The TBU® HSP trigger current must be above the maximum current required by the protected circuit without triggering the TBU® HSP device into the protected state ($I_{TRIGGER} > I_{LOAD}$). Multiple TBU® HSP devices can be connected in parallel to handle more current.
- Power loss and thermal dissipation due to the TBU® HSP device's R_{DEVICE} must be taken into consideration and included in the power budget for the final design.
- The TBU® HSP's impulse withstand voltage (V_{IMP}) must be higher than the primary protection component's maximum clamp voltage (V_C).

3. For the primary protection component selection such as varistors (MOVs), GMOV™, and IsoMOV™:

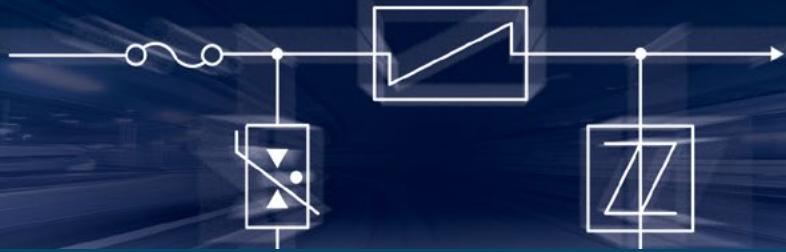
- The primary protection device's I_{NOM} must meet the final design's surge requirements.
- The MCOV_{DC} rating must be higher than the TISP® device minimum V_{BO} .
- The maximum clamp voltage (V_C) must be lower than the TBU® HSP's impulse withstand voltage (V_{IMP}).

4. For the fuse selection:

- The fuse's rated current must be higher than the TBU® HSP device's $I_{TRIGGER}$.
- The fuse must tolerate the surges up to the final design's surge requirements.
- Bourns has tested its primary protection components and demonstrated that they will clear a fuse rated up to 10 A on catastrophic failure.

It is always recommended that all circuit protection recommendations be checked and correlated with actual bench measurements of typical devices in the actual use environment and tested to the final design's surge requirements.





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CONCLUSION

Using the SinglFuse™ SMD fuse together with Bourns' innovative primary protection devices, such as varistors (MOVs), GMOV™, and IsoMOV™, this Universal AC Protection design provides continuously available protection in four small components. This protection was previously unattainable using much larger components that included disconnecting the overvoltage protection and the risk of fire and destruction.

Bourns supplies the cutting-edge components to enable this permanently connected AC line input protection in a space less than one square inch. The protection components are exactly coordinated together so they protect each other and the designer's load from lightning surges, AC line noise, AC line surges, and any other overvoltage condition that would otherwise reach the user's equipment.



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