

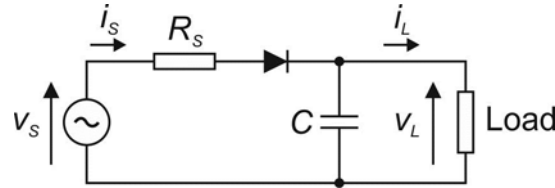
## Half-wave and full-wave rectifier efficiencies

Note for Luke Morton, ASH 21.02.16

Assumptions:

- Sinusoidal voltage source  $v_s$  with amplitude  $v_0$  and purely resistive source impedance  $R_s$
- Ideal diodes, with zero forward voltage and zero reverse current
- Large reservoir capacitance, giving DC output voltage  $v_L$  with negligible ripple

### Half-wave rectifier



The current drawn from the source is:

$$i_s = \begin{cases} (v_s - v_L)/R_s & v_s > v_L \\ 0 & \text{otherwise} \end{cases}$$

The steady state load current  $i_L$  is just the average value of  $i_s$ :

$$i_L = \bar{i}_s = \frac{1}{2\pi R_s} \int_{-\Delta\phi/2}^{\Delta\phi/2} (v_0 \cos \theta - v_L) d\theta$$

where  $\Delta\phi$  is the conduction angle of the diode, which is given by:

$$\Delta\phi = 2 \cos^{-1}(v_L/v_0)$$

Evaluating the above integral we find:

$$i_L = \bar{i}_s = \frac{v_0}{\pi R_s} \left[ \sqrt{1 - u^2} - u \cos^{-1} u \right]$$

where  $u = v_L/v_0$ .

The (constant) power delivered to the load is then:

$$P_{L_{hw}} = v_L i_L = \frac{v_0^2}{8R_s} \frac{8u}{\pi} \left[ \sqrt{1 - u^2} - u \cos^{-1} u \right]$$

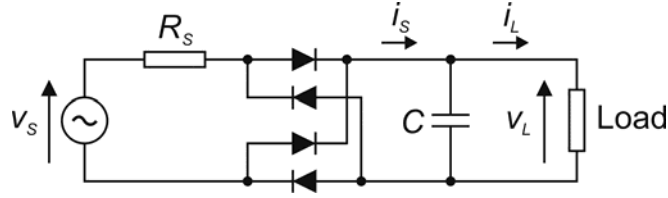
At the same time, the average power drawn from the source is:

$$P_{S_{hw}} = \overline{i_s v_s} = \frac{1}{2\pi R_s} \int_{-\frac{\Delta\phi}{2}}^{\frac{\Delta\phi}{2}} v_0 \cos \theta (v_0 \cos \theta - v_L) d\theta$$

Evaluating this integral gives:

$$P_{S\_hw} = \overline{i_S v_S} = \frac{v_0^2}{8R_S} \frac{4}{\pi} \left[ \cos^{-1} u - u \sqrt{1 - u^2} \right]$$

### Full-wave rectifier



For this case the source current  $i_S$  (NB measured on output side of rectifier) is:

$$i_S = \begin{cases} (|v_S| - v_L)/R_S & |v_S| > v_L \\ 0 & \text{otherwise} \end{cases}$$

For any given value of  $u = v_L/v_0$ , there will be two current pulses per cycle, each having the same form as the single current pulse that occurred in the half-wave case. It follows that, for a given value of  $u$ , the load current, load power and average source power will all be twice as large as in the half-wave case, i.e.:

$$P_{L-fw}(u) = 2P_{L-hw}(u) \quad ; \quad P_{S-fw}(u) = 2P_{S-hw}(u)$$

It also follows that, for a given value of  $u$ , the overall system efficiency  $P_L/P_S$ , taking into account the power loss in the source resistance, is the same for both configurations. (NB the rectifiers themselves are 100% efficient in this analysis because there are no diode losses.)

### Performance comparison

The plot below shows the variations of the normalised output power and overall efficiency for the idealised half-wave and full-wave rectifiers, as a function of normalised output voltage  $u = v_L/v_0$ . The output powers are normalised to  $v_0^2/(8R_S)$  which is the power that would be delivered to a matched load.

