Nonlinear modes of vibration of systems undergoing unilateral contact through the semi-smooth Newton approach

Oral defence of master's thesis

Yulin Shi supervisor: Mathias Legrand

Structural Dynamics and Vibration Laboratory
McGill University

May 9, 2016



Modes of free conservative linear systems



Governing equation

$$\mathbf{M}\ddot{\mathbf{u}}(t) + \mathbf{K}\mathbf{u}(t) = \mathbf{0}, \quad \forall t$$
 (1)

Assume a periodic solution $\mathbf{u}(t) = \bar{\mathbf{u}}e^{i\omega t}$ and plug into Eq. (1) to build an eigenvalue problem

$$\left(-\omega^2 \mathbf{M} + \mathbf{K}\right) \bar{\mathbf{u}} = \mathbf{0} \tag{2}$$

- ► Example: for $k_1 = k_2 = 1$, and $m_1 = m_2 = 1$
 - ▶ Mode 1

$$\bar{\mathbf{u}}_1 = \begin{pmatrix} -0.53 \\ -0.85 \end{pmatrix}, \quad \omega_1 = 0.618$$

▶ Mode 2

$$\mathbf{\bar{u}}_2 = \begin{pmatrix} -0.85\\0.53 \end{pmatrix}, \quad \omega_2 = 1.618$$

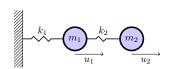


Figure 1: System of interest

Figure 2: Mode 1

Forced damped linear systems and energy-frequency plots



Why looking for modes of vibration?

▶ in industry: slightly damped system

energy response E at different ω

ightharpoonup excited by periodic forcing at ω



Figure 4: Automotive structure test rig

Because *modes* predict vibratory *resonances*

two peaks at the two natural frequencies

$$\mathbf{M\ddot{u}} + \mathbf{D\dot{u}} + \mathbf{Ku} = \mathbf{f}\cos(\omega t)$$
 (3)

► Backbone curves of free systems predict resonance curves of forced systems

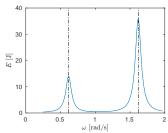


Figure 5: Energy-frequency plot of solution **u** to Eq. (3)

Modes of nonlinear smooth systems

Example: free Duffing oscillator

$$\ddot{u} + (k + \epsilon u^2)u = 0 \tag{4}$$

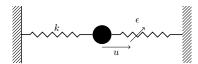


Figure 6: Simple Duffing oscillator

Natural frequency depends on u

$$\omega_n = \sqrt{\operatorname{eig}(k + \epsilon u^2)} = ? \tag{5}$$

► Forced Duffing oscillator

$$\ddot{u} + 0.1\dot{u} + u + \epsilon u^3 = \cos(\omega t) \quad (6)$$

- ▶ Limit cycles → periodicity
- ▶ new: not elliptic → non-harmonic
- resonance in energy-frequency plot
- new: bending of resonance: hardening

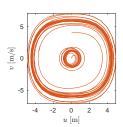


Figure 7: Limit cycles at $\omega=$ 1.5 rad/s

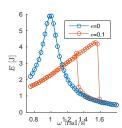


Figure 8: Energy-frequency plot

Periodic solutions of nonlinear systems: Harmonic balance method



Governing equations of (discrete) mechanical systems

free:
$$r(\ddot{u}, u) = 0$$
, forced: $r(\ddot{u}, \dot{u}, u, t) = 0$ (7)

- Periodic solutions are of interest in vibration analysis (either forced or free)
- Harmonic Balance Method: seeks solutions in the form of truncated Fourier series
 - Truncated Fourier series

$$u(t) \approx \bar{u}_0 + \sum_{m=1}^{M} \cos(m\omega t)\bar{u}_{2m-1} + \sin(m\omega t)\bar{u}_{2m} = \phi(t)\bar{\mathbf{u}}$$
 (8)

where $\omega = 2\pi/T$ is the frequency, and M is the number of harmonics.

ightharpoonup Galerkin projection ightharpoonup nonlinear equations in $\bar{\mathbf{u}}$ (and ω when free)

$$\bar{\mathbf{r}}(\bar{\mathbf{u}}) = \int_0^T \phi^\top(t) r(\ddot{\phi}(t)\bar{\mathbf{u}}, \dot{\phi}(t)\bar{\mathbf{u}}, \phi(t)\bar{\mathbf{u}}, t) dt = \mathbf{0}$$
(9)

Newton-Raphson solution procedure can be used if $\bar{\mathbf{r}}(\bar{\mathbf{u}})$ is smooth.

$$\bar{\mathbf{u}}^{(k+1)} \leftarrow \bar{\mathbf{u}}^{(k)} - (\nabla \bar{\mathbf{r}}(\bar{\mathbf{u}}^{(k)}))^{-1} \bar{\mathbf{r}}(\bar{\mathbf{u}}^{(k)})$$

$$\tag{10}$$

Unilateral contact conditions



- Unilateral mass-spring system
 - governing equation (statics)

$$r(u) = ku - \lambda - f = 0 \tag{11}$$

contact condition

Open gap:
$$u-g \le 0, \ \lambda = 0$$

Closed gap: $u-g=0, \ \lambda \le 0$ (12)

where g is the initial gap and λ , the contact force.

Newton method does not work because $\lambda(u)$ is multi-valued.

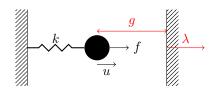


Figure 9: Vibro-impact oscillator



Figure 10: Non-differentiable contact constitutive law

Regularizations of the non-differentiable contact constitutive law



- ▶ Allow penetration: $\max\{0, u g\}$
- contact force is proportional to penetration: $\lambda = -\epsilon \max\{0, u g\}$
- $\mathbf{v}^{(k)} \to \mathbf{u}^{(\infty)} \text{ when } \epsilon \to \infty$

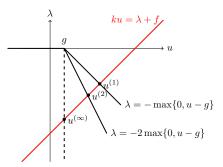


Figure 11: Penalty method

 Other treatments: Augmented Lagrange method, linear complementarity problem, active set method, Nitsche method

Implicit form of complementarity conditions



 Contact condition seen as the root set of the semismooth function

$$s(u,\lambda) = \lambda + \max\{0, c(u-g) - \lambda\} = 0$$
(13)

- ▶ plot in Figure 12
- nonlinear function (actually piecewise linear)
- semi-smooth function only (Newton method does not apply)
- Augmented system equations

$$ku - \lambda - f = 0$$

$$\lambda + \max\{0, c(u - g) - \lambda\} = 0$$
 (14)

to be solved in displacement u and contact force λ using an appropriate solver: addressed next

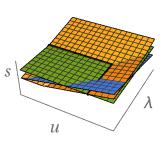


Figure 12: (Yellow) Semismooth surface $s(u, \lambda)$

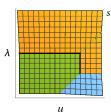


Figure 13: Above view: (-) root set

Semismooth Newton method



Issues arise when implementing the Newton-Raphson method for nonsmooth systems

► Example of semismooth function

$$r(u) = \max\{-u, u\} \tag{15}$$

Semismooth Newton method

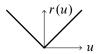


Figure 14: Simple semismooth function

Concept of sub-differential

Attributes

$$\partial r(0) := \left[\lim_{u \to 0^{-}} \frac{r(u) - r(0)}{u}, \lim_{u \to 0^{+}} \frac{r(u) - r(0)}{u} \right] = [-1, 1]$$
 (16)

Function $r(u)$	smooth	semismooth
Iteration	$\Delta u = -(G(u))^{-1}r(u)$	$\Delta u = -(G(u))^{-1}r(u)$
Jacobian matrix	$G(u) = \nabla r(u)$	$G(u) \in \partial r(u)$
Convergence speed	quadratic	linear

Smooth Newton method

Harmonic balance method for contact problems



For the reformulated system equation of a contact problem

$$r(\ddot{u}(t), \dot{u}(t), u(t), \lambda(t), t) = m\ddot{u}(t) + \delta \dot{u}(t) + ku(t) - \lambda(t) - f\cos(\omega t) = 0, \quad \forall t$$

$$s(u(t), \lambda(t)) = \lambda(t) + \max\{0, c(u(t) - g) - \lambda(t)\} = 0, \quad \forall t$$

Solutions approximated by truncated Fourier series

$$u(t) \approx \sum_{i=1}^{M} \phi_i(t) \bar{u}_i = \phi(t) \bar{\mathbf{u}} \quad \text{and} \quad \lambda(t) \approx \sum_{i=1}^{M} \phi_i(t) \bar{\lambda}_i = \phi(t) \bar{\lambda}$$
 (18)

▶ Galerkin projection \rightarrow nonlinear equations w.r.t. $\bar{\bf u}$, $\bar{\lambda}$ and ω (when unknown)

$$\int_{0}^{T} \phi(t)^{\top} r(\ddot{\phi}(t)\mathbf{\bar{u}}, \dot{\phi}(t)\mathbf{\bar{u}}, \phi(t)\mathbf{\bar{u}}, \phi(t)\mathbf{\bar{u}}, \phi(t)\mathbf{\bar{\lambda}}, t)dt = 0$$
(19)

$$\int_{0}^{T} \boldsymbol{\phi}(t)^{\top} s(\boldsymbol{\phi}(t)\bar{\mathbf{u}}, \boldsymbol{\phi}(t)\bar{\boldsymbol{\lambda}}) dt = 0$$
 (20)

- ► Equation (20) is semismooth only: can be solved by semismooth Newton method.
- Advantages over penalty method etc. where contact is enforced in time domain.

Harmonic balance method for contact problems



Example: one degree-of-freedom mass-spring contact system

$$\ddot{u} + 0.1\dot{u} + u = \lambda + 0.2\cos(\omega t), \quad u - 1 \le 0, \quad \lambda \le 0, \quad (u - 1)\lambda = 0$$
 (21)

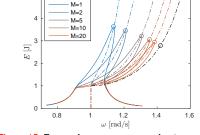


Figure 15: Energy-frequency curves of autonomous system [dashed] and forced system [solid]

Advantages:

- resonance
- energy-frequency dependency properties are reflected

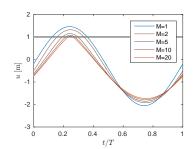


Figure 16: Displacements

Drawbacks:

- slow in convergence
- unavoidable residual penetrations.

Resonance of one degree-of-freedom contact problem



Figure 17: Travelling along resonance

Resonance of two degree-of-freedom contact problem



Figure 18: Travelling along resonance

Summary of the research



- Treatment of contact condition
 - ▶ complementarity contact conditions ⇒ semismooth implicit functions
 - Augmented system
 - Semismooth Newton methods for static contact problems
- ▶ Solving *nonlinear modes* of dynamic contact problems
 - ▶ Harmonic balance methods
 - Proof of the semismooth functions $\bar{\mathbf{s}}(\bar{\mathbf{u}},\bar{\lambda})$ can be solved by the semismooth Newton method
 - Advantages over penalty methods and augmented Lagrange methods
- Properties of the modes of contact problems
 - Resonance
 - ▶ Energy-frequency dependence
 - Sub-harmonic resonance
 - Generalization to multiple degree-of-freedom systems