

## Shallow water

### Partial differential equations

### Model formulation

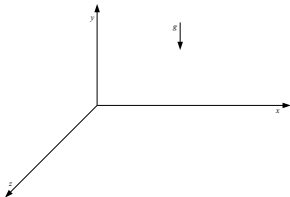
#### Case of smooth solutions

#### Linearization

#### Traveling wave solutions

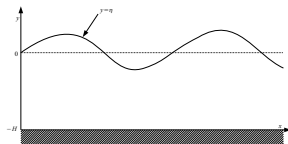
### Spatial domain

We consider the motion of a body of water that is infinite in the  $z$  direction, with or without boundary in the  $x$  direction, and the vertical direction of gravity taken as the  $y$  direction.



From now on, suppose  $z$  direction uniform (the same for all  $z$ ), so ignore  $z$  except for the sake of argument.

- ▶ Water depth at rest,  $H$ , small compared to distance  $L_0$  over which significant changes can occur in the  $x$  direction.
- ▶ Undisturbed water surface,  $y = 0$ .
- ▶ Moving upper free surface  $y = \eta$ , measured from  $y = 0$ .
- ▶ Sea floor  $y = -H$ .

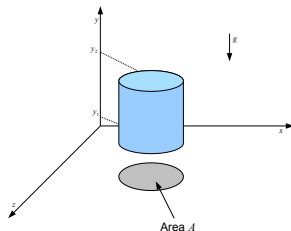


- ▶  $u$  velocity in the  $x$  direction. Assume independent of depth  $y$ .
- ▶  $\rho$  mass density of water.
- ▶  $p(x, y, t)$  pressure in fluid at point  $(x, y)$  at time  $t$ . In water, magnitude at any  $(x, y)$  is same in all directions.

Fluid motion independent of  $z$ , so

- ▶  $u = u(x, t)$
- ▶  $\eta = \eta(x, t)$ .

Take a cylindrical water column, with base area  $A$ , between  $y_1$  and  $y_2 > y_1$ .



Force equilibrium in the  $y$  direction in this cylinder requires balance of weight of water column and pressure differential between bottom face  $y = y_1$  and top face  $y = y_2$ .

Weight of water column:

$$\iiint_A \int_{y_1}^{y_2} (-\rho g) dy dx dz$$

Pressure differential:

$$\iint_A (p(x, y_2, t) - p(x, y_1, t)) dx dz$$

So we must have

$$\iiint_A \int_{y_1}^{y_2} (-\rho g) dy dx dz = \iint_A (p(x, y_2, t) - p(x, y_1, t)) dx dz$$

$$\iiint_A \int_{y_1}^{y_2} (-\rho g) dy dx dz = \iint_A (p(x, y_2, t) - p(x, y_1, t)) dx dz$$

is equivalent to

$$\iint_A \int_{y_1}^{y_2} \left( \frac{\partial p}{\partial y} + \rho g \right) dy dx dz = 0$$

This must be true for any water column, i.e., any  $A, y_1, y_2$ . Therefore,

$$\frac{\partial p}{\partial y} + \rho g = 0$$

(otherwise, we would be able to find a water column where the integrand is positive, leading to a positive value of the integral on that column).

# Water is incompressible

If you force a body of water to deform, the volume of that body of water remains constant, i.e., water is an *incompressible fluid*.

⇒  $\rho$ , the density, is a constant, and from

$$\frac{\partial p}{\partial y} + \rho g = 0$$

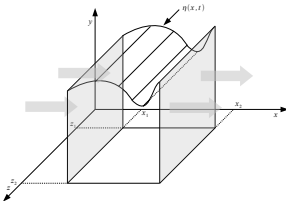
we get

$$p = -\rho g y + C,$$

so if  $p$  is measured relative to the pressure above the free upper surface  $y = \eta$ ,

$$p = \rho g (\eta - y)$$

Water enters  $V$  through  $x_1$  face and leaves  $V$  through  $x_2$  face.



Rate of water accumulation in  $V$  is

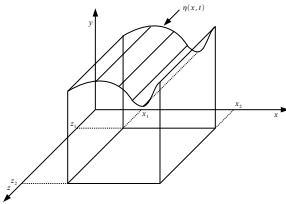
$$\frac{d}{dt} \int_{z_1}^{z_2} \int_{x_1}^{x_2} \int_{-H}^{\eta} \rho \, dy \, dx \, dz = \Delta z \frac{d}{dt} \int_{x_1}^{x_2} \rho h \, dx,$$

with  $\Delta z = z_2 - z_1$ , and  $h(x, t) = \eta + H$  the height of water at time  $t$  at spatial location  $x$ .

# Water accumulation

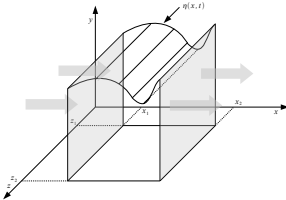
Consider a fixed volume  $V$ ,

$$V = \{z_1 \leq z \leq z_2, x_1 \leq x \leq x_2, -H \leq y \leq \eta\}$$



# Water flux

Net flux of water entering  $V$  through its faces  $x = x_1$  and  $x = x_2$  is



$$\left[ \int_{z_1}^{z_2} \int_{-H}^{\eta} u \, dy \, dz \right]_{x=x_1} - \left[ \int_{z_1}^{z_2} \int_{-H}^{\eta} u \, dy \, dz \right]_{x=x_2} = -\Delta z [\rho u h]_{x_1}^{x_2}$$

There is no flux through  $y = -H$  and  $y = \eta$ , and no net flux through  $z = z_1$  and  $z = z_2$ .

# Conservation of mass

Of course, the mass must conserve in  $V$ , so the two expressions must be equal, i.e.,

$$\frac{d}{dt} \int_{x_1}^{x_2} \rho h \, dx + [\rho u h]_{x_1}^{x_2} = 0$$

Newton's second law for deformable media (Euler): rate of increase of horizontal momentum (in the  $x$  direction) in  $V$  must equal the sum of the net influx of momentum into the volume and the net horizontal force acting on the column.

(Momentum: product of mass and velocity of an object).

Rate of increase of momentum

$$\frac{d}{dt} \int_{z_1}^{z_2} \int_{x_1}^{x_2} \int_{-H}^{\eta} \rho u \, dy dx dz = \Delta z \frac{d}{dt} \int_{x_1}^{x_2} \rho u h dx$$

# Momentum flux

Net influx of momentum through faces  $x = x_1$  and  $x = x_2$  is

$$\left[ \int_{z_1}^{z_2} \int_{-H}^{\eta} (\rho u) u \, dy dz \right]_{x=x_1} - \left[ \int_{z_1}^{z_2} \int_{-H}^{\eta} (\rho u) u \, dy dz \right]_{x=x_2} = -\Delta z [\rho u^2 h]_{x_1}^{x_2}$$

There is no flux through  $y = -H$  and  $y = \eta$ , and no net flux through  $z = z_1$  and  $z = z_2$ .

# Forces acting on $V$

Ignore friction at  $y = -H$ . Then only contributions to horizontal forces come from pressure at  $x = x_1$  and  $x = x_2$ , so net horizontal forces acting on  $V$  is

$$\begin{aligned} \left[ \int_{z_1}^{z_2} \int_{-H}^{\eta} p \, dy dz \right]_{x_1}^{x_2} &= - \left[ \Delta z \int_{-H}^{\eta} \rho g (\eta - y) \, dy \right]_{x_1}^{x_2} \\ &= \left[ -\Delta z \rho g \left( \eta y - \frac{1}{2} y^2 \right) \right]_{-H}^{\eta} \Big|_{x_1}^{x_2} \\ &= \left[ -\frac{1}{2} \Delta z \rho g h^2 \right]_{x_1}^{x_2} \end{aligned}$$

Pressure magnitude:

$$p = \rho g (\eta - y) \tag{1}$$

Horizontal velocity:

$$\frac{d}{dt} \int_{x_1}^{x_2} \rho u h \, dx + \left[ \rho u^2 h + \frac{1}{2} \rho g h^2 \right]_{x_1}^{x_2} = 0 \tag{2}$$

Free surface height:

$$\frac{d}{dt} \int_{x_1}^{x_2} \rho u h \, dx + \left[ \rho u^2 h + \frac{1}{2} \rho g h^2 \right]_{x_1}^{x_2} = 0 \tag{3}$$

Suppose  $u$  and  $h$  are smooth (with continuous first order partial derivatives), then (2) and (3) take a much simpler form,

$$\int_{x_1}^{x_2} \left( \frac{\partial h}{\partial t} + \frac{\partial}{\partial x} (uh) \right) dx = 0$$

and

$$\int_{x_1}^{x_2} \left( \frac{\partial}{\partial t} (uh) + \frac{\partial}{\partial x} (u^2 h + \frac{1}{2} g h^2) \right) dx = 0$$

Since the intervals of integration  $[x_1, x_2]$  are arbitrary, and that the integrands are continuous, we have

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x} (uh) = 0$$

and

$$\frac{\partial}{\partial t} (uh) + \frac{\partial}{\partial x} (u^2 h + \frac{1}{2} g h^2) = 0$$

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We write

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(uh) = 0$$

and

$$\frac{\partial}{\partial t}(uh) + \frac{\partial}{\partial x}(u^2h + \frac{1}{2}gh^2) = 0$$

as

$$h_t + (uh)_x = 0 \quad (4)$$

and

$$(uh)_t + (u^2h + \frac{1}{2}gh^2)_x = 0 \quad (5)$$

From (4),

$$h_t = -(uh)_x = -(u_xh + uh_x)$$

Equation (5) can be rewritten as

$$\begin{aligned} (5) &\Leftrightarrow u_t h + u h_t + (u^2 h + \frac{1}{2} g h^2)_x = 0 \\ &\Leftrightarrow u_t h - u(u_x h + u h_x) + 2 u u_x h + u^2 h_x + g h h_x = 0 \\ &\Leftrightarrow u_t h - u u_x h - \cancel{u^2 h_x} + 2 u u_x h + \cancel{u^2 h_x} + g h h_x = 0 \\ &\Leftrightarrow u_t h + u u_x h + g h h_x = 0 \end{aligned}$$

Therefore, provided  $h \neq 0$ , we get

$$h_t + (uh)_x = 0 \quad (6a)$$

$$u_t + u u_x + g h_x = 0 \quad (6b)$$

which describes the evolution of  $u$  and  $h$ .

## The model for smooth solutions

$$h_t + (uh)_x = 0 \quad (6a)$$

$$u_t + u u_x + g h_x = 0 \quad (6b)$$

If  $-\infty < x < \infty$ , then all we need is an initial condition, i.e., functions describing the initial state of  $u$  and  $h$ :

$$u(x, 0) = u_0(x), \quad h(x, 0) = h_0(x), \quad -\infty < x < \infty.$$

If  $x$  has a boundary, then we need boundary conditions.

### Model formulation

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Suppose the bottom is flat ( $H$  is constant), and that the deviation from the undisturbed depth  $H$  is small compared to  $H$  itself, then

$$h = (H + \zeta) = H(1 + \frac{\zeta}{H}) \simeq H, \quad h_t = \zeta_t, \quad h_x = \zeta_x.$$

If  $|u|$  is also small, then  $uu_x$  can be neglected. Then we can linearize

$$h_t + (uh)_x = 0 \quad (6a)$$

$$u_t + uu_x + gh_x = 0, \quad (6b)$$

getting

$$\zeta_t + Hu_x = 0 \quad (7a)$$

$$u_t + g\zeta_x = 0 \quad (7b)$$

Differentiate (7b) with respect to  $x$ :

$$u_{tx} + g\zeta_{xx} = 0$$

and therefore,

$$u_{tx} = -g\zeta_{xx} \quad (8)$$

Differentiate (7a) with respect to  $t$ :

$$\zeta_{tt} + Hu_{xt} = 0 \quad (9)$$

If  $u$  has continuous second-order partial derivatives, then from Clairaut's theorem,  $u_{tx} = u_{xt}$ . Therefore, substituting (8) into (9),

$$\zeta_{tt} - HG\zeta_{xx} = 0$$

that is

$$\zeta_{tt} = c^2\zeta_{xx}, \quad c^2 = Hg$$

## The one-dimensional wave equation (1)

The partial differential equation

$$\zeta_{tt} = c^2\zeta_{xx} \quad (10)$$

with  $c^2 = Hg$ , is the one-dimensional wave equation. Initial conditions are given by

$$\zeta(x, 0) = h_0(x) - H \equiv \zeta_0(x)$$

$$\zeta_t(x, 0) = -Hu_x(x, 0) = -H[u_0(x)]_x \equiv v_0(x)$$

## The one-dimensional wave equation (2)

Things can also be expressed in terms of  $u$ . Using the same type of simplification used before for  $\zeta$ , we get

$$u_{tt} = c^2u_{xx} \quad (11)$$

with  $c^2 = Hg$ . Initial conditions are given by

$$u(x, 0) = u_0(x)$$

$$u_t(x, 0) = -g\zeta_x(x, 0) = -g[h_0(x)]_x \equiv v_0(x)$$

## Model formulation

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This was obtained by d'Alembert. Consider

$$u_{tt} = c^2 u_{xx} \quad (11)$$

Note that this can be written as

$$\left( \frac{\partial}{\partial t} - c \frac{\partial}{\partial x} \right) \left( \frac{\partial}{\partial t} + c \frac{\partial}{\partial x} \right) u = 0$$

This implies that for any  $F, G$ , the sum

$$u(x, t) = F(x - ct) + G(x + ct)$$

satisfies (11).

Traveling wave solutions

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## Derivation of the solution

Introduce the new variables

$$a = x - ct \quad \text{and} \quad b = x + ct$$

We have

$$\frac{\partial u}{\partial x} = \frac{\partial u}{\partial a} + \frac{\partial u}{\partial b} \quad \frac{\partial u}{\partial t} = -c \frac{\partial u}{\partial a} + c \frac{\partial u}{\partial b}$$

$$\frac{\partial^2}{\partial x^2} u = \left( \frac{\partial}{\partial a} + \frac{\partial}{\partial b} \right)^2 u = \frac{\partial^2 u}{\partial a^2} + 2 \frac{\partial^2 u}{\partial a \partial b} + \frac{\partial^2 u}{\partial b^2}$$

$$\frac{\partial^2}{\partial t^2} u = \left( -c \frac{\partial}{\partial a} + c \frac{\partial}{\partial b} \right)^2 u = c^2 \left( \frac{\partial^2 u}{\partial a^2} - 2 \frac{\partial^2 u}{\partial a \partial b} + \frac{\partial^2 u}{\partial b^2} \right)$$

So the equation

$$u_{tt} = c^2 u_{xx} \quad (11)$$

is written

$$4 \frac{\partial^2 u}{\partial a \partial b} = 0$$

Integrate with respect to  $b$ :

$$\frac{\partial u}{\partial a} = \xi(a)$$

and thus

$$\begin{aligned} u(x, t) = u(a, b) &= \int \xi(a) da + G(b) \\ &= F(a) + G(b) \\ &= F(x - ct) + G(x + ct) \end{aligned}$$



Set

$$u(x, 0) = f(x) \quad u_t(x, 0) = g(x)$$

Then d'Alembert's formula gives

$$u(x, t) = \frac{f(x - ct) + f(x + ct)}{2} + \frac{1}{2c} \int_{x-ct}^{x+ct} g(s) ds$$

Suppose  $u_0(x) = 0$  and  $v_0(x) = \delta(x)$ , for  $-\infty < x < \infty$ , with  $\delta$  the Dirac delta,

$$\delta(x) = \begin{cases} \infty & \text{if } x = 0 \\ 0 & \text{otherwise.} \end{cases}$$

Therefore,

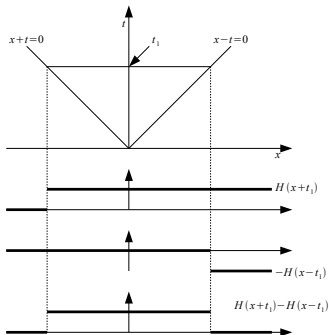
$$u(x, t) = \frac{1}{2c} \int_{x-ct}^{x+ct} \delta(z) dz = \frac{1}{2c} \{H(x + ct) - H(x - ct)\},$$

with  $H$  the Heaviside function,

$$H(x) = \begin{cases} 0 & \text{if } x < 0 \\ 1 & \text{if } x > 0. \end{cases}$$

For simplicity, take  $c = 1$ . This gives

$$u(x, t) = \frac{1}{2} \{H(x + t) - H(x - t)\},$$



As  $t$  increases, we move further up in the top graph in  $(x, t)$ -space, resulting in a wider and wider square pulse.

