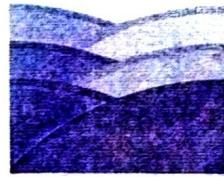


A40401- SIGNALS, SYSTEMS AND STOCHASTIC PROCESSES



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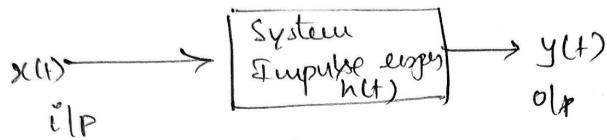
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UNIT - I

System \downarrow A system is defined as a set of ^{U-T} elements of functional blocks which are connected together & produces an o/p in response of an i/p sig.



A system is represented by a block diagram as shown in figure. An arrow entering the box is the i/p sig (called excitation, source or driving function) and an arrow leaving the box is an o/p sig (called response). Generally denoted by $x(t)$ & o/p in $y(t)$

The relation b/w $x(t)$ & $y(t)$ of System has a form

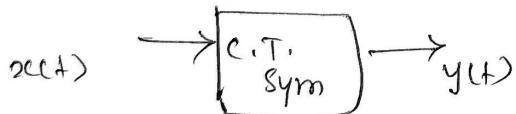
mathematically

$$y(t) = T[x(t)]$$

\downarrow
Transfer function

Systems are broadly classified
 1. C.T. Sys
 2. D.T. Sys

C.T Sym



D.T Sym



Again C.T & D.T sys are classified into

1. Lumped & Distributed Sym
2. Static (memoryless) & Dynamic Systems
3. Causal & Non Causal Sym
4. Linear & Non Linear Sym
5. Time Varying & Time-invariant Sym
6. Stable & Unstable System
7. Invertible & Non Invertible System
8. FIR & IIR Systems

→ 1 Linear & Non linear Systems

A sys which obeys the principle of superposition & principle of homogeneity is called a linear system. which doesn't obey the principle of superposition and homogeneity is called non-linear system.

Homogeneity property means a system which produces an o/p $y(t)$ for an i/p $x(t)$ must produce an o/p $a y(t)$ for an i/p $a x(t)$.

Superposition means a system which produces an o/p $y_1(t)$ for an input $x_1(t)$ & an o/p $y_2(t)$ for an arbitrary i/p $x_2(t)$ produces an o/p $y_1(t) + y_2(t)$ then the weighted sum of i/p's $a x_1(t) + b x_2(t)$ where a, b are constants, produces an o/p $a y_1(t) + b y_2(t)$ which is the sum of weighted o/p. that is

$$T[a x_1(t) + b x_2(t)] = a T[x_1(t)] + b T[x_2(t)]$$

Note:- In general, if the describing equation contains square or higher order terms & i/p's and product of i/p & its derivative of a constant, the system will definitely be non-linear

$$1. \quad y(n) = n^2 x(n)$$

$$\text{sgt } y(n) = n^2 x_1(n)$$

$$y_2(n) = n^2 x_2(n)$$

$$\text{Weighted sum of o/p's} \\ a y_1(n) + b y_2(n) = a[n^2 x_1(n)] + b[n^2 x_2(n)]$$

$$\text{o/p due to weighted sum of i/p's} \\ y_3(n) = T[a x_1(n) + b x_2(n)]$$

$$y_3(n) = n^2 [a x_1(n) + b x_2(n)]$$

∴ System is linear

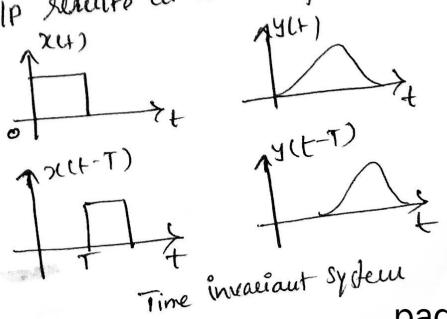
Time varying & Time invariant system

Time invariance is the property of a system which makes the behaviour of the system independent of time. Means behaviour of the sys doesn't depend on the time at which the i/p is applied.

A System is said to be time-invariant (or shift-invariant) if its i/o characteristics do not change with time i.e. if a time shift in the i/p results in a corresponding time shift in the output

$$\text{Then } x(t) \rightarrow y(t) \\ x(t-T) \rightarrow y(t-T)$$

A System not satisfying the above requirements is called a time-varying system (or shift varying system)



Ex: Determine whether the following systems are time-invariant or not.

(a) $y(t) = t^2 x(t)$
~~if~~ $y(t+T) = (t+T)^2 x(t+T)$
 $y(t-T) = (t-T)^2 x(t-T)$

$$y(t) \neq y(t-T)$$

Time-invariant System

(d) $y(t) = x(-2t)$
~~if~~ $y(t+T) = x(-2t-T)$
 $y(t-T) = x(-2(t-T))$

$$y(t) \neq y(t-T)$$

Time-variant system

(g) $y(n) = x(n)$
~~if~~ $y(n, k) = x(n-k)$
 $y(n-k) = x(n-k)$

Time-invariant system

(b) $y(t) = x(t) \sin \omega_0 t$
~~if~~ $y(t+T) = x(t+T) \sin \omega_0 t$
 $y(t-T) = x(t-T) \sin \omega_0 (t-T)$

$$y(t) \neq y(t-T)$$

Time-invariant system

(c) $y(t) = x(t^2)$
~~if~~ $y(t-T) = x((t-T)^2)$

$$y(t) \neq y(t-T)$$

Time-variant system.

(e) $y(t) = e^{2x(t)}$
~~if~~ $y(t-T) = e^{2x(t-T)}$
 $y(t-T) = e^{2x(t-T)}$

Time-invariant system

(f) $y(n) = x(n/2)$
~~if~~ $y(n-k) = x(\frac{n-k}{2})$
 $y(n-k) = x(\frac{n-k}{2})$

$$y(n) \neq y(n-k)$$

Time-variant

(h) $y(n) = n^2 (n-2)$
~~if~~ $y(n, k) = n^2 (n-k-2)$
 $y(n-k) = n^2 (n-k-2)$

Time-invariant system

(i) $y(n) = x(n) + n x(n-2)$
~~if~~ $y(n-k) = x(n-k) + (n-k) x(n-k-2)$
 $y(n-k) = x(n-k) + n x(n-k-2)$

Time-variant

3. Causal and Non-causal Systems
A system is said to be causal (or non-anticipative) if the output of the system at any time t depends only on the present and past values of the input but not on future inputs.

Causal systems are real time systems. They are physically realizable. The impulse response of a causal system is zero for $t < 0$ since $\delta(t)$ [$\delta(n)$] exists only at $t = 0$.

$$h(t) = 0 \text{ for } t < 0 \text{ and } h(n) = 0 \text{ for } n < 0.$$

A system said to be non-causal (anticipative) if the OLP of the system at any time t depends on future IIPs. They do not exist in real time. They are not physically realizable.

Ex: Check whether the following systems are causal or not.

(a) $y(t) = x^2(t) + x(t-u) \Rightarrow y(-2) = x(-2) + x(-6)$

~~if~~ $t = -2 \quad y(-2) = x^2(-2) + x(-2-4)$

$$y(-2) = x^2(0) + x(-4)$$

$t = 0 \quad y(0) = x^2(0) + x(-u)$

$$y(0) = x^2(2) + x(-2)$$

$t = 2 \quad y(2) = x^2(2) + x(-4)$

The OLP depends only on present & past values of IIP.

Therefore the system is causal.

(b) $y(t) = x(2-t) + x(t-u)$

$t = -1 \quad y(-1) = x(1) + x(-5)$

$$y(-1) = x(2) + x(-4)$$

$t = 0 \quad y(0) = x(2) + x(-u)$

$$y(0) = x(1) + x(-3)$$

$t = 1 \quad y(1) = x(1) + x(-3)$

$y(1) = x(0) + x(-2)$

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4 Stable & Unstable Systems

A bounded signal is a signal whose magnitude is always a finite value. For example, a sine wave is a bounded signal. A system is said to be bounded-input, bounded-output (BIBO) stable if and only if every bounded input produces a bounded output. i.e., a stable system does not diverge or does not grow unreasonably large.

The input signal $x(t)$ be bounded (finite) i.e,

$$|x(t)| \leq M_x < \infty \text{ for all } t.$$

M_x is the real number

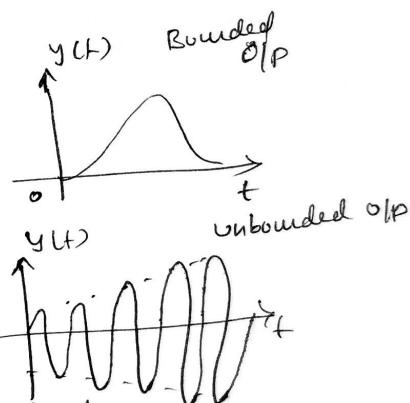
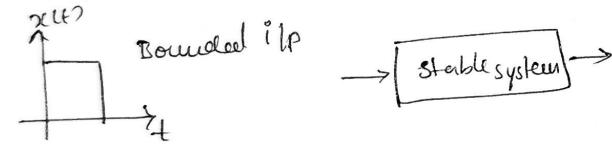
$$\begin{cases} \because e^{\infty} = \infty \\ e^{-\infty} = 0 \end{cases}$$

$$|y(t)| \leq M_y < \infty$$

$y(t)$ is also bounded, then the system is BIBO stable. Otherwise the system is unstable.

BIBO stability criterion: $\int_{-\infty}^{\infty} |h(t)| dt < \infty$

where $h(t)$ is the impulse response of the system. This is called BIBO stability criterion.



Ex: Find whether the following systems are stable or not.

(a) $y(t) = e^{x(t)}$; $|x(t)| \leq 8$

sgn: $|x(t)| \leq 8$ I/P Bounded

$$e^8 \leq y(t) \leq e^8$$

O/P also bounded.

∴ System is stable

(b) $y(t) = (t+5) u(t)$

sgn: $y(t) = (t+5) \quad t \geq 0$

$t \rightarrow \infty ; y(t) \rightarrow \infty$

Hence O/P grows without any bounded & hence the given system is unstable.

(c) $h(t) = (2 + e^{-3t}) u(t)$

$$\int_{-\infty}^{\infty} h(t) dt = \int_0^{\infty} (2 + e^{-3t}) dt$$

$$= 2[\infty - 0] + \frac{e^{-3t}}{-3} \Big|_0^{\infty}$$

(d) $h(t) = e^{2t} u(t)$

$$\int_{-\infty}^{\infty} h(t) dt = \int_{-\infty}^{\infty} e^{2t} u(t) dt = \int_{-\infty}^{\infty} h(t) dt = \infty$$

System is unstable.

(e) $h(t) = \frac{1}{RC} e^{-t/RC} u(t)$

$$= \frac{1}{RC} \int_0^{\infty} e^{-t/RC} dt$$

$$= \frac{1}{RC} (-RC) [e^{-\infty} - e^0]$$

$$= \frac{1}{RC} (-RC) [0 - 1] = \frac{1}{RC}$$

Hence stable

$$\int_{-\infty}^{\infty} h(t) dt = \int_{-\infty}^{\infty} e^{2t} u(t) dt$$

$$= \int_0^{\infty} e^{2t} dt$$

$$= \frac{e^{2t}}{2} \Big|_0^{\infty} = \infty \text{ Hence unstable}$$

5. Static & Dynamic System

A System is said to be static or memoryless if the response is due to present input alone i.e., for a static or memoryless system, the o/p at any instant t (δt) depends only on the ip applied at that instant t (δu) but not over the past or future values of input.

Ex:- $y(t) = x(t)$ $y(u) = x(u)$
 $y(t) = x^2(t)$ $y(u) = x^2(u)$

In contrast, a system is said to be dynamic or memory system if the response depends upon past / future inputs. $y(u) = x(u) + x(u-2)$.

Ex:- $y(t) = x(t-1)$ $y(t) = \frac{d^2x(t)}{dt^2} + x(t)$
 $y(t) = x(t) + x(t+2)$ $y(u) = x(2u)$

For C.T-Sym \rightarrow Static System \rightarrow purely resistive electrical Ckt
 \rightarrow Dynamic system \rightarrow ele ckt having inductors and/or capacitors.

For D.T-Sym \rightarrow static system \rightarrow Summer / Accumulator
 \rightarrow Dynamic system \rightarrow A delay is also D.T-Sym with memory

Ex:- find whether the following systems are dynamic or not.

(a) $y(t) = x(t-3)$

$y(0) = x(0-3) = x(-3)$

$y(1) = x(1-3) = x(-2)$

$y(2) = x(2-3) = x(-1)$

$y(3) = x(3-3) = x(0)$

depends on past I/P

\therefore Dynamic system

(b) $y(t) = x(2t)$

$y(0) = x(0)$

$y(1) = x(2)$

$y(2) = x(4)$

depends on future I/P,
Dynamic system

(c) $y(t) = \frac{d^2x(t)}{dt^2} + 2x(t)$

$y(0) = \frac{d^2x(0)}{dt^2} + 2x(0)$

$y(1) = \frac{d^2x(1)}{dt^2} + 2x(1)$

$y(2) = \frac{d^2x(2)}{dt^2} + 2x(2)$

\therefore Dynamic systems
Differential Equations
come under

(d) $y(u) = x(u+2)$

Dynamic system

(e) $y(u) = x^2(u)$

static system

(f) $y(u) = x(u-2) + x(u)$

Dynamic system.

⑥ Lumped & Distributed System

Lumped parameter systems are the systems in which each component is lumped at one point in space. These systems are described by ordinary differential equations.

Distributed systems are the systems in which signals are functions of space as well as time. These systems are described by partial differential equations.

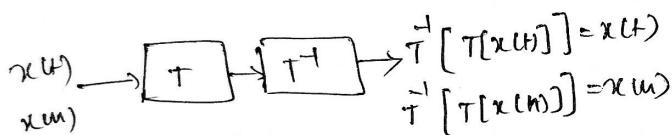
7. Invertible & Non-invertible Systems

If a system has a unique relationship b/w its I/p $x(t)$ (or $x[n]$) and output $y(t)$ [or $y[n]$] the system is known as invertible. Therefore, for an invertible system if $y(t)$ [or $y[n]$] is known $x(t)$ [or $x[n]$] can be found out unambiguously and uniquely.

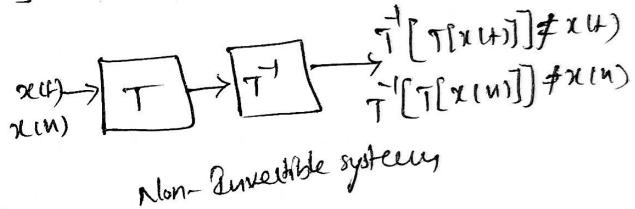
On the other hand, if the system does not have a unique relationship b/w its I/p and O/p. the system is said to be non-invertible. In other words a system is known as invertible only if an inverse system exists which when cascaded with the original system produces an o/p equal to the I/p of the first system.

Mathematically \Rightarrow a system is to be invertible if

$$x(t) = T^{-1}\{T\{x(t)\}\}$$



Invertible System



Non-Invertible system

8. FIR and IIR Systems

LTI sys. can be classified according to the type of impulse response.
 If impulse response sequence is of finite duration - finite impulse response
 If impulse response sequence is of infinite duration - infinite impulse response

$$\text{FIR } h(n) = \begin{cases} 2 & n=0 \\ 0 & \text{otherwise} \end{cases}$$

$$\text{IIR } h(n) = 2^n u(n)$$

Q State whether the following system is linear, causal, time invariant and stable

$$y(n) + y(n-1) = x(n) + x(n-2)$$

Given $y(n) = -y(n-1) + x(n) + x(n-2)$

1. $a_1 y_1(n) + b y_2(n) = -[a_1 y_1(n-1) + b y_2(n-2)]$

Weighted sum of o/p = $-a_1 y_1(n-1) + a_1 x_1(n) + a_1 x_1(n-2) + b y_2(n-1)$
 $+ b x_2(n) + b x_2(n-2)$

$$= [a_1 y_1(n-1) + b y_2(n-1)] + [a_1 x_1(n) + b x_2(n)] \\ + [b x_2(n-1) + b x_2(n-2)] \rightarrow (1)$$

2. O/p of weighted sum if $y_3(n) = [a_1 y_1(n-1) + b y_2(n-1)]$

$$+ [a_1 x_1(n) + b x_2(n)] + [a_1 x_1(n-1) \\ + b x_2(n-2)] \rightarrow (2)$$

From Eqn (1) & (2) both are equal then

System is linear system

2. The o/p depends only on the present & past o/p's & past o/p's.
 So the system is causal.

3. All the coeff of the differential equation are constants.. So the system
 is time invariant.

4. For $x(n) = \delta(n)$ $y(n) = h(n)$

$$h(n) = -h(n-1) + \delta(n) + \delta(n-2)$$

$$h(0) = -h(-1) + \delta(0) + \delta(-2) = 1$$

$$h(1) = -h(0) + \delta(1) + \delta(-1) = -1$$

$$h(2) = -h(1) + \delta(2) + \delta(0) = 1 + 0 + 1 = 2$$

$$h(3) = -h(2) + \delta(3) + \delta(1) = -2 + 0 + 1 = -1$$

$$\sum_{n=-\infty}^{\infty} |h(n)| = 1 + 1 + 2 + 2 + \dots = \infty$$

Summable

integrable so the

impulse response is not absolutely

system is unstable

Comment about the linearity, stability, time invariance and causality we
the following filter.

$$y(n) = 2x(n+1) + [x(n-1)]^2$$

Given $y(n) = 2x(n+1) + [x(n-1)]^2$

1. There is a square term of delayed ip [i.e. $x(n-1)^2$] in the differential equation. So the system is non-linear.

2. The oip depends on the future value of ip [i.e., $x(n+1)$] So the system is non-causal.

3. If $x(n) = \delta(n)$, $y(n) = h(n)$
 $\therefore h(n) = 2\delta(n+1) + [\delta(n-1)]^2$

$$h(0) = 2\delta(1) + [\delta(-1)]^2 = 0+0=0$$

$$h(1) = 2\delta(2) + [\delta(0)]^2 = 0+1=1$$

$$h(-1) = 2\delta(0) + [\delta(-2)]^2 = 2+0=2$$

$$h(-2) = 2\delta(-1) + [\delta(-3)]^2 = 0+0=0$$

$$h(n) = 0 \text{ for any other } n$$

$$\sum_{n=-\infty}^{\infty} |h(n)| = 0+1+2+0+0+\dots = 3 < \infty$$

Impulse response is absolutely summable so system is stable.

4. The oip due to delayed input is given by

$$y(n, k) = 2x(n+1-k) + [x(n-1-k)]^2$$

The delayed output is

$$y(n-k) = 2x(n+1-k) + [x(n-k-1)]^2$$

$$y(n, k) = y(n-k)$$

\therefore The system is time-invariant.

Convolution :- It is a mathematical way of combining two signals to form a third signal. It is important because it relates the input signal & impulse response of the system to the output of the system.

Correlation :- It compares two signals in order to determine the degree of similarities b/w them.

Auto correlation - when one signal is correlated with itself to form another signal.

Cross correlation - when one signal is correlated with another signal to form a third signal.

Concept of Convolution :-

Convolution is a mathematical operation which is used to Express the input & output relationship of an LTI system.

Let us consider an LTI system which is initially relaxed at $t = 0$ if the input to the system is an impulse, then the output of the system is denoted by $h(t)$ and is called Impulse response of the system.

$$\text{Impulse response } h(t) = T[\delta(t)] \rightarrow ①$$

For any arbitrary signal $x(t)$ can be represented as

$$x(t) = \int_{-\infty}^{\infty} x(\tau) \delta(t-\tau) d\tau \rightarrow ②$$

$$\begin{aligned} \text{System o/p } y(t) &= T[x(t)] = T \left[\int_{-\infty}^{\infty} x(\tau) \delta(t-\tau) d\tau \right] \\ &= \int_{-\infty}^{\infty} x(\tau) T[\delta(t-\tau)] d\tau \end{aligned}$$

$$y(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau \rightarrow ③$$

This is called Convolution integral, or simply convolution

The Convolution of two signals can be represented as

$$y(t) = x(t) * h(t)$$

$$y(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau \quad \begin{array}{l} \text{when } x(t), h(t) \text{ are non causal} \\ \text{when } h(t) \text{ is causal } x(t) \text{ non causal} \end{array}$$

$$y(t) = \int_{-\infty}^t x(\tau) h(t-\tau) d\tau \quad \begin{array}{l} \text{when } h(t) \text{ is non causal } x(t) \text{ is causal} \end{array}$$

$$y(t) = \int_0^t x(\tau) h(t-\tau) d\tau \quad \begin{array}{l} \text{when both } x(t), h(t) \text{ are causal} \end{array}$$

Properties of Convolution

1. Commutative property

$$x_1(t) * x_2(t) = x_2(t) * x_1(t)$$

2. Distributive property

$$x_1(t) * [x_2(t) + x_3(t)] = [x_1(t) * x_2(t)] + [x_1(t) * x_3(t)]$$

3. Associative property

$$x_1(t) * [x_2(t) * x_3(t)] = [x_1(t) * x_2(t)] * x_3(t)$$

4. Shift property -

$$x_1(t) * x_2(t) = z(t)$$

$$x_1(t) * x_2(t-T) = z(t-T)$$

$$x_1(t-T) * x_2(t) = z(t-T)$$

$$x_1(t-T_1) * x_2(t-T_2) = z(t-T_1-T_2)$$

5. Convolution with impulse

$$x(t) * \delta(t) = x(t)$$

6. wide property - let duration of $x_1(t)$ & $x_2(t)$ be T_1 & T_2 respectively
then the duration of the signal obtained by convoluting $x_1(t)$ & $x_2(t)$
is $T_1 + T_2$.

Ex find convolution of the following signals.

$$x_1(t) = e^{-2t} u(t) \quad x_2(t) = e^{-4t} u(t)$$

$$\begin{aligned}
 x_1(t) * x_2(t) &= \int_{-\infty}^{\infty} x_1(\tau) x_2(t-\tau) d\tau \\
 &= \int_{-\infty}^{\infty} e^{-2\tau} u(\tau) e^{-4(t-\tau)} u(t-\tau) d\tau \\
 &= \int_0^t e^{-2\tau} e^{-4t} e^{4\tau} d\tau \\
 &= e^{-4t} \int_0^t e^{2\tau} d\tau \\
 &= e^{-4t} \left[\frac{e^{2\tau}}{2} \right]_0^t = \frac{e^{-4t}}{2} [e^{2t} - e^0] \\
 &= \frac{e^{-2t}}{2} - \frac{e^{-4t}}{2} = \frac{e^{-2t} - e^{-4t}}{2} u(t).
 \end{aligned}$$

$$u(\tau) = 1 \text{ for } \tau > 0$$

$$u(t-\tau) = 1 \text{ for } t > \tau$$

Correlation Concept q- it compares two signals in order to determine the degree of similarities b/w them.

The integral $\int_{t_1}^{t_2} x_1(t) x_2(t) dt$ forms the basis of comparison of the two signals $x_1(t)$ & $x_2(t)$ over the interval (t_1, t_2)

If $x_1(t)$ & $x_2(t)$ have no similarities over the interval (t_1, t_2) then

$$\int_{t_1}^{t_2} x_1(t) x_2(t) dt = 0.$$

→ Auto correlation - it gives the measure of match similarities & relatedness or coherence b/w a signal & its time delayed version. It is defined as the

correlation of a signal with itself.

It is represented with $R(\tau) = R(\tau) = \int_{-\infty}^{\infty} x(t) x^*(t-\tau) dt$.

$$① R_1(\tau) = R(-\tau) - \text{Conjugate symmetry}$$

$$② R(\tau) \geq R(0) \geq R(\tau)$$

$$③ F[R(\tau)] \leftrightarrow S(\omega)$$

→ Cross correlation - it measures the similarities of two different signals in that one signal, another signal delayed version of $x_1(t)$.

The cross correlation b/w two different waveforms of signals is a measure of similarity or match or relatedness or coherence b/w one signal and time delayed version of another signal. That means it indicates how much one signal is related to the time delayed version of another signal.

It is represented with $R_{12}(\tau) = \int_{-\infty}^{\infty} x_1(t) x_2^*(t-\tau) dt$

$$R_{21}(\tau) = \int_{-\infty}^{\infty} x_2(t) x_1^*(t-\tau) dt$$

$$(d) R_{12}(-\tau) = \int_{-\infty}^{\infty} x_1(t+\tau) x_2^*(t) dt$$

① Conjugate symmetry - $R_{12}(\tau) = R_{21}^*(-\tau)$ means two signals are orthogonal signals.

② If $\int_{-\infty}^{\infty} x_1(t) x_2^*(t) dt = 0$ means multiplication of the FT of one &

③ $R_{12}(\tau) \leftrightarrow X_1(\omega) X_2^*(\omega)$, Complex conjugate of FT of second signal

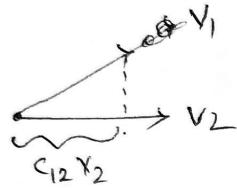
Analogy b/w vectors & signals :- (Summary)

Vector

- The dot product b/w the vectors v_1 & v_2 is $v_1 \cdot v_2$

$$v_1 \cdot v_1 = v_1^2$$

- Consider two vectors v_1 & v_2



the component v_1 along $v_2 = c_{12} v_2$

- The value of c_{12} in $c_{12} = \frac{v_1 \cdot v_2}{v_2^2}$

- If two vectors v_1 & v_2 are orthogonal to each other $v_1 \cdot v_2 = 0$

5. If x_1, x_2, \dots, x_n unit vectors along 'n' mutually 1D axes then any vector A which has components c_1, c_2, \dots, c_n along these mutually 1D can be written as

$$A = c_1 x_1 + c_2 x_2 + \dots + c_n x_n$$

- The component ' c_k ' is

$$c_k = \frac{A \cdot x_k}{x_k \cdot x_k}$$

Signal

- The dot product is equivalent to

$$v_1 \cdot v_2 \approx \int_{t_1}^{t_2} x_1(t) x_2(t) dt$$

$$v_1 \cdot v_2 \approx \int_{t_1}^{t_2} x_1^2(t) dt$$

- Consider two signals $x_1(t), x_2(t)$ in the interval $t_1 < t < t_2$

then $x_i(t)$ can be approximated using

$$x_i(t) \approx c_{12} x_2(t). \quad t_1 < t < t_2$$

- The value of c_{12} at which mean square error will be minimum is

$$c_{12} = \frac{\int_{t_1}^{t_2} x_1(t) x_2(t) dt}{\int_{t_1}^{t_2} x_2^2(t) dt}$$

- If two signals $x_1(t) \& x_2(t)$ are orthogonal in interval $t_1 < t < t_2$

$$\int_{t_1}^{t_2} x_1(t) x_2(t) dt = 0.$$

- If $g_1(t), g_2(t), \dots, g_n(t)$ are mutually orthogonal signals in interval $t_1 < t < t_2$ then any function $x(t)$ can be approximated

$$x(t) \approx c_1 g_1(t) + c_2 g_2(t) + \dots + c_n g_n(t) \quad t_1 < t < t_2$$

$$c_k = \frac{\int_{t_1}^{t_2} x(t) g_k(t) dt}{\int_{t_1}^{t_2} g_k^2(t) dt}$$

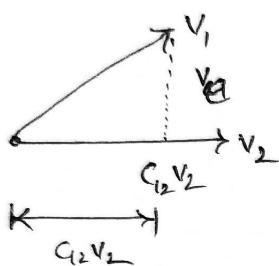
Analogy b/w vectors & signals

(Similarities)

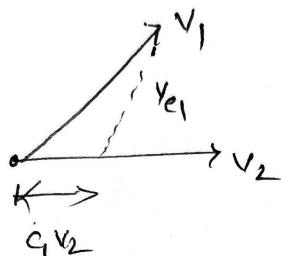
Vector :- Any physical quantity which has both magnitude & direction is called a "vector".

Ex Velocity, Acceleration, force, ele fld, etc.

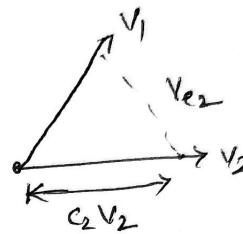
Let us consider two vectors v_1 & v_2



$$v_1 = c_{12} v_2 + v_{1\parallel}$$



$$v_1 = c_1 v_2 + v_{1\perp}$$



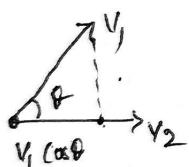
$$v_1 = c_2 v_2 + v_{2\perp}$$

$$\boxed{\cos \theta = \frac{v_2}{v_1}}$$

$$v_2 = v_1 \cos \theta$$

where $v_{1\parallel}, v_{1\perp}, v_{2\perp}$ are zero vectors.

The component of v_1 along $v_2 = c_{12} v_2$



$$v_1 \cos \theta = c_{12} v_2$$

From dot product definition

$$v_1 \cdot v_2 = v_1 v_2 \cos \theta$$

$$\frac{v_1 \cdot v_2}{v_2} = v_1 \cos \theta$$

$$\frac{v_1 \cdot v_2}{v_2} = c_{12} v_2$$

$$\boxed{c_{12} = \frac{v_1 \cdot v_2}{v_2^2}}$$

$$\text{If } c_{12} = 0 \text{ then } 0 = \frac{v_1 \cdot v_2}{v_2^2}$$

$$\boxed{v_1 \cdot v_2 = 0}$$

i.e., two vectors v_1 & v_2 are mutually \perp to each other.

In other words there is no component of v_1 along v_2

$$\text{Ex:- } v_1 = 3i + 3j + 3k$$

$$v_2 = i + j + k$$

$$v_1 = c_{12} v_2$$

$$c_{12} = \frac{v_1 \cdot v_2}{v_2^2} = \frac{(3i + 3j + 3k) \cdot (i + j + k)}{(i^2 + j^2 + k^2)^2} = \frac{3+3+3}{(1+1+1)^2} = \frac{9}{3} = 3.$$

$$\boxed{c_{12} = 3} \\ v_1 = 3v_2$$

Signals :- Let us consider two signals $x_1(t)$ & $x_2(t)$ in the interval $t_1 < t < t_2$. Approximate $x_1(t)$ in terms of $x_2(t)$ over a certain interval ($t_1 < t < t_2$) as follows.

$$x_1(t) = c_{12} x_2(t) \quad \text{for } t_1 < t < t_2.$$

To minimize the error b/w the actual function & the approximated function over the interval ($t_1 < t < t_2$)

The error function $x_e(t)$ is defined as:

$$x_e(t) = x_1(t) - c_{12} x_2(t)$$

To minimize the error $x_e(t)$ over the interval t_1 to t_2 by minimizing the average value of $x_e(t)$ over this interval. i.e., by minimizing

$$\frac{1}{t_2 - t_1} \int_{t_1}^{t_2} x_e(t) dt \quad \text{if } \frac{1}{t_2 - t_1} \int_{t_1}^{t_2} [x_1(t) - c_{12} x_2(t)] dt$$

It may give wrong result being large due to -ve errors present in t_1 to t_2 that may cancel one another in the process of averaging and give the false indication that the error is zero.

To overcome this we choose to minimize the mean square of the error instead of the error itself.

Let us designate the average of squared error $x_e^2(t)$ by ϵ

$$\epsilon = \frac{1}{t_2 - t_1} \int_{t_1}^{t_2} x_e^2(t) dt = \frac{1}{t_2 - t_1} \int_{t_1}^{t_2} [x_1(t) - c_{12} x_2(t)]^2 dt$$

The value of c_{12} which minimizes ϵ can be found from $\frac{d\epsilon}{dc_{12}} = 0$

$$\text{The value of } c_{12} \text{ which minimizes } \left[\frac{1}{t_2 - t_1} \int_{t_1}^{t_2} [x_1(t) - c_{12} x_2(t)]^2 dt \right] = 0.$$

$$\frac{d\epsilon}{dc_{12}} = \frac{d}{dc_{12}} \left[\frac{1}{t_2 - t_1} \int_{t_1}^{t_2} [x_1(t) - c_{12} x_2(t)]^2 dt \right] = 0$$

$$\frac{1}{t_2 - t_1} \left[\frac{d}{dc_{12}} \int_{t_1}^{t_2} [x_1(t)^2 + c_{12}^2 x_2(t)^2 - 2 x_1(t) c_{12} x_2(t)] dt \right] = 0$$

$$\frac{1}{t_2 - t_1} \left[\int_{t_1}^{t_2} \frac{d}{dc_{12}} [x_1(t)^2] dt + \int_{t_1}^{t_2} \frac{d}{dc_{12}} [c_{12}^2 x_2(t)^2] dt + 2 \int_{t_1}^{t_2} \frac{d}{dc_{12}} [c_{12} x_1(t) x_2(t)] dt \right] = 0$$

$$\frac{1}{t_2 - t_1} \left[0 + \int_{t_1}^{t_2} 2 c_{12} x_2(t)^2 dt - 2 \int_{t_1}^{t_2} x_1(t) x_2(t) dt \right] = 0$$

$$c_{12} \int_{t_1}^{t_2} x_2^2(t) dt = \int_{t_1}^{t_2} x_1(t) x_2(t) dt$$

$$c_{12} = \frac{\int_{t_1}^{t_2} x_1(t) x_2(t) dt}{\int_{t_1}^{t_2} x_2^2(t) dt}$$

By Analogy with vectors; we say that $x_1(t)$ has comp.

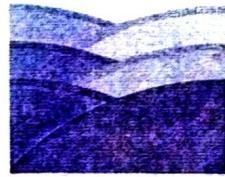
$$C_{12} = \frac{v_1 v_2}{v_2^2}$$

$$C_{12} = \frac{\int_{t_1}^{t_2} x_1(t) x_2(t) dt}{\int_{t_1}^{t_2} x_2^2(t) dt}$$

If $C_{12} = 0$ then the signal $x_1(t)$ obtains no components of the signal $x_2(t)$.
 The two functions are orthogonal over the interval (t_1, t_2) .

$$\int_{t_1}^{t_2} x_1(t) x_2(t) dt = 0$$

A40401- SIGNALS, SYSTEMS AND STOCHASTIC PROCESSES



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Fourier Series

A sigl is said to be a continuous-time signal if it is available at all instants of time. A real time naturally available signal is in the form of time domain.

The analysis of a signal is far more convenient in the frequency domain. There are three important classes of transformation methods available for

C.T. They are,

1. Fourier Series
2. Fourier Transform
3. Laplace Transform

Fourier Series :- The representation of signals over a certain interval of time in terms of a linear combination of orthogonal functions is called Fourier Series.

It is applicable only for periodic signals. A periodic sigl is one which repeats itself at regular intervals of time periodically over $\rightarrow \infty$.

Three methods

- Trigonometric form
- Cosine form
- Exponential form

To exist for a periodic sigl, it must satisfy certain conditions

1. The function $x(t)$ must be a single-valued function
2. $x(t)$ has only a finite number of maxima & minima
3. $x(t)$ has a finite number of discontinuities
4. The $x(t)$ is absolutely integrable over one period, that is

$$\int_0^T |x(t)| dt < \infty$$

Trigonometric form :-

A sinusoidal sigl $x(t) = A \sin(\omega t + \phi)$ is a periodic signal with period $T = \frac{2\pi}{\omega}$. Also sum of two sinusoids is periodic provided that their frequencies are integral multiples of a fundamental frequency ω_0 .

The signal $x(t)$, a sum of sine & cosine functions whose frequencies are integral multiples of ω_0 is a periodic signal.

Let the signal $x(t)$ be

$$x(t) = a_0 + a_1 \cos \omega_0 t + a_2 \cos 2\omega_0 t + \dots + a_K \cos K\omega_0 t + b_1 \sin \omega_0 t + b_2 \sin 2\omega_0 t + \dots + b_K \sin K\omega_0 t$$

$$x(t) = a_0 + \sum_{n=1}^K a_n \cos n\omega_0 t + b_n \sin n\omega_0 t.$$

For periodic signal must satisfy the condition $x(t) = x(t+T)$ for all 't'

$$\begin{aligned} x(t+T) &= a_0 + \sum_{n=1}^K a_n \cos n\omega_0 (t+T) + b_n \sin n\omega_0 (t+T) \\ &\approx a_0 + \sum_{n=1}^K a_n \cos n\omega_0 \left(t + \frac{2\pi}{\omega_0}\right) + b_n \sin \left(n\omega_0 \left(t + \frac{2\pi}{\omega_0}\right)\right) \end{aligned}$$

$$\begin{aligned} &= a_0 + \sum_{n=1}^K a_n \cos (n\omega_0 t + 2n\pi) + b_n \sin (n\omega_0 t + 2n\pi) \\ &= a_0 + \sum_{n=1}^K (a_n \cos n\omega_0 t + b_n \sin n\omega_0 t) \end{aligned}$$

$$x(t+T) = x(t)$$

The infinite series of sine & cosine terms of frequencies $0, \omega_0, 2\omega_0, \dots$ is known as trigonometric form of FS & can be written as

$$x(t) = \sum_{n=0}^{\infty} a_n \cos n\omega_0 t + b_n \sin n\omega_0 t \quad \rightarrow (1)$$

$$x(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos n\omega_0 t + b_n \sin n\omega_0 t. \quad a_0 \text{ is called dc component.}$$

a_n, b_n are constants.

$a_1 \cos \omega_0 t + b_1 \sin \omega_0 t$ is first harmonic

$a_2 \cos 2\omega_0 t + b_2 \sin 2\omega_0 t$ is second harmonic.

$a_n \cos n\omega_0 t + b_n \sin n\omega_0 t$ is n th harmonic

Since $\sin n\omega_0 t = 0$ for $n=0$,

The constant $a_0 = 0$

are called Fourier Coeff.

$a_0, a_1, a_2, \dots, b_0, b_1, b_2, \dots, b_n$ are called Fourier Coeff.

To find a_0 : Integrate both sides of eqn (1) over one period T i.e. $t_0 \rightarrow t_0 + T$ at an arbitrary time t_0 .

$$\int_{t_0}^{t_0+T} x(t) dt = a_0 \int_{t_0}^{t_0+T} dt + \int_{t_0}^{t_0+T} \left[\sum_{n=1}^{\infty} [a_n \cos n\omega t + b_n \sin n\omega t] \right] dt \quad (3)$$

$$= a_0 \int_{t_0}^{t_0+T} dt + \sum_{n=1}^{\infty} \left[\int_{t_0}^{t_0+T} a_n \cos n\omega t dt + \int_{t_0}^{t_0+T} b_n \sin n\omega t dt \right]$$

$$= a_0 T + a_0 \cdot 0$$

$$\int_{t_0}^{t_0+T} x(t) dt = a_0 T$$

$$a_0 = \frac{1}{T} \int_{t_0}^{t_0+T} x(t) dt$$

$\therefore \int_{t_0}^{t_0+T} a_n \cos n\omega t = a_0 \cdot 0$
 $\int_{t_0}^{t_0+T} b_n \sin n\omega t = 0$ (for
 net area under any
 sinusoidal over
 any complete period
 is zero.)

To find a_n is

Multiply eqn (3) with $\cos m\omega t$ & integrate over one period.

$$\int_{t_0}^{t_0+T} x(t) \cos m\omega t dt = a_0 \int_{t_0}^{t_0+T} \cos m\omega t dt + \sum_{n=1}^{\infty} a_n \int_{t_0}^{t_0+T} \cos n\omega t \cos m\omega t dt$$

$$+ \sum_{n=1}^{\infty} b_n \int_{t_0}^{t_0+T} \sin n\omega t \cos m\omega t dt$$

First & third integrals are zero

If $m=n$

$$\int_{t_0}^{t_0+T} x(t) \cos n\omega t dt = a_n \frac{T}{2}$$

$$a_n = \frac{2}{T} \int_{t_0}^{t_0+T} x(t) \cos n\omega t dt$$

To find b_n multiply eqn (3) with $\sin m\omega t$ & integrate over one period

$$\int_{t_0}^{t_0+T} x(t) \sin m\omega t dt = a_0 \int_{t_0}^{t_0+T} \sin m\omega t dt + \sum_{n=1}^{\infty} a_n \int_{t_0}^{t_0+T} \cos n\omega t \sin m\omega t dt$$

$$+ \sum_{n=1}^{\infty} b_n \int_{t_0}^{t_0+T} \sin n\omega t \sin m\omega t dt$$

a_0, a_n, b_n are called trigonometric Fourier coefficients

$$\int_{t_0}^{t_0+T} \cos m\omega_0 t \cos n\omega_0 t dt = \begin{cases} 0 & \text{for } m \neq n \\ T/2 & \text{for } m = n \neq 0 \end{cases}$$

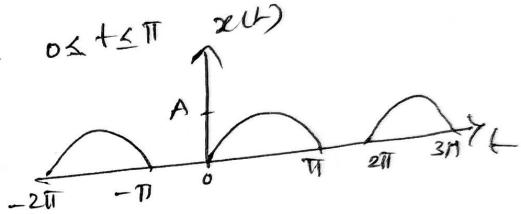
$$\int_{t_0}^{t_0+T} \sin m\omega_0 t \sin n\omega_0 t dt = \begin{cases} 0 & \text{for } m \neq n \\ T/2 & \text{for } m = n \neq 0 \end{cases}$$

$$\int_{t_0}^{t_0+T} \sin m\omega_0 t \cos n\omega_0 t dt = 0 \quad \text{for all } m \neq n.$$

Ex:- Find the Fourier Series expansion of the half wave rectified sine wave shown below

$$\text{Sol} \quad x(t) = \begin{cases} A \sin \frac{2\pi}{T} t & 0 \leq t \leq \pi \\ 0 & \pi \leq t \leq 2\pi \end{cases}$$

fundamental period $T = 2\pi$



Exponential Fourier Series

The function $x(t)$ is expressed as a weighted sum of the complex exponential functions.

A set of complex exponential functions $e^{jn\omega_0 t}$, $n = 0, \pm 1, \pm 2, \pm 3, \dots$ form a closed orthogonal set over an interval $(t_0, t_0 + T)$ where $T = 2\pi/\omega_0$. for any value of t_0 and therefore it can be used as a Fourier series.

Using Euler's identity,

$$A_n \cos(n\omega_0 t + \theta_n) = \text{Re} \left[e^{j(n\omega_0 t + \theta_n)} + e^{-j(n\omega_0 t + \theta_n)} \right] \rightarrow (1)$$

$$A_n \cos(n\omega_0 t + \theta_n) = A_0 + \sum_{n=1}^{\infty} A_n [\cos(n\omega_0 t + \theta_n)] \rightarrow (2)$$

Cosine representation of $x(t) = A_0 + \sum_{n=1}^{\infty} A_n \cos(n\omega_0 t + \theta_n)$

sub eqn (2) in eqn (1)

$$x(t) = A_0 + \sum_{n=1}^{\infty} \frac{A_n}{2} \left[e^{j(n\omega_0 t + \theta_n)} + e^{-j(n\omega_0 t + \theta_n)} \right]$$

$$= A_0 + \sum_{n=1}^{\infty} \frac{A_n}{2} \left[e^{j\omega_0 t} e^{j\theta_n} + e^{-j\omega_0 t} e^{-j\theta_n} \right]$$

$$= A_0 + \sum_{n=1}^{\infty} \frac{A_n}{2} e^{j\theta_n} \left[e^{j\omega_0 t} + \sum_{n=1}^{\infty} \frac{A_n}{2} e^{-j\theta_n} \left[e^{j\omega_0 t} \right] \right]$$

Let $n = -k$ in second summation of above eqns, we have

$$x(t) = A_0 + \sum_{n=1}^{\infty} \left(\frac{A_n}{2} e^{j\theta_n} \right) e^{j\omega_0 t} + \sum_{k=-1}^{\infty} \left(\frac{A_k}{2} e^{j\theta_k} \right) e^{jk\omega_0 t}$$

on comparing above eqns we get

$$A_n = A_k \quad n > 0 \\ A_n = \frac{A_k}{2} e^{j\theta_k} \quad k < 0$$

$$C_0 = A_0 \quad C_n = \frac{A_n}{2} e^{j\theta_n} \quad n > 0$$

$$x(t) = A_0 t + \sum_{n=1}^{\infty} \frac{A_n}{2} e^{j\theta_n} e^{j\omega_0 t} + \sum_{n=-1}^{-\infty} \frac{A_n}{2} e^{j\theta_n} e^{j\omega_0 t}$$

$$x(t) = \sum_{n=-\infty}^{\infty} C_n e^{jn\omega_0 t}$$

This is called known as exponential form of Fourier Series. The

above eqn is called synthesis equation.

Exponential Series from cosine series $\begin{aligned} C_0 &= A_0 \\ C_n &= \frac{A_n}{2} e^{j\theta_n} \end{aligned}$

Coeff of Exponential terms $C_n e^{jn\omega_0 t}$

$x(t) = \sum_{n=-\infty}^{\infty} C_n e^{jn\omega_0 t}$ where $\omega_0 = \frac{2\pi}{T}$

Multiplying both sides by $e^{-jk\omega_0 t}$ & integrating over one period, we get

$$\int_{t_0}^{t_0+T} x(t) e^{-jk\omega_0 t} dt = \int_{t_0}^{t_0+T} \left(\sum_{n=-\infty}^{\infty} C_n e^{jn\omega_0 t} \right) e^{-jk\omega_0 t} dt$$

$$= \sum_{n=-\infty}^{\infty} C_n \int_{t_0}^{t_0+T} e^{jn\omega_0 t} e^{-jk\omega_0 t} dt$$

We know

$$\int_{t_0}^{t_0+T} e^{jn\omega_0 t} e^{-jk\omega_0 t} dt = \begin{cases} T & \text{for } k = n \\ 0 & \text{for } k \neq n \end{cases}$$

$$\int_{t_0}^{t_0+T} x(t) e^{-jk\omega_0 t} dt = T C_k$$

$$C_k = \frac{1}{T} \int_{t_0}^{t_0+T} x(t) e^{-jk\omega_0 t} dt$$

(*)

$$C_n = \frac{1}{T} \int_{t_0}^{t_0+T} x(t) e^{-jn\omega_0 t} dt$$

$$C_0 = A_0 = \frac{1}{T} \int_{t_0}^{t_0+T} x(t) dt$$

C_n exist only for discrete values of n . As represented a complex spectrum, it has both magnitude & phase spectra. The following points may be noted:

1. magnitude line spectrum is always an even function of n .
2. phase line spectrum is always an odd function of n .

Fourier Spectrum

Fourier spectrum of a periodic signal $x(t)$ is a plot of its Fourier Co-eff versus frequency ω .

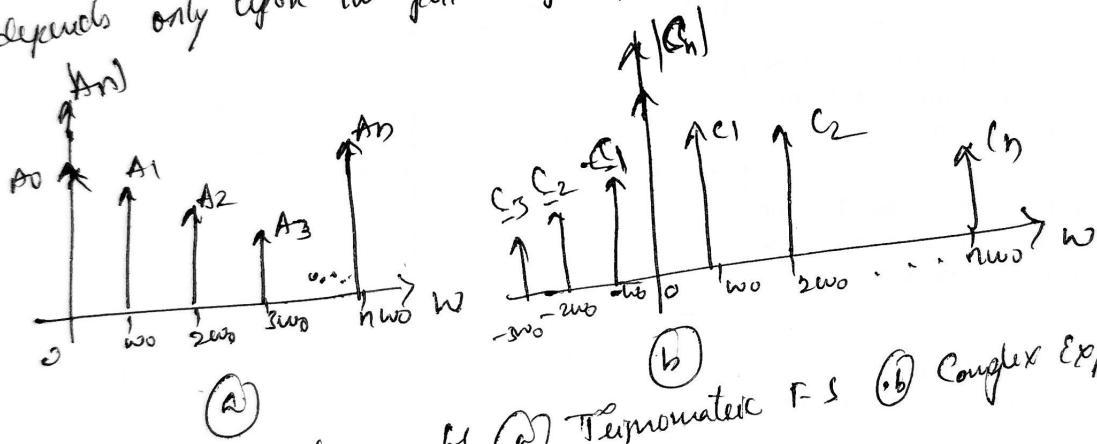
if it has two parts

- Amplitude Spectrum - Amp of F-coeff Vs Frequency
- phase spectrum - phase of F-coeff Vs Frequency

Both plot together in called Fourier frequency spectra of $x(t)$ - this type of representation is called frequency domain representation.

F. Spectrum exists only at discrete frequencies $n\omega_0$ where $n=0, \pm 1, \pm 2, \dots$

Acuse known as discrete spectrum / Line spectrum. The Envelope of the spectrum depends only upon the pulse shape, but not upon the period of repetition.



Complex frequency spectrum for (a) Thermometric F.S (b) Complex Exponential F.S

$$c_n = |c_n| e^{j\theta_n}$$

$$c_{-n} = |c_n| e^{-j\theta_n}$$

$$(c_n) = (c_{-n})$$

The magnitude spectrum is symmetrical about the vertical axis because through origin & phase spectrum is asymmetric about the vertical axis. It has odd symmetry.

Properties :-

1. Linearity property

$$x_1(t) \xleftrightarrow{FS} c_n \quad \& \quad x_2(t) \xleftrightarrow{FS} d_n$$

$$Ax_1(t) + Bx_2(t) \xleftrightarrow{FS} Ac_n + Bd_n$$

2. Time shifting property

$$x(t) \xleftrightarrow{FS} c_n$$

$$x(t-t_0) \xleftrightarrow{FS} e^{-j\omega_0 t_0} c_n$$

3. Time reversal property

$$x(t) \xleftrightarrow{FS} c_n$$

$$x(-t) \xleftrightarrow{FS} c_{-n}$$

4. Time scaling property

$$x(t) \xleftrightarrow{FS} c_n$$

$$x(\alpha t) \xleftrightarrow{FS} c_n \text{ with fundamental frequency } \alpha \omega_0$$

5. Time differentiation property

$$x(t) \xleftrightarrow{FS} c_n$$

$$\frac{d}{dt} x(t) \xleftrightarrow{FS} j\omega_0 c_n$$

6. Time integration property

$$x(t) \xleftrightarrow{FS} c_n$$

$$\int_{-\infty}^t x(u) du \xleftrightarrow{FS} \frac{c_n}{j\omega_0} \quad [\text{if } \omega_0 \neq 0]$$

$$x_1(t) \xleftrightarrow{FS} c_n \quad \& \quad x_2(t) \xleftrightarrow{FS} d_n$$

$$x_1(t) * x_2(t) \xleftrightarrow{FS} T c_n d_n$$

8. Modulation / Multiplication property

$$x(t) \xleftrightarrow{FS} c_n \quad \& \quad x_2(t) \xleftrightarrow{FS} d_n$$

$$x_1(t)x_2(t) \xleftrightarrow{FS} \sum_{l=-\infty}^{\infty} c_l d_{n-l}$$

9. Conjugation & Conjugate Symmetry property

$$x(t) \xleftrightarrow{FS} c_n$$

Conjugate $x^*(t) \xleftrightarrow{FS} c_n^* \quad [\text{for complex } x(t)]$

Conjugate Symmetry $c_{-n} = c_n^* \quad [\text{for real } x(t)]$

10. Parseval's theorem / property / relation

$$x_1(t) \xleftrightarrow{FS} c_n$$

$$x_2(t) \xleftrightarrow{FS} d_n$$

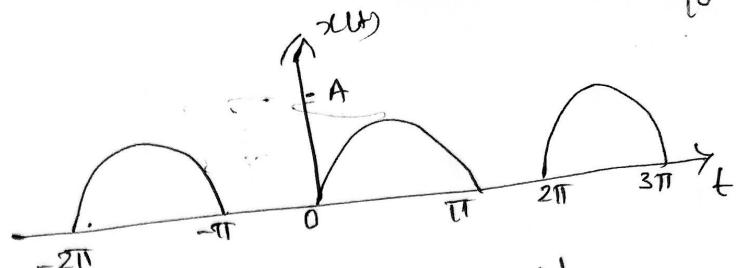
The parseval's relation states that

$$\frac{1}{T} \int_{t_0}^{t_0+T} x_1(t) x_2(t) dt = \sum_{n=-\infty}^{\infty} c_n d_n^*$$

Parseval's identity

$$\frac{1}{T} \int_{t_0}^{t_0+T} |x(t)|^2 dt = \sum_{n=-\infty}^{\infty} |c_n|^2 \quad \text{if } x_1(t) = x_2(t) = x(t)$$

Ex Find the f-s expansion of the half wave rectified sine wave as shown in figure



sof From figure
of ~~is~~ a periodic signal

with period $T = 2\pi$

$$x(t) = \begin{cases} A \sin \omega t & \text{if } \frac{2\pi}{T} t \\ 0 & \text{if } T \leq t \leq 2\pi \end{cases}$$

fundamental time period $T = 2\pi$

fundamental frequency

$$\omega_0 = \frac{2\pi}{T} = \frac{2\pi}{2\pi} = 1$$

$$\text{let } a_0 = \frac{1}{T} \int_0^{2\pi} x(t) dt = \frac{1}{2\pi} \int_0^{\pi} A \sin t dt = \frac{A}{2\pi} \left[\int_0^{\pi} \sin t dt \right]$$

$$= \frac{A}{2\pi} [-\cos \pi + \cos 0]$$

$$= \frac{A}{2\pi} [(-1) + 1]$$

$$= \frac{2A}{2\pi} = \frac{A}{\pi}$$

$$a_0 = \frac{A}{\pi}$$

$$a_n = \frac{2}{T} \int_0^{2\pi} x(t) \cos nt dt$$

$$= \frac{2}{2\pi} \int_0^{\pi} A \sin t \cos nt dt = \frac{1}{2\pi} \int_0^{\pi} [\sin(t+nt) + \sin(t-nt)] dt$$

$$= \frac{1}{2\pi} \left[-\frac{\cos(1+n)t}{1+n} \Big|_0^\pi - \frac{\cos(1-n)t}{1-n} \Big|_0^\pi \right]$$

$$= \frac{-1}{2\pi} \left[\frac{\cos(1+n)\pi - \cos 0}{1+n} + \frac{\cos(1-n)\pi - \cos 0}{1-n} \right]$$

$$= \frac{-1}{2\pi} \left[\frac{(-1)^{1+n}-1}{1+n} + \frac{(-1)^{n-1}-1}{1-n} \right]$$

$$= \frac{-1}{2\pi} \left[\frac{1-1}{1+n} + \frac{1-1}{1-n} \right]$$

$$= 0 //$$

for odd n

$$a_n = 0$$

$$b_n = \frac{2}{T} \int_0^T x(t) \sin nt dt$$

$$= \frac{A}{2\pi} \int_0^\pi A \sin t \sin nt dt$$

$$= \frac{A}{2\pi} \int_0^\pi (\cos((n-1)t) - \cos((n+1)t)) dt$$

$$= \frac{A}{2\pi} \left[\frac{\sin(n-1)t}{n-1} \Big|_0^\pi - \frac{\sin(n+1)t}{n+1} \Big|_0^\pi \right]$$

$$= \frac{A}{2\pi} \left[\frac{\sin(n-1)\pi - \sin 0}{n-1} - \frac{\sin(n+1)\pi - \sin 0}{n+1} \right]$$

~~for n=1~~ This is zero
for all values of n except $n=1$

$$b_n = \frac{A}{2\pi} \left[\frac{\sin(n-1)\pi - \sin 0}{n-1} - \frac{\sin(n+1)\pi - \sin 0}{n+1} \right] = \frac{A}{2\pi} \left[\frac{\pi(-1)^{n-1} - 0}{n-1} - \frac{\pi(-1)^{n+1} - 0}{n+1} \right]^n$$

$$b_n = \frac{A}{2\pi} \left[\cancel{0} = \frac{A}{2\pi} \right]$$

$$a_n = \frac{A}{2\pi} \left[\frac{-1-1}{1+n} + \frac{-1-1}{1-n} \right] = \frac{A}{2\pi} \left[\frac{2}{n+1} - \frac{2}{n-1} \right]$$

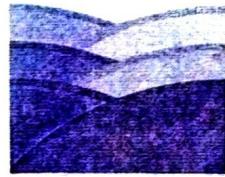
$$= \frac{-2A}{\pi(n^2-1)} .$$

$$a_n = \frac{-2A}{\pi(n^2-1)} \quad (\text{for even } n)$$

-1. Trigonometric Fourier series in
 $x(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos nt + b_n \sin nt$

$$x(t) = \frac{A}{\pi} + \frac{A}{2\pi} \sin t - \sum_{n \text{ even}}^{\infty} \frac{2A}{\pi(n^2-1)} \cos nt //$$

A40401- SIGNALS, SYSTEMS AND STOCHASTIC PROCESSES



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Fourier Transform

Definition :- It is a transformation technique which transforms signals from the continuous-time domain to the corresponding frequency domain & vice-versa, and which applies for both periodic as well as aperiodic signals. It is extremely useful technique used in analysis of linear time-invariant LTI system.

Derivation of the F.T of Non periodic Signal from the F.S of periodic signal
 Let $x(t)$ be a non-periodic function & $x_T(t)$ be periodic with period T . & let their relation is given by

$$x(t) = \lim_{T \rightarrow \infty} x_T(t)$$

F.S of a periodic signal $x_T(t)$ is

$$x_T(t) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega_0 t}$$

$$c_n = \frac{1}{T} \int_{-T/2}^{T/2} x_T(t) e^{-jnw_0 t} dt \quad \text{where } w_0 = \frac{2\pi}{T}$$

$$T c_n = \int_{-T/2}^{T/2} x_T(t) e^{-jnw_0 t} dt$$

Let $nw_0 = w_0$ & $T \rightarrow \infty$. As $T \rightarrow \infty$ we have $w_0 = 2\pi/T \rightarrow 0$ and discrete Fourier spectrum becomes continuous; the summation becomes integration $x_T(t) \rightarrow x(t)$.

thus at $T \rightarrow \infty$

$$T c_n = \lim_{T \rightarrow \infty} \int_{-T/2}^{T/2} x_T(t) e^{-jnw_0 t} dt = \int_{-\infty}^{\infty} [x(t)] e^{-jnw_0 t} dt$$

$$= \int_{-\infty}^{\infty} x(t) e^{-jnw_0 t} dt$$

$$\therefore X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

$= X(\omega)$
 F.T

$$x_T(t) = \sum_{n=-\infty}^{\infty} c_n e^{j\omega_0 t}$$

$$= \sum_{n=-\infty}^{\infty} \frac{x(\omega)}{T} e^{j\omega_0 t}$$

$$\therefore T(n) = x(\omega)$$

$$c_n = \frac{x(\omega)}{T}$$

$$T = \frac{2\pi}{\omega_0}$$

$$= \sum_{n=-\infty}^{\infty} \frac{x(\omega)}{2\pi} e^{j\omega_0 t} \omega_0$$

$$x(t) = \frac{1}{T} \int_{-\infty}^{\infty} x(\omega) e^{j\omega_0 t} d\omega$$

As $T \rightarrow \infty$; $\omega_0 = \frac{2\pi}{T}$ becomes infinitesimally small & may be represented by $d\omega$

$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} x(\omega) e^{j\omega_0 t} d\omega$$

$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} x(\omega) e^{j\omega t} d\omega$$

Here $x(t)$ is called inverse F.T of $x(\omega)$.

The equations

$$x(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} x(\omega) e^{j\omega t} d\omega$$

$x(\omega)$ & $x(t)$ are known as F-T pair & can be denoted as

$$x(\omega) = F[x(t)]$$

$$x(t) = F^{-1}[x(\omega)]$$

Properties

1. Linearity property

$$x_1(t) \xleftrightarrow{FT} X_1(\omega) \quad x_2(t) \xleftrightarrow{FT} X_2(\omega)$$

$$ax_1(t) + bx_2(t) \xleftrightarrow{FT} aX_1(\omega) + bX_2(\omega)$$

2. Time shifting property

$$x(t) \xleftrightarrow{FT} X(\omega)$$

$$x(t-t_0) \xleftrightarrow{FT} e^{j\omega t_0} X(\omega)$$

3. Frequency shifting property

$$x(t) \xleftrightarrow{FT} X(\omega)$$

$$e^{j\omega t} x(t) \xleftrightarrow{FT} X(\omega - \omega_0)$$

4. Time reversal property

$$x(t) \xleftrightarrow{FT} X(-\omega)$$

5. Time scaling property

$$x(at) \xleftrightarrow{FT} \frac{1}{|a|} X\left(\frac{\omega}{a}\right)$$

6. Differentiation in time domain property

$$\frac{d}{dt} x(t) \xleftrightarrow{FT} j\omega X(\omega)$$

7. Differentiation in frequency domain property

$$t x(t) \xleftrightarrow{FT} j \frac{d}{dt} X(\omega)$$

8. Time integration property

$$\int_{-\infty}^t x(\tau) d\tau \xleftrightarrow{FT} \frac{1}{j\omega} X(j\omega) \quad \text{if } X(0) = 0$$

9. Convolution property

$$x_1(t) \xleftrightarrow{FT} X_1(\omega) \quad x_2(t) \xleftrightarrow{FT} X_2(\omega)$$

$$x_1(t) * x_2(t) \xleftrightarrow{FT} X_1(\omega) X_2(\omega)$$

10. Multiplication property

$$x_1(t) x_2(t) \xleftrightarrow{FT} \frac{1}{2\pi} X_1(\omega) * X_2(\omega)$$

11. Duality (symmetry) property if $x(t) \xleftrightarrow{FT} X(\omega)$ then $x(t) \xleftrightarrow{FT} 2\pi X(-\omega)$

12. Modulation property $x(t) \cos \omega_0 t \xleftrightarrow{FT} \frac{1}{2} [X(\omega - \omega_0) + X(\omega + \omega_0)]$

13. Conjugation Property $x(t) \xleftrightarrow{FT} x^*(-\omega)$

14. Autocorrelation property $R(\tau) \xleftrightarrow{FT} |X(\omega)|^2$

15. $x_1(t) \xleftrightarrow{FT} X_1(\omega)$ $x_2(t) \xleftrightarrow{FT} X_2(\omega)$ Parseval's relation

$$\int_{-\infty}^{\infty} x_1(t) x_2^*(t) dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} X_1(\omega) X_2^*(\omega) d\omega$$

$$E = \int_{-\infty}^{\infty} |x(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X(\omega)|^2 d\omega.$$

16. Area under the curve

$$\int_{-\infty}^{\infty} x(t) dt = \frac{1}{2\pi} X(0)$$

$$\int_{-\infty}^{\infty} x(\omega) d\omega = X(0)$$

17. FT of complex & real functions

$$x(t) = x_R(t) + j x_I(t)$$

$$x_R(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} [x_R(\omega) \cos \omega t - x_I(\omega) \sin \omega t] d\omega$$

$$x_I(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} [x_R(\omega) \sin \omega t + x_I(\omega) \cos \omega t] d\omega$$

$$x_I(\omega) = -j \int_{-\infty}^{\infty} x_R(t) \sin \omega t dt$$

* FT of standard signals

Impulse function $\delta(t)$

$$\delta(t) = \begin{cases} 1 & \text{for } t=0 \\ 0 & \text{for } t \neq 0 \end{cases}$$

$$X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt = \int_{-\infty}^{\infty} \delta(t) e^{-j\omega t} dt = \left[e^{-j\omega t} \right]_{t=0}^{\infty} = 1$$

$$F[\delta(t)] = 1$$

$$\delta(t) \xleftrightarrow{FT} 1$$

$$\delta(t-t_0) \xleftrightarrow{FT} e^{j\omega t_0}$$

* Single-sided Real Exponential function $e^{-at} u(t)$

$$\text{Given } x(t) = e^{-at} u(t) \quad u(t) = \begin{cases} 1 & \text{for } t \geq 0 \\ 0 & \text{for } t < 0 \end{cases}$$

$$\begin{aligned} X(\omega) &= \int_{-\infty}^{\infty} x(t) e^{j\omega t} dt = \int_{-\infty}^{\infty} e^{-at} u(t) e^{j\omega t} dt \\ &= \int_0^{\infty} e^{-(a+j\omega)t} dt \\ &= \frac{e^{-(a+j\omega)t}}{-(a+j\omega)} \Big|_0^{\infty} = \frac{1 - e^0}{-(a+j\omega)} = \frac{1}{a+j\omega} \end{aligned}$$

$$e^{-at} u(t) \xrightarrow{\text{FT}} \frac{1}{a+j\omega}$$

* Unit step function $\frac{1}{a+j\omega} u(t)$.

$$u(t) = \begin{cases} 1 & \text{for } t \geq 0 \\ 0 & \text{for } t < 0 \end{cases}$$

unit step function not absolutely integrable, we can't directly find its Fourier transform so express the unit step function in terms of signum function.

$$u(t) = \frac{1}{2} + \frac{1}{2} \operatorname{sgn} t$$

$$x(\omega) = F[u(t)] \Rightarrow F\left[\frac{1}{2} + \frac{1}{2} \operatorname{sgn} t\right]$$

$$= \frac{1}{2} F[1] + \frac{1}{2} F[\operatorname{sgn}(t)]$$

$$F[u(t)] = \frac{1}{2} \left[\pi \delta(\omega) + \frac{j}{2} \frac{2}{j\omega} \right] = \pi \delta(\omega) + \frac{1}{j\omega}$$

$$\boxed{u(t) \xrightarrow{\text{FT}} \pi \delta(\omega) + \frac{1}{j\omega}}$$

* Signum function $(\operatorname{sgn}(t))$

$$\operatorname{sgn}(t) = \begin{cases} 1 & \text{for } t > 0 \\ -1 & \text{for } t < 0 \end{cases}$$

This is not absolutely integrable so we cannot directly find its FT but we consider $e^{-at} \operatorname{sgn}(t)$ & sub $a \rightarrow 0$, to obtain $\operatorname{sgn}(t)$

$$x(t) = \operatorname{sgn}(t) = \lim_{a \rightarrow 0} \int_{-\infty}^t e^{-at} \operatorname{sgn}(t) dt$$

$$= \lim_{a \rightarrow 0} \left[e^{-at} u(t) - e^{at} u(-t) \right]$$

$$X(\omega) = \int_{-\infty}^{\infty} dt \lim_{a \rightarrow 0} \left[e^{-at} u(t) - e^{at} u(-t) \right]$$

$$= \lim_{a \rightarrow 0} \left\{ \frac{1}{a+j\omega} - \frac{1}{a-j\omega} \right\} = \frac{1}{j\omega} - \frac{1}{-j\omega} = \frac{2}{j\omega}$$

Sampling :- The process of converting C.T signal into D.T. signal is called Sampling. After sampling the signal is defined at discrete instants of time & the time interval b/w two successive sampling instants is called Sampling period & Sampling interval.

Important fact in sampling is Sampling rate (f_s) must be kept sufficiently high so that the original signal can be reconstructed from its samples.

Sampling theorem :- This theorem states that a band limited signal $x(t)$ with $X(\omega) = 0$ for $\omega > \omega_m$ [i.e., $x(t) = 0$ for $\omega > f_m$] can be represented into a uniquely determined form from its samples $x(nT)$ if the sampling frequency $f_s \geq 2f_m$.

where f_m - highest frequency component present in it

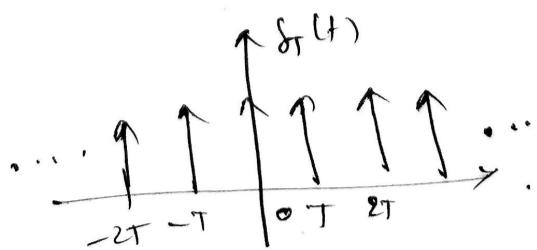
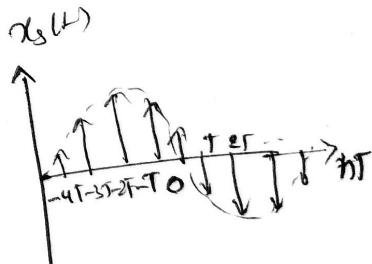
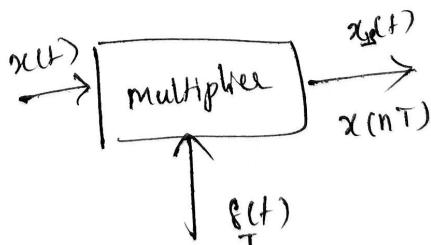
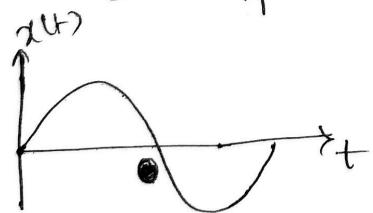
f_s - Sampling frequency

Sampling frequency must be atleast twice the highest frequency present in the signal for signal recovery.

Signal for signal recovery.

It is also called as uniform sampling theorem & low pass sampling theorem.
(Uniform intervals $\frac{1}{f_s}$ sec)

Proof :- Let us consider a C.T band limited signal $x(t)$ as shown in figure. which has no spectral components above f_m cycles/sec. i.e. $X(\omega) = 0$ for $\omega > \omega_m$. $s(t)$ is impulse train which samples at a rate of f_s Hz & $x_s(t)$ is the sampled signal. T is sampling period & $f_s = \frac{1}{T}$ Sampling frequency



Sampling operation

$$x_s(t) = x(t) \delta_T(t) \rightarrow ①$$

where $\delta_T(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT)$

Exponential form of F.S of $\delta_T(t)$ is

$$\delta_T(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega t}$$

$$c_n = \frac{1}{T} \int_{-T/2}^{T/2} \delta(t) e^{-jn\omega t} dt = \frac{1}{T}$$

$$\delta_T(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT) = \sum_{n=-\infty}^{\infty} \frac{1}{T} e^{jn\omega t} = \frac{1}{T} \sum_{n=-\infty}^{\infty} e^{jn\omega t} \rightarrow ②$$

Sub ② in ①

$$x_s(t) = x(t) \delta_T(t) = \frac{1}{T} \sum_{n=-\infty}^{\infty} x(t) e^{jn\omega t}$$

Taking FT on both sides

$$FT[x_s(t)] = FT\left[\frac{1}{T} \sum_{n=-\infty}^{\infty} x(t) e^{jn\omega t}\right]$$

$$X_s(\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} FT[x(t)] e^{jn\omega t}$$

$$X_s(\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(\omega - \frac{2\pi}{T} n)$$

$$X_s(\omega) = f_s \sum_{n=-\infty}^{\infty} X(\omega - n\omega_s)$$

where $X(\omega)$ & $X_s(\omega)$ are spectrums of ~~impulse sampled signal~~ sampled signal.

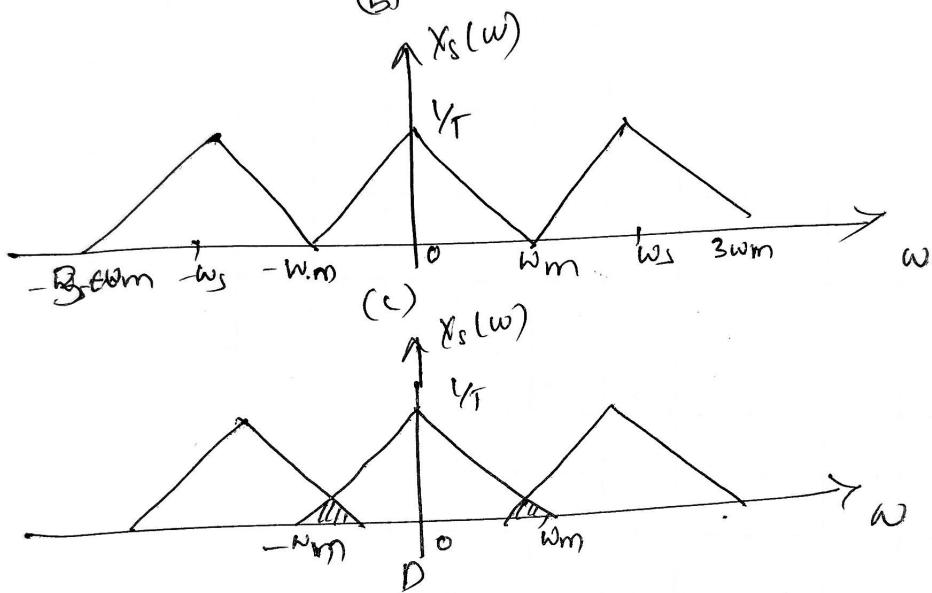
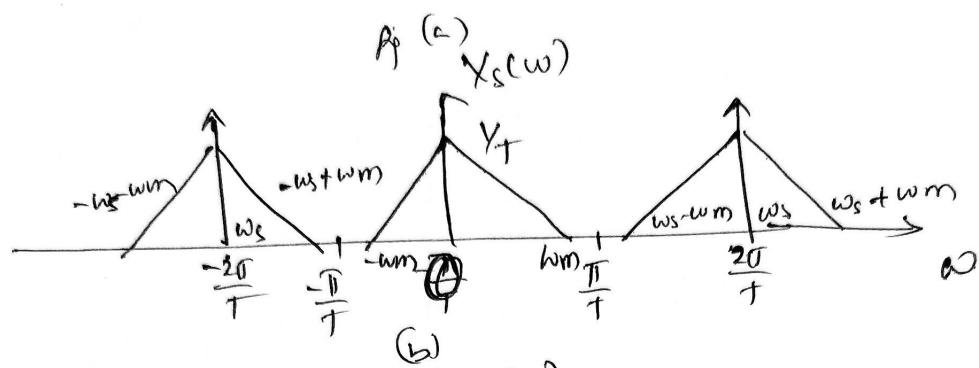
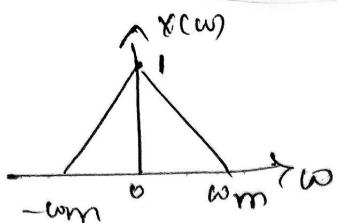
Thus, the FT of a sampled signal is given by an infinite sum

of shifted replicas of the FT of the original sigl.

Two basic conditions to be satisfied if $x(t)$ is to be recovered back from its samples

→ $x(t)$ should be band limited to some frequency ω_m .

→ The sampling frequency f_s should at least twice the band limited frequency ω_m (ie $\omega_s \geq 2\omega_m$)



Frequency Spectrum of C.T. Sgl $x(t)$
b1, ω_s & frequency spectrum of Sampled signals $x_s(t)$ Rl
 $(\frac{\pi}{T}) > \omega_m \Rightarrow (\frac{\pi}{T}) = \omega_m \Rightarrow (\frac{\pi}{T}) < \omega_m$ respectively

From figure we observe
The spectral replicates have a large separation b/w them known as guard band
1. ~~$\omega_s > 2\omega_m$~~ - it makes the process of filtering much easier & effective. not have sharp cutoff.

2. $\omega_s = 2\omega_m$ - no separation b/w the replicates. So no guard band exist & $X(cw)$ can be obtained from $X_s(cw)$ by using only an ideal low pass filter with sharp cut-off.

3. $\omega_s < 2\omega_m$ - low frequency components are overlap on the high frequency components of $X(cw)$, there is distortion & $X(cw)$ can not recovered from $X_s(cw)$ by using filters. this type of distortion is called aliasing.

Nyquist rate $f_N = 2f_m$ Hz

$$\text{Nyquist interval} = \frac{1}{f_N} = \frac{1}{2f_m} \text{ sec}$$

Effects of Under sampling

When $\omega_s < 2\omega_m$ i.e., when the signal is under sampled $X_s(\omega)$, the spectrum of $x(t)$ is no longer replicated in $X_s(\omega)$ & and thus there is no longer recoverable by CPF. This effect in which the individual terms in eqn $X_s(\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} x(n) e^{-jn\omega T}$ overlap is referred to as aliasing. This process of spectral overlap is also called frequency folding effect.

Aliasing can occur if either of the following conditions exists

1. The SSI is not band-limited or finite length.

2. The Sampling rate is too low.

To avoid aliasing, it should be ensured that

1. $x(t)$ is strictly a band-limited (Very anti aliasing filter).

2. f_s is greater than $2f_m$.

Anti-Aliasing Filter



fig: Anti-Aliasing filter.

Sampling theorem states that a signal can be perfectly reconstructed from its samples only if it is a band limited. In practice no signal is strictly band limited. If SSI has low & high noise frequencies, then such type of SSI sampled it may create aliasing. To avoid aliasing error caused by high frequency of SSI, it is necessary to first band limit $x(t)$ to some appropriate frequency. An appropriate CPF such that most part of energy is retained. The CPF before Sampling is referred as an anti-aliasing filter. It is used primarily for preventing aliasing.

Reconstruction

The process of obtaining the analog signal $x(t)$ from the sampled signal $x_s(t)$ is called data reconstruction or interpolation. We know that

$$x_s(t) = x(t) \delta_T(t) = x(t) \sum_{n=-\infty}^{\infty} \delta(t-nT)$$

$$(1) \quad x_s(t) = \sum_{n=-\infty}^{\infty} x(nT) \delta(t-nT)$$

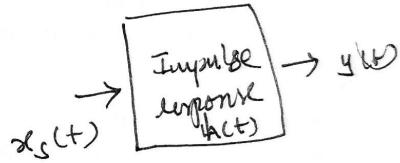
Since $\delta(t-nT)$ is zero except at the sampling instants $t=nT$, the reconstruction filter, which is assumed to be linear & time invariant has unit impulse response $h(t)$. The reconstruction filter output, $y(t)$ is given by the convolution.

$$y(t) = \sum_{n=-\infty}^{\infty} \sum_{\lambda=-\infty}^{\infty} x(\lambda T) \delta(\lambda - nT) h(t-\lambda) d\lambda$$

or, upon changing the order of summation & integration

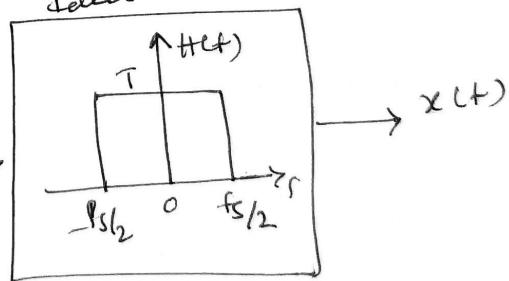
$$y(t) = \sum_{n=-\infty}^{\infty} x(nT) \int_{-\infty}^{\infty} \delta(\lambda - nT) h(t-\lambda) d\lambda$$

$$y(t) = \sum_{n=-\infty}^{\infty} x(nT) h(t-nT)$$



Ideal Reconstruction filter

If $x(t)$ is sampled at the frequency exceeding the Nyquist rate & if the sampled signal $x_s(t)$ is passed through an ideal LPF, with B.W. $\sum_{n=-\infty}^{\infty} x(nT) \delta(t-nT)$ greater than f_m but less than f_s , the pass band amplitude response $H(f)$ of the filter will be $x(t)$. We choose the B.W. of the ideal reconstruction filter to be $0.5 f_s$.



Reconstruction filtering

$$H(f) = \begin{cases} T & |f| < 0.5 f_s \\ 0 & \text{otherwise} \end{cases}$$

The impulse response of the ideal reconstruction filter is given by

$$h(t) = \int_{-fs/2}^{fs/2} T e^{j2\pi f t} df$$

which is

$$\begin{aligned} h(t) &= T \left[\frac{e^{j2\pi f t}}{j2\pi f} \right] \Big|_{-fs/2}^{fs/2} \\ &= \frac{T}{j2\pi t} \left[e^{j\pi f s t} + e^{-j\pi f s t} \right] \\ &= \frac{1}{\pi f s t} \left[\frac{e^{j\pi f s t} - e^{-j\pi f s t}}{2j} \right] \end{aligned}$$

$$h(t) = \frac{\sin \pi f s t}{\pi f s t}$$

$$h(t) = \text{sinc } f s t \rightarrow \textcircled{2}$$

Q/p $y(t) = x(t) = \sum_{n=-\infty}^{\infty} x(nT) \sin fs(t-nT)$

A more convenient form for this expression, which is often referred to as a interpolation formula is

$$x(t) = \sum_{n=-\infty}^{\infty} x(nT) \text{sinc}\left(\frac{t}{T} - n\right)$$

The reconstruction filter is non-causal & impulse response is not limited so it cannot be used for real time applications.

Other practical methods are

1. Zero order hold
2. First order hold
3. Linear interpolation

* Zero order hold

Most widely used interpolator in the ZOH. The ZOH reconstructs the cont signal from its samples by holding the given sample for an interval until the next sample is received.

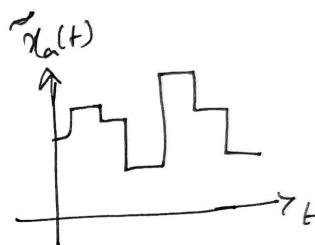
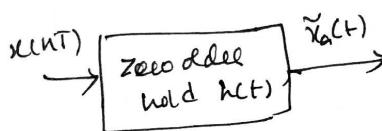
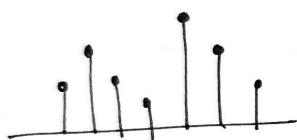
$$\tilde{x}_a(t) = x(n) \quad \text{for } nT \leq t \leq (n+1)T$$

$$\begin{aligned}\tilde{x}_a(t) &= x(n) \quad \text{for } 0 \leq t \leq T \\ &= x(1) \quad \text{for } T \leq t \leq 2T \\ &= x(2T) \quad \text{for } 2T \leq t \leq 3T\end{aligned}$$

:

Impulse response of a zero order hold is given by

$$h(t) = \begin{cases} 1 & 0 \leq t \leq T \\ 0 & \text{otherwise} \end{cases}$$



* Transfer function of a zero order hold

The O/P of ZOH is convolution of its I/P & its ~~impulse~~ response

$$h(t) \text{ i.e. } \tilde{x}_a(t) = x(nT) * h(t)$$

$$= \sum_{n=-\infty}^{\infty} x(nT) h(t-nT).$$

$$\text{For zero order hold } h(t) = u(t) - u(t-T)$$

$$h(t-nT) = u(t-nT) + u(t-(n+1)T)$$

$$\tilde{x}_a(t) = \sum_{n=-\infty}^{\infty} x(nT) [u(t-nT) + u(t-(n+1)T)]$$

$$\tilde{x}_a(t) = \sum_{n=-\infty}^{\infty} x(nT) u(t-nT) + \sum_{n=-\infty}^{\infty} x(nT) u(t-(n+1)T)$$

Taking Laplace Transform on both sides

$$L[\tilde{x}_a(t)] = \left[\frac{1-e^{-Ts}}{s} \right] X(s)$$

$$L[\tilde{x}_a(t)] = \frac{\tilde{x}_a(s)}{X(s)} = \frac{1-e^{-Ts}}{s}$$

T-F of zero order hold consists of steps, it consists of

Since the O/P of the ZOH consists of steps, it consists of higher order harmonics. To remove these harmonics, the O/P of ZOH is applied to an LPF. This filter tends to smooth the corners on ZOH. Hence filter is often called a smoothing filter.

(P) Determine the Nyquist rate corresponding to each of the following signals.

(a) $x(t) = 1 + \cos 2000\pi t + \sin 4000\pi t$

(b) $x(t) = \sin(4000\pi t)/\pi t$

(c) $x(t) = \left(\frac{\sin(4000\pi t)}{\pi t}\right)^2$

soln (a) Given $x(t) = 1 + \cos 2000\pi t + \sin 4000\pi t$.

highest frequency component $f_m = \frac{4000\pi}{2\pi t} = 2000 \text{ Hz}$

Nyquist rate $f_N = 2f_m = 2 \times 2000 \text{ Hz} = 4000 \text{ Hz}$

Nyquist interval $\frac{1}{f_N} = 0.25 \text{ msec}$

$$= \frac{1}{4000 \text{ Hz}} = 0.25 \text{ msec}$$

$\omega_m = 4000\pi$

$$2\pi f_m = 4000\pi$$

$$f_m = 2000 \text{ Hz}$$

Nyquist rate $f_N = 2f_m$

$$= 4000 \text{ Hz}$$

Nyquist interval $\frac{1}{f_N} = \frac{1}{2f_m} = \frac{1}{4000} = 0.25 \text{ ms}$

$\omega_m = 8000\pi$

$f_m = 4000 \text{ Hz}$

(c) highest frequency component $\omega_m = 8000\pi$

$$x(t) = \left(\frac{\sin 4000\pi t}{\pi t}\right) \left(\frac{\sin 8000\pi t}{\pi t}\right) = \frac{\sin^2 4000\pi t}{(\pi t)^2} = \frac{1 - \cos 8000\pi t}{(\pi t)^2}$$

Nyquist rate $f_N = 2f_m = 8000 \text{ Hz}$

Nyquist interval $\frac{1}{f_N} = \frac{1}{2f_m} = \frac{1}{8000} = 0.125 \text{ ms}$

$$(d) x(t) = \sin(80\pi t) \sin(120\pi t)$$

$$\omega_{m1} = 80\pi \text{ rad/sec} \quad \omega_{m2} = 120\pi \text{ rad/sec}$$

$$\omega_m = \omega_{m1} + \omega_{m2} = 200\pi \text{ rad/sec}$$

$$f_m = \frac{\omega_m}{2\pi} = \frac{200\pi}{2\pi} = 100 \text{ Hz}$$

$$\text{Nyquist sampling rate } f_N = 2f_m = 200 \text{ Hz} \approx \\ \text{Nyquist interval} = \frac{1}{f_N} = \frac{1}{2f_m} = \frac{1}{200\pi} = 5 \text{ ms}$$

Laplace Transforms :-

A Linear time invariant (LTI) system is described by differential equations. The response of a system for a given IIP is obtained by solving the differential equations which is quite tedious and time consuming compared to the solution of algebraic equations. So the Laplace transform is used to solve the differential equations.

Laplace transform is powerful mathematical tool used to convert the differential equations into algebraic equations. It is a simple & systematic method which provides the complete solution in one stroke by taking into account the initial conditions in a natural way at the beginning of the process itself.

The Laplace transform of a time function $x(t)$ is defined as

$$L[x(t)] = X(s) = \int_{-\infty}^{\infty} x(t) e^{-st} dt$$

where s is complex variable & equal to $s = \sigma + j\omega$.

Operator L is called the LT operator which transforms the time domain function $x(t)$ into frequency domain function $X(s)$.

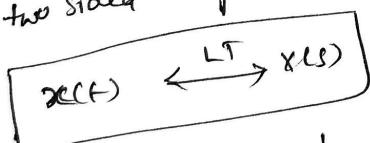
$$\text{ILT}[X(s)] = \frac{1}{2\pi j} \int_{-\infty - j\omega}^{\infty + j\omega} X(s) e^{st} ds$$

Unilateral / one sided Laplace transform

$$L[x(t)] = X(s) = \int_0^{\infty} x(t) e^{-st} dt$$

Bilateral / two sided Laplace transform

$$L[x(t)] = X(s) = \int_{-\infty}^{\infty} x(t) e^{-st} dt$$



Laplace Transform pair.

* Existence of Laplace Transform :-

The necessary and sufficient conditions for the existence of the Laplace transform are:

1. $x(t)$ should be continuous in the given closed interval.

2. $x(t) e^{-\sigma t}$ must be absolutely integrable.

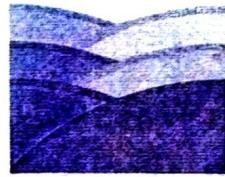
$X(s)$ exists only if $\int_{-\infty}^{\infty} |x(t)| e^{-\sigma t} dt < \infty$

& only if

$$\lim_{t \rightarrow \infty} e^{-\sigma t} x(t) = 0$$

The range of σ for which the LT converges is known as the region of convergence (ROC).

A40401- SIGNALS, SYSTEMS AND STOCHASTIC PROCESSES



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UNIT - III

Signal Transmission through Linear Systems

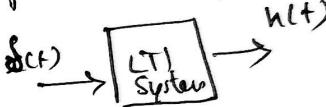
Linear System :- which obeys principle of superposition & principle of homogeneity are called a linear system.

Superposition - weighted sum of ilp sigs = corresponding weighted sum of o/p sigs of the system to each of the ilp sigs.

Homogeneity - $x_1(t)$ produces $y_1(t)$ then $a x_1(t)$ produce $a y_1(t)$.

Impulse response :- Impulse response is the o/p of system for a unit impulse if $x(t)$ is ilp $\Rightarrow \delta(t)$, o/p $y(t) = h(t)$.

For understanding system behaviour, Unit impulse response is very important.



$$L[\delta(t)] = 1 \quad \& \quad F[\delta(t)] = 1$$

Transfer function $H(s)$ of an LTI system is known in s-domain. The impulse response of sys can be found by taking inverse L.T. of $H(s)$

$$h(t) = L^{-1}[H(s)]$$

Response of a linear system :-

$y(t)$ is obtained by convoluting ilp $x(t)$ with impulse response of the system $h(t)$.

$$y(t) = h(t) * x(t) = x(t) * h(t).$$

If a non-causal signal is applied to a non-causal system then

$$y(t) = \int_{-\infty}^{\infty} h(\tau) x(t-\tau) d\tau = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau.$$

If a causal sig is applied to a non-causal system then

$$y(t) = \int_{-\infty}^t h(\tau) x(t-\tau) d\tau = \int_0^{\infty} x(\tau) h(t-\tau) d\tau$$

If a non-causal sig is applied to a causal system, then

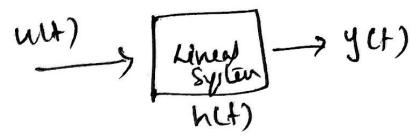
$$y(t) = \int_{-\infty}^t x(\tau) h(t-\tau) d\tau$$

If a causal signal is applied to a causal system, then

$$y(t) = \int_0^t h(\tau) x(t-\tau) d\tau = \int_0^t x(\tau) h(t-\tau) d\tau.$$

Step response

$$s(t) = h(t) * u(t)$$



For system in non-causal system

$$s(t) = \int_{-\infty}^t h(\tau) u(t-\tau) d\tau = \int_{-\infty}^t h(\tau) d\tau$$

for system in causal, then $s(t) = \int_0^t h(\tau) d\tau$

∴ The impulse unit step response of a C.R LTI system is integral of its impulse response

Linear Time Invariant (LTI) - system is linear as well as Time Invariant

$$y(t, T) = y(t-T)$$

O/p due to delayed i/p = delayed o/p

Linear Time Variant (LTV) - system is linear & time variant

$$y(t, T) \neq y(t-T)$$

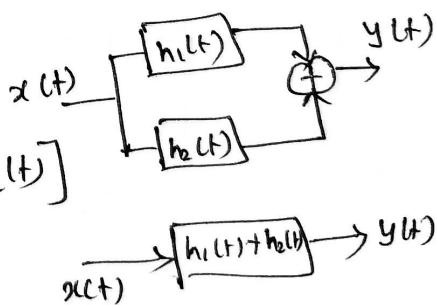
Properties of LTI System

1. Commutative property

$$x(t) * h(t) = h(t) * x(t)$$

2. Distributive property

$$x(t) * [h_1(t) + h_2(t)] = [x(t) * h_1(t)] + [x(t) * h_2(t)]$$



3. Associative property

$$x(t) * [h_1(t) * h_2(t)] = [x(t) * h_1(t)] * h_2(t)$$

4. Memoryless & memory system

Memoryless $h(t) = 0$ for $t \neq 0$

Memory $h(t) \neq 0$ for $t \neq 0$

then $y(t) = kx(t)$ k -constant

then $h(t) = k\delta(t)$

if $k=1$ then $h(t) = \delta(t)$

Causality

For causal LTI system $h(t) = 0$ for $t < 0$

for noncausal sysl o/p of LTI system is

$$y(t) = \int_0^{\infty} h(\tau) x(t-\tau) d\tau = \int_{-\infty}^t x(\tau) h(t-\tau) d\tau$$

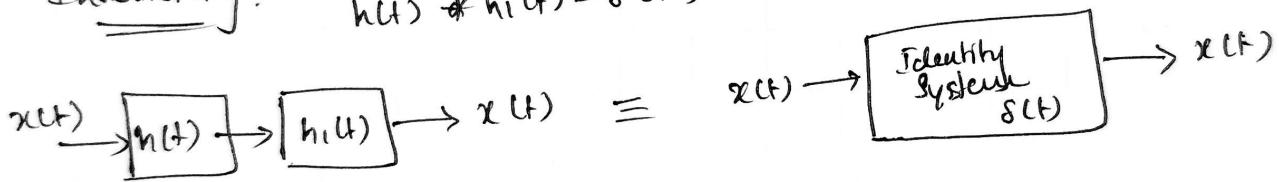
for general sysl o/p of LTI system is

$$y(t) = \int_0^t h(\tau) x(t-\tau) d\tau = \int_0^t x(\tau) h(t-\tau) d\tau$$

→ for Non causal LTI systems $h(t) \neq 0$ for $t < 0$

stability :- $\int_{-\infty}^{\infty} |h(\tau)| d\tau < \infty$

Invertibility :- $h(t) * h_1(t) = \delta(t)$



Unit step Response

The unit step response $s(t)$ of an LTI system is the o/p of the system for a unit step i/p $u(t)$

The response can be obtained by convolving the i/p unit step $u(t)$ with the impulse response $h(t)$ of the system.

$$s(t) = h(t) * u(t) = u(t) * h(t)$$

$$s(t) = \int_{-\infty}^t h(\tau) d\tau$$

∴ Unit step response of a c.t. LTI system is the sum integral of its impulse response

$$h(t) = \frac{d s(t)}{dt}$$

The unit impulse response is the first derivative of the unit step response.

Transfer function of an LTI system

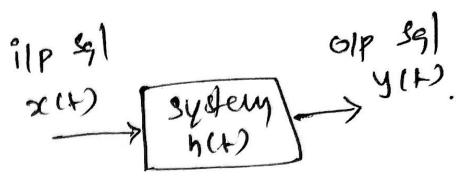
A C.T system is shown in figure below

$$y(t) = x(t) * h(t)$$

Apply L.T. on both side

$$Y(s) = X(s) H(s)$$

$$\frac{Y(s)}{X(s)} = H(s) = \frac{Y(s)}{X(s)}$$



$$H(s) = \mathcal{L}[h(t)] \text{ & } h(t) = \mathcal{L}^{-1}[H(s)]$$

The T.F of a C.T LTI system may be defined using Fourier transform of L.T. The T.F is defined only under zero initial conditions.

The T.F of a LTI system $H(\omega)$ is defined as the ratio of the F.T of the o/p sgl to the F.T of the i/p sgl when the initial conditions are zero.

$$H(\omega) = \frac{Y(\omega)}{X(\omega)} : g(\omega)$$

$$H(\omega) = |H(\omega)| e^{j\phi(\omega)}$$

The T.F in frequency domain $H(\omega)$ is also called the frequency response of the system. The frequency response is amplitude response plus phase response. $H(\omega) = A(\omega) e^{j\phi(\omega)}$ = amplitude response of the system

$$A(\omega) = |H(\omega)| X(\omega)$$

$$|Y(\omega)| = |H(\omega)| |X(\omega)|$$

$$\angle Y(\omega) = \angle H(\omega) + \angle X(\omega)$$

$H(\omega)$ has conjugate symmetry property

$$H(-\omega) \equiv H^*(\omega)$$

$$|H(-\omega)| = |H(\omega)|$$

$$\angle H(-\omega) = -\angle H(\omega)$$

The impulse response $h(t)$ of a system is the inverse F.T of its T.F. $H(\omega) = F[h(t)]$

$$h(t) = \mathcal{F}^{-1}[H(\omega)]$$

Filter characteristics of linear system

$$y(t) = x(t) * h(t)$$

Apply F.T.O.B.S.

$$Y(\omega) = X(\omega) H(\omega)$$

Here $H(\omega)$ is T.F. or sym function of the system

$X(\omega)$ - Spectral density function of the i/p sig $x(t)$

$Y(\omega)$ - Spectral density function of the response signal $y(t)$

\therefore The sym modifies the spectral density function of the i/p.

so it acts like as a kind of filter for various frequency components.
Some freq components are boosted in strength i.e. they are amplified

Some freq components are weekend in strength i.e. they are attenuated

Some may remain unaffected.

Now Each frequency component suffers a different

amount of phase shift in the process of transmission system.
Modifies the spectral characteristics density function of the i/p according
to its filter characteristics. The modification is carried out according
to the transfer function $H(\omega)$ which represents the response of the

System to various frequency components.

$H(\omega)$ acts as a weighting function | Spectral shaping function
to the different frequency components in the i/p sig. An LTI system
therefore acts as a filter. A filter is basically a frequency selective

nlw.

→ Some LTI sysm allow the transmission of only low freq comp &
stop high freq - LPF

→ Some LTI sysm allow the transmission only high freq & stop low freq
- HPF.

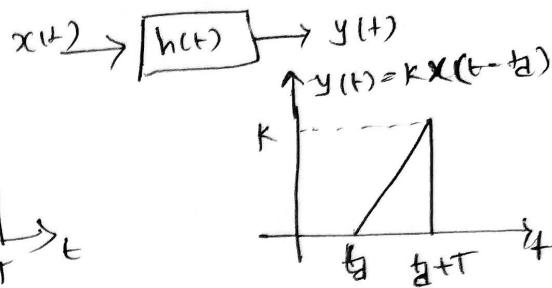
→ Some LTI sysm allows particular band of freq & rejects other
freq - BPF

→ Some LTI sysm rejects particular band of freq & stop other
freq comp - BRF.

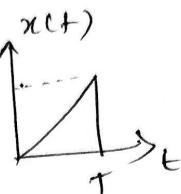


Distortionless transmission through system

The change of shape of the signal when it is transmitted through a system is called distortion.



Transmission of a sigl through a system is said to be distortionless if the o/p is an exact replica of the i/p sigl. This replica may have different magnitude & also it may have different time delay.



Distortionless Sym

Mathematically $y(t) = kx(t-\tau)$

where k is a constant representing the change in amplitude & τ is delay time. A distortionless system and typical i/p & o/p waveforms are shown in figure.

- Take i/p $F.T - D.B.S.$

$$Y(w) = k e^{-jw\tau} X(w)$$

$$\frac{Y(w)}{X(w)} = k e^{-jw\tau}$$

$$H(w) = k e^{-jw\tau}$$

By taking inverse F.T. the corresponding impulse response must be

$$h(t) = k \delta(t-\tau)$$

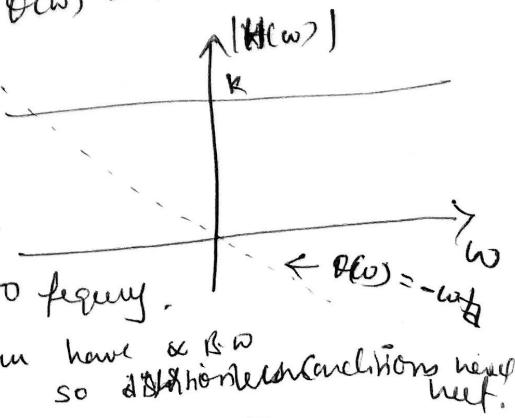
$$(h(w)) = k ; \quad \Phi(w) = L(h(w)) = -\omega\tau \quad \text{it varies linearly with frequency}$$

$$\Phi(w) = n\pi - \omega\tau \quad (\text{n integer})$$

So for distortionless transmission of a signal through a system, the magnitude

$|H(w)|$ should be a constant. ie all the frequency components of the o/p sigl must undergo the same amount of amplification

and attenuation ie, the system B.W is infinite and the phase spectrum should be proportional to freq.



But in practice no system can have such conditions hence

Linear phase system :- For distortionless transmission, there should not be any phase distortion. No phase distortion means the phase should be linear. So for distortionless transmission, the system must be of linear phase type.

For linear phase systems; the impulse response is symmetrical about $t=0$ this can be proved as follows,

$$\text{For linear phase system } H(\omega) = |H(\omega)| e^{-j\omega t_0}$$

For linear phase system

The impulse response of such a system is obtained by finding the

$$\text{Inverse F.T. } h(t) = \mathcal{F}^{-1}[H(\omega)] = \mathcal{F}^{-1}[|H(\omega)| e^{-j\omega t_0}]$$

$$\begin{aligned} &= \frac{1}{2\pi} \int_{-\infty}^{\infty} |H(\omega)| e^{j\omega t_0} e^{j\omega t} d\omega \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} |H(\omega)| e^{j\omega(t-t_0)} d\omega \\ &= \frac{1}{2\pi} \left[\int_{-\infty}^0 |H(\omega)| e^{j\omega(t-t_0)} d\omega + \int_0^{\infty} |H(\omega)| e^{j\omega(t-t_0)} d\omega \right] \\ &= \frac{1}{2\pi} \left[\int_0^{\infty} |H(\omega)| e^{-j\omega(t-t_0)} d\omega + \int_0^{\infty} |H(\omega)| e^{j\omega(t-t_0)} d\omega \right] \\ &= \frac{1}{2\pi} \left[\int_0^{\infty} |H(\omega)| [e^{-j\omega(t-t_0)} + e^{j\omega(t-t_0)}] d\omega \right] \\ &= \frac{1}{2\pi} \left[\int_0^{\infty} |H(\omega)| 2\cos \omega(t-t_0) d\omega \right] \end{aligned}$$

$$h(t) = \frac{1}{\pi} \int_0^{\infty} |H(\omega)| \cos \omega(t-t_0) d\omega$$

$$h(t_0 + t) = \frac{1}{\pi} \int_0^{\infty} |H(\omega)| \cos \omega t d\omega$$

$$h(t_0 - t) = \frac{1}{\pi} \int_0^{\infty} |H(\omega)| \cos \omega t d\omega$$

$$h(t_0 + t) = h(t_0 - t)$$

$\therefore h(t)$ for linear phase system is symmetrical about t_0 , and it is non-causal. Causal $\Rightarrow h(t) = \frac{1}{\pi} \int_0^{\infty} |H(\omega)| d\omega$

$$h_{\max} = h(0) = \frac{1}{\pi} \int_0^{\infty} |H(\omega)| d\omega$$

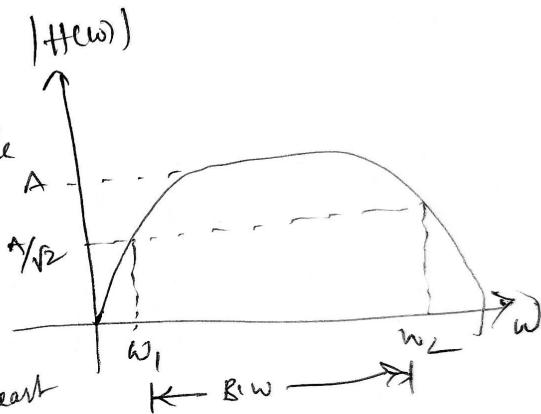
Signal Bandwidth

Spectral components of a signal extend from $-\infty$ to ∞ . Any practical signal has finite energy. As a result, the spectral components approach zero as ω tends to ∞ . Therefore, we neglect the spectral components which have negligible energy & select only a band of frequency components which have most of the signal energy. This band of frequencies that contain most of the signal energy is known as the B.W of the signal. Normally, the band is selected such that it contains around 90% of total energy depending on the precision.

System Bandwidth

The B.W of a system is defined as the range of frequencies over which the magnitude $|H(\omega)|$ remains within $\frac{1}{\sqrt{2}}$ times (with in 3dB) of its value at midband.

The Band limited Sgl can be transmitted without distortion if the system B.W is atleast equal to the signal B.W.



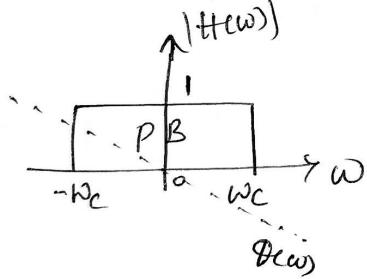
Ideal filter characteristics :-

A filter is a frequency selective N/W. It allows transmission of signal of certain frequencies with no attenuation & with very little attenuation, and it rejects or heavily attenuates signals of all other frequencies.

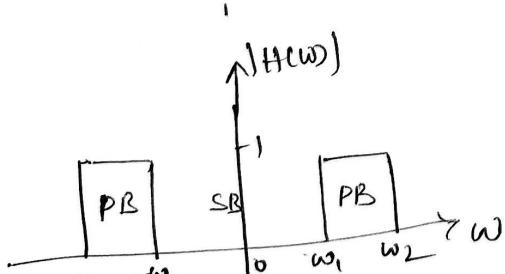
An ideal filter has very sharp cutoff characteristics, and it passes signals of certain specified band of frequencies exactly and totally rejects signals of frequencies outside this band. Its phase spectrum is linear.

Filters are usually classified according to their frequency response characteristics as low-pass filter (LPF), high-pass filter (HPF) band-pass filter (BPF) and band-elimination or band-stop or band-reject filter (BEF, BSF, BRF).

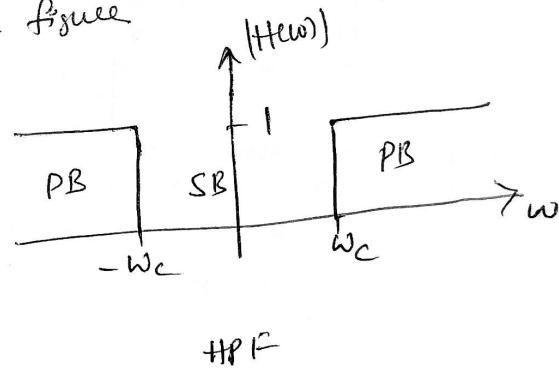
Ideal versions of these filters are described below and their magnitude responses are shown in figure



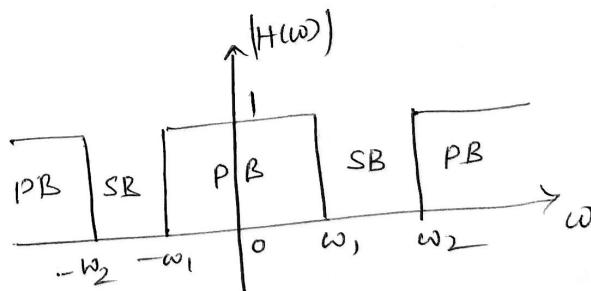
LPF



BPF



HPF



BRF

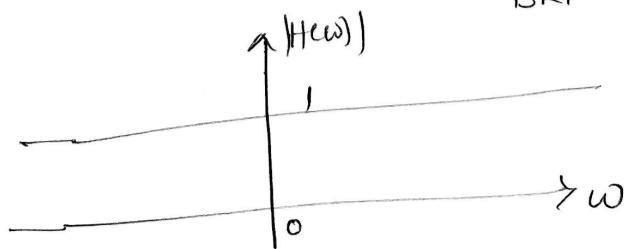


Fig:- Frequency Response of filters. ^{All Pass} ₀₋₁₁

Ideal LPF :- An ideal LPF transmits, without any distortion, all of the signals of frequencies below a certain frequency ω_c rad/sec. The signals of frequencies above ω_c rad/sec are completely attenuated.

The ω_c - cut-off frequency
phase function $\phi(\omega)$ for distortionless transmission is $-\omega t$.

Ideal HPF :- An ideal HPF transmits, without any distortion, all of the signals of frequencies above a certain frequency ω_c rad/sec and attenuates completely the signals of frequencies below ω_c rad/sec.

$$T.F \quad |H(\omega)| = \begin{cases} 0, & |\omega| < \omega_c \\ 1, & |\omega| > \omega_c \end{cases}$$

Ideal BPF :- An ideal BPF transmits, without any distortion, all of the signals of frequencies within a certain frequency band $(\omega_2 - \omega_1)$ rad/sec and attenuates completely the signals of frequencies outside this band. The corresponding phase function for distortionless transmission is $-\omega t$.

$$T.F \quad |H(\omega)| = \begin{cases} 1, & \omega_1 < \omega < \omega_2 \\ 0, & \omega < \omega_1 \text{ or } \omega > \omega_2 \end{cases}$$

Ideal BRF :- An ideal band rejection filter totally attenuates all of the signals of frequencies within a certain frequency band $(\omega_2 - \omega_1)$ rad/sec and transmits without any distortion all signals of frequencies outside this band. The corresponding phase function for distortionless transmission is $-\omega t$.

$$T.F \quad |H(\omega)| = \begin{cases} 0, & \omega_1 < \omega < \omega_2 \\ 1, & \omega < \omega_1 \text{ or } \omega > \omega_2 \end{cases}$$

All pass filter & All pass filter transmits signals of all frequencies without any distortion, that is, its B.W is as ∞

$$T.F \quad |H(\omega)| = 1 \quad \text{for all frequencies.}$$

The corresponding phase function for distortionless transmission is $-\omega t$.

All ideal filters are non-causal systems. Hence none of them is physically realizable.

* Causality and paley-wiener criterion for physical realization :-

A system is said to be causal if it does not produce an output before the input is applied. For a system to be causal, the condition to be satisfied is its impulse response must be zero for $t < 0$.

From ZOH, i.e., $h(t) = 0 \text{ for } t < 0$.
Physical realization implies that it is physically possible to construct that system in real time.

A physically realizable system cannot have a response before I/P is applied. This is known as causality condition.

$h(t)$ must be causal for a physically realizable sys.

In frequency domain, this criterion implies that a necessary & sufficient condition for a magnitude function $H(\omega)$ to be physically realizable is

$$\int_{-\infty}^{\infty} \frac{|H(j\omega)|}{1+\omega^2} d\omega < \infty.$$

The magnitude function $|H(\omega)|$ must, however, be square integrable before the paley-wiener condition is valid. That is

$$\int_{-\infty}^{\infty} |H(\omega)|^2 d\omega < \infty.$$

A sys whose magnitude function violates the paley-wiener criterion has a non-causal impulse response.

→ Following conclusions can be drawn from paley-wiener criterion

1. $|H(\omega)|$ may be zero at some discrete frequencies (but $\int_{-\infty}^{\infty} |H(\omega)|^2 d\omega = \infty$)

2. $|H(\omega)|$ cannot fall off to zero faster than a function of exponential order.

Relationship b/w B.W & rise time

$$\text{T.R of LPF} \cdot H(w) = |H(w)| e^{-j\omega t_d}$$

$$\text{where } |H(w)| = \begin{cases} 1, & |w| < w_c \\ 0, & |w| > w_c \end{cases}$$

w_c - cut-off frequency

$$H(w) = e^{-j\omega t_d} \quad -w_c \leq w \leq w_c$$

$$= 0 \quad w > w_c$$

The impulse response $h(t)$ of the LPP is obtained by taking the inverse Fourier Transform of $H(w)$.

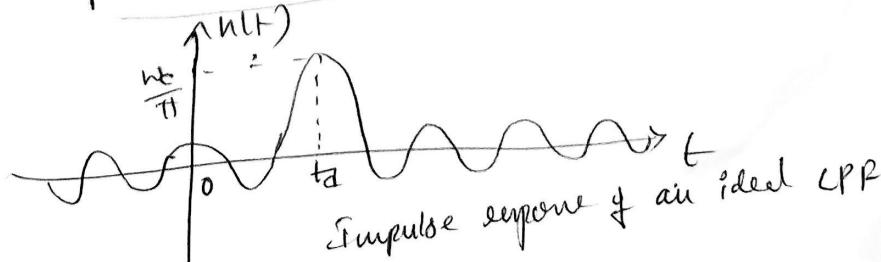
$$\begin{aligned} h(t) &= \tilde{F}^{-1}(H(w)) = \frac{1}{2\pi} \int_{-w_c}^{w_c} e^{j\omega t_d} e^{j\omega t} d\omega \\ &= \frac{1}{2\pi} \int_{-w_c}^{w_c} e^{j\omega(t-t_d)} d\omega \\ &= \frac{1}{2\pi} \left[\frac{e^{j\omega_c(t-t_d)}}{j\omega_c(t-t_d)} \right]_{-w_c}^{w_c} e^{-j\omega_c(t-t_d)} \\ &= \frac{1}{\pi(t-t_d)} \left[\frac{e^{j\omega_c(t-t_d)} - e^{-j\omega_c(t-t_d)}}{2j} \right] \end{aligned}$$

$$= \frac{1}{\pi(t-t_d)} \operatorname{sinc} w_c(t-t_d)$$

$$= \frac{1}{\pi} \frac{\sin w_c(t-t_d)}{(t-t_d)} \times \frac{w_c}{w_c}$$

$$= \frac{w_c}{\pi} \frac{\sin w_c(t-t_d)}{w_c(t-t_d)}$$

$$h(t) = \frac{w_c}{\pi} \operatorname{sinc} w_c(t-t_d)$$



$$\text{step response } y(t) = h(t) * u(t)$$

$$= \int_{-\infty}^t h(\tau) d\tau$$

$$= \int_{-\infty}^t \frac{\omega_c}{\pi} \frac{\sin \omega_c(t-\tau)}{\omega_c(t-\tau)} d\tau$$

$$x = \omega_c(t-\tau)$$

$$dx = \omega_c d\tau \quad \text{or} \quad d\tau = \frac{dx}{\omega_c}$$

$$y(t) = \int_{-\infty}^{\omega_c(t-\tau)} \frac{\omega_c}{\pi} \frac{\sin x}{x} \frac{dx}{\omega_c} = \frac{1}{\pi} \int_{-\infty}^{\omega_c(t-\tau)} \frac{\sin x}{x} dx$$

$$= \frac{1}{\pi} [Si(x)]_{-\infty}^{\omega_c(t-\tau)}$$

$$Si(-x) = -Si(x)$$

where Si is sine integral function
properties 1. $Si(0) = 0$

$$2. Si(\infty) = \frac{\pi}{2}$$

$$3. Si(-x) = -Si(x)$$

The step response can be expressed as

$$y(t) = \frac{1}{\pi} [Si(\omega_c t - \tau_0) - Si(-\infty)]$$

$$= \frac{1}{\pi} \left\{ [Si(\omega_c t - \tau_0)] + \frac{\pi}{2} \right\}$$

$$= \frac{1}{\pi} Si(\omega_c(t - \tau_0)) + \frac{1}{2}$$

if $\omega_c \rightarrow \infty$ then the response is:

$$y(t) = \frac{1}{2} + \frac{1}{\pi} Si(\infty) = \frac{1}{2} + \frac{1}{\pi} \left(\frac{\pi}{2} \right) = 1$$

if $\omega_c \rightarrow -\infty$ then the response is

$$y(t) = \frac{1}{2} + \frac{1}{\pi} Si(-\infty) = \frac{1}{2} + \frac{1}{\pi} \left(-\frac{\pi}{2} \right) = 0$$

The step response of LPF is shown in figure

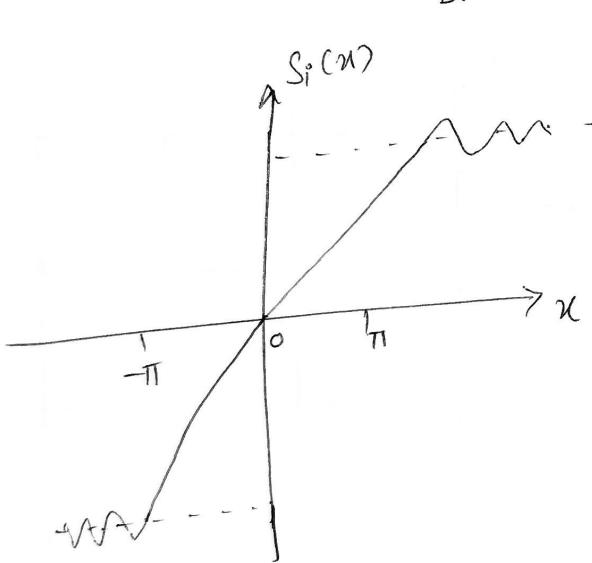
From fig(b) we can observe that $y(t)$ approaches a delay unit step $u(t-t_0)$ but the abrupt rise of $y(t)$ corresponds to more gradual rise of the OP by

The rise time t_r is defined as the time required for the response to reach from 0% to 100% of the final value. To find it, draw a tangent at $t=t_0$ with the line $y(t)=0$ and $y(t)=1$ $\frac{d}{dt}$

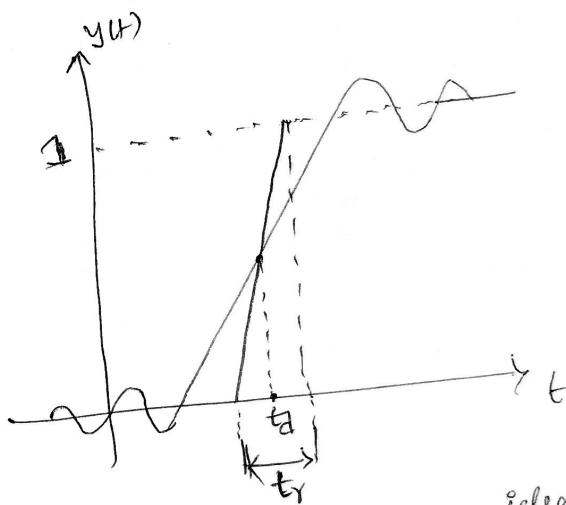
$$\frac{dy(t)}{dt} = \frac{1}{t_r} = \frac{\omega_c}{\pi} \left. \frac{\sin \omega_c(t-t_0)}{\omega_c(t-t_0)} \right|_{t=t_0} = \frac{\omega_c}{\pi}.$$

$$t_r = \frac{\pi}{\omega_c}$$

For a low-pass filter cut-off frequency ω_c = Band width
rise time is inversely proportional to the Bandwidth
Bandwidth \times Rise time = constant.



(a) S_i function



(b) Step response of an ideal LPF.

Energy Density Spectrum

Spectral density it is the distribution of Energy or power of a signal per unit B.W as a function of frequency.

Energy Signals — Signals with finite Energy and zero average power, i.e., $0 < E < \infty$ and $P = 0$ are called Energy signals, e.g.: Aperiodic signals like pulse.

Normalized energy - It defined as the Energy dissipated by a voltage signal applied across 1Ω resistor

$$E = \int_{-\infty}^{\infty} |x(t)|^2 dt$$

For Energy signal exists only if E is finite i.e., $0 < E < \infty$.

Parseval's theorem for Energy signals (Rayleigh energy theorem)

This theorem defines the Energy of a signal in terms of its F.T. Every $x(t)$ can directly evaluated from its frequency spectrum $X(\omega)$ without the knowledge of its time domain version i.e. $x(t)$.

$$E = \int_{-\infty}^{\infty} |x(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X(\omega)|^2 d\omega$$

$$E = \int_{-\infty}^{\infty} |X(f)|^2 df$$

Proof :- Consider a function $x(t)$ such that

$$x(t) \longleftrightarrow X(\omega)$$

Let $x^*(t)$ be the conjugate of $x(t)$ such that

$$x^*(t) \longleftrightarrow X^*(\omega).$$

The energy of signal $x(t)$ is given by

$$E = \int_{-\infty}^{\infty} |x(t)|^2 dt = \int_{-\infty}^{\infty} x(t) x^*(t) dt = \int_{-\infty}^{\infty} x^*(t) x(t) dt$$

Express $x(t)$ with IFT of $X(\omega)$

$$E = \int_{-\infty}^{\infty} x^*(t) \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} X(\omega) e^{j\omega t} d\omega \right) dt$$

interchanging the order of integration

$$E = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(w) \left[\int_{-\infty}^{\infty} x(t) e^{j\omega t} dt \right] dw$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} X(w) X^*(-w) dw$$

$$E = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X(w)|^2 dw$$

Let $w = 2\pi f$

$$dw = 2\pi df$$

normally $X(2\pi f)$ written as $X(f)$.

$$E = \int_{-\infty}^{\infty} |X(f)|^2 df$$

This is called Parseval's theorem for energy signals

Energy Spectral Density (ESD).

It gives the distribution of energy of a signal in the frequency domain for an energy signal; the total area under the spectral density curve plotted as a function of frequency is equal to the total energy of the signal.

it is also called Energy density spectrum
is denoted as $\Phi(w) = |X(w)|^2$

$$Y(w) = H(w)X(w)$$

$$\text{ESD of iip } \Phi_x(w) = |X(w)|^2$$

$$\text{ESD of oip } \Phi_y(w) = |Y(w)|^2$$

$$\begin{aligned} \Phi_y(w) &= |Y(w)|^2 = |X(w)H(w)|^2 \\ &= |X(w)|^2 |H(w)|^2 \end{aligned}$$

$$\Phi_y(w) = |H(w)|^2 \Phi_x(w)$$

thus, the ESD of the oip of a linear system is the product of ESD of iip (Excitation) & square of the magnitude of the T.F.

$$\text{Energy of the OLP sol } E_y = \int_{-\infty}^{\infty} \psi_y(t) dt$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} \psi_y(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} |H(\omega)|^2 \psi_x(\omega) d\omega$$

$$E_y = \frac{1}{\pi} \int_{-\infty}^{\infty} |H(\omega)|^2 \psi_x(\omega) d\omega$$

If the LTI system is an ideal LPF with lower & upper cutoff frequency $f_L \leq f_H$ respectively then $H(\omega) = 1$ for $f_L \leq f \leq f_H$

$$E_y = \frac{1}{\pi} \int_{f_L}^{f_H} \psi_x(\omega) d\omega$$

$$E_y = \frac{1}{\pi} \int_{f_L}^{f_H} \psi_x(2\pi f) 2\pi df = 2 \int_{f_L}^{f_H} \psi_x(f) df$$

Properties of ESD

- Total area under the energy density spectrum is equal to the total energy of the signal.

$$E = \frac{1}{2\pi} \int_{-\infty}^{\infty} \psi(\omega) d\omega = \int_{-\infty}^{\infty} \psi(f) df$$

- If $x(t)$ is the IIP to an LTI system with impulse response $h(t)$, then the IIP & OLP ESD functions are related as

$$\psi_y(\omega) = |H(\omega)|^2 \psi_x(\omega)$$

$$\text{or } \psi_y(f) = |H(f)|^2 \psi_x(f)$$

- The auto correlation function $R(\tau)$ & ESD $\psi(\omega)$ are

$$R(\tau) \xleftrightarrow{FT} \psi(\omega)$$

$$R(\tau) \xleftrightarrow{IFT} \psi(f)$$

Power Density Spectrum

power signals = signals with finite average power & infinite energy i.e., $0 < P < \infty$ and $E = \infty$ are called power signals, e.g. periodic signals.

$$\text{Average power } P = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} |x(t)|^2 dt$$

Power P is actually mean square value of time average of the squared signal

$$P = \overline{|x(t)|^2} = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T |x(t)|^2 dt$$

Parseval's theorem defines the power of a signal in terms of its F.S coeff i.e., in terms of the harmonic components present in the signal.

mathematically it is given by

$$P = \sum_{n=-\infty}^{\infty} |c_n|^2$$

$$\text{Proof: } P = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} |x(t)|^2 dt = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} x(t) x^*(t) dt$$

Exponential Fourier series $x(t) = \sum_{n=-\infty}^{\infty} c_n e^{jnw_0 t}$

$$P = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} \sum_{n=-\infty}^{\infty} c_n e^{jnw_0 t} \sum_{m=-\infty}^{\infty} c_m e^{-jmw_0 t} x^*(t) dt$$

Interchanging the order of summation & integration

$$P = \sum_{n=-\infty}^{\infty} c_n \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} x^*(t) c_n e^{jnw_0 t} dt$$

$$= \sum_{n=-\infty}^{\infty} c_n c_n^* = \sum_{n=-\infty}^{\infty} |c_n|^2$$

$$P = \sum_{n=-\infty}^{\infty} |c_n|^2 //$$

Called Parseval's power theorem

PSD $\frac{d}{dt}$ Power Spectral Density

The distribution of average power of the signal in the frequency domain is called power spectral density or power density spectrum (PSD or PD).¹⁹

To derive the PSD, assume the power signal as a limiting case of the Energy Signal. Consider a power signal $x(t)$. Extending to infinity as shown.

Let us truncated this signal so that it is zero outside the interval T_2 .

Let this truncated signal be $x_T(t)$

$$x_T(t) = \begin{cases} x(t), & |t| < \frac{T}{2} \\ 0, & \text{elsewhere} \end{cases}$$

The signal $x_T(t)$ is of finite duration T & hence it is an energy signal

with energy E given by

$$E = \int_{-\infty}^{\infty} |x_T(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X_T(\omega)|^2 d\omega$$

where

$$x_T(t) \leftrightarrow X_T(\omega).$$

As $x(t)$ over the interval $(-\frac{T}{2} \text{ to } \frac{T}{2})$ is same as $x_T(t)$ over the interval $-\infty \text{ to } \infty$, we have,

$$\int_{-\infty}^{\infty} |x_T(t)|^2 dt = \int_{-T_2}^{T_2} |x(t)|^2 dt$$

$$\frac{1}{T} \int_{-T_2}^{T_2} |x(t)|^2 dt = \frac{1}{2\pi T} \int_{-\infty}^{\infty} |X_T(\omega)|^2 d\omega$$

If $T \rightarrow \infty$ the left hand side of above eqn represents the average power P of the function $x(t)$.

$$P = \frac{1}{2\pi} \int_{-\infty}^{\infty} \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T_2}^{T_2} |x_T(\omega)|^2 d\omega$$

If $T \rightarrow \infty$, $|X_T(\omega)|^2 / T$ approaches a finite value.

Let this finite value is denoted by $S(\omega)$ i.e,

$$S(\omega) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T_2}^{T_2} |x_T(\omega)|^2 d\omega$$

$$P = \overline{x^2(t)} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S(\omega) d\omega = \int_{-\infty}^{\infty} S(f) df.$$

where $\overline{x^2(t)}$ is the MSE of $x(t)$.

The average power is

$$P = 2 \frac{1}{2\pi} \int_0^\infty S(\omega) d\omega = \frac{1}{\pi} \int_0^\infty S(\omega) d\omega = 2 \int_0^\infty S(f) df$$

The PSD of a periodic function is given by

$$S(\omega) = 2\pi \sum_{n=-\infty}^{\infty} |C_n|^2 \delta(\omega - n\omega_0)$$

and alternately $S(f) = \sum_{n=-\infty}^{\infty} |C_n|^2 \delta(f - nf_0)$

The i/p & o/p relation of a linear system in terms of PSD is given by $S_y(\omega) = |H(\omega)|^2 S_x(\omega)$

$$S_y(f) = |H(f)|^2 S_x(f)$$

Properties of PSD

1. The area under the PSD function is equal to the average power of that signal i.e,

$$P = \frac{1}{2\pi} \int_{-\infty}^{\infty} S(\omega) d\omega = \int_{-\infty}^{\infty} S(f) df$$

2. The i/p & o/p PSD of an LTI system are related as

$$S_y(\omega) = |H(\omega)|^2 S_x(\omega)$$

3. The autocorrelation function $R(\tau)$ & PSD $S(\omega)$ form a Fourier pair i.e,

$$R(\tau) \leftrightarrow S(\omega)$$

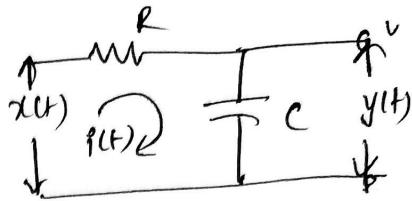
~~The comparison of PSD & PSF~~

Find the o/p voltage of the RC low pass filter shown in figure for an i/p voltage of $+e^{-t/RC}$

21

Sol:

$$H(s) = \frac{Y(s)}{X(s)} = \frac{1/s}{R + 1/s}$$



$$= \frac{1}{1 + RCS}$$

$$x(t) = t e^{-t/RC}$$

$$Y(s) = \frac{1}{1 + RCS} X(s) \quad \text{if}$$

$$X(s) = \frac{1}{(s + \frac{1}{RC})^2}$$

$$Y(s) = \frac{1}{RC(s + \frac{1}{RC})} \cdot \frac{1}{(s + \frac{1}{RC})^2}$$

$$Y(s) = \frac{1}{RC (s + \frac{1}{RC})^3}$$

B-side is

Apply \mathcal{L}^{-1} on.

$$y(t) = \frac{1}{RC} t^2 e^{-t/RC} u(t)$$

Ex

$$y(t) = e^{-t} u(t)$$

$$x(t) = e^{-2t} u(t)$$

find

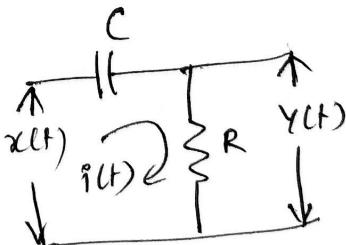
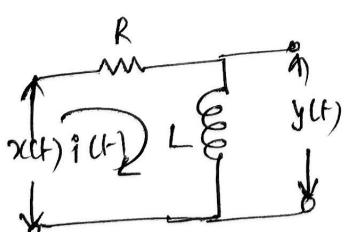
impulse response & frequency response of the system

find o/p

Ex

$$x(t) = e^{3t} u(t)$$

$$u(t) = e^{-2t} u(t) + e^{2t} u(-t)$$



Ex

Ex: Consider a stable LTI system that is characterized by the differential equation $\frac{d^2y(t)}{dt^2} + 4 \frac{dy(t)}{dt} + 3y(t) = \frac{dx(t)}{dt} + 2x(t)$ 22

Find its response for i/p $x(t) = e^{ut}$.

$$X(s) = \frac{1}{s+1}$$

$$s^2 Y(s) + 4s Y(s) + 3 Y(s) = s X(s) + 2 X(s)$$

$$(s^2 + 4s + 3) Y(s) = (s+2) X(s)$$

$$\frac{Y(s)}{X(s)} = \frac{s+2}{s^2 + 4s + 3} = \frac{s+2}{(s+1)(s+3)}$$

$$\frac{Y(s)}{X(s)} = \frac{s+2}{(s+1)(s+2)} \cdot \frac{1}{s+1} = \frac{s+2}{(s+1)^2(s+2)}$$

$$\frac{A}{s+1} + \frac{B}{(s+1)^2} + \frac{C}{s+2} = \frac{s+2}{(s+1)^2(s+2)}$$

$$A(s+1)(s+2) + B(s+1) + C(s+1)^2 = s+2$$

$$A + C = 0 \quad ; 3A + B + 2C = 1 \quad 2A + B + C = 2$$

$$3A + 3C = 0 \quad ; 3C = 0$$

$$2A$$

$$\log\left(\frac{1+s}{s}\right)$$

$$X(s) = \log\left(\frac{1+s}{s}\right)$$

$$x(t) = L^{-1}(X(s))$$

$$X(s) = L(x(t))$$

$$L[x(t)] = \log\left(\frac{1+s}{s}\right)$$

From property of differentiation in domain $-x(t) = -\frac{d}{ds} \left[\log\left(\frac{1+s}{s}\right) \right]$

$$= -\frac{d}{ds} \left[\log(1+s) - \log s \right]$$

$$= \frac{-1}{s+1} + \frac{1}{s}$$

$$-e^{-t} u(t) + u(t)$$

$$x(t) = \frac{(-e^{-t} u(t) + u(t))}{t}$$

Random process - Temporal characteristics

(1)

Definition: Random process is a family of functions $\{X \leq x(t, s)\}$

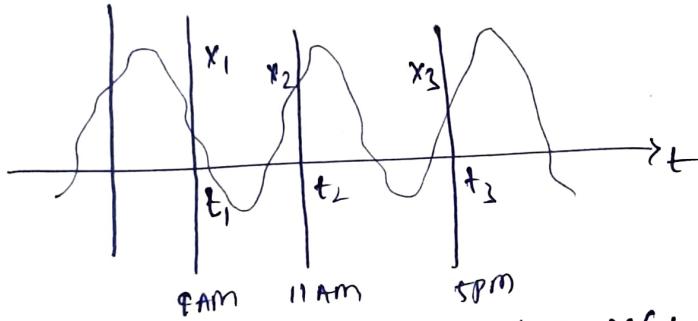
$s \in S$ & $t \in T\}$ defined with random variables $\{X \leq x\}$ on a sample space S and with a function of time T .

Random process is a function of two variables 1. Sample space
2. Time

Ex: ① Let us consider an experiment which measures the number of calls received in peak hours. The calls received (sample space) is a random process as the number of calls received at different time intervals may be different.

thus the number of calls is a function of both sample space & time.

②



Random process is represented $X(t, s) = x(t_1, t_2, t_3; x_1, x_2, x_3)$

Sample space $S = \{x_1, x_2, x_3\}$

$$x(t_1, s) = x_1(t)$$

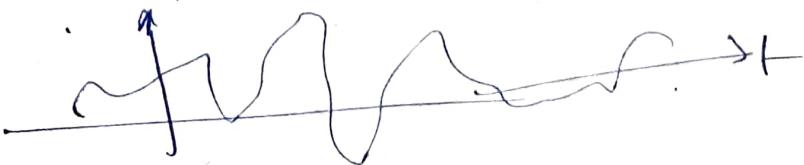
⇒ Deterministic Random process - A process is called deterministic random process if future values of any sample function can be predicted from its past values.

$$\text{ex: } x(t) = A \sin(\omega_0 t + \theta)$$

- predicted is known & from known shape

⇒ Non Deterministic Random process - The future values of a sample function cannot be predicted from observed past values.

Ex:



Classification of random processes.

(2)

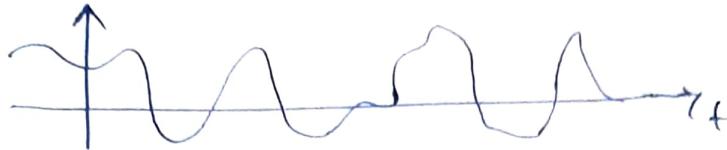
Four types based on time t and amplitude of random variable X .

1. Continuous Random Processes

Both the random variable X & time are continuous over the entire time.

(6)

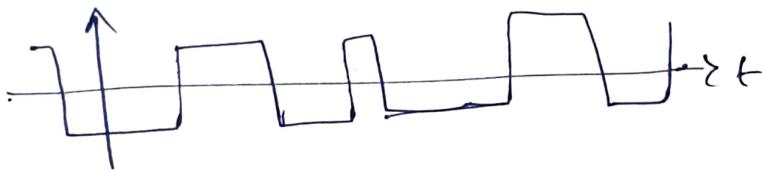
Ex: noise in any n/w.



2. Discrete Random Processes

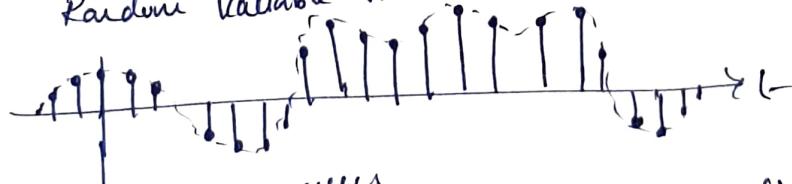
the random variable X has only discrete values while time t is continuous.

Ex: Digital Encoded Signal has only two discrete values



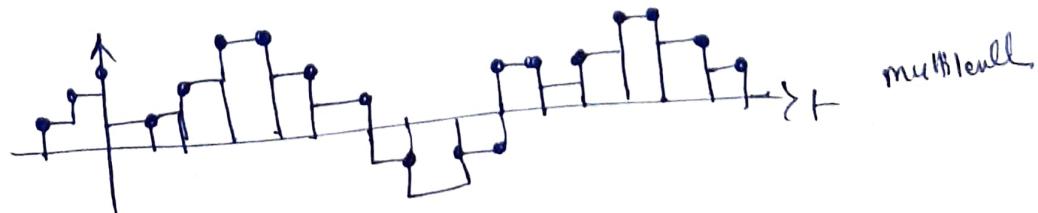
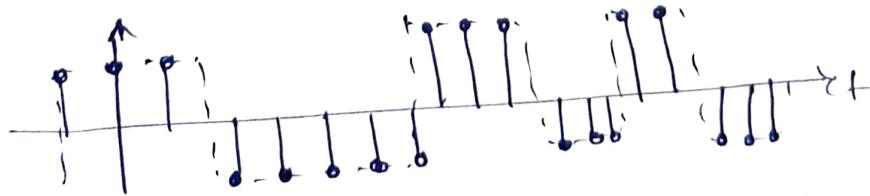
3. Continuous Random Sequences

Random Variable X is continuous but time t has discrete value



4. Discrete Random Sequences

Both random variables X and t are discrete - it is obtained by sampling & quantizing a random signal. Called digital process.



Distribution & Density functions of random process

(3)

A random variable can be obtained from a random process at a particular instant of time t . The random variable has all the properties that are related to its probability density function.

If two random variables are obtained from the random process at two different times. They will have all the statistical properties related to their joint probability density functions.

If N random variables defined at N time instants will have the statistical properties related to their N -dimensional joint probability density functions.

Joint distribution function of a random process

Let a random process $x(t)$, for a single random variable at time t_1 , $x_1 = x(t_1)$ the cumulative distribution function is defined as

$$F_x(x_1; t_1) = P\{x(t_1) \leq x_1\}$$

where x_1 is any real number. The function $F_x(x_1; t_1)$ is

known as the first order distribution function of $x(t)$.

Two random variables at time instants t_1, t_2 $x(t_1) = x_1, x(t_2) = x_2$

$$x(t_2) = x_2 \quad F_x(x_1, x_2; t_1, t_2) = P\{x(t_1) \leq x_1, x(t_2) \leq x_2\}$$

Called second order joint distribution function.

N order joint distribution function is

$$F_x(x_1, x_2, x_3, \dots, x_N; t_1, t_2, \dots, t_N) = P\{x(t_1) \leq x_1, x(t_2) \leq x_2, \dots, x(t_N) \leq x_N\}$$

$$F_x(x_1, x_2, x_3, \dots, x_N; t_1, t_2, \dots, t_N)$$

Joint Density function of ~~JDF~~ JDF of a random process can be obtained from the derivatives of the distribution function.

1. First order density function

$$f_x(x_1; t) = \frac{dF_x(x_1; t)}{dx_1}$$

2. Second order joint density function

$$f_x(x_1, x_2; t_1, t_2) = \frac{\partial^2 F_x(x_1, x_2; t_1, t_2)}{\partial x_1 \partial x_2}$$

3. N^{th} order joint density function

$$f_x(x_1, x_2, \dots, x_N; t_1, t_2, \dots, t_N) = \frac{\partial^N F_x(x_1, x_2, \dots, x_N; t_1, t_2, \dots, t_N)}{\partial x_1 \partial x_2 \dots \partial x_N}$$

4. If $x(t)$ is a discrete time process, then N^{th} order probability mass function is

$$P_x(x_1, x_2, \dots, x_N; t_1, t_2, \dots, t_N) = P\{x(t_1) = x_1, x(t_2) = x_2, \dots, x(t_N) = x_N\}$$

* Independent random process

Consider a random process $x(t)$, let $x(t_i) = x_i$; $i = 1, 2, 3, \dots, N$

N random variables defined at time instants t_1, t_2, \dots, t_N with density functions $f_x(x_1; t_1); f_x(x_2; t_2), \dots, f_x(x_N; t_N)$.

If the random process $x(t)$ is statistically independent, then the N^{th} order joint density function of $x(t)$ is equal to the product of individual joint functions of $x(t)$.

$$f_x(x_1, x_2, x_3, \dots, x_N; t_1, t_2, t_3, \dots, t_N) = f_x(x_1; t_1) \cdot f_x(x_2; t_2) \cdot f_x(x_3; t_3) \cdots f_x(x_N; t_N)$$

Now, let us consider two random processes $x(t)$ and $y(t)$ with joint density

have random variables $x(t_1), x(t_2), x(t_3), \dots, x(t_N)$ and $y(t)$ have random variables $y(t'_1), y(t'_2), \dots, y(t'_N)$ with joint density function:

$$f_{xy}(y_1, y_2, y_3, \dots, y_N; t'_1, t'_2, t'_3, \dots, t'_N)$$

(3)

statistical properties of Random process

1. Mean :- The mean value of a random process $x(t)$ is equal to the expected value of the random process $x(t)$ is denoted as

$$X(t) = E[x(t)] = \int_{-\infty}^{\infty} x f_x(x; t) dx.$$

where $f_x(x; t)$ is the probability density function of the random process $x(t)$. The mean value $E[X(t)]$ is also called Ensemble average of $x(t)$.

2. Autocorrelation :- Consider a random process $x(t)$. Let x_1 & x_2 be two random variables defined at times t_1 and t_2 respectively with joint density function $f_{x_1, x_2}(u_1, u_2; t_1, t_2)$.

The correlation of x_1 and x_2 $\cdot E[x_1 x_2] = E[x(t_1)x(t_2)]$ is called the autocorrelation function of the random process $x(t)$ is denoted as

$$R_{xx}(t_1, t_2) = E[x(t_1)x(t_2)] = E[x_1 x_2]$$

$$\text{or } R_{xx}(t_1, t_2) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x_1 x_2 f_{x_1, x_2}(u_1, u_2; t_1, t_2) du_1 du_2.$$

3. Cross Correlation :- Consider two random process $x(t)$ and $y(t)$ denoted with random variables x and y at time instants t_1 and t_2 respectively. The joint density function is $f_{x,y}(x, y; t_1, t_2)$. Then the correlation of x & y $E[x y] = E[x(t_1)y(t_2)]$ is called the cross correlation function of the random processes $x(t)$ and $y(t)$ if it is denoted as

$$R_{xy}(t_1, t_2) = E[x(t_1)y(t_2)] = E[xy]$$

$$\text{or } R_{xy}(t_1, t_2) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} xy f_{x,y}(x, y; t_1, t_2) dx dy$$

Stationary processes: A random process is said to be stationary if all its statistical properties such as mean, moments, variances etc. do not change with time. (6)

The stationary which depends on the density functions of the random variables of the process has different levels & orders.

1st order stationary process: A random process is said to be stationary to order one or first order stationary if its first order stationary process $f_x(x_1, t)$ density function does not change with time or shift in time value. If $x(t)$ is first order stationary process, then

$$f_x(x_1, t_1) = f_x(x_1, t_1 + \Delta t) \text{ for any } t_1.$$

Δt - shift in time value

$\Rightarrow f_x(x_1, t_1)$ is independent of t_1 , so the mean value of the process is constant.

$$\text{from } E[x(t_1)] = E[\bar{x}_1] = \int_{-\infty}^{\infty} x_1 f_x(x_1, t_1) dx_1$$

$$E[x(t_2)] = E[\bar{x}_2] = \int_{-\infty}^{\infty} x_2 f_x(x_2, t_2) dx_2$$

$$\text{sub } t_2 = t_1 + \Delta t$$

$$E[x(t_1 + \Delta t)] = \int_{-\infty}^{\infty} x_1 f_x(x_1, t_1 + \Delta t) dx_1$$

For stationary random process, we know that

$$f_x(x_1, t_1 + \Delta t) = f_x(x_1, t_1)$$

$$E[x(t_1 + \Delta t)] = \int_{-\infty}^{\infty} x_1 f_x(x_1, t_1) dx_1$$

$$E[x(t_1 + \Delta t)] = E[x(t_1)] = \text{a constant}$$

2nd order stationary process:

$$f_x(x_1, x_2, t_1, t_2) = f_x(x_1, x_2, t_1 + \Delta t, t_2 + \Delta t) \text{ for all } t_1, t_2, \Delta t.$$

It is a function of time differences $(t_2 - t_1)$ and not absolute time t .

Note that a second order stationary process is also a first order stationary process

$$R_{xx}(t_1, t_2) = E[x(t_1)x(t_2)]$$

$$\text{if } \tau = t_2 - t_1 \text{ then } R_{xx}(t_1, t_1 + \tau) = E[x(t_1)x(t_1 + \tau)] = R_{xx}(\tau)$$

$R_{xx}(\tau)$ should be independent of time t .

$R_{xx}(\tau)$ should be independent of time t .

Wide Sense Stationary Processes (WSS)

If a random process $X(t)$ is a second order stationary process, then it is called a wide sense stationary process (WSS) or a weak sense stationary process X . However the converse is not true.

The conditions for a wide sense stationary process are

1. $E[X(t)] = \bar{X} = \text{constant}$
2. $E[X(t)X(t+T)] = R_{XX}(T)$ is independent of absolute time t .

Joint Wide Sense Stationary Processes

Consider two random processes $x(t)$ & $y(t)$. If they are jointly wide sense stationary, then the cross correlation function of $x(t)$ & $y(t)$ is a function of the time difference $\tau = t_2 - t_1$. Only and absolute time.

The cross correlation function

$$R_{XY}(t_1, t_2) = E[x(t_1), y(t_2)].$$

If the time difference $\tau = t_2 - t_1$ & $t = t_1$ then

$$R_{XY}(t, t+T) = E[x(t), y(t+T)] = R_{XY}(\tau).$$

Therefore, the conditions for a process to be a joint wide sense stationary process are

1. $E[X(t)] = \bar{X} = \text{constant}$
2. $E[Y(t)] = \bar{Y} = \text{constant}$
3. $E[X(t)Y(t+T)] = R_{XY}(T)$ is independent of time t .

Strict Sense Stationary Processes (SSS)

A random process $x(t)$ is said to be strictly sense stationary if its N th order joint density function does not change with time or shift in time value

$$f_X(x_1, x_2, x_3, \dots, x_N; t_1, t_2, \dots, t_N) = f_X(x_1, x_2, \dots, x_N; t_1 + \Delta t, t_2 + \Delta t, \dots, t_N + \Delta t).$$

$$f_X(x_1, x_2, x_3, \dots, x_N; t_1, t_2, \dots, t_N) \in \Delta t.$$

for all $t_1, t_2, t_3, \dots, t_N$

Ex A random process $y(t)$ is given as $y(t) = x(t) \cos(\omega t + \theta)$, where $x(t)$ is a wss, ω is a constant & θ is a random phase independent of $x(t)$, uniformly distributed on $(-\pi, \pi)$. Find (a) $E[y(t)]$

sol for uniformly distributed $f_\theta(\theta) = \begin{cases} \frac{1}{2\pi} & -\pi < \theta \\ 0 & \text{else} \end{cases}$

(a) $E[y(t)] = \int_{-\pi}^{\pi} E[x(t) \cos(\omega t + \theta)]$
 $x(t) \& \cos(\omega t + \theta) \text{ are independent so}$

$$\begin{aligned} &= E[x(t)] E[\cos(\omega t + \theta)] \\ &= E[x(t)] \int_{-\pi}^{\pi} (\cos(\omega t + \theta)) f_\theta(\theta) d\theta \\ &= E[x(t)] \int_{-\pi}^{\pi} \cos(\omega t + \theta) \frac{1}{2\pi} d\theta \\ &= E[x(t)] \frac{1}{2\pi} \left[\sin(\omega t + \theta) \right]_{-\pi}^{\pi} \\ &= E[x(t)] \frac{1}{2\pi} \left[\sin(\omega t + \pi) - \sin(\omega t - \pi) \right] \\ &= E[x(t)] \frac{1}{2\pi} \left[-\sin \omega t + \sin \omega t \right] \\ &= E[x(t)] \frac{1}{2\pi} (0) \end{aligned}$$

$$E[y(t)] = 0$$

(b) $R_{yy}(t) = E[y(t) y(t+\tau)]$
 $= E[x(t) x(t+\tau)] E[\cos(\omega t + \theta) \cos(\omega t + \omega\tau + \theta)]$
 ~~$= \frac{1}{2} R_{xx}(t) \cos(\omega\tau)$~~ $+ [0 + \cos \omega \tau]$
 $R_{yy}(t) = \frac{1}{2} R_{xx}(t) \cos \omega \tau$

- * Time Average of Random process :-
Time average function:- Let $x(t)$ be a sample function which exist for all time t at a fixed value in the given sample space S . A fixed value in the given sample space S is called the time average value of $x(t)$ taken over all time is called the time average of $x(t)$: it is also called mean value of $x(t)$.

Expressed as $\bar{x} = A[x(t)] = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T x(t) dt$

\Rightarrow Time autocorrelation function :-

Consider a random process $x(t)$. The time average of the product $x(t) \& x(t+\tau)$ is called the autocorrelation function of $x(t)$ and is denoted as.

$$R_{xx}(\tau) = A[x(t) x(t+\tau)]$$

$$(ii) R_{xx}(\tau) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T x(t) x(t+\tau) dt$$

τ is time difference of time shift int.

\Rightarrow Time mean square function :-

If $\tau = 0$, the time average of value of $x(t)$. It is denoted as $x^2(t)$ is called the mean square

$$A[x^2(t)] = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T x^2(t) dt.$$

\Rightarrow Time cross correlation function :- Let $x(t)$ & $y(t)$ be two random processes with sample functions $x(t)$ & $y(t)$ respectively. The time average of the product of $x(t) \& y(t+\tau)$ is called time cross correlation function if $x(t) \& y(t)$ is denoted as

$$R_{xy}(\tau) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T x(t) y(t+\tau) dt.$$

Note:- The ensemble averages & time averages are not always same.
 1. $E[A[x(t)]] = E[x(t)] = \bar{x}$ 3. $E[R_{xy}(\tau)] = R_{xy}(\tau)$
 2. $E[R_{xx}(\tau)] = R_{xx}(\tau)$

* Ergodic theorem (or) Ergodic processes

It states that for any random variable process $x(t)$, all the time averages of the sample function $x(t)$ are equal to the corresponding statistical or Ensemble averages of $x(t)$

$$\text{i.e. } \bar{x} = \overline{\bar{x}}$$

$$R_{xx}(T) = R_{\bar{x}\bar{x}}(T)$$

Ergodic process :- Random process that satisfy the Ergodic theorem are called Ergodic processes. Analysis of Ergodicity is extremely complex. In most physical apps, it is assumed that all stationary processes are ergodic processes.

1. Joint Ergodic processes

Let $x(t), y(t)$ - R.P. with sample function $x(t) \in y(t)$. respectively. Then the two R.P. jointly called jointly Ergodic process if they are individually Ergodic. & their time cross correlation functions are equal to their respective Ensemble cross correlation functions, that is

$$1. \bar{x} = \overline{\bar{x}} \quad 3. R_{xx}(T) = R_{\bar{x}\bar{x}}(T)$$

$$2. \bar{y} = \overline{\bar{y}} \quad 4. R_{xy}(T) = R_{\bar{x}\bar{y}}(T)$$

$$5. R_{yy}(T) = R_{\bar{y}\bar{y}}(T).$$

2. Maximal Ergodic process

$$E[x(t)] = \bar{x} = A[x(t)] = \bar{x}$$

3. Auto correlation Ergodic process

$$A[x(t) x(t+\tau)] = E[x(t) x(t+\tau)]$$

$$(on) R_{xx}(T) = R_{\bar{x}\bar{x}}(T)$$

4. Cross correlation Ergodic process

$$A[x(t) y(t+\tau)] = E[x(t) y(t+\tau)]$$

$$R_{xy}(T) = R_{\bar{x}\bar{y}}(T).$$

* Properties of Autocorrelation functions.

Consider $x(t)$ is WSS.

ACF $R_{xx}(t, t+T) \quad T = t_2 - t_1$

(ii)

1. Mean square value of $x(t)$

$$E[x^2(t)] = R_{xx}(0)$$

it is equal to the power of the process $x(t)$

Proof:- $R_{xx}(\tau) = E[x(t)x(t+\tau)]$

If $\tau = 0$

$$R_{xx}(0) = E[x^2(t)]$$

Autocorrelation function is maximum at the origin i.e.,

2. Autocorrelation function is $|R_{xx}(\tau)| \leq R_{xx}(0)$

Proof:- Let $x(t_1), x(t_2)$ are two R.V of R.P. defined at t_1 & t_2

$$[x(t_1) \pm x(t_2)]^2 \geq 0$$

Consider a tve quantity \therefore take expected value ~~cancel~~

$$E[x(t_1) \pm x(t_2)]^2 \geq 0$$

$$E[x^2(t_1) + x^2(t_2) \pm 2x(t_1)x(t_2)] \geq 0$$

$$E[x^2(t_1)] + E[x^2(t_2)] \pm 2E[x(t_1)x(t_2)] \geq 0$$

$$E[x^2(t_1)] + E[x^2(t_2)] + 2R_{xx}(t_1, t_2) \geq 0$$

$$R_{xx}(0) + R_{xx}(0) + 2R_{xx}(t_1, t_1 + \tau) \geq 0 \quad \tau = t_2 - t_1$$

$$2R_{xx}(0) + 2R_{xx}(\tau) \geq 0$$

$$2R_{xx}(0) \geq 2R_{xx}(\tau) \geq 0$$

$$2R_{xx}(0) \geq 2R_{xx}(\tau)$$

$$R_{xx}(0) \geq R_{xx}(\tau) //$$

3. $R_{xx}(\tau)$ is an even function of τ i.e.

$$R_{xx}(-\tau) = R_{xx}(\tau)$$

Proof $R_{xx}(\tau) = E[x(t) \cdot x(t+\tau)]$

let $\tau = -\tau'$

$$R_{xx}(-\tau) = E[x(t) \cdot x(t-\tau')]$$

let $u = t - \tau'$

$$R_{xx}(-\tau) = E[x(u+\tau) \cdot x(u)]$$

$$R_{xx}(-\tau) = R_{xx}(\tau)$$

4. If a R.P $x(t)$ has a non-zero mean value, $E[x(t)] \neq 0$ & ergodic with no periodic components, then

let $R_{xx}(\tau) = \overline{x^2}$
 $|\tau| \rightarrow \infty$

Proof $R_{xx}(\tau) = E[x(t) \cdot x(t+\tau)] = E[x(t_1) \cdot x(t_2)]$

Since process has no periodic components as $t_1 \rightarrow \infty$, the independent \therefore that is

R.V become independent \therefore that is

let $R_{xx}(\tau) = E[x(t_1)] E[x(t_2)]$
 $|\tau| \rightarrow \infty$ $x(t_1)$ is ergodic $\therefore E[x(t_1)] = E[x(t_2)] = \bar{x}$

let $R_{xx}(\tau) = E[x(t)^2] = \bar{x}^2$
 $|\tau| \rightarrow \infty$

if $x(t)$ is periodic, then its autocorrelation function is also periodic
 $x(t)$ with periodic

5. If $x(t)$ is periodic, then its autocorrelation function is also periodic

$$x(t) = x(t \pm T_0)$$

$$x(t \pm T) = x(t + T \pm T_0)$$

$$R_{xx}(\tau) = E[x(t) \cdot x(t+\tau)]$$

$$R_{xx}(\tau \pm T_0) = E[x(t) \cdot x(t+\tau \pm T_0)]$$

$$x(t)$$
 is wss then

$$R_{xx}(\tau \pm T_0) = E[x(t) \cdot x(t+\tau)]$$

$$R_{xx}(\tau \pm T_0) = R_{xx}(\tau)$$

$R_{xx}(\tau)$ is periodic

7. The autocorrelation function of a random process $R_{XX}(T)$ -
cannot have any arbitrary shape.

(18)

Proof $R_{XX}(T)$ is even function of T & Max value is at origin
is also related to PSD through F.T. The spectrum is not arbitrary
arbitrary shape.

Hence $R_{XX}(T)$ also cannot have the DC components

8. If a random process $x(t)$ with zero mean has the DC components
A as $y(t) = A + x(t)$. Then $R_{YY}(T) = A^2 + R_{XX}(T)$.

9. If the random process $z(t)$ is a sum of two random processes
 $x(t) \in y(t)$, then

$$z(t) = x(t) + y(t)$$

$$\text{Then } R_{ZZ}(T) = R_{XX}(T) + R_{XY}(T) + R_{YX}(T) + R_{YY}(T)$$

Properties of CCF

Consider $x(t) \in y(t)$ are two R.P are Jointly WSS.

The CCF $R_{XY}(t, t+T)$ is function of only $\tau = t_2 - t_1$ then

the following properties are

1. $R_{XY}(T) = R_{YX}(-T)$ is a symmetry property

1. $R_{XY}(T) = R_{YX}(-T)$ is a symmetry property

2. If $R_{XX}(T) \in R_{YY}(T)$ are the autocorrelation functions of

$x(t) \in y(t)$ respectively then CCF satisfies the inequality

$$|R_{XY}(T)| \leq \sqrt{R_{XX}(0) R_{YY}(0)}$$

3. If $x(t) \in y(t)$ are two random processes with ACF $R_{XX}(T)$
and $R_{YY}(T)$ then the cross correlation function satisfies the

$$\text{inequality } |R_{XY}(T)| \leq \frac{1}{2} [R_{XX}(0) + R_{YY}(0)]$$

4. If two random processes $X(t)$ & $Y(t)$ are statistically independent (i) and are atleast wide sense stationary

$$R_{XY}(T) = \bar{X} \bar{Y}$$

5. If the two random processes $X(t)$ & $Y(t)$ have zero mean & are
widely wss. Then $\lim_{T \rightarrow R} R_{XY}(T) = 0$

* Covariance Functions for Random Processes :-

1. Autocovariance Function :-

The autocovariance function is a measure of interdependence b/w two random variables. The same concept of random variables can be extended to random processes.

Consider random process $x(t), x(t+T)$ at two time intervals t and $t+T$. The autocovariance is defined and can be expressed as

$$C_{xx}(t, t+T) = E[(x(t) - E[x(t)]) \cdot (x(t+T) - E[x(t+T)])]$$

$$(a) C_{xx}(t, t+T) = R_{xx}(t, t+T) - E[x(t)] E[x(t+T)]$$

(@) If $x(t)$ is atleast a wide sense stationary random process,
then $C_{xx}(T) = R_{xx}(T) - \bar{x}^2$
The autocovariance function is not a function of absolute time.

(b) At $T=0$ $C_{xx}(0) = R_{xx}(0) - \bar{x}^2 = E[x^2] - \bar{x}^2 = \sigma_x^2$
∴ at $T=0$ the autocovariance function becomes the variance of the random process i.e. $\sigma_x^2 = C_{xx}(0)$.

(c) The A.C. Coeff. of the random process $x(t)$ is defined as

$$\rho_{xx}(t, t+T) = \frac{C_{xx}(t, t+T)}{\sqrt{C_{xx}(t, t) C_{xx}(t+T, t+T)}}$$

$$\text{if } T=0 \quad \rho_{xx}(0) = \frac{C_{xx}(0)}{C_{xx}(0)} = 1$$

$$\text{Also } |\rho_{xx}(t, t+T)| \leq 1.$$

(15)

Cross covariance Function

If two random processes $X(t)$ & $Y(t)$ have random variables at $x(t) \in Y(t+T)$, then the cross covariance function is defined as

$$C_{XY}(t, t+T) = E[(X(t) - E[X(t)]) (Y(t+T) - E[Y(t+T)])]$$

$$(d) C_{XY}(t, t+T) = R_{XY}(t, t+T) - E[X(t)]E[Y(t+T)]$$

1. If the random processes are atleast jointly wss, then

$$C_{XY}(\tau) = R_{XY}(\tau) - \bar{X}\bar{Y}$$

The cross covariance function is not a function of absolute time t .

The cross covariance function is not a function of absolute time t .

2. If two random processes $X(t)$ & $Y(t)$ are uncorrelated, then

$$C_{XY}(t, t+T) = 0$$

$$\text{or } R_{XY}(t, t+T) = E[X(t)]E[Y(t+T)]$$

This is the condition for two random processes to be statistically independent. Therefore, the independent random processes are uncorrelated.

But the converse is not always true.

3. The cross correlation Co-Eff of the random processes $X(t)$ and $Y(t)$ is defined as

$$\rho_{XY}(t, t+T) = \frac{C_{XY}(t, t+T)}{\sqrt{C_{XX}(t, t)C_{YY}(t+T, t+T)}}$$

$$\text{if } \tau=0 \quad \rho_{XY}^{(0)} = \frac{C_{XY}^{(0)}}{\sigma_X \sigma_Y}$$

Eg A random process is given as $x(t) = At$ where A is an uniformly distributed random variable on $(0, 2)$ find whether it is WSS or not. (16)

Sol: The condition for WSS is

$E[x(t)] = \bar{x} = \text{constant}$
and $R_{xx}(T)$ is independent of time t .

Given $x(t) = At$

$$\text{and } f_A(A) = \begin{cases} \frac{1}{2} & \cdot 0 \leq A \leq 2 \\ 0 & \text{otherwise} \end{cases}$$

(a) $E[x(t)]$

$$\begin{aligned} E[x(t)] &= \int_{-\infty}^{\infty} x(t) f_A(A) dA \\ &= \int_0^2 \frac{1}{2} At dA \\ &= \frac{t}{2} \left[\frac{A^2}{2} \right]_0^2 \\ &= \frac{t}{2} \left[\frac{4t^2 - 0}{2} \right] \end{aligned}$$

$$E[x(t)] = t$$

(b) $R_{xx}(T) = E[x(t)x(t+T)]$

$$\begin{aligned} &= E[At \cdot A(t+T)] \\ &= E(t+t+T) E[A^2] \\ &= E(t+t+T) \cdot \int_0^2 \frac{A^2}{2} dA \\ &= t(t+T) \left[\frac{A^3}{8} \right]_0^2 \\ &= t(t+T) [8-0] \end{aligned}$$

$$R_{xx}(T) = \frac{4}{3} t(t+T)$$

Hence mean value is not constant

and $R_{xx}(T)$ is a function of t .

$x(t)$ is not a WSS.

Ex2

$$x(t) = A, (0, 1)$$

$$\begin{aligned} E[x(t)] &= \int_0^1 A \cdot 1 dA \\ &= \frac{A^2}{2} \Big|_0^1 = \frac{1}{2} \end{aligned}$$

$\therefore x(t)$ is WSS

$$R_{xx}(T) = E[x(t)x(t+T)]$$

$$= E \left[\int_0^1 A \cdot A(t+T) dA \right] \cancel{f_A(A)}$$

$$= E[A \cdot A] = \frac{E[A^3]}{E[A^3]}$$

$$\begin{aligned} &= E[A^2] \\ &= \frac{A^3}{3} \Big|_0^1 = \frac{1}{3} \end{aligned}$$

$R_{xx}(T)$ is independent of time

Expt If a random process, $x(t) = A \cos \omega t + B \sin \omega t$ is given, where A & B are uncorrelated, zero mean random variables having the variance σ^2 . Find (a) Auto correlation & (b) show that $x(t)$ is WSS.

Given $x(t) = A \cos \omega t + B \sin \omega t$
~~A & B are uncorrelated so~~
 $E[AB] = E[A]E[B] = 0$
 $\sigma_A^2 = E[A^2], \sigma_B^2 = E[B^2]$

(a) Auto correlation function

$$\begin{aligned}
 R_{XX}(\tau) &= E[x(t)x(t+\tau)] \\
 &= E[(A \cos \omega t + B \sin \omega t)(A \cos \omega(t+\tau) + B \sin \omega(t+\tau))] \\
 &= E[A^2 \cos \omega t \cos \omega(t+\tau) + AB \cos \omega t \sin \omega(t+\tau) + AB \sin \omega t \cos \omega(t+\tau) \\
 &\quad + B^2 \sin \omega t \sin \omega(t+\tau)] \\
 &= E[\cancel{A^2}] E[\cos \omega t \cos \omega(t+\tau)] + E[\cancel{AB}] E[\cos \omega t \cos \omega(t+\tau)] \\
 &\quad + E[\cancel{AB}] E[\sin \omega t \sin \omega(t+\tau)] + E[B^2] E[\sin \omega t \sin \omega(t+\tau)] \\
 &= \cancel{\sigma_A^2} + \sigma^2 E[\cos \omega t \cos \omega(t+\tau)] + 0 + \cancel{\sigma_B^2} E[\sin \omega t \sin \omega(t+\tau)] \\
 &= \sigma^2 [E[\cos \omega t \cos \omega(t+\tau)] + E[\sin \omega t \sin \omega(t+\tau)]] \\
 &= \sigma^2 E[\cos(\omega t + \omega\tau - \omega t)] \\
 &= \sigma^2 E[\cos(\omega\tau)]
 \end{aligned}$$

$$\therefore R_{XX}(\tau) = \sigma^2 \cos \omega\tau$$

$$\begin{aligned}
 (b) \text{ The mean value } E[x(t)] &= E[A \cos \omega t + B \sin \omega t] \\
 &= E[A \cos \omega t] + E[B \sin \omega t] \\
 &= E[A] \cos \omega t + E[B] \sin \omega t \\
 E[x(t)] &= 0 \text{ constant & the ACF.}
 \end{aligned}$$

$$R_{XX}(\tau) = \sigma^2 \cos \omega\tau \text{ is independent of time } t.$$

Hence the random process is WSS.

(18)

Gaussian Random processes

Consider a continuous random process $x(t)$. Let N random variables $X_1 = x(t_1), X_2 = x(t_2), \dots, X_N = x(t_N)$ be defined at time instants $t_1, t_2, t_3, \dots, t_N$ respectively.

If these random variables are jointly Gaussian for any $N = 1, 2, \dots$ and at anytime instants t_1, t_2, \dots, t_N , then the random process $x(t)$ is called a Gaussian random process. The joint density function for n Gaussian random variable is given as.

$$f_x(x_1, x_2, \dots, x_N | t_1, t_2, \dots, t_N) = \frac{\exp\left\{-\frac{1}{2}(x - \bar{x})^T C_{xx}^{-1}(x - \bar{x})\right\}}{\sqrt{(2\pi)^N |C_{xx}|}}$$

$$\text{where } \bar{x} = E[x_i] = E[x(t)]$$

$[C_{xx}]$ = Covariance matrix and its elements are

$$C_{ik} = (x_i x_k) = E[(x_i - \bar{x}_i)(x_k - \bar{x}_k)]$$

$$= E[x(t_i) - \bar{x}(t_i)(x(t_k) - \bar{x}(t_k))]$$

$C_{ik} = C_{xx}(t_i, t_k)$
 C_{ik} is the autocovariance of $x(t_i) \in x(t_k)$. Also by expanding

the above eqn, we can get
 $C_{xx}(t_i, t_k) = R_{xx}(t_i, t_k) - E[x(t_i)] \cdot E[x(t_k)].$

$C_{xx}(t_i, t_k)$ is the autocorrelation function of x .

where $R_{xx}(t_i, t_k)$ is the autocorrelation function of x ,

If the process is WSS, then it should satisfy the following conditions.

Condition 1: Mean value will be constant, i.e.,

$$\bar{x}_i = E[x(t_i)] = \bar{x} \text{ a constant}$$

(2) The mean autocorrelation & covariance functions will depend only on time difference and not on absolute time.

$$C_{xx}(t_i, t_k) = C_{xx}(t_k - t_i)$$

$$R_{xx}(t_i, t_k) = R_{xx}(t_k - t_i)$$

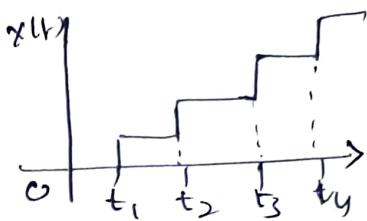
Poisson Random Processes

The poisson random process $X(t)$ is a discrete random process which represents the number of time that some event has occurred as a function of time. $X(t)$ has integer valued, non-decreasing sample functions, such as check-in (eg. arrivals), arrival of a customer, arrival of vehicles at a particular point etc.

A single event occurs at a random time.

Counting the number of occurrences with time is a poisson process. also called counting process.

The conditions for a poisson process $X(t)$ are



A poisson counting process.

1. $X(0) = 0$
2. Only one event occurs in any instant of time, i.e., in an infinitesimal time interval.
3. The number of events that occurs in any given time interval is independent of the number of events in any other non-overlapping time intervals i.e., $X(t)$ has independent increments.

Probability density function :- If the number of occurrences of an event in any finite interval of time, is described by a poisson distribution with the average rate of occurrences is λ , then the probability of exactly K occurrences over a time interval (t_0, t) is

$$P[X(t) = k] = \frac{(\lambda t)^k e^{-\lambda t}}{k!}, \quad k=0, 1, 2, \dots$$

E PDF $f_X(x) = \sum_{k=0}^{\infty} \frac{(\lambda t)^k e^{-\lambda t}}{k!} \delta(x-k)$

Mean value :- $E[X(t)] = \int_{-\infty}^{\infty} x f_X(x) dx = \int_{-\infty}^{\infty} x \sum_{k=0}^{\infty} \frac{(\lambda t)^k e^{-\lambda t}}{k!} \delta(x-k) dx$

Since $\int_{-\infty}^{\infty} x \delta(x-k) dx = k$

From poisson density function of a random variable that the mean

value is λt So $E[X(t)] = \lambda t$

$$E[X(t)] = \sum_{k=0}^{\infty} \frac{(k \lambda t)^k e^{-\lambda t}}{k!} = \lambda t$$

Second moment

(20)

The second moment is

$$E[X^2(t)] = \int_{-\infty}^{\infty} x^2 f_X(x) dx$$

$$\int_{-\infty}^{\infty} x^2 \sum_{k=0}^{\infty} \frac{(\lambda t)^k e^{-\lambda t}}{k!} g(x-k) dx$$

Since $\int_{-\infty}^{\infty} x^2 g(x-k) dx = k^2$

$$E[X^2(t)] = \sum_{k=0}^{\infty} \frac{k^2 (\lambda t)^k e^{-\lambda t}}{k!}$$

But we know that the second moment is

$$E[X^2] = \bar{x}^2 + \sigma_x^2$$

$$= \lambda t + (\lambda t)^2 = \lambda t + \lambda^2 t^2$$

$$E[X^2(t)] = \sum_{k=0}^{\infty} \frac{k^2 (\lambda t)^k e^{-\lambda t}}{k!} = \lambda t + \lambda^2 t^2.$$

Ex Given $\bar{x} = 6$ & $R_{XX}(t, t+T) = 36 + 25 \exp(-T)$ for a random process $x(t)$. Indicate which of the following statements are true based on what is known, with certainty: $x(t)$.

- (a) First order stationary
- (b) Has total average power of 61W
- (c) is Ergodic
- (d) is WSS
- (e) Has a periodic component
- (f) has an AC power of 36W

Q Given - the random process $\bar{x} = 6$
 $R_{XX}(t, t+T) = 36 + 25 \exp(-T)$.

Given - the random process $\bar{x} = 6$ constant & $R_{XX}(t, t+T) = 36 + 25 \exp(-T)$ is independent of t .

- (a) $\bar{x} = 6$ constant & $R_{XX}(t, t+T) = 36 + 25 \exp(-T)$ is independent of t .
- (b) $x(t)$ is first order stationary process

(b) Total average power is $P_{avg} = R_{xx}(0)$

$$P_{avg} = 36 + 25 \exp(-7) = 36 + 25 \exp(0) \\ = 36 + 25 \\ = 61 \text{ W.}$$

\therefore Avg power = 61 W

(c) If $x(t)$ is Ergodic process all its Ensemble averages are equal to time averages.

$$\therefore A[x(t)] = \bar{x} = 6$$

$$E[A[R_{xx}(t, t+T)]] = R_{xx}(t, t+T) = 36 + 25 e^{-|T|}$$

\therefore process is Ergodic.

(d) WSS - Conditions are $\bar{x} = \text{constant}$
 $R_{xx}(t, t+T)$ is independent of t .

Mean $\bar{x} = 6$ constant

$R_{xx}(t, t+T) \neq 36 + 25 \exp(-T)$ independent of t hence

$x(t)$ is WSS

(e) The process $\because \lim_{T \rightarrow \infty} R_{xx}(t, t+T) = E[x]^2$ if no periodic components

$$\lim_{T \rightarrow \infty} R_{xx}(t, t+T) = 36 + 25 e^{-|T|} = 36$$

$$= 36 + 0 = 36$$

$$\therefore E[x^2] = 36.$$

\therefore The process has no periodic components.

The AC power of the process is the Variance of $x(t)$

$$\sigma_x^2 = E[x(t)^2] - E[x(t)]^2$$

$$E[x(t)^2] = R_{xx}(t, t+T)|_{T=0} = R_{xx}(0) = 61$$

$$\therefore \sigma_x^2 = 61 - 6^2 = 61 - 36 = 25$$

AC power is 25 watts

Ex - A stationary process has an autocorrelation function given by

$$R(\tau) = \frac{25\tau^2 + 36}{6.25\tau^2 + 4} \quad \text{Find mean value, mean square value}$$

(2e)

Variance of the process

Given $R(\tau) = \frac{25\tau^2 + 36}{6.25\tau^2 + 4}$

(a) The mean value is

$$\bar{x}^2 = \lim_{T \rightarrow \infty} R(\tau)$$

$$\begin{aligned} E[x(t)]^2 &= \lim_{T \rightarrow \infty} \frac{25\tau^2 + 36}{6.25\tau^2 + 4} \\ &= \lim_{T \rightarrow \infty} \frac{\cancel{T} \left[25 + \frac{36}{T^2} \right]}{\cancel{T} \left[6.25 + \frac{4}{T^2} \right]} = \frac{25}{6.25} \\ &= \frac{2500}{625} = 4. \end{aligned}$$

$$\bar{x}^2 = 4$$

$$\bar{x} = 2$$

(b) Mean square value

$$\begin{aligned} E[x^2] &= \lim_{T \rightarrow \infty} R(\tau) \Big|_{\tau=0} \\ &= \lim_{T \rightarrow \infty} \frac{25\tau^2 + 36}{6.25\tau^2 + 4} \Big|_{\tau=0} \end{aligned}$$

$$E[x^2] = \frac{36}{4} = 9$$

$$\boxed{E[x^2] = 9}$$

$$\begin{aligned} (c) \text{ Variance } \sigma_x^2 &= E[x^2] - \bar{x}^2 \\ &= 9 - 4 \\ &= 5 \end{aligned}$$

Ex - Assume that an ergodic process $x(t)$ has an autocorrelation function

$$R_{xy}(\tau) = 18 + \frac{2}{6+\tau^2} (1+4\cos(2\tau))$$

(a) Find \bar{x}

$$\bar{x}^2 = \lim_{T \rightarrow \infty} R_{xx}(\tau)$$

$$= \lim_{T \rightarrow \infty} 18 + \frac{2}{6+\tau^2} (1+4\cos(2\tau))$$

$$\bar{x}^2 = 18$$

$$\bar{x} = 4.2426$$

(b) Average power of $x(t)$ is

$$\begin{aligned} E[x^2] &= R_{xx}(0) \\ &= 18 + \frac{2}{6+0} (1+4\cos 0) = 18 + \frac{10}{6} = 19.667 \end{aligned}$$

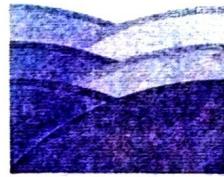
(b) For a periodic component

$$\lim_{T \rightarrow \infty} R_{xx}(\tau) = \lim_{T \rightarrow \infty} \left(18 + \frac{2}{6+\tau^2} \right)$$

$$\begin{aligned} &= E[x^2] \\ &= R(\tau) \Big|_{\tau=0} \\ &= (18 + \frac{2}{6}) (1+4\cos 0) \\ &= \infty \end{aligned}$$

So the process has a periodic component.

A40401- SIGNALS, SYSTEMS AND STOCHASTIC PROCESSES



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UNIT - IV
Stochastic processes - Spectral characteristics

Introduction :- Consider a random process $x(t)$. The amplitude of the random process, when it varies randomly with time; doesn't satisfy the strict conditions. Therefore it is not possible to apply FT directly on the random process for a frequency domain analysis. Thus, the ACF of WSS RP is used to study spectral characteristics such as power spectral density or power density spectrum.

Definition of Power Spectrum Density :-

① The PSD of a WSS random process $x(t)$ is defined as the Fourier Transform of the autocorrelation $R_{xx}(\tau)$ of $x(t)$ can be expressed as

$$S_{xx}(w) = \int_{-\infty}^{\infty} R_{xx}(\tau) e^{jw\tau} d\tau.$$

We can obtain $R_{xx}(\tau)$ from $S_{xx}(w)$ by taking IFT.

$$R_{xx}(\tau) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(w) e^{-jw\tau} dw$$

∴ PSD $S_{xx}(w) \propto R_{xx}(\tau)$ are Fourier Transform Pairs.

② The PSD can also be defined as

$$S_{xx}(w) = \lim_{T \rightarrow \infty} \frac{E[X_T(w)]^2}{2T}$$

where $X_T(w)$ = Fourier Transform of $x(t)$ in the interval $[-T, T]$

Average power of the random process :-

The average power P_{xx} of a WSS random process $x(t)$ is defined as the time average of its second moment / autocorrelation function at $\tau=0$

Mathematically

$$P_{xx} = E \{ X^2(t) \}$$

$$R_{xx} = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^{T} E [X^2(t)] dt$$

$$\text{OR } R_{xx} = R_{xx}(0) \Big|_{\tau=0}$$

$$\text{we know that } R_{XX}(T) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^{j\omega T} d\omega$$

At $T=0$

$$P_{XX} = R_{XX}(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^0 d\omega$$

Average Power

$$P_{XX} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) d\omega.$$

Proof: Let us consider a WSS random process $x(t)$. To obtain FT of $x_T(t)$ let $x_T(t)$ be defined in the interval $[-T, T]$

$$x_T(t) = \begin{cases} x(t) & -T < t < T \\ 0 & \text{otherwise} \end{cases}$$

$$\text{FT of } x_T(t) = X_T(\omega) = \int_{-\infty}^{\infty} x_T(t) e^{-j\omega t} dt = \int_{-T}^{+T} x(t) e^{-j\omega t} dt$$

Now from Parseval's theorem; the energy contained in $x_T(t)$ is

$$\text{Energy} = \int_{-T}^{+T} x_T^2(t) dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X_T(\omega)|^2 d\omega.$$

The average power over the interval $[-T, T]$ is

$$P(T) = \frac{1}{2T} [\text{Energy}] = \frac{1}{2T} \int_{-T}^{+T} (x_T^2(t)) dt = \frac{1}{2T} \frac{1}{2\pi} \int_{-\infty}^{\infty} |X_T(\omega)|^2 d\omega$$

$$P(T) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{|X_T(\omega)|^2}{2T} d\omega$$

The average power of the random process $x(t)$ in the entire time interval $-\infty < t < \infty$ is equal to the mean value of $P(T)$ as $T \rightarrow \infty$

$$P_{XX} = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^{+T} E[x^2(t)] dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{dt}{t \rightarrow \infty} \frac{E[(X_T(\omega))^2]}{2T} d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{dt}{t \rightarrow \infty} \int_{-T}^{+T} \frac{E[(X_T(\omega))^2]}{2T} d\omega d\omega$$

$$P_{XX} = A \left\{ \int_{-\infty}^{\infty} E[x^2(t)] dt \right\},$$

Thus the average power P_{XX} is the time average of its second moment

$$\text{Also } P_{XX} = \frac{1}{2\pi} \int_{-\infty}^{\infty} dt \underset{T \rightarrow \infty}{\lim} \frac{E[(X_T(\omega))^2]}{2T} d\omega$$

If power spectral density is defined as

$$S_{XX}(\omega) = \underset{T \rightarrow \infty}{\lim} \frac{E[(X_T(\omega))^2]}{2T}$$

$$P_{XX} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) d\omega$$

$$\therefore P_{XX} = R_{XX}(0)$$

$\therefore P_{XX} = R_{XX}(0)$ at the origin.

The average power is autocorrelation of $x(t)$

Properties of PSD :-

The properties of WSS random process are

1. $S_{XX}(\omega) \geq 0$ - Always non negative

From definition $S_{XX}(\omega) = \underset{T \rightarrow \infty}{\lim} \frac{E[(X_T(\omega))^2]}{2T}$ is always expected value of a non negative function $E[(X_T(\omega))^2]$ is always a non negative hence $S_{XX}(\omega) \geq 0$.

2. The PSD at zero frequency is equal to the area under the curve of the autocorrelation $R_{XX}(r)$.

$$R_{XX}(0) = \int_{-\infty}^{\infty} R_{XX}(r) dr$$

$$\text{Proof: } S_{XX}(\omega) = \int_{-\infty}^{\infty} R_{XX}(r) e^{j\omega r} dr$$

$$\text{At } \omega=0 \quad S_{XX}(0) = \int_{-\infty}^{\infty} R_{XX}(r) e^0 dr = \int_{-\infty}^{\infty} R_{XX}(r) dr$$

3. The PSD of a real process $x(t)$ is real

$$S_{XX}(\omega) = S_{XX}(-\omega) \quad x(t) \text{ is real}$$

$$\text{Proof: } S_{XX}(\omega) = \int_{-\infty}^{\infty} R_{XX}(r) e^{j\omega r} dr$$

$$S_{XX}(-\omega) = \int_{-\infty}^{\infty} R_{XX}(r) e^{-j\omega r} dr$$

$$\text{sub } \gamma = -\tau$$

$$S_{XX}(-\omega) = \int_{-\infty}^{\infty} R_{XX}(-\tau) e^{-j\omega\tau} d\tau$$

$x(t)$ is real, from properties of ACF we know that

$$R_{XX}(\gamma) = R_{XX}(-\gamma)$$

$$\text{So } S_{XX}(-\omega) = \int_{-\infty}^{\infty} R_{XX}(\gamma) e^{-j\omega\gamma} d\gamma$$

$$\therefore S_{XX}(\omega) = S_{XX}(-\omega).$$

$\therefore S_{XX}(\omega)$ is always a real function

4. $S_{XX}(\omega)$ is always a real function

$$\text{proof: } S_{XX}(\omega) = \lim_{T \rightarrow \infty} \frac{E[X_T(\omega)]^2}{2T}$$

$|X_T(\omega)|^2$ is always real function hence $S_{XX}(\omega)$ also always real.

5. If $S_{XX}(\omega)$ is a psd of wss random process $x(t)$ then

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) d\omega = A \left\{ E[X^2(t)] \right\} = R_{XX}(0)$$

(d)
Time average of the mean square value of a wss RP equal the area under the curve of the psd.

$$\text{proof: } R_{XX}(\gamma) = A \left\{ E[(x(t+\gamma))x(t)] \right\}$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^{j\omega\gamma} d\omega$$

Now at $\gamma = 0$

$$R_{XX}(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^{j\omega 0} d\omega$$

$$R_{XX}(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) d\omega = \text{Area under the curve of } S_{XX}(\omega),$$

6. If $x(t)$ is a WSS random process with PSD $S_{xx}(w)$. Then the PSD of the derivative of $x(t)$ is equal to ω^2 times of the PSD $S_{xx}(w)$

$$S_{\dot{x}x}(w) = \omega^2 S_{xx}(w)$$

Proof :- $S_{xx}(w) = \lim_{T \rightarrow \infty} \frac{E[(X_T(w))^2]}{2T}$

$$S_{\dot{x}x}(w) = \lim_{T \rightarrow \infty} \frac{E[(\dot{X}_T(w))^2]}{2T}$$

$$= \lim_{T \rightarrow \infty} \frac{E[((-jw) X_T(w))^2]}{2T}$$

$$= \lim_{T \rightarrow \infty} \frac{\omega^2 E[(X_T(w))^2]}{2T}$$

$$= \omega^2 \lim_{T \rightarrow \infty} \frac{E[(X_T(w))^2]}{2T}$$

$$\therefore X_T(w) = \int_{-T}^T x(t) e^{-j\omega t} dt$$

$$\dot{X}_T(w) = \frac{d}{dt} X_T(w) = \frac{d}{dw} \int_{-T}^T x(t) e^{-j\omega t} dt$$

$$= \int_{-T}^T x(t) \frac{d}{dw} e^{-j\omega t} dt$$

$$= \int_{-T}^T x(t) (-j\omega) e^{-j\omega t} dt$$

$$= (-j\omega) \int_{-T}^T x(t) e^{-j\omega t} dt$$

$$\dot{X}_T(w) = (-j\omega) X_T(w)$$

$$S_{\dot{x}x}(w) = \omega^2 S_{xx}(w)$$

The PSD and the time average of the ACF from a Fourier transform pair.

$$S_{xx}(w) = \int_{-\infty}^{\infty} R_{xx}(t) e^{-j\omega t} dt$$

$$R_{xx}(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} B_{xx}(w) e^{j\omega t} dw.$$

Proof :- Consider a WSS random process $x(t)$. The time average of autocorrelation function is

$$A[R_{xx}(t, t+T)] = A \{ E[x(t) \cdot x(t+T)] \}$$

$$\text{For WSS } A[R_{xx}(t, t+T)] = R_{xx}(T)$$

$$\text{PSD } S_{xx}(w) = \lim_{T \rightarrow \infty} \frac{E[(X_T(w))^2]}{2T}$$

$$|X_T(\omega)|^2 = X_T(\omega) X_T^*(\omega)$$

$$X_T(\omega) = \int_{-T}^T x(t_1) e^{j\omega t_1} dt_1$$

$$X_T^*(\omega) = \int_{-T}^T x(t_1) e^{-j\omega t_1} dt_1$$

$$S_{XX}(\omega) = \lim_{T \rightarrow \infty} E \left[\frac{1}{2T} \int_{-T}^T x(t_1) e^{j\omega t_1} dt_1 \int_{-T}^T x(t_2) e^{-j\omega t_2} dt_2 \right]$$

$$S_{XX}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T E[x(t_1)x(t_2)] e^{-j\omega(t_1-t_2)} dt_1 dt_2$$

below $E[x(t_1)x(t_2)] = R_{XX}(t_1, t_2)$

$$S_{XX}(\omega) = \lim_{T \rightarrow \infty} E \left[\frac{1}{2T} \int_{-T}^T x(t_1) e^{j\omega t_1} dt_1 \int_{-T}^T x(t_2) e^{-j\omega t_2} dt_2 \right]$$

$$S_{XX}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T E[x(t_1)x(t_2)] e^{-j\omega(t_1-t_2)} dt_1 dt_2$$

we know $E[x(t_1)x(t_2)] = R_{XX}(t_1, t_2)$

$$S_{XX}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{XX}(t_1, t_2) e^{-j\omega(t_1-t_2)} dt_1 dt_2$$

By taking Fourier transform.

$$\begin{aligned} \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^{j\omega t} d\omega &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{XX}(t_1, t_2) \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} e^{j\omega t_1} e^{-j\omega(t_1-t_2)} dt_1 \right) d\omega dt_2 \\ &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{XX}(t_1, t_2) \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} e^{-j\omega(t_1-t_2)} d\omega \right) dt_1 dt_2 \\ &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{XX}(t_1, t_2) \delta(t_1 - t_2 - T) dt_1 dt_2 \end{aligned}$$

$$\int_{-\infty}^{\infty} e^{-j\omega(t_1-t_2-T)} d\omega = 2\pi \delta(t_1 - t_2 - T)$$

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^{j\omega t} d\omega = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T R_{XX}(t, t+T) \underbrace{\int_{-T}^T \delta(t_1 - t - T) dt_1}_{\stackrel{=1}{\text{let } t_1 = t+T}} dt$$

$$\begin{aligned} \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) e^{j\omega t} d\omega &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T R_{XX}(t, t+T) dt \\ &= A [R_{XX}(t, t+T)] \end{aligned}$$

$$A[R_{xx}(t_1 + t)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(\omega) e^{j\omega t} d\omega$$

Taking RT

$$S_{xx}(\omega) = \int_{-\infty}^{\infty} A[x_x(t, t+T)] e^{-j\omega T} dt$$

$$\text{For wss } R_{xx}(t_1 + T) = R_{xx}(T)$$

$\therefore R_{xx}(T) \& S_{xx}(\omega)$ are a Fourier Transform pair.

Ex:- Determine which of the following functions are valid power spectrum density & why?

$$(a) \frac{\cos(\omega)}{2+\omega^4}$$

$$\text{so that } S_{xx}(\omega) = \frac{\cos(\omega)}{2+\omega^4}$$

$$S_{xx}(-\omega) = \frac{\cos(-\omega)}{2+(-\omega)^4}$$

$$= \frac{\cos \omega}{2+\omega^4}$$

$$S_{xx}(\omega) = S_{xx}(-\omega)$$

and $S_{xx}(\omega)$ is real & even

\therefore Given function is valid PSD

Baseband process RMS bandwidth

$$W_{rms}^2 = \frac{\int_{-\infty}^{\infty} \omega^2 S_{xx}(\omega) d\omega}{\int_{-\infty}^{\infty} S_{xx}(\omega) d\omega}$$

Bandpass process RMS B.W

$$W_{rms}^2 = \frac{4 \int_{-\infty}^{\infty} (\omega - \bar{\omega}_0)^2 S_{xx}(\omega) d\omega}{\int_{-\infty}^{\infty} S_{xx}(\omega) d\omega}$$

Q: If $R_{XX}(T) = a e^{-b|T|}$; $H(w) = \frac{1}{2+jw}$ show that PSD is $\frac{2ab}{b^2+w^2}$

$$\text{Given } R_{XX}(t) = a e^{-b|t|}$$

$$S_{XX}(w) = \int_{-\infty}^{\infty} R_{XX}(t) e^{-jwT} dt$$

$$= \int_{-\infty}^{\infty} a e^{-b|t|} e^{-jwT} dt$$

$$= a \int_{-\infty}^{\infty} e^{-b|t|} e^{-jwT} dt$$

$$= a \left[\int_{-\infty}^0 e^{+(b-jw)T} dt + \int_0^{\infty} e^{-(b+jw)T} dt \right]$$

$$= a \left[\frac{e^{(b-jw)T}}{b-jw} \Big|_{-\infty}^0 + \frac{e^{-(b+jw)T}}{-b-jw} \Big|_0^{\infty} \right]$$

$$= a \left\{ \left[\frac{e^0}{b-jw} - \left(\frac{e^0}{b-jw} \right) \right] + \left[\frac{e^{\infty}}{-b-jw} - \left(\frac{e^0}{-b-jw} \right) \right] \right\}$$

$$= a \left[\left[\frac{1}{b-jw} - 0 \right] + \left[0 + \frac{1}{b+jw} \right] \right]$$

$$= a \left[\frac{(b+jw)+(b-jw)}{b^2-(jw)^2} \right]$$

$$= a \frac{2b}{b^2+w^2}$$

$$S_{XX}(w) = \frac{2ab}{b^2+w^2}$$

Cross power spectral density

* Relation b/w cross correlation power & spectral density & cross correlation function

Let $x(t)$ and $y(t)$ are two random processes $x(t), y(t)$ are sample functions & $x_T(t), y_T(t)$ are truncated portions in the interval $(-T, T)$.

$x_T(w), y_T(w)$ are Fourier Transforms of $x_T(t), y_T(t)$

$$x_T(w) = \int_{-T}^T x(t_1) e^{j\omega t_1} dt_1, \quad y_T(w) = \int_{-T}^T y(t_2) e^{-j\omega t_2} dt_2$$

$$x_T^*(w) = \int_{-T}^T x(t_1) e^{j\omega t_1} dt_1.$$

We know

$$\begin{aligned} S_{xy}(w) &= \lim_{T \rightarrow \infty} \frac{dt}{2T} E[x_T^*(w) x_T(w)] \\ &= \lim_{T \rightarrow \infty} \frac{1}{2T} E \left[\int_{-T}^T x(t_1) e^{j\omega t_1} dt_1 \cdot \int_{-T}^T x(t_2) e^{-j\omega t_2} dt_2 \right] \\ &= \lim_{T \rightarrow \infty} \frac{1}{2T} \left[\int_{-T}^T \int_{-T}^T E[x(t_1) y(t_2)] e^{-j\omega(t_2-t_1)} dt_2 dt_1 \right] \\ &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{xy}(t_1, t_2) e^{-j\omega(t_2-t_1)} dt_2 dt_1 \end{aligned}$$

Taking inverse Fourier Transform

$$\begin{aligned} \text{IFT}[S_{xy}(w)] &= \frac{1}{2\pi} \int_{-\infty}^{\infty} dt \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{xy}(t_1, t_2) e^{-j\omega(t_2-t_1)} dt_2 dt_1 dw \\ &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{xy}(t_1, t_2) \left[\frac{1}{2\pi} \int_{-\infty}^{\infty} e^{-j\omega(t_2-(t_1+T))} dw \right] dt_2 dt_1 \end{aligned}$$

$$\text{IFT} [S_{XY}(w)] = \lim_{T \rightarrow \infty} \frac{1}{2\pi} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} R_{XY}(t_1, t_2) S(t_2 - (t_1 + T)) dt_2 dt_1$$

$$= \lim_{T \rightarrow \infty} \frac{1}{2\pi} \int_{-\pi}^{\pi} R_{XY}(t_1, t_1 + T) dt_1$$

$$\text{IFT} [S_{XX}(w)] = A [R_{XY}(t_1, t_1 + T)] e^{-jwT} dt_1$$

$$S_{XY}(w) = \int_{-\infty}^{\infty} A [R_{XY}(t_1, t_1 + T)] e^{-jwT} dt_1$$

$\therefore S_{XY}(w) \xleftrightarrow{FT} A[R_{YY}(t_1, t_1 + T)]$

$$\text{For WSS } S_{XY}(w) = \int_{-\infty}^{\infty} R_{XY}(T) e^{-jwT} dT.$$

$$R_{XY}(T) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XY}(w) e^{jwT} dw$$

$$\text{II}^{\text{(a)}} \quad S_{YY}(w) = \int_{-\infty}^{\infty} R_{YY}(T) e^{-jwT} dT$$

$$R_{YY}(T) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{YY}(w) e^{jwT} dw.$$

* Expression for close power spectral density $\frac{1}{2}$

Let us consider two random processes $x(t)$ & $y(t)$ truncated whose random functions are all $x(t)$ & $y(t)$ truncated portions $x_T(t)$, $y_T(t)$ in interval $(-T, T)$.

$$\text{i.e. } x_T(t) = \begin{cases} x(t) & \text{for } -T < t < T \\ 0 & \text{otherwise} \end{cases}$$

$$y_T(t) = \begin{cases} y(t) & \text{for } -T < t < T \\ 0 & \text{otherwise} \end{cases}$$

$$x_T(t) \xleftrightarrow{FT} X_T(\omega) \quad Y_T(t) \xleftrightarrow{FT} Y_T(\omega)$$

Power in time and frequency domains.

$$P_{XY}(T) = \frac{1}{2T} \int_{-T}^T x_T(t) Y_T(t) dt$$

By Parseval's theorem

$$P_{XY}(T) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{X_T^*(\omega) Y_T(\omega)}{2T} d\omega$$

Let $T \rightarrow \infty$ and apply expected value

Total average power

$$P_{XY} = \lim_{T \rightarrow \infty} \frac{1}{2T} E \left[\int_{-T}^T X_T^*(\omega) Y_T(\omega) d\omega \right]$$

$$= \lim_{T \rightarrow \infty} \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{E[X_T^*(\omega) Y_T(\omega)]}{2T} d\omega$$

$$= \lim_{T \rightarrow \infty} \frac{1}{2\pi} \int_{-\infty}^{\infty} R_{XY}(t, +) dt$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} dt \lim_{T \rightarrow \infty} \frac{E[X_T^*(\omega) Y_T(\omega)]}{2T}$$

Total cross power

$$\boxed{P_{XY} = P_{YX}}$$

$$R_{XX} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(\omega) d\omega$$

where

$$S_{XX}(\omega) = \lim_{T \rightarrow \infty} \frac{E[X_T^*(\omega) X_T(\omega)]}{2T}$$

$$\text{Hence } S_{YY}(\omega) = \lim_{T \rightarrow \infty} \frac{E[Y_T^*(\omega) Y_T(\omega)]}{2T}$$

Properties

1. $S_{xy}(\omega) = S_{yx}(-\omega) = S_{yx}^*(\omega)$
2. $\text{Re}[S_{xy}(\omega)]$ and $\text{Re}[S_{yx}(\omega)]$ are even function of ω .
3. $\text{Im}[S_{xy}(\omega)]$ & $\text{Im}[S_{yx}(\omega)]$ are odd function of ω .
4. $S_{xy}(\omega) = 0$ & $S_{yx}(\omega) = 0$ if $x(t)$ & $y(t)$ are orthogonal.
5. If $x(t)$ and $y(t)$ are uncorrelated & have central means \bar{x} & \bar{y} then $S_{xy}(\omega) = S_{yx}(\omega) = 2\pi \bar{x} \bar{y} \delta(\omega)$
6. $A[R_{xy}(t, t+T)] \leftrightarrow S_{xy}(\omega)$
 $A[R_{yx}(t, t+T)] \leftrightarrow S_{yx}(\omega)$.

For WSS

$$R_{xy}(T) \leftrightarrow S_{xy}(\omega)$$

$$R_{yx}(T) \leftrightarrow S_{yx}(\omega)$$

Properties of CPSD

$$1. S_{xy}(w) = S_{yx}(w) = S_{yx}^*(w)$$

proof :- $S_{xy}(w) = \int_{-\infty}^{\infty} R_{xy}(\tau) e^{j\omega\tau} d\tau$

$$\text{Let } \tau = -\tau' \quad S_{xy}(w) = \int_{\infty}^{-\infty} R_{xy}(-\tau') e^{j\omega(-\tau')} d\tau'$$

$$\text{We know } R_{xy}(\tau) = R_{yx}(\tau + \tau')$$

$$S_{xy}(w) = \int_{-\infty}^{\infty} R_{yx}(\tau') e^{j\omega\tau'} d\tau'$$

$$S_{xy}(w) = S_{yx}(-w) = S_{xy}^*(w)$$

$$4. S_{xx}(w) = 0 \& S_{yy}(w) = 0 \quad \text{if } x(t) \& y(t) \text{ are orthogonal.}$$

proof :- $S_{xy}(w) = \int_{-\infty}^{\infty} R_{xy}(\tau) e^{j\omega\tau} d\tau$
if $x(t) \& y(t)$ are orthogonal

$$\text{then } R_{xy}(\tau) = R_{yx}(\tau) = 0$$

$$\text{then } S_{xy}(w) = 0 \& S_{yx}(w) = 0.$$

$$5. \text{ if } x(t) \& y(t) \text{ are uncorrelated \& have constant mean values } \bar{x}, \bar{y} \text{ then}$$

$$S_{xy}(w) = 2\pi \bar{x} \bar{y} \delta(w)$$

Proof :- $S_{xy}(w) = \int_{-\infty}^{\infty} R_{xy}(\tau) e^{j\omega\tau} d\tau$
 $= \int_{-\infty}^{\infty} E[x(t)y(t+\tau)] e^{j\omega\tau} d\tau$
 $= \int_{-\infty}^{\infty} E[x(t)] E[y(t+\tau)] e^{j\omega\tau} d\tau$
 $= \bar{x} \bar{y} \int_{-\infty}^{\infty} e^{j\omega\tau} d\tau \quad \left(\int_{-\infty}^{\infty} e^{j\omega\tau} d\tau = 2\pi \delta(w) \right).$
 $\therefore S_{xy}(w) = \bar{x} \bar{y} 2\pi \delta(w)$

2. Real part of $S_{xy}(w) \& S_{yx}(w)$ are even functions of w .

Proof :- $S_{xy}(w) = \int_{-\infty}^{\infty} R_{xy}(\tau) e^{j\omega\tau} d\tau$
 $e^{j\omega\tau} = \cos \omega \tau + j \sin \omega \tau$

$$\text{Re}[S_{xy}(w)] = \int_{-\infty}^{\infty} R_{xy}(\tau) \cos \omega \tau d\tau$$

$\cos \omega \tau$ is even function means

$$\cos(-\omega\tau) = \cos \omega \tau$$

$$\text{Re}[S_{xy}(-w)] = \int_{-\infty}^{\infty} R_{xy}(\tau) \cos(-\omega\tau) d\tau$$
 $= \int_{-\infty}^{\infty} R_{xy}(\tau) \cos \omega \tau d\tau$

$$\text{Re}[S_{xy}(-w)] = \text{Re}[S_{xy}(w)] /$$

Here $\text{Re}[S_{yx}(-w)] = \text{Re}[S_{yx}(w)] /$

3. Imaginary part of $S_{xy}(w) \& S_{yx}(w)$ are odd functions.

Proof :- $S_{xy}(w) = \int_{-\infty}^{\infty} R_{xy}(\tau) e^{j\omega\tau} d\tau$
 $e^{j\omega\tau} = \cos \omega \tau + j \sin \omega \tau$

$$\text{Im}[S_{xy}(w)] = \int_{-\infty}^{\infty} R_{xy}(\tau) [j \sin \omega \tau] d\tau$$
 $= + \int_{-\infty}^{\infty} R_{xy}(\tau) \sin \omega \tau d\tau$

$\sin \omega \tau$ is odd function means

$$\sin(-\omega\tau) = -\sin \omega \tau$$

$$\text{Im}[S_{xy}(w)] = \int_{-\infty}^{\infty} R_{xy}(\tau) \sin(-\omega\tau) d\tau$$
 $= - \int_{-\infty}^{\infty} R_{xy}(\tau) \sin \omega \tau d\tau$

$$\text{Im}[S_{xy}(-w)] = -\text{Im}[S_{xy}(w)]$$

$$\text{Im}[S_{yx}(-w)] = -\text{Im}[S_{yx}(w)]$$

(P) The cross PSD is given as $S_{XY}(w) = \frac{1}{(a+jw)^2}$ $a > 0$, a is constant. Find cross correlation function.

$$S_{XY}(w) = \frac{1}{(a+jw)^2}$$

$$R_{XY}(w) = F^{-1}[S_{XY}(w)] = F\left(\frac{1}{(a+jw)^2}\right) = t e^{-at} u(t)$$

(P) Consider the random process $x(t) = A \cos(wt + \theta)$ where A & w are real constants and θ is random variable uniformly distributed over $[0, 2\pi]$. Find average power P_{XX} .

$$P_{XX} = A^2 \{ E[x^2(t)] \}$$

Uniformly distributed function $f_\theta(\theta) = \begin{cases} \frac{1}{2\pi}, & 0 < \theta < 2\pi \\ 0, & \text{otherwise} \end{cases}$

$$\therefore \frac{1}{2\pi} = \frac{1}{2\pi - 0} = \frac{1}{2\pi}$$

Now $x(t) = A \cos(wt + \theta)$

$$\begin{aligned} E[x^2(t)] &= \int_0^{2\pi} x^2(t) f_\theta(\theta) d\theta \\ &= \int_0^{2\pi} A^2 \cos^2(wt + \theta) \frac{1}{2\pi} d\theta \\ &= \frac{A^2}{2\pi} \int_0^{2\pi} \left(1 + \frac{\cos 2(wt + \theta)}{2} \right) d\theta \\ &= \frac{A^2}{4\pi} \left[\theta + \left[\frac{-\sin 2(wt + \theta)}{2} \right] \right] \Big|_0^{2\pi} \\ &= \frac{A^2}{4\pi} \left\{ 2\pi - \frac{1}{2} [\sin 2(4\pi + 2wt) - \sin 2wt] \right\} \end{aligned}$$

$$\begin{aligned} &= \frac{A^2}{4\pi} \left\{ 2\pi - \frac{1}{2} [+\sin 2wt - \sin 2wt] \right\} \\ &= \frac{A^2}{4\pi} \left\{ 2\pi - 0 \right\} \\ &= \frac{A^2}{2} \cancel{\frac{1}{\pi}} \sin 2wt \quad \left[\because \sin(4\pi + 2wt) = \sin 4\pi \cos 2wt + \cos 4\pi \sin 2wt = 0 + \cos 4\pi \sin 2wt = \sin 2wt \right] \end{aligned}$$

Time Average power $P_{XX} = A \{ E[x^2(t)] \}$

$$= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \frac{A^2}{2} dt$$

$$= \frac{1}{2} \left(\frac{1}{2} \frac{A^2}{2} [t] \right) \Big|_{-T}^T$$

$$P_{XX} = \frac{1}{2} \cdot \frac{A^2}{2} (T + (-T)) = \frac{A^2}{2} \quad \text{II}$$

If $R_{XX}(t) = \frac{A_0^2}{2} \sin \omega_0 t$ find $S_{XX}(w)$

sol $S_{XX}(w) = FT[R_{XX}(t)]$

$$= \int_{-\infty}^{\infty} \frac{A_0^2}{2} \sin \omega_0 t e^{-j\omega t} dt$$

$$\boxed{S_{XX}(w) = j \frac{A_0^2}{2} \pi [\delta(w+\omega_0) - \delta(w-\omega_0)]}$$

(P) If $R_{XX}(t) = \frac{A_0^2}{2} \cos \omega_0 t$ find $S_{XX}(w)$

sol $S_{XX}(w) = FT[R_{XX}(t)] = \int_{-\infty}^{\infty} \frac{A_0^2}{2} \cos \omega_0 t e^{-j\omega t} dt$

$$= \frac{A_0^2}{2} \pi [\delta(w+\omega_0) + \delta(w-\omega_0)]$$

(P) The cross spectral density is given as $S_{XY}(w) = \frac{w^2}{w^2+1}$. find out cross correlation function

sol Given $S_{XY}(w) = \frac{w^2}{w^2+1}$

$$R_{XY}(t) = F^{-1}[-S_{XY}(w)] = F\left[\frac{w^2}{w^2+1}\right]$$

$$R_{XY}(t) = F\left[\frac{w^2}{w^2+1}\right]$$

$$= F\left[\frac{w^2+1-1}{w^2+1}\right]$$

$$= F\left[\frac{w^2+1}{w^2+1} - \frac{1}{w^2+1}\right]$$

$$= F\left[1 - \frac{1}{w^2+1}\right]$$

$$= F[1] - F\left[\frac{1}{w^2+1}\right]$$

$$= F[1] - F\left[\frac{1}{w^2+1}\right] = \sqrt{2\pi} \delta(t) - \sqrt{\frac{\pi}{2}} e^{-|t|}$$

$$R_{XY}(t) = \sqrt{2\pi} \delta(t) - \sqrt{\frac{\pi}{2}} e^{-|t|}$$

$$\begin{aligned} & \int_{-\infty}^{\infty} \frac{w^2}{w^2+1} dw \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{w^2}{w^2+1} dw \quad \text{[using } \int_{-\infty}^{\infty} \frac{x^2}{x^2+a^2} dx = \frac{-x}{2(a^2+x)} + \frac{1}{2a} \tan^{-1}\left(\frac{x}{a}\right)\Big|_{-\infty}^{\infty}\text{]} \\ &= \frac{1}{2\pi} \left[\frac{-w}{2(w^2+1)} + \frac{1}{2} \tan^{-1}\left(\frac{w}{\sqrt{w^2+1}}\right) \right]_{-\infty}^{\infty} \\ &= \frac{1}{2\pi} \left[\dots \right] \end{aligned}$$

$$\begin{aligned} F[1] &= \sqrt{2\pi} \delta(t) \\ F\left[\frac{1}{w^2+1}\right] &= \sqrt{\frac{\pi}{2}} e^{-|t|} \end{aligned}$$

(P) The autocorrelation function of a random process $R_{XX}(T) = 4 \cos \omega_0 T$ where ω_0 is a constant obtain its power spectral density.

$$\begin{aligned}
 S_{XX}(w) &= \text{FT} [R_{XX}(T)] \\
 &= 4 \int_{-\infty}^{\infty} \cos \omega_0 T e^{-jwT} dT \\
 &= 4 \int_{-\infty}^{\infty} \left(\frac{e^{j\omega_0 T} + e^{-j\omega_0 T}}{2} \right) e^{-jwT} dT \\
 &= \frac{4}{2} \int_{-\infty}^{\infty} e^{-j(w-w_0)T} + e^{-j(w+w_0)T} dT \\
 &= 2 \left[\int_{-\infty}^{\infty} e^{-j(w-w_0)T} dT + \int_{-\infty}^{\infty} e^{-j(w+w_0)T} dT \right] \\
 &= 2 [2\pi \delta(w-w_0) + 2\pi \delta(w+w_0)]
 \end{aligned}$$

$$S_{XX}(w) = 4\pi [\delta(w-w_0) + \delta(w+w_0)]$$

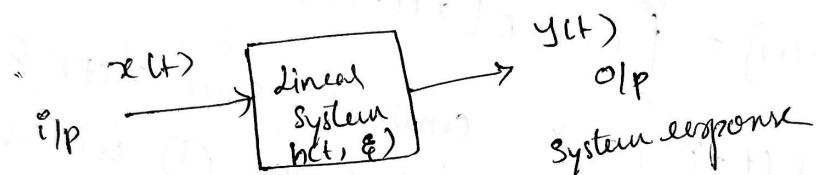
(P) If $R_{XX}(T) = \frac{A_0^2}{2} \sin \omega_0 T$ find $S_{XX}(w)$

$$\begin{aligned}
 S_{XX}(w) &= \text{FT} [R_{XX}(T)] \\
 &= \text{FT} \left[\frac{A_0^2}{2} \sin \omega_0 T \right] \\
 &= \frac{A_0^2}{2} \int_{-\infty}^{\infty} \sin \omega_0 T e^{-jwT} dT \\
 &= \frac{A_0^2}{2} \int_{-\infty}^{\infty} \left[\frac{e^{j\omega_0 T} - e^{-j\omega_0 T}}{2j} \right] e^{-jwT} dT \\
 &= \frac{A_0^2}{2} \int_{-\infty}^{\infty} \left[e^{-j(w-w_0)T} - e^{-j(w+w_0)T} \right] dT \\
 &= \frac{A_0^2}{4j} \left[\int_{-\infty}^{\infty} e^{-j(w-w_0)T} dT - \int_{-\infty}^{\infty} e^{-j(w+w_0)T} dT \right] \\
 &= \frac{A_0^2}{4j} \left[\left[\int_{-\infty}^{\infty} e^{j(w-w_0)T} dT \right] - \left[\int_{-\infty}^{\infty} e^{j(w+w_0)T} dT \right] \right] \\
 &= \frac{A_0^2}{4j} \left[2\pi \delta(w-w_0) - 2\pi \delta(w+w_0) \right] \\
 &= \frac{A_0^2 \pi}{2} \left[-(\delta(w+w_0) - \delta(w-w_0)) \right] = \frac{A_0^2 \pi}{2} \begin{bmatrix} \delta(w+w_0) \\ -\delta(w-w_0) \end{bmatrix}
 \end{aligned}$$

UNIT - 5 : Linear System Response to Random Inputs

Linear System :- A system is called linear if it has two mathematical properties: homogeneity & additivity.

LTI :- (Linear Time Invariant System) \rightarrow LIP doesn't change with time.
 LIPs for a linear combination of LIPs are same as a linear combination of individual responses to those LIPs.



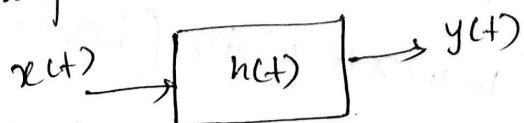
$$\text{System response } y(t) = L\{x(t)\}$$

where L -operator

\rightarrow LTI System - The system that are both linear & time-invariant are called LTI systems.

System response :- Consider a continuous LTI system with impulse response $h(t)$. Assume that system is always causal & stable. When continuous random process $x(t)$ is applied on this system, the LIP response is also continuous time random process $y(t)$. If $x(t) \& y(t)$ are discrete time random processes, then the linear system is called discrete ~~time~~ time system.

Let a random process $x(t)$ be applied to a continuous LTI system whose impulse response is $h(t)$ as shown in figure. Then the LIP response $y(t)$ is also a random process.



$$\begin{aligned} \text{The LIP response is Convolution integral } y(t) &= h(t) * x(t) \\ &= \int_{-\infty}^t h(\tau) x(t-\tau) d\tau \end{aligned}$$

Mean value of o/p response :- Consider a random process $x(t)$ is WSS Random process.

$$\text{Mean value of o/p response} = E[Y(t)]$$

$$\text{then } E[Y(t)] = E[h(t) * x(t)]$$

$$= E\left[\int_{-\infty}^{\infty} h(\tau) x(t-\tau) d\tau\right]$$

$$E[Y(t)] = \int_{-\infty}^{\infty} h(\tau) E[x(t-\tau)] d\tau \rightarrow ①$$

but $E[x(t-\tau)] = \bar{x} = \text{constant}$, since $x(t)$ is WSS

so above eqn ① becomes as below

$$\bar{y} = \bar{x} \int_{-\infty}^{\infty} h(\tau) d\tau \rightarrow ②$$

$$FT[h(\tau)] = H(\omega) = \int_{-\infty}^{\infty} h(\tau) e^{-j\omega\tau} d\tau \rightarrow ③$$

At $\omega=0$ $H(0) = \int_{-\infty}^{\infty} h(t) dt$ is called zero frequency

response of System.

$$\bar{y} = \bar{x} \int_{-\infty}^{\infty} h(\tau) d\tau$$

Thus the mean value of a o/p response $Y(t)$ of a WSS Random process is equal to the product of the mean value of o/p process & zero frequency response of the system.

Mean Square Value of o/p response :-

$$E[Y^2(t)] = E[(h(t) * x(t))^2]$$

$$= E[(h(t) * x(t)) (h(t) * x(t))]$$

$$= E\left[\int_{-\infty}^{\infty} h(\tau_1) x(t-\tau_1) d\tau_1 \int_{-\infty}^{\infty} h(\tau_2) x(t-\tau_2) d\tau_2\right]$$

$$= E\left[\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x(t-\tau_1) x(t-\tau_2) h(\tau_1) h(\tau_2) d\tau_1 d\tau_2\right]$$

$$E[y^2(t)] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E[x(t-\tau_1)x(t-\tau_2)] h(\tau_1) h(\tau_2) d\tau_1 d\tau_2$$

where τ_1 & τ_2 are shifts in time intervals. if $x(t)$ is a wss rp

then $E[x(t-\tau_1)x(t-\tau_2)] = R_{xx}(\tau_1 - \tau_2)$

Therefore $E[y^2(t)] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_{xx}(\tau_1 - \tau_2) h(\tau_1) h(\tau_2) d\tau_1 d\tau_2$

This expression is independent of time t .
it represents o/p power.

$$\begin{aligned} & E[x(t)x(t+\tau)] \\ &= R_{xx}(\tau) \\ &= R_{xx}(t + \tau - t) \end{aligned}$$

Autocorrelation function of o/p response of

$$\begin{aligned} R_{yy}(\tau_1, \tau_2) &= E[y(t_1)y(t_2)] \\ &= E[(h(t_1) * x(t_1))(h(t_2) * x(t_2))] \\ &= E \left[\int_{-\infty}^{\infty} h(\tau_1) x(t_1 - \tau_1) d\tau_1 \int_{-\infty}^{\infty} h(\tau_2) x(t_2 - \tau_2) d\tau_2 \right] \\ &= E \left[\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x(t_1 - \tau_1) x(t_2 - \tau_2) h(\tau_1) h(\tau_2) d\tau_1 d\tau_2 \right] \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E[x(t_1 - \tau_1) x(t_2 - \tau_2)] h(\tau_1) h(\tau_2) d\tau_1 d\tau_2 \end{aligned}$$

$$E[x(t_1 - \tau_1) x(t_2 - \tau_2)] = R_{xx}(t_2 - t_1 + \tau_1 - \tau_2)$$

We know that $E[x(t_1 - \tau_1) x(t_2 - \tau_2)] = R_{xx}(t_2 - t_1 + \tau_1 - \tau_2)$
if $x(t)$ is a wss gaussian process, set the time difference

$$\begin{aligned} \tau &= t_1 - t_2 \text{ & } t = t_1 \\ t_2 &= \tau + t \\ &= \tau + t \end{aligned}$$

$$E[x(t - \tau) x(t + \tau - \tau)] = R_{xx}(t + \tau_1 - \tau_2) \text{ then } \begin{cases} R_{xx}(t + \tau_1 - \tau_2) \\ -t + \tau_1 \\ R_{xx}(\tau + \tau_1 - \tau_2) \end{cases}$$

$$R_{yy}(t, t + \tau) = R_{yy}(\tau) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_{xx}(t + \tau_1 - \tau_2) h(\tau_1) h(\tau_2) d\tau_1 d\tau_2$$

$R_{yy}(t, t + \tau)$ is the autocorrelation function is a function of only τ .

If $R_{yy}(\tau) = R_{yy}(\tau)$ is the autocorrelation function is a function of only τ .

Hence o/p random process $y(t)$ is also wss random process.
 $R_{yy}(t, t + \tau) = R_{yy}(\tau) = R_{yy}(\tau)$
 $R_{yy}(\tau) = h(\tau) * h(-\tau)$ i.e. $R_{yy}(\tau) = h(\tau) * h(-\tau)$
 ACF is two fold convolution of applied input & impulse response

Cross correlation function of o/p response

If the i/p $x(t)$ is wss random process, then the cross correlation function of i/p $x(t)$ and o/p $y(t)$ is

$$\begin{aligned} R_{xy}(t, t+\tau) &= E[x(t)y(t+\tau)] \\ &= E\left[x(t)\int_0^\infty h(\tau_1)x(t+\tau-\tau_1)d\tau_1\right] \\ &= \int_{-\infty}^{\infty} E[x(t)x(t+\tau-\tau_1)]h(\tau_1)d\tau_1 \end{aligned}$$

$$R_{xy}(t+\tau) = \int_{-\infty}^{\infty} R_{xx}(t-\tau_1)h(\tau_1)d\tau_1,$$

which is the convolution of $R_{xx}(\tau)$ & $h(\tau)$

$\therefore R_{xy}(\tau) = R_{xx}(\tau) * h(\tau)$ similarly we can show that

$$\text{Hence } R_{yx}(\tau) = R_{xx}(\tau) * h(-\tau)$$

This shows that $x(t)$ and $y(t)$ are jointly wss. And we can also relate the auto correlation functions & cross correlation functions as

$$R_{yy}(\sigma) = R_{xy}(\sigma) * h(-\sigma)$$

$$R_{yy}(\sigma) = R_{yx}(\sigma) * h(\sigma)$$

Spectral characteristics of a System Response

Consider that the random process $x(t)$ is a wss random process with autocorrelation function $R_{xx}(\sigma)$, applied through an LTI system. It is noted that o/p response $y(t)$ is also a wss & processes $x(t)$ & $y(t)$ are jointly wss. We can obtain power spectral characteristics of the o/p process $y(t)$ by taking the Fourier transform of the correlation function.

PSD of response Consider that a random process $x(t)$ is applied on an LTI system having a transfer function $H(j\omega)$. The o/p response is $y(t)$. If the power spectrum of the i/p process is $S_{xx}(\omega)$, then the power spectrum of the o/p response is given by

$$S_{yy}(\omega) = |H(j\omega)|^2 S_{xx}(\omega)$$

Proof: Let $R_{yy}(\tau)$ be the autocorrelation of the output response $y(t)$. Then the power spectrum of the response is the FT of $R_{yy}(\tau)$. Therefore $S_{yy}(w) = F[S_{yy}(\omega)] = \int_{-\infty}^{\infty} R_{yy}(\tau) e^{j\omega\tau} d\tau$

$$\text{we know that } R_{yy}(\tau) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_{xx}(\tau + \tau_1 - \tau_2) h(\tau_1) h(\tau_2) d\tau_1 d\tau_2$$

$$\text{then } S_{yy}(w) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_{xx}(\tau + \tau_1 - \tau_2) h(\tau_1) h(\tau_2) e^{j\omega\tau} d\tau_1 d\tau_2 e^{j\omega\tau}$$

$$= \int_{-\infty}^{\infty} h(\tau_1) \int_{-\infty}^{\infty} h(\tau_2) \left[R_{xx}(\tau + \tau_1 - \tau_2) e^{j\omega(\tau - (\tau_1 - \tau_2))} \right] d\tau_1 d\tau_2 d\tau$$

$$= \int_{-\infty}^{\infty} h(\tau_1) e^{j\omega\tau_1} \int_{-\infty}^{\infty} h(\tau_2) e^{-j\omega\tau_2} \int_{-\infty}^{\infty} R_{xx}(\tau + \tau_1 - \tau_2) e^{j\omega(\tau - (\tau_1 - \tau_2))} d\tau_2 d\tau_1 d\tau$$

$$\text{let } \tau + \tau_1 - \tau_2 = t; dt = d\tau; T = t - (\tau_1 - \tau_2)$$

$$\therefore S_{yy}(w) = \int_{-\infty}^{\infty} h(\tau_1) e^{j\omega\tau_1} \int_{-\infty}^{\infty} h(\tau_2) e^{-j\omega\tau_2} \int_{-\infty}^{\infty} R_{xx}(t) e^{j\omega t} dt$$

$$\text{we know that } H(w) = \int_{-\infty}^{\infty} h(\tau) e^{j\omega\tau} dt; H(-w) = \int_{-\infty}^{\infty} h(\tau) e^{-j\omega\tau} dt$$

$$\therefore S_{yy}(w) = H(w) H^*(w) S_{xx}(w) = H(w) H^*(-w) S_{xx}(w)$$

$$\boxed{\text{Average power } P_{yy} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{yy}(w) dw}$$

Hence proved

Now we can prove that the cross PSD function is $S_{xy}(w) = S_{xx}(w) H(w)$ & $S_{yx}(w) = S_{xx}(w) H(-w)$

Spectrum Bandwidth: The spectral density is mostly concentrated at a certain frequency value. It decreases at other frequencies. The BW of spectrum is the range of frequencies having significant values. It is defined as the measure of spread of spectral density and is also called rms BW or normalized BW. It is given by

$$\boxed{W_{rms}^2 = \frac{\int_{-\infty}^{\infty} w^2 S_{xx}(w) dw}{\int_{-\infty}^{\infty} S_{xx}(w) dw}}$$

Types of random processes

Depending upon frequency components random processes are classified into 4 types.

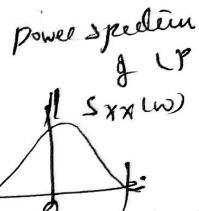
1. Lowpass random process

2. Bandpass random process

3. Band limited random process

4. Narrow Band random process

Broadband signals.

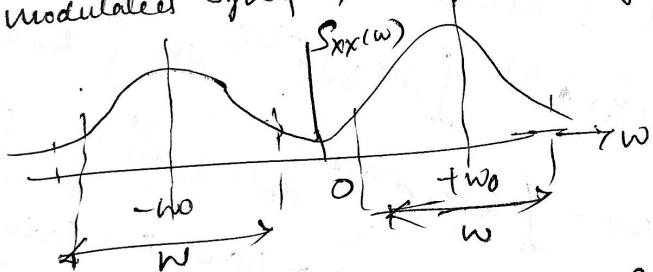


1. Lowpass RP - Ex - Speech, Image, Video.

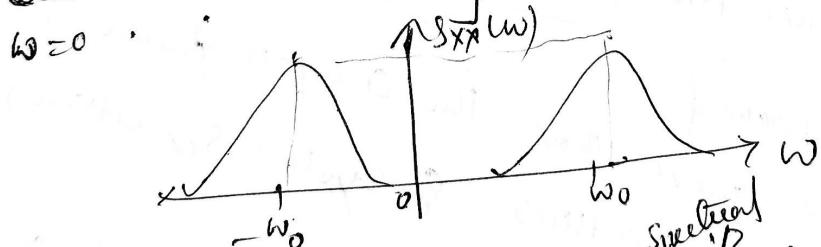
2. Bandpass RP - $S_{xx}(w)$ have significant components within a BW 'w' that doesn't include w_0 . BW practically small. amount of power.

Spectrum at w_0

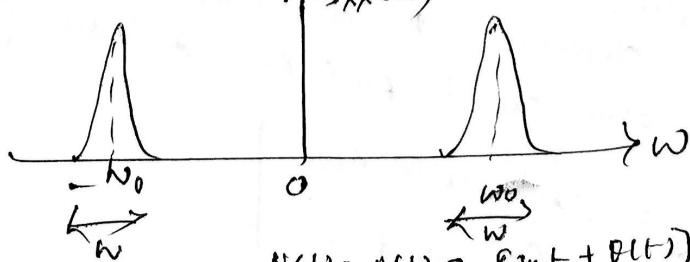
Ex: modulated signal, Non transmitting over communication channel



3. Band limited random process - if power spectrum components are outside the frequency band of width w that doesn't include $w_0 = 0$.



4. Narrow Band Random process - Spectral BW is very small compared to the band center frequency, i.e., $w \ll w_0$ where w - Band width and w_0 is frequency at which the power spectrum is maximum.



$$N(t) = A(t) \cos\{w_0 t + \theta(t)\}$$

$A(t)$ - Amp & $\theta(t)$ phase of RP

Representation of a narrow Band process

For any arbitrary wss RP. $N(t)$ the quadrature form of narrow band process can be represented as $N(t) = X(t) \cos \omega t - Y(t) \sin \omega t$.

where $X(t), Y(t)$ are respectively called the in-phase & quadrature phase components of $N(t)$, they can be expressed as

$$X(t) = A(t) \cos(\phi(t))$$

$$Y(t) = A(t) \sin(\phi(t)) \quad \text{and relation b/w these processes } A(t) \& \phi(t)$$

are given by $A(t) = \sqrt{X^2(t) + Y^2(t)}$

$$\phi(t) = \tan^{-1} \left(\frac{Y(t)}{X(t)} \right)$$

Properties of Band limited Random Process

Let $N(t)$ is Band limited wss random process with zero mean value and power spectral density $S_{NN}(w)$. $N(t) = X(t) \cos \omega t - Y(t) \sin \omega t$

i. If $N(t)$ is wss then $X(t) \& Y(t)$ are jointly wss

ii. If $N(t)$ has zero mean ie $E[N(t)] = 0$, then $E[X(t)] = E[Y(t)] = 0$

iii. MSV $E[N^2(t)] = E[X^2(t)] = E[Y^2(t)]$

iv. Autocorrelation function $R_{XX}(r) = R_{YY}(r)$.

v. $X(t) \& Y(t)$ have same autocorrelation function $R_{XX}(r) = R_{YY}(r)$.

vi. The cross correlation function $R_{XY}(r) = R_{YX}(r)$.

vii. If processes are orthogonal, then $R_{XY}(r) = R_{YX}(r) = 0$.

viii. $X(t), Y(t)$ have same PSD's

ix. Both $X(t), Y(t)$ have same PSD's

$$S_{YY}(w) = S_{XX}(w) = \begin{cases} S_N (\omega_{w_0}) e^{j(\omega_{w_0} + \omega)t} & \text{for } |\omega| < \omega_0 \\ 0 & \text{otherwise} \end{cases}$$

x. CPSD $S_{XY}(w) = S_{YX}(w)$

xi. If $N(t)$ is a Gaussian random process, then $X(t) \& Y(t)$ are jointly Gaussian.

xii. The relation b/w autocorrelation & power spectrum $S_{NN}(w)$ is

$$R_{XX}(r) = \frac{1}{\pi} \int_0^\infty [S_{NN}(w) \cos(w - w_0)r] dw$$

$$R_{YY}(r) = \frac{1}{\pi} \int_0^\infty [S_{NN}(w) \cos(w - w_0)r] dw$$

10. If $N(t)$ is zero mean gaussian and its psd, $S_N(\omega)$ is ~~symmetric~~
symmetric about ω_0 , then $x(t), y(t)$ are statistically independent.

(Q) Consider a linear system shown below. $x(t)$ is i/p, $y(t)$ is o/p
ACF of $x(t)$ is $R_{xx}(r) = 3 \sin r$ find PSD, ACF & MS of
the o/p $y(t)$

$$x(t) \rightarrow \boxed{\frac{1}{6+j\omega}} \rightarrow y(t)$$

sol Given $H(\omega) = \frac{1}{6+j\omega}$

$$(i) PSD = S_{xx}(\omega) |H(\omega)|^2 \quad H(\omega) = \frac{1}{6+j\omega}$$

$$\begin{aligned} S_{xx}(\omega) &= F\{R_{xx}(t)\} \\ &= F\{3 \delta(t)\} \\ &= 3 \delta(1) = 3. \end{aligned} \quad \begin{aligned} |H(\omega)| &= \sqrt{\frac{1}{36+\omega^2}} \\ |H(\omega)| &= \frac{1}{\sqrt{36+\omega^2}} \end{aligned}$$

$$PSD = 3 \left(\frac{1}{\sqrt{36+\omega^2}} \right)^2 = \frac{3}{36+\omega^2}$$

$$\begin{aligned} (ii) R_{yy}(r) &= F\{S_{yy}(\omega)\} \\ &= F\left\{ \frac{3}{6+j\omega} \right\} = \frac{1}{j}\left\{ \frac{2ab}{b^2+\omega^2} \right\} = tae^{-tr} \\ &= \frac{3}{12} e^{-6|t|} \end{aligned}$$

$$t = \frac{1}{6^2+0} = \frac{1}{36+0} = \frac{1}{12}$$

$$\begin{aligned} (iii) E\{y(t)\} &= R_{yy}(0) = P \\ &= \frac{1}{4} e^{-6|0|} = \frac{1}{4} e^0 = \frac{1}{4} = 0.25 \end{aligned}$$

$$\textcircled{2} \quad x(t) \text{ is wss } E[x(t)] = 0 \quad R_{xx}(t) = e^{-2|t|} \geq 0 \Rightarrow \frac{1}{2+j\omega} = \frac{1}{2+\omega}$$

Find $S_{yy}(\omega)$ & $E[Y(t)]$

$$\text{sol 1)} S_{yy}(\omega) = S_{xx}(\omega) |1 + j\omega|^2$$

$$S_{xx}(\omega) = \text{FT}[R_{xx}(t)] = \text{FT}[e^{-2|t|}] = \frac{2(1)(2)}{\omega^2 + \omega^2} = \frac{4}{4 + \omega^2}$$

$$|1 + j\omega|^2 = \left| \frac{1}{2 + j\omega} \right|^2 = \left(\frac{1}{\sqrt{4 + \omega^2}} \right)^2 = \frac{1}{4 + \omega^2}$$

$$S_{yy}(\omega) = \frac{4}{4 + \omega^2} \cdot \frac{1}{4 + \omega^2} = \frac{4}{(4 + \omega^2)^2} //$$

$$\textcircled{2} \quad P_{xx} = E[X^2]$$

$$R_{xx}(t) = \text{IFT}[S_{xx}(\omega)] = \text{IFT}\left[\frac{4}{4 + \omega^2}\right] =$$

$$\textcircled{2} \quad E[Y(t)] = \bar{x} + t^0$$

$$= E[X(t)] + t^0$$

$$E[Y(t)] = 0 \cdot \frac{1}{2} = 0 //$$

$$\textcircled{3} \quad \text{If } x(t) \text{ is wss, } E[X(t)] = 2; \quad R_{xx}(t) = 3e^{-2|t|}, \quad h(t) = e^{-ut}$$

$$\text{find } S_{yy}(\omega), E[Y(t)]$$

$$\text{sol ①} \quad S_{yy}(\omega) = S_{xx}(\omega) |1 + j\omega|^2$$

$$= \text{FT}[R_{xx}(t)] \left[\left(\frac{1}{2 + j\omega} \right)^2 \right]$$

$$= \text{FT}[3e^{-2|t|}] \left[\frac{1}{j\omega + 4} \right]^2$$

$$= 3 \left(\frac{4}{4 + \omega^2} \right) \left(\frac{1}{\omega^2 + 16} \right) = \frac{12}{(\omega^2 + 4)(\omega^2 + 16)} //$$

$$\textcircled{2} \quad E[Y(t)] = E[X(t)] + t^0$$

$$= 2 \left(\frac{1}{2 + \omega} \right) + 2 = \frac{2}{\omega} = \frac{1}{2} = 0.5 //$$

- ① A random process noise $\mathbf{x}(t)$ having power spectrum $S_{XX}(w) = \frac{3}{49+w^2}$ is applied to a LTI system which $h(t) = t^2 e^{-7tT}$. The output $y(t)$ is

- Avg power of $x(t)$
- Find power spectrum of $y(t)$
- Final average power of $y(t)$.

$$\text{sgn} \therefore (1) P_{XX} = R_{XX}(0)$$

$$R_{XX}(0) = F^{-1} \left\{ S_{XX}(f) \right\} = F \left\{ \frac{3}{49+w^2} \right\} = \frac{3}{49} \int_{-\infty}^{\infty} \frac{1}{1+\frac{w^2}{49}} \frac{1}{T} dw = \frac{3}{14} e^{-7T}$$

$$P_{XX} = R_{XX}(0)$$

$$\boxed{P_{XX} = \frac{3}{14} e^{-7T} = \frac{3}{14} \text{ watts}}$$

$$(2) S_{YY}(w) = S_{XX}(w) |H(w)|^2$$

$$S_{XX}(w) = \frac{3}{49+w^2}, |H(w)|^2 = F \left\{ h(t) \right\}$$

$$= F \left\{ t^2 e^{-7tT} \right\}$$

$$= \frac{2}{(s+7)^3} = \frac{2}{(jw+7)^3}$$

$$|H(w)| = \left| \frac{2}{(jw+7)^3} \right| = \frac{2}{(\sqrt{49+w^2})^3}$$

$$S_{YY}(w) = S_{XX}(w) |H(w)|^2 \quad |H(w)|^2 = \frac{4}{(49+w^2)^3}$$

$$= \frac{3}{49+w^2} \cdot \frac{4}{(49+w^2)^3}$$

$$(3) P_{XX} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{YY}(w) dw = \frac{1}{2\pi} \int_0^{\infty} \frac{12}{(49+w^2)^4} dw$$

$$= \frac{12}{2\pi} \left[\int_0^{\infty} \frac{1}{(49+w^2)^4} dw \right]$$

$$= \frac{12}{2\pi} \cdot \frac{5\pi}{16(49)^3} = 2.276 \times 10^6 \text{ s/w}$$

$$\int_0^{\infty} \frac{1}{(a^2+w^2)^4} dw = \frac{5\pi}{16a^4}$$

$$\text{Average power } P_{yy} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{yy}(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(\omega) |H(\omega)|^2 d\omega$$

Cross power density spectrum of ip & o/p of system

$$S_{xy}(\omega) = \text{PT} \{ R_{xy}(t) \} = \int_{-\infty}^{\infty} R_{xy}(t) e^{j\omega t} dt$$

$$= \int_{-\infty}^{\infty} R_{xx}(t-h(t)) e^{j\omega t} dt$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_{xx}(t-\tau_1) h(\tau_1) e^{j\omega t} d\tau_1 dt$$

$$\begin{aligned} \text{Let } t - \tau_1 &= t \\ t &= t + \tau_1 \quad d\tau = dt \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_{xx}(t) h(\tau_1) e^{-j\omega(t+\tau_1)} dt d\tau_1 \\ &= \int_{-\infty}^{\infty} R_{xx}(t) e^{-j\omega t} dt \int_{-\infty}^{\infty} h(\tau_1) e^{-j\omega \tau_1} d\tau_1 \\ &= \text{PT} \{ R_{xx}(t) \} \text{PT} \{ h(t) \} \end{aligned}$$

$$\boxed{S_{xy}(\omega) = S_{xx}(\omega) H(\omega)}$$

$$\text{Now } S_{yx}(\omega) = S_{xx}(\omega) H^*(\omega)$$

$$= S_{xx}(\omega) H^*(\omega)$$

$$\text{Cross power } P_{xy} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xy}(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(\omega) H(\omega) d\omega$$

$$P_{yx} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{yx}(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(\omega) H^*(\omega) d\omega$$

$$\text{Total power } P = P_{xy} + P_{yx} = \text{Total average power.}$$

Q) A wss RP $x(t)$ is applied to the input of an LTI system whose impulse response is $5 + e^{-2t}$. The mean of $x(t)$ is 3. Find mean of system response.

Sol Given $h(t) = 5 + e^{-2t}$

$$E[x(t)] = \bar{x} = 3$$

$$E[y(t)] = E[x(t)]H(0)$$

$$= \bar{x} \cdot H(0)$$

$$H(j\omega) = H(\omega) = \frac{5(1)}{(s+2)^2} = \frac{5}{(s+2)^2} = \frac{5}{(j\omega+2)^2}$$

$$H(0) = \frac{5}{(0+2)^2} = \frac{5}{4}$$

$$E[y(t)] = \bar{x} \cdot H(0)$$

$$= 3 \left(\frac{5}{4} \right) = \frac{15}{4} = 3.75$$

Q) $\bar{x} = 3$; $h(t) = 5 + e^{-2t}$ mean of system

$$H(j\omega) = 5 \left[\frac{1}{(s+2)^3} \right] = \frac{10}{(s+2)^3} = \frac{10}{(j\omega+2)^3}$$

$$H(0) = \frac{10}{(0+2)^3} = \frac{10}{8} = \frac{5}{4} = 1.25$$

$$E[y(t)] = \bar{x} \cdot H(0)$$

$$= 3 \times 1.25 = 3.75.$$

Q) $\bar{x} = 2$; $h(t) = 2e^{-2t}u(t)$

$$\begin{aligned} H(j\omega) &= E[u(t)] = E[2e^{-2t}u(t)] \\ &= \int_{-\infty}^{\infty} 2e^{-2t}u(t) e^{j\omega t} dt \\ &= \int_0^{\infty} 2e^{-(2+j\omega)t} dt \\ &= 2 \left[\frac{e^{-(2+j\omega)t}}{-(2+j\omega)} \right] \Big|_0^{\infty} \end{aligned}$$

$$H(j\omega) = \frac{2}{-(2+j\omega)} \left[e^0 - 1 \right] = \frac{2}{2+j\omega}$$

$$H(0) = \frac{2}{2} = 1 ; \bar{x} = 2 ; E[y(t)] = \bar{x} \cdot H(0) = \frac{2}{2+j\omega} = 2$$

Random process: Spectral characteristics!

① power spectrum density (or) power density spectrum

Definition:

The power spectral density of a wide sense stationary (wss) random process $X(t)$ is defined as the Fourier Transform of the autocorrelation function $[R_{XX}(\tau)]$ of $X(t)$. It can be expressed as

$$S_{XX}(w) = FT [R_{XX}(\tau)]$$

$$\therefore S_{XX}(w) = \int_{-\infty}^{\infty} R_{XX}(\tau) e^{-jw\tau} d\tau$$

∴ we can obtain the autocorrelation function from the PSD by taking Inverse Fourier

Transform

$$R_{XX}(\tau) = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{XX}(w) e^{jw\tau} dw.$$

∴ Power density spectrum $S_{XX}(w)$ and the auto correlation function $R_{XX}(\tau)$ are Fourier Transform pairs.

(2)

Definition(2):-

The power spectral density

can also be defined as

$$S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{E[|X_T(\omega)|^2]}{2T}$$

where $|X_T(\omega)|$ is a Fourier Transform of $x(t)$
in the interval $[-T, T]$.

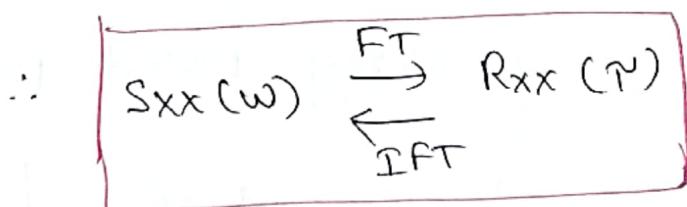
VVimp
sem(2)

Relationship between power spectral density & autocorrelation function of random process

(or)

Weiner Khinchin relation

Ans:- The power spectral density and the time average of the autocorrelation function form a Fourier transform pair.



Proof: we have power spectral density

$$S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{E[|X_T(\omega)|^2]}{2T}$$

(3)

~~we know that~~
we know that, we can write

$$\boxed{|x_T(\omega)|^2 = \hat{x}_T^*(\omega) x_T(\omega)}$$

$$\therefore S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{E[\hat{x}_T^*(\omega) x_T(\omega)]}{2T} \quad \text{--- (1)}$$

here

$$x_T(\omega) = \int_{-T}^T x(t_2) e^{-j\omega t_2} dt_2$$

$$\hat{x}_T^*(\omega) = \int_{-T}^T x(t_1) e^{j\omega t_1} dt_1$$

\therefore eq (1) can be written as

$$S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{2T} E \left[\int_{-T}^T x(t_1) e^{j\omega t_1} dt_1 \cdot \int_{-T}^T x(t_2) e^{-j\omega t_2} dt_2 \right]$$

$$= \lim_{T \rightarrow \infty} \frac{1}{2T} E \left[\int_{-T}^T \int_{-T}^T x(t_1) x(t_2) e^{-j\omega(t_2 - t_1)} dt_1 dt_2 \right]$$

$$= \lim_{T \rightarrow \infty} \frac{1}{2T} \left[\int_{-T}^T \int_{-T}^T E[x(t_1)x(t_2)] \cdot e^{-j\omega(t_2 - t_1)} dt_1 dt_2 \right]$$

$$S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{xx}(t_1, t_2) e^{-j\omega(t_2 - t_1)} dt_1 dt_2$$

(4)

By taking Inverse Fourier transform on both sides

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(w) e^{\int w \tilde{r}} dw = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left[\underset{T \rightarrow \infty}{\lim} \frac{1}{2T} \int_{-T}^{T} R_{xx}(t_1, t_2) \right. \\ \left. e^{-\int w(t_2-t_1)} dt_1 dt_2 \right] e^{\int w \tilde{r}} dw$$

$$= \underset{T \rightarrow \infty}{\lim} \frac{1}{2T} \int_{-T}^{T} \int_{-T}^{T} R_{xx}(t_1, t_2) \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{-\int w(t_2-t_1)} \\ \cdot e^{\int w \tilde{r}} dw dt_1 dt_2.$$

$$= \underset{T \rightarrow \infty}{\lim} \frac{1}{2T} \int_{-T}^{T} \int_{-T}^{T} R_{xx}(t_1, t_2) \cdot \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{\int w(\tau - t_2 + t_1)} \\ dw dt_1 dt_2$$

we have

$$F[\delta(t)] = 1$$

$$\delta(t) = F^{-1}[1]$$

$$\delta(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} 1 \cdot e^{\int w t} dw$$

from the above eqn, we can write

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} e^{\int w (\tau - t_2 + t_1)} dw = \delta(\tau - t_2 + t_1)$$

(8)

$$\therefore \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{xx}(\omega) e^{j\omega\tau} d\omega = \underset{T \rightarrow \infty}{\text{LT}} \frac{1}{2T} \int_{-T}^T \int_{-T}^T R_{xx}(t_1, t_2) \cdot \delta(\tau - t_2 + t_1) dt_1 dt_2$$

we know that

$$\boxed{\int_{-T}^T \delta(\tau - t_2 + t_1) dt_2 = 1 \text{ at } \tau - t_2 + t_1 = 0}$$

$$\text{i.e. } t_2 = \tau + t_1$$

$$\therefore F^{-1}[S_{xx}(\omega)] = \underset{T \rightarrow \infty}{\text{LT}} \frac{1}{2T} \int_{-T}^T R_{xx}(t_1, \tau + t_1) dt_1$$

$$\text{Let } t_1 = t, dt_1 = dt$$

$$\therefore F^{-1}[S_{xx}(\omega)] = \underset{T \rightarrow \infty}{\text{LT}} \frac{1}{2T} \int_{-T}^T R_{xx}(t, \tau + t) dt$$

\therefore The RHS of the above equation is the time average of the autocorrelation function.

average of the autocorrelation function.

Thus the time average of the autocorrelation function and the power spectral density form a Fourier Transform pair, if the process is stationary, the time average of autocorrelation

$R_{xx}(t, t+\tau)$ will be $R_{xx}(\tau)$. Since the

autocorrelation function of stationary process is independent of time.

(6)

$$\text{So } \bar{F} [S_{xx}(\omega)] = R_{xx}(T)$$

$$\boxed{\therefore R_{xx}(T) \xrightarrow{\text{IFT}} S_{xx}(\omega) \xleftarrow{\text{FT}}}$$

hence proved.

Note: This equation also known as weiner khinchin relation.

(3) properties of the power density spectrum:-

property 1 $S_{xx}(\omega) \geq 0$ i.e PSD is non negative.

proof: → from the definition (2) of PSD is

$$S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{E[|x_T(\omega)|^2]}{2T}$$

→ from the above equation, the expected value of a non negative function $E[|x_T(\omega)|^2]$ is always non negative.

Hence

$$\boxed{S_{xx}(\omega) \geq 0}$$

(7)

Property 2 The power spectral density at zero frequency
is equal to the area under the curve of
the autocorrelation $R_{XX}(\tau)$

i.e.

$$S_{XX}(0) = \int_{-\infty}^{\infty} R_{XX}(\tau) d\tau$$

Proof: from the definition we know that-

$$S_{XX}(\omega) = \int_{-\infty}^{\infty} R_{XX}(\tau) e^{-j\omega\tau} d\tau$$

At $\omega=0$, then

$$S_{XX}(0) = \int_{-\infty}^{\infty} R_{XX}(\tau) d\tau$$

Hence proved.

Property 3 The power spectral density of a real
process $x(t)$ is an even function

i.e.

$$S_{XX}(-\omega) = S_{XX}(\omega)$$

Proof: we know that

$$S_{XX}(\omega) = \int_{-\infty}^{\infty} R_{XX}(\tau) e^{-j\omega\tau} d\tau$$

(8)

Also

$$S_{xx}(-\omega) = \int_{-\infty}^{\infty} R_{xx}(r) e^{-j\omega r} dr$$

Now substitute $r = -\tau$ then

$$\therefore S_{xx}(-\omega) = \int_{-\infty}^{\infty} R_{xx}(-\tau) e^{-j\omega \tau} d\tau$$

from the properties of Auto correlation

$$\boxed{R_{xx}(-\tau) = R_{xx}(\tau)}$$

$$\therefore S_{xx}(-\omega) = \int_{-\infty}^{\infty} R_{xx}(\tau) e^{-j\omega \tau} d\tau$$

$$\therefore \boxed{S_{xx}(-\omega) = S_{xx}(\omega)}$$

$S_{xx}(\omega)$ is an even function.

proof $S_{xx}(\omega)$ is always real function.

Proof: from the defⁿ of PSD, we know that

$$S_{xx}(\omega) = \lim_{T \rightarrow \infty} \frac{E[|x_T(\omega)|^2]}{2T}$$

since the function $|x_T(\omega)|$ is a real function

so, $S_{xx}(\omega)$ is always real.

(9)

Property (9) : If $x(t)$ is a WSS random process with power spectral density $S_{xx}(w)$, then the PSD of the derivative of $x(t)$ is equal to w^2 times the PSD $S_{xx}(w)$.

i.e
$$S_{\dot{x}\dot{x}}(w) = w^2 S_{xx}(w)$$