



## CHAPTER 4

# THE CONTINUOUS- TIME FOURIER TRANSFORM

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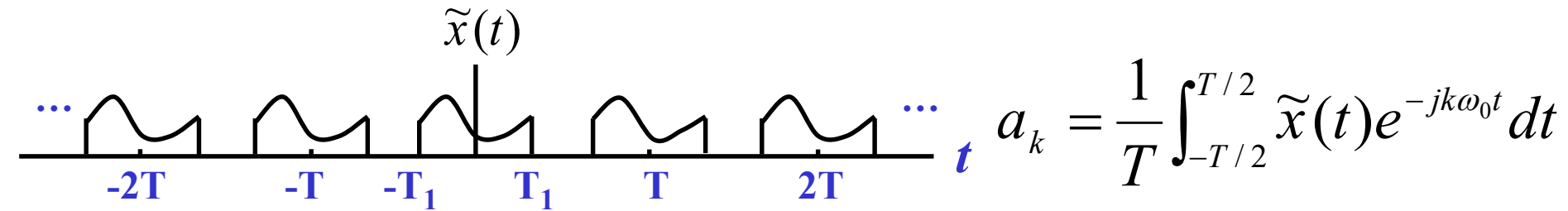
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Sampling

- Representation of continuous-time **aperiodic** signals as linear combination of complex exponentials — Inverse Fourier Transform
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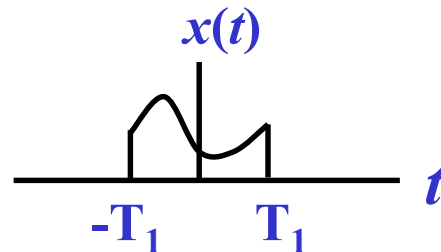
# 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

## 4.1.1 Fourier Transform and Inverse Fourier Transform



$$Ta_k = \int_{-T/2}^{T/2} \tilde{x}(t) e^{-jk\omega_0 t} dt$$

As  $T \rightarrow \infty$ ,  $\lim_{T \rightarrow \infty} Ta_k = \int_{-\infty}^{\infty} x(t) e^{-jk\omega_0 t} dt = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$



Use  $X(j\omega)$  to denote this integral, then we have:

Frequency spectrum of  $x(t)$   $\rightarrow$   $X(j\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$   $\leftarrow$  Fourier transform of  $x(t)$

## 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

Since  $X(j\omega) = \lim_{T \rightarrow \infty} T a_k = \lim_{\omega_0 \rightarrow 0} 2\pi \frac{a_k}{\omega_0},$

$X(j\omega)$  is actually spectrum-density function(频谱密度函数).

$$\begin{aligned}\tilde{x}(t) &= \sum_{k=-\infty}^{\infty} a_k e^{jk\omega_0 t} = \sum_{k=-\infty}^{\infty} \left[ \frac{1}{T} \int_{-T/2}^{T/2} \tilde{x}(t) e^{-jk\omega_0 t} dt \right] e^{jk\omega_0 t} \\ &= \frac{\omega_0}{2\pi} \sum_{k=-\infty}^{\infty} \left[ \int_{-T/2}^{T/2} \tilde{x}(t) e^{-jk\omega_0 t} dt \right] e^{jk\omega_0 t}\end{aligned}$$

As  $T \rightarrow \infty$ ,  $x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega) e^{j\omega t} d\omega$  ← *Inverse Fourier transform*

*analysis* equation:  $X(j\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$

*synthesis* equation:  $x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega) e^{j\omega t} d\omega$

Fourier Transform  
Pair

## 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

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Comparing the synthesis equations in:

$$CTFS: \quad x(t) = \sum_{k=-\infty}^{\infty} a_k e^{jk\omega_0 t} \quad CTFT: \quad x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega) e^{j\omega t} d\omega$$

$$a_k \Leftrightarrow \frac{X(j\omega) d\omega}{2\pi}$$

This fact means: Aperiodic signals can also be decomposed as linear combination of infinite numbers of complex exponentials, which occur at a continuum of frequencies, but have amplitudes infinitesimally small — approaching zero!

$|X(j\omega)|$  indicate the relative amplitudes of all components, and angle  $\angle X(j\omega)$  indicate the phases of all components.

## 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

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An useful relationship:  $a_k = \frac{1}{T} X(j\omega) \Big|_{\omega=k\omega_0}$

Where,  $\tilde{x}(t) \xleftrightarrow{FS} a_k$ ,  $x(t) \xleftrightarrow{FT} X(j\omega)$ .

This relationship is also valid for aperiodic signals with unlimited duration!

### ➤ Convergence of Fourier Transforms

Dirichlet conditions:

1.  $x(t)$  is absolutely integrable; that is  $\int_{-\infty}^{\infty} |x(t)| dt < \infty$
  2.  $x(t)$  have a finite number of maxima and minima within any finite interval.
  3.  $x(t)$  have a finite number of discontinuities within any finite interval.
- Furthermore, each of these discontinuities must be finite.

If **impulse functions are permitted** in the transform, some signals which are **not absolutely integrable** over an infinite interval, can also be considered to have Fourier transforms. This will be convenient in the discussion of Fourier methods.



# 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

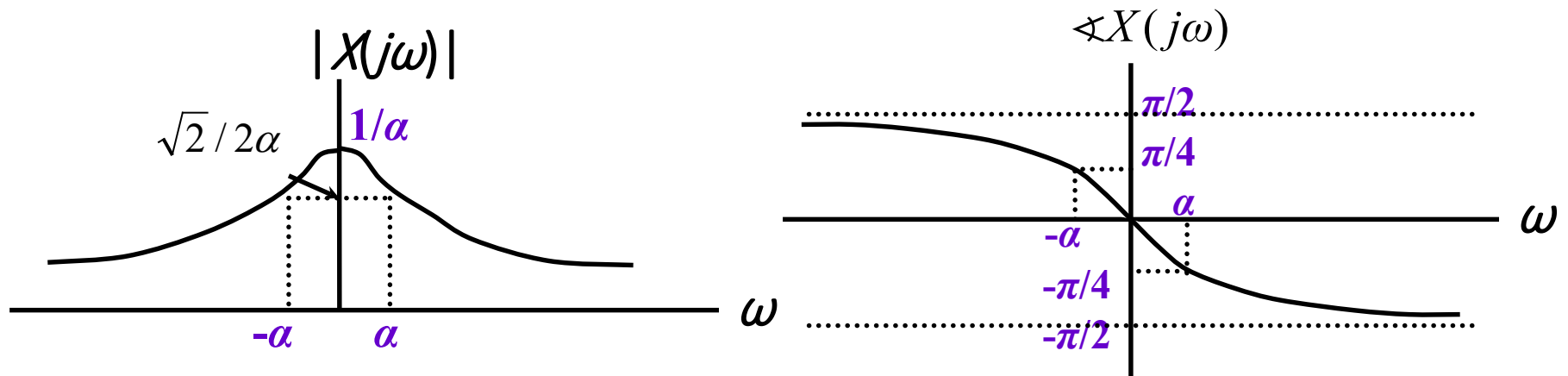
## 4.1.2 Examples

### Example 4.1

Consider the signal  $x(t) = e^{-\alpha t} u(t)$   $\alpha > 0$ .

$$X(j\omega) = \int_0^{\infty} e^{-\alpha t} e^{-j\omega t} dt = -\frac{1}{\alpha + j\omega} e^{-(\alpha + j\omega)t} \bigg|_0^{\infty} = \frac{1}{\alpha + j\omega}, \quad \alpha > 0$$

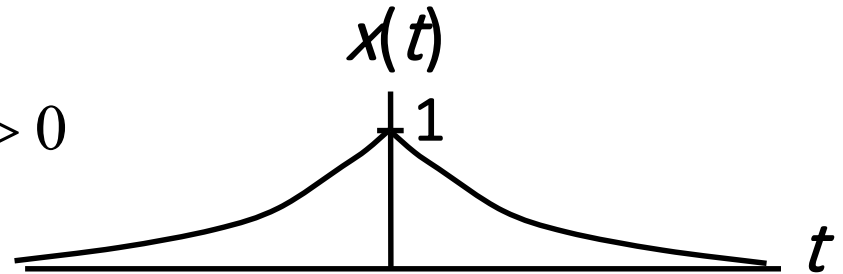
$$|X(j\omega)| = \frac{1}{\sqrt{\alpha^2 + \omega^2}}, \quad \angle X(j\omega) = -\tan^{-1}\left(\frac{\omega}{\alpha}\right)$$



## 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

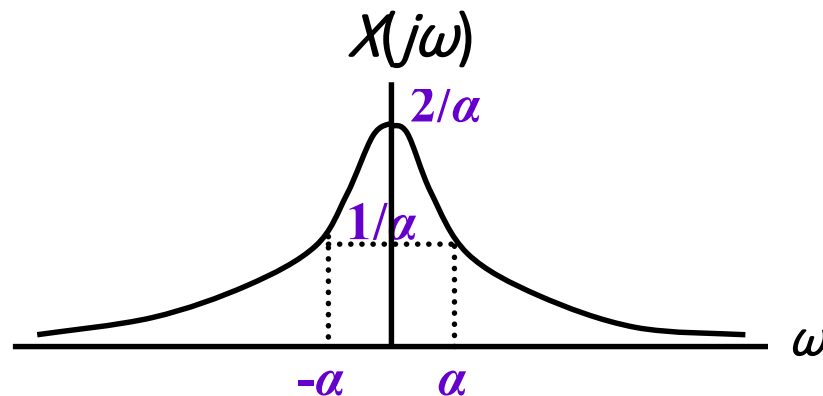
### Example 4.2

Consider the signal  $x(t) = e^{-\alpha|t|}$ ,  $\alpha > 0$



Sol: The Fourier transform of the signal is

$$\begin{aligned} X(j\omega) &= \int_{-\infty}^{\infty} e^{-\alpha|t|} e^{-j\omega t} dt = \int_{-\infty}^0 e^{\alpha t} e^{-j\omega t} dt + \int_0^{\infty} e^{-\alpha t} e^{-j\omega t} dt \\ &= \frac{1}{\alpha - j\omega} + \frac{1}{\alpha + j\omega} = \frac{2\alpha}{\alpha^2 + \omega^2} \end{aligned}$$



## 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

### Example 4.3

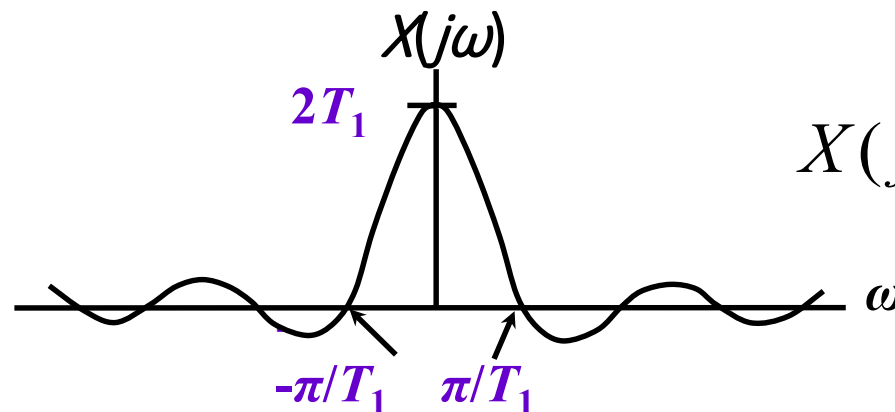
Determine the Fourier transform of the unit impulse  $x(t) = \delta(t)$

$$X(j\omega) = \int_{-\infty}^{\infty} \delta(t) e^{-j\omega t} dt = 1$$

That is, the unit impulse has a Fourier transform consisting of equal contribution at all frequencies. This spectrum is referred to as **white-spectrum**.

### Example 4.4

Consider the rectangular pulse signal  $x(t) = \begin{cases} 1, & |t| < T_1 \\ 0, & |t| > T_1 \end{cases}$



$$X(j\omega) = \int_{-T_1}^{T_1} e^{-j\omega t} dt = \frac{2 \sin \omega T_1}{\omega}$$

## 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform

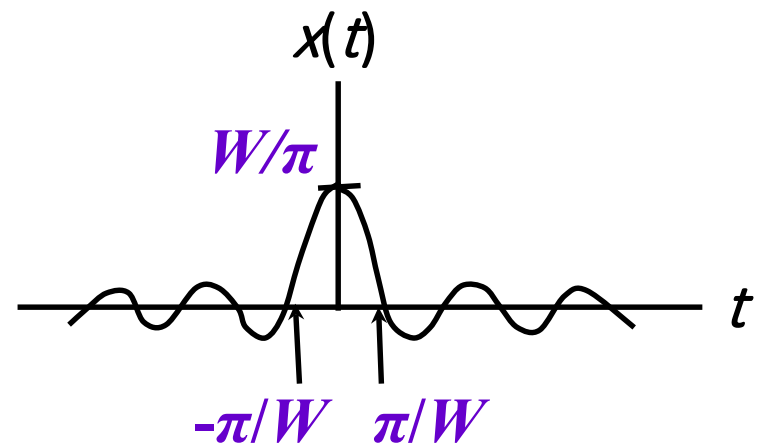
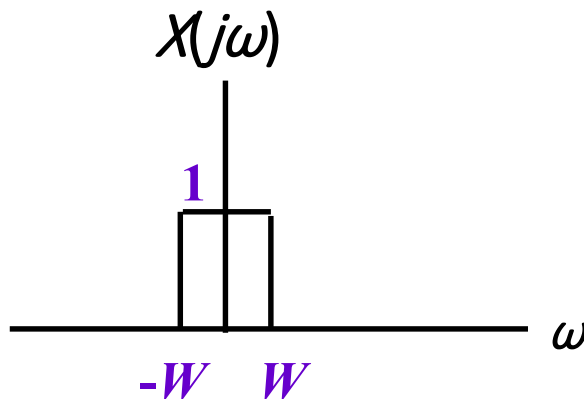
### Example 4.5

Consider the signal  $x(t)$  whose Fourier transform is

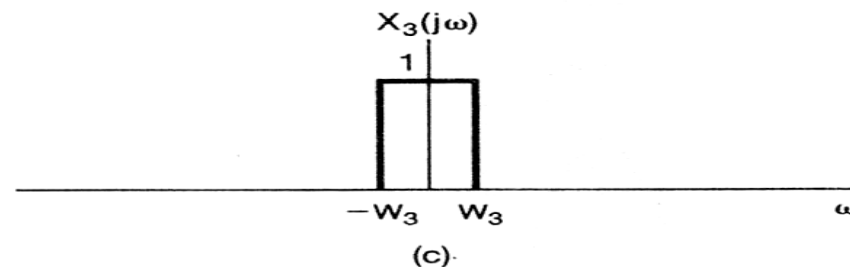
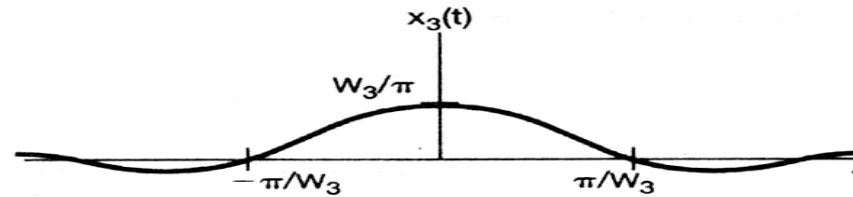
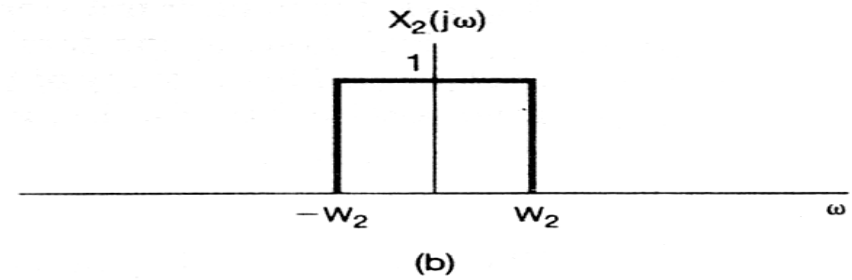
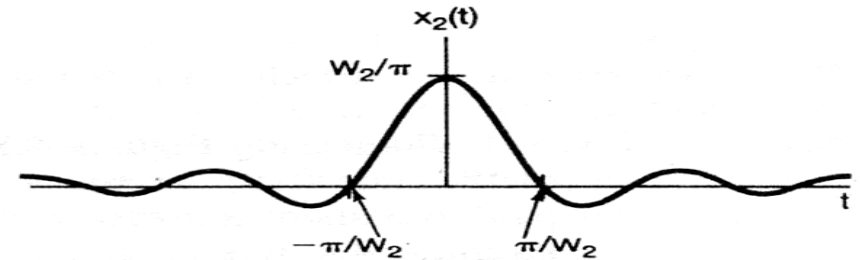
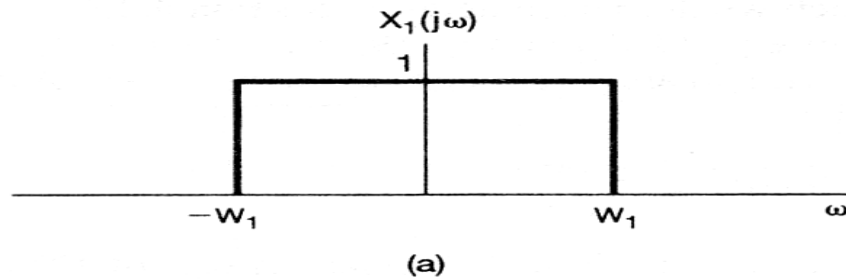
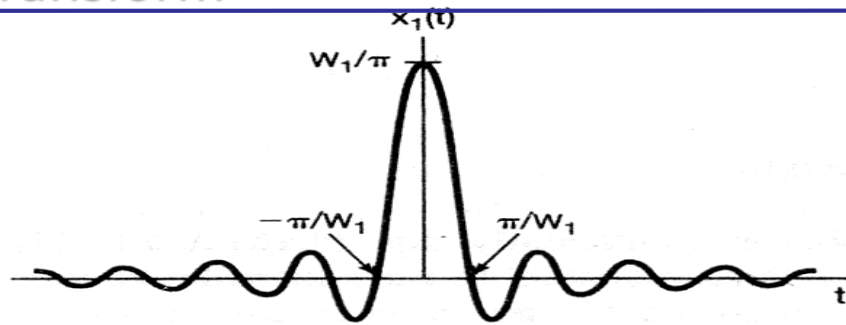
$$X(j\omega) = \begin{cases} 1, & |\omega| < W \\ 0, & |\omega| > W \end{cases}$$

Sol: Using the synthesis equation, we can determine

$$x(t) = \frac{1}{2\pi} \int_{-W}^W e^{j\omega t} d\omega = \frac{\sin Wt}{\pi t}$$



# 4.1 Representation of Aperiodic Signals: The Continuous-Time Fourier Transform



## 4.2 The Fourier Transform for Periodic Signals

$$\mathcal{F}\{e^{j\omega_0 t}\} = ?$$

From the analysis equation,

$$X(j\omega) = \int_{-\infty}^{\infty} e^{j\omega_0 t} e^{-j\omega t} dt = \frac{1}{j(\omega_0 - \omega)} e^{j(\omega_0 - \omega)t} \Bigg|_{-\infty}^{\infty}$$

Does not converge !

We have obtained  $\delta(t) \leftrightarrow 1$ , so  $\delta(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} 1 \cdot e^{j\omega t} d\omega$

$$2\pi\delta(t) = \int_{-\infty}^{\infty} 1 \cdot e^{j\omega t} d\omega$$

$$2\pi\delta(-\omega) = \int_{-\infty}^{\infty} e^{-ja\omega} da \Rightarrow 1 \xleftrightarrow{FT} 2\pi\delta(-\omega) = 2\pi\delta(\omega)$$

$$2\pi\delta(\omega_0 - \omega) = \int_{-\infty}^{\infty} e^{-jt(\omega - \omega_0)} dt = \int_{-\infty}^{\infty} e^{j\omega_0 t} e^{-j\omega t} dt \Rightarrow \mathcal{F}\{e^{j\omega_0 t}\} = 2\pi\delta(\omega - \omega_0)$$

The Fourier transform of the complex exponential signal  $e^{j\omega_0 t}$  is an impulse located at  $\omega = \omega_0$  with its area  $2\pi$ .

## 4.2 The Fourier Transform for Periodic Signals

For an arbitrary periodic signal  $x(t)$ , if it can be represented by Fourier series as

$$x(t) = \sum_{k=-\infty}^{\infty} a_k e^{jk\omega_0 t}$$

We can obtain its Fourier transform as

$$X(j\omega) = \sum_{k=-\infty}^{\infty} a_k 2\pi\delta(\omega - k\omega_0) = \sum_{k=-\infty}^{\infty} 2\pi a_k \delta(\omega - k\omega_0)$$

The Fourier transform of a periodic signal with Fourier series coefficients  $\{a_k\}$  can be interpreted as a train of impulses occurring at the harmonically related frequencies and for which the area of the impulse at the  $k$ th harmonic frequency  $k\omega_0$  is  $2\pi$  times the  $k$ th Fourier series coefficient  $a_k$ .

## 4.2 The Fourier Transform for Periodic Signals

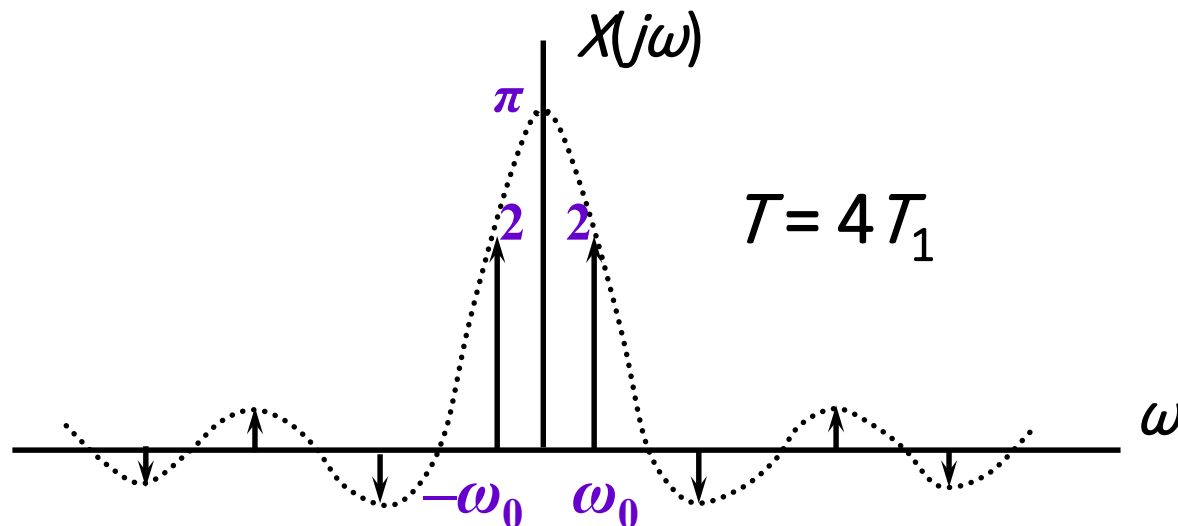
### Example 4.6

Consider the periodic square wave with FS coefficients are

$$a_k = \frac{\sin k\omega_0 T_1}{k\pi}$$

Sol: From the formula its Fourier transform is

$$X(j\omega) = \sum_{k=-\infty}^{\infty} 2\pi \cdot \frac{\sin k\omega_0 T_1}{k\pi} \delta(\omega - k\omega_0) = \sum_{k=-\infty}^{\infty} \frac{2 \sin k\omega_0 T_1}{k} \delta(\omega - k\omega_0)$$





## 4.2 The Fourier Transform for Periodic Signals

### Example 4.7

Find the Fourier Transforms of  $x_1(t) = \sin \omega_0 t$  and  $x_2(t) = \cos \omega_0 t$ .

Sol: The Fourier series coefficients for  $x_1(t)$  are

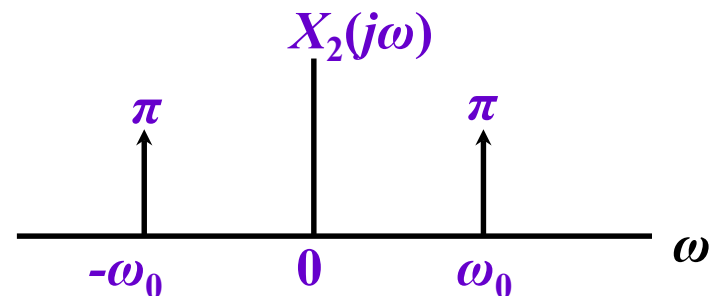
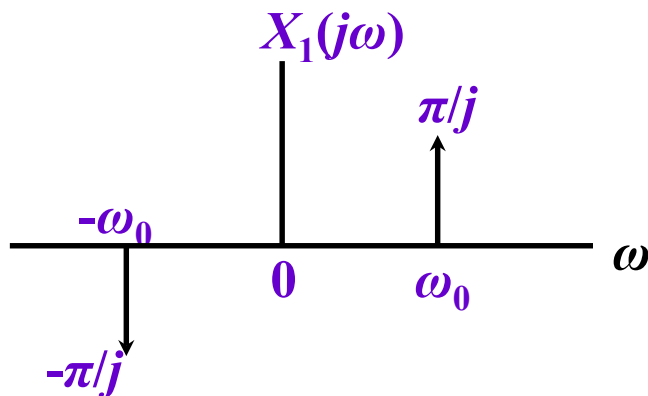
$$a_1 = \frac{1}{2j}, \quad a_{-1} = -\frac{1}{2j}, \quad a_k = 0, \quad k \neq \pm 1$$

The Fourier series coefficients for  $x_2(t)$  are

$$a_1 = a_{-1} = \frac{1}{2}, \quad a_k = 0, \quad k \neq \pm 1$$

$$\sin \omega_0 t \longleftrightarrow j\pi [\delta(\omega + \omega_0) - \delta(\omega - \omega_0)]$$

$$\cos \omega_0 t \longleftrightarrow \pi [\delta(\omega + \omega_0) + \delta(\omega - \omega_0)]$$

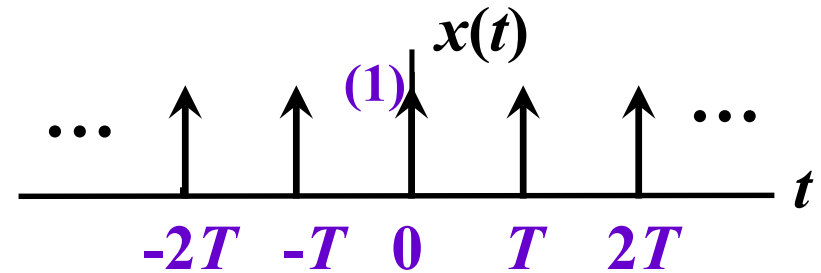


## 4.2 The Fourier Transform for Periodic Signals

### Example 4.8

Consider the impulse train

$$x(t) = \sum_{k=-\infty}^{\infty} \delta(t - kT)$$

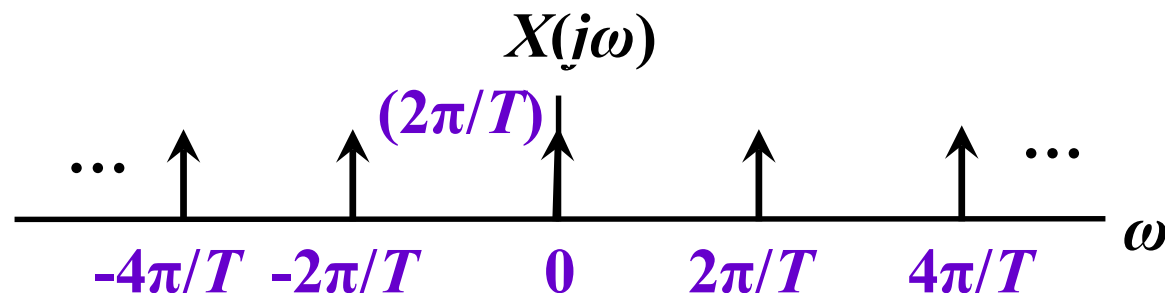


Sol: The Fourier series coefficients for this signal are

$$a_k = \frac{1}{T} \int_{-T/2}^{T/2} \delta(t) e^{-jk\omega_0 t} dt = \frac{1}{T}$$

Thus, its Fourier transform is

$$X(j\omega) = \frac{2\pi}{T} \sum_{k=-\infty}^{\infty} \delta(\omega - \frac{2k\pi}{T}) = \omega_0 \sum_{k=-\infty}^{\infty} \delta(\omega - k\omega_0)$$



## 4.3 Properties of The Continuous-Time Fourier Transform

### 4.3.1 Linearity

If  $x(t) \xleftrightarrow{FT} X(j\omega)$  and  $y(t) \xleftrightarrow{FT} Y(j\omega)$

then  $ax(t) + by(t) \xleftrightarrow{FT} aX(j\omega) + bY(j\omega)$

### 4.3.2 Time Shifting

If  $x(t) \xleftrightarrow{FT} X(j\omega)$ ,

$$\mathcal{F}\{e^{-j\omega t_0} X(j\omega)\} = \mathcal{F}\{X(j\omega)\} - \omega t_0$$

then  $x(t - t_0) \xleftrightarrow{FT} e^{-j\omega t_0} X(j\omega)$

A signal which is shifted in time does not have the magnitude of its Fourier transform altered. The effect of a time shift on a signal is to introduce into its transform a phase shift, namely,  $-\omega t_0$ .

## 4.3 Properties of The Continuous-Time Fourier Transform

### Example 4.9

Determine the Fourier transform of  $x(t)$  shown in the figure.

Sol: Since

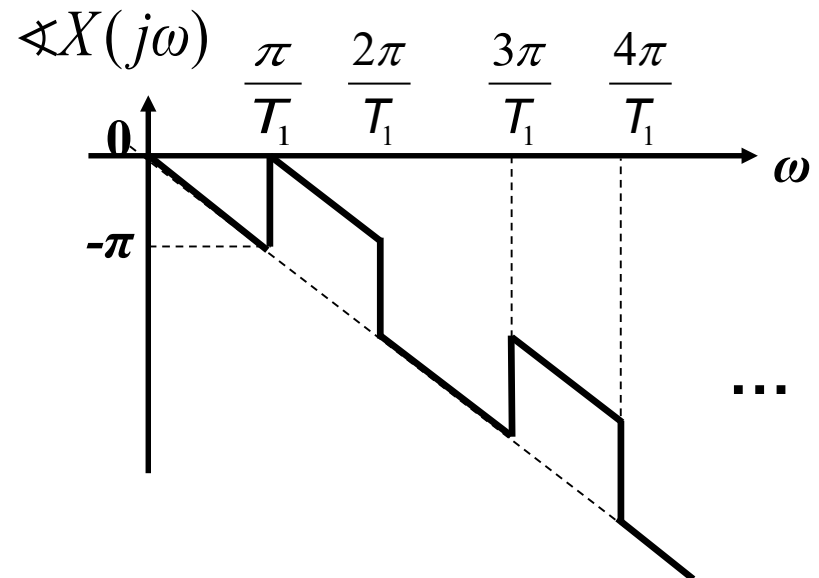
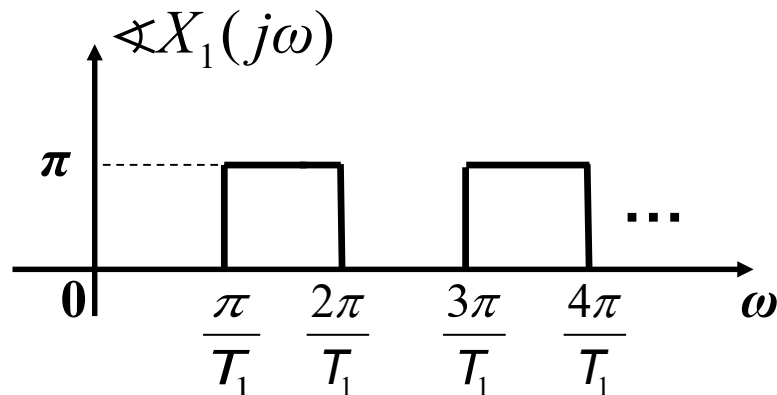
$$x_1(t) = u(t + T_1) - u(t - T_1) \leftrightarrow X_1(j\omega) = \frac{2 \sin \omega T_1}{\omega}$$

$$\text{and } x(t) = Ax_1(t - T_1)$$

From the time shifting property, we have

$$X(j\omega) = AX_1(j\omega)e^{-j\omega T_1} = \frac{2A \sin \omega T_1}{\omega} e^{-j\omega T_1}$$

$$\angle X(j\omega) = \angle X_1(j\omega) - \omega T_1$$



## 4.3 Properties of The Continuous-Time Fourier Transform

### 4.3.3 Conjugation and Conjugate Symmetry

If  $x(t) \xleftrightarrow{FT} X(j\omega)$ , then  $x^*(t) \xleftrightarrow{FT} X^*(-j\omega)$

➤ If  $x(t)$  is real, then  $X(-j\omega) = X^*(j\omega)$

$$\operatorname{Re}\{X(j\omega)\} = \operatorname{Re}\{X(-j\omega)\}, \operatorname{Im}\{X(j\omega)\} = -\operatorname{Im}\{X(-j\omega)\}$$

*even*  $|X(j\omega)| = |X(-j\omega)|$ ,  $\angle X(j\omega) = -\angle X(-j\omega)$  *odd*

➤ If  $x(t)$  is both real and even, so is  $X(j\omega)$ , i.e.,  $X(j\omega) = \operatorname{Re}\{X(j\omega)\}$

➤ If  $x(t)$  is real and odd,  $X(j\omega)$  is purely imaginary and odd, i.e.,  $X(j\omega) = j \operatorname{Im}\{X(j\omega)\}$

➤ 
$$x(t) = x_e(t) + x_o(t)$$

$$x_e(t) \xleftrightarrow{FT} \operatorname{Re}\{X(j\omega)\} \quad x_o(t) \xleftrightarrow{FT} j \operatorname{Im}\{X(j\omega)\}$$

## 4.3 Properties of The Continuous-Time Fourier Transform

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### Example 4.10

Consider again the Fourier transform evaluation of  $x(t) = e^{-\alpha|t|}$

Sol:  $e^{-\alpha|t|} = e^{-\alpha t}u(t) + e^{\alpha t}u(-t) = 2 \left[ \frac{e^{-\alpha t}u(t) + e^{\alpha t}u(-t)}{2} \right] = 2\text{Ev}\{e^{-\alpha t}u(t)\}$

and 
$$e^{-\alpha t}u(t) \xleftrightarrow{FT} \frac{1}{\alpha + j\omega}$$

From the symmetry properties of the Fourier transform, we have

$$X(j\omega) = 2 \operatorname{Re} \left\{ \frac{1}{\alpha + j\omega} \right\} = \frac{2\alpha}{\alpha^2 + \omega^2}$$

## 4.3 Properties of The Continuous-Time Fourier Transform

### 4.3.4 Differentiation and Integration

If  $x(t) \xleftrightarrow{FT} X(j\omega)$ , then  $\frac{dx(t)}{dt} \xleftrightarrow{FT} j\omega X(j\omega)$

$$\frac{d^n x(t)}{dt^n} \xleftrightarrow{FT} (j\omega)^n X(j\omega)$$

**Consequence:** Strengthening the high-frequencies in the signal.

$$\int_{-\infty}^t x(\tau) d\tau \xleftrightarrow{FT} \frac{1}{j\omega} X(j\omega) + \pi X(0) \delta(\omega)$$

**Consequence:** Strengthening the low-frequencies in the signal.

#### Example 4.11

Determine the Fourier transform of the unit step  $x(t) = u(t)$ .

*Sol:*  $u(t) = \frac{1}{2} + \frac{1}{2} \text{sgn}(t)$        $\text{sgn}(t) = \lim_{\alpha \rightarrow 0} [e^{-\alpha t} u(t) - e^{\alpha t} u(-t)] (\alpha > 0)$

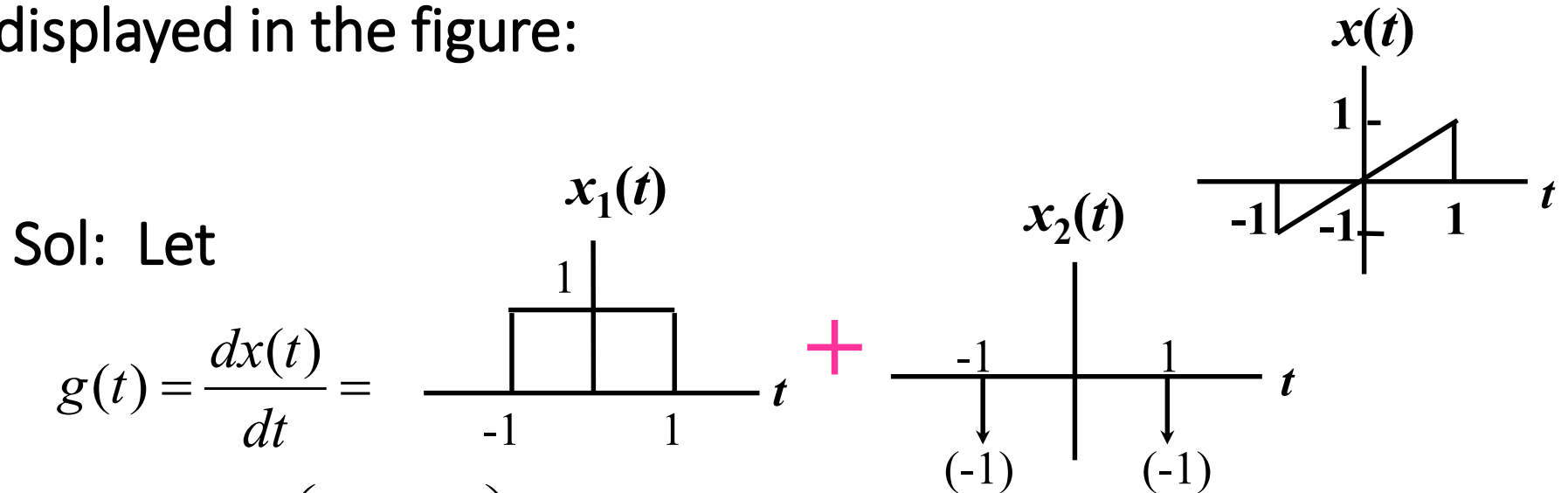
$$\mathcal{F}\{\text{sgn}(t)\} = \lim_{\alpha \rightarrow 0} \left( \frac{1}{\alpha + j\omega} - \frac{1}{\alpha - j\omega} \right) = \frac{2}{j\omega}$$

$$X(j\omega) = \frac{1}{j\omega} + \pi\delta(\omega)$$

## 4.3 Properties of The Continuous-Time Fourier Transform

### Example 4.12

Calculate the Fourier transform  $X(j\omega)$  for the signal  $x(t)$  displayed in the figure:



$$X_1(j\omega) = \left( \frac{2 \sin \omega}{\omega} \right), \quad X_2(j\omega) = -e^{j\omega} - e^{-j\omega}$$

$$G(j\omega) = j\omega X(j\omega) = \left( \frac{2 \sin \omega}{\omega} \right) - e^{j\omega} - e^{-j\omega}$$

$$X(j\omega) = \frac{2 \sin \omega}{j\omega^2} - \frac{2 \cos \omega}{j\omega}$$



## 4.3 Properties of The Continuous-Time Fourier Transform

### 4.3.5 Time and Frequency Scaling

If  $x(t) \xleftrightarrow{FT} X(j\omega)$ , then  $x(at) \xleftrightarrow{FT} \frac{1}{|a|} X\left(\frac{j\omega}{a}\right)$ ,  $a$  is real

A linear scaling in time by a factor of  $a$  corresponds to a linear scaling in frequency by a factor of  $1/a$ , and vice versa.

Specially, when  $a = -1$ , we have  $x(-t) \xleftrightarrow{FT} X(-j\omega)$

### 4.3.6 Duality

If  $x(t) \xleftrightarrow{FT} X(j\omega)$ , then  $X(jt) \xleftrightarrow{FT} 2\pi x(-\omega)$

#### Example 4.13

Using duality to find  $G(j\omega)$  of the signal  $g(t) = \frac{2}{1+t^2}$ .

Sol: From pair  $x(t) = e^{-|t|} \xleftrightarrow{FT} X(j\omega) = \frac{2}{1+\omega^2}$

By duality property, we can write

$$g(t) = \frac{2}{1+t^2} \xleftrightarrow{FT} G(j\omega) = 2\pi e^{-|-\omega|} = 2\pi e^{-|\omega|}$$

## 4.3 Properties of The Continuous-Time Fourier Transform

Duality property shows that for any Fourier transform pair there is a *dual pair* with the time and frequency variables interchanged.

Differentiation in Frequency-domain:

$$-jtx(t) \xleftrightarrow{FT} \frac{dX(j\omega)}{d\omega}$$

Integration in Frequency-domain:

$$-\frac{1}{jt}x(t) + \pi x(0)\delta(t) \xleftrightarrow{FT} \int_{-\infty}^{\omega} X(\eta)d\eta$$

Frequency Shifting:

$$e^{j\omega_0 t}x(t) \xleftrightarrow{FT} X(j(\omega - \omega_0))$$

## 4.3 Properties of The Continuous-Time Fourier Transform

### 4.3.7 Parseval's Relation

$$\int_{-\infty}^{\infty} |x(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X(j\omega)|^2 d\omega$$

*energy-density spectrum*  
(能量密度谱)

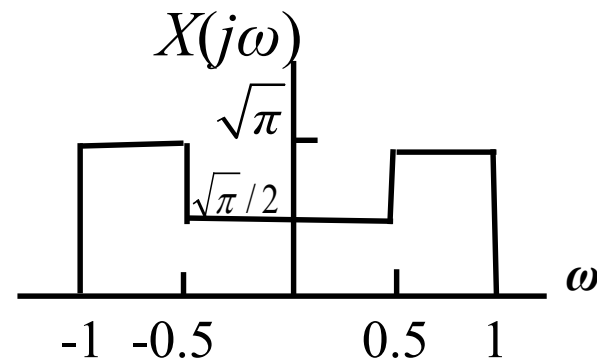
Parseval's relation says that this total energy may be determined either by computing energy per unit time (  $|x(t)|^2$  ) and integrating over all time or by computing the energy per unit frequency (  $|X(j\omega)|^2 / 2\pi$  ) and integrating over all frequencies.

## 4.3 Properties of The Continuous-Time Fourier Transform

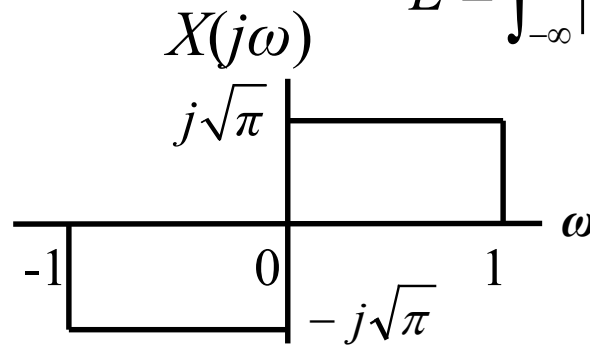
### Example 4.14

For each of the Fourier transforms shown in figures (a) and (b), evaluate the following time-domain expressions:

$$E = \int_{-\infty}^{\infty} |x(t)|^2 dt, \quad D = \left. \frac{d}{dt} x(t) \right|_{t=0}$$



(a)



(b)

Sol:  $E_a = \frac{5}{8}$      $E_b = 1$  (Parseval's Relation)

$$g(t) = \frac{d}{dt} x(t) \xleftrightarrow{FT} G(j\omega) = j\omega X(j\omega)$$

$$D = g(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} G(j\omega) d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} j\omega X(j\omega) d\omega$$

$$D_a = 0 \quad D_b = -\frac{\sqrt{\pi}}{2\pi}$$

## 4.4 The Convolution Property

Consider the convolution integral:  $y(t) = x(t) * h(t) = \int_{-\infty}^{\infty} x(\tau)h(t - \tau)d\tau$

The Fourier transform of  $y(t)$  is:

$$Y(j\omega) = \mathcal{F}\{y(t)\} = \int_{-\infty}^{\infty} \left[ \int_{-\infty}^{\infty} x(\tau)h(t - \tau)d\tau \right] e^{-j\omega t} dt$$

Interchanging the order of integration and noting that  $x(\tau)$  does not depend on  $t$ , we have  $Y(j\omega) = \int_{-\infty}^{\infty} x(\tau) \left[ \int_{-\infty}^{\infty} h(t - \tau)e^{-j\omega t} dt \right] d\tau$


$$e^{-j\omega\tau} H(j\omega)$$

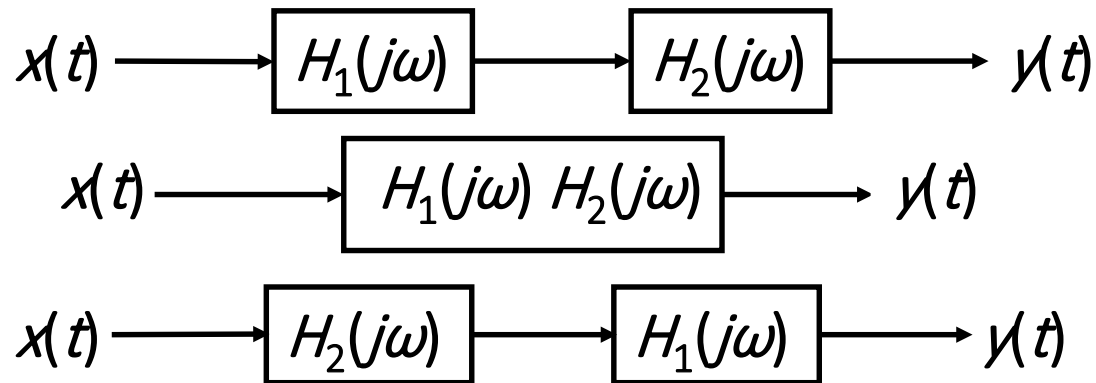
$$Y(j\omega) = \int_{-\infty}^{\infty} x(\tau)e^{-j\omega\tau} H(j\omega)d\tau = H(j\omega) \int_{-\infty}^{\infty} x(\tau)e^{-j\omega\tau} d\tau = H(j\omega)X(j\omega)$$

$$y(t) = h(t) * x(t) \xleftrightarrow{FT} Y(j\omega) = H(j\omega)X(j\omega)$$

The Fourier transform maps the convolution of two signals into the product of their Fourier transforms.  $H(j\omega)$ , the frequency response, is the Fourier transform of the impulse response  $h(t)$ . It captures the change in complex amplitude of the Fourier transform of the input at each frequency  $\omega$ .

## 4.4 The Convolution Property

➤ The frequency response  $H(j\omega)$  also can characterize an LTI system, just as its inverse transform, the unit impulse response  $h(t)$ .



Three equivalent LTI systems. Here, each LTI system is represented by  $H(j\omega)$

➤  $H(j\omega)$  **cannot** be defined for every LTI system.

➤ Since essentially all **physical or practical** signals satisfy the last two conditions in Dirichlet conditions, the condition of absolutely integrable becomes the determining factor which can guarantee the existence of the Fourier transform  $H(j\omega)$  of  $h(t)$ . That is, only **a stable LTI system has a frequency response  $H(j\omega)$** .

## 4.4 The Convolution Property

### Example 4.15

Consider an integrator — that is, an LTI system specified by the equation

$$y(t) = \int_{-\infty}^t x(\tau) d\tau$$

Sol: Since  $y(t) = x(t) * u(t) = \int_{-\infty}^{\infty} x(\tau)u(t-\tau)d\tau = \int_{-\infty}^t x(\tau)d\tau$

So the impulse response for this system is the unit step  $u(t)$ .

The frequency response of the system is  $H(j\omega) = \frac{1}{j\omega} + \pi\delta(\omega)$

Using the convolution property, we have

$$Y(j\omega) = H(j\omega)X(j\omega)$$

$$= \frac{1}{j\omega} X(j\omega) + \pi X(j\omega)\delta(\omega)$$

$$= \frac{1}{j\omega} X(j\omega) + \pi X(0)\delta(\omega)$$

## 4.4 The Convolution Property

### Example 4.16

Find the response of an LTI system with  $h(t) = e^{-at}u(t)$ ,  $a > 0$  to the input signal  $x(t) = e^{-bt}u(t)$ ,  $b > 0$ .

Sol:  $X(j\omega) = \frac{1}{b + j\omega}$ ,  $H(j\omega) = \frac{1}{a + j\omega} \Rightarrow Y(j\omega) = \frac{1}{(a + j\omega)(b + j\omega)}$

Expand  $Y(j\omega)$  in a *partial-fraction expansion* (部分分式展开法).

When  $b \neq a$ , let  $Y(j\omega) = \frac{A}{(a + j\omega)} + \frac{B}{(b + j\omega)} = \frac{1}{b - a} \left[ \frac{1}{a + j\omega} - \frac{1}{b + j\omega} \right]$

$$A = (a + j\omega)Y(j\omega) \Big|_{j\omega = -a} = \frac{1}{b + j\omega} \Big|_{j\omega = -a} = \frac{1}{b - a}$$

$$B = (b + j\omega)Y(j\omega) \Big|_{j\omega = -b} = \frac{1}{a + j\omega} \Big|_{j\omega = -b} = \frac{-1}{b - a}$$

$$y(t) = \frac{1}{b - a} \left[ e^{-at}u(t) - e^{-bt}u(t) \right] \quad b \neq a$$



## 4.4 The Convolution Property

$$\text{When } b = a, \quad Y(j\omega) = \frac{1}{(a + j\omega)^2} = j \frac{d}{d\omega} \left[ \frac{1}{(a + j\omega)} \right]$$

From the differentiation in the frequency-domain property,

$$e^{-at}u(t) \xleftrightarrow{FT} \frac{1}{a + j\omega}$$

$$te^{-at}u(t) \xleftrightarrow{FT} j \frac{d}{d\omega} \left[ \frac{1}{a + j\omega} \right] = \frac{1}{(a + j\omega)^2}$$

$$\text{Consequently,} \quad y(t) = te^{-at}u(t) \quad b = a$$

## 4.4 The Convolution Property

### Example 4.17

Determine the response of an ideal low-pass filter to an input signal  $x(t)$  that has the form of a *sinc* function,  $x(t) = \frac{\sin \omega_i t}{\pi t}$

Sol: The impulse response of the ideal low-pass filter is of a similar form:  $h(t) = \frac{\sin \omega_c t}{\pi t}$

$$X(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_i \\ 0 & \text{elsewhere} \end{cases}, \quad H(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & \text{elsewhere} \end{cases}$$

Therefore,  $Y(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_0 \\ 0 & \text{elsewhere} \end{cases}$  where  $\omega_0 = \min(\omega_i, \omega_c)$ .

Finally, the inverse Fourier transform of  $Y(j\omega)$  is given by

$$y(t) = \begin{cases} \frac{\sin \omega_c t}{\pi t} = h(t) & \text{if } \omega_c \leq \omega_i \\ \frac{\sin \omega_i t}{\pi t} = x(t) & \text{if } \omega_i \leq \omega_c \end{cases}$$

## 4.5 The Multiplication Property

$$r(t) = s(t)p(t) \xleftrightarrow{FT} R(j\omega) = \frac{1}{2\pi} [S(j\omega) * P(j\omega)]$$

**amplitude modulation property (幅度调制定理)**

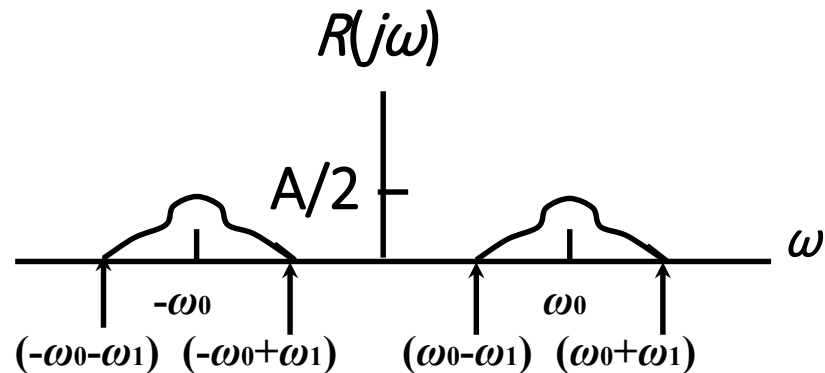
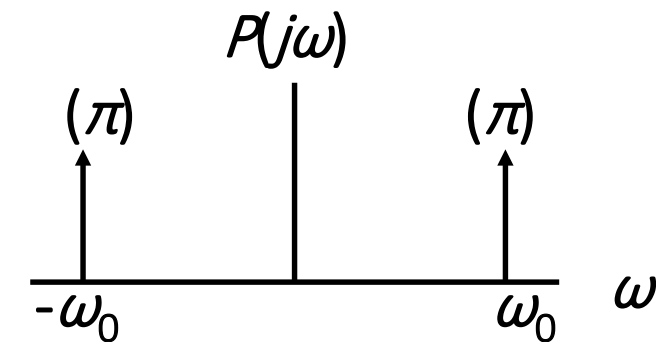
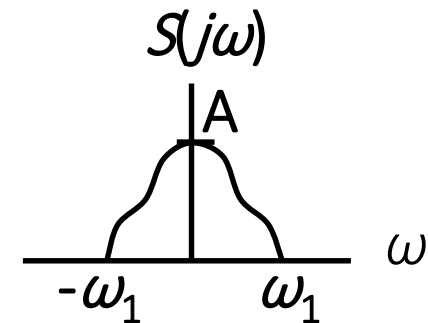
Example 4.18

Let  $s(t)$  be a signal whose spectrum  $S(j\omega)$  is depicted in the following Figure. Also, consider the signal  $p(t) = \cos \omega_0 t$ ,

Sol: Since  $P(j\omega) = \pi\delta(\omega - \omega_0) + \pi\delta(\omega + \omega_0)$

From the multiplication property:

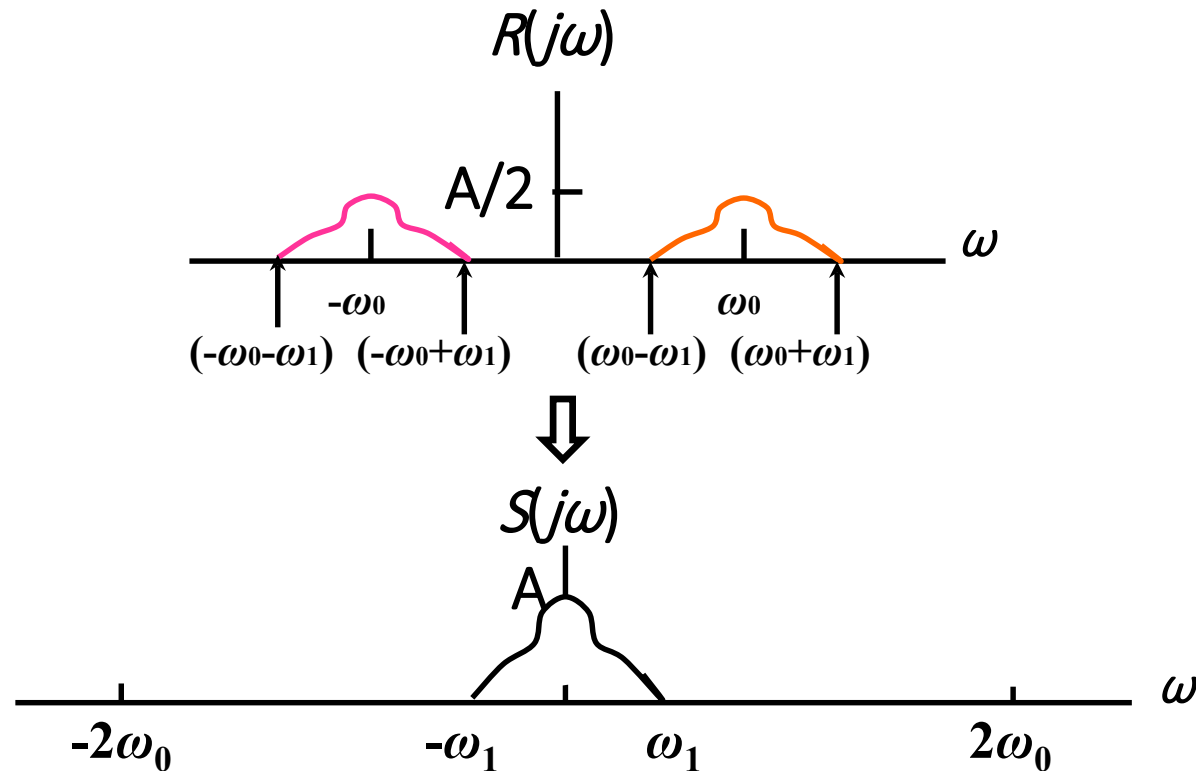
$$R(j\omega) = \frac{1}{2\pi} S(j\omega) * P(j\omega) = \frac{1}{2} S(j(\omega - \omega_0)) + \frac{1}{2} S(j(\omega + \omega_0))$$



## 4.5 The Multiplication Property

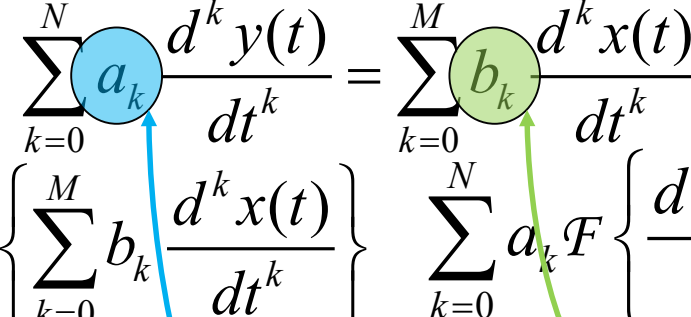
### Example 4.19

Let us consider  $r(t)$  as obtained in Example 4.18, and let  $g(t) = r(t)p(t)$ , we will show how to recover the modulated signal  $s(t)$ .



## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations

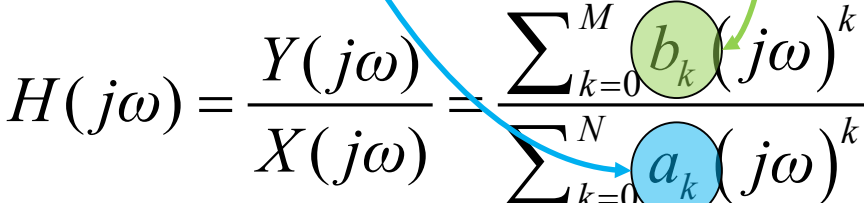
For a *stable* LTI system which is described by a linear constant-coefficient differential equation of the form :

$$\sum_{k=0}^N a_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^M b_k \frac{d^k x(t)}{dt^k}$$
$$\mathcal{F} \left\{ \sum_{k=0}^N a_k \frac{d^k y(t)}{dt^k} \right\} = \mathcal{F} \left\{ \sum_{k=0}^M b_k \frac{d^k x(t)}{dt^k} \right\} \quad \sum_{k=0}^N a_k \mathcal{F} \left\{ \frac{d^k y(t)}{dt^k} \right\} = \sum_{k=0}^M b_k \mathcal{F} \left\{ \frac{d^k x(t)}{dt^k} \right\}$$


$$\sum_{k=0}^N a_k (j\omega)^k Y(j\omega) = \sum_{k=0}^M b_k (j\omega)^k X(j\omega) \quad \text{(differentiation)}$$

Equivalently,

$$Y(j\omega) \left[ \sum_{k=0}^N a_k (j\omega)^k \right] = X(j\omega) \left[ \sum_{k=0}^M b_k (j\omega)^k \right]$$

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{\sum_{k=0}^M b_k (j\omega)^k}{\sum_{k=0}^N a_k (j\omega)^k} \quad \text{(Convolution)}$$


➤  $H(j\omega)$  is a ratio of polynomials in  $(j\omega)$ , so it is a rational function.

## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations

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### Example 4.20

Consider a stable LTI system that is characterized by the differential equation  $\frac{d^2 y(t)}{dt^2} + 4\frac{dy(t)}{dt} + 3y(t) = \frac{dx(t)}{dt} + 2x(t)$ , determine its impulse response.

Sol: The frequency response is

$$H(j\omega) = \frac{(j\omega) + 2}{(j\omega)^2 + 4(j\omega) + 3}$$

To determine the corresponding impulse response, we use the method of partial-fraction expansion:

$$H(j\omega) = \frac{\frac{1}{2}}{j\omega + 1} + \frac{\frac{1}{2}}{j\omega + 3}$$

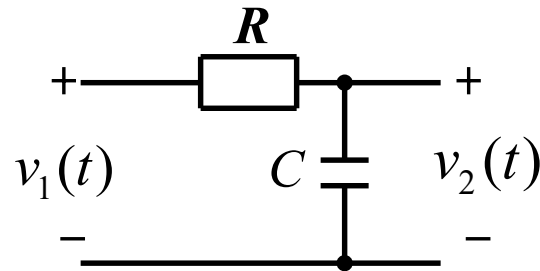
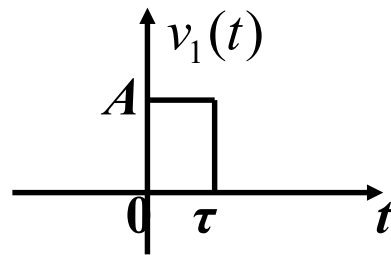
Thus, the impulse response is

$$h(t) = \frac{1}{2}e^{-t}u(t) + \frac{1}{2}e^{-3t}u(t)$$

## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations

### Example 4.21

A RC circuit is as follows,  $v_1(t)$  is the input, determine  $v_2(t)$ .



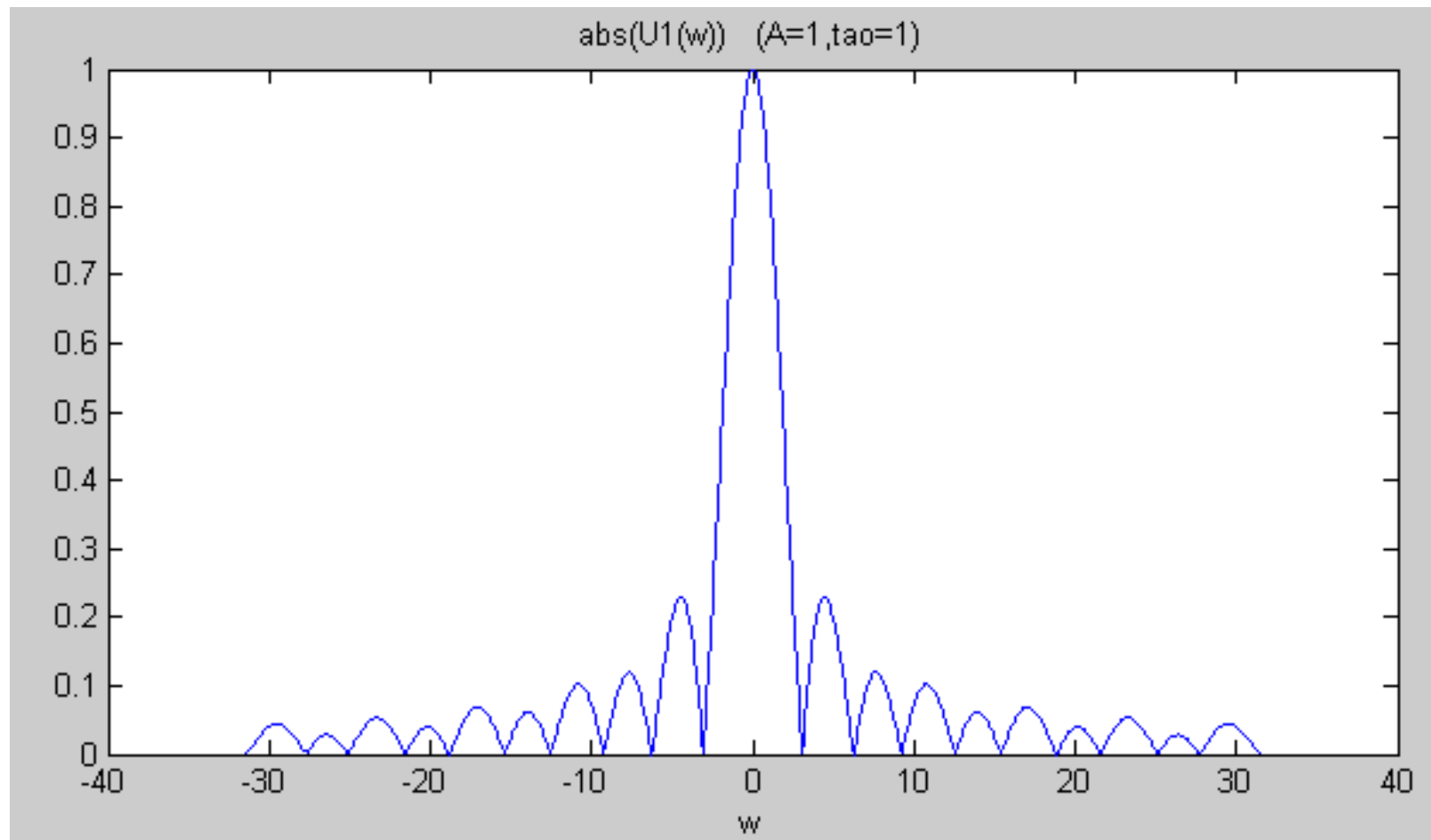
Sol: 1) Compute  $V_1(j\omega)$

$$v_1(t) = A[u(t) - u(t - \tau)]$$

$$V_1(j\omega) = A\left[\pi\delta(\omega) + \frac{1}{j\omega} - \pi\delta(\omega)e^{-j\omega\tau} - \frac{e^{-j\omega\tau}}{j\omega}\right]$$

$$= \frac{A}{j\omega}(1 - e^{-j\omega\tau}) = \frac{2A}{\omega} \sin \frac{\omega\tau}{2} e^{-j\frac{\omega\tau}{2}} = A\tau \text{Sa}\left(\frac{\omega\tau}{2}\right) e^{-j\frac{\omega\tau}{2}}$$

## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations





## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations

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2) Compute  $H(j\omega)$

$$H(j\omega) = \frac{V_2(j\omega)}{V_1(j\omega)} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{1}{1 + j\omega RC} = \frac{\frac{1}{RC}}{\frac{1}{RC} + j\omega}$$

Let  $\frac{1}{RC} = \alpha = \frac{1}{\tau_0}$

$$H(j\omega) = \frac{\alpha}{\alpha + j\omega} = \frac{\alpha}{\sqrt{\alpha^2 + \omega^2}} e^{-j \arctan \frac{\omega}{\alpha}}$$

## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations

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### 3) Compute $V_2(j\omega)$

$$V_2(j\omega) = V_1(j\omega)H(j\omega)$$

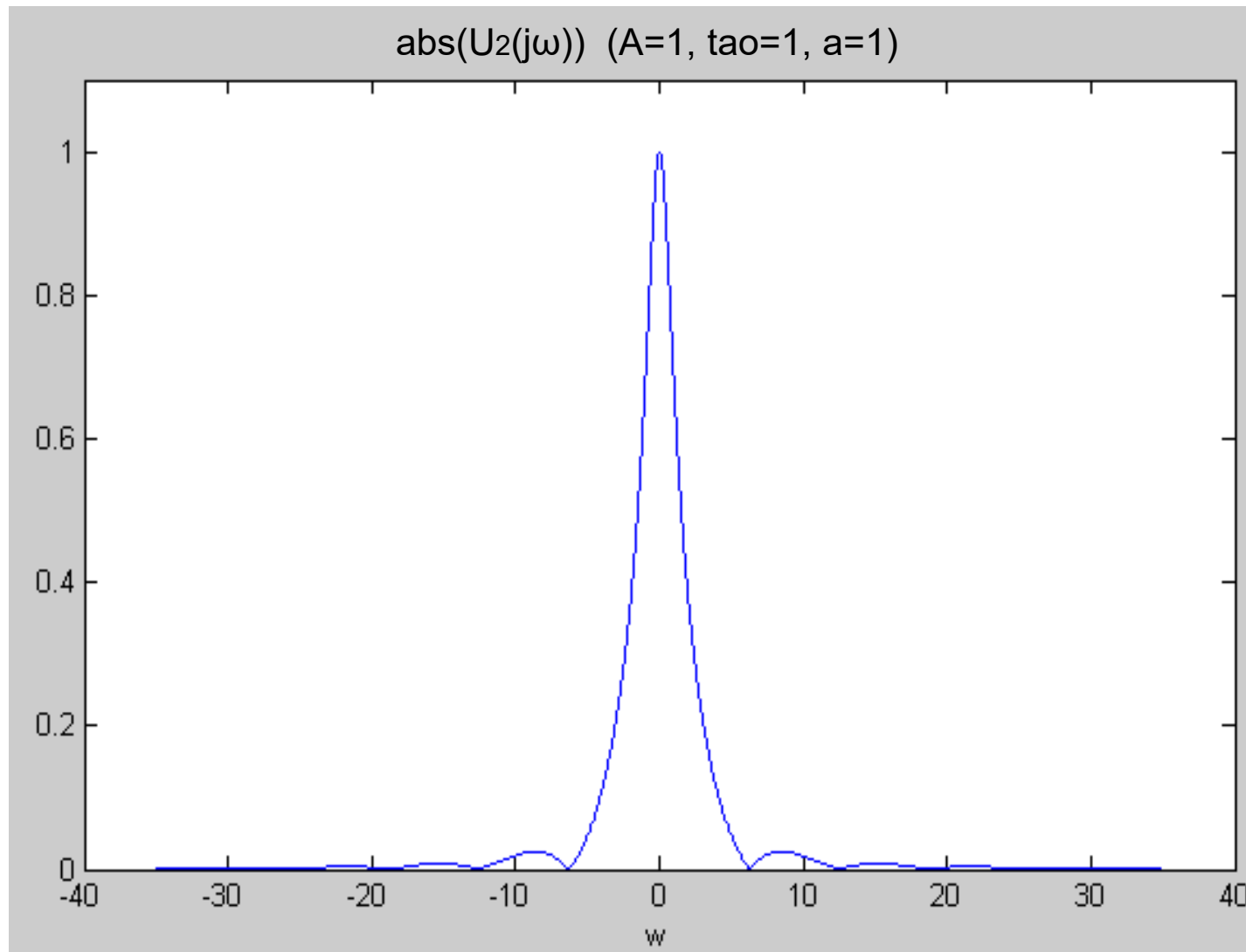
$$= A\tau \text{Sa}\left(\frac{\omega\tau}{2}\right)e^{-j\frac{\omega\tau}{2}} \cdot \frac{\alpha}{\sqrt{\alpha^2 + \omega^2}} e^{-j\arctan\frac{\omega}{\alpha}}$$

$$= \frac{\alpha A\tau}{\sqrt{\alpha^2 + \omega^2}} \text{Sa}\left(\frac{\omega\tau}{2}\right)e^{-j\left(\frac{\omega\tau}{2} + \arctan\frac{\omega}{\alpha}\right)}$$

$$|V_2(j\omega)| = \frac{\alpha A\tau}{\sqrt{\alpha^2 + \omega^2}} \left| \text{Sa}\left(\frac{\omega\tau}{2}\right) \right| = \frac{2\alpha A \left| \sin\left(\frac{\omega\tau}{2}\right) \right|}{\omega\sqrt{\alpha^2 + \omega^2}}$$

$$\varphi_2(\omega) = \begin{cases} -\left(\frac{\omega\tau}{2} + \arctan\frac{\omega}{\alpha}\right), \sin\left(\frac{\omega\tau}{2}\right) > 0 \\ \pm\pi - \left(\frac{\omega\tau}{2} + \arctan\frac{\omega}{\alpha}\right), \sin\left(\frac{\omega\tau}{2}\right) < 0 \end{cases}$$

## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations



## 4.6 Systems Characterized By Linear Constant Coefficient Differential Equations

4) Compute  $v_2(t) = \mathcal{F}^{-1}[V_2(j\omega)]$

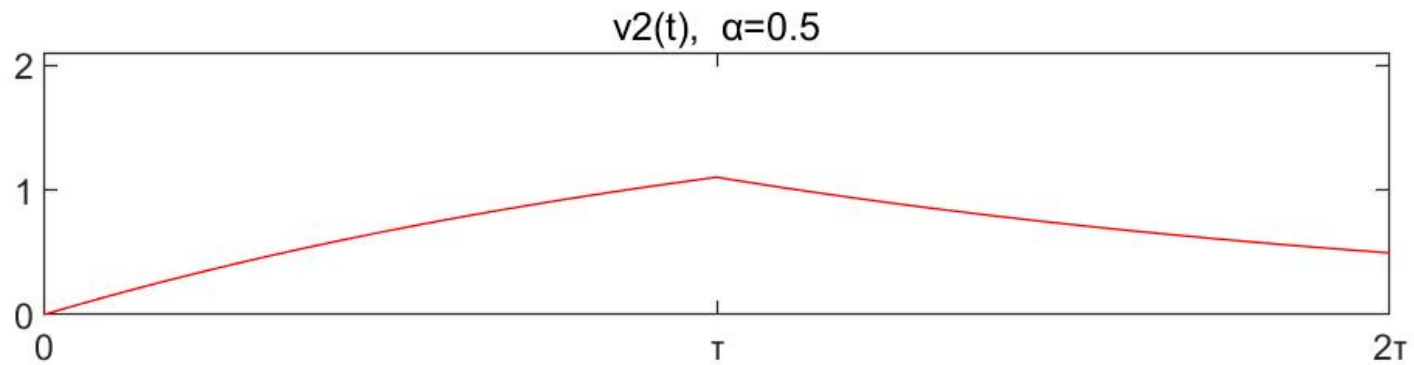
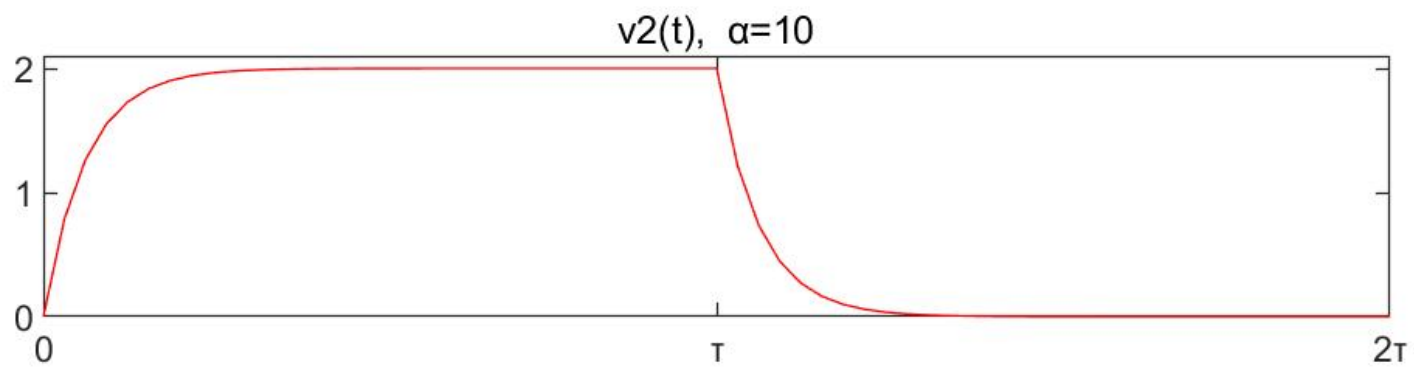
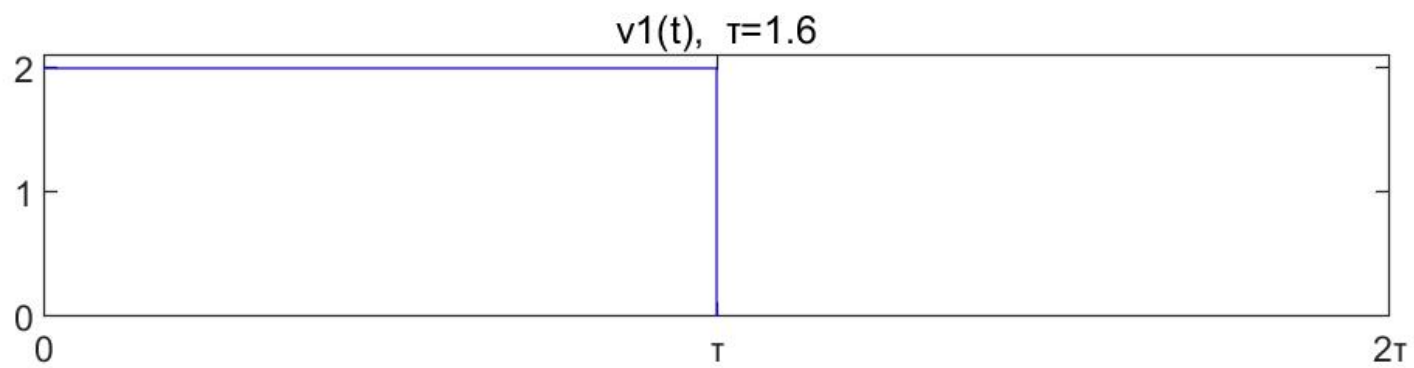
$$V_1(j\omega) = \frac{A}{j\omega}(1 - e^{-j\omega\tau})$$

$$\begin{aligned} V_2(j\omega) &= A(1 - e^{-j\omega\tau}) \frac{\alpha}{j\omega(\alpha + j\omega)} = A(1 - e^{-j\omega\tau}) \left( \frac{1}{j\omega} - \frac{1}{j\omega + \alpha} \right) \\ &= \frac{A(1 - e^{-j\omega\tau})}{j\omega} - \frac{A}{\alpha + j\omega} + \frac{A}{\alpha + j\omega} e^{-j\omega\tau} \end{aligned}$$

$$\begin{aligned} \therefore v_2(t) &= A[u(t) - u(t - \tau)] - Ae^{-\alpha t}u(t) + Ae^{-\alpha(t-\tau)}u(t - \tau) \\ &= A(1 - e^{-\alpha t})u(t) - A[1 - e^{-\alpha(t-\tau)}]u(t - \tau) \end{aligned}$$

Rising and falling characteristics in time domain:

$v_1(t) : t = 0, \tau$  Change very fast (jump) — **Abundant high frequencies**  
 $v_2(t) : t = 0, \tau$  Change slowly, need a period of time to rise or fall  
— **High frequencies are attenuated**



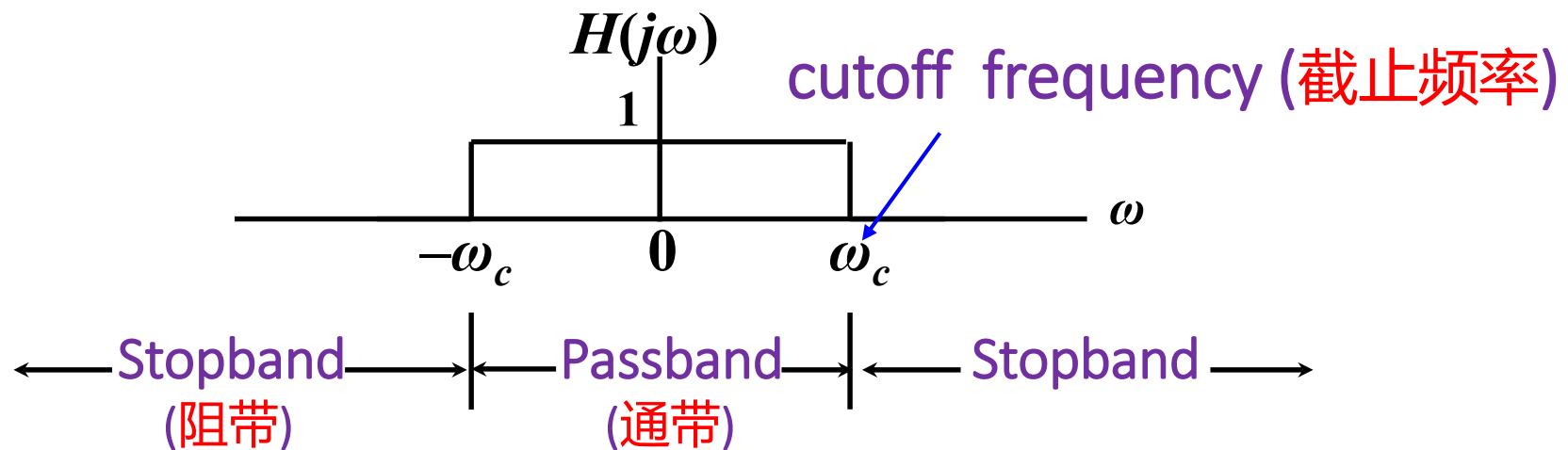
## 4.7 Frequency-Selective Filters

### 4.7.1 Introduction to Ideal Frequency-Selective Filters

- *Filtering*: a process in which the relative amplitudes of the frequency components in a signal are changed or some frequency components are eliminated entirely.
- *Frequency-selective filters* (频选滤波器): systems that are designed to pass some frequencies essentially undistorted and significantly attenuate or eliminate others.
- Types of frequency-selective filters
  - ✓ low-pass filter (低通滤波器)
  - ✓ high-pass filter (高通滤波器)
  - ✓ band-pass filter (带通滤波器)
  - ✓ band-stop filter (带阻滤波器)

## 4.7 Frequency-Selective Filters

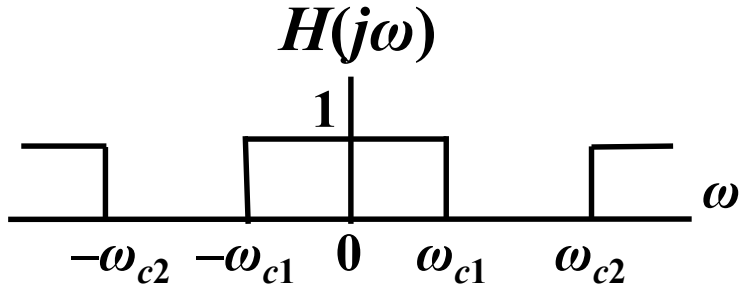
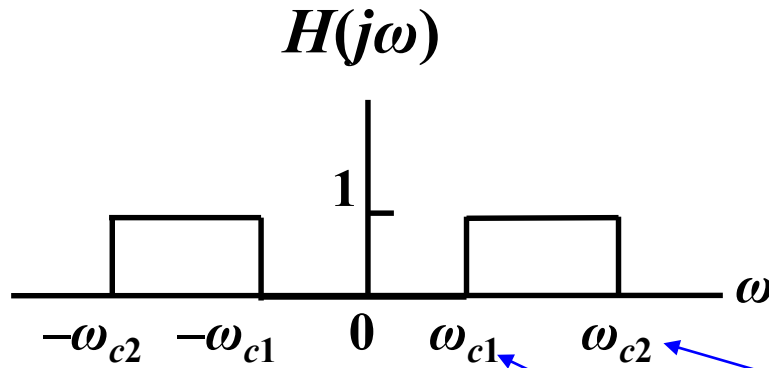
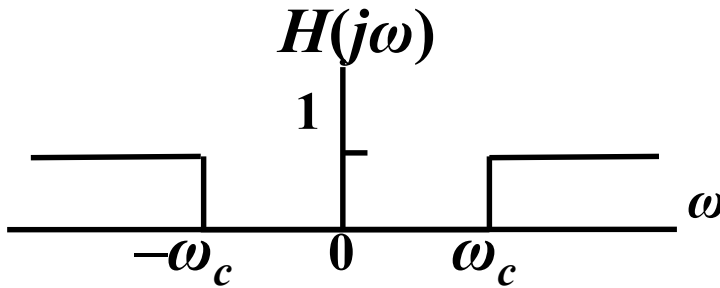
The frequency responses of a *zero-phase ideal* low-pass filter, a *zero-phase ideal* high-pass filter, a *zero-phase ideal* band-pass filter and a *zero-phase ideal* band-stop filter are illustrated in the following figures, respectively:



$$H(j\omega) = \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & |\omega| > \omega_c \end{cases}$$

# 4.7 Frequency-Selective Filters

$$H(j\omega) = \begin{cases} 1, & |\omega| \geq \omega_c \\ 0, & |\omega| < \omega_c \end{cases}$$



$$H(j\omega) = \begin{cases} 1, & \omega_{c_2} \geq |\omega| \geq \omega_{c_1} \\ 0, & |\omega| < \omega_{c_1} \text{ or } |\omega| > \omega_{c_2} \end{cases}$$

upper cutoff frequency  
(上截止频率)  
lower cutoff frequency  
(下截止频率)



## 4.7 Frequency-Selective Filters

- The impulse response of the ideal low-pass filter is:

$$h(t) = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega t} d\omega = \frac{\sin \omega_c t}{\pi t}$$

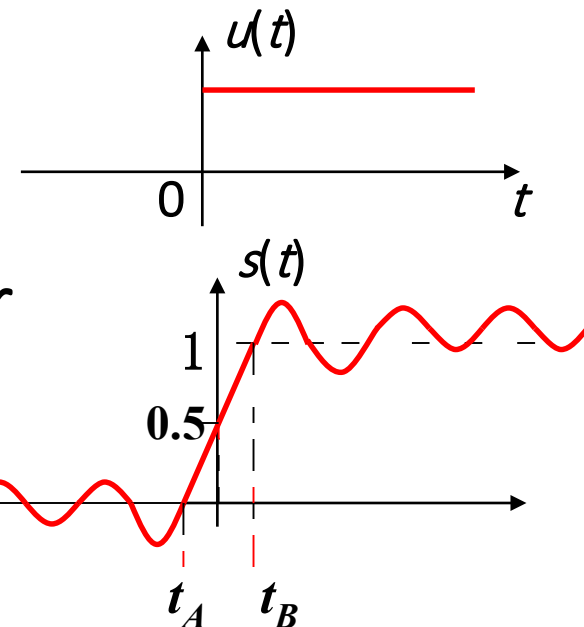
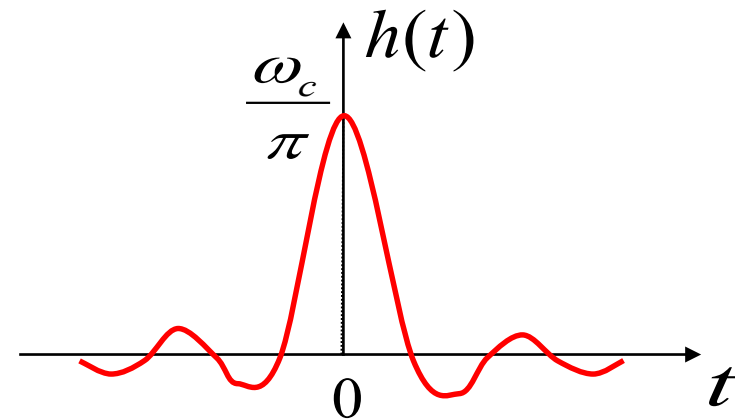
- The step response is:

$$s(t) = \frac{1}{2} + \frac{1}{\pi} \text{Si}(\omega_c t)$$

Here,  $\text{Si}(\omega_c t) = \int_0^{\omega_c t} \frac{\sin x}{x} dx$

Different from the input signal —  $u(t)$ , output signal  $s(t)$  needs a period of time to rise from 0 to 1, because frequencies higher than  $\omega_c$  in  $u(t)$  are rejected. And the period

$$t_r = t_B - t_A = \frac{3.84}{\omega_c}$$



## 4.7 Frequency-Selective Filters

- The frequency response of the ideal high-pass filter can be represented in terms of the frequency response of the low-pass filter as:

$$H_h(j\omega) = \begin{cases} 1, & |\omega| \geq \omega_c \\ 0, & |\omega| < \omega_c \end{cases} = 1 - \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & |\omega| > \omega_c \end{cases} = 1 - H_l(j\omega)$$

Thus, the impulse response of the ideal high-pass filter is:

$$h(t) = \delta(t) - \frac{\sin \omega_c t}{\pi t}$$

Clearly  $h(t)$  is not causal, so the ideal high-pass filter **cannot be implemented**.

## 4.7 Frequency-Selective Filters

### 4.7.2 Realizable Systems and Binding Characteristic of $H(j\omega)$

- A physically realizable system must have its impulse response  $h(t)$  satisfy  $h(t) = h(t) \cdot u(t)$  (**sufficient and necessary condition**) – Time Domain condition
- Imposing causality on the system restricts the  $H(j\omega)$  in significant ways. The **Paley-Wiener Criterion** says if  $|H(j\omega)|^2$  is integrable, i.e.,  $\int_{-\infty}^{\infty} |H(j\omega)|^2 d\omega < \infty$ , it can be proved that the **necessary condition** for a realizable  $|H(j\omega)|$  (causal system) is:

$$\int_{-\infty}^{\infty} \frac{|\ln |H(j\omega)||}{1 + \omega^2} d\omega < \infty \quad (\text{I})$$

- ✓ To satisfy above condition,  $H(j\omega)$  cannot be zero in any band of frequencies (although it can be zero at a finite number of frequencies).

## 4.7 Frequency-Selective Filters

✓ The decay rate of  $|H(j\omega)|$  cannot be greater than that of exponentials.

Consider the causality of system with  $|H(j\omega)| = e^{-|\omega|}$ ,

$$\begin{aligned}\lim_{B \rightarrow \infty} \int_{-B}^B \frac{|\ln |H(j\omega)||}{1 + \omega^2} d\omega &= \lim_{B \rightarrow \infty} \int_{-B}^B \frac{|\ln e^{-|\omega|}|}{1 + \omega^2} d\omega = \lim_{B \rightarrow \infty} \int_{-B}^B \frac{|\omega|}{1 + \omega^2} d\omega \\ &= 2 \times \lim_{B \rightarrow \infty} \int_0^B \frac{\omega}{1 + \omega^2} d\omega = \lim_{B \rightarrow \infty} \ln(1 + \omega^2) \Big|_0^B \rightarrow \infty\end{aligned}$$

This shows that exponential magnitude response  $|H(j\omega)| = e^{-|\omega|}$  does not satisfy the equation (I). Consequently, a system with a magnitude response function which decays faster than exponential must be non-causal so that cannot be implemented.

□ It can be proved that a magnitude response function  $|H(j\omega)|$  that is composed of rational polynomials can satisfy equation (I).

## 4.7 Frequency-Selective Filters

➤ Because of the causality restriction ( $h(t) = h(t) \cdot u(t)$ ) there is some kind of mutually binding character between the real and imaginary parts or the magnitude and phase of  $H(j\omega)$ . Specifically, if let

$$H(j\omega) = H_R(j\omega) + jH_I(j\omega)$$

then

$$H_R(j\omega) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{H_I(j\eta)}{\omega - \eta} d\eta \quad (\text{II})$$

$$H_I(j\omega) = -\frac{1}{\pi} \int_{-\infty}^{\infty} \frac{H_R(j\eta)}{\omega - \eta} d\eta \quad (\text{III})$$

Equations (II) and (III) are referred to as *Hilbert Transform pair*.

*Conclusion*: The real and imaginary parts of the transform of a real, causal impulse response  $h(t)$  can be determined from one another using the *Hilbert Transform*. (Problems 4.47 and 4.48) So do the phase and logarithm of the magnitude of  $H(j\omega)$ .

## 4.7 Frequency-Selective Filters

### 4.7.3 A Real Simple $RC$ Low-pass Filter with rational $H(j\omega)$

Input: source voltage  $v_s(t)$ ;

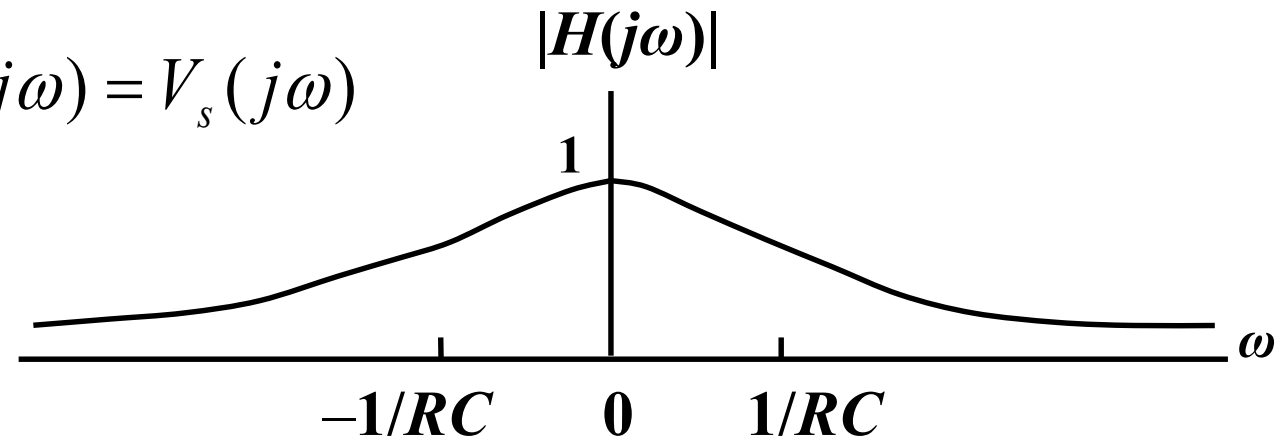
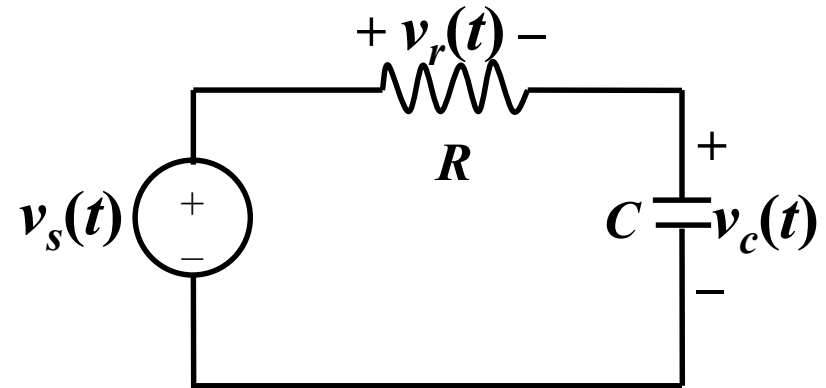
Output: capacitor voltage  $v_c(t)$

$$RC \frac{dv_c(t)}{dt} + v_c(t) = v_s(t)$$

$$RCj\omega V_c(j\omega) + V_c(j\omega) = V_s(j\omega)$$

$$H_{lp}(j\omega) = \frac{V_c(j\omega)}{V_s(j\omega)}$$

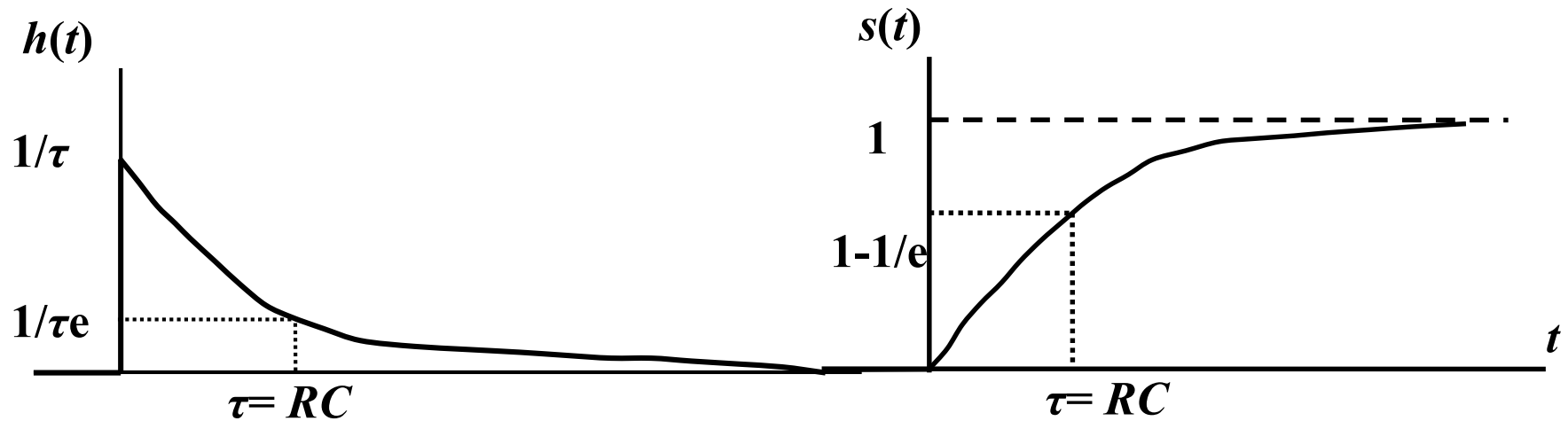
$$= \frac{1}{1 + RCj\omega} = \frac{1/RC}{1/RC + j\omega}$$



## 4.7 Frequency-Selective Filters

$$h(t) = \frac{1}{RC} e^{-t/RC} u(t)$$

$$s(t) = \left[1 - e^{-t/RC}\right] u(t)$$



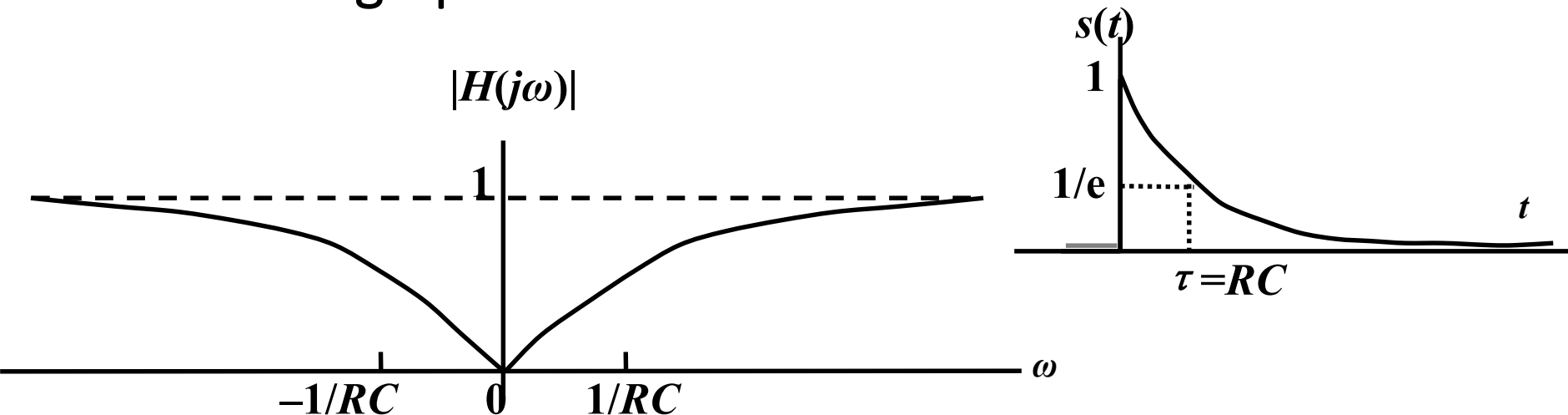
## 4.7 Frequency-Selective Filters

### 4.7.4 A Real Simple $RC$ High-pass Filter with rational $H(j\omega)$

Input: source voltage  $v_s(t)$ ; Output: resistor voltage  $v_r(t)$

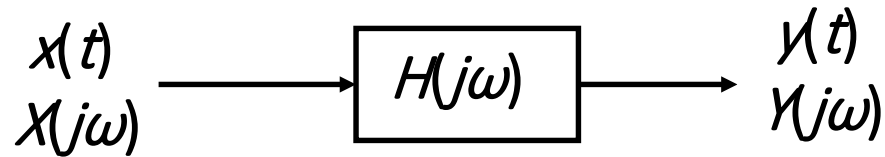
$$RC \frac{dv_r(t)}{dt} + v_r(t) = RC \frac{dv_s(t)}{dt}$$
$$H_{hp}(j\omega) = \frac{j\omega RC}{1 + j\omega RC} = 1 - \frac{1/RC}{1/RC + j\omega}$$
$$s(t) = e^{-t/RC} u(t)$$

Non-ideal high-pass filter





## 4.8 Transmission without Distortion



If the waveform of  $y(t)$  is different from that of  $x(t)$ , distortion occurs.

➤ Linear systems can only introduce *linear distortion*, in which there isn't new frequencies generated.

➤ We can see from  $Y(j\omega) = |H(j\omega)| |X(j\omega)| e^{j(\arg H(j\omega) + \arg X(j\omega))}$  that linear distortions include *magnitude distortion* and *phase distortion*.

In the case of  $y(t) = Kx(t - t_0)$ ,  $x(t)$  is transmitted without distortion.

Applying Fourier transform we have  $Y(j\omega) = KX(j\omega)e^{-j\omega t_0}$

$$H(j\omega) = Ke^{-j\omega t_0} \quad \text{or} \quad \begin{cases} |H(j\omega)| = K \\ \angle H(j\omega) = -\omega t_0 \end{cases}$$

## 4.8 Transmission without Distortion

Suppose  $x(t) = E_1 \sin \omega_0 t + E_2 \sin 2\omega_0 t$

Then

$$\begin{aligned} y(t) &= KE_1 \sin(\omega_0 t + \varphi_1) + KE_2 \sin(2\omega_0 t + \varphi_2) \\ &= KE_1 \sin \omega_0 \left(t + \frac{\varphi_1}{\omega_0}\right) + KE_2 \sin 2\omega_0 \left(t + \frac{\varphi_2}{2\omega_0}\right) \end{aligned}$$

To guarantee undistorted,

$$\frac{\varphi_1}{\omega_0} = \frac{\varphi_2}{2\omega_0} = \text{const} = -t_0$$

Consider non-periodic inputs case, we can write without loss of generality that

$$\varphi(\omega) = -\omega t_0 = \angle H(j\omega)$$

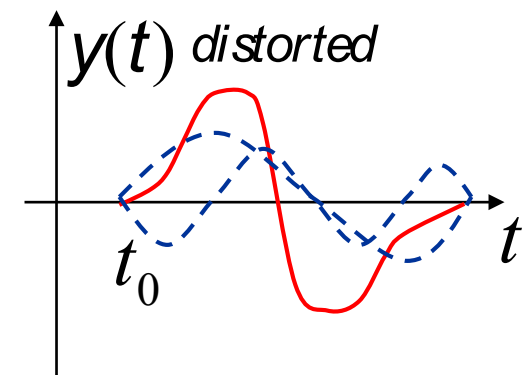
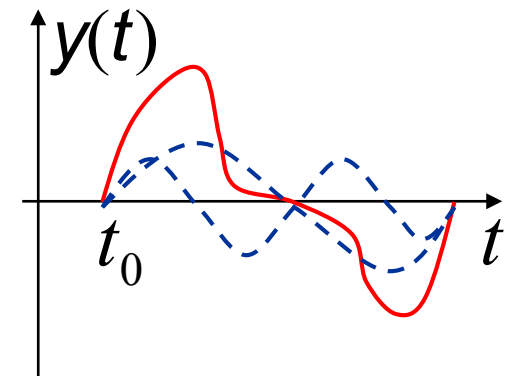
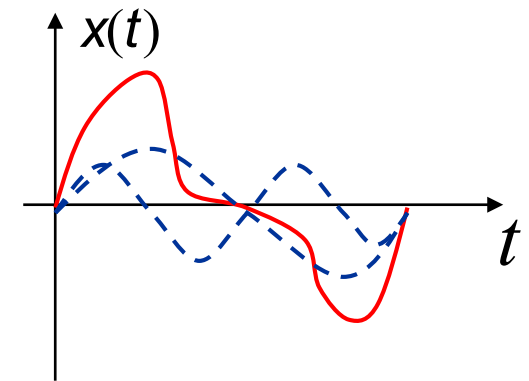
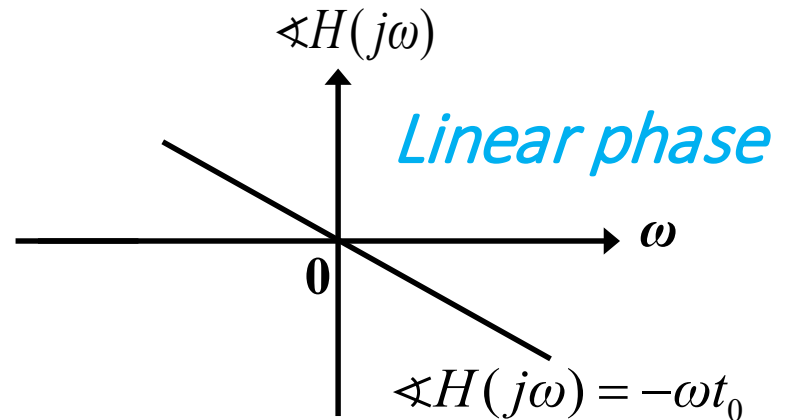
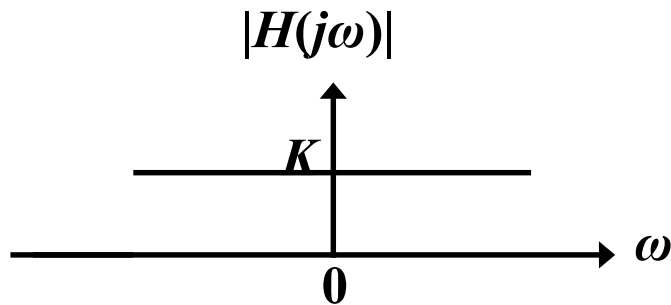


Illustration of phase distortion

## 4.8 Transmission without Distortion

➤ Conclusions: a linear system that can transmit signals applying to it as input without distortion must have a constant magnitude response and a phase response directly proportional to frequencies.



Linear phase shifts lead to very simple and easily understood change in a signal.

*Group Delay:*  $\tau(\omega) = -\frac{d\{\angle H(j\omega)\}}{d\omega}$

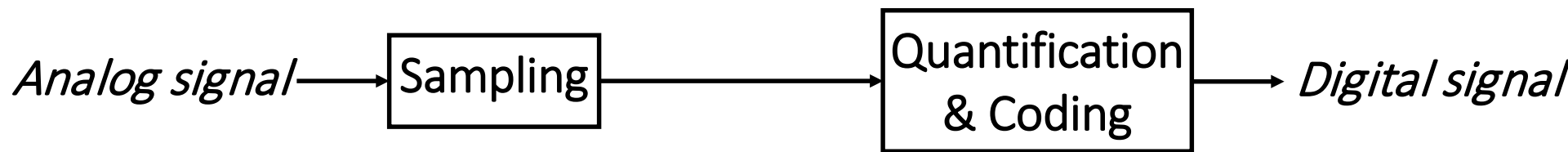
$$h(t) = K\delta(t - t_0)$$

Systems with this impulse response is ideal!

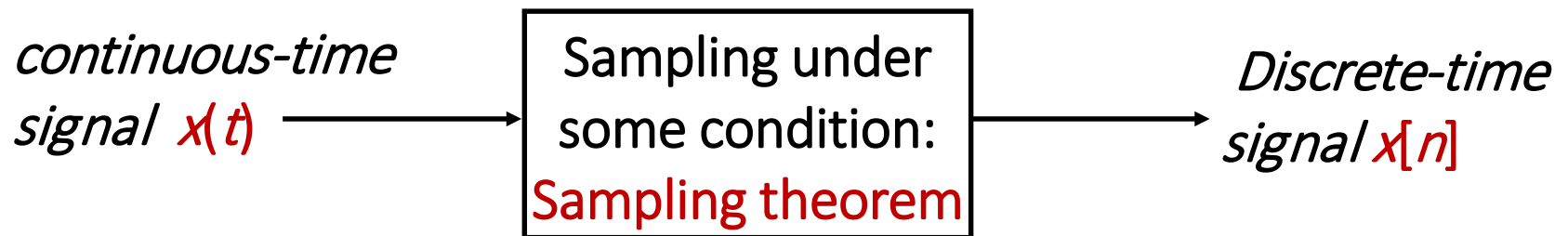
More about this refer to Section 6.2.

## 4.9 Sampling

### 4.9.1 Introduction



Analog to digital signals conversion process



- Sampling theorem is a bridge between continuous-time signals and discrete-time signals.

## 4.9 Sampling

### 4.9.2 Representation of a continuous-time signal by its samples: The Sampling Theorem

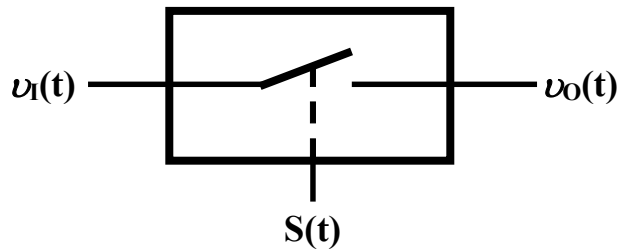
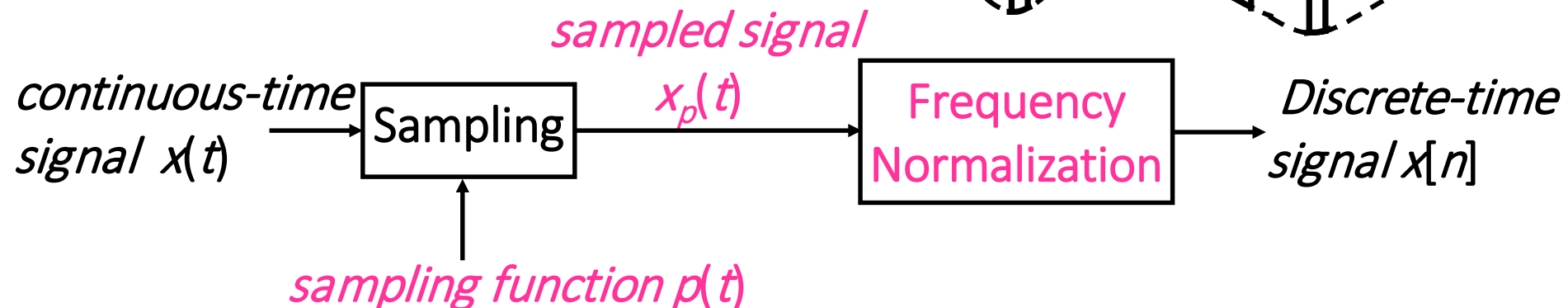
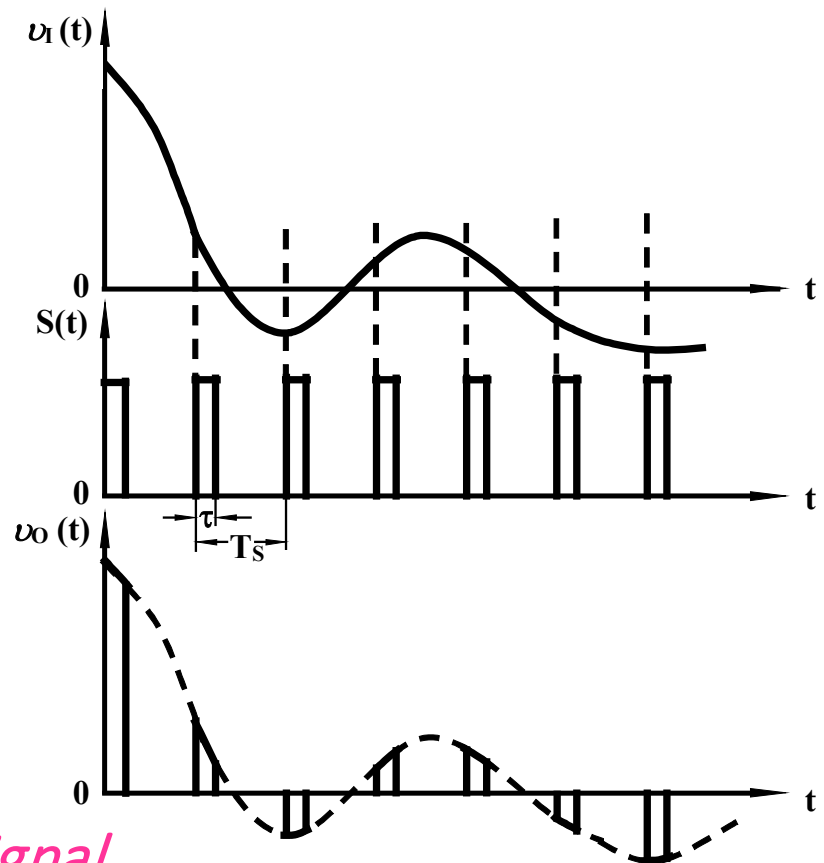


Diagram of sampling circuit

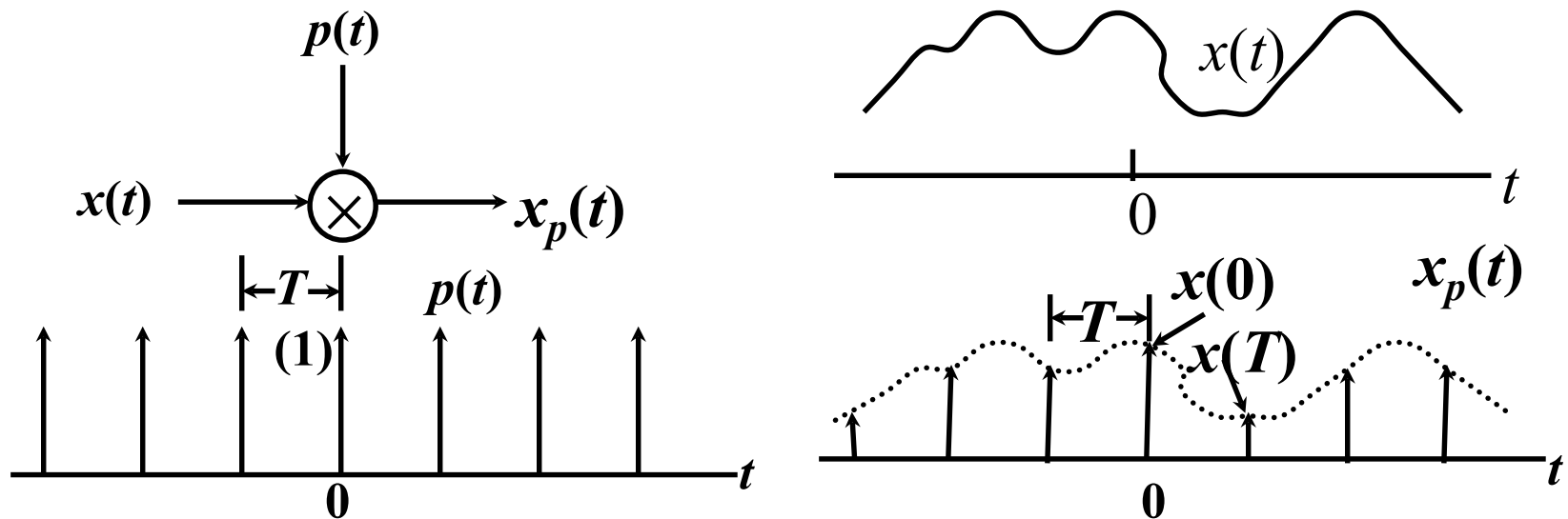


To make sure that  $x[n]$  can keep most information in  $x(t)$ , or  $x(t)$  can be recovered from  $x[n]$ , what are the conditions a *sampling* procedure must satisfy? Let's consider the problems:

- 1、 What is the Fourier transform of  $x_p(t)$ ?
- 2、 How is it related to that of  $x(t)$  ?

## 4.9 Sampling

### 4.9.2.1 Impulse-train sampling (冲激串采样)



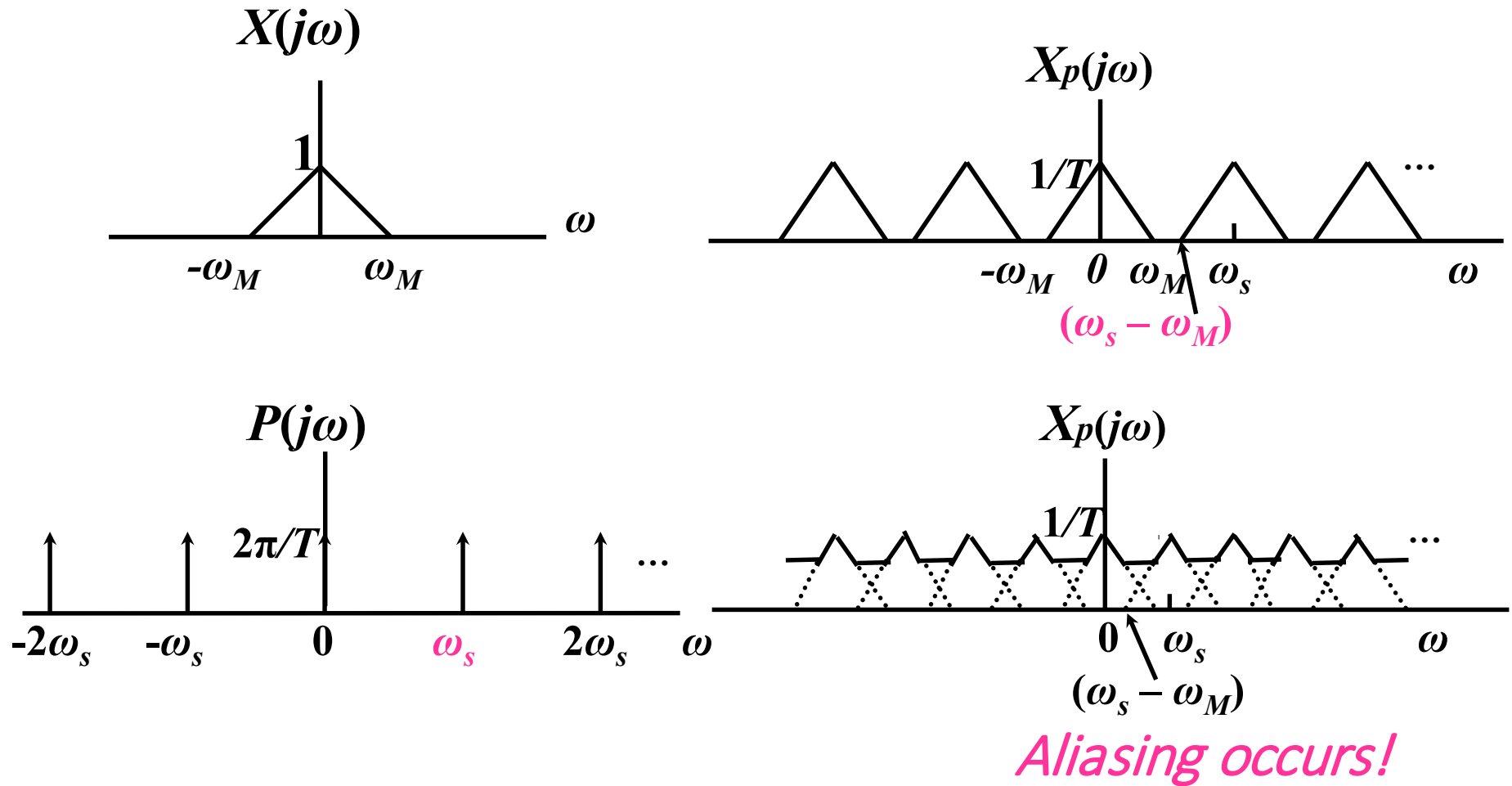
#### Mechanism of Impulse-train sampling

$$x_p(t) = x(t) \cdot \sum_{n=-\infty}^{\infty} \delta(t - nT) \quad X_p(j\omega) = \frac{1}{2\pi} [X(j\omega) * P(j\omega)] \quad P(j\omega) = \frac{2\pi}{T} \sum_{k=-\infty}^{\infty} \delta(\omega - k\omega_s)$$

$$X_p(j\omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} X(j(\omega - k\omega_s))$$

Answer for Q1&2:  $X_p(j\omega)$  is a periodic function of  $\omega$  consisting of a superposition of shifted replicas of  $X(j\omega)$ , scaled by  $\frac{1}{T}$ .

## 4.9 Sampling



Effect in the frequency domain of sampling in the time domain



## 4.9 Sampling

### Sampling Theorem (采样定理)

Let  $x(t)$  be a band-limited signal with  $X(j\omega)=0$  for  $|\omega|>\omega_M$ . Then  $x(t)$  is uniquely determined by its samples  $x(nT)$ ,  $n=0, \pm 1, \pm 2, \dots$ , if

$$\omega_s > 2\omega_M$$

where

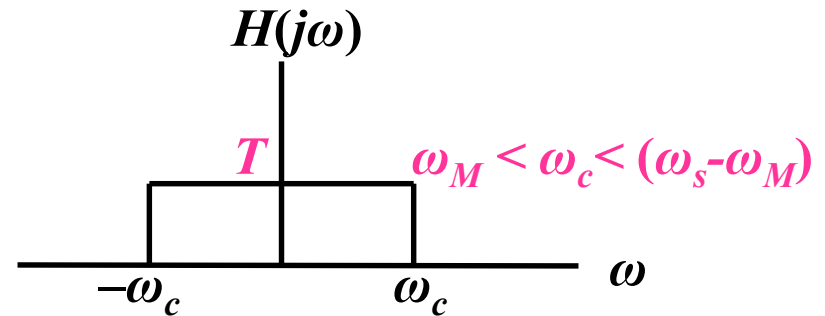
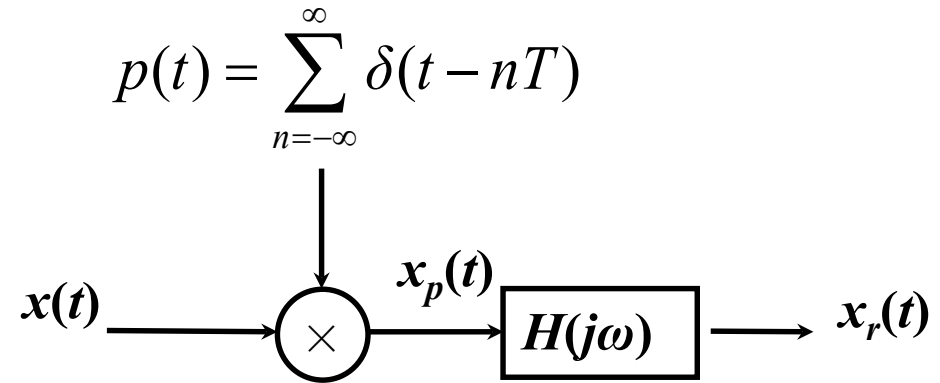
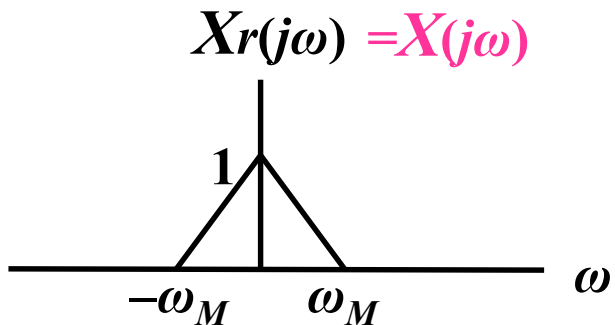
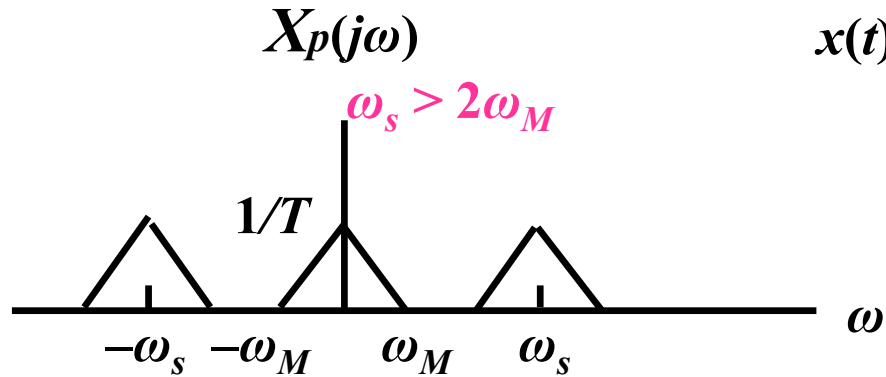
$$\omega_s = \frac{2\pi}{T}$$

*Nyquist frequency*  
(奈奎斯特频率)



Given these samples, we can reconstruct  $x(t)$  by generating a periodic impulse train in which successive impulses have amplitudes that are successive sample values. This impulse train is then processed through an ideal low-pass filter with **gain**  $T$  and **cutoff frequency** greater than  $\omega_M$  and less than  $\omega_s - \omega_M$ . The resulting output signal will exactly equal  $x(t)$ .

## 4.9 Sampling



Exact recovery of a continuous-time signal from its samples using an ideal low-pass filter

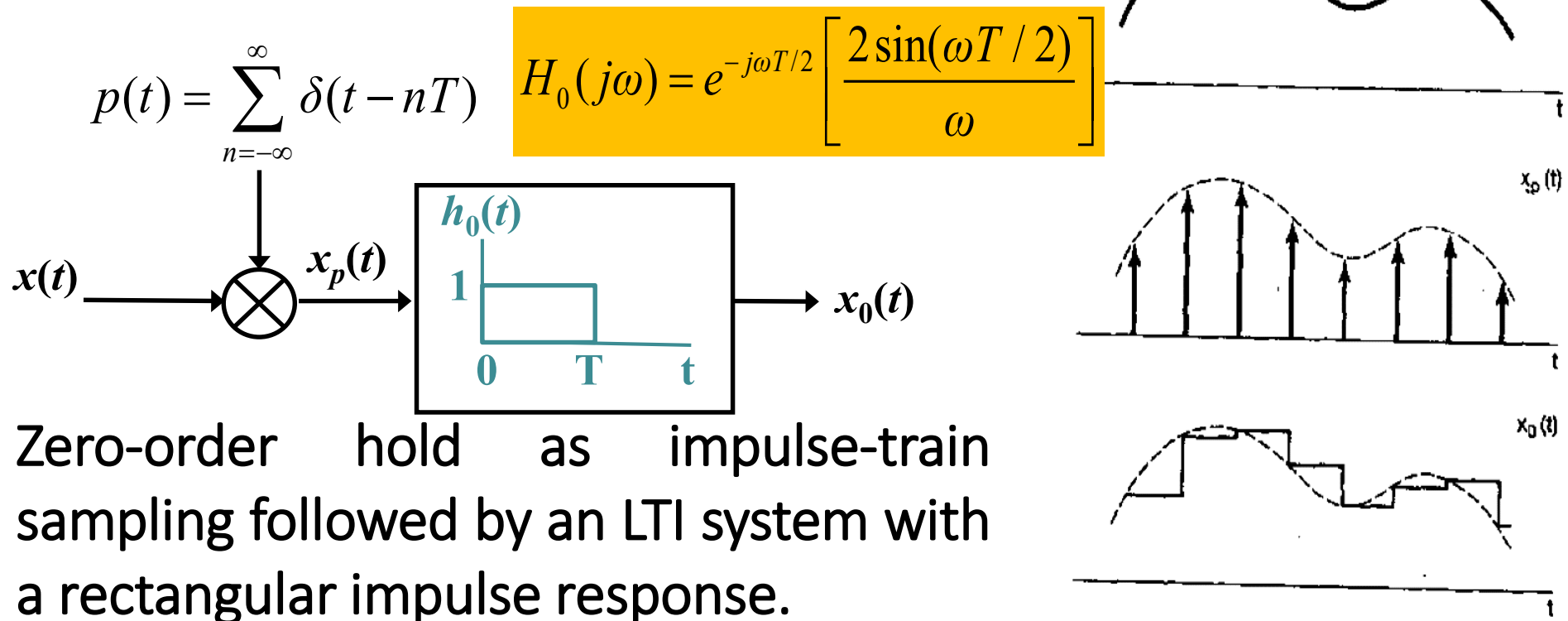
## 4.9 Sampling

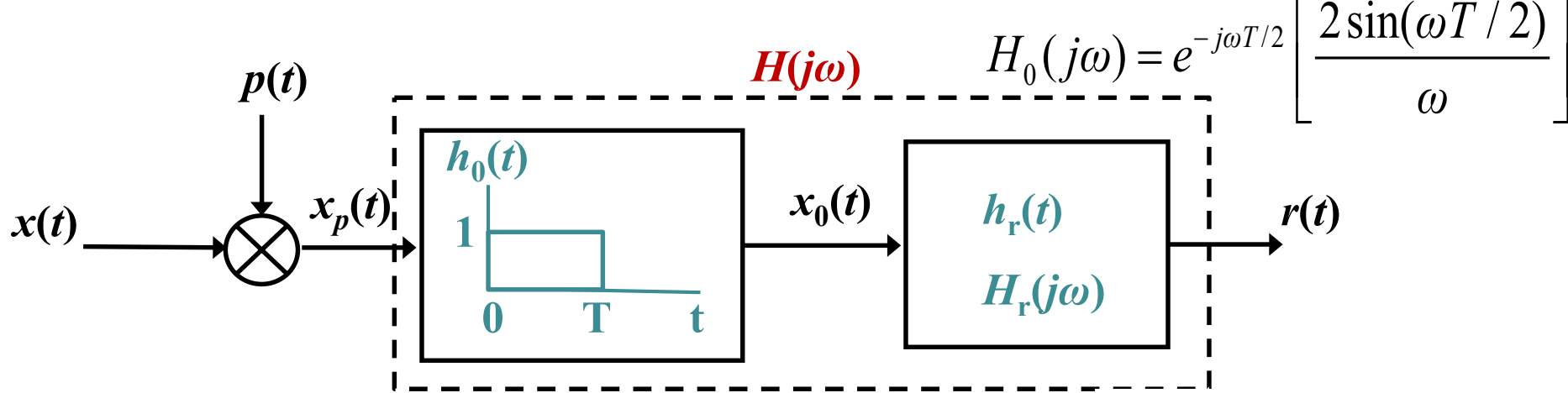
### 4.9.2.2 Sampling with a Zero-Order Hold



Sampling utilizing a zero-order hold

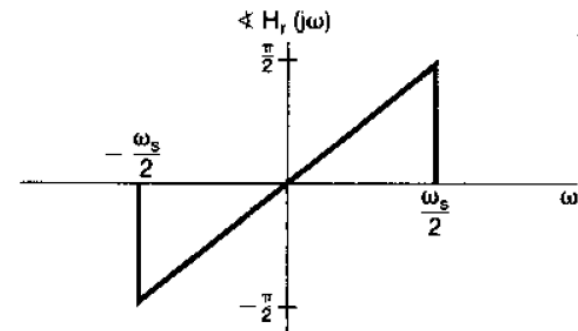
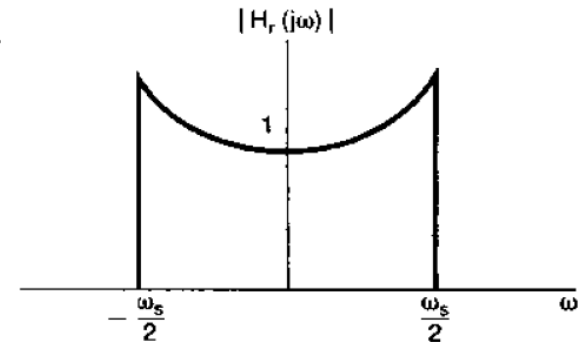
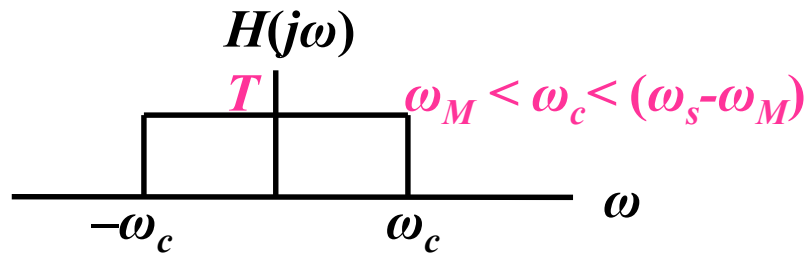
➤ How to generate  $x_0(t)$ ?





Cascade of the representation of a zero-order hold with a reconstruction filter.

Here,  $H(j\omega)$  is the ideal low-pass filter



$$H_r(j\omega) = \frac{e^{j\omega T/2} H(j\omega)}{\frac{2 \sin(\omega T / 2)}{\omega}}$$

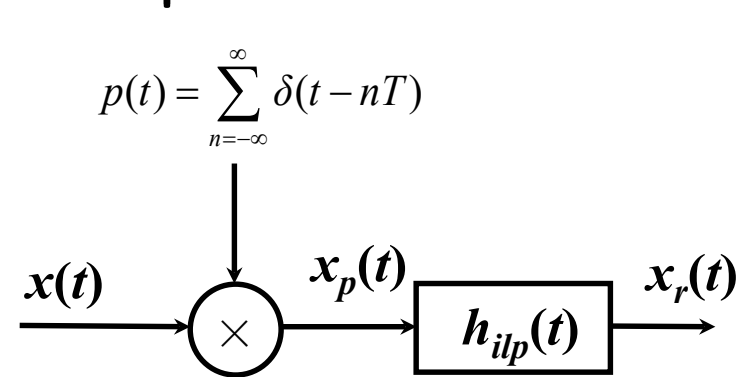
Magnitude and phase for the reconstruction filter for a zero-order hold with the cut-off frequency of  $H(j\omega)$  equal to  $\omega_s/2$ .

## 4.9 Sampling

### 4.9.3 Reconstruction of A Signal From Its Samples Using Interpolation

➤ *Interpolation* (插值): a procedure in which the fitting (拟合) of a continuous-time signal to a set of sample values. It is commonly used for reconstruction of a function from samples.

➤ Ways to interpolate: zero-order hold interpolation、linear interpolation、band-limited interpolation ...



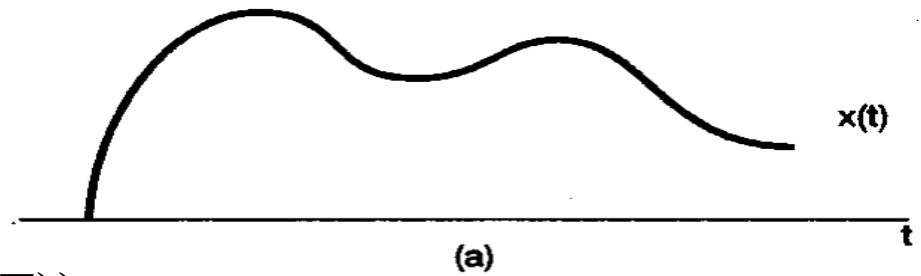
$$x_r(t) = x_p(t) * h(t) = \sum_{n=-\infty}^{\infty} x(nT)h(t - nT)$$

$$h(t) = \frac{\omega_c T \sin(\omega_c t)}{\pi \omega_c t}$$

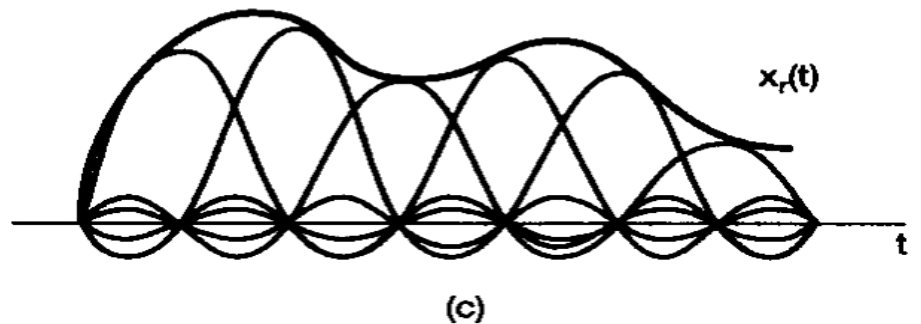
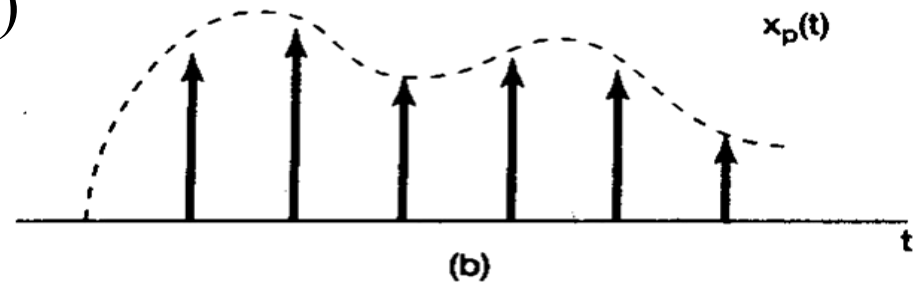
$$x_r(t) = \sum_{n=-\infty}^{\infty} x(nT) \frac{\omega_c T}{\pi} \frac{\sin(\omega_c (t - nT))}{\omega_c (t - nT)}$$

↑  
*Interpolation formula*

## 4.9 Sampling



$$x_r(t) = \sum_{n=-\infty}^{\infty} x(nT) \frac{\omega_c T}{\pi} \frac{\sin(\omega_c(t - nT))}{\omega_c(t - nT)}$$



Ideal band-limited interpolation using the *sinc* function with  $\omega_c = \frac{\omega_s}{2}$

## 4.9 Sampling

### 4.9.4 The Effect of Under-Sampling (欠采样): Aliasing(混叠)

$$x(t) = \cos \omega_0 t,$$

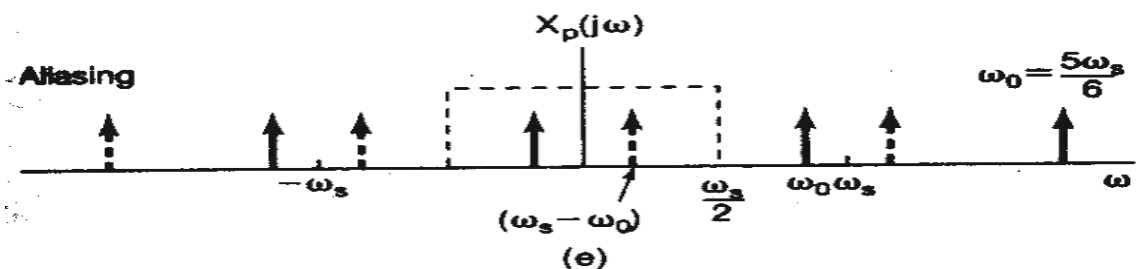
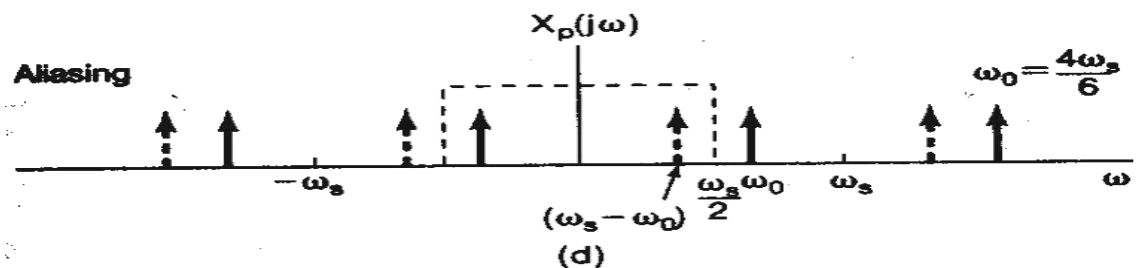
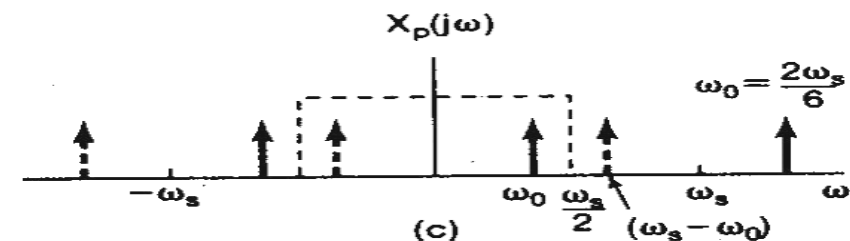
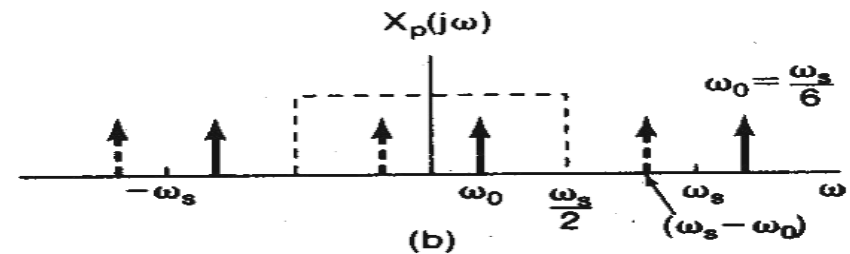
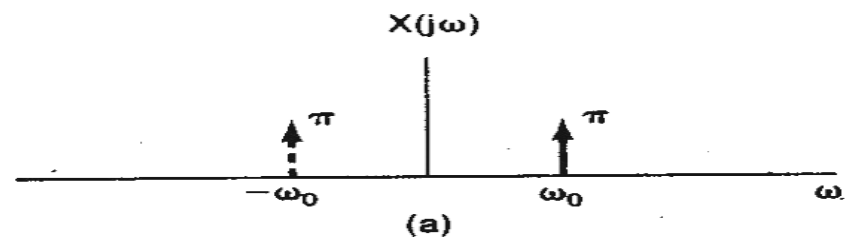
$$x(t) = \cos 1000t$$

is sampled with

$$\omega_s = 1500 \text{ rad/s}$$

$$\text{and } \omega_s = 1200 \text{ rad/s}$$

respectively.



## 4.10 SUMMARY

- The Fourier transform for both non-periodic and periodic continuous-time signals;
- The properties of the Fourier transform (relationships between characteristics of a continuous-time signal in time and frequency domains);
- Fourier analysis (Frequency domain analysis) for continuous-time LTI systems including both characteristics of systems and responses to some input signals;
- Frequency response and the way to obtain it;
- Continuous-time signals' sampling and their reconstruction.



# Homework

4.21 (b)(c) (d) (h)      4.22 (a) (b) (c) (d)

4.24    4.27

4.28 (a) 、 (i)(iv)(vi)(viii) in (b)

4.32 (b) (c)      4.34

4.35      7.22      7.23