\$   C=5A \ \ \pi^2 V = \frac{32V}{2} + \frac{32V}{2} \ \ \Justin Yang	ECE 329 Final Note Sheet
$\frac{2}{E} \left  \begin{array}{cc} C = SA \\ E & N/c = V/m \end{array} \right  = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial z^2} \left  \begin{array}{cc} Justin Yang \\ Justin Yz \end{array} \right $	Section X, Fall 2017
B V. s/m= W/m2=7 = -d charge inside conductor=0	
P C/m3 Laplacei eqn: P=0 > 02V=0	V(2)=V+e-182+V-e
P C/m³  Laplacei eqn: P=0→ V²V=0  A/m²  Poisson eqn: ¬²V=-£ if €, indep.	Î(t) = V+e-iBt-V-e.
Contombs:  Goldonbs:  J=E Ohn's law  Goldonbs:  Goldonbs:  J=E Ohn's law	
Conlombs: $Q = \int_{-\infty}^{\infty} \int_{-\infty}^$	V(d) = V + e > pd + V - e
	I(d) = V+eind -V-
10 - 10 - 10 ply Einste CL medicande Co in the	41 - 1 42 27
Mo= 4 Tix10=7 N/m J= Nav arrent succeptibility Xe  eo = (36 Ti x167) + F/m J= Nav Jersity	$\omega_0 = \frac{1}{\int LC}$ $\beta = \frac{2\pi}{2}$
e. = (36 T x18) + F/m Jensity Jensity suceptibility Xe	$Z_L = A_L + jX_L$
C= 3x/08 m/s Corent force F=g(E+vxB)	- Marin peffici
ECE 329 Milterm 2 Notecard Et, Et Et Lt 1(H, -Hc) L Js in - Justin Your	load reflection wested
Section X, Fall 2017 = Bus -HE Anx (HI-HE)E Js justing?	
ECE 329 Milterm 2 Notecard $E_{\xi}$ , $E_{\xi} = C_{\xi}$ $(\Pi_1 - \Pi_2) \cdot J_3 \times G_1$ Justin Yang Section X, Fall 2017 $\longrightarrow H_{\xi}$ , $G_{n} \times (H_1 - H_2) \cdot J_3$ justing 2  Ampere's law $\overrightarrow{B} = \underbrace{M_0 \cdot \overrightarrow{I}}_{2\pi r} \cdot J_0 \cdot \overrightarrow{H} = \overrightarrow{B}$ $G_{\overline{I}} = G_{\overline{I}} \cdot J_0 \cdot J_0$	eneralized reflection a
The state of the s	generalized reflection $C$ $P(d) = P_L e^{-j2pd}$
$\frac{1}{2} = \frac{1}{2} \int_{\mathcal{C}} J \cdot dS \qquad J(x, y, z) = J_{\mathcal{C}}(y, z) \frac{1}{2} \frac{1}$	line impedance
V 4F=qV×B C J(X, Z)== 1(2)d(X-X <sub>0</sub> /3(y-y <sub>0</sub> ))	=(1) = V(d) - 1+ P(d
raraday's law 4xE = - 1t, 9c 1.11 = - 1 3t . 15 = - 11 8.45	$Z(J) = \frac{V(G)}{I(J)} = Z_0 \frac{I + \Gamma(J)}{I - \Gamma(d)}$
王= So B·d3、 E=- 立を(Faraday) (Am), と=- 生き めっぱ、 I= を、 C= (にいり)	7-2-20 3-14
Inductance L= OE, E - Late B = MOIN #516 Page >2 shorter	
Inductance (= ?\vec{T}, \vec{C} = -1 \div \vec{H} = \wolder \overline{H} = \wolder \overline{H} = \vec{M} \overlin	
P=- V. J D=eE, B= WHA (0+ B)=P HING B-M BO 27 27 27 1	$y(a) = \frac{1}{2(a)}  Y = \frac{y}{2a}$
T. D= P Gans law Amger O. (B+-B)=0 = 4H I = 9 Mo In DI	Voltage Standing Wave
THE DE PARTY OF THE PARTY OF TH	$VSWR = \frac{ V(J_{max}) }{ V(d_{mla}) } = \frac{1}{1- V(d_{mla}) }$
FCE 329 Miller 2 Note cond	1 V(dm/a) 1-
Section X, Fall 2017  Section X, Fall 2017  Justiny 2	$ \Gamma_L  = \frac{VSWR-1}{VSWR+1}$
<3'>=	1+ M(dmax)
Poynting than 3= Exil < Exil >= {Re{Exilus IE = 1 B = U = wave however	$VSWR = \frac{1 + P(d_{max})}{1 - P(d_{min})}$
St (26E. E+2 uH.H)+7 (ExH)+J=E=0 sin > 1 Enamone frequency  change of total electrical enemy Joule heating (12-21) N=27/8, T=27 = E	
2 may energy density wasport pover absorbal/unit to = = = = = =	Z(dmax) = VSWR
J.D=P T.D=8 STREAM - ONE OF LONDON SELACE REMINING JULE)	P(d) = 12 Re {V(d) I*(
Q. R= O Q. B= Elliptical Rumpinests And their Road conducts the dept.	p(d) = 2 ne(2) + 12
Transmission Lines 2= EGF Diff melia Widiff properties	$=\frac{1V^{4}l^{2}-1V^{-1^{2}}}{220}$
Signature 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
Mary and A complete and the market method method in the complete in the comple	$\sum_{i,n} = \frac{24}{2i}$
10- july (0+jule 10 fg+20 # 44 GE = 21 E- & E - & E - A - (D+-D-) Ps	
Notified The standing waves Find the standing waves of the standin	
7 The Title and Balcolust Hiel Stre & Z Hr Jane	

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(2) = V+e-iB2+ V-eiB2  $\hat{r}(t) = \frac{\hat{V} + e^{-j\beta^2} - \hat{V} - e^{j\beta^2}}{2}$ i(d) = V + e jpd + V - e - isd (d) = V+eind - V-e-ind W. = 1 B = 2 T  $Z_{L} = R_{L} + jX_{L}$ oad neflection wefficient  $n_L = \frac{21 - 20}{21 + 20}$ eneralized reflection coefficient (d) = MLe-12Bd ine impedance  $(J) = \frac{V(d)}{I(J)} = Z_0 \frac{1 + \Gamma(d)}{1 - \Gamma(d)}$  $7 = \frac{2-20}{2+20} \quad \frac{2}{70} = \frac{1+17}{1-17} = 2$  $y(a) = \frac{1}{2(a)} \quad Y = \frac{y}{2a}$ 'o Hage Standing Wave Matto (VSWR) /SWR = \frac{1V(Jmax)/}{1V(dm/2)/} = \frac{1+1F\_L1}{1-|F\_L1} Ir. | = VSWR-1  $/SWR = \frac{1 + P(dmax)}{1 - P(dmin)}$ Z (dmax) = VSWR (d) = = = Re {V(d) I\*(d)}  $=\frac{1V^{4}l^{2}-1V^{-1^{2}}}{220}$  $2_{in} = \frac{24}{3}$ 

Justin Yang

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Smith Chart Find Z(1), V(1) and I(1) given 21820 line E = + ITIEOF 1. Calculate ZL = ZL/Zo 8 × € == 0 € eurl-free gradient OV(2x, 2y, 22) = E=-VV 2. Mark & on SC sheet  $E = \hat{x} = \hat{x} = syn(x)$ 3. center of SC to 21 is dist ITL dab E = 1 PX V(b)-V(e)=- So E. dt LTL is measured CCW from Reaxis  $\overrightarrow{\nabla} \cdot \overrightarrow{D} = \overrightarrow{P}$  divergence ScE.II = SoxEds 4. Find Z(l): rotate CW (toward generator) Stoke's that for Edde OxE =0 Dx Dy Dz p by 0= 1 (360/0.50) 7 x = 9 7. D = P, D = E. E 5. Calculate 2(1)==(1)Z., [(1)=|Tilk[i F=OE, E=-PV parallel pl: C=EoT 6. Use VDR: V(P)=1/2[Z(R)(Zg+Z(R))] C)  $\vec{\nabla} \times \vec{E} = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial x}\right) \times \left(\vec{E}_{x}, \vec{e}_{y}, \vec{E}_{z}\right) \quad \vec{D} = \vec{x} \quad \vec{\nabla}_{A}, \quad \alpha = cv$ 1. Calc V+: V(1)= V+(e-iBA+17, eiBl)  $= \left| \frac{\partial \mathcal{L}}{\partial x} \right| = \hat{\chi} \left( \frac{\partial \mathcal{L}}{\partial y} - \frac{\partial \mathcal{L}}{\partial z} \right) - g \left( \frac{\partial \mathcal{L}}{\partial x} - \frac{\partial \mathcal{L}}{\partial z} \right) + 2 \left( \frac{\partial \mathcal{L}}{\partial x} - \frac{\partial \mathcal{L}}{\partial y} \right)$ 8. Calculate V(l) for any e by sub Vi, (4) TEM Wave Solns  $\vec{\nabla}^{2}\vec{E} = \frac{3^{2}\vec{E}}{3^{2}\vec{L}} + \frac{3^{2}\vec{L}}{3^{2}\vec{L}} + \frac{3^{2}\vec{L}$  $\frac{9^{2}V}{2} = \frac{3kV}{2k^{2}} + \frac{3^{2}V}{3y^{2}} + \frac{3^{2}V}{3k^{2}}$ 9. I(l)= V(l)/2(l) at any given l Querter Ware transformer  $\frac{\partial^2 E_x}{\partial z^2} = ME \frac{\partial^2 E_y}{\partial z^2} \quad \eta = \frac{1}{ME} \frac{\partial E_y}{\partial z^2} \quad \frac{\partial E_y}{\partial z^2} = \frac{\partial^2 E_y}{\partial z^2} \quad \frac{\partial^2 E_y}{\partial z^2} = \frac{\partial^2 E_y}{\partial$ 1. Calculate Z = Z1/20 2. Mark 2, on SC 3. Dist center SC+ ZL is IPL, LPL is H= + 9/ (w(+ = )) polarized ++++ (M= 4 T × 10-7 H/m  $H = \pm i \int_{-\infty}^{\infty} \omega S(\omega(t + i)) \frac{1}{2} \frac{$ measured CCW from real axis 4. Draw circle contered a SC U/r=17,1 并 差 15= 产以(E) 产士=一文 2月(七-美) 5. 21 point (intersection on real exis) # = I F(6 I =) 220 E NC=V/m (impedance is purely next) B V. 5/m2 = Wb/m2 = T TBn2 = BA 6. Rotate toward gonerator (CW)  $\vec{E} = \hat{g} \cos(\omega(t \mp \vec{E}))$ D C/m2 S A/m2 L H= Wb polarized ZL -> Z'. Angle is dist d, of quarter. 日= IX ws(w(t = 三)) defendant C/m3 & V wave transformer from load in I units J Am I Wb an f f 7. Impedance at di is 2(di)=2021  $\nabla^{2} V = \frac{\partial^{2} V}{\partial x^{2}} + \frac{\partial^{2} V}{\partial y^{2}} + \frac{\partial^{2} V}{\partial z^{2}}$   $\frac{\partial^{2} V}{\partial y^{2}} + \frac{\partial^{2} V}{\partial x^{2}} + \frac{\partial^{2} V}{\partial z^{2}} + \frac{\partial^{2} V}{\partial z^{2}}$   $\frac{\partial^{2} V}{\partial x^{2}} = \frac{\partial^{2} V}{\partial x^{2}} + \frac{\partial^{2} V}{\partial z^{2}} + \frac{\partial^{2} V}$ V(をも)= 多星(にな) をはまっつき) 8. Characteristic impedance of quarter-+241, \$ (1,19) "8(++ \$ = (41) 2) ware transformer Zgo=1202(d,) 王冠的三至是《见明》《任一是一个是》 Calculate Zi given VSWR ◆- 毎几笠(ng)%(t+ま-(4川県) 1. Calculate I min or doman using fact that on TL, 2 minima or 2 maxima NO=4710-7 H/M 32E = 31E + 31E + 31E - ME 31E TEM WELLE 2=RC E = (36 T x 10-9) -1 F/m are separated by 0.57 C= 3×10 m/3 20= 120 m 52 2= 12 GF = W/J purallel plate 2. On SC, mark  $2(d_{max}) = VSWR + jo$ = 300 m/ms
1 /- A L [H=Wb/A=V-S/A [H=[h] GF- cosh-1 D/2a trin-lead Z(dmin) = (1/VSWR) +jo, as A, B, resp. N/C=V/m C|F=A·S/V=C/V current E4=E4 (H,-H2) Ex=EoCTX2 etBE 3. Radins of USWR cords on SC How A.B B V-s/m2=Wb/m2=T IWI sheet Ex = Eoe For 2 cos(wtfp2) Rx(F,-H2), J.  $\bigcap_{j_k} = \frac{Z_k - Z_j}{Z_{k+} + Z_j} j \to k$ 4. Start at pt B, notate CCW (toward B rad/m & NPIMBrad/m 1 Pag C/m2 w rads & NP/moral cos leads sin leads-cos load) by dist dmin (in 2 units). \$ >pfc Tonz Tem Fr of Cread it. On 1 - Dnz = 15 | Bn, = Bnz 5. Dist from center of SC to C is ITLI and Longle LPL = - 1800 + dmin (360/0.52) / 25 6. Solve for IV+land IV-lasing IVment 5 225 = 1V+1+1V-1, |Vmin| = |V+1V-7 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100