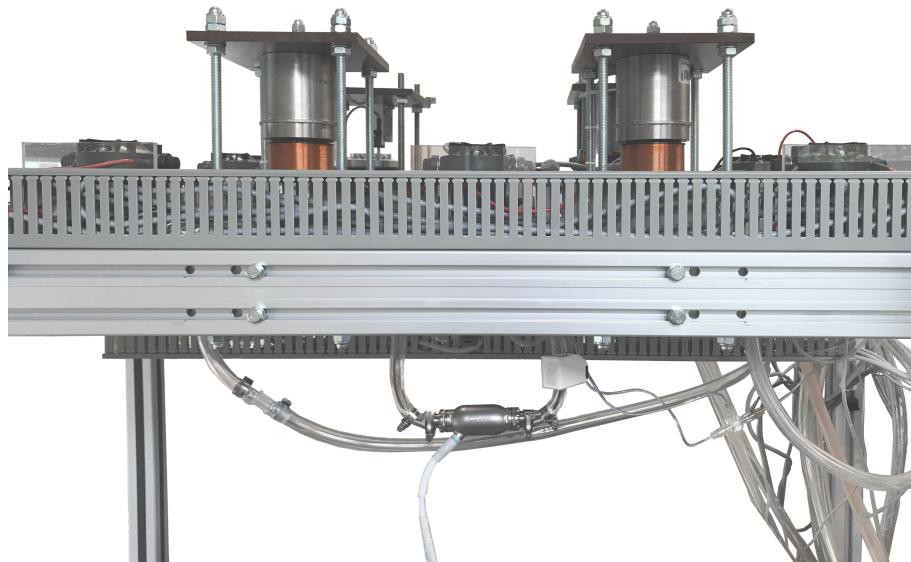


Master Thesis

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Modeling and flow control for a left ventricular assist device



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Abstract

Contents

Abstract	v
Contents	vii
List of Figures	ix
List of Tables	xiii
List of Symbols	xv
1 Introduction	1
1.1 Motivation and goal	1
1.2 Thesis structure	1
2 Medical Fundamentals	3
2.1 Cardiovascular System	3
2.2 Heart failure	8
2.3 Ventricular Assist Devices	9
2.3.1 Therapeutic objective	9
2.3.2 Technology	11
3 Control Theory	15
3.1 Fundamentals	15
3.2 PI-controller	17
3.2.1 Tuning rules	18
3.3 Iterative Learning Control	21
4 Identification	25
4.1 Sputnik VAD	25
4.2 Hardware in the Loop Test Bench	26
4.3 System Identification	29

Contents

5 Flow Control	35
5.1 PI Controller	35
5.1.1 Design and Implementation	35
5.1.2 Evaluation	38
5.2 Iterative Learning Control	41
5.2.1 Design and Implementation	41
5.2.2 Evaluation	43
5.3 Iterative Learning Control with repeating disturbance	47
5.3.1 Reference trajectories	48
5.3.2 Evaluation	49
5.4 Iterative Learning Control with varying disturbance	57
5.4.1 Design and Implementation	57
5.4.2 Evaluation	59
6 Conclusion and future work	67
A Appendix	69
Bibliography	77

List of Figures

2.1	Blood distribution in the circulatory system [Hal16]	3
2.2	Anatomy of the human heart [Hal16]	5
2.3	Action phases of left ventricular cardiac cycle [Hal16]	6
2.4	P-V diagram [Hal16]	7
2.5	P-V diagram for heart failure	9
3.1	General structure of a control loop	15
3.2	Transfer function of a PT_1 -element	17
3.3	Step response of a PI-Controller	19
3.4	Inflection tangent method for Ziegler Nichols and Chien Hrones Reswick	20
3.5	Standard ILC control loop	21
3.6	Parallel architecture of ILC with feedback controller	22
4.1	Cross-section of Sputnik VAD [ST16]	26
4.2	HiL test bench	27
4.3	Sputnik VAD and flowmeter in HiL setup	28
4.4	Signal curves for creation of the static map.	30
4.5	Static map for different tube length in 60 % water 40 % glycerin solution	31
4.6	Static map for varying fluid solution with 15 cm long tubes	32
4.7	Static map for solution of 60 % water 40 % glycerin with 15 cm long tubes	33
4.8	Transfer function of Sputnik VAD	33
5.1	Signal curves for determination of PI controller parameters	36
5.2	Signal curves for determination of PI controller parameters at $\Delta p = 40 \text{ mmHg}$	37
5.3	Step response for determination of PI controller tuning parameters	38
5.4	Reference signals for PI controller performance evaluation	39
5.5	Test measurement for PI controller tuned according to Chien Hrones Reswick at $\Delta p = 40 \text{ mmHg}$	40
5.6	Control error for PI Controllers	40
5.7	Smoothed reference signal for ILC tuning.	42
5.8	Test measurement for ILC at cut off frequency $f_c = 20 \text{ Hz}$	43

5.9	Test measurement for ILC at cut off frequency $f_c = 34 \text{ Hz}$	44
5.10	Test measurement for ILC at cut off frequency $f_c = 25 \text{ Hz}$	45
5.11	Comparison of RMSE values for different cut off frequency of ILC Q-Filter	46
5.12	Comparison of RMSE values of the ILC at different differential pressure operating points	47
5.13	Sinusoidal reference signal	48
5.14	Triangular reference signal	49
5.15	Rectangular reference signal	49
5.16	Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 1$ for constant reference flow	50
5.17	RMSE Comparison of ILC at constant reference flow for varying left ventricular contractilities	51
5.18	Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 1$ for sinusoidal reference flow	52
5.19	RMSE Comparison of ILC at sinusoidal reference flow for varying left ventricular contractilities	52
5.20	Measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 1$ for triangular reference flow	53
5.22	RMSE Comparison of ILC at triangular reference flow for varying left ventricular contractilities	54
5.23	Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 1$ for rectangular reference flow	55
5.24	RMSE Comparison of ILC for a rectangular reference flow for varying left ventricular contractilities	56
5.25	RMSE Comparison of ILC at rectangular reference flow for varying heart rates	56
5.26	Illustration of HR change	58
5.27	Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for constant reference flow without data resampling	60
5.28	Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for constant reference flow with data resampling	61
5.29	Comparison of RMSE values for ILC measurement using a constant reference flow for unchanged and resampled data	61

5.30 Comparison of RMSE values for ILC measurement using a sinusoidal reference flow for unchanged and resampled data	62
5.31 Comparison of RMSE values for ILC measurement using a triangular reference flow for unchanged and resampled data	63
5.32 Comparison of RMSE values for ILC measurement using a rectangular reference flow for unchanged and resampled data	64
A.1 Static map for different tube length in 100 % water	69
A.2 Static map for different tube length in 80 % water 20 % glycerin solution	69
A.3 Static map for different tube length in 40 % water 60 % glycerin solution	70
A.4 Static map for varying liquid solutions with 10 cm tube length . . .	70
A.5 Static map for varying liquid solutions with 5 cm tube length . . .	71
A.6 Test measurement for PI controller tuned according to Chien Hrones Reswick	71
A.7 Test measurement for PI controller tuned according to Ziegler Nichols	72
A.8 Test measurement for PI controller tuned according to Ziegler Nichols at $\Delta p = 40 \text{ mmHg}$	72
A.9 Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for sinusoidal reference flow without data resampling	73
A.10 Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for sinusoidal reference flow with data resampling	73
A.11 Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for triangular reference flow without data resampling	74
A.12 Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for triangular reference flow with data resampling	74
A.13 Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for rectangular reference flow without data resampling	75
A.14 Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for rectangular reference flow with data resampling	75

List of Tables

2.1	Relation between INTERMACS Score and NYHA-classification	10
2.2	Distribution of VAD types and therapeutic objectives	13
3.1	Tuning parameters Chien Hrones Reswick	21
4.1	Specifications of Sputnik VAD	25
5.1	RMSE values for different reference trajectories of standard ILC and revised ILC	65

List of Symbols

Abbreviations

A

AV Atrioventricular

B

BTD Bridging to decision
BTR Bridging to recovery
BTT Bridging to transplantation
BVAD Biventricular Assist Device

C

CHR Chien Hrones Reswick
CO Cardiac Output
CVDs Cardiovascular Diseases
CVS Cardiovascular System

D

DT Destination therapy

E

EDV End-diastolic volume
EF Ejection fraction
ESV End-systolic volume

H

HiL Hardware in the Loop
HR Heart rate
HTx Heart transplantation

List of Symbols

I

ILC	Iterative learning control
IMACS	International Mechanically Assisted Circulatory Support
INTERMACS	Interagency Registry for Mechanically Assisted Circulatory Support

L

LVAD	Left Ventricular Assist Device
------	--------------------------------

M

MCL	Mock circulatory loop
MCS	Mechanical Circulatory Support
MISO	Multiple-input-single-output

R

RMSE	Root Mean Square Error
RWTH	Rheinisch-Westfälische Technische Hochschule

S

SISO	Single-input-single-output
SL	Semilunar
SV	Stroke Volume

V

VADs	Ventricular Assist Devices
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W

WHO	World Health Organization
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Z

ZN	Ziegler Nichols
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1 Introduction

1.1 Motivation and goal

1.2 Thesis structure

2 Medical Fundamentals

An important prerequisite to the work addressed in this thesis is comprehending the physiology of the human heart and the cardiovascular system. Therefore, the theoretical foundations of these topics will be introduced in the following chapter.

2.1 Cardiovascular System

The fundamental task of the cardiovascular system is to supply all organs with blood through circulation. The human cardiovascular system is divided into two components, the systemic circulation and the pulmonary circulation. The systemic circulation is supplying blood flow to all tissues and organs apart from the lungs. Figure 2.1 represents the blood distribution over the circulatory system. [Hal16]

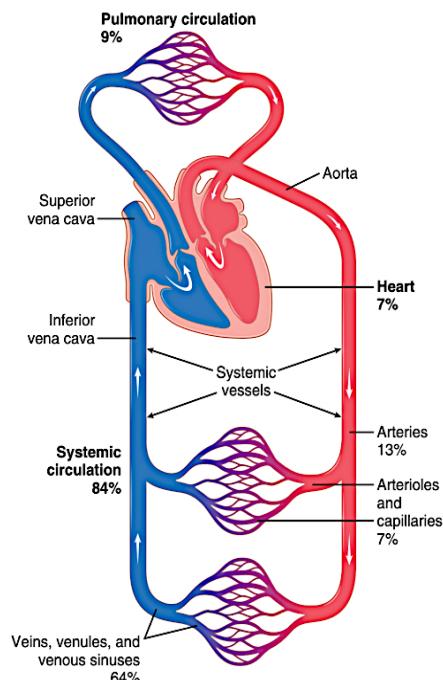


Figure 2.1: Blood distribution in the circulatory system [Hal16]. Red highlighting representing oxygenated, blue highlighting depicting deoxygenated blood flow.

The center of the cardiovascular system is the heart. The heart itself consists of two mechanical pumps, which are functionally connected in series but are united in one organ. It is separated into two sides, which themselves are divided into an atrium and a ventricle each. The atria act as weak primer pumps required to provide blood flow to the ventricles. [SLH11] Both the atria and the ventricles are surrounded by the myocardium, which serves as the working muscle of the heart. Through contraction of the myocardium, blood is pumped into the circulatory system. [SK07] The left ventricle is pumping oxygenated blood through the aorta into the systemic circulation. There, oxygen stored in the blood is delivered to the organs. The blood, now low in oxygen, is then led into the right atrium through the inferior and superior vena cava. From the right atrium, the deoxygenated blood then enters the right ventricle. Afterwards, it is directed into the pulmonary circulation via the pulmonary artery. When the blood is oxygenated in the lungs, it is returned to the left atrium through the pulmonary vein. [SLH11] In addition to the atria and the ventricles, each side of the heart has an atrioventricular (A-V) valve, as well as a semilunar (SL) valve. The A-V valve of the left heart is called the mitral valve, the one of the right heart is referred to as the tricuspid valve. The aortic valve and pulmonary valve are the SL valves of the left and right heart, respectively. The valves determine the direction of blood flow and thus prevent backflow. [SK07] A graphic overview of the anatomy and the course of blood flow through the heart is provided by Figure 2.2.

The amount of blood pumped through each side of the heart, called cardiac output (CO), is equal at all times. It is determined by multiplying the heart rate (HR) by the stroke volume (SV). For an average adult at rest with a heart rate of approximately 70 min^{-1} and a stroke volume of 70 ml , this leads to

$$CO = HR \times SV = 70 \text{ min}^{-1} \times 70 \text{ ml} = 5 \frac{\text{l}}{\text{min}}. \quad (2.1)$$

In case of maximum physical load, given at a stroke volume of 110 ml and a heart rate of 190 min^{-1} , the cardiac output can increase to up to $20 \frac{\text{l}}{\text{min}}$. [SLH11]

The cardiac cycle comprises all events that occur during the time-span of one heartbeat. The cycle is triggered by an electrochemical action potential originating from the sinus node. The cycle is divided into four phases. Figure 2.3 illustrates these action phases and events of the cardiac cycle for the left ventricle.

During the period of isovolumic contraction, the ventricular pressure increases. For the left ventricle, the pressure increases from about $4 - 6 \text{ mmHg}$ to 80 mmHg , whilst

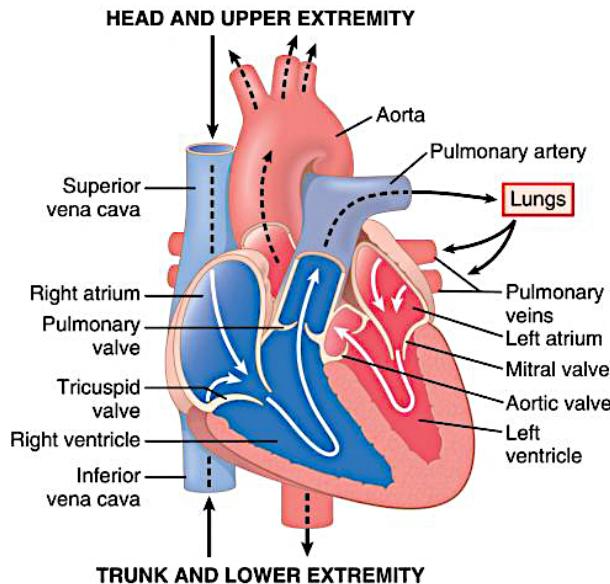


Figure 2.2: Anatomy of the human heart [Hal16]. Red highlighting representing oxygenated, blue highlighting depicting deoxygenated blood flow.

the pressure values for the right ventricle are much lower. This increase is occurring as a direct result of the ventricular contraction. The A-V valves, as well as the SL valves, are closed during this process, leading to a constant blood volume in the ventricles. As soon as the ventricular pressure exceeds the arterial pressure, the pulmonary and aortic valves open and blood can flow into the aorta and the pulmonary artery. This phase is called ejection phase, as the blood is ejected into the circulatory system. The period of isovolumic contraction combined with the ejection phase comprises the ventricular systole. [SLH11] During the systole, the blood volume in the ventricle decreases by 55 – 60 %, resulting in an end-systolic volume (ESV) of about 40 – 50 ml [Hal16]. Due to the contraction of the myocardium, the ventricular pressure keeps increasing for a while before decreasing again as relaxation of the myocardium sets in. As soon as the outflow of blood ends, the semilunar valves close, initiating the period of isovolumic relaxation. During this period, pressure in the ventricles is decreasing while blood volume remains constant. When the pressure in the atrium exceeds the ventricular pressure, the A-V valves open. This leads to blood flowing into the ventricles until pressure levels in the atria and ventricles are equalized. [SLH11] This phase is referred to as period of rapid filling of the ventricles. This period, in combination with the isovolumic relaxation, forms the diastole. The end-diastolic volume (EDV) amounts to about 110 – 120 ml. [Hal16] While at rest,

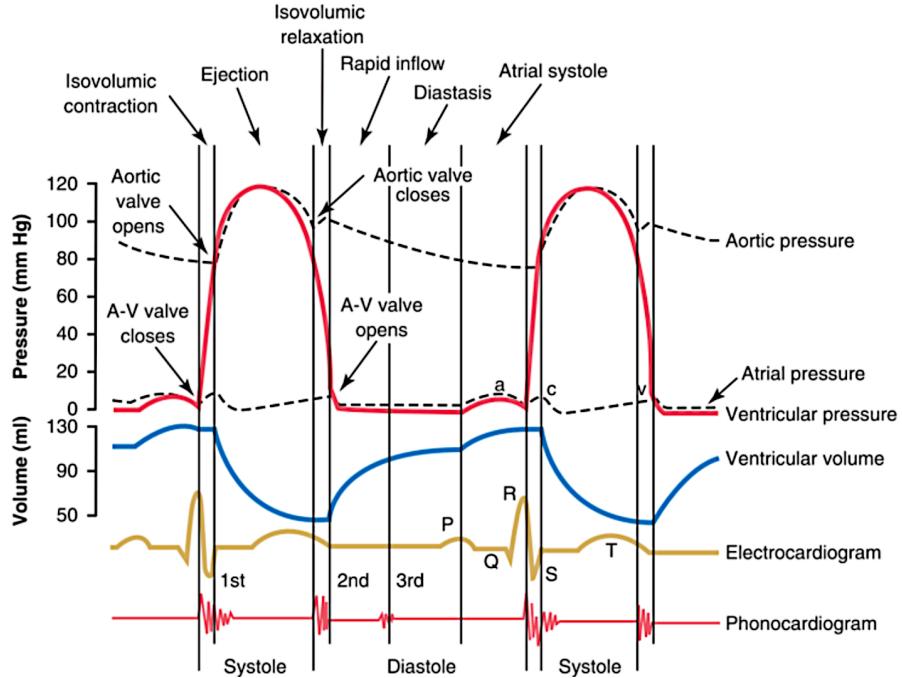


Figure 2.3: Action phases of the cardiac cycle based on the example of the left ventricle [Hal16].

the diastole lasts about twice as long as the systole. Above a heart rate of 150 min^{-1} however, the two phases are about equal [SLH11].

The pumping mechanism of the left ventricle can be illustrated using a pressure-volume diagram (P-V diagram). Construction of the P-V diagram first requires discussing the relationship between the left ventricular volume and the ventricular pressure during diastole and systole, as displayed in Figure 2.4a. The figure displays two curves named *diastolic pressure* and *systolic pressure*. Diastolic pressure is defined as the lowest point of each pulse during the relaxed state of the heart, whilst systolic pressure represents the highest point of each pulse, occurring while the heart is contracting and ejecting blood. [SLH11] The blue curve in Figure 2.4a, representing the diastolic pressure, is determined by gradually filling the heart with higher blood volumes and subsequently measuring the diastolic pressure just before ventricular contraction occurs. It describes the heart's mechanical properties when the myocardium is in a relaxed state. The green curve in Figure 2.4a, named systolic pressure, is plotted by measuring the systolic pressure over varying filling volumes for constant ventricle volumes. The red lines in Figure 2.4a and Figure 2.4b indicate

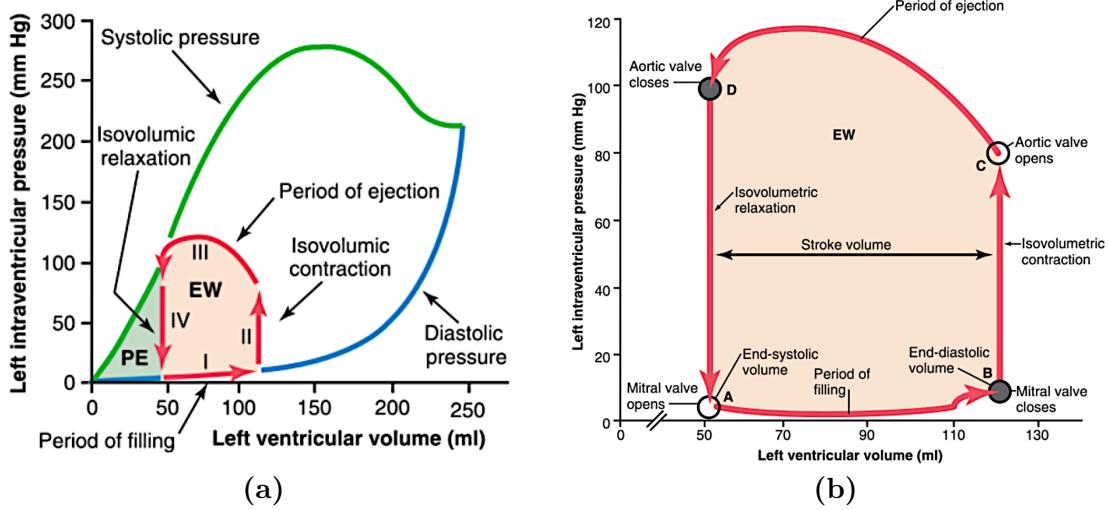


Figure 2.4: (a) Working diagram of the left ventricle with the P-V diagram. (b) Close-up P-V diagram. [Hal16]

the cardiac cycle and its four action phases, as described above. The line between points A and B in Figure 2.4b depicts the period of rapid filling. The isovolumic contraction is represented by line II in Figure 2.4a, respectively between points B and C in Figure 2.4b. The ejection phase is depicted by III in Figure 2.4a and the line referred to as IV represents the period of isovolumic relaxation. The area of the work diagram, marked with EW in Figure 2.4 is a measure of the work done by the heart. The P-V diagram furthermore enables calculation of the ejection fraction (EF), which describes the percentage value of the ventricle volume ejected during systole. It is determined by

$$EF = \frac{SV}{EDV} * 100. \quad (2.2)$$

For a healthy heart at rest, with a stroke volume of about 70 ml and an EDV of about $110 - 120\text{ ml}$, the EF amounts to about $50 - 60\%$. In cases of heart failure, the EF can decrease to about $20 - 25\%$. Therefore, knowledge of the P-V diagram is an important prerequisite in understanding myocardial diseases. [SLH11]

2.2 Heart failure

The World Health Organization (WHO) lists cardiovascular diseases (CVDs) as the global number one cause of death. In 2016, about 17.9 million people died from CVDs, representing 31 % of all global death that year. [Wor20]

In case of heart failure, the heart is unable to provide the required amount of blood flow to the cardiovascular system in order to supply all organs and tissue with oxygen. Heart failure does not directly represent a disease but rather a clinical syndrome. Nevertheless, the symptoms of different forms of heart failure are very similar and eventually manifest themselves in a decreased cardiac output. One acute consequence of heart failure, for example, is the perceiving shortness of breath. In the long term, however, severe heart failure can also lead to muscle weakness and a lack of concentration.

According to Schmidt et al. [SLH11], heart failure can be attributed to either systolic or diastolic dysfunction. Systolic dysfunction can manifest itself in several ways. One is a reduced contractility and stroke volume of the heart. Causes may be, for example, a coronary artery disease that limits oxygen supply or a preceding myocardial infarction. Secondly, there may be increased pumping resistance due to an outflow obstruction. This may be the result of arterial hypertension, among other things. Furthermore, cardiac arrhythmias or a heart attack can lead to systolic dysfunction. Figure 2.5a displays the variation of the P-V diagram, comparing a normal functioning heart (dotted line) to one impaired by heart failure with a systolic dysfunction (solid line). In diastolic functional impairment, the dysfunction is evident in the course of the filling phase. This can be triggered, among other things, by reduced compliance of the myocardium due to hypertrophy or fibrosis. The change in the P-V diagram for diastolic heart failure is illustrated in Figure 2.5b. For treatment of heart failure, drug therapy using beta-blockers is initially targeted in most cases. However, if this is not successful, the use of ventricular assist devices can be a useful alternative in order to relieve the heart and provide sufficient blood flow. [SLH11]

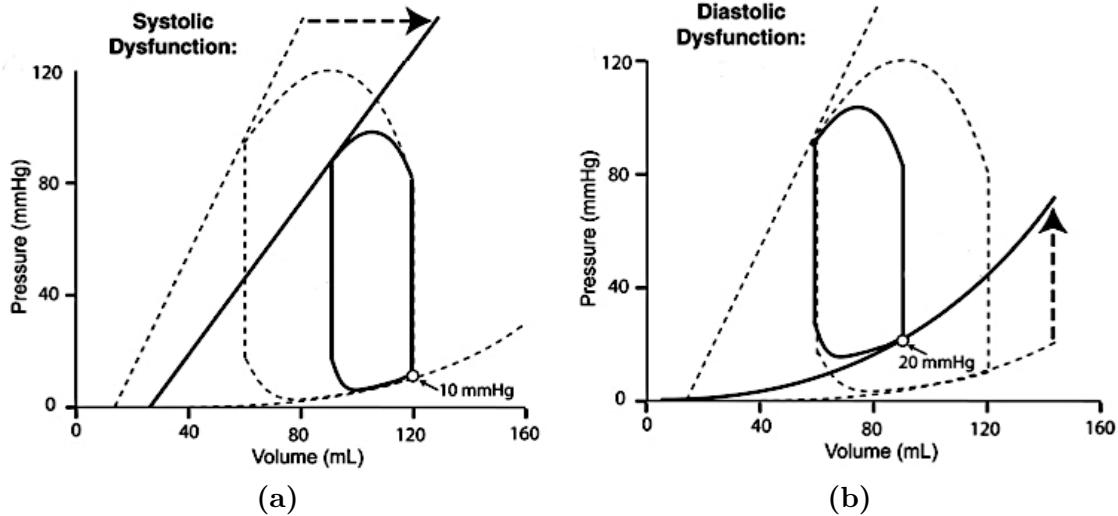


Figure 2.5: P-V diagram for heart failure in case of (a) a systolic dysfunction and (b) a diastolic dysfunction according to [KR15]. The dotted lines symbolize normal heart function in comparison to the dysfunction represented by solid lines.

2.3 Ventricular Assist Devices

Despite heart transplantation (HTx) still being the gold standard for treatment of patients with terminal heart failure [Sch10], ventricular assist devices (VADs), as a kind of mechanical circulatory support (MCS) technology, are becoming increasingly important in treating patients with CVDs. There are two reasons for this. On the one hand, CVDs are gaining in importance due to demographic change. On the other hand, there is an increasing shortage of donor organs. [DMH19]

2.3.1 Therapeutic objective

Traditionally, the therapeutic goals of VAD treatment can be divided into three categories: *bridging to transplantation* (BTT), *bridging to recovery* (BTR) and *destination therapy* (DT). However in some cases, the classification into *bridging to decision* (BTD) and *bridging to transplantability* are mentioned additionally. The decision for one of these goals is based on the type of CVD and the condition the patient is in

when receiving VAD assistance. [KSS⁺¹¹]

In clinical practice, different classification techniques connecting the patient's condition with the estimated survival time and the need for VAD assistance are used. An overview of the relation between the Interagency Registry for Mechanically Assisted Circulatory Support (INTERMACS) Score, the New York Heart Association(NYHA)-classification and the patient's condition is presented in Table 2.1. The INTERMACS Score, which is based on data from patients which have

INTERMACS Score	NYHA	Patient condition	Survival time
1	IV	critical cardiogenic shock	hours
2	IV	increasing catecholamine demand	days
3	IV	stable under inotropics	a week
4	IV	frequent decompensation	weeks-month
5	IV	rest discomfort/ not resilient	weeks-month
6	IV	rest discomfort/ merely resilient	month
7	IIIB	merely resilient	one year survival rate: 50-70%

Table 2.1: Relation between INTERMACS Score, NYHA-classification, patient condition and approximate survival time based on [Eif18].

received VAD treatment, links the need for a VAD and the appropriate time frame in which the device needs to be implanted. It is of high importance in deciding the therapeutic objective for VAD treatment. [DMH19]

The goal of *bridging to transplantation* is of great relevance with patients in NYHA-IV stadium showing hemodynamical instability. Due to a heart transplantation being the desired final treatment for these patients, there must be no contraindication to HTx. In case the patient does show a contraindication such as malignant tumors or an uncontrollable sepsis, the therapeutic objective changes from BTT to DT. In order for a treatment with a VAD as destination therapy being indicated, all conservative treatment options need to be exhausted. Due to the ever-growing shortage of donor organs, DT as a therapeutic approach in patients with heart insufficiency will become more relevant in the future even in cases usually suited for heart transplantation. [DMH19] There may occur some cases first contraindicating HTx, for which the concentration later on may dissolve. These indicate a therapy based on a *bridging to transplantability* goal. [KSS⁺¹¹]

The indication for a *bridging to recovery* approach is twofold. Either the patient shows heart failure as a result of ischemia reperfusion damage or due to infectious genesis. In the first case the myocardium usually is able to recover within a few days, whereas in the second one the potential and the time necessary for recovery depend on how badly the tissue is damaged. In either scenario, a weaning from the VAD is an essential part of therapy. [DMH19]

If a patient is admitted in cardiogenic shock and medical treatment is not sufficient, *bridging to decision* becomes a relevant form of therapy. By providing the patient with a VAD, a more accurate assessment of the patient's condition is possible. Based on this, the decision on further treatment can be analysed more thoroughly. [KSS⁺11]

2.3.2 Technology

Since the first artificial blood-pump has been implanted in 1963, technology of VADs has improved significantly [LHH⁺63].

The general aim of ventricular assist devices is to provide mechanical support in pumping blood through the human body with the heart remaining inside the patient's body. Despite there being several types of VADs, all of them are working according to the same principle. Blood is taken from the circulatory system through the pump's inlet and ejected at another location via the pump's outlet. [LW16]

VADs are differentiated by three criteria: localization of the device inside the human body, flow profile and implantation strategy.

Regarding localization of the assistance device, three different options exist. With around 93 % of all implemented devices, the most commonly used ones are left ventricular assist devices (LVADs). [DMH19] LVADs are connected to the left ventricle, from where they are pumping blood into the aorta [GSL⁺03]. The second localization option is placing the device as support for the right ventricle. These devices are therefore called right ventricular assist devices (RVADs). RVADs are positioned in a way that blood is taken from the right atrium and ejected into the pulmonary artery. [DMH19] In some cases, RVADs in combination with the aforementioned LVADs are used to build a biventricular assist device (BVAD). This type of heart support is mainly used for more severe heart diseases with a high risk of developing right heart

failure. [SH19]

The flow profile, as the second criterion for VAD distinction, is represented by pulsatile and continuous flow devices. Assistance with pulsatile devices can either be implemented to support the heart in a counter pulsation approach, working synchronous to the heart cycle, or as an asynchronous support. The most commonly known type of pulsatile device is a pneumatically driven pump ventricle. [LW16] However, according to the INTERMACS, over 95 % of all implanted devices are continuous flow devices [KPK⁺17]. These, in their most commonly used form, are electrically driven rotational blood pumps. A technological difficulty with these devices is the high probability of blood damage due to small gaps and very high rotational speed. However, these devices enable a dynamic adaption to the patient's physiological needs by being able to quickly adjust parameters such as the motor current. The possibility to keep track of these signal characteristics furthermore makes it possible to detect malfunctions or misplacement of the pump. [LW16]

Implantation of the VADs can be performed in one of three ways: paracorporeal, intracorporeal or percutaneous [DMH19]. For VAD systems which follow a paracorporeal approach, only the in- and outflow cannulas are located inside the human body. The cannulas are connecting the pump located outside the body with the ventricle and the vessels. Due to the pump being placed outside of the patient's body, these systems provide the option for pediatric MCS. This is not possible for most other systems due to the device being too large to fit inside a child's body. [SBL19] One example for paracorporeal systems are the aforementioned pneumatically driven pump ventricles [LW16]. In contrast to the paracorporeal devices, where the pump itself as well as its control unit are situated outside the body, in percutaneous devices the pump is placed inside the body. The control unit, however, remains outside the patient's body and is connected to the pump via leads. The intracorporeal devices are fully implanted into the body. [SBL19]

As far as the other two criteria for VAD differentiation are concerned, all combinations of localization and flow control are possible [SBL19]. As an example of a percutaneous device, [DMH19] names the Impella 2.5, a rotary blood pump with continuous flow used for left ventricular assistance.

The proportions of different VAD types and therapeutic goals, as based on the International Mechanically Assisted Circulatory Support (IMACS) register are illustrated in Table 2.2.

VAD type		Therapeutic objective	
LVAD	93%	DT	40%
BVAD	4%	BTD	30%
TAH	2%	BTT	29%
unknown	0.1%	others (BTR, ...)	1%
RVAD	0.05%		

Table 2.2: Percentages of VAD types and therapeutic objectives in mechanical heart support based on [DMH19].

3 Control Theory

Since this thesis addresses the implementation of flow control algorithms for a left ventricular assist device, this section will focus on the fundamentals of notation and structure of a standard control loop. Furthermore, the basic principles of PI-controllers and iterative learning control (ILC) are discussed, since these are used within the practical part of the thesis.

3.1 Fundamentals

The basic task of control engineering is to externally influence a time-varying process with the goal of executing the process in a predetermined manner. A control system is characterized in particular by the feedback of the controlled variable to the reference variable. The reference variable comprises the state that has to be achieved. In theory, this is represented by a control loop with the components shown in Figure 3.1. The plant $G(s)$ transfers the actuating variable $u(t)$, as well as the influence of the disturbance $d(t)$, to the controlled variable $y(t)$. This variable is permanently compared with the reference variable $w(t)$ by means of a feedback loop, providing the control error

$$e(t) = w(t) - y(t). \quad (3.1)$$

The controller $G_c(s)$ then transforms the control error to the actuating variable again. The aim of the control loop is to achieve the smallest possible control error with the highest possible damping. Since these goals contradict each other, a trade off must

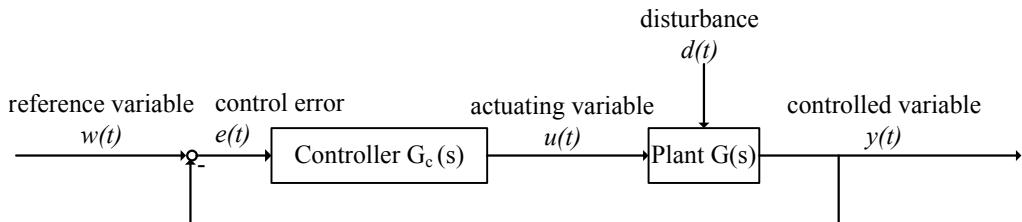


Figure 3.1: General structure of a control loop

always be accepted here. [ZR17]

However, there are some general requirements for the closed control loop which have to be fulfilled. The first requirement states that the closed loop needs to be stable, which is met if the control loop responds to a finite excitation with a finite output signal. The second condition is the requirement for disturbance rejection, stating that the controlled variable needs to follow the reference variable asymptotically, so that

$$\lim_{t \rightarrow \infty} e(t) = 0. \quad (3.2)$$

Another requirement is that the dynamic relationship between the reference variable $w(t)$ and the controlled variable $y(t)$ must satisfy specified quality requirements. Finally, these three requirements must be satisfied despite uncertainties in the plant, forming the robustness requirement. More detailed information on these requirements can be found in [Lun10].

The plant $G(s)$ corresponds to the part of the system in which the physical quantity to be controlled is influenced by the controller. The calculation of the plant by setting up and solving differential equations is possible only in a few cases. Furthermore, calculation in many cases is very time consuming. Due to this, the determination of the plant's characteristic values is usually carried out experimentally. There are several basic types of plants, classified according to their dynamic behavior. As only the PT₁-element is used in the practical part of this thesis, all other variations will not be discussed at this point. Detailed information on this topic can, once more, be found in [Lun10].

The PT₁-element is the plant type which is most common in technical equipment. A PT_n-element in its steady state reacts proportionally to the input value and has a distinct transition behavior. The index n describes the order of the system. Therefore, a PT₁-element is a proportional delay element of first order. The mathematical formulation of the transfer function of a PT₁-element is

$$G(s) = \frac{k_s}{1 + sT}. \quad (3.3)$$

The value k_s describes the static gain, which for a unit step and $h(t = 0) = 0$ is defined as

$$k_s = h(t \rightarrow \infty). \quad (3.4)$$

The time constant T gives an impression of the speed with which the system can react to changes at the input. It is defined as the time at which the transfer function reaches 63 % of its static gain. [Lun10] Figure 3.2 shows the transfer function of a PT_1 -element (blue curve) and its significant parameters.

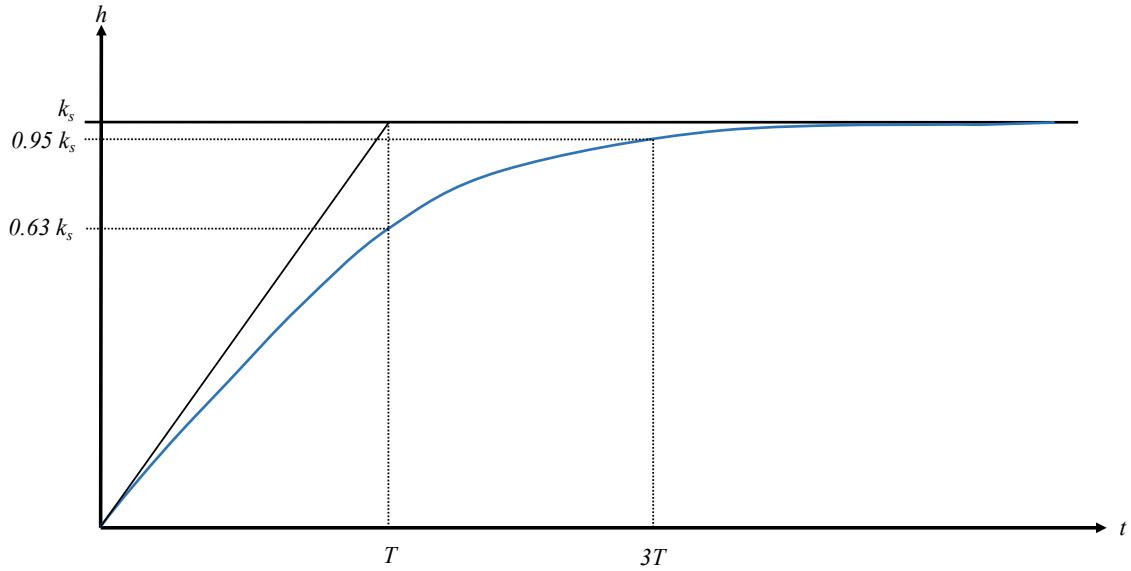


Figure 3.2: Transfer function of a PT_1 -element [Lun10].

3.2 PI-controller

A PI-controller is a control structure commonly used for linear systems. This structure consists of both a proportional (P) and an integral (I) control element. The output value of a P-controller is proportional to its input value. In relation to the control loop in Figure 3.1 this leads to

$$u(t) = K_P e(t). \quad (3.5)$$

Using Laplace transformation, the transfer function for a P-controller can be determined as

$$G(s) = \frac{u(s)}{e(s)} = K_P. \quad (3.6)$$

Therefore, the step response of this controller equals a step weighted with the parameter K_P .

The relationship between input and output value of an I-controller is described through

$$u(t) = K_I \cdot \int e(t)dt. \quad (3.7)$$

Just as for the P-controller, Laplace transformation can be used to determine the transfer function of the I-controller. This leads to

$$G(s) = \frac{u(s)}{e(s)} = \frac{K_I}{s}, \quad (3.8)$$

which indicates a step response in form of a ramp with slope K_I . In order to generate a PI-controller, the elements from (3.5) and (3.7) can be added, which leads to

$$u(t) = K_P e(t) + K_I \cdot \int e(t)dt. \quad (3.9)$$

The Laplace transformation can be used again to compute the transfer function

$$G(s) = \frac{u(s)}{e(s)} = K_P + \frac{K_I}{s}. \quad (3.10)$$

The step response of the PI-controller, illustrated in Figure 3.3, shows both the weighted step from the P-controller and the ramp from the I-controller.

3.2.1 Tuning rules

Tuning the controller parameters, i.e adjusting their values depending on the system, is of great importance. Incorrectly chosen parameters can lead to poor performance or unstable system behavior, which may result in system damage. There are many different approaches to tune a PI-Controller in order to achieve optimal system performance. These range from heuristic methods over analysis of pole-zero plots to computer-aided numerical parameter optimization. [Lun10] At this point, the tun-

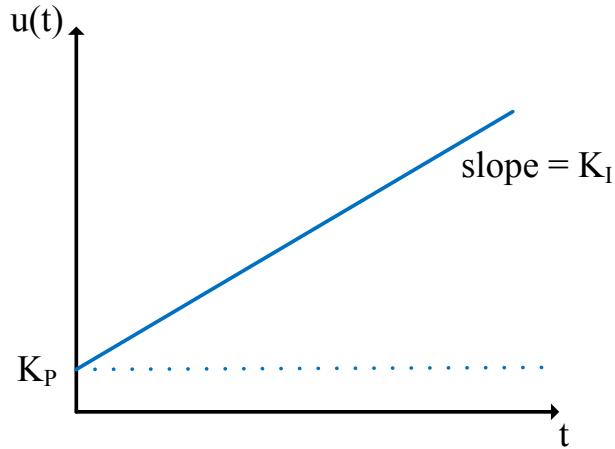


Figure 3.3: Step response of a PI-Controller based on [ZR17].

ing rules according to Ziegler Nichols (ZN) and the rules according to Chien Hrones Reswick (CHR) will be discussed, as these are used for the implementation of flow control in the practical work. Information on other approaches can be found in [AHR11].

Tuning rules according to Ziegler Nichols

The tuning rules according to Ziegler Nichols are one of the most commonly used heuristic methods in tuning controller parameters for PI-controllers. They are used especially if a mathematical model of the plant is not available but the plant can be approximated as a PT_n -element. [ZR17] A necessary condition is the possibility to experimentally identify the step response of the plant without risk of damage to the system. After the step response has been determined, it is displayed graphically. Then the inflection tangent is drawn into the step response as shown in Figure 3.4. The blue line represents the step response, the red line the inflection tangent, respectively. The gain K_S , the delay time T_v and the settling time T_g can be read from the graph. Using these, following [ZR17], the factor K_P is calculated as

$$K_P = 0.9 \cdot \frac{T_g}{K_S T_v}. \quad (3.11)$$

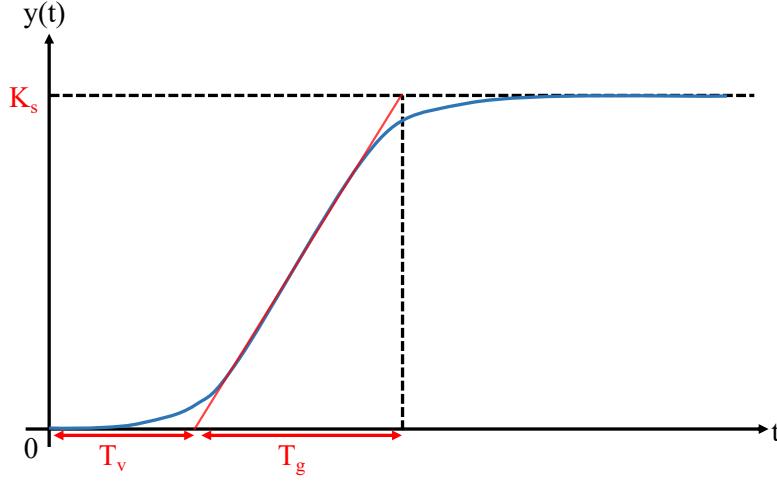


Figure 3.4: Inflection tangent method for Ziegler Nichols and Chien Hrones Reswick based on [ZR17].

The factor K_I is calculated according to:

$$K_I = \frac{K_P}{T_N}, \quad (3.12)$$

with

$$T_N = 3.3 \cdot T_v. \quad (3.13)$$

Tuning rules according to Chien Hrones Reswick

The tuning method according to Chien Hrones Reswick is very similar to the one by Ziegler Nichols. However, this method provides the ability to adjust the transient response of the control loop. The tuning parameters can either be chosen in a way to provide an overdamped behavior or a course providing 20 % overshoot. [AHR11] For both options, the step response and its inflection tangent are graphically displayed, as for the Ziegler Nichols approach in Figure 3.4. The values for K_S , T_v and T_g can be read from the plot. The parameter value K_I again is calculated following (3.12). The formulas for calculating K_P , T_N and T_D are given in Table 3.1.

overdamped		20% overshoot	
K_P	T_N	K_P	T_N
$0.35 \cdot \frac{T_g}{K_S T_v}$	$1.2 \cdot T_v$	$0.6 \cdot \frac{T_g}{K_S T_v}$	T_v

Table 3.1: Tuning parameters according to Chien Hrones Reswick based on [ZR17].

3.3 Iterative Learning Control

The use of iterative learning control aims to improve control performance for systems which execute the same task repeatedly under constant operating conditions. This improvement is based on the idea that it is possible to include error information from previous iterations into the adjustment of the actuation variable during the current iteration. The standard control structure of an ILC algorithm is presented in Figure 3.5.

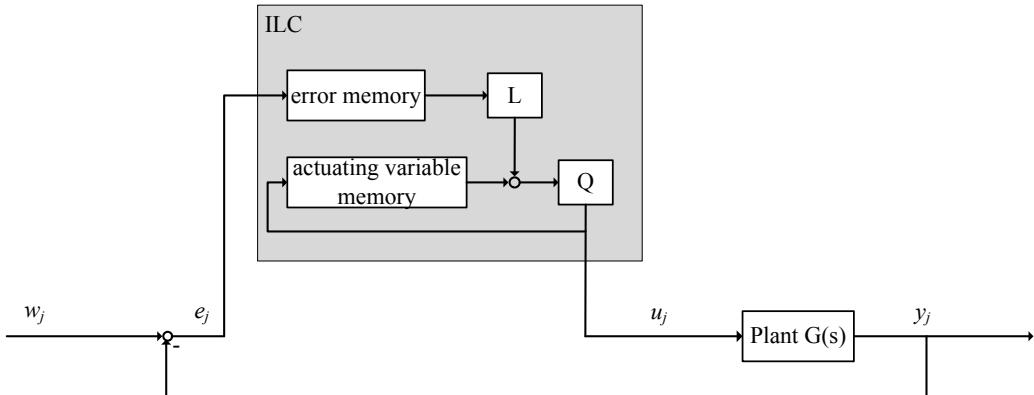


Figure 3.5: Standard ILC control loop based on [BTA06].

Considering a linear-time-invariant single-input-single-output (SISO) system, the ILC learning algorithm is as follows:

$$u_{j+1} = Q(q)[u_j(k) + L(q)e_j(k+1)] \quad (3.14)$$

where k is the time index, j is the iteration index, q is the forward time-shift operator $qx(k) \equiv x(k+1)$, $Q(q)$ is defined as the Q-Filter and $L(q)$ represents the learning

function. The performance error signal e_j is defined as

$$e_j = w_j - y_j. \quad (3.15)$$

Feedback controllers such as PI-controllers are only able to consider the current changes in control error. By taking into account the information from previous iterations, low tracking errors are achievable through an ILC. This results in exceptional performance with convergence during the first few iterations. This can be achieved even for systems prone to repeating disturbances and model uncertainties. While feedback control shows a lag in transient tracking due to reacting to inputs and disturbances, ILC, as a feedforward controller, does not. Another advantage of ILC use is that there is no need for disturbances to be known or measured, as long as these signals show repeating behavior during each iteration. Furthermore, by storing signal information during each iteration, ILC enables advanced filtering and signal processing of the control error. However, ILC utilization holds some issues in regard to non-repeating disturbances or noise influences. In these cases it may be useful to combine ILC approaches with a feedback controller. A combination of the systems is furthermore required if the behavior of the plant is not stable. [BTA06] A parallel architecture of a feedback controller in combination with an ILC is illustrated in Figure 3.6.

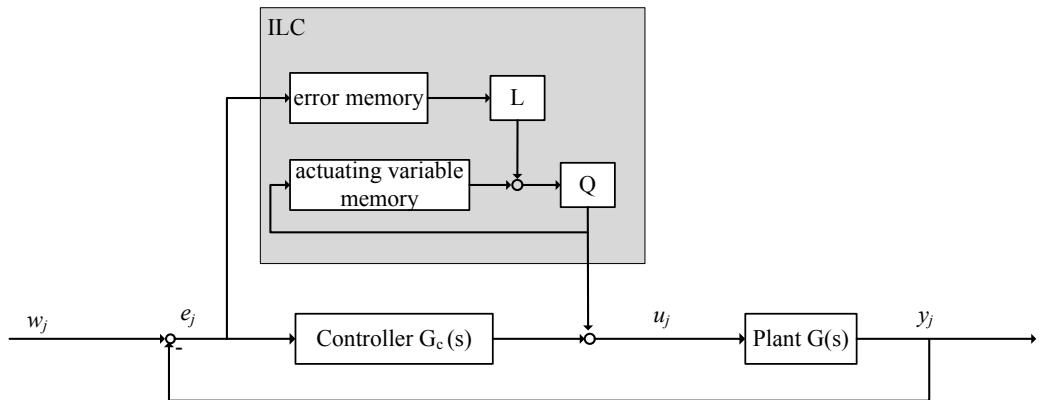


Figure 3.6: Parallel architecture of ILC with feedback controller based on [BTA06].

There are several approaches to design an ILC. In general, an ILC ideally learns only the repeating disturbance patterns without being influenced by noise. The most common types of ILC learning functions are the P-, D- and PD-type learning func-

tions. As an ILC does have a natural integrator action from one iteration to the next, I-type learning functions are rarely used.

The discrete-time learning function for a standard PD-type ILC is given as

$$u_{j+1}(k) = u_j(k) + k_p e_j(k) + k_d [e_j(k+1) - e_j(k)]. \quad (3.16)$$

k_p represents the proportional gain while k_d is the derivative gain. In case a P-type learning function is implemented, the derivation gain is set to $k_d = 0$. For a D-type learning function, $k_p = 0$ is used, respectively.

The performance of these ILC types depends mainly on accurate parameter tuning and does not require an accurate mathematical model of the plant. Despite these approaches being frequently used, there are no tuning guidelines similar to the ones mentioned for PI-controller tuning. However, a commonly used way to influence the process behavior is to modify the learning algorithm to include a Q-Filter. This filter can be used to disable learning at high frequencies in order to filter noise at these frequencies. This increases robustness of the system. First, a filter type such as Butterworth or Chebyshev is specified. The bandwidth can then be interpreted as a tuning parameter in addition to the proportional gain k_p . Initially, learning gain and filter bandwidth are set to low values. When a steady baseline behavior and error performance is achieved, the parameter values can be increased to improve performance. The learning gain influences the rate of error convergence while the Q-Filter influences the error performance. Performance increases proportionally with filter bandwidth. However, this includes a trade-off with robustness. For lower filter bandwidth, high robustness can be achieved in a trade-off with performance.

Besides the P-,D- and PD-type ILC there are other design approaches. The H_∞ method can be used to design a robustly convergent ILC controller, with a trade-off in performance. A quickly converging ILC approach can be achieved by using the plant inversion method. This however depends on accurate modeling of the plant. The quadratically optimal ILC approach uses quadratic performance criteria to design an optimal ILC. Further information on these alternative design methods is provided in [BTA06].

4 Identification

4.1 Sputnik VAD

The Sputnik VAD is an axial-flow blood pump, developed in a cooperative project of the National Research University of Electronic Technology, OJSC Zelenograd Innovation-Technology Center of Medical Equipment, FSBI "Academician V.I. Shumakov Federal Research Center of Transplantology and Artificial Organs", Ministry of Health of Russian Federation, DONA-M LLC and BIOSOFT-M LLC in 2009. [ST15]

This device is used for left ventricular assistance in patients with acute heart failure. The therapeutic objective in implantation of a Sputnik VAD is bridging to transplantation. The VAD is able to pump up to 10 liters of blood per minute with a continuous flow profile. The implantable pump weighs about 200 g, has a length of 81 mm and a maximum diameter of 34 mm. It consists of a moving and a stationary part. The moving part, the impeller, a rotor with four blades, contains a permanent NdFeB-magnet, which is actuated by a brushless DC motor. The rotor spins clockwise with speed values between 4000 – 10000 rpm. An overview of the pump's specification is presented in Table 4.1.

Blood flow	0-10 l/min
Rotational speed	4000-10000 rpm
Length	81 mm
Diameter	34 mm
Weight	200 g

Table 4.1: Specifications of Sputnik VAD

The stator is located inside a titanium housing with a diameter of 16 mm. The stationary part of the pump consists of a flow straightener with three stationary blades and a flow diffusor with three twisted blades. The flow straightener is located in front of the rotor and straightens the incoming blood flow into the rotor. Behind the rotor, blood is directed into the diffusor. Figure 4.1 depicts a cross-section of the Sputnik VAD and identifies its individual components. The connection between the

pump and the cardiovascular system is performed using in- and outflow cannulas, a felt ferule and vascular prosthesis which is sewed to the aorta. [ST15]

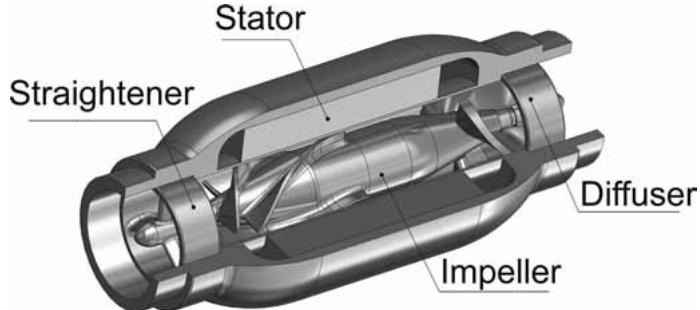


Figure 4.1: Cross-section of the Sputnik VAD [ST16].

The Sputnik VAD is powered using two lithium-ion batteries, fully charged providing enough energy for up to eight hours of system support. The maximum charging time for the batteries is less than five hours. During this time the batteries can either be exchanged by another set of batteries or the system can be powered through connection to an AC network. A microprocessor-based driving unit is used to regulate the pump speed, manage the power supply and store parameter data. It is connected percutaneously to the pump with an up to 170 cm long and 5 cm wide lead. [ST15] During the practical part of this work, the pump was controlled using the servo controller module ESCON 50/4 EC-S from maxon motor. This is a 4-quadrant pulse width modulation controller for controlling motors without Hall sensors.

4.2 Hardware in the Loop Test Bench

For all measurements and tests performed during this thesis, a hardware in the loop (HiL) test bench of the Chair of Medical Information Technology at RWTH Aachen University was used. The test bench is set up as a feedback controlled human circulatory system simulator. With the aid of the test rig, it is possible to test MCS systems under various physiological and pathological conditions of the CVS.

The structure of the mock circulatory loop (MCL) is depicted in Figure 4.2. The boxes marked V_1 and V_2 are pressure compartments simulating the volume of the left ventricle and the aorta, respectively. Therefore, the pressure values of these

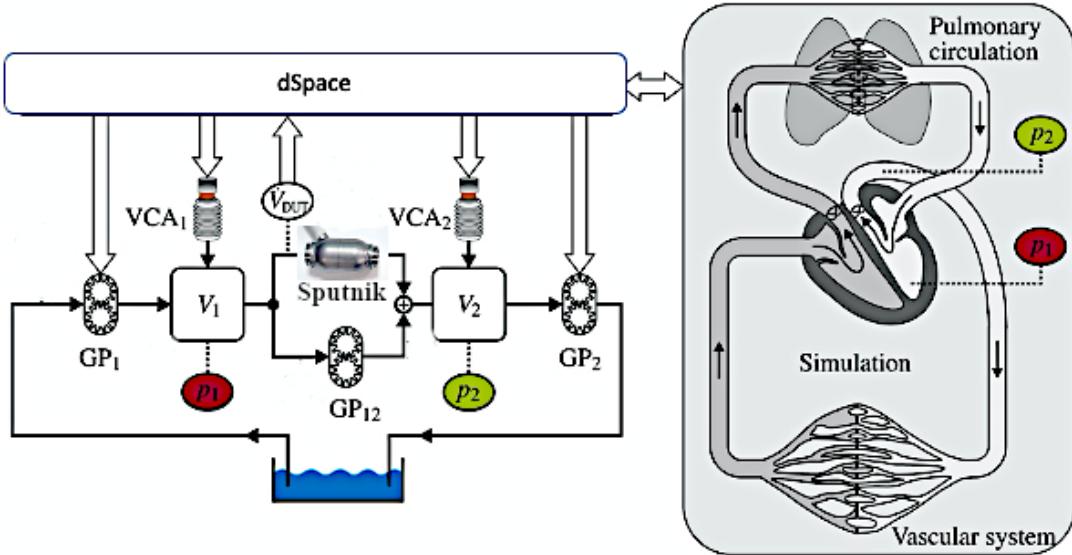


Figure 4.2: Structure of the HiL human circulatory system simulator based on [MRS⁺15].

compartments, referred to as p_1 and p_2 , can be physiologically compared to the pressure values of the left ventricle and aorta. The MCL is actuated by three gear pumps (GP_1 , GP_{12} and GP_2) and two voice coil actuators (VCA_1 and VCA_2). The Sputnik VAD is connected to the pressure chambers in parallel, enabling tests similar to real use cases. This way, the VAD can be subjected to comparable pressure changes in the differential pressure between the aorta and ventricle as would be the case when used on the beating heart.

By controlling the MCL through a dSpace system (DS1103), pressure in the chambers can be adjusted in real time to simulate different cardiac dysfunctions. The dSpace system furthermore enables recording of reference signals presented to the MCL, as well as real time measurements.

As the Sputnik VAD is not usually included into the MCL setup, flow through the device can not be measured without further equipment. For this purpose the Transonic Systems Inc. T110 flowmeter is included in the setup. The flow sensor measurement is based on ultrasonic technology. The sensor probe, as presented in Figure 4.3, is mounted onto the tube leading from the pressure chamber representing the left ventricle to the VAD. The flowmeter too is connected to the dSpace system,

4 Identification

enabling recording of the measured flow values. In Figure 4.2 the measurement of the device is represented by \dot{V}_{DUT} .

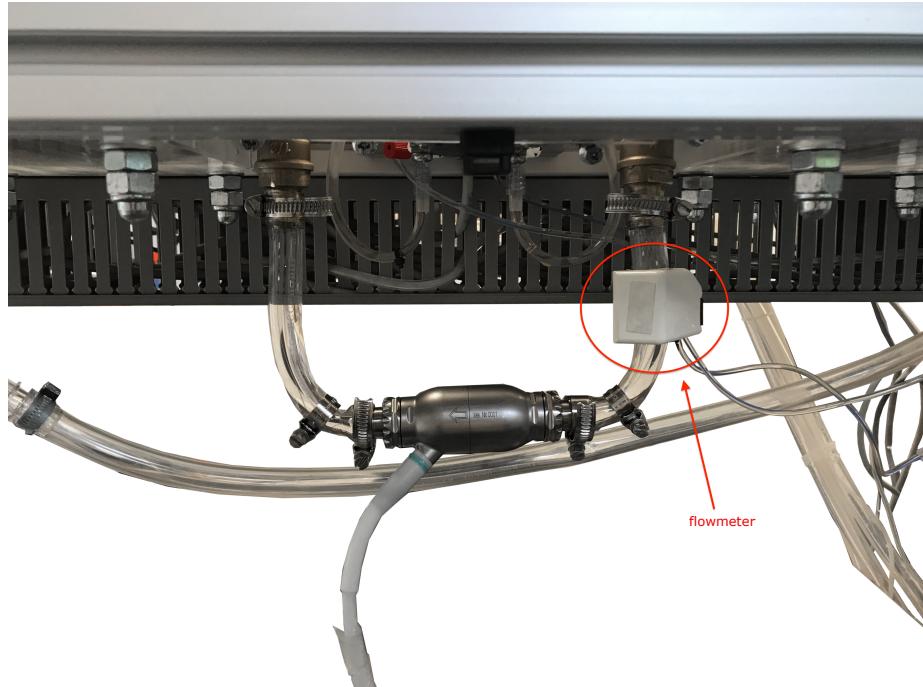


Figure 4.3: Sputnik VAD and flowmeter in HiL setup.

The ESCON servo controller mentioned in chapter 4.1, as well as the flowmeter and the MCL, is connected to the dSpace system. Using the digital input port of the controller, a set value for regulation of the rotational speed can be transferred to the controller after defining the value in the system.

The dSpace system itself is controlled with the use of the program ControlDesk. This software provides the opportunity to include Matlab and Simulink source code. By this, controllers designed with the use of Simulink can directly be tested at the HiL test bench. It furthermore enables downloading all measured data in form of Matlab matrices.

4.3 System Identification

For the implementation of flow control algorithms for the Sputnik VAD, knowledge of the system behavior is required. In order to gain this information, various tests have been performed to determine a static map for the system. For this purpose, a multiple-input-single-output (MISO) system with input variables differential pressure Δp in $mmHg$, rotational speed v in rpm and output variable blood flow q in l/min is assumed. The differential pressure is defined as

$$\Delta p = p_{ao} - p_{lv} = p_2 - p_1, \quad (4.1)$$

with p_{ao} depicting the pressure of the aorta and p_{lv} corresponding to the left ventricular pressure.

Using the HiL test rig, the differential pressure was increased in steps of 20 mmHg starting at 0 mmHg and ending at 140 mmHg . For each differential pressure step, the reference speed of the pump was increased from 4000 rpm in steps of 1000 rpm to 9000 rpm . Flow for each reference speed was measured for 5 s . In order to eliminate inaccuracies due to transient processes, solely the last quarter of each measurement stage was considered for the evaluation using Matlab. Figure 4.4 depicts the signal curves for the measurement described above. The upper graph shows the course of the reference differential pressure (Δp_{ref}) and the differential pressure measured at the HiL test stand (Δp_{HiL}). In the middle, the curves of the reference velocity (v_{ref}) and the measured velocity of the Sputnik VAD (v_{vad}) are shown. The lower graph shows the resulting flow through the blood pump (q_{vad}).

To determine the static map, the flow data is first broken down into individual parts corresponding to the various differential pressure levels. These are then split into data sections for each velocity rate. Finally, the mean of the last quarter of each section is calculated. The average flow values are then displayed as a function of the differential pressure. The values of equal velocity levels are connected with each other.

At the beginning of the practical work, the Sputnik VAD was connected to the test stand via tubes of about 30 cm length on both sides. Since in clinical use, the pump is implemented in the patient's body and connected to the left ventricle and aorta, the tube length is not representative of a real application. To test the effect tube length

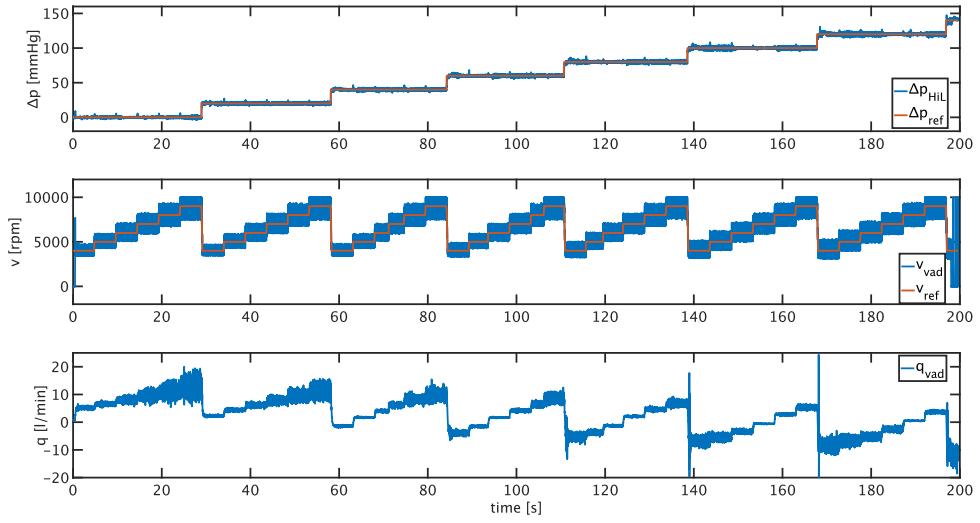


Figure 4.4: Signal curves for creation of the static map for 60 % water, 40 % glycerin solution with 15 cm long tubes. Top: differential pressure, middle: rotational speed, bottom: flow through VAD.

has on the operating range of the pump, three different tube lengths for attachment of the VAD to the test rig are compared. The measurements have been performed with tubes of approximately 5 cm, 10 cm and 15 cm length. Figure 4.5 depicts the static maps for all three tube lengths measured with a fluid solution of 60 % water 40 % glycerin.

Under inspection of the blue curves corresponding to a tube length of 5 cm it is evident that measurements in this case were only performed up to a differential pressure of $\Delta p = 100 \text{ mmHg}$. This is a result of the abrupt change in differential pressure and reference speed which lead to spontaneous reduction of the flow and possibly high backflow values through the pump. As a result, the pump's rotor comes to a stop. For longer tubes (10 cm and 15 cm length) and therefore, higher flow resistance, this phenomenon occurs at a differential pressure $\Delta p = 140 \text{ mmHg}$. However, the deviation of the curves is insignificant when comparing all three cases. Due to this the tubes of 15 cm length were chosen for reasons of improved handling of the MCL.

In addition to different tube lengths, another preliminary investigation was carried out with regard to the influence of the test liquid used. Since blood viscosity varies between patients and also with fluid intake, knowledge on the effect a change in

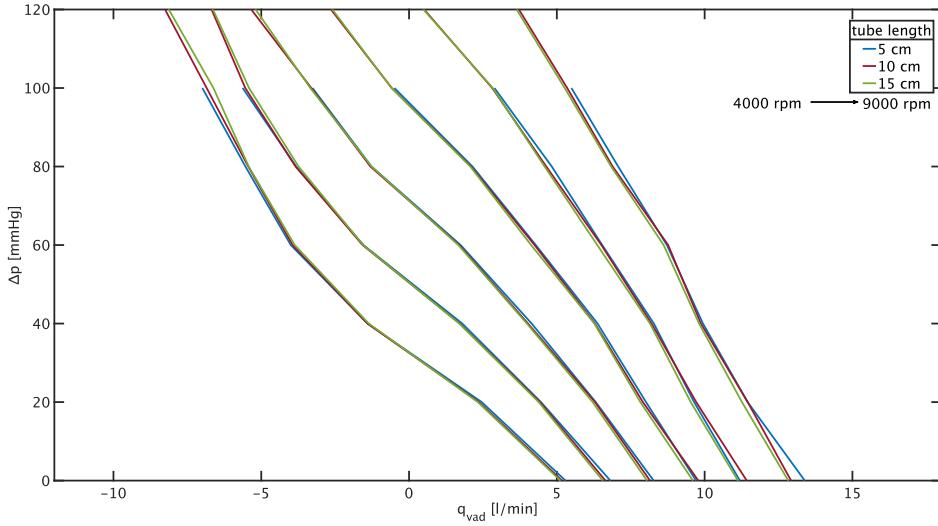


Figure 4.5: Static map for varying tube length in 60 % water 40 % glycerin solution.

liquid condition has on the control performance is required. The same measurements for determining the static map were performed in pure water, a solution of 80 % water 20 % glycerin, a solution of 60 % water 40 % glycerin and a solution of 40 % water 60 % glycerin. Representing the static maps for all four solutions measured, Figure 4.6 discloses significant deviations between the fluids.

Since the resistance of the liquid falls with decreasing proportion of glycerin in the solution, differences in reachable differential pressure occur due to the aforementioned reason of spontaneous increase in backflow. However, as the fluid resistance increases, the pumpable flow decreases. All further measurements of this thesis are performed for a solution of 60 % water 40 % glycerin as this mixture most closely reflects the standard properties of blood. While Figure A.1 to Figure A.3 in the appendix show comparisons of the static maps for varying tube length in different mixing ratios of water and glycerin, Figure A.4 and Figure A.5 depict comparisons of the static maps for varying solutions with 5 cm and 10 cm tube length. The resulting static map for the chosen final setup of the MCL is depicted in Figure 4.7.

As part of the system identification, the transfer function of the Sputnik VAD is determined. For this purpose, the step response of the pump to a 1000 rpm step in reference speed is analyzed.

Initially, the measured flow values from the static map determination measurement

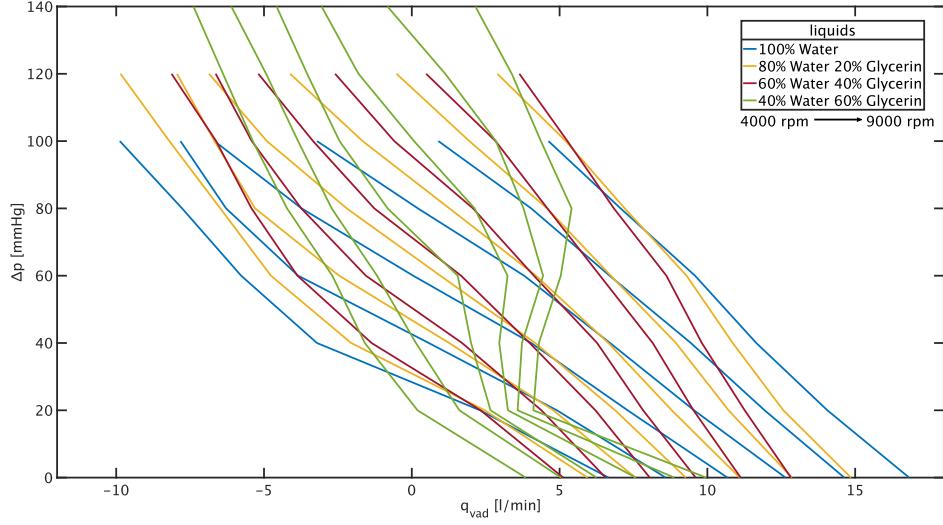


Figure 4.6: Static map for varying fluid solutions with 15 cm long tubes.

are prepossessed by using a 2nd-order butterworth filter with a cut-off frequency of $f_c = 5 \text{ Hz}$ and sampling frequency $f_s = 1000 \text{ Hz}$. For determination of the transfer function, filtered flow for an increase from $v_{ref,low} = 5000 \text{ rpm}$ to $v_{ref,high} = 6000 \text{ rpm}$ in reference speed at a differential pressure of $\Delta p = 40 \text{ mmHg}$ is analyzed. The blue line in Figure 4.8 depicts the filtered flow for this measurement. It is evident that the system's behavior can be approximated by a PT_1 -element. The characteristic parameters of the transfer function according to equation (3.3) are represented in Figure 4.8. The static gain k_s is determined as

$$k_s = \frac{k_{high} - k_{low}}{v_{ref,high} - v_{ref,low}} = 0.0018 \quad (4.2)$$

with $k_{high} = 2.3008$ and $k_{low} = 0.4672$. The time constant T , defined as the time span between initialization of the jump and reaching $0.63 \cdot k_s$, is determined to $T = 0.081$. According to equation (3.3) the transfer function for the plant results in

$$G(s) = \frac{0.0018}{1 + 0.081s}. \quad (4.3)$$

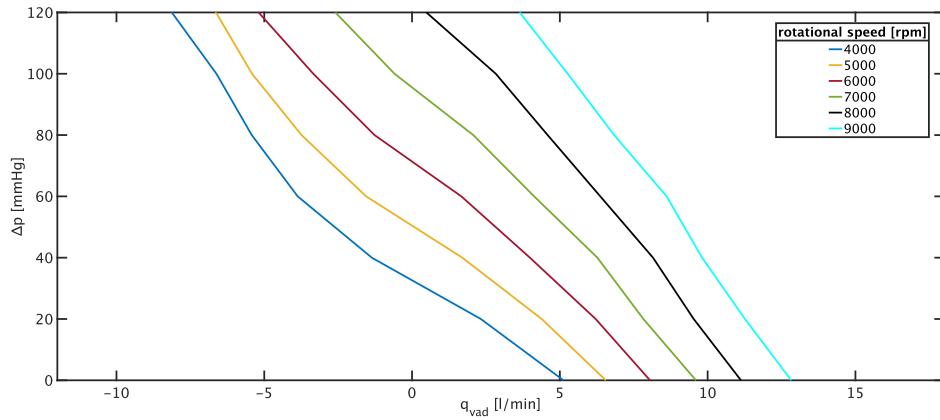


Figure 4.7: Static map for solution of 60 % water 40 % glycerin with 15 cm long tubes.

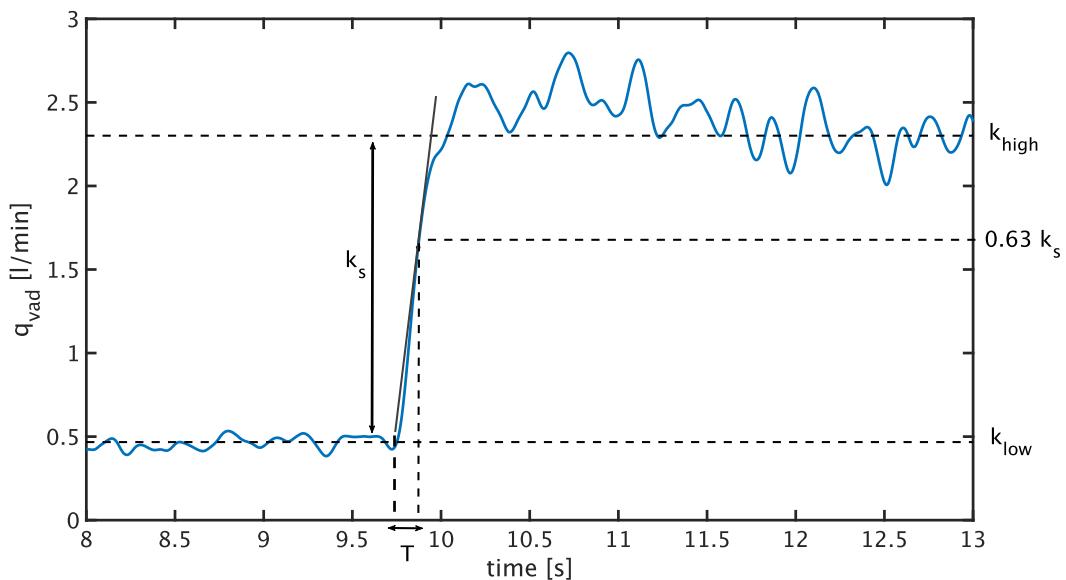


Figure 4.8: Step in flow, triggered by a step in reference speed by 1000 rpm with identification of the variables for determining the transfer function of a PT_1 element.

5 Flow Control

In this chapter, implementation and evaluation of various control algorithms for flow control purposes will be presented. At first, the aim is to enable regulation of flow to a constant value. Later on, the system's ability to follow different reference flow trajectories will be tested. In a final step, the system will be subjected to disturbances through the HiL test rig in form of heart beats at different heart rates. Performances of the implemented control algorithms will be compared.

5.1 PI Controller

PI control implementation is performed on the basis of the tuning rules according to Ziegler Nichols as well as according to Chien Hrones Reswick (Chapter 3.2.1). The performance of both controllers later on is compared and evaluated.

5.1.1 Design and Implementation

As a preparation for utilization of the inflection tangent method for these tuning approaches, a measurement similar to the one for determining the static map is performed. Figure 5.1 depicts the signal curves for determination of the tuning parameters. As presented in the upper graph, differential pressure is increased in steps of 20 mmHg from $\Delta p = 0 \text{ mmHg}$ to $\Delta p = 100 \text{ mmHg}$. For each level the sequence of reference velocities depicted exemplary for $\Delta p = 40 \text{ mmHg}$ in the center graph of Figure 5.2 is targeted. Starting at $v_{ref} = 4000 \text{ rpm}$ the velocity is first increased in three steps of varying height and then decreased by the same values. The first step amounts to 200 rpm , the second to 400 rpm and the third to 600 rpm . The reference value is then increased by 1000 rpm and again the three steps are executed. This sequential behavior is repeated up to a start value of $v_{ref} = 8000 \text{ rpm}$. For determination of the parameters for controller design the step from $v_{ref,low} = 5000 \text{ rpm}$ to $v_{ref,high} = 5400 \text{ rpm}$ at $\Delta p = 40 \text{ mmHg}$, which is located in the center of the pump's

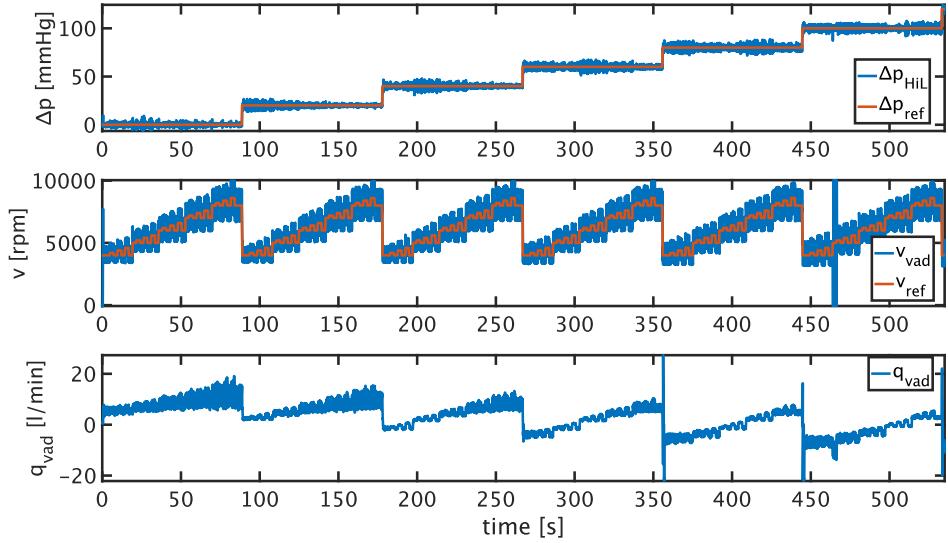


Figure 5.1: Signal curves for determination of PI controller parameters. Top: differential pressure as reference and measured signal, middle: reference and measured rotational speed, bottom: measured flow through Sputnik VAD.

operating range, is used. Since the flow signal is affected by high measurement noise, the signal is preprocessed using an 8th-order butterworth filter with cut off frequency $f_c = 5 \text{ Hz}$ and sampling frequency $f_s = 1000 \text{ Hz}$. The resulting signal and the characteristic parameters needed for parameter tuning of the PI controller are depicted in Figure 5.3. With $k_{high} = 2.8149$ and $k_{low} = 1.7783$ the static gain is determined as in equation (4.2) to

$$k_s = \frac{k_{high} - k_{low}}{v_{ref,high} - v_{ref,low}} = 0.0026. \quad (5.1)$$

The time constants amount to $T_g = 0.193$ and $T_v = 0.1$.

For determination of a PI controller tuned according to Ziegler Nichols equations (3.11) to (3.13) are used. By this K_P is determined as

$$K_P = 0.9 \cdot \frac{0.193}{0.0026 \cdot 0.1} = 670.3052 \quad (5.2)$$

and K_I as

$$K_I = \frac{670.3052}{3.3 \cdot 0.1} = 2031.2278. \quad (5.3)$$

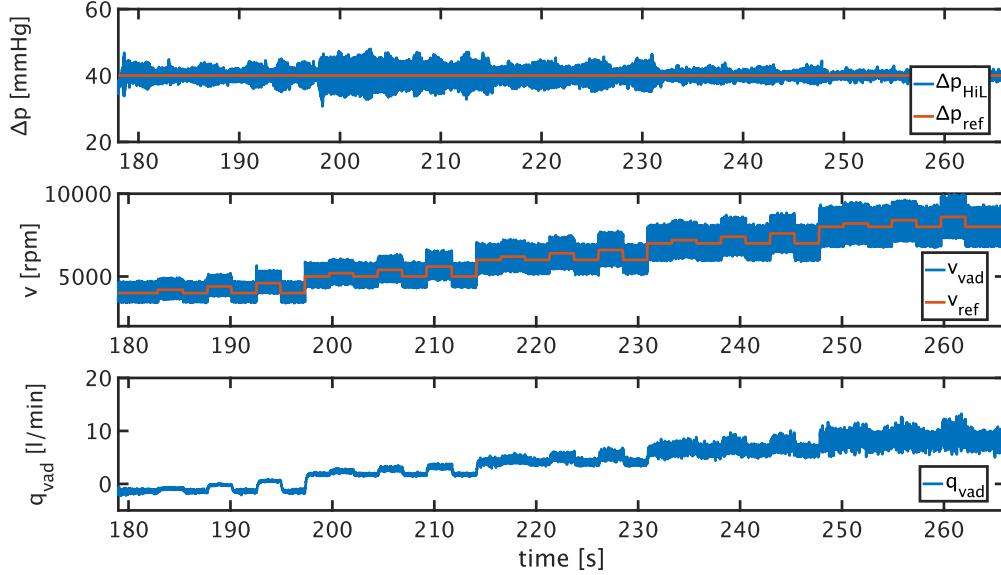


Figure 5.2: Signal curves for determination of PI controller parameters at $\Delta p = 40 \text{ mmHg}$.

Substituting these values in equation (3.10) results in the transfer function

$$G_{PI,ZN}(s) = 670.3052 + \frac{2031.2278}{s}. \quad (5.4)$$

Calculation for overdamped controller behavior was chosen for controller tuning using Chien Hrones Reswick. Determination of the parameters K_P and K_I is performed following the equations presented in Table 3.1, resulting in

$$K_P = 0.35 \cdot \frac{0.193}{0.0026 \cdot 0.1} = 260.6742 \quad (5.5)$$

and

$$K_I = \frac{260.6742}{1.2 \cdot 0.1} = 2172.2853. \quad (5.6)$$

This in turn leads to the transfer function

$$G_{PI,CHR}(s) = 260.6742 + \frac{2172.2853}{s}. \quad (5.7)$$

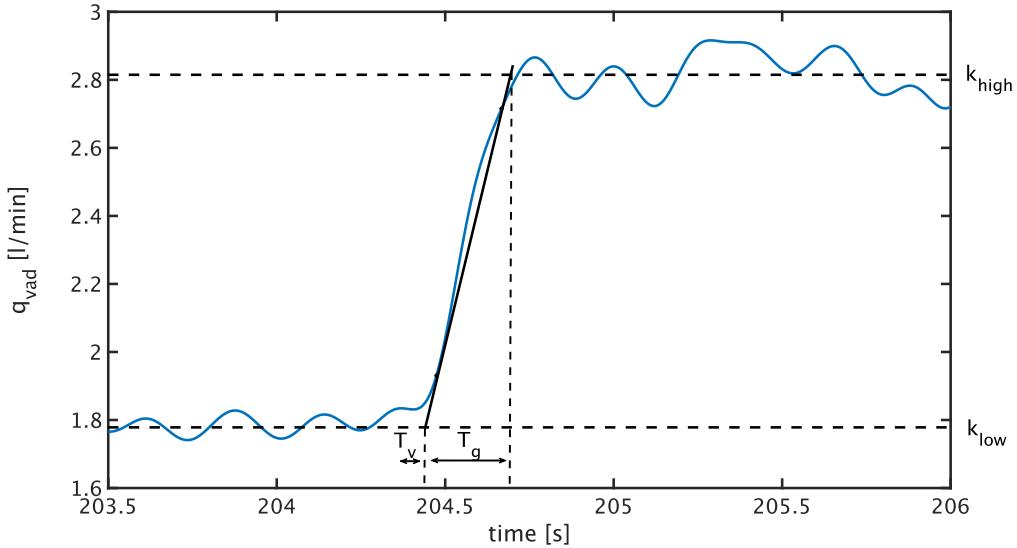


Figure 5.3: Step response for a step in rotational speed of 400 rpm for determination of PI controller tuning parameters.

5.1.2 Evaluation

The main purpose for utilization of a PI controller, in this work, is to stabilize the closed loop system behavior in preparation for an ILC implementation. Both controllers are tested under the same operating conditions and their performance is compared.

Even though the controllers are tuned at $\Delta p = 40 \text{ mmHg}$, both of them are tested in the differential pressure operating range from $\Delta p = 0 \text{ mmHg}$ to $\Delta p = 100 \text{ mmHg}$ to ensure sufficient performance in all use cases. For each differential pressure level three consecutive steps up and down throughout the operating range of flow are performed. Each reference flow is targeted for 5 s and flow through the VAD is measured. A graphical representation of the reference signal curves is depicted in Figure 5.4. Figure 5.5 depicts the differential pressure and flow reference values, the measured pressure and flow value and the actuation variable in form of the reference rotational speed v_{act} and rotational speed of the VAD v_{vad} for the differential pressure level $\Delta p = 40 \text{ mmHg}$ using the PI controller tuned according to Chien Hrones Reswick.

The complete signal curves for the tests of the controllers are depicted in Figure A.6

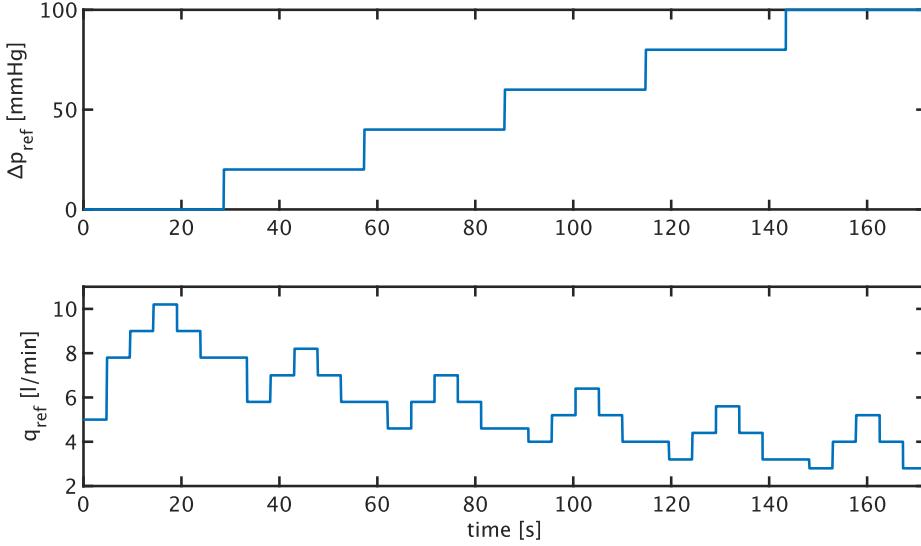


Figure 5.4: Reference signals for PI controller performance evaluation. Top: differential pressure reference value. Bottom: targeted flow trajectory.

and Figure A.7 in the appendix. Furthermore, the graphical representation of the test measurement at $\Delta p = 40 \text{ mmHg}$ for the controller tuned according to Ziegler Nichols is depicted in Figure A.8 of the appendix.

The course of the control error throughout the test measurements of the controller tuned according to Ziegler Nichols and the controller tuned according to Chien Hrones Reswick are depicted in Figure 5.6a and Figure 5.6b, respectively.

Throughout this work, for evaluation of controller performance the root mean square error (RMSE), according to [CD14], defined as

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=0}^n e_i^2} \quad (5.8)$$

is used. The RMSE for the differential pressure level of $\Delta p = 40 \text{ mmHg}$ for Ziegler Nichols tuned controller amounts to

$$RMSE_{ZN,40} = 0.4013 \text{ l/min} \quad (5.9)$$

while RMSE of the Chien Hrones Reswick tuned controller amounts to

$$RMSE_{CHR,40} = 0.2753 \text{ l/min}. \quad (5.10)$$

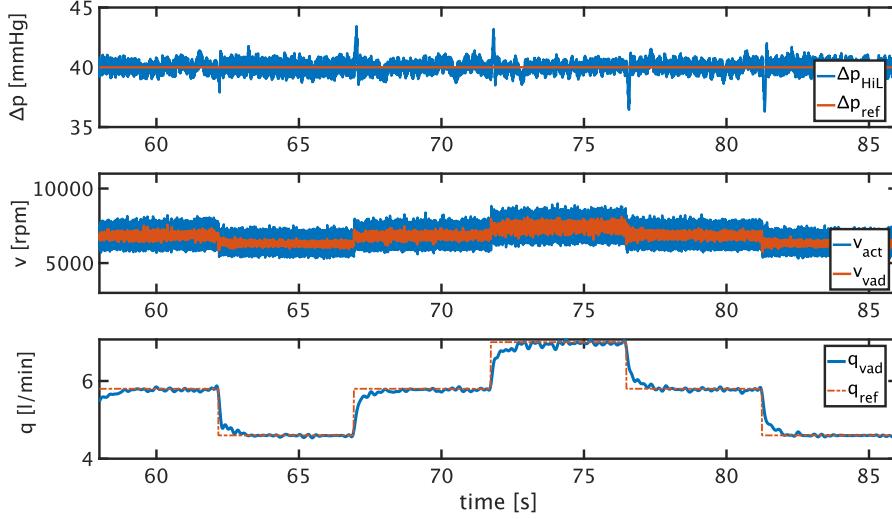


Figure 5.5: Test measurement for PI controller tuned according to Chien Hrones Reswick at $\Delta p = 40 \text{ mmHg}$.

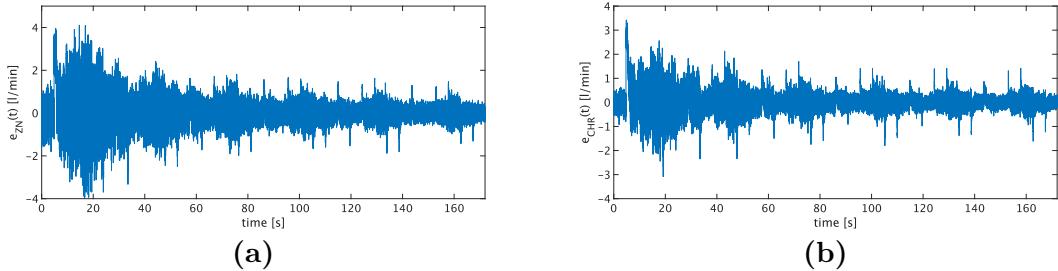


Figure 5.6: Control error for PI controllers tuned according to (a) Ziegler Nichols, (b) Chien Hrones Reswick

Taking into account the full differential pressure operating range for RMSE calculation these values amount to

$$RMSE_{ZN} = 0.5396 \text{ l/min} \quad (5.11)$$

and

$$RMSE_{CHR} = 0.3705 \text{ l/min}. \quad (5.12)$$

Comparing these results it is evident that both controllers perform more precise in the range of $\Delta p = 40 \text{ mmHg}$, for which tuning has been performed. Performance of the controller tuned according to Chien Hrones Reswick surpasses the Ziegler Nichols

tuned one in both ranges. RMSE values for full range CHR control even indicate a higher performance in comparison to the Ziegler Nichols tuned controller in the range of $\Delta p = 40 \text{ mmHg}$.

Due to its higher performance, for all following measurements the PI controller tuned in reference to Chien Hrones Reswick is used.

5.2 Iterative Learning Control

As shown in Figure 5.5, the exclusive use of a PI controller for flow control leads to necessity of long measurement times to allow the flow to settle at a new reference value. However, one goal of this thesis is to enable flow control following different reference trajectories which may imply the need for faster reference tracking. By implementing an ILC approach, the necessary reduction of the settling time, by gaining information from error values of the preceding iteration, should be made possible.

5.2.1 Design and Implementation

During this work a P-type ILC is implemented and optimized.

The implementation is based on a parallel architecture as depicted in Figure 3.6. This leads to the basic learning function for this ILC being represented by

$$u_{j+1}(k) = u_j(k) + k_p e_j(k). \quad (5.13)$$

The learning gain k_p is experimentally chosen as

$$k_p = 225 \quad (5.14)$$

to ensure quick error convergence.

As described in chapter 3.3, the basic ILC is extended to include a Q-Filter to enable more precise tuning of the ILC and increase its robustness. This expansion results

in the learning function being described by

$$u_{j+1}(k) = Q(q)[u_j(k) + k_p e_j(k)]. \quad (5.15)$$

The Q-Filter is implemented as a 2nd-order butterworth filter, with sampling frequency $f_s = 1000 \text{ Hz}$. The cut off frequency f_c is set to several values in order to compare and thus optimize performance and robustness of the iterative learning control system.

An additional part of the implementation is the generation of a repeating reference and a trigger signal. The trigger signal indicates the beginning of each new iteration and thus initiates calculation of the new values $u_{j+1}(k)$ in the ILC block. Figure 5.7 depicts three iterations of the reference signal for this ILC.

The signal is created by first generating a square wave signal with the upper stage at 6 l/min and the lower stage at 4 l/min . Thus, the signal encloses the average value of 5 l/min of the cardiac output of a healthy heart. The reference values are each held for 0.5 s , so that a complete iteration would correspond to a frequency of $60 \text{ beats per minute (bpm)}$ when compared to the heart rate. To avoid abrupt transitions in the flow, which could lead to problems on the part of the pump, the reference signal was filtered with a first order Butterworth filter with cut off frequency $f_c = 20 \text{ Hz}$ and sampling frequency $f_s = 1000 \text{ Hz}$, resulting in radiusued transitions. Afterwards, the signal is shifted by 0.25 s to avoid placing the beginning of the signal at a jump point. The trigger signal is set from 0 to 1 at the beginning of each iteration for the duration of one sample.

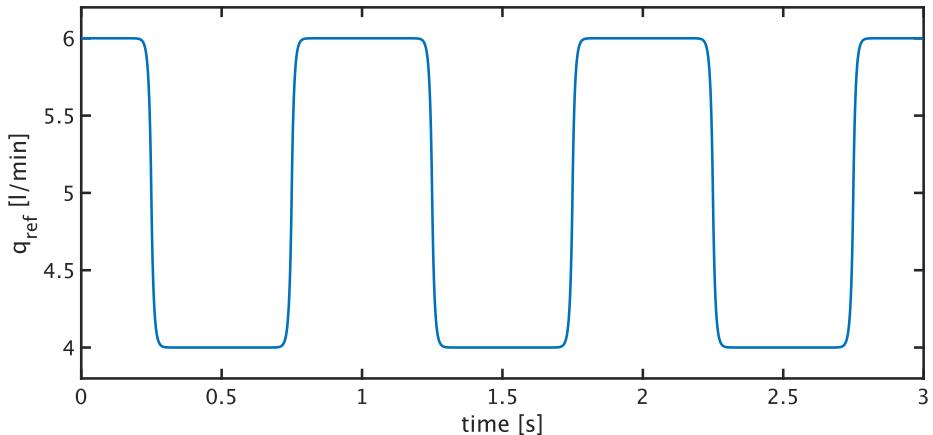


Figure 5.7: Three iterations of smoothed reference signal for ILC tuning.

5.2.2 Evaluation

As mentioned above, various cut off frequencies for the Q-Filter of the ILC are tested with the aim of optimizing the ILC's performance and robustness.

The test signal for this purpose, is given by repeatedly presenting the reference signal from Figure 5.7 to the system over a duration of 600 s. During the first 60 s exclusively PI control is activated. By this, stable system performance at the beginning of ILC control can be ensured. Once the 60 s are up, the trigger signal will set off indications for beginnings of new iterations. From this point, ILC and PI controller are working simultaneously. During the complete test measurement differential pressure is set to $\Delta p = 40 \text{ mmHg}$. Measurements with this setup are performed for cut off frequencies $f_c = 20 \text{ Hz}$, $f_c = 25 \text{ Hz}$, $f_c = 8 \text{ Hz}$ and $f_c = 34 \text{ Hz}$.

Figure 5.8 exemplifies a sequence of the measurement performed for the Q-Filter set to a cut off frequency of $f_c = 20 \text{ Hz}$. The segment shows the transition from exclusive PI control to the parallel control structure of PI control and ILC. The upper graph depicts the measured differential pressure at the MCL. The spikes in this curve occur due to varying flow through the blood pump resulting in changing volumes inside the pressure chambers. The middle graph represents the rotational speed values for the actuating variable v_{act} and the actual velocity of the pump's rotor v_{vad} .

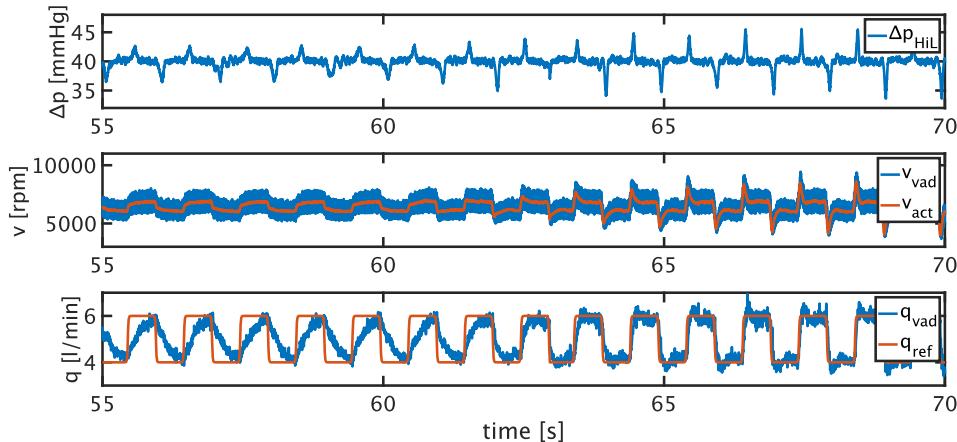


Figure 5.8: Test measurement for ILC at cut off frequency $f_c = 20 \text{ Hz}$. Top: differential pressure value of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD.

The bottom graph of Figure 5.8 depicts the reference flow trajectory q_{ref} and the

measured flow q_{vad} that is conveyed by the VAD. Looking at this curve, it can be seen that by solely using the PI controller (corresponding to 55 s to 60 s of the graph), the flow through the VAD cannot be adjusted fast enough and thus the reference trajectory cannot be followed successfully. However, from the onset of the ILC at about 60 s, it can be seen that the measured flow continues to adapt to the given reference flow within a few iterations.

While the system shows stable behavior over the complete measurement time for a cut off frequency of $f_c = 20 \text{ Hz}$, in case of $f_c = 34 \text{ Hz}$ the system shows oscillatory behavior. Figure 5.9 depicts part of the measurement for a cut off frequency set to $f_c = 34 \text{ Hz}$.

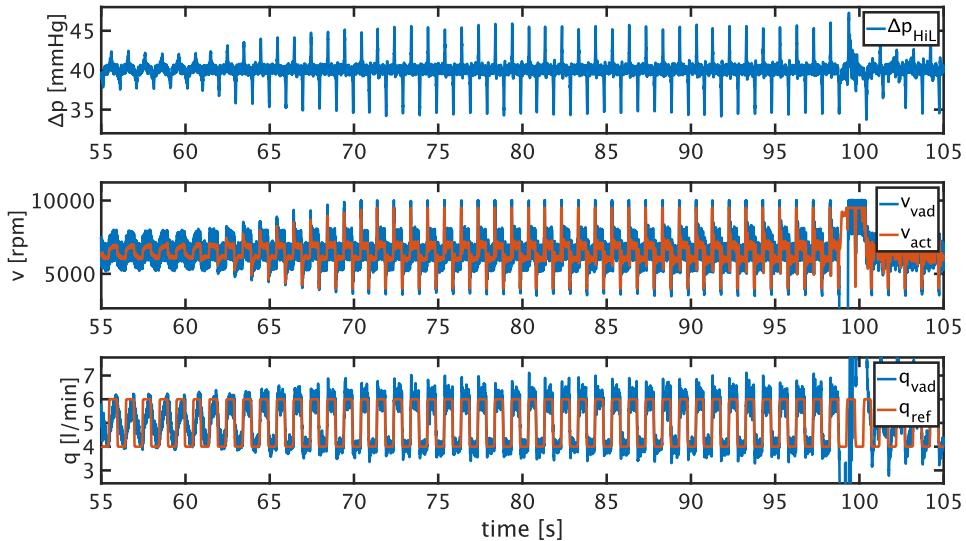


Figure 5.9: Test measurement for ILC at cut off frequency $f_c = 34 \text{ Hz}$. Top: differential pressure value of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD.

The structure is the same as for Figure 5.8. However, in this case, looking at the middle graph it is evident that with each additional ILC iteration the actuation variable v_{act} rises further towards its saturation values 4000 rpm and 9000 rpm . This ultimately leads to the pump's rotor to stop, due to abrupt changes in speed and flow at approximately 98 s measurement time.

Behavior of the system for a cut off frequency set to $f_c = 25 \text{ Hz}$, as shown in Figure 5.10, is similar to behavior with $f_c = 34 \text{ Hz}$. The oscillatory system behavior

again results in the pump's to stop at approximately 96 s.

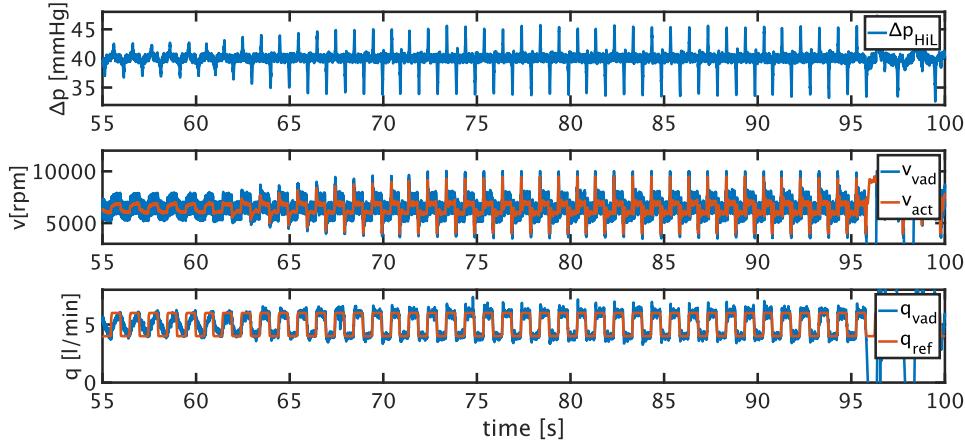


Figure 5.10: Test measurement for ILC at cut off frequency $f_c = 25 \text{ Hz}$. Top: differential pressure value of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD.

The measurement with $f_c = 8 \text{ Hz}$ as cut off frequency of the Q-Filter shows stable behavior over the complete measurement time, similar to the measurement performed with $f_c = 20 \text{ Hz}$.

In order to determine which cut off frequency is most suited for the ILC implementation the RMSE values of the iterations for each of the measurements are compared to another. Figure 5.11 depicts the RMSE of each measurement as a function of the iteration for the first 39 iterations of the ILC. The figure also represents the RMSE value of the exclusive performing PI controller in form of the first iteration value:

$$RMSE_{PI} = RMSE(1) \approx 0.85 \text{ l/min} \quad (5.16)$$

It is evident that the curves for $f_c = 25 \text{ Hz}$ and $f_c = 35 \text{ Hz}$ show abrupt increases in RMSE for the iterations when the pump stopped. Due to this instable behavior these cut off frequencies are not suitable for ILC implementation.

Comparing the RMSE values of the 39th iteration of the other two frequencies it is obvious that performance of the ILC with Q-filter cut off frequency at $f_c = 20 \text{ Hz}$ with

$$RMSE_{f_c=20 \text{ Hz}}(39) = 0.1984 \quad (5.17)$$

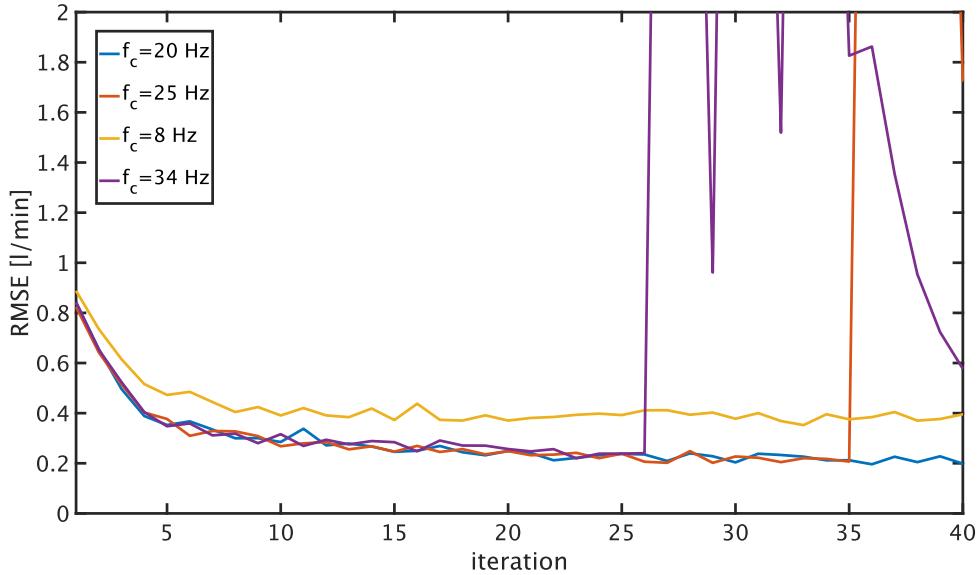


Figure 5.11: Comparison of RMSE values for different cut off frequency of ILC Q-Filter.

is higher than for $f_c = 8 \text{ Hz}$ with

$$RMSE_{f_c=8 \text{ Hz}}(39) = 0.3951. \quad (5.18)$$

Therefore, the cut off frequency of the Q-Filter in all following measurements will be set to $f_c = 20 \text{ Hz}$.

As these measurements only took into account a differential pressure value of $\Delta p = 40 \text{ mmHg}$ the ILC with the optimized Q-Filter cut off frequency is tested at pressure levels in equal steps of 20 mmHg between $\Delta p = 20 \text{ mmHg}$ and $\Delta p = 80 \text{ mmHg}$ to ensure stable system behavior in all operating points. For this the same measurement as before is executed.

A comparison of the RMSE values over all iterations of the ILC for the four differential pressure levels is depicted in Figure 5.12. The course of the RMSE values of all four measurements indicate stable system behavior. With values of approximately 0.3 l/min the RMSE of the other operating points is only slightly higher than of the 40 mmHg operating point with an RMSE of approximately 0.2 l/min . Therefore, the implemented ILC is suitable for all of the tested operating points.

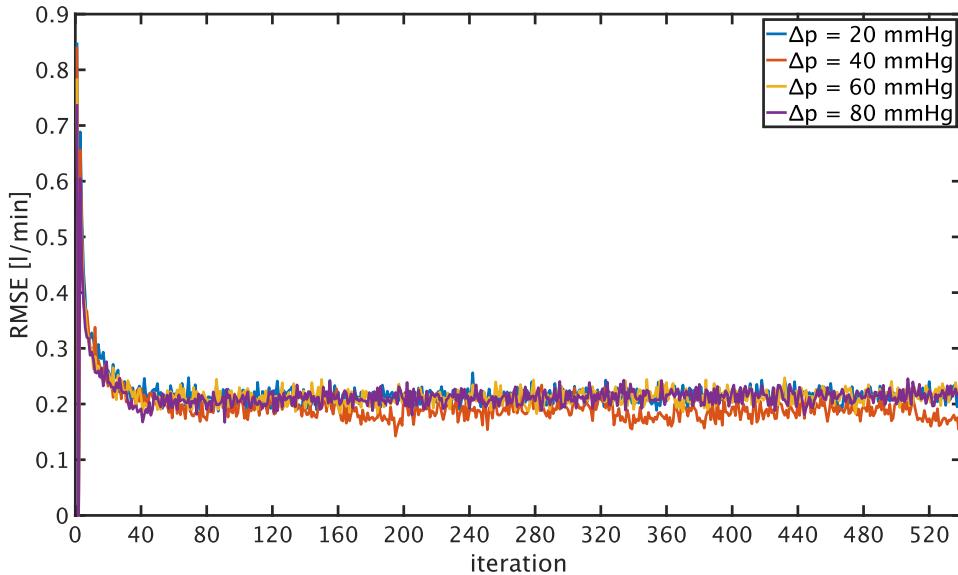


Figure 5.12: Comparison of RMSE values of the ILC at different differential pressure operating points.

5.3 Iterative Learning Control with repeating disturbance

The ILC implemented in the previous section was tested and optimized under idealized conditions without being influenced by any disturbances. Since in real use, the VAD is exposed to disturbances by pressure changes due to the beating of the heart this section aims to include this influence into the measurements through usage of the circulatory system simulator's functionality to simulate the heart beat including anticipated pressure changes.

Initially, only repeating disturbances are taken into account as the standard P-type ILC used is only setup to compensate these. The MCL will be used to introduce the setup to a disturbance in form of heart beats at a constant heart rate. Including the influence of the heart beat as a disturbance requires changing the trigger signal from a manually programmed one to using the start of each heart beat as the trigger of new iterations.

5.3.1 Reference trajectories

Testing of the ILC subjected to repeating disturbances is performed for several reference flow trajectories. These are generated using Matlab and are selectable during runtime via ControlDesk through the use of an indicator variable.

As a first reference, the flow is set to a constant value of $q_{ref} = 5 \text{ l/min}$. By this, the controller's ability to balance out the pressure fluctuations during a heart beat is tested.

The second signal, which is used as a reference trajectory, is a sinusoidal signal that oscillates around a value of 4 l/min , has a maximum value of 5 l/min and a minimum value of 3 l/min . One iteration of this signal is set to 1 s , matching a 60 bpm heart rate. The signal course is depicted in Figure 5.13.

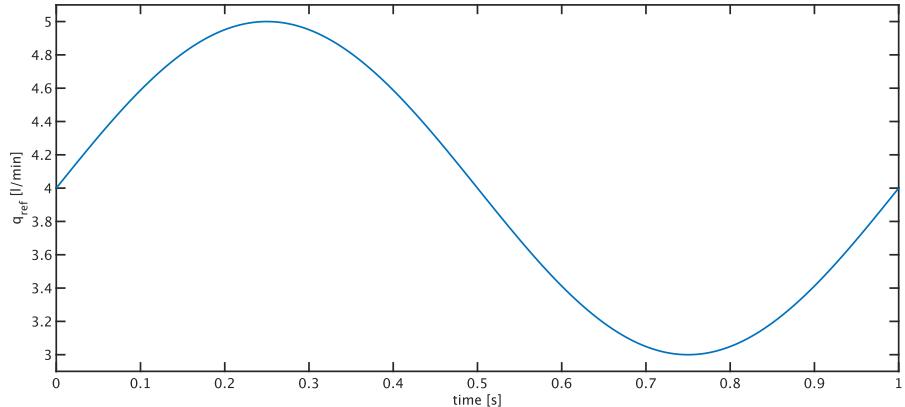


Figure 5.13: Sinusoidal reference signal.

The third reference trajectory is given in form of a triangular signal. As for the sinusoidal signal, the maximum value is set to $q_{ref} = 5 \text{ l/min}$ and the minimum to 3 l/min . Again the full signal length is set to 1 s to match a 60 bpm heart rate. Figure 5.14 depicts one iterations of the reference trajectory.

As a last trajectory a rectangular signal similar to the one used in chapter 5.2 is chosen. The upper step is set to $q_{ref} = 5 \text{ l/min}$ and the lower one to $q_{ref} = 3 \text{ l/min}$. Both are hold for 0.5 s . Again the signal is filtered using a 1^{st} order butterworth filter with cut off frequency $f_c = 20 \text{ Hz}$ and sampling frequency $f_s = 1000 \text{ Hz}$.

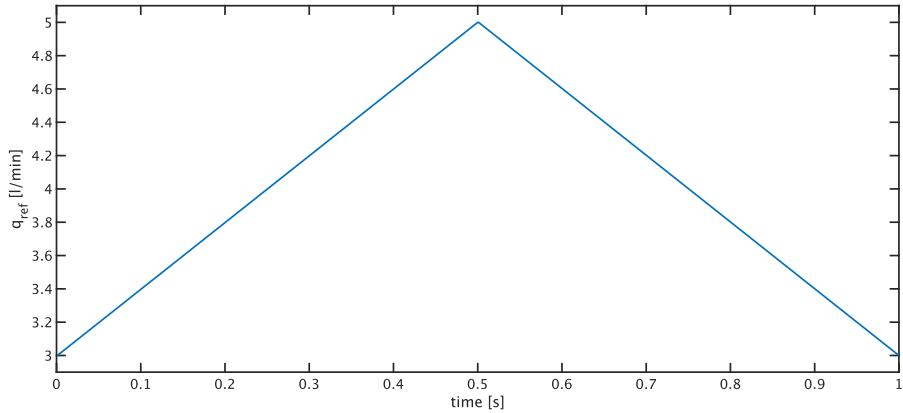


Figure 5.14: Triangular reference signal.

Figure 5.15 depicts one iteration of the reference.

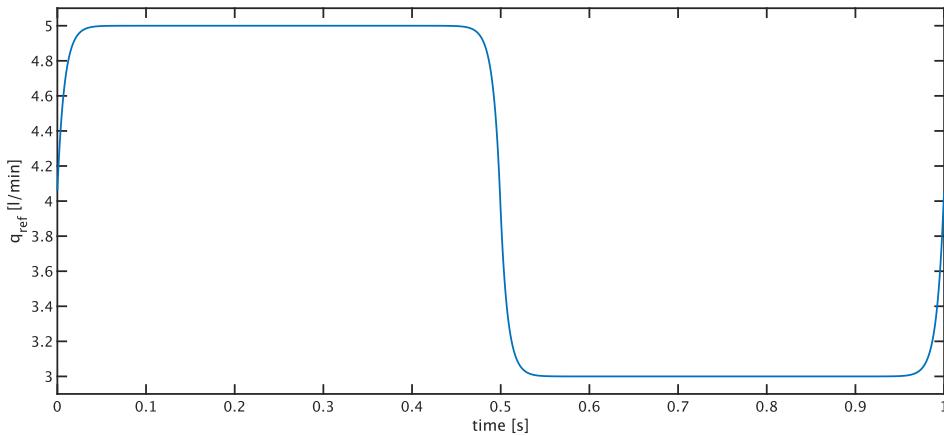


Figure 5.15: Rectangular reference signal.

5.3.2 Evaluation

Using the reference trajectories described above, several measurements are performed and evaluated to determine performance of the ILC subjected to repeating disturbances. Measurements were performed for varying levels of contractility of the left ventricle for all reference trajectories. The performance results of the contractility

levels are compared to each other. Contractility is decreased in steps of 0.25 from $cf_{Lv} = 1$ representing contractility of a healthy heart to $cf_{LV} = 0.25$ correlating to a severe impairment of heart functionality.

During all measurements for the first 120 s, exclusively PI control is activated to ensure stable system behavior at the beginning of additional ILC control.

In a first step, measurements are performed using the constant reference flow of $q_{ref} = 5 l/min$. Figure 5.16 depicts the transition from exclusive PI control (115 – 120 s) to use of the parallel control structure (120 – 130 s) for a contractility of $cf_{LV} = 1$. It is evident that the PI controller alone is not able to suppress the disturbance's influence on the flow. As soon as ILC control sets in the flow settles further towards the constant reference flow with each ILC iteration.

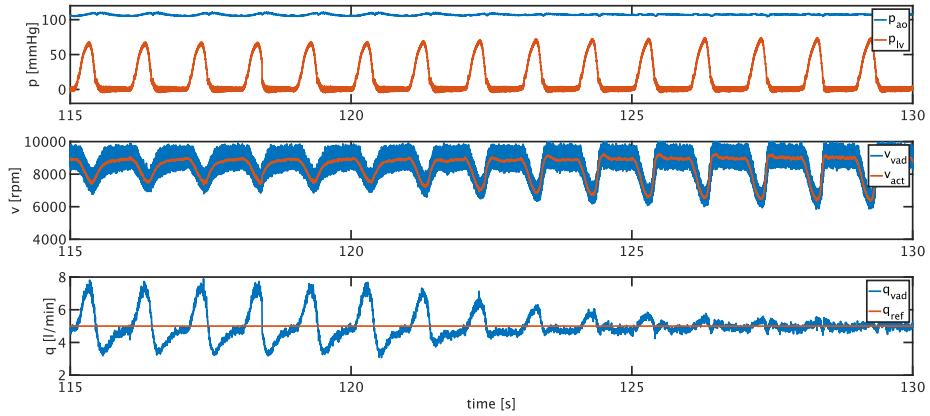


Figure 5.16: Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 1$ for constant reference flow. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD.

Measurements for all contractility levels are running stable until the end of measurement time is reached at 600 s. A comparison of the RMSE values for each iteration is presented in Figure 5.17.

Up to iteration 120, the graph represents the RMSE of the PI controller. For this time, it is evident that with decreasing left ventricular contractility RMSE also decreases from $RMSE_{PI,const,cf_{Lv}=1} \approx 1.2 l/min$ to $RMSE_{PI,const,cf_{Lv}=0.25} \approx 0.4 l/min$. This can be explained with the lower influence of pressure changes due to weakened

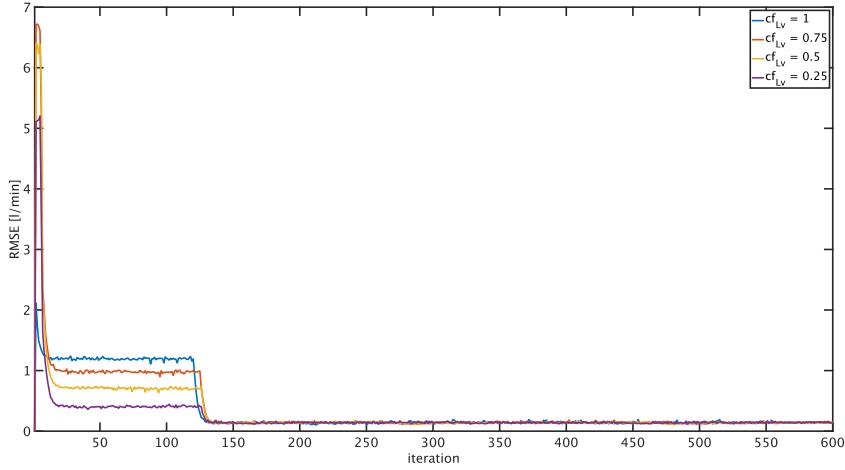


Figure 5.17: Comparison of RMSE values of the ILC for constant reference flow with disturbance of $HR = 60 \text{ bpm}$ for varying contractility values of the left ventricle.

contractility. The RMSE values for all four contractility levels using combined PI and ILC control amount to

$$RMSE_{ILC,const} \approx 0.14 \text{ l/min}. \quad (5.19)$$

It is evident that using the combined control approach results in significantly higher performance in all contractility ranges for a constant reference flow.

The next measurements performed are the ones testing the controller's ability to follow the sinusoidal reference trajectory. The trajectory is placed synchronous to the heart beat. Figure 5.18 illustrates the transition phase from PI to combined control for the sinusoidal reference at $cf_{LV} = 1$. Similar to the constant reference flow, the PI controller alone is not able to follow the reference trajectory. The combination between PI controller and ILC, however, leads to a clearly recognizable improvement of the following behavior within some iterations. The comparison of RMSE values (see Figure 5.19) leads similar conclusions as for the constant reference flow. During the first 120 iterations when only PI control is active RMSE decreases with decreasing contractility of the left ventricle. However, the decrease between contractility values from $cf_{LV} = 1$ to $cf_{LV} = 0.75$ and $cf_{LV} = 0.5$ with $RMSE_{PI,sine,cf_{LV}=1} \approx 1.85 \text{ l/min}$, $RMSE_{PI,sine,cf_{LV}=0.75} \approx 1.75 \text{ l/min}$ and

5 Flow Control

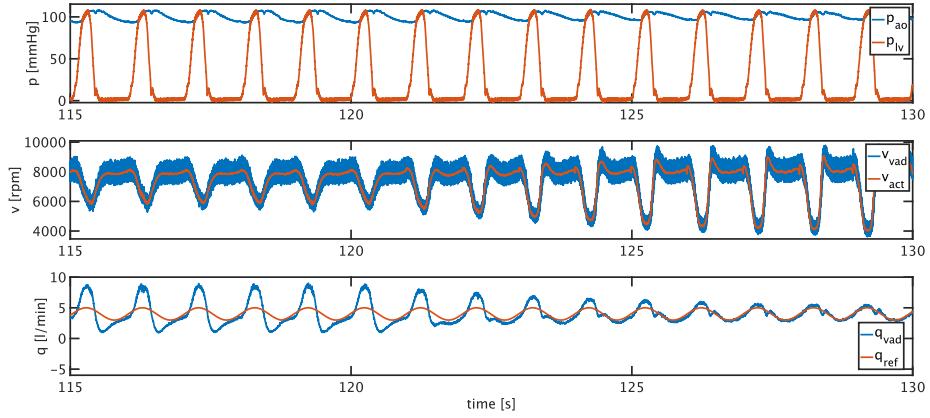


Figure 5.18: Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 1$ for sinusoidal reference flow. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

$RMSE_{PI,sine,cf_{Lv}=1} \approx 1.85 \text{ l/min}$, are less significant than the reduction of contractility to $cf_{Lv} = 0.25$ with $RMSE_{PI,sine,cf_{Lv}=0.25} \approx 0.93 \text{ l/min}$. Performance for the

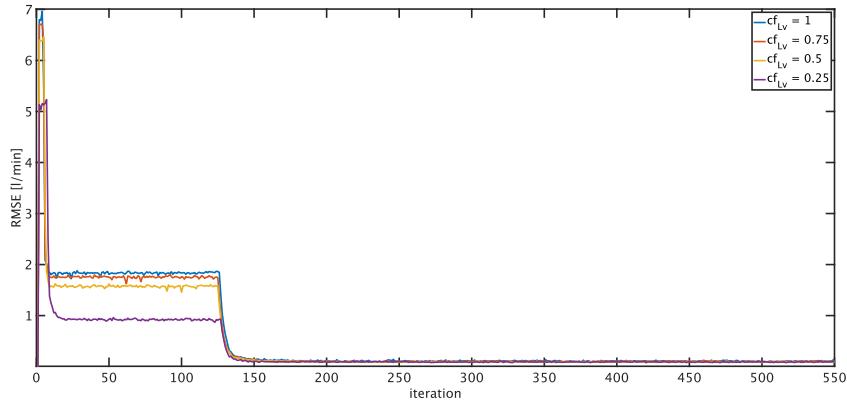


Figure 5.19: Comparison of RMSE values of the ILC for sinusoidal reference flow with disturbance of $HR = 60 \text{ bpm}$ for varying contractility values of the left ventricle.

combined control approach is almost equal for all contractility values with

$$RMSE_{ILC,sine} \approx 0.09 \text{ l/min} \quad (5.20)$$

and RMSE indicates an increased performance in all cases.

5.3 Iterative Learning Control with repeating disturbance

Measurement for the triangular reference trajectory shows slowly increasing instable behavior for left ventricular contractility at $cf_{LV} = 1$ and $cf_{LV} = 0.75$. Figure 5.20, representing the measurement at $cf_{LV} = 1$, shows that from the onset of the ILC, a clear approximation to the reference signal is initially achieved, but the actuating variable v_{act} (middle graph) continues to reach its saturation limits with each iteration. This ultimately leads to a stoppage of the pump.

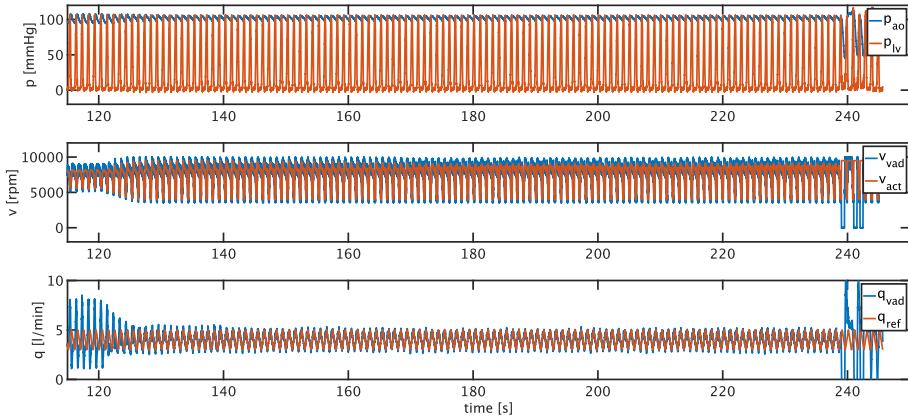


Figure 5.20: Measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{LV} = 1$ for triangular reference flow. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

Measurements for contractility values $cf_{LV} = 0.5$ and $cf_{LV} = 0.25$ show stable behavior over the complete measurement time of 600 s . The transition segment for the measurement at $cf_{LV} = 0.5$ shown in Figure 5.21 again indicates an improved performance for the ILC. This is endorsed by comparison of the RMSE values as shown in Figure 5.22. While RMSE for the PI controller segments lie at $RMSE_{PI,triang,cf_{LV}=0.5} \approx 1.9 \text{ l/min}$ and $RMSE_{PI,triang,cf_{LV}=0.25} \approx 1.2 \text{ l/min}$, the RMSE for the combined control structure amounts to

$$RMSE_{ILC,triang} \approx 0.11 \text{ l/min}. \quad (5.21)$$

The last measurements for analysis of controller performance of the ILC subjected to a repeating disturbance are performed using the rectangular reference trajectory.

5 Flow Control

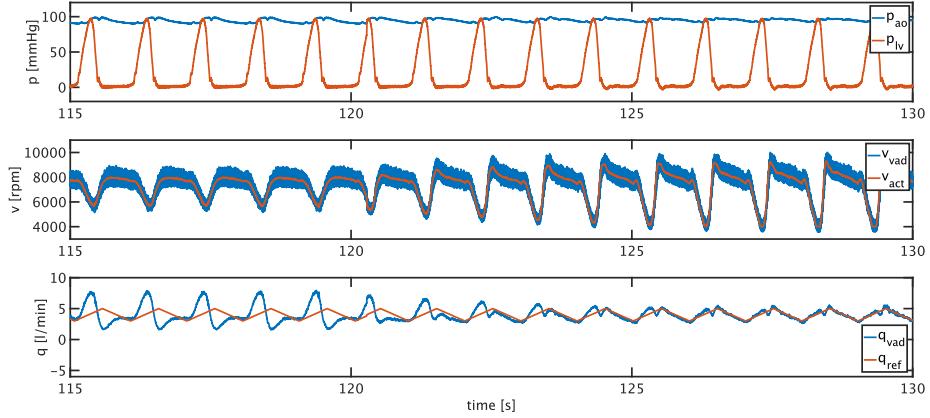


Figure 5.21: Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $cf_{Lv} = 0.5$ for triangular reference flow. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

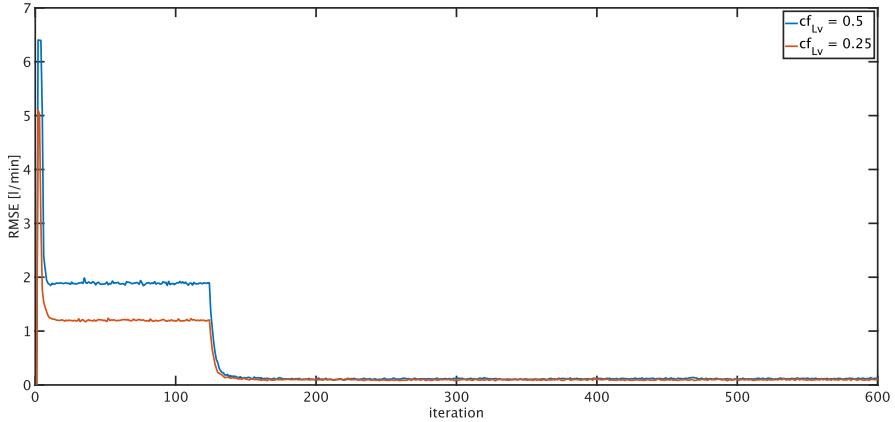


Figure 5.22: Comparison of RMSE values of the ILC for triangular reference flow with disturbance of $HR = 60 \text{ bpm}$ for varying contractility values of the left ventricle.

As in all previous measurements, the exclusive use of the PI controller is not suitable to track the reference. Combined control however, once more shows adjustment to the reference in a few iterations. Figure 5.23 depicts the course of pressure in the aorta and left ventricle, the actuating variable and the rotational speed of the VAD as well as the reference trajectory and the actually achieve flow through the VAD for the transitional segment of the measurement at $cf_{Lv} = 1$.

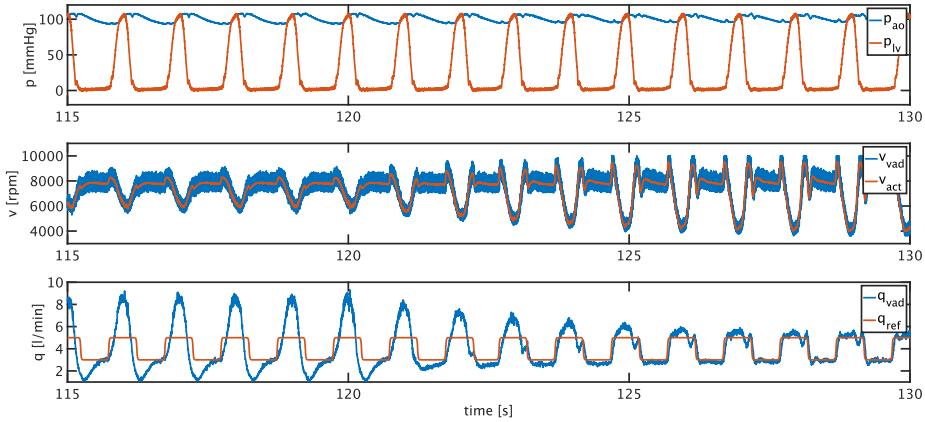


Figure 5.23: Segment of measurement for ILC with disturbance of $HR = 60 \text{ bpm}$ with $c_{fLv} = 1$ for rectangular reference flow. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

The comparison of RMSE courses for all four left ventricular contractility levels is depicted in Figure 5.24. Once more, contractility decrease directly influences the performance of the PI controller while the end value for RMSE of the ILC for all contractility levels amounts to

$$RMSE_{ILC,rect} \approx 0.22 \text{ l/min.} \quad (5.22)$$

To prepare measurements considering different disturbances, in addition to measurements considering different contractility values for the left ventricle, measurements are performed at several heart rates for the rectangular reference. Heart rate is defined in four steps of 20 bpm from $HR = 40 \text{ bpm}$ to $HR = 100 \text{ bpm}$. All of these measurements show stable behavior throughout the complete measurement time of 500 s . Looking at Figure 5.25, it can be concluded that the performance of the PI controller improves only for the slowest heart rate of $HR = 40 \text{ bpm}$ compared to the rest. Also the results for the RMSE of the ILC control show that the control for a disturbance with $HR = 40 \text{ bpm}$ with

$$RMSE_{ILC,40\text{bpm}} \approx 0.16 \quad (5.23)$$

5 Flow Control

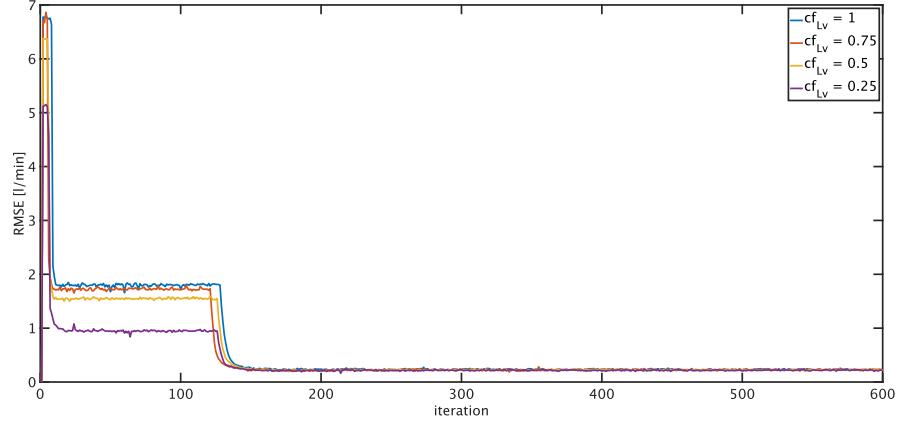


Figure 5.24: Comparison of RMSE values of the ILC for rectangular reference flow with disturbance of $HR = 60\text{ bpm}$ for varying contractility values of the left ventricle.

succeeds the results for the other three heart rates with

$$RMSE_{ILC,60/80/100\text{ bpm}} \approx 0.22. \quad (5.24)$$

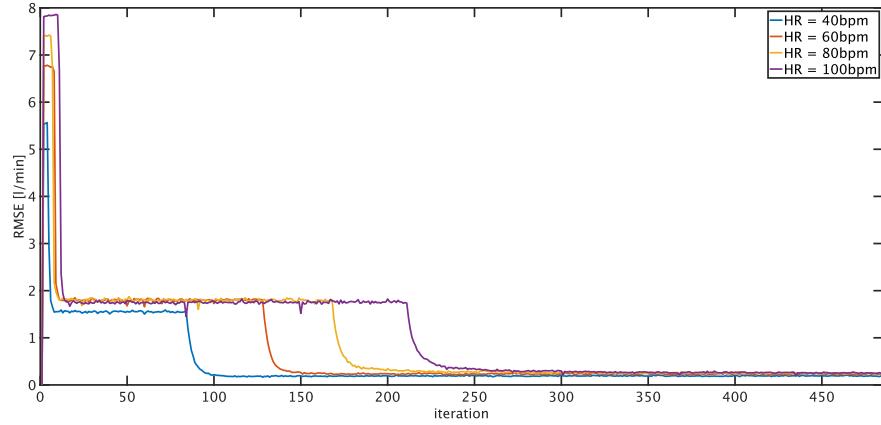


Figure 5.25: Comparison of RMSE values of the ILC for rectangular reference flow with $cf_{Lv} = 1$ for varying heart rates.

However, the results indicate that using ILC control is a suitable option for all of these heart rates.

5.4 Iterative Learning Control with varying disturbance

Due to the fact that a person's heartbeat does not always occur at a uniform heart rate, but is subject to fluctuations, the ILC is tested for use in suppressing varying disturbances.

5.4.1 Design and Implementation

As the standard P-type ILC is not set up for use under the influence of non repeating disturbances some changes have to be implemented.

To perform the tests under the influence of changing disturbances, an additional function programmed in Matlab is added to the Simulink model. This allows a constant variation of the heart rate. The function is designed in such a way that by receiving the trigger signal of a new heartbeat, a new heart rate is determined and passed on to the mock circulatory loop and the ILC. In addition to the trigger signal, the function has three more inputs in the form of an upper and lower limit of the heart rate and a step size for a variation of the heart rate. These variables can be set via ControlDesk before starting the measurement. Starting at the lower limit, the heart rate is increased by the defined step size with each heartbeat until the upper limit of the heart rate is reached. Then, with each heartbeat, the heart rate is decreased by the step size until the lower limit is reached. This is repeated until the measurement is stopped. An example of this sequence with a lower limit of 60 bpm , a step size of 1 bpm and an upper limit of 100 bpm is shown in Figure 5.26.

Since the variation of the heart rate leads to changing iteration duration an additional preprocessing step is implemented within the ILC function. This introduces a functionality which allows to resample the stored data of the previous iteration and adapt it to the duration of the current iteration. This process is performed after the data filtering step of the ILC, before the data is output to the control loop.

To adjust the resampling of the data to the length of the iterations knowledge of the

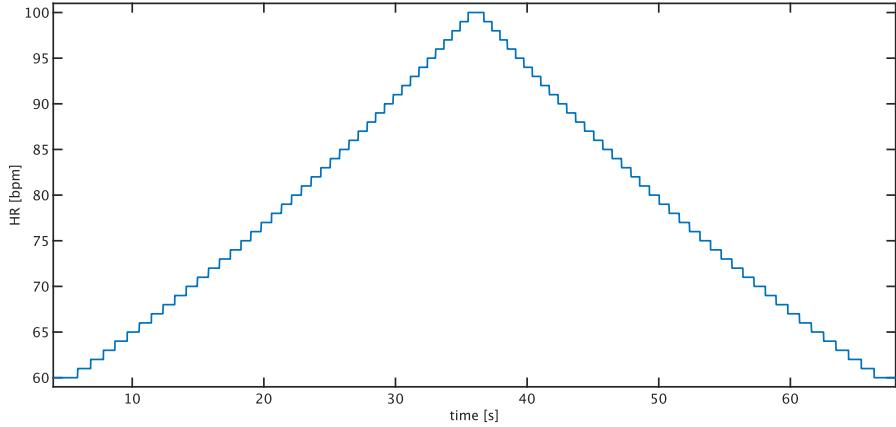


Figure 5.26: Illustration of HR change.

heart rates is required. Within the tests at the MCL this requirement is fulfilled. For an application on the patient, an additional use of an ECG would be necessary. The resampling function calculates the iteration length according to

$$it_len = \lfloor \frac{60}{HR} \cdot 1000 \rfloor \quad (5.25)$$

with HR being the heart rate. The duration of the last iteration is stored in the variable it_len_prev . Using this variable and the current iteration length an index factor is calculated to

$$idx = \frac{it_len_prev}{it_len}. \quad (5.26)$$

This factor is required to determine the indices of the stored actuating variable values which are to be used to calculate the new values. In the next step, the lengths of the last and current iteration are compared. In case the iteration times correspond to each other, the stored data are used unchanged for the output to the control loop

$$\mathbf{u}_{j,ILC}(i) = \mathbf{u}_{j,ILC,prev}(i) \quad (5.27)$$

for all entries i . $\mathbf{u}_{j,ILC,prev}$ corresponds to the filtered data stored the actuating variable memory during the last iteration while $\mathbf{u}_{j,ILC}$ represents the data output during the current iteration.

Calculation steps for different iteration durations differ only for the first entry. In

case the current iteration length is shorter than the last ($it_len < it_len_prev$)

$$\mathbf{u}_{j,ILC}(1) = \mathbf{u}_{j,ILC,prev}(1) \quad (5.28)$$

is always valid for the first entry of the actuating variable. A weighting factor is required for all other entries i of the actuating variable vector to determine resampled data. This is calculated as

$$weight = i \cdot idx - \lfloor i \cdot idx \rfloor. \quad (5.29)$$

The value for the current entry i is than determined as

$$\mathbf{u}_{j,ILC}(i) = (1 - weight) \cdot \mathbf{u}_{j,ILC,prev}(\lfloor i \cdot idx \rfloor) + weight \cdot \mathbf{u}_{j,ILC,prev}(\lceil i \cdot idx \rceil). \quad (5.30)$$

By using this calculation, the data from the previous iteration is compressed or stretched to the current iteration length accordingly.

5.4.2 Evaluation

In order to determine whether resampling of data improves the ILC performance under varying disturbances, two sets of tests are performed. One without resampling the data under variable disturbances and one using the resampling function described above. The results of the tests are compared with each other. The reference trajectories described in section 5.3.1 are used to perform the measurements. All measurements considered here are performed assuming a left ventricular contractility of $cf_{LV} = 1$.

At first, a constant reference flow of $4 l/min$ is presented to the system. Figure 5.27 depicts a segment of the measurement without resampling of the actuating variable data representing the transition form exclusive PI control to the combined control approach at 120s . At about 152s the pump stops due to the steadily increasing instable behavior of the actuating variable. As can be seen in Figure 5.28, similar behavior is observed for the measurement with the resampled actuating variable data. However, looking at the lower graphs of the two figures, it can be seen that

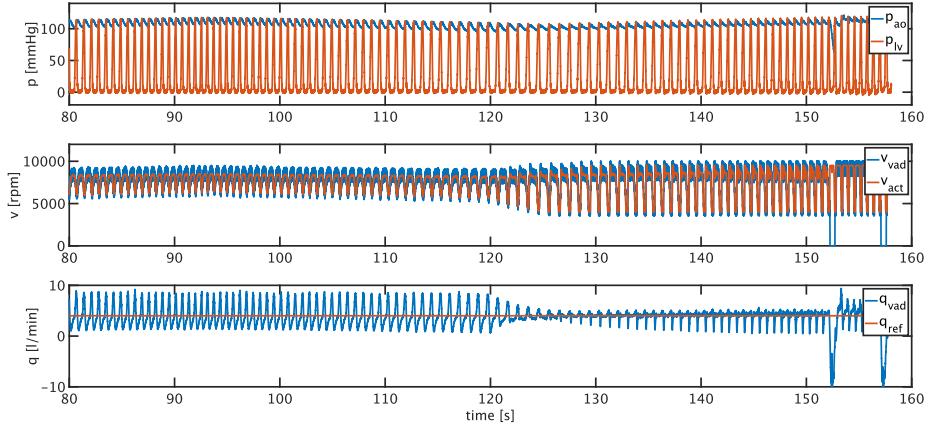


Figure 5.27: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for constant reference flow without data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

for the unchanged actuating variable data in Figure 5.27 the measured flow q_{vad} first approaches the reference, but then moves further away from it again, while the flow through the VAD for the measurement with resampling of the actuating variable data in Figure 5.28 continuously approaches the reference.

This suggests a higher performance of the ILC using the resampling functionality. This assumption can be confirmed when comparing the RMSE values of the two measurements. While at the beginning of the combined control both measurements decrease to an average error value of

$$RMSE_{const,low} = RMSE_{resampled,const} \approx 0.05 \text{ l/min} \quad (5.31)$$

the value of the measurement without resampling the data afterwards increases continuously to a value of

$$RMSE_{const,high} \approx 1.13 \text{ l/min}. \quad (5.32)$$

The value of the measurement with resampled data remains at about 0.05 l/min . Thus, for a constant reference flow, a significant improvement in performance can be achieved by resampling the data of the actuating variable before the output to the control loop. Figure 5.29 depicts a graphical comparison of the RMSE courses of the two measurements.

5.4 Iterative Learning Control with varying disturbance

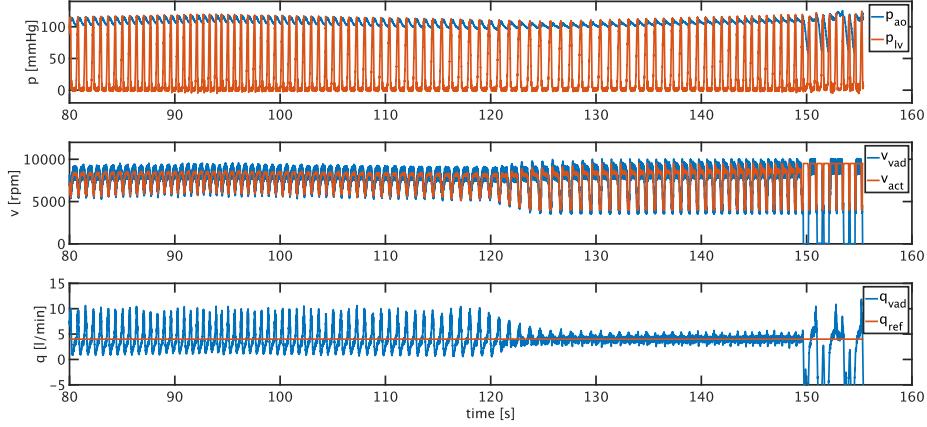


Figure 5.28: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for constant reference flow with data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

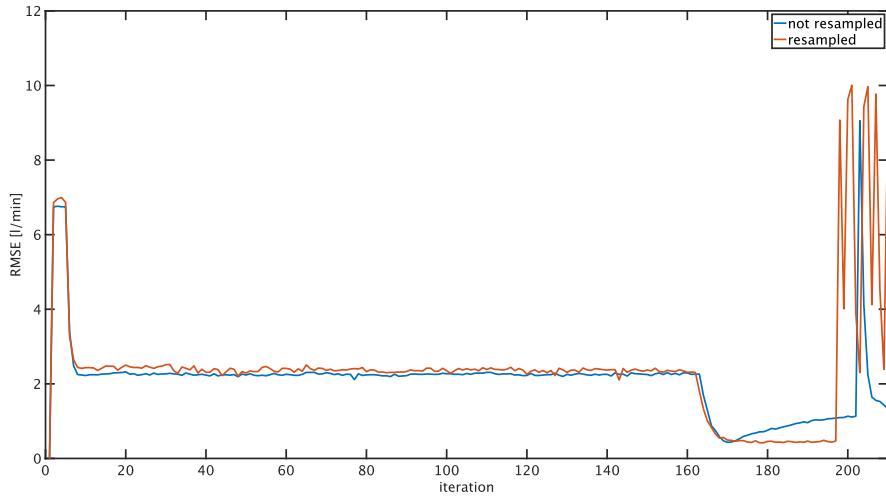


Figure 5.29: Comparison of RMSE values for ILC measurement using a constant reference flow for unchanged and resampled data.

The second set of measurements is performed using the sinusoidal reference signal. Other than for the constant reference flow for which both the unchanged ILC and the resampling measurement result in a pump failure after approximately 155 s, the measurements following a sinusoidal trajectory run stable over the full measurement time of 600 s. Looking at the graphical comparison of the RMSE values of the two

measurements, which is shown in Figure 5.30, significantly lower error values can be seen for the complete measurement period in the measurement using the resampling functionality. For this, the RMSE is about

$$RMSE_{resampled,sine} \approx 0.3 l/min \quad (5.33)$$

from the onset of the ILC. For the measurement with the standard P-type ILC, permanent fluctuations of the RMSE between

$$RMSE_{sine,low} \approx 0.3 l/min \quad (5.34)$$

and

$$RMSE_{sine,high} \approx 0.9 l/min \quad (5.35)$$

can be seen. Thus, an increased performance of the revised ILC can also be concluded for this reference trajectory.

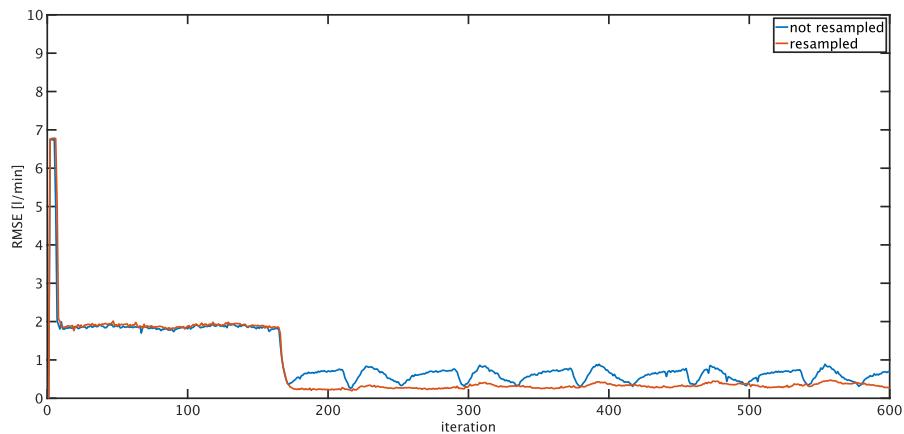


Figure 5.30: Comparison of RMSE values for ILC measurement using a sinusoidal reference flow for unchanged and resampled data.

The measurements using the triangular reference trajectory show very similar system behavior to those using the constant reference flow. Both when using the standard ILC and the revised ILC, the pump stops due to oscillating system behavior. This occurs slightly earlier for the measurement using the revised ILC than for the standard ILC. However, when comparing the RMSE values in Figure 5.31 it is clear that the performance of the revised ILC exceeds that of the unmodified ILC. While the

5.4 Iterative Learning Control with varying disturbance

revised ILC has average error values of about

$$RMSE_{resampled,triang} \approx 0.38 \text{ l/min}, \quad (5.36)$$

the value for the standard ILC initially drops to about

$$RMSE_{triang,low} \approx 0.46 \text{ l/min} \quad (5.37)$$

but then rises continuously to a value of

$$RMSE_{triang,high} \approx 0.79 \text{ l/min}. \quad (5.38)$$

Thus, even though the pump stops earlier, the use of the revised ILC would be advisable.

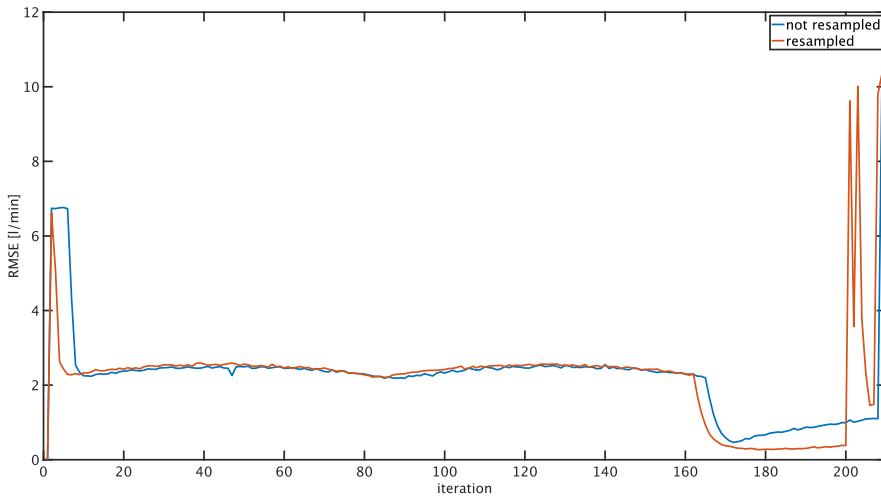


Figure 5.31: Comparison of RMSE values for ILC measurement using a triangular reference flow for unchanged and resampled data.

Lastly, the tests of the two ILC species were performed using the rectangular reference trajectory. As with the constant reference flow and the triangular trajectory, the actuating variable again oscillates, resulting in the pump rotor stopping. Unlike the previous measurements, however, the evaluation of the error values for both measurements is similar in this case. At the beginning of the combined control, the averaged error values for both tests drop sharply compared to the PI control. However, a fluctuation of the average error values can be observed for both measurements.

This occurs somewhat more slowly for the revised ILC than for the standard ILC. Nevertheless, both measurements have best values of about

$$RMSE_{resampled,rect,low} = RMSE_{rect,low} \approx 0.4 l/min, \quad (5.39)$$

but in the worst case they are both about

$$RMSE_{resampled,rect,high} = RMSE_{rect,high} \approx 0.77 l/min. \quad (5.40)$$

A graphical comparison is presented in Figure 5.32. Due to this perception, no clear

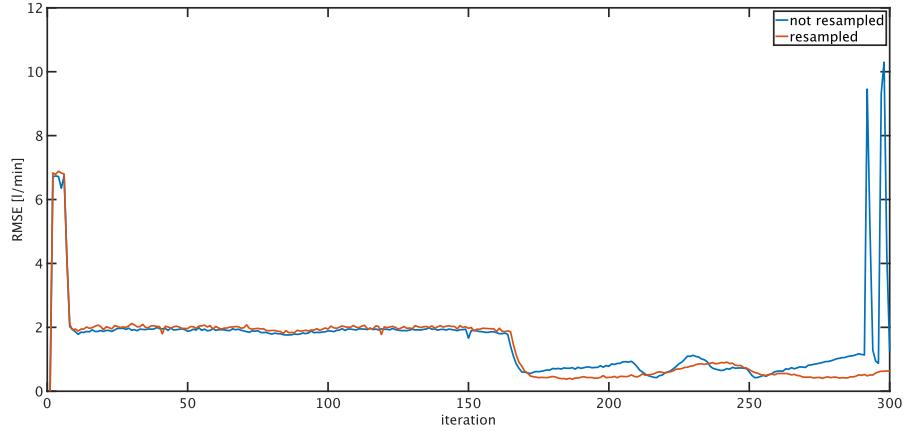


Figure 5.32: Comparison of RMSE values for ILC measurement using a rectangular reference flow for unchanged and resampled data.

statement can be made for the reference tracking of this trajectory as to which of the ILC approaches is more suited.

Graphical representations of the transitional segments for the performed measurements using sinusoidal, triangular and rectangular reference trajectories can be found in Figure A.9 to Figure A.14 of the appendix.

Table 5.1 depicts an overview on the worst case RMSE values of the standard ILC and the RMSE values for the revised ILC for all reference trajectories. It furthermore gives the difference between these error values as $\Delta RMSE$.

The highest improvement is achieved for the constant reference flow with $\Delta RMSE = 1.08 l/min$. Also for constant reference flow the highest overall performance is achieved with an RMSE of only $0.05 l/min$. This can be explained by the fact

5.4 Iterative Learning Control with varying disturbance

reference trajectory	$RMSE_{std_ILC,high}$	$RMSE_{resampled}$	$\Delta RMSE$
constant flow	$1.13 l/min$	$0.05 l/min$	$1.08 l/min$
sinusoidal	$0.9 l/min$	$0.3 l/min$	$0.6 l/min$
triangular	$0.79 l/min$	$0.38 l/min$	$0.41 l/min$
rectangular	$0.77 l/min$	$0.77 l/min$	-

Table 5.1: RMSE values for different reference trajectories of standard ILC and revised ILC.

that the length of the reference signal does not change for a constant flow, while this is the case for all other signals.

6 Conclusion and future work

A Appendix

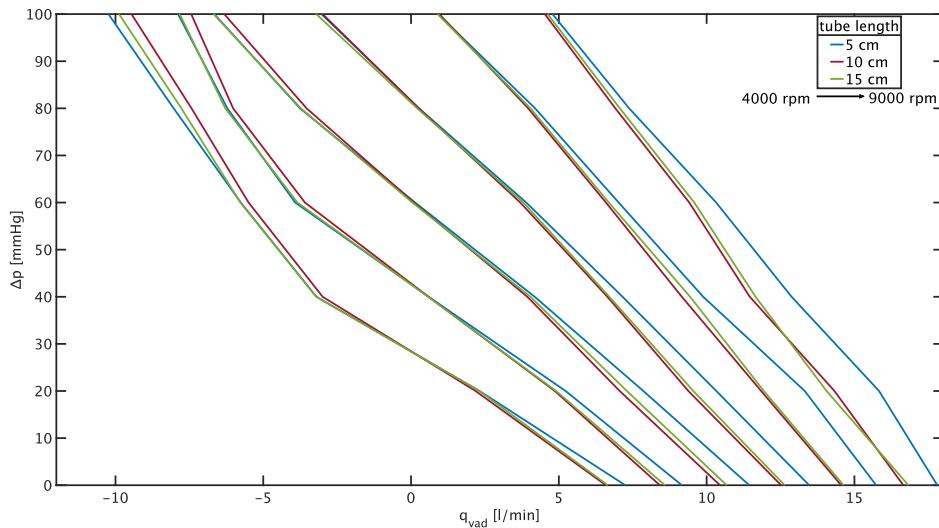


Figure A.1: Static map for varying tube length in 100 % water

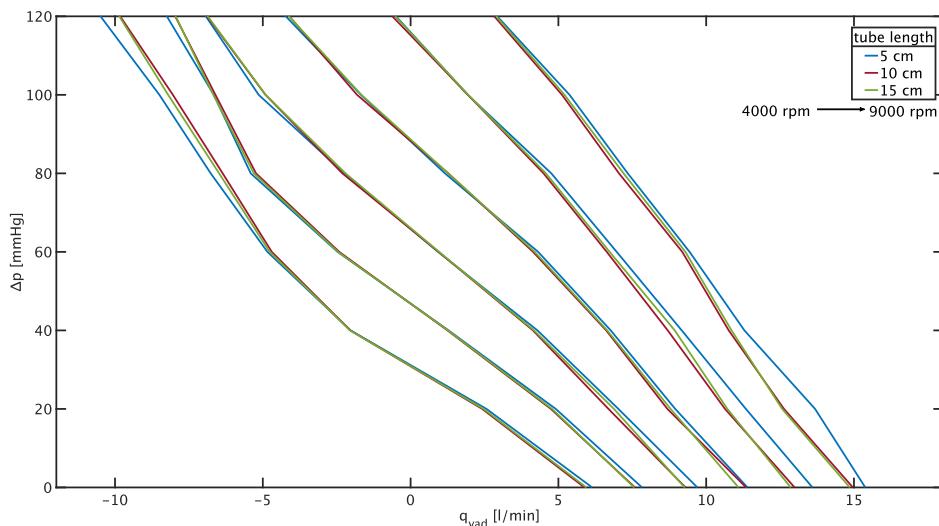


Figure A.2: Static map for varying tube length in 80 % water 20 % glycerin solution

A Appendix

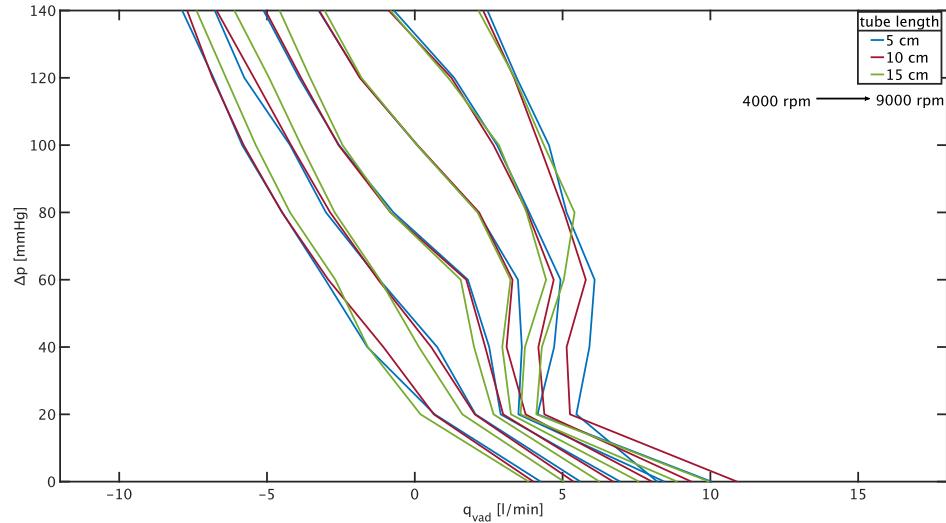


Figure A.3: Static map for varying tube length in 40 % water 60 % glycerin solution

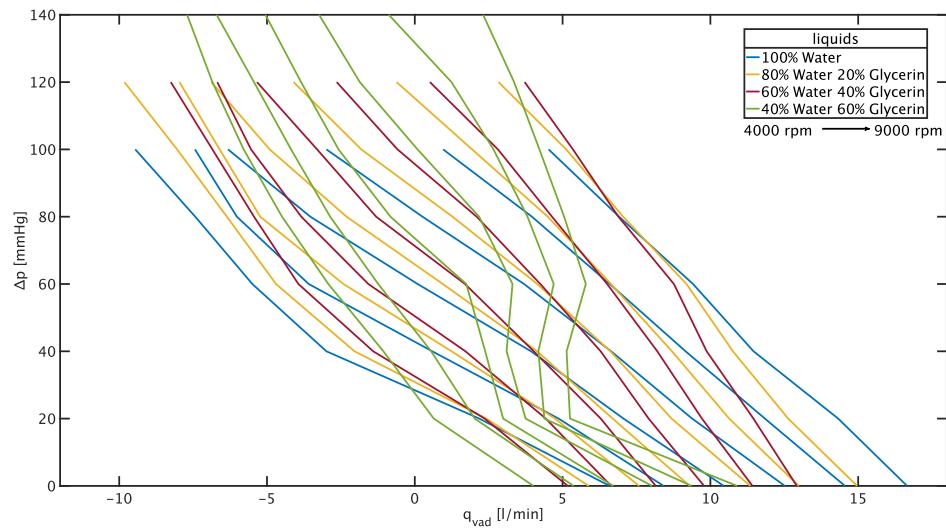


Figure A.4: Static map for varying liquid solutions with 10 cm tube length.

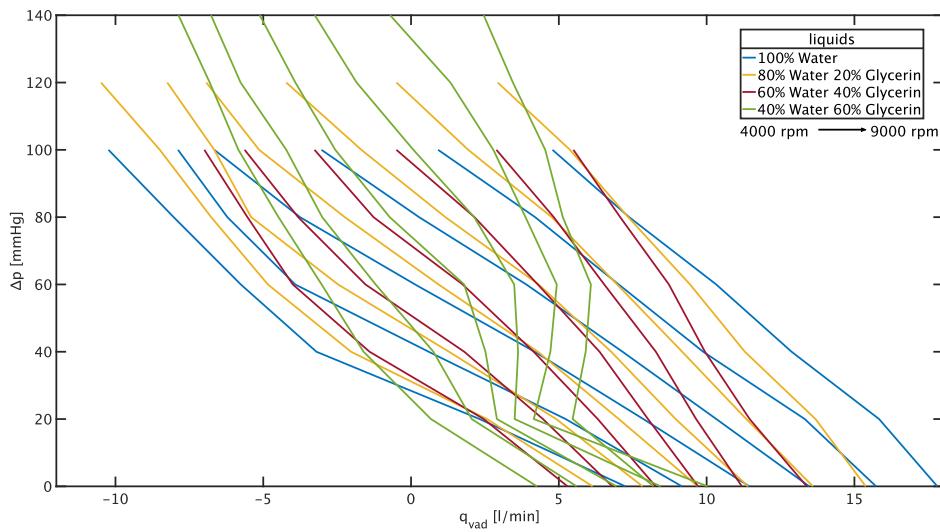


Figure A.5: Static map for varying liquid solutions with 5 cm tube length.

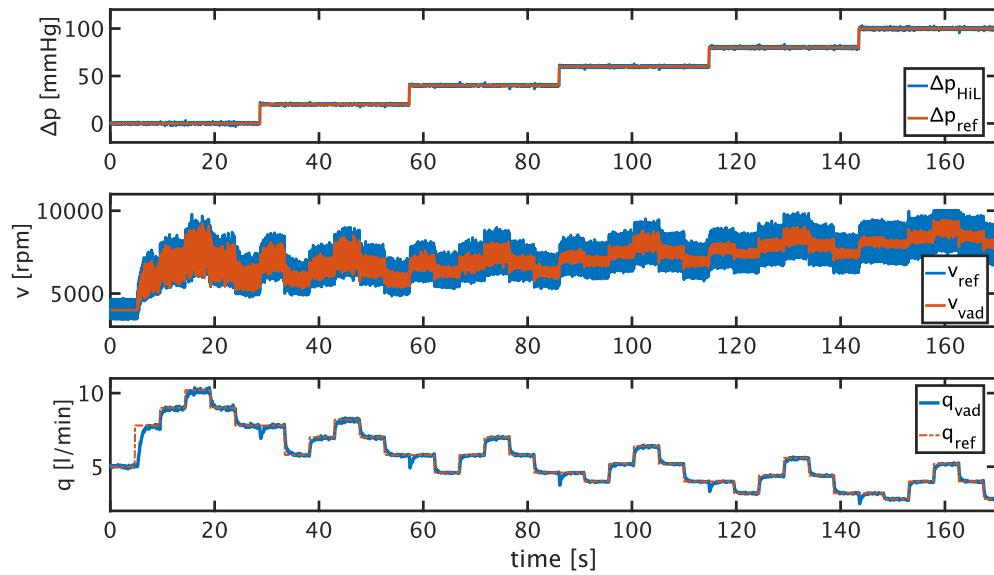


Figure A.6: Test measurement for PI controller tuned according to Chien Hrones Reswick.

A Appendix

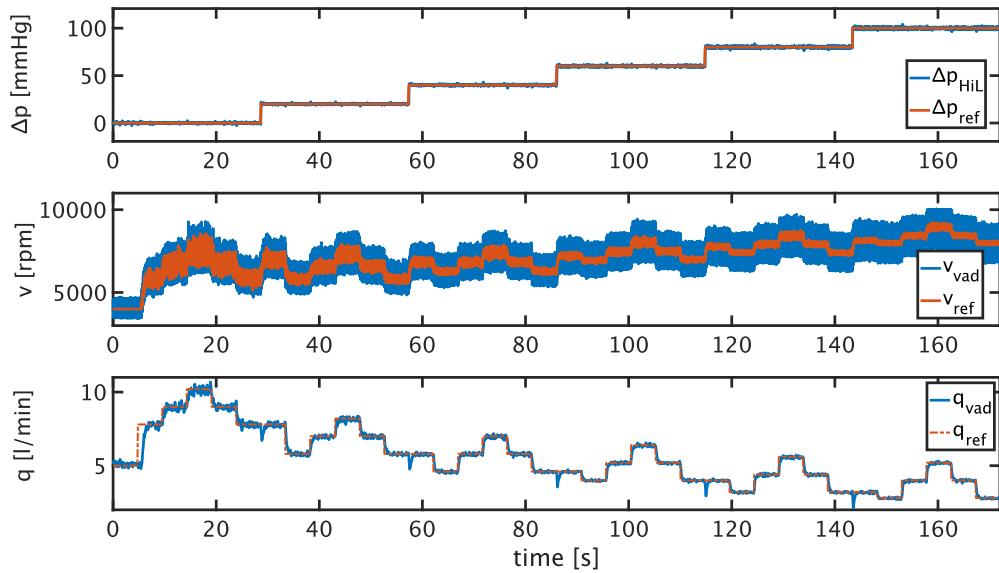


Figure A.7: Test measurement for PI controller tuned according to Ziegler Nichols.

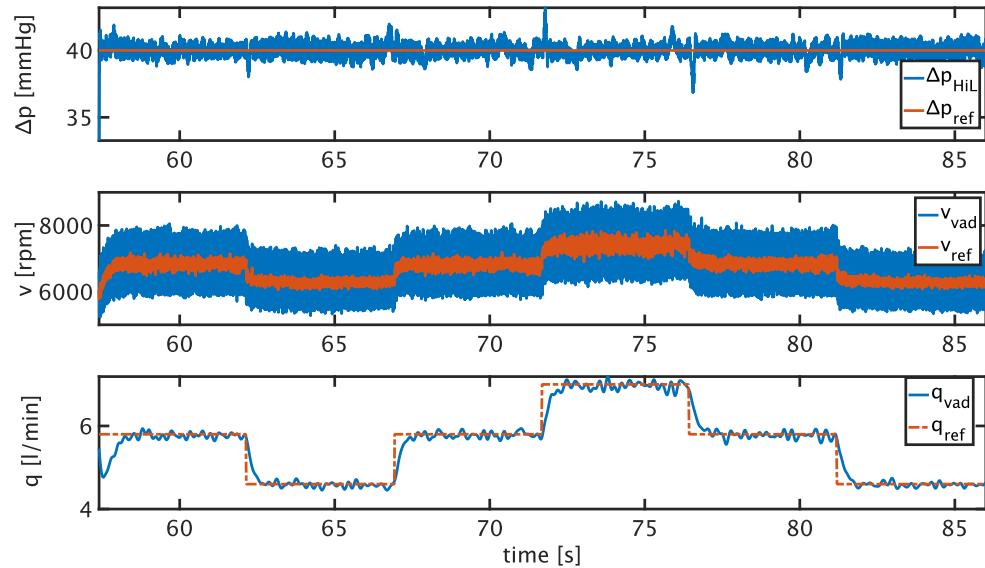


Figure A.8: Test measurement for PI controller tuned according to Ziegler Nichols at $\Delta p = 40 \text{ mmHg}$.

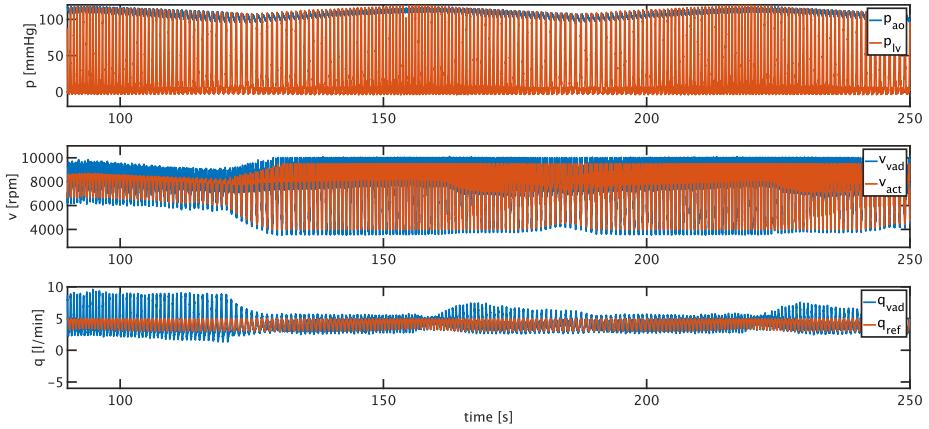


Figure A.9: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for sinusoidal reference flow without data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

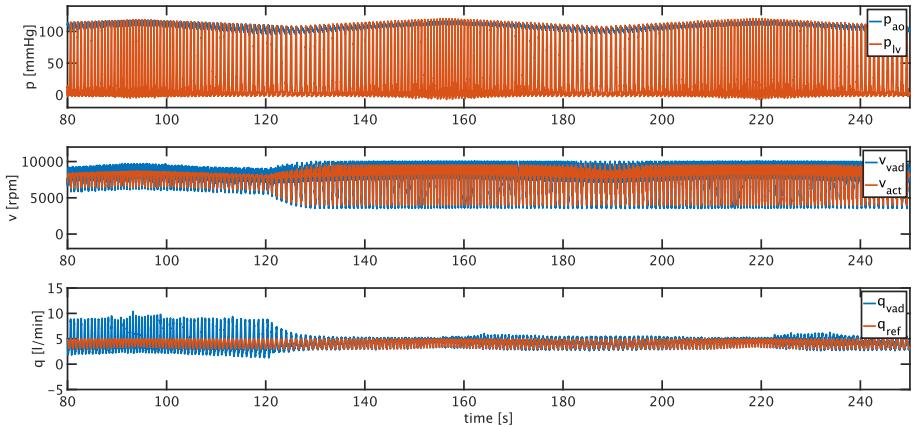


Figure A.10: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for sinusoidal reference flow with data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

A Appendix

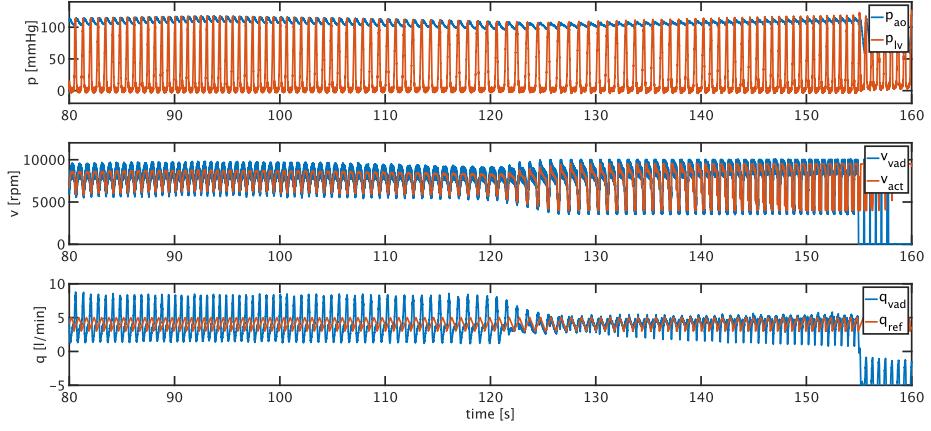


Figure A.11: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for triangular reference flow without data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

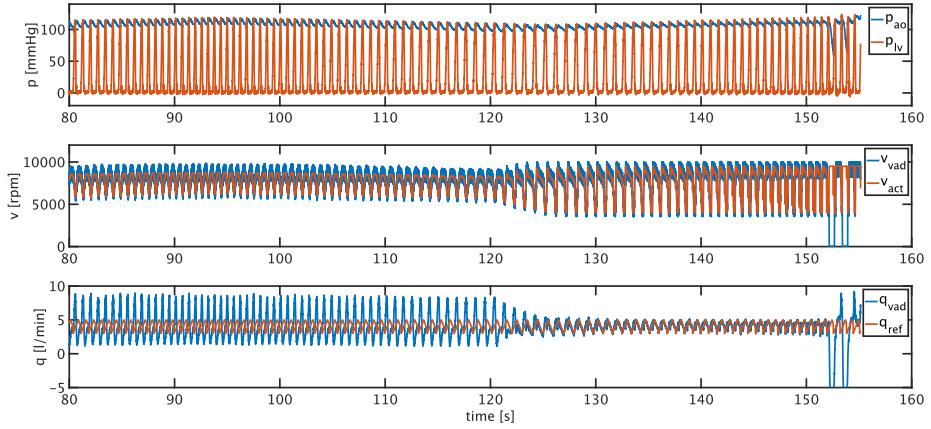


Figure A.12: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for triangular reference flow with data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

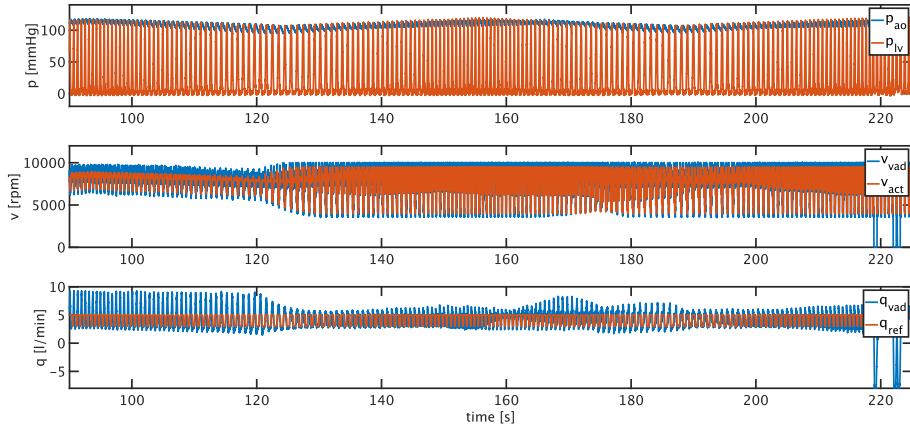


Figure A.13: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for rectangular reference flow without data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

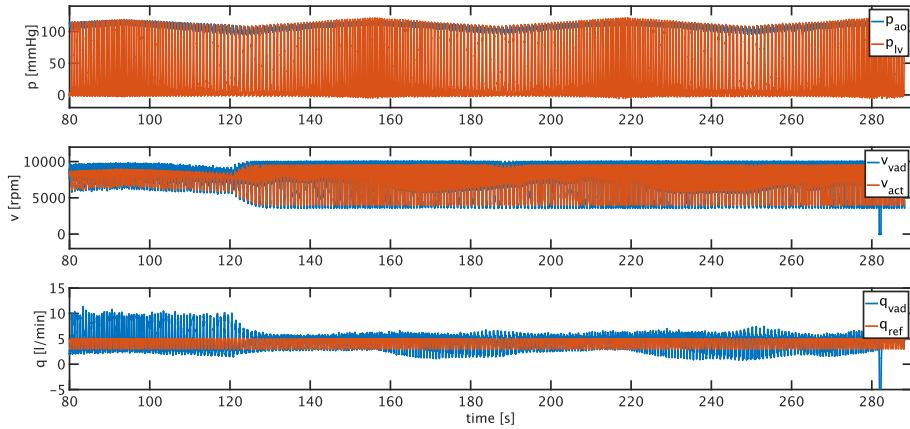


Figure A.14: Segment of measurement for ILC with varying disturbance with $cf_{Lv} = 1$ for rectangular reference flow with data resampling. Top: pressure values of the MCL. Middle: actuating variable and measured rotational speed of the VAD. Bottom: targeted flow trajectory and measured flow through the VAD

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