INF5620 — Project 1

Emilie Fjørner

e.s.fjorner@fys.uio.no

Jonas van den Brink

j.v.d.brink@fys.uio.no

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Description

In this project, we develop a general solver for the vertical motion of a body with quadratic air drag. The ability to reproduce a linear solution and the convergence rate solver is verified using the method of manufactured solutions. The solver is then applied to a skydiver performing a jump.

Differential Equation

A falling body is subject to two forces: gravity and air drag. Using a quadratic model for the air drag and applying Newton's 2. law of motion gives the differential equation

$$m\dot{v} = mg - \frac{1}{2}C_D\rho A|v|v,$$

where v is the downward velocity of the body, C_D is the body's drag coefficient, ρ is the density of the air and A is the cross-sectional area of the body perpendicular to the motion. All of these parameters will in reality vary during a skydive. The drag coefficient and cross-sectional area due to the skydiver changing posture and the density of the air as a function of height. Starting of, we will consider all three parameters as constant throughout the skydive.

To have a tidier notation, we introduce the parameter

$$a \equiv C_D\rho A/2,$$

meaning our ODE can be written as

$$m\dot{v} = mg - a|v|v.$$

Numerical Scheme

The time domain is now discretized uniformly with a step length of Δt, and the ODE sampled between two mesh points, at the time $t_{n+1/2}$. Applying a Crank-Nicolson finite difference approximation to the time derivative of the velocity

gives

$$\left[D_t v = g - \frac{a}{m}\overline{(|v|v)}^t\right]^{n+1/2}.$$

Writing this out, and using a geometric average for the for the square of the velocity gives

$$\frac{v^{n+1} - v^n}{\Delta t} = g - \frac{a}{m}|v^n|v^{n+1}.$$

Solving for the unknown, v^{n+1}, gives the numerical scheme

$$v^{n+1} = \frac{v^n + g\Delta t}{1 + a\Delta t|v^n|/m}.$$

Method of Manufactured Solution

To verify our solver, we apply the MMS. This means we include a source term to our ODE and numerical scheme. Naming the source term $f(t)$, we get the ODE

$$m\dot{v} = mg - a|v|v + f(t).$$

And the numerical scheme now looks as follows

$$v^{n+1} = \frac{v^n + g\Delta t + \Delta t f(t_{n+1/2})/m}{1 + a\Delta t|v^n|/m}.$$

To test our solver, we will attempt to reproduce an exact solution on a linear form

$$v(t) = bt + c,$$

where b and c are general constants. Insterting this exact solution into the discrete ODE gives

$$\left[D_t(bt + c) = g - \frac{a}{m}\overline{(|bt + c|bt + c)}^t + \frac{1}{m}\overline{f(t)}^t\right]^{n+1/2}.$$

The Crank-Nicolson finite difference approximation exactly reproduces the derivative of a linear function, we also use the geometric average. Solving for the source term then gives

$$f(t_{n+1/2}) = a|bt_n + c|(bt_{n+1} + c) + m(b - g),$$

shifting by a half time-step, we can write it

$$f(t) = a|bt_{n-1/2} + c|(bt_{n+1/2} + c) + m(b - g).$$

And we further rewrite it using the fact that $t_n = n\Delta t$

$$f(t) = a\left|b(t - \Delta t/2) + c\right|\left(b(t + \Delta t/2) + c\right) + m(b - g).$$

Using this source term, and comparing with the exact solution $v(t) = bt + c$ should result in an error on the order of machine precision.

Testing Convergence Rate

We are using a Crank Nicolson finite difference approximation, which is 2. order accurate. This means we should have an error that is close to proportional to Δt^2. To test this convergence rate, we need to have an exact solution to compare with. To find this exact solution, we again use the MMS. We cannot use the source term as earlier, as that already solves the discrete ODE to machine precision, it cannot possibly have an error proportional to Δt. Instead we insert our exact solution into the continous ODE and solve for the source term. The ODE becomes

$$mb = mg - a|bt + c|(bt + c) + f(t),$$

which yields

$$f(t) = a|bt + c|(bt + c) + m(b - g).$$

And it is this source term we use to test the convergence rate of the solver.

The convergence rate is calculated using the numerical L_2-norm of the difference between the computed and the exact linear solution. We assume that the error will follow a form such as

$$E = C\Delta t^r,$$

where r is the convergence rate. If we calculate the error E for two different values of Δt, and divide them, we get

$$\frac{E_i}{E_{i-1}} = \frac{C\Delta t_i^r}{C\Delta t_{i-1}^r},$$
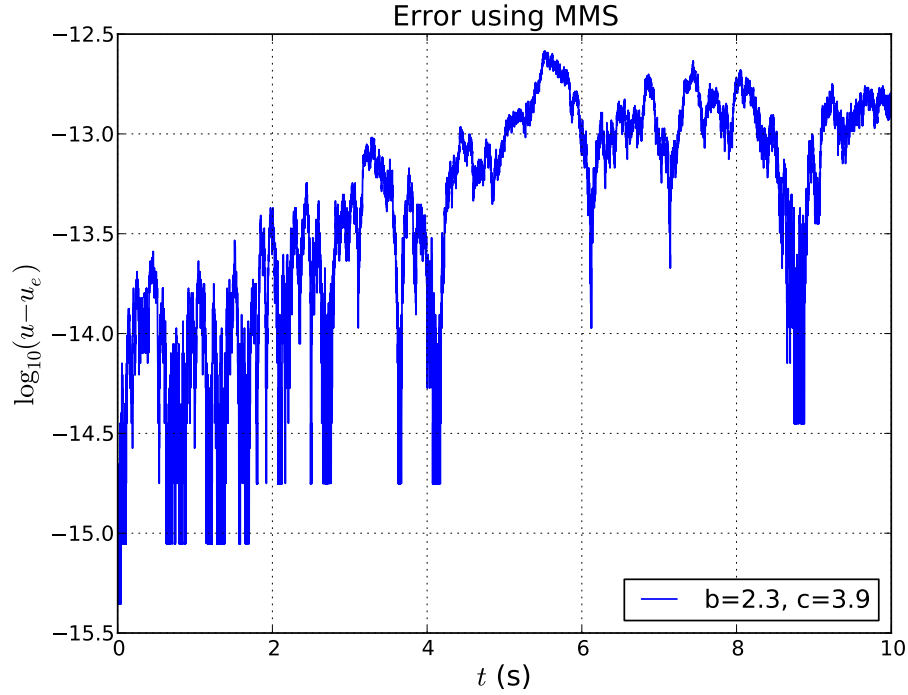
taking the logarithm gives

$$\log E_i - \log E_{i-1} = r\big(\log \Delta t_i - \log \Delta t_{i-1}\big),$$

and solving for the convergen rate we get

$$r = \frac{\log E_i - \log E_{i-1}}{\log \Delta t_i - \log \Delta t_{i-1}}.$$

Results of Verification

To test the ability of the numerical scheme to reproduce the linear solution with the source term fitted to the discrete ODE, we run the test for the exact solution $v(t) = 2.3t + 3.9$, and get the following plot of the error.

And we see that we achieve machine precision.

Testing the convergence rate for the exact solution $v(t) = 3t$ gives the following results.

Δt	E	r
10^{-1}	$7.624395 \cdot 10^{-04}$	2.01564
10^{-2}	$7.599604 \cdot 10^{-06}$	2.00141
10^{-3}	$7.597157 \cdot 10^{-08}$	2.00014
10^{-4}	$7.598826 \cdot 10^{-10}$	1.9999
10^{-5}	$7.535791 \cdot 10^{-12}$	2.00362

And so we see that our solver has a convergence rate of 2 to one decimal place. For other exact solutions it might be slightly better or worse, but it is fairly close to 2 for all linear solutions.

Simulating Skydiving

To model a skydive we let the drag coefficient and the cross-sectional area change gradually in order to simulate the parachute opening. This we achieve by letting them be variables defined at the mesh points. We keep their values constant for the part of the jump where the jumper is in free fall, and as the parachute is opened we increase their values gradually over a period of 8 seconds until they reach the appropriate values for a fully opened parachute. By making this stepwise increase we avoid the abrupt change in velocity an instantaneous change would give. As a consequence our model becomes more realistic and our skydiver gets to experience a more pleasant (and far less deadly) jump, as shown in the plot below which llustrates the velocity as a function of time.
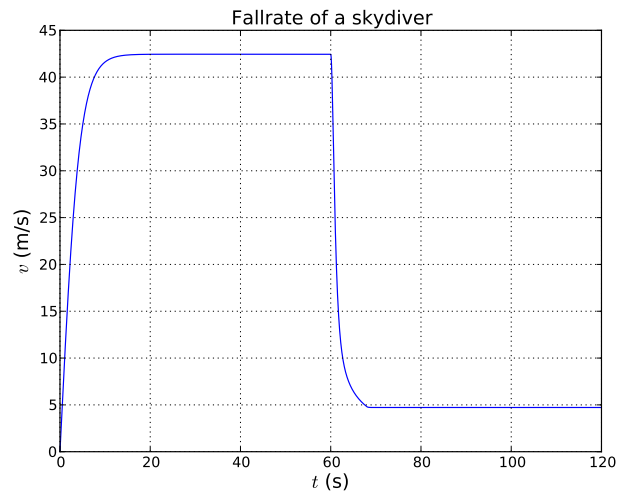
If we plot the gravity force and air drag as functions of time for this simulation, we see that the opening produces a maximum g-force of slightly more than 3 g. In this month's issue of *Parachutist*, (the official monthly publication of the United States Parachute Association) the maximum g-force experienced during a typical canopy deployment is said to fall between 3 and 5 g's. The value found therefore seems very reasonable.