



Study of the Impact of Fire Attack Utilizing Interior and Exterior Streams on Firefighter Safety and Occupant Survival

Part I: Air Entrainment and Water Distribution

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To assist the design and implementation of the experiments for the Fire Attack study, UL - FSRI has gathered fire service experts from across the world with knowledge in fire suppression and the impact of interior and exterior fire streams. The individuals below provided direction for the project, assisting in planning the experiments, witnessing the testing, and developing concrete conclusions. Their tireless support and effort make this project relevant to the fire service across the world.

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Abstract

As research continues into how fire department interventions affect fire dynamics in the modern fire environment; questions continue to arise on the impact and implications of interior versus exterior fire attack on both firefighter safety and occupant survivability. Previous research into various types of fire ground ventilation, flow paths, and exterior fire streams has provided the fire service with a more in-depth understanding of fire dynamics in addition to causing concern about certain fire attack methods stemming from differing traditions and myths. This knowledge gap and lack of previous research in this area has driven the need for further study into fire department interventions at structure fires with a focus on hose streams and suppression tactics. Statistics show that both firefighters and building occupants continue to lose their lives due to fire. As such, research into the various methods of fire attack will allow a broader understanding of how firefighter interventions on the fire ground can impact the outcome of both life safety and property protection.

This study will build and expand upon the fire research conducted to date by analyzing how firefighting tactics, specifically suppression methods, affect the thermal exposure and survivability of both firefighters and building occupants in addition to impacting fire behavior in structures. The purpose of this study is to improve firefighter safety, fireground tactics, and the knowledge of fire dynamics by providing the fire service with credible scientific information, developed from both water flow and full-scale fire testing, in representative single family homes. The project will be comprised of 3 parts:

- Part I: Air Entrainment and Water Distribution.
- Part II: Full-Scale Residential Fire Experiments.
- Part III: Acquired Structure Fire Testing.

This report details the results and analysis from the air entrainment and water distribution experiments. These tests were conducted without the presence of fire in order to gain a basic understanding of air flow and water flow before Parts II and III of the study were conducted as full-scale fire experiments. Each test was designed to quantify the air entrainment in hose streams and determine where water is distributed within compartments by evaluating the differences caused by various application methods, hose stream types, nozzle movements, pressures/flow rates, and stream locations and elevation angles. Over 150 tests were conducted in Part I of the overall study. Results from these experiment series were analyzed and reviewed with assistance from our technical panel. These results were summarized and can be seen below:

Air Entrainment -

- Air entrainment is dependent on hose stream type. (smooth bore, straight stream, fog)
- Air entrainment is dependent on structure size, compartmentation, and ventilation configurations.
- Increases in nozzle movement increase overall air entrainment.
- Different nozzle movement patterns have little effect on overall air entrainment. (O, T, Z, inverted U)
- Air entrainment, either into or out of the structure, is dependent on the horizontal distance of the nozzle to the ventilation opening.

Water Distribution -

- Water distribution is dependent on hose stream type. (smooth bore, straight stream, fog)
- Water distribution is dependent on stream elevation angle within a compartment.
- Varying water pressure at the nozzle and flow rate can affect the total amount of water applied to a given area; however, the distribution location can remain constant.
- Deflecting the hose stream off the ceiling or opposite wall of a compartment can coat the surfaces while applying little water to the center of the room.

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1 Background

Recent fire service research has highlighted the importance of applying water to the fire as quickly as possible. This tactical consideration has highlighted a knowledge gap and increased the interest in better understanding the impact of water applied as part of an interior or exterior attack. Many variables exist in fire attack that impact firefighter effectiveness and victim survivability including stream placement, the time required to get water on the fire, stream type, stream movement, air entrainment, steam development, hot gas cooling and contraction, and position of flow paths. The most important firefighting tool for many years at structure fires has been their hoseline; however, many questions have arisen as more research shows the impact of ventilation, flow paths, and exterior fire streams. Whether a fire attack crew chooses to apply water as part of an interior attack or as part of an exterior or “transitional attack,” they need to know what impact their stream has on the fire environment ahead of them. This is difficult on the fire ground because visibility is commonly limited and therefore most experience and first-hand accounts are from behind the nozzle. This results in beliefs about conditions (e.g. temperature) ahead of the nozzle team and the impact of their tactics on victim survivability; but knowledge of the actual impact has yet been researched. Additionally, when the fire is ultimately suppressed, there is no assurance the attack was conducted in the most effective, efficient, and safe manner even if the experience gained suggests that it was. Fire service adages such as “don’t put water on smoke,” “you will steam the victims,” and “fog nozzles always disrupt the thermal layer” have been passed on from generation to generation with little context or substantiation. Without the context, these concepts get treated like rules and can severely limit firefighters understanding of fire suppression.

Current fire training curriculum defines 3 fire attack methods: direct attack, indirect attack, and combination attack. Direct attack involves the discharge of water directly onto the burning fuel. Indirect attack involves directing the stream toward the ceiling of a compartment in order to generate a large amount of steam in order to cool the compartment. Converting the water to steam displaces oxygen, absorbs the heat of the fire and cools the hot gas layer sufficiently for firefighters to safely enter and make a direct attack. Combination attack extinguishes a fire by using both a direct and indirect attack. Another technique to safely approach a fire that cannot be reached with a direct attack is gas cooling. Gas cooling provides a buffer zone around the attack team but the larger the compartment, the less the impact on cooling the hot gas layer. Gas cooling must be a continuous process while advancing toward a shielded fire. Techniques for effective gas cooling and the upper limit of the volume where gas cooling is effective is not well known.

*** ADD BACKGROUND SPECIFIC TO AIR ENTRAINMENT AND ADD *** DAN TO ORGANIZE

Fire suppression effectiveness and firefighter safety are not achieved by water flow rate alone, but by appropriate use of a given flow rate under specific fire ground conditions. A flow rate must meet the critical flow rate to extinguish a fire depending on the heat release rate and should be higher to reduce the time to extinguishment. Drastically exceeding the critical flow rate has less known impact on time to extinguishment but has a significant impact on the total amount of water used. To-date, there is little data to connect the critical flow rate to firefighter safety. However, it has been estimated that only 5 to 10 percent of water applied during fire attack contributes to extinguishment. It is difficult for firefighters to realize the efficiency of various hose stream techniques due to poor visibility on the fireground. However, by developing data in realistic structures, fuel sources, and fire scenarios, important inferences may be developed relative to different hose stream techniques, and use of water.

2 Objectives

2.1 Objectives

The purpose of this part to the overall study was to provide the fire service with scientific based knowledge on the impact of hose streams during interior and exterior fire attack on firefighter safety and trapped occupants to improve training and decision making on the fire ground. This was accomplished with the completion of the following objectives:

- Improve firefighter safety by increasing knowledge of fire suppression.
- Develop knowledge of hose streams applied during an interior and exterior fire attack and its impact on firefighter safety and victim survivability.
- Understand where water goes and how air flows during interior and exterior fire attack utilizing common equipment, practices, and tactics.
- Gain understanding of the impact of water streams depending on the volume of the fire compartment/structure.
- Bring the ‘Science to the Streets’ by transferring science based conclusions founded on experimental results that can be incorporated into firefighting standard operating procedures.

2.2 Limitation and Scope

The purpose is to quantify the amount of air entrainment in hose streams given certain parameters as well as determine where water is distributed within a compartment. This is all without fire involvement in order to provide a baseline understanding before moving forward with the remainder of the study. This baseline knowledge is intended to bridge the gap in the fire service understanding about the use of various nozzles, hose stream types, nozzle movements, and advancement techniques in specific scenarios. Knowing how hose streams affect air movement and how water is distributed can allow for better decision making capabilities across the fire service when it comes to use during an actual emergency incident.

When analyzing the air entrainment and water distribution, equipment from various manufacturers was tested. For the purpose of the study, the companies will be referred to as Manufacturer I, Manufacturer II, and Manufacturer III. The air entrainment experiments yielded results that showed little to no difference among the various manufacturers. Therefore, a single manufacturer was chosen for the remainder of Part I of the study. More specifically, Part I of the study is not intended to purchasing of one type of nozzle over another.

The intent of the air entrainment experiments was to determine how much air hose streams entrain. This involved several components:

- Does the hose stream type (smooth bore versus straight stream versus narrow fog) effect air entrainment?
- Does the amount of air entrainment vary dependent on manufacturer given set flow rates/pressures?
- How do different building geometries, compartment layouts, and ventilation configurations effect air entrainment?
- Do various nozzle movements effect air entrainment (fixed, sweeping, O, T, Z, inverted U)?
- Does the distance from a ventilation opening effect the air entrainment?

Additionally, the intent of the water distribution experiments was to determine where water goes within a compartment. In order to answer this question, the tests considered the following:

- Does interior versus exterior attack effect water distribution?
- Does the hose stream type (smooth bore versus straight stream versus narrow fog) effect water distribution?
- Does the hose stream elevation angle effect water distribution?
- Does adjusting the flow rates/pressures of the nozzles effect water distribution?
- Do various nozzle movements effect water distribution (fixed, sweeping, O)?
- How does a first floor exterior attack effect the water distribution when compared to a second floor exterior attack?

For the purpose of these experiments we utilized the same structure throughout all of the air entrainment experiments. The water distribution testing utilized another structure, which also remained the same for the duration of those experiments. The only component of the firefighting equipment that was varied among the tests was the nozzle, and sometimes the hoseline size. The hoseline diameter was either 1 3/4 in. or 2 1/2 in. and was always 200 ft. in length. By creating some aspects that were not varied and by bounding other variables, we ensured that all aspects of the air entrainment and water distribution were examined as a baseline for further future evaluation in different structures with different conditions.

3 Previous Literature

At the start of the study, a literature review was performed to identify and analyze the following:

- Previous research in the field of air entrainment, water distribution, and fire suppression.
- Both past and current fire suppression tactics.
- Knowledge gaps in fire suppression operations. (choice of tactics, myths, traditions, etc.)

The following section outlines some of the material as it relates to the fire attack study. The literature review encompassed past research work, various articles in fire service publications, fire service training manuals, as well as fire department standard operating procedures to highlight some of the critical areas of information which drove the project at hand.

3.1 Literature Overview

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Hose, nozzles and water have been used by the fire service for hundreds of years. Despite their frequent use, there has been little scientific research conducted on the effective use of these tools for fire suppression. It is common in the fire service to find discussions about which nozzle is better or which flow rate is required for what sized fire but this is based on experience and usually not science.

In 1950 Chief Lloyd Layman presented a paper titled Little Drops of Water at the Fire Department Instructors Conference. He introduced what he called indirect method of attack to suppress interior building fires by using the heat absorbing properties of expanding and condensing steam, produced in great quantities by fog streams. The conclusions were based on Coast Guard experiments that Layman was in charge of conducting at the Coast Guard Firefighting School at Fort McHenry in Baltimore, MD. Layman continued his experiments after he returned to his position as fire chief in Parkersburg, WV where he applied his tactic in building fires. This research had a very large impact on the fire service and their suppression techniques to this day.

Throughout the 1950s a National Committee began conducting experiments to collect data on the growth and behavior of interior fires and how to most effectively suppress them. Keith Royer and Bill Nelson were members of this committee, and as the heads of the firemanship training program at the Iowa State Universitys Engineering Extension, they collected and analyzed data from hundreds of experimental fires. Through this research the fire service was taught about fire behavior and how to suppress fire with a combination fire attack. They examined the amount of heat generated by common fuels, the heat absorbing capacity of water, the impact of compartment volume during suppression and they developed the Iowa formula. The Iowa formula or critical rate of flow formula is still used today and it determines the amount of water needed to control a fire in the largest open space within a structure by dividing the cubic foot volume of the space by 100.

While the physics of fire development has not changed over time, the fire environment for specifically the single family home has evolved. Several factors including home size, geometry, contents and construction materials have changed significantly over the past 50 or more years. Each of these factors has impacted firefighter and occupant safety. Faster fire propagation, shorter times to flashover, rapid changes in fire dynamics and shorter escape times all impact fire service suppression techniques and effectiveness. Many of the variables in Royer and Nelsons analysis have changed and more research is needed to see how suppression techniques used in the 1950s with 1950s fuel loads and firefighting tools translates to todays firefighter safety and effectiveness.

Beginning in 1994, the Naval Research Laboratory carried out a series of full-scale fire experiments to compare straight stream attack versus fog pattern attack. These experiments were conducted on the Navy ship ex-USS Shadwell with a fire volume of approximately 110 m³. In these experiments one 60 degree fog pattern was applied at a 45 degree angle into the smoke layer. They examined cooling effects, steam generation and thermal layer disruption. Their experiments examined shielded and non-shielded fires and concluded that using fog to cool the upper layer was more effective and safer than straight stream attack when the fire could not be attacked directly and the firefighters heart rates and body temperatures were lower utilizing the fog attack.

In 1998 NIST conducted a series of experiments to demonstrate the suppression effectiveness of water-based firefighting agents. This was a step toward creating test procedures to determine suppression effectiveness to develop a standardized test method for evaluating the fire fighting effectiveness of water and other agents. This study provides preliminary data upon which firefighting effectiveness test may be developed by it suggests additional research on application technique, tests reflective of the complexities found in firefighting and experiments involving structural-fire suppression.

In 2002, The National Research Council of Canada conducted a literature search on 3D water fog techniques for firefighting. It discusses the impact of water fog characteristics associated with properties of the nozzle (e.g., droplet size, momentum, flow rate, spray angle and pattern) and discharge techniques (e.g., discharge angle, and discharge duration related to the bursts) on performance of the 3D water fog technique are discussed. This technique is to supplement a direct attack by controlling the environment the firefighters are in until they are in a position to apply water directly to the fire. Opponents of flowing water into smoke have concerns that include: (i) effectiveness of controlling the fire, compared to traditional straight stream attack; (ii) possible disruption of the thermal balance; (iii) possible generation of a large amount of hot steam that produces burn injuries to firefighters; and (iv) the performance of this technique is complex and requires extensive training. Advocates of this technique have attempted to respond to these concerns but very limited experimental studies have been undertaken do to complexity of the problems. Application techniques and fire conditions on the the performance of fog technique is not well studied and therefore there are little guidelines and adoption will be greatly limited.

Several theoretical studies had been conducted that examine droplet size and their ability to suppress fire gases. For example, when droplet diameter is reduced from 1000 nanometers to 100 nanometers the total surface area increases 10 times from 6 m² to 60 m² for 1 liter of water. Since these smaller droplets evaporate sooner, others have examined the lifetime of the droplet to determine how far it can travel based on temperature of the surrounding gases and droplet size. Further complicating this theory is that droplets all have an impact on each other as they turn to steam. Residence time can be further reduced compared to an individual droplet, because leading droplets impart forward momentum to the surrounding gas, reducing the air drag on the following droplets and resulting in better penetration. In 2010, the University of Maryland examined spray characteristics from fire hose nozzles. They examined the breakup of a smooth bore nozzle utilizing techniques such as shadowgraphy and a patternator and concluded that more research was needed to fully understand the water spray from fire hose nozzles.

In 2000, Lund University examined the demand for extinguishing media in manual firefighting. They examined critical flow rates required to suppress fires by reviewing available literature and conducted a series of experiments that examined suppression of wood pallets at a fire training academy. They examined the five ways that water can be applied during fire extinguishment, on hot gases, on flames, on burning fuel, on fuel that is not yet burning and on hot surfaces. They highlight that what is most effective against the fire is not necessarily best for the firefighters since there are other constraints during firefighting operations such as limited air supply and multiple priorities. The optimum flow rate corresponds to an optimum control time, a control time that gives the lowest total demand for resources. Most of the current data for optimum water flow rate include experiments utilizing wood cribs or pallets, but not todays synthetic fuel loads in actual structures. These studies also did not investigate the effect of flow paths or the impact of steam generation on firefighters or victims.

In 2003, a fire service group at the Rockland County (NY) Fire Training Center conducted a series of

tests in their concrete training building. They measured the amount of air moved by solid bore and combination nozzles using common fire ground methods. They concluded that air volumes moved by smooth bore nozzles and combination nozzles in the straight stream setting are very similar if not the same, and that combination nozzles in the fog pattern move significant amounts of air which can over pressurize the fire area and send steam over the attack crew even with a ventilation opening opposite the attack crew. These tests were performed either with no fire or with a training fire but which are very different than actual fire conditions. Their tests do provide a good range of airflows that can be expected in our experiments. The authors state, Our nozzle testing program was not as controlled and as precise as we would have liked. They also did not have measurement devices that were able to accurately measure air flows from a fog pattern.

The Firefighting Technology Group at NIST has a current project that is examining hose streams. This project examines a variety of fire fighting hose stream characteristics related to flow, distribution and thermal impact from both solid and fog stream nozzles. A series of real scale, laboratory based experiments have been started to look specifically at the water discharge and distribution characteristics, the impact of hose streams on a hot gas layer in a compartment, the impact of hose streams on gas flows through multi-compartment structures, and the suppression effectiveness on burning piles of wooden pallets. The proposed project will build on their results by utilizing real-scale structures with common residential fuels and making additional measurements to better characterize the impact of flow path, nozzle technique and steam generation on fire dynamics, firefighter exposure and occupant survivability.

3.2 Fire Service Publications

[MIKE]

3.3 Fire Service Training Manuals

[MIKE]

3.4 Research Work

[MIKE]

4 Air Entrainment Experiments

4.1 Test Setup

4.1.1 Structures

The air entrainment testing was conducted at the Delaware County Emergency Services Training Center in Sharon Hill, PA. A two-story concrete structure was built on a concrete slab as shown in Fig. 4.1. It was designed to simulate a representative residential structure.



Figure 4.1: Delaware County, PA Fire Test Structure

The outer walls of the first floor of the structure were composed of interlocking concrete blocks 2 ft. wide, 2 ft. high, and 4 ft. long. The interior dimensions of the structure were 20 ft. wide, 36 ft. long, and 8 ft. high. The joints and gaps between the blocks were filled with high temperature insulation. The interior walls of the first floor were framed with steel studs set to 16 in. centers and track and were lined with 0.5 in. thick cement board. The walls were composed of 0.6 in. Type X gypsum board. Additionally, the ceiling was composed of two layers of 0.5 in. thick cement board. The first floor ceiling support of the structure was composed of wood truss joist I-beams (TJIs) with a 11.75 in. depth. Each TJI was composed of laminated veneer lumber flanges with a cross section of 1.13 in. x 1.75 in. and an 0.43 in. thick oriented strand board web. Tongue and groove oriented strand board of 0.72 in. thickness was screwed to the top of the TJIs.

A stairwell was built to connect the two floors of the structure. The stairs had a 7.25 in rise and 7.5 in run and started 5.25 ft off the south wall with a width of 14 ft off the east wall. The second story walls were wood framed with 2 in by 4 in studs. The studs were set to 16 in centers. The interior walls were

protected by 0.63 in fire rated gypsum board, 0.63 in Durock board, and a second layer of 0.63 in fire rated gypsum board. The exterior walls were protected with 0.31 in oriented strand board and 0.31 in fiber cement lap siding. Dimensioned drawings of the first and second floor are shown in Figures 4.2 and 4.3 respectively.

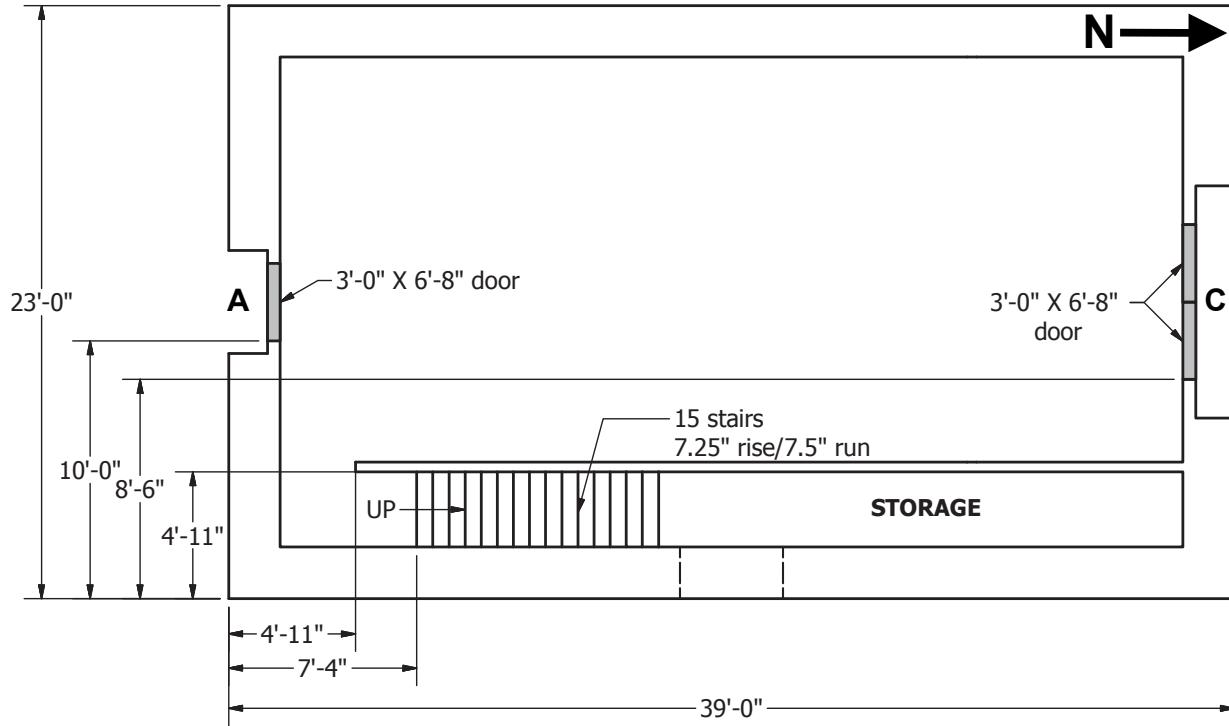


Figure 4.2: Delaware County, PA Fire Test Structure First Floor

The exterior doorways of each structure were steel doors that were opened or closed at certain instances during tests to change the ventilation configuration within the structure. All other doorways in the structures did not contain a door. If it was determined that these doors needed closed during a test, a sheet of either gypsum board or oriented strand board was used to cover the opening and remained as such until the conclusion of the given test.

4.1.2 Instrumentation

Gas velocity, a measure of air entrainment by hose streams, was obtained through the use of an array of bi-directional probes. Bi-directional probes were connected to a pressure transducers to evaluate the change in pressure associated with the gas flow. The differential pressure transducer was a Setra Model 264 with a range of +/- 0.5 in. WC (+/- 124.5 Pa.). The uncertainty given by the manufacturer is 1% or 1.2 Pa.

A gas velocity measurement study examining the doorway flow of pre-flashover compartment fires yielded expanded uncertainty measurements ranging from ± 0.14 to ± 0.22 for bi-directional probes of similar design [?]. The total expanded uncertainty for gas velocity in these experiments is estimated to be $\pm 18\%$.

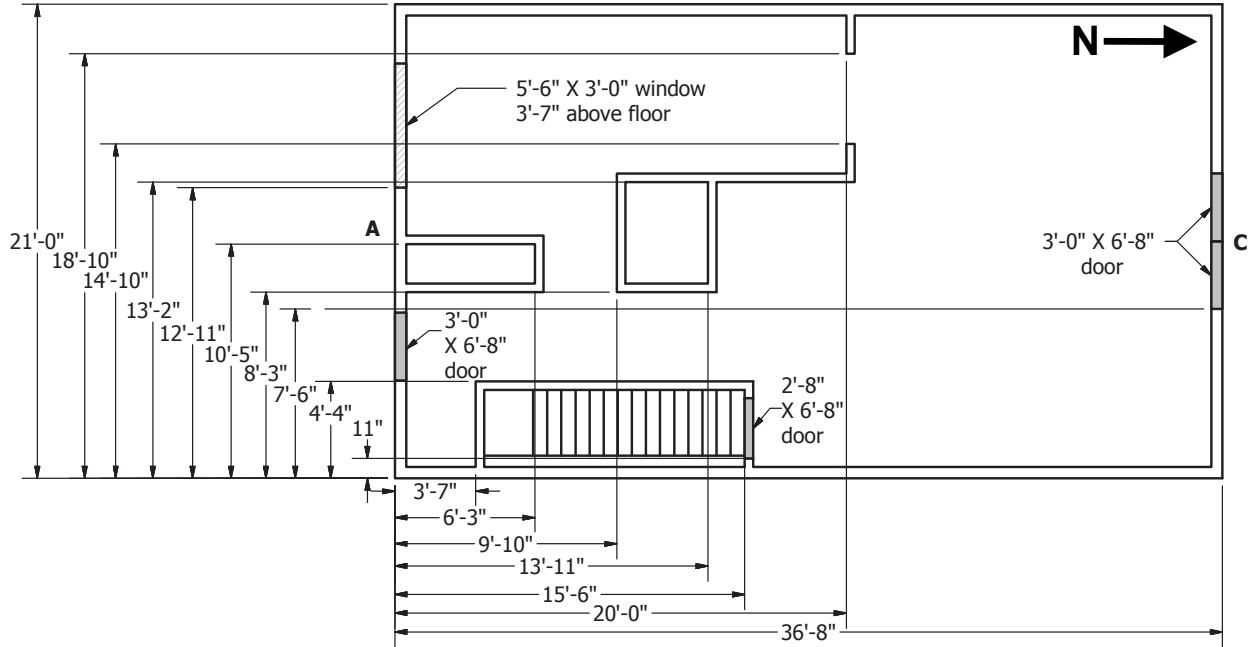


Figure 4.3: Delaware County, PA Fire Test Structure Second Floor

4.1.3 Measurement Locations

There were several challenges associated with measuring air entrainment from hose streams. The first challenge existed because the experiments were conducted outside, therefore considering wind was critical. Additionally, the instrumentation used in data collection is best in a dry environment to maintain the smallest level of uncertainty and remain operational. To address these challenges, the measurement location was set at the doorway at the top of the stairwell. Figure 4.4 shows the position of the bi-direction probe array on the second floor.

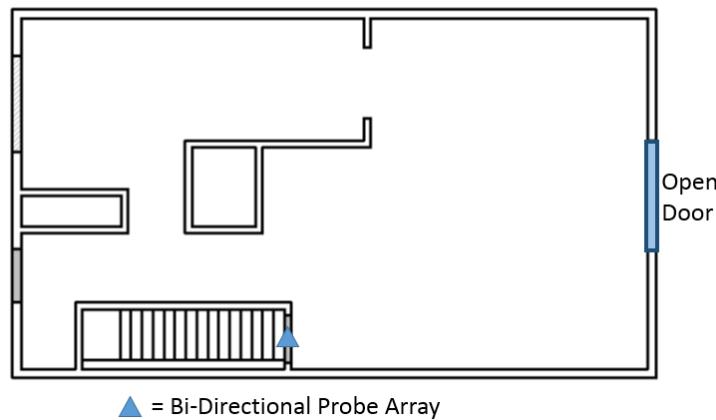


Figure 4.4: Measurement Location (Second Floor)

Figures 4.5 and 4.6 show the experimental configuration for the interior flow tests and exterior flow tests, respectively. The arrows indicate the flow direction based on the hose stream being the source of the flow through air entrainment.

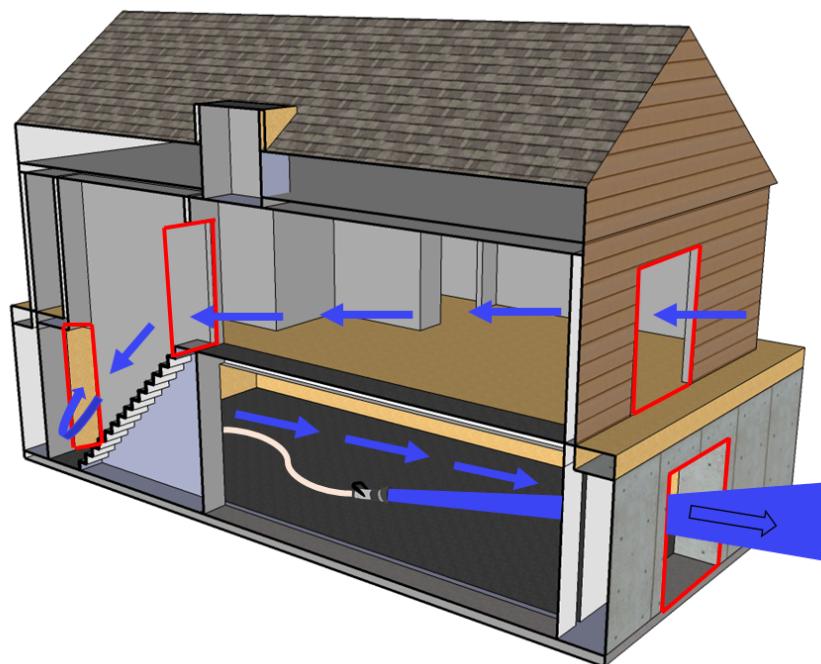


Figure 4.5: Air Entrainment Flowpath, Interior Experiments

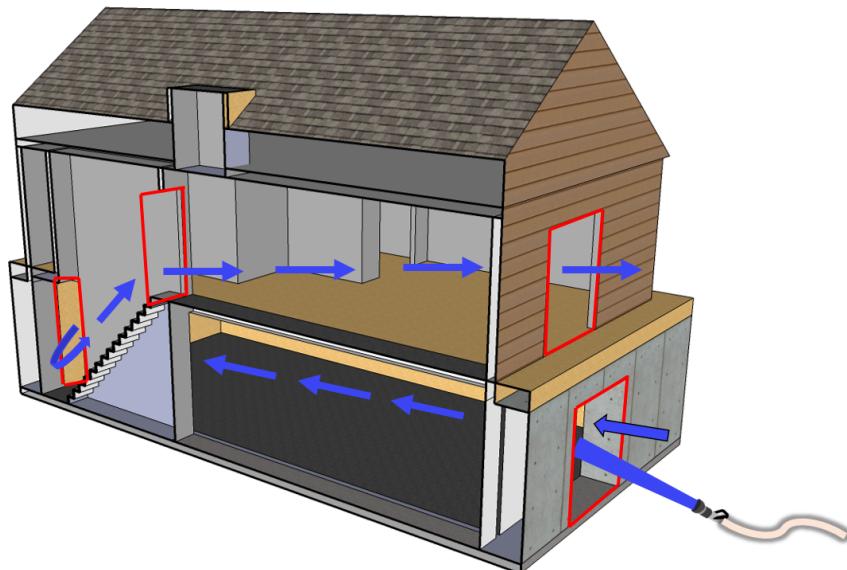


Figure 4.6: Air Entrainment Flowpath, Exterior Experiments

The measurement location was placed at the top of the stairs, within the flow path of both test configurations. This location kept the instrumentation dry and out of the reach of a hose stream. While this location did guarantee isolation from wind effects due to open vents, this represented the best location to minimize those effects.

4.1.4 Equipment Used

In order to ensure the data collected and associated results were applicable to the majority of the fire service, our technical panel was tasked with creating a list of representative nozzles, specified flow rates/pressures, and nozzle movement techniques. All of these variables were tested during the air entrainment experiments; however, several other aspects were held constant such as the length of hose used. The nozzles utilized during these experiments can be seen in the Table 4.1.

Table 4.1: Nozzles Used In Testing

Line Size	Nozzle	Tip (in)	Nozzle Pressure (psi)	Approximate Flow Rate (gpm)
1 3/4 in.	Smooth Bore	1	50	210
	Smooth Bore	15/16	50	180
	Smooth Bore	7/8	50	150
	Fog		100	100
	Fog		100	150
	Fog		75	150
	Fog		50	150
2 1/2 in.	Smooth Bore	1 1/8	50	260
	Smooth Bore	1 1/4	50	320
	Fog		100	250
	Fog		75	250
	Fog		50	250
Portable Monitor	Smooth Bore	1 3/8	80	500
	Fog		75	500
Master Stream	Smooth Bore	1 1/2	80	600
	Smooth Bore	1 3/4	80	800
	Fog		100	500-1000

When determining how to create a test setup that would involve the repetition of nozzle movements and patterns, it was vital to ensure human fatigue of the nozzle operator would not affect the results. Thus, the UL - FSRI engineers designed a nozzle prop to serve as the ‘backup’ firefighter by supporting the hoseline and nearly eliminating any potential nozzle reaction and fatigue.



Figure 4.7: Nozzle Prop

The hose was affixed to the prop with ‘C’ clamps and locking nuts to ensure the hose did not move during a given experiment. The prop served as support for both 1.5 in. and 2.5 in. hoseline sizes. The distance from the nozzle to the ventilation opening was measured from the tip of the nozzle, and not the base of the prop, and thus the measurements between the experiments were consistent.



Figure 4.8: Nozzle Prop in Use

4.2 Experiments Conducted

The experiments to determine the amount of air entrained by hose streams consisted of several test series to gain a wholeistic view of how varying different components, either with the structure or equipment utilized, affected the end result.

Prior to determining the parameters for the test series' below, several preliminary experiments were conducted in order to provide insight into several key components including the setback distance from the nozzle to the ventilation opening, the hose stream type, and various nozzle movements.

- **Setback Distance**

Two experiments were conducted on the interior of the structure utilizing a 1.5 in. combination nozzle with a flow rate of 150 gpm to determine the effects of altering the setback distance of the nozzle to the ventilation opening on the overall air entrainment in the hose stream. The first of the two tests examined setback distances of 3, 6, 9, 12, and 15 feet from the open double door at a pressure of 50 psi. The second test examined the same setback distances at a nozzle pressure of 100 psi.

- **Hose Stream Type**

To gain an initial look into the hose stream type, a fixed setback distance of 3 ft. was chosen and the nozzle was varied to a wide fog pattern (nearly occluding the ventilation opening), a narrow fog pattern (roughly 30 deg.), and a straight stream pattern. This provided preliminary information that aided in the test setup for the remainder of the experiments. The nozzle used during this test was a 1.5 in. combination nozzle with a flow rate of 150 gpm and a pressure of 100 psi.

- **Nozzle Movements**

Because there are numerous nozzle movements that firefighters can employ during suppression operations, it was vital that the UL - FSRI team identify any differences in air entrainment prior to conducting the remainder of the study. This would provide information into whether or not the various nozzle movements would all be tested or if some could be eliminated due to similarities in results. These tests were conducted with a fixed setback distance of 18 ft. from the ventilation opening and utilized both a 1.5 in. combination nozzle with a flow rate of 150 gpm and a pressure of 100 psi and a 1.5" smooth bore nozzle with a 1" tip flowing 210 gpm at a pressure of 50 psi.

- **Manufacturer Comparison**

Similar to the issue above with various nozzle movements, fire departments across the world used nozzles made from different manufacturers. To provide some insight into the accuracy of manufacturer ratings of flow rate and pressure in addition to air entrainment, several experiments were conducted to determine the differences in nozzle manufacturers. These experiments were all conducted with both a 1.5 in. combination nozzle and a 1.5 in. smooth bore nozzle. This would provide information into the differences in air entrainment between nozzles with similar flow rates and pressures made by different manufacturers.

4.2.1 Total Air Entrainment Comparison

The first test series of the air entrainment experiments looked at the differences in total entrainment given a single nozzle manufacturer with varying flow rates and pressures. These tests were conducted from both the interior and exterior of the structure at a setback distance of 18 ft. from the ventilation opening.

An ‘Event’ is defined as a specific measurement period during the experiment in which a specific variable is being analyzed. For example, during the total air entrainment experiment for 1.5 in. combination nozzles from the interior, 6 different events were incorporated within the test: 1) Straight Stream, 2) Straight Stream ‘O’, Straight Stream ‘Z’, Straight Stream ‘n’, Narrow Fog, and Narrow Fog ‘O’. In order to ensure consistency among results, each of the ‘Events’ within the experiments was designed to be 1 minute in duration.

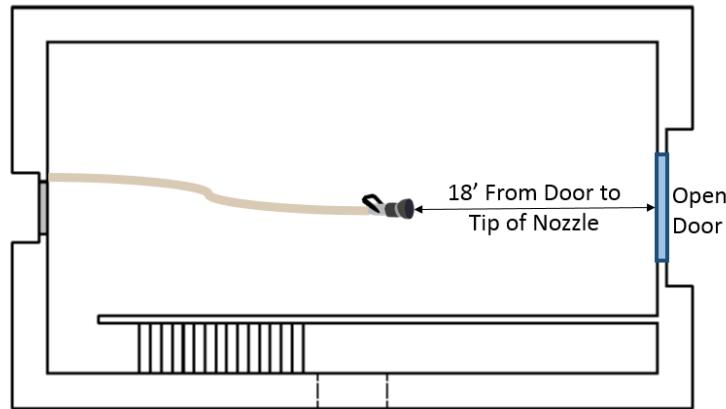


Figure 4.9: First Floor Setup - Total Entrainment Interior Tests

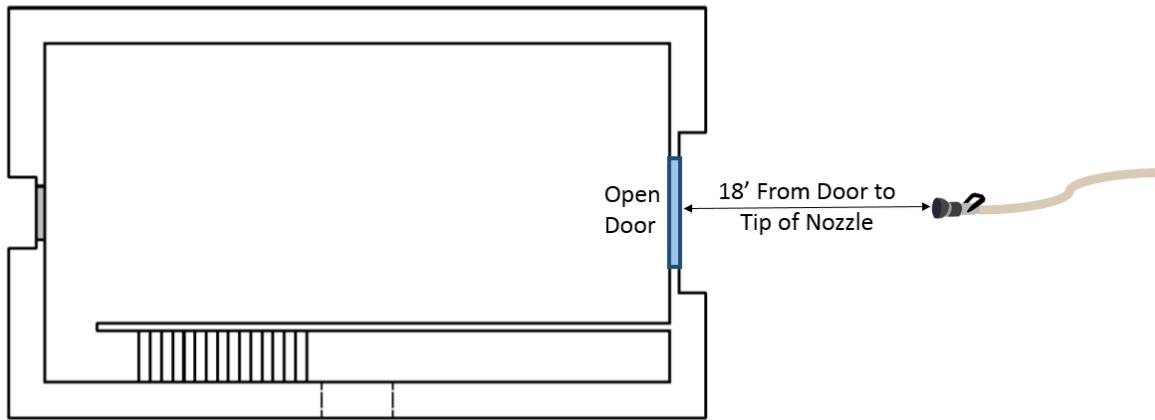


Figure 4.10: First Floor Setup - Total Entrainment Exterior Tests

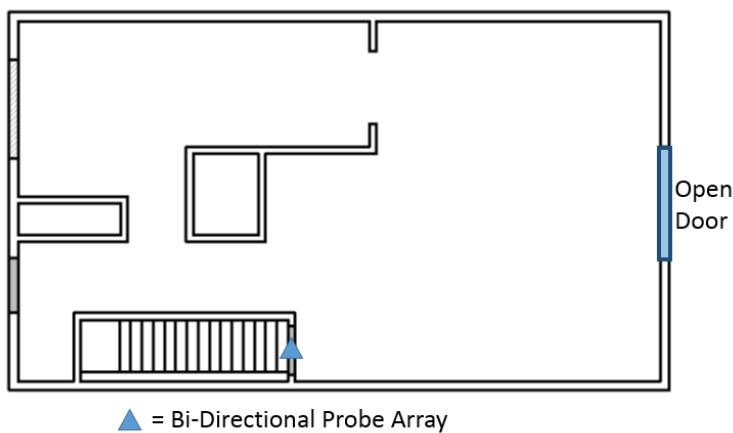


Figure 4.11: Second Floor Measurement Location

Table 4.2: Air Entrainment Experiments

Location	Nozzle Size	Nozzle Type	Tip Size	Flow Rate	Pressure
Interior	1.5	Combination		95	100
Interior	1.5	Combination		150	50
Interior	1.5	Combination		150	75
Interior	1.5	Combination		150	100
Interior	1.5	Smooth Bore	7/8	150	50
Interior	1.5	Smooth Bore	15/16	180	50
Interior	1.5	Smooth Bore	1	210	50
Interior	2.5	Combination		250	50
Interior	2.5	Combination		250	75
Interior	2.5	Combination		250	100
Interior	2.5	Smooth Bore	1 1/8	260	50
Interior	2.5	Smooth Bore	1 1/4	320	50
Interior	MS	Combination		500	100
Interior	MS	Combination		750	100
Interior	MS	Smooth Bore	1 1/2	600	80
Interior	MS	Smooth Bore	1 3/4	800	80
Interior	PM	Combination		500	80
Interior	PM	Smooth Bore	1 3/8	480	80
Exterior	1.5	Combination		150	75
Exterior	1.5	Smooth Bore	15/16	180	50
Exterior	2.5	Combination		250	75
Exterior	2.5	Smooth Bore	1 1/4	320	50
Exterior	PM	Combination		500	75
Exterior	PM	Smooth Bore	1 3/8	500	80

4.2.2 Ventilation Configuration

The second series of tests conducted to analyze air entrainment in hose streams involved varying the ventilation configurations within the flow path. The inlet and exhaust of the flow path were varied between both different sized doors as well as windows to show the effect on overall air entrainment. The tests were conducted from both the interior and the exterior of the structure with a fixed setback distance of 18 ft. from the ventilation opening. The measurement location during these experiments remained the same as that used during the total air entrainment experiments with the instrumentation remaining in the doorway at the top of the stairs on the second floor. (Figure 4.14)

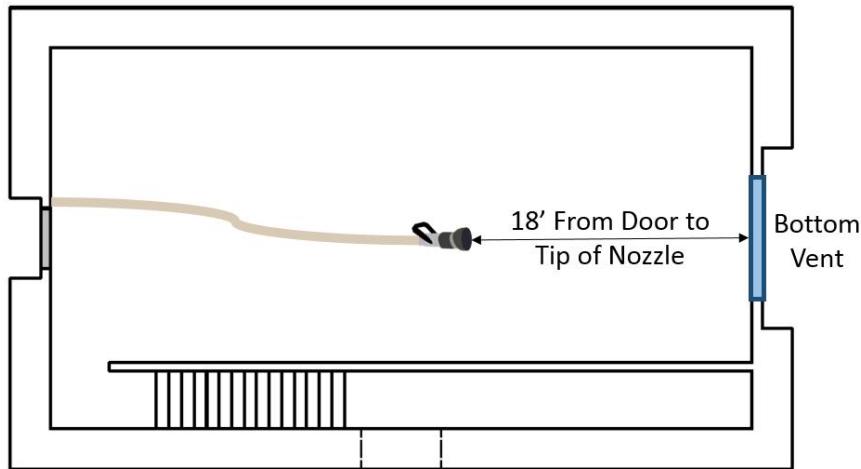


Figure 4.12: First Floor Ventilation Configuration Interior

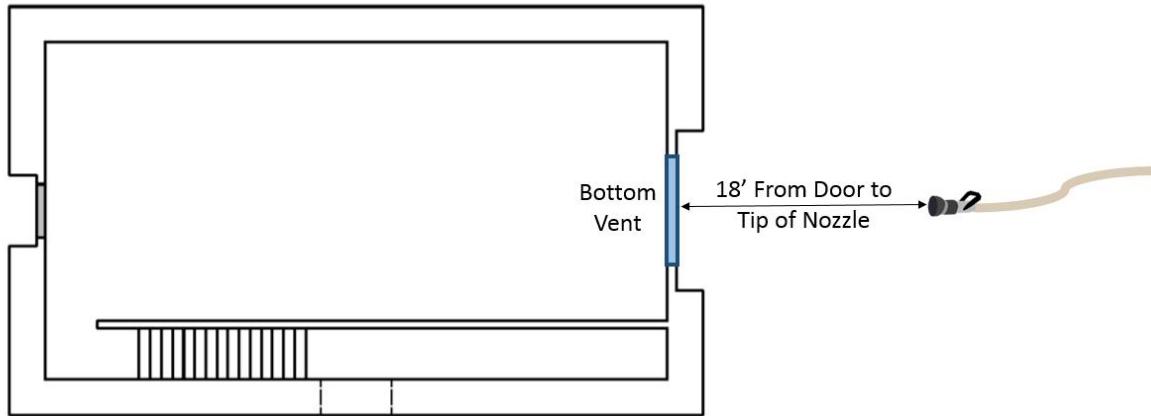


Figure 4.13: First Floor Ventilation Configuration Exterior

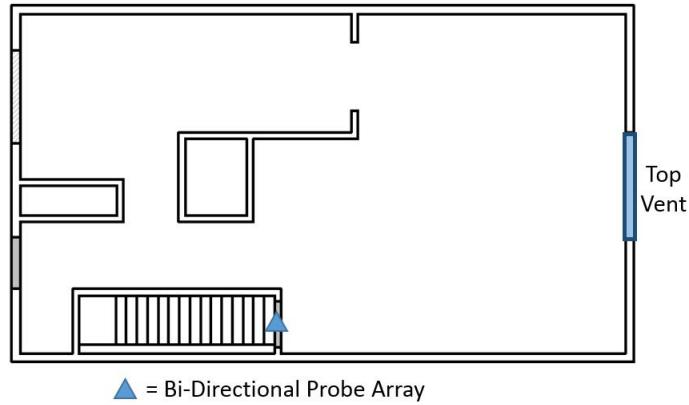


Figure 4.14: Second Floor Ventilation Configuration

In order to evaluate how ventilation openings affect the air entrainment due to hose streams, different ventilation openings were considered to include both doors as well as windows of common sizes. The measurement location within the structure was a fixed location and fixed opening size. The measurement location was the size of a common single doorway as seen below. The remainder of the ventilation openings varied between a single and double door as well as a single and double window. Additionally, a controlled door was evaluated to show the impact of a reduced inlet size on the total air entrainment in hose streams. This is a common practice among fire departments based on previous research conducted showing the benefits to closing down the flow path and limiting the available oxygen to the fire. The effect of the controlled door on air entrainment has yet been analyzed and thus was vital to be included in this study.

Table 4.3: Ventilation Opening Sizes

	Width	Height	Width (in)	Height (in)	Area (sq. in.)
Measurement Location	2' 8"	6' 8"	32	80	2560
Single Window	2'	4'	24	48	1152
Double Window	4'	5'	48	60	2880
Single Door	3'	6' 8"	36	80	2880
Double Door	6'	6' 8"	72	80	5760
Controlled Door	8"	6' 8"	8	80	640

Table 4.4: Ventilation Configuration Experiments

Location	Top Vent	Bottom Vent	Nozzle Size	Nozzle Type	Tip Size	Flow Rate	Pressure
Interior	Controlled Door	Single Window	1.5	Combination		150	75
Interior	Double Door	Double Door	1.5	Combination		150	75
Interior	Double Door	Single Door	1.5	Combination		150	75
Interior	Double Door	Single Window	1.5	Combination		150	75
Interior	No Opening	Double Door	1.5	Combination		150	75
Interior	No Opening	Single Door	1.5	Combination		150	75
Interior	No Opening	Single Window	1.5	Combination		150	75
Interior	Single Door	Double Door	1.5	Combination		150	75
Interior	Single Door	Single Door	1.5	Combination		150	75
Interior	Single Door	Double Window	1.5	Combination		150	75
Interior	Single Door	Single Window	1.5	Combination		150	75
Interior	Controlled Door	Single Window	1.5	Smooth Bore	15/16	180	50
Interior	Double Door	Single Window	1.5	Smooth Bore	15/16	180	50
Interior	Single Door	Double Window	1.5	Smooth Bore	15/16	180	50
Interior	Single Door	Single Window	1.5	Smooth Bore	15/16	180	50
Exterior	Double Door	Double Door	1.5	Combination		150	75
Exterior	Double Door	Single Door	1.5	Combination		150	75
Exterior	No Opening	Double Door	1.5	Combination		150	75
Exterior	No Opening	Single Door	1.5	Combination		150	75
Exterior	No Opening	Single Window	1.5	Combination		150	75
Exterior	Single Door	Double Door	1.5	Combination		150	75
Exterior	Single Door	Single Door	1.5	Combination		150	75
Exterior	Single Door	Double Window	1.5	Combination		150	75
Exterior	Single Window	Single Window	1.5	Combination		150	75
Exterior	Single Window	Single Door	1.5	Combination		150	75
Exterior	No Opening	Single Window	1.5	Smooth Bore	15/16	180	50
Exterior	Single Door	Double Window	1.5	Smooth Bore	15/16	180	50
Exterior	Single Door	Single Window	1.5	Smooth Bore	15/16	180	50
Exterior	Single Window	Single Door	2.5	Combination		250	75
Exterior	Single Door	Single Window	2.5	Combination		250	75
Exterior	Single Window	Single Door	2.5	Smooth Bore	1 1/4	320	50
Exterior	Single Door	Single Window	2.5	Smooth Bore	1 1/4	320	50
Exterior	Single Window	Single Door	PM	Combination		500	80
Exterior	Single Door	Single Window	PM	Combination		500	80
Exterior	Single Window	Single Door	PM	Smooth Bore	1 3/8	500	80
Exterior	Single Door	Single Window	PM	Smooth Bore	1 3/8	500	80
Transitional	Single Window	Single Window	1.5	Combination		150	75
Transitional	No Opening	Single Window	1.5	Combination		150	75
Transitional	Single Door	Single Window	1.5	Combination		150	75
Transitional	Single Window	Single Window	1.5	Smooth Bore	15/16	180	50
Transitional	No Opening	Single Window	1.5	Smooth Bore	15/16	180	50
Transitional	Single Door	Single Window	1.5	Smooth Bore	15/16	180	50

4.2.3 Room Configuration

The last test series of the air entrainment experiments involved reconfiguring the first floor of the structure to analyze how compartmentation and varying building geometries affect the end result. The air entrainment from various attacks, both fixed position and advancements, was studied. Additionally, the tests were conducted from both the interior and exterior of the structure. The nozzles utilized during these experiments included both a 1.5 in. combination nozzle and a 1.5 in. smooth bore nozzle with a 15/16 in. tip.

The dimensioned drawing below shows the changes to the first floor of the structure. A wall was constructed to create a room adjacent to the bottom ventilation opening. Attached to the room via a standard 2 ft. 6 in. by 6 ft. 8 in. doorway was a 16 ft. by 4 ft. hallway. This allowed for the team to study entrainment in a structure configuration most comparable to residential single family homes. This setup would best simulate the configuration for a suppression crew advancing down a hallway towards a bedroom including single door entry with a window present in the room.

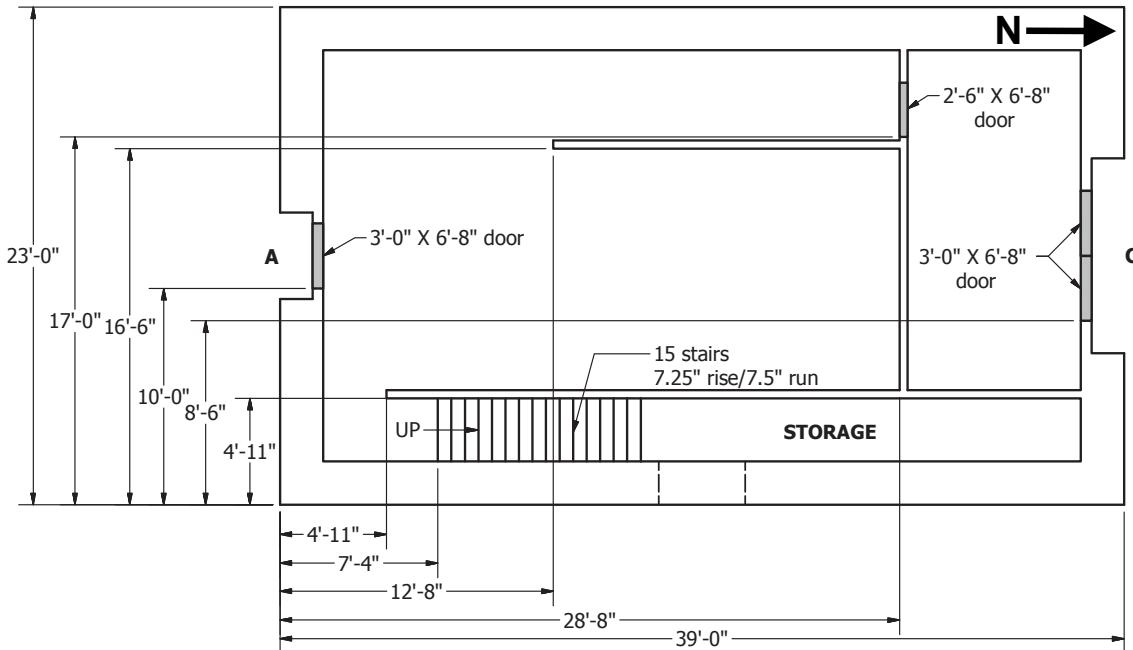


Figure 4.15: First Floor Alterations Room Configuration

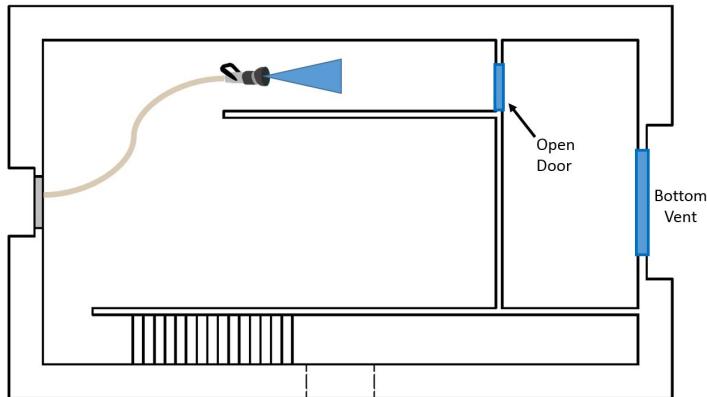


Figure 4.16: First Floor Room Configuration, Interior Experiments

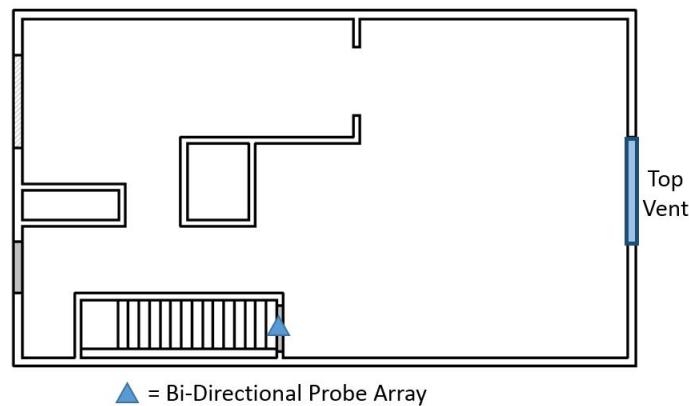


Figure 4.17: Second Floor Room Configuration

Table 4.5: Room Configuration Experiments

Location	Nozzle Size	Nozzle Type	Tip Size	Flow Rate	Pressure
Interior	1.5	Smooth Bore	15/16	180	50
Interior	1.5	Smooth Bore	15/16	180	50
Interior	1.5	Smooth Bore	15/16	180	50
Interior	1.5	Combination		150	50
Interior	1.5	Combination		150	50
Interior	1.5	Combination		150	50
Interior	1.5	Combination		150	75
Exterior	1.5	Combination		150	50

4.3 Analysis & Results

After the air entrainment testing was complete and the results were analyzed, several conclusions were drawn:

- Air entrainment is dependent on hose stream type. (smooth bore, straight stream, fog)
- Air entrainment is dependent on structure size, compartmentation, and ventilation configurations.
- Increases in nozzle movement increase overall air entrainment.
- Different nozzle movement patterns have little effect on overall air entrainment. (O, T, Z, inverted U)
- Air entrainment, either into or out of the structure, is dependent on the horizontal distance of the nozzle to the ventilation opening.

Each of these conclusions is explained in detail below with supporting results.

Manufacturer Comparison The table below shows the series of tests that were conducted to compare similar nozzles from differing manufacturers. Within each of these tests, the air entrainment from various hose stream types was determined.

Table 4.6: Manufacturer Comparison Experiments

Location	Nozzle Size	Manufacturer	Nozzle Type	Tip Size	Flow Rate	Pressure
Interior	1.5	MF3	Combination		95	100
Interior	1.5	MF3	Combination		150	50
Interior	1.5	MF3	Combination		150	75
Interior	1.5	MF3	Combination		150	100
Interior	1.5	MF3	Smooth Bore	7/8	150	50
Interior	1.5	MF3	Smooth Bore	15/16	180	50
Interior	1.5	MF3	Smooth Bore	1	210	50
Interior	1.5	MF2	Combination		95	100
Interior	1.5	MF2	Combination		150	50
Interior	1.5	MF2	Combination		150	75
Interior	1.5	MF2	Combination		150	100
Interior	1.5	MF2	Smooth Bore	7/8	150	50
Interior	1.5	MF2	Smooth Bore	15/16	180	50
Interior	1.5	MF2	Smooth Bore	1	210	50
Interior	1.5	MF1	Combination		95	100
Interior	1.5	MF1	Combination		150	50
Interior	1.5	MF1	Combination		150	75
Interior	1.5	MF1	Combination		150	100
Interior	1.5	MF1	Smooth Bore	7/8	150	50
Interior	1.5	MF1	Smooth Bore	15/16	180	50
Interior	1.5	MF1	Smooth Bore	1	210	50

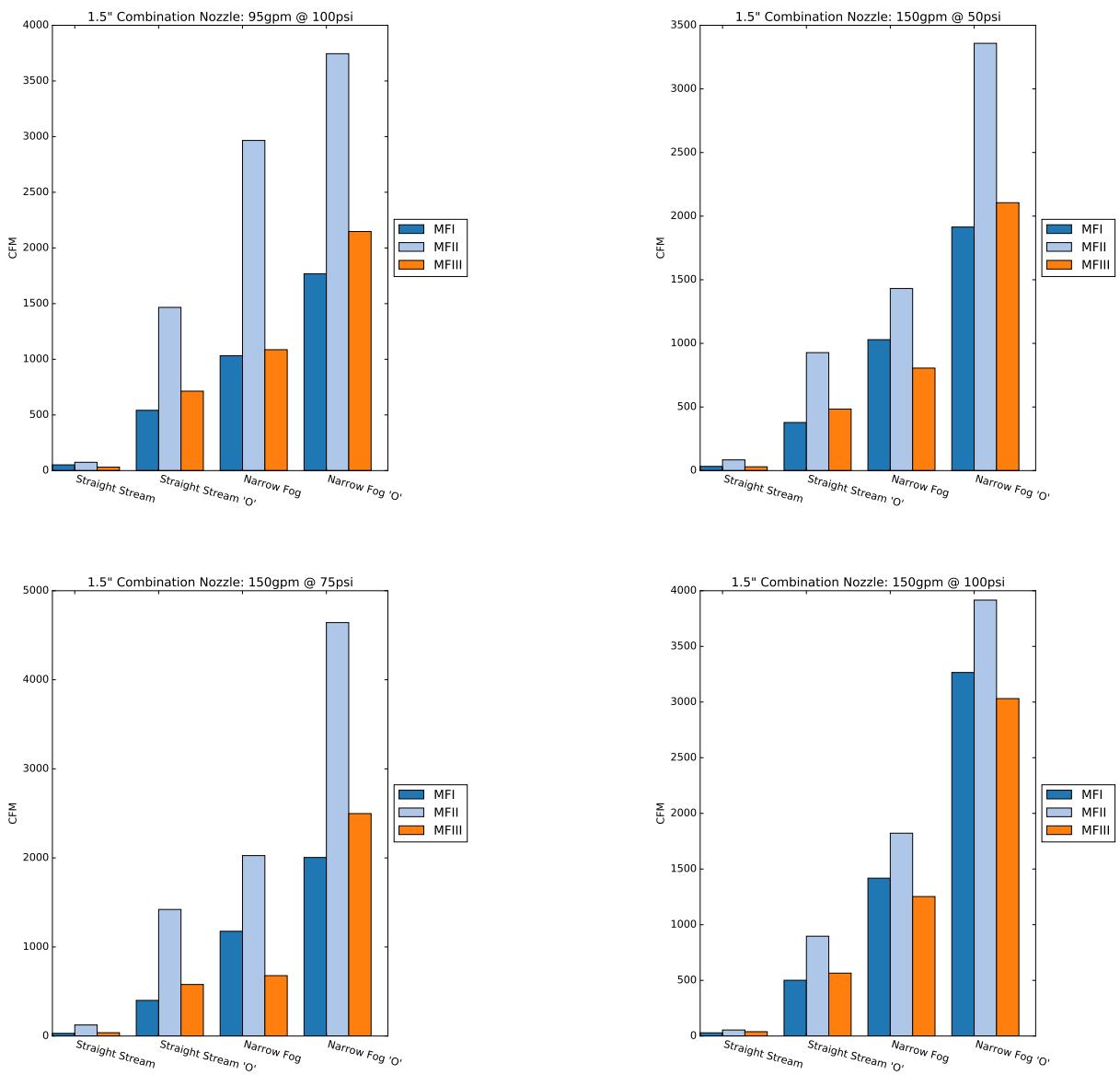


Figure 4.18: Figures showing manufacturer comparison of air entrainment results for 1.5 in combination nozzles.

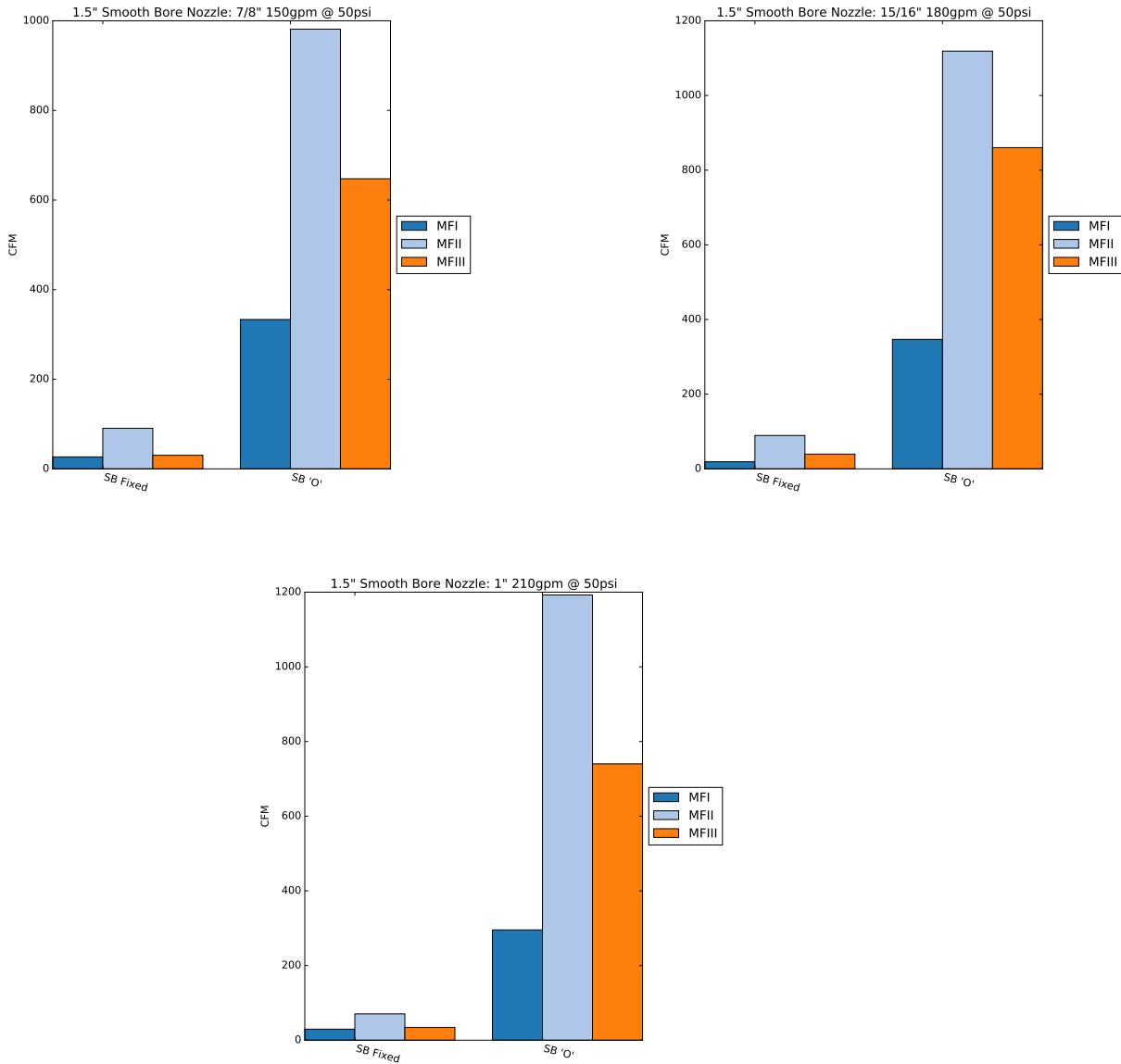


Figure 4.19: Figures showing manufacturer comparison of air entrainment results for 1.5 in smooth bore nozzles.

As shown by the results for both the 1.5 in. combination and smooth bore nozzles examined, manufacturers have different design details for their given product and that is evident in the differing air entrainment results. The spread amongst manufacturers in the combination nozzle varies anywhere from less than 1000 CFM to over 2000 CFM. Due to the more simple design features of the smooth bore nozzles, the differences across manufacturers was less.

With that being said, several trends were consistent amongst the different experiments:

- Increases in nozzle movement (i.e. fixed compared to 'O' pattern) increase overall air entrainment.
- The wider the hose stream pattern, the larger the amount of air entrained. (i.e. narrow fog when compared to straight stream or smooth bore)

Air entrainment is dependent on hose stream type. (smooth bore, straight stream, fog)

The initial opening occlusion test was conducted to determine how varying the hose stream type from a single nozzle can effect the air entrainment at a given setback distance (3 ft.). This test showed that given a fixed setback distance, a combination nozzle flowing a common flow rate of 150 gpm at a pressure of 50 psi had increasing air entrainment with an increase in the width of the pattern. As the pattern became wider, approaching the size of the ventilation opening, the air entrainment increased, with straight stream experiencing the smallest airflow.

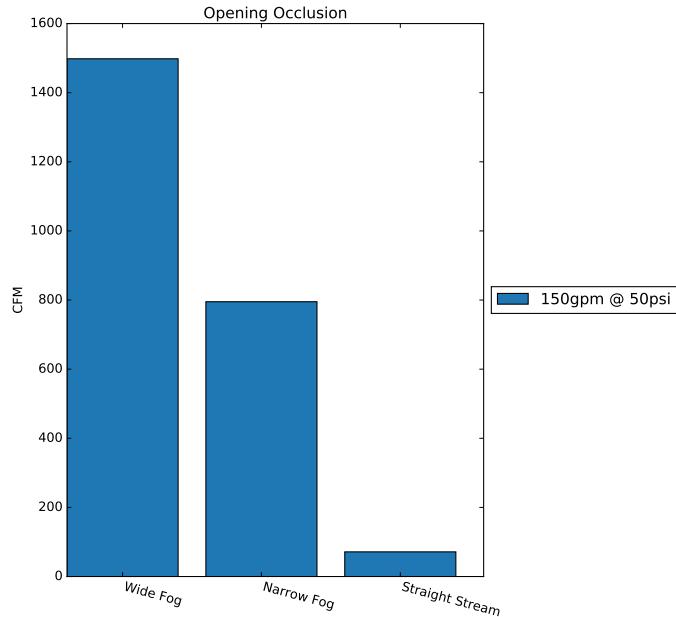


Figure 4.20: Varying air entrainment in varying hose stream types utilizing a 1.5" combination nozzle with a flow rate of 150gpm at 50 psi.

Varying the hose stream type was analyzed in various other experiments as well. These were conducted with an interior fixed setback distance of 18 ft. and utilized 1.5" nozzles.

Table 4.7: Hose stream type comparison for interior 1.5" nozzles.

Hose Stream Type	Flow Rate (GPM)	Pressure (PSI)	Air Entrainment (CFM)
Straight Stream	150	50	3440
Straight Stream 'O'	150	50	10441
Narrow Fog	150	50	17645
Narrow Fog 'O'	150	50	22873
Smooth Bore	150	50	3319
Smooth Bore 'O'	150	50	9738

Air entrainment is dependent on structure size, compartmentation, and ventilation configurations.

The first set of experiments in which the ventilation openings were examined utilized a 1.5 in. combination (150 gpm @ 75 psi) nozzle and a smooth bore nozzle (15/16" tip, 180 gpm @ 50 psi). Four different intake openings were examined including no door, controlled door, single door, and double door. These were looking at scenarios in which a fire attack crew makes entry into the structure via a doorway and is flowing water towards an exhaust of varying size and shape. A window was not examined as one of the intake openings as the assumption was made that the attack crew would be entering the building through a door and not a window. The distance from the nozzle to the opening was 18 ft.

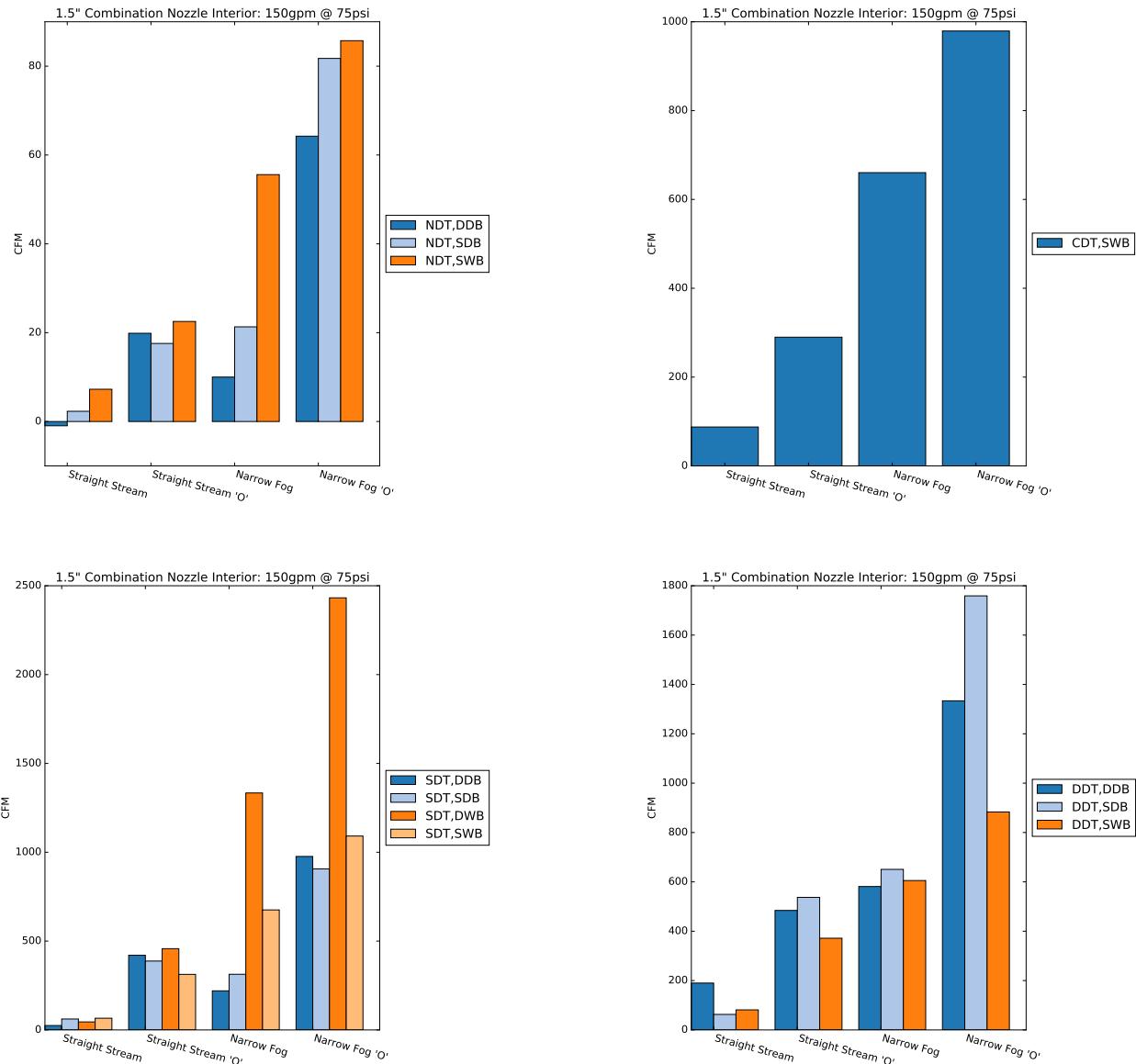


Figure 4.21: Figures showing interior air entrainment results for 1.5" combination nozzles with fixed intake openings and varying exhaust openings.

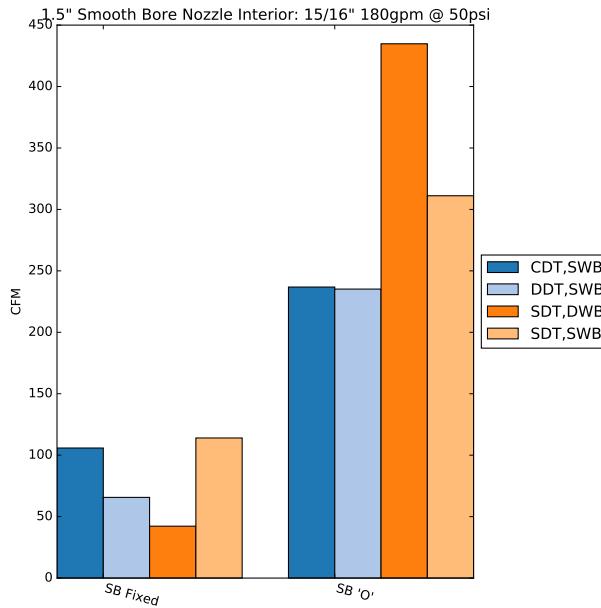


Figure 4.22: Figures showing interior air entrainment results for 1.5" smooth bore nozzles with fixed intake openings and varying exhaust openings.

Several conclusions can be drawn from the first set of ventilation experiments looking at interior attacks:

- As the size of the intake opening increases, so does the amount of air entrained into the hose stream.
- Controlling the door after entry by the fire attack team significantly reduces the amount of air entrainment.
- Something about exhaust vent sizes

The next set of experiments utilized the same nozzles as the interior attack tests above; however these examined the differences in air entrainment from exterior streams. These tests incorporated fixed exhaust openings and varied intake shapes and sizes. The distance from the nozzle to the opening was 18 ft.

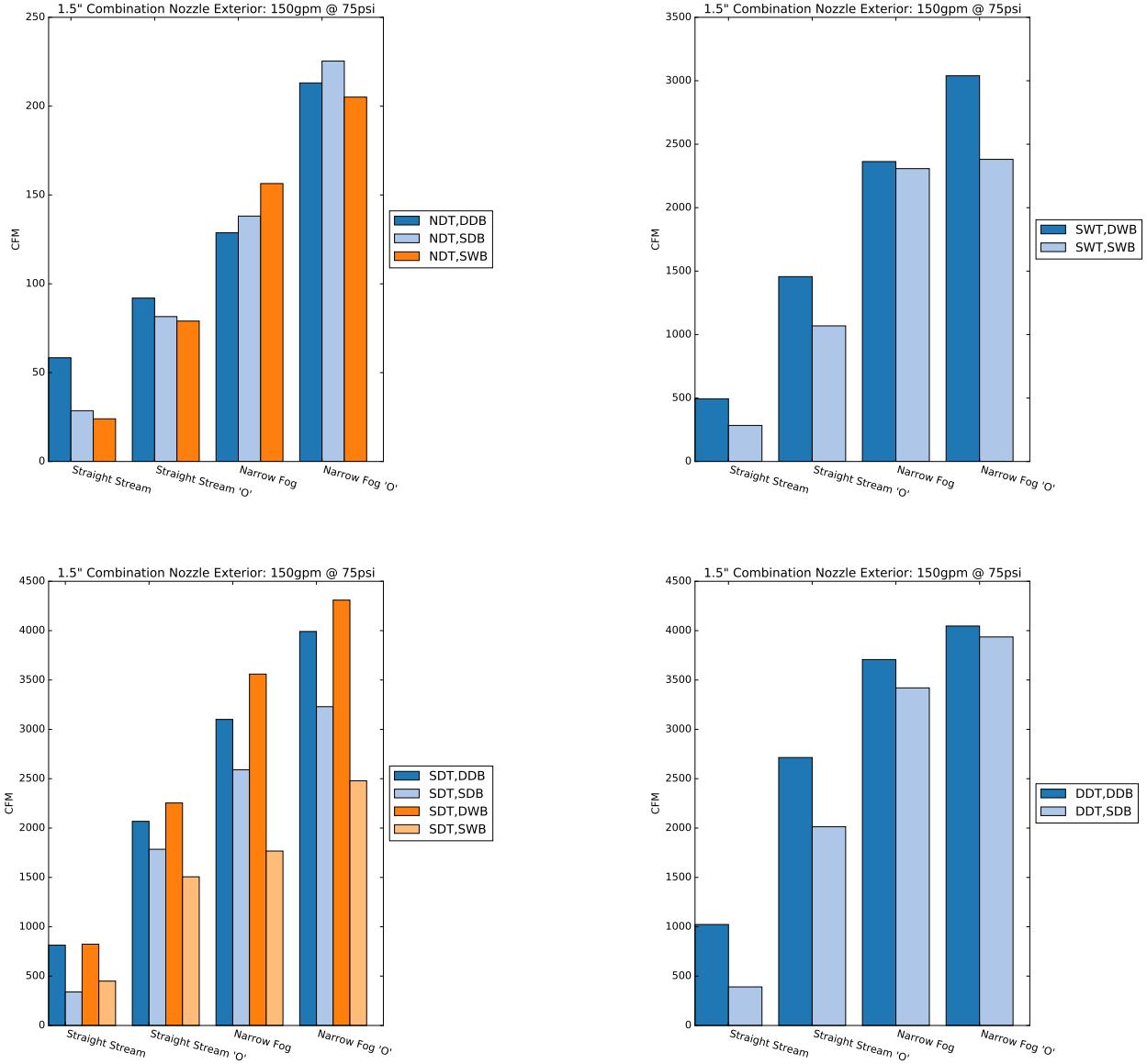


Figure 4.23: Figures showing exterior air entrainment results for 1.5" combination nozzles with fixed exhaust openings and varying intake openings.

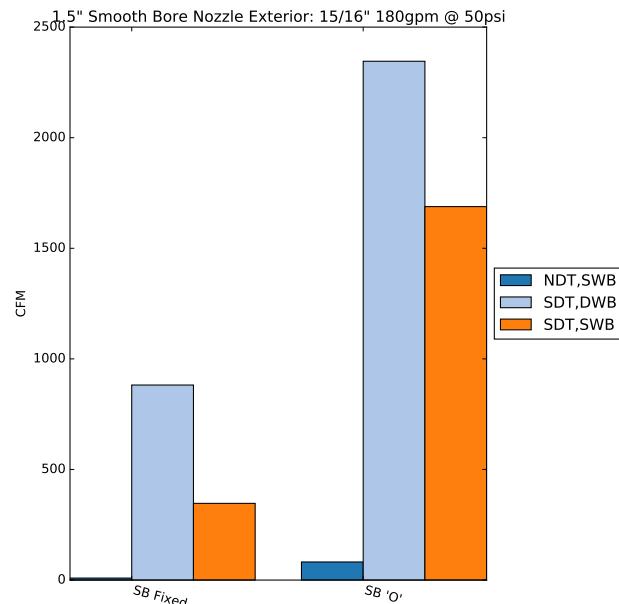


Figure 4.24: Figures showing exterior air entrainment results for 1.5" smooth bore nozzles with fixed exhaust openings and varying intake openings.

Several conclusions can be drawn from the second set of ventilation experiments looking at exterior attacks:

- The amount of air entrained into the hose stream and moved throughout the structure is dependent on the size of the available exhaust opening.
- The larger the intake opening, the more air available to be entrained into the hose stream.

The following experiments looked at the scenario in which a crew would be much closer to the ventilation opening, utilizing exterior streams in what is known as a transitional attack. The fire attack crew would be located on the exterior of the structure, flowing water into the building via a single window. The distance from the nozzle to the opening was less than 3 ft.

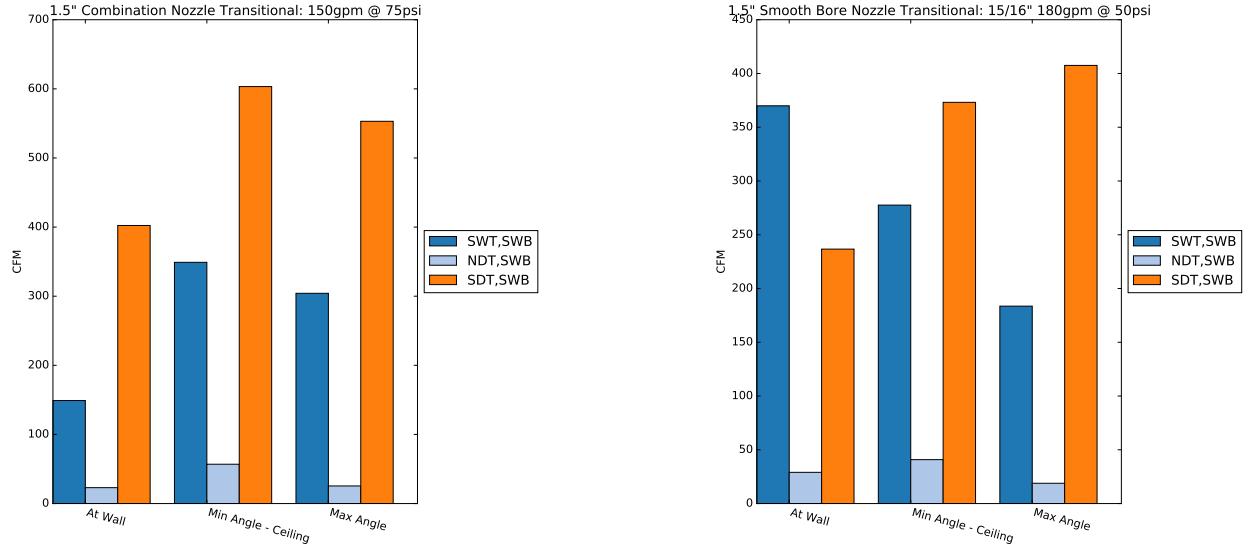


Figure 4.25: Figures showing transitional air entrainment results for 1.5" nozzles with fixed intake openings and varying exhaust openings.

Several conclusions can be drawn from this set of ventilation experiments looking at transitional attacks:

- The amount of air entrained into the hose stream and moved throughout the structure is dependent on the size of the available exhaust opening.
- The larger the exhaust opening, the more air available to be entrained into the hose stream.

Several tests were conducted with hose lines of 2.5 in. diameter in which 2.5 in. nozzles were examined as well as portable monitors.

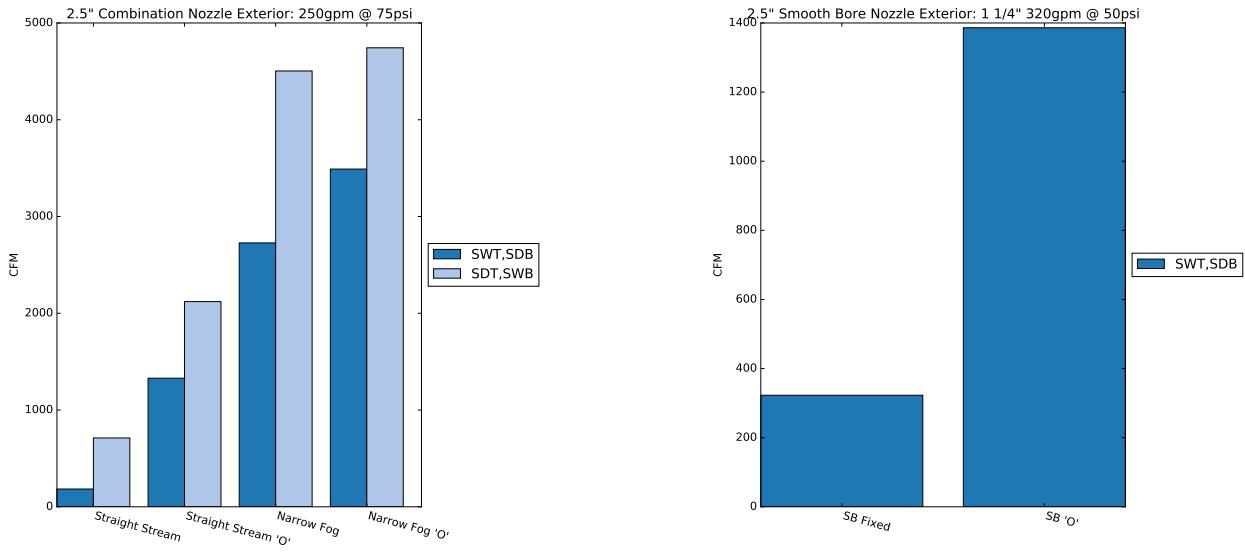


Figure 4.26: Figures showing air entrainment results for 2.5" nozzles with varying exhaust and intake openings.

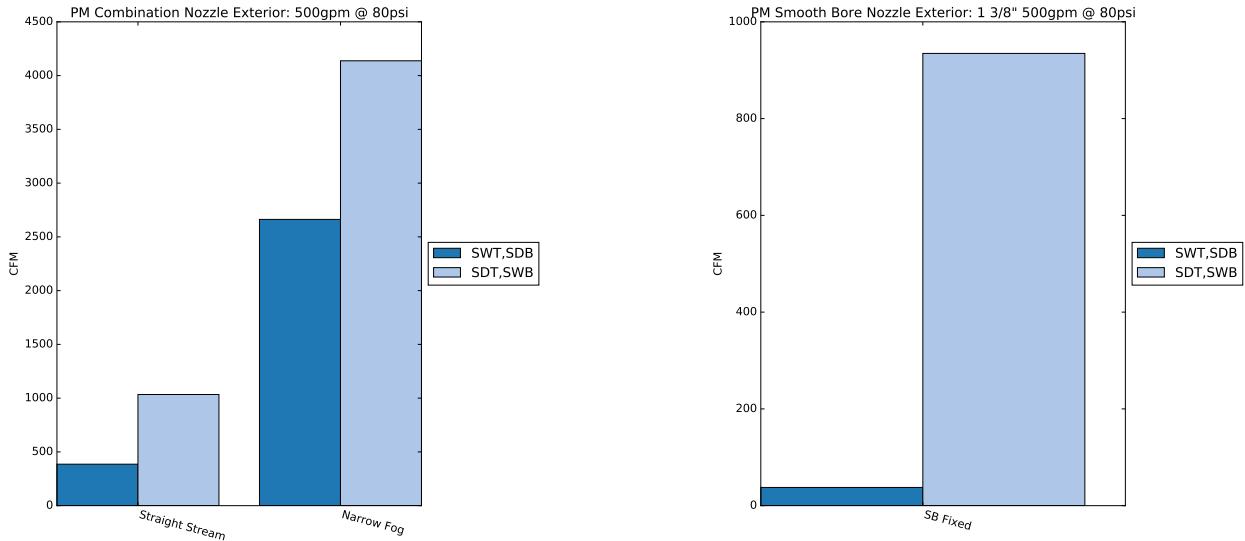


Figure 4.27: Figures showing air entrainment results for portable monitor nozzles with varying exhaust and intake openings.

Increases in nozzle movement increase overall air entrainment A single test was conducted to determine the differences in air entrainment when a given 1.5 in. smooth bore nozzle of fixed flow rate of 210 gpm and pressure of 50 psi was utilized with a ‘O’ pattern at different rotation speeds. Using a metronome, the ‘O’ pattern was applied at 50, 100, and 150 revolutions per minute. This test was conducted at the fixed interior setback distance of 18 ft. from the tip of the nozzle to the ventilation opening.

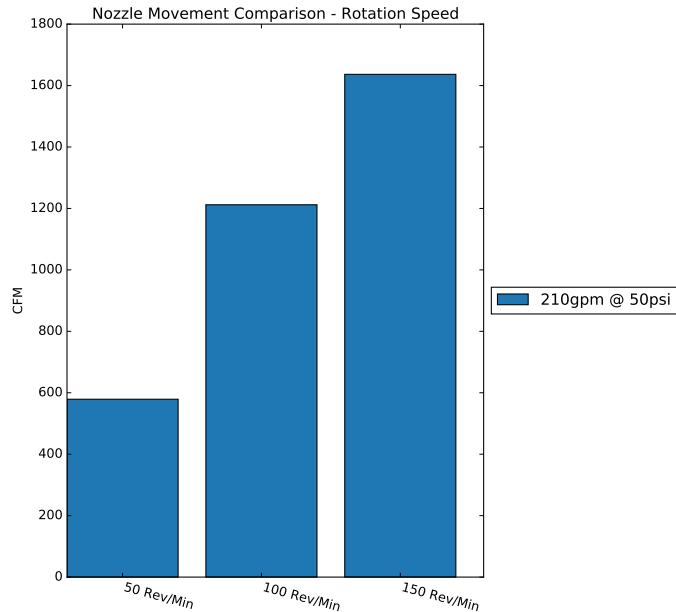


Figure 4.28: Figure showing various rotation speeds of an ‘O’ pattern for an interior 1.5” smooth bore nozzle with a 1” tip.

As shown in the figure above, an increase in the rotation speed while applying a specified pattern yeilded an increase in the air entrainment seen within the stream.

Additionally, in various other experiments, both fixed and moving patterns were examined. The results confirm that an increase in movement, increase entrainment. The figure below shows that a narrow fog 'O' pattern yields higher entrainment than a fixed narrow fog patter and a straight stream 'O' pattern yields higher entrainment than a fixed straight stream pattern.

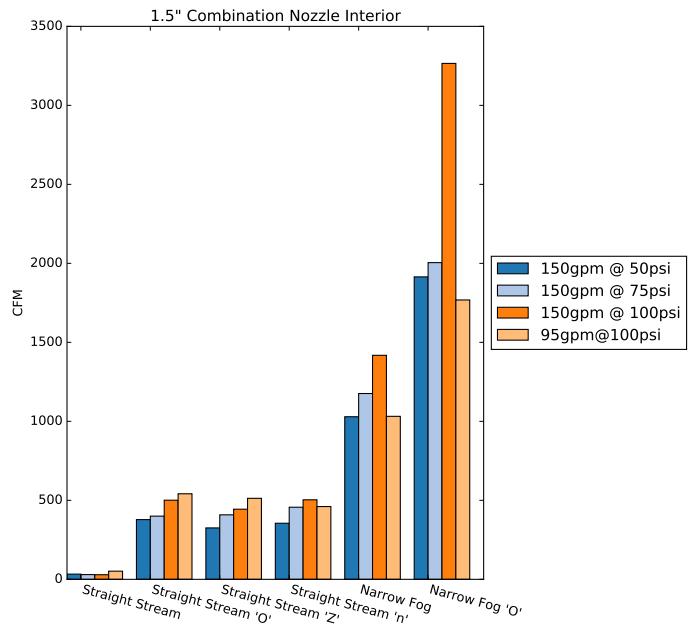


Figure 4.29: Figure showing entrainment results of interior 1.5" combination nozzles.

Differing nozzle movement patterns have little effect on overall air entrainment.

Various tests were conducted to determine how different nozzle movements effect the overall air entrainment. Common nozzle movements seen in the fire service today are the 'O', 'Z', and 'n' patterns. Differences in these were examined utilizing nozzles of various flow rates and pressures for both 1.5 in. combination as well as 1.5 in. smooth bore nozzles from the interior of the structure at a fixed setback distance of 18 ft. The results show that there is less than a +/- 1000 CFM difference between the patterns across the various nozzle types and settings.

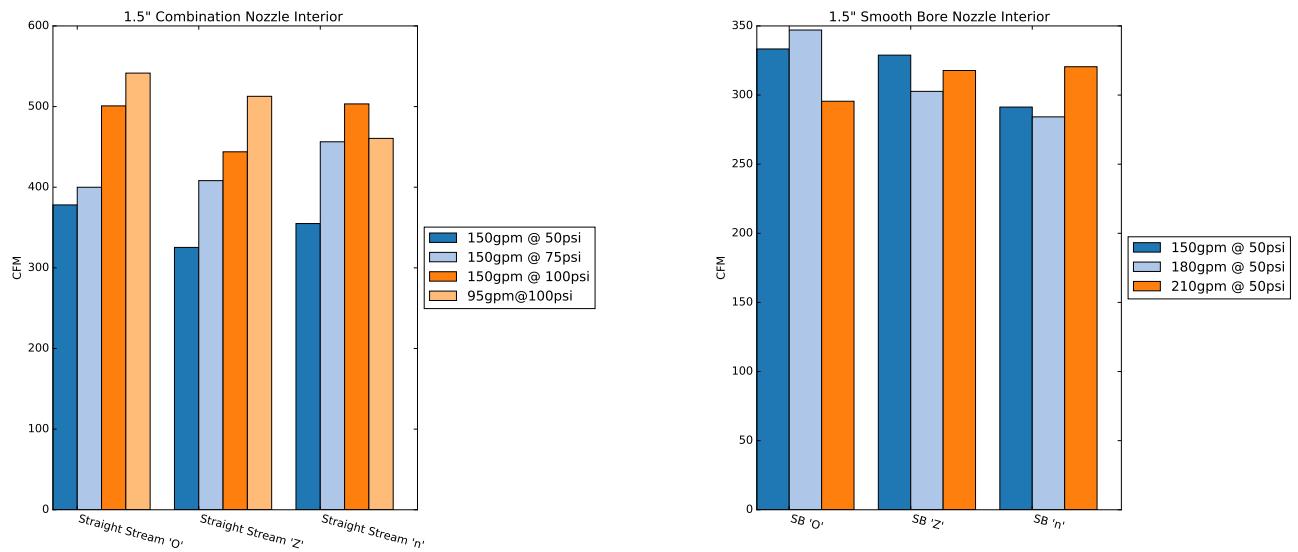


Figure 4.30: Figures showing air entrainment given various nozzle movements for interior 1.5" nozzles.

A test was also conducted to determine if a standard utilized nozzle movement in an ‘O’ pattern would differ from a ‘Spray and Pray’ technique in which the nozzle operator moves the hose stream across the ventilation opening as fast as possible with no discernible pattern. Once again, the results showed little to no difference in the air entrainment.

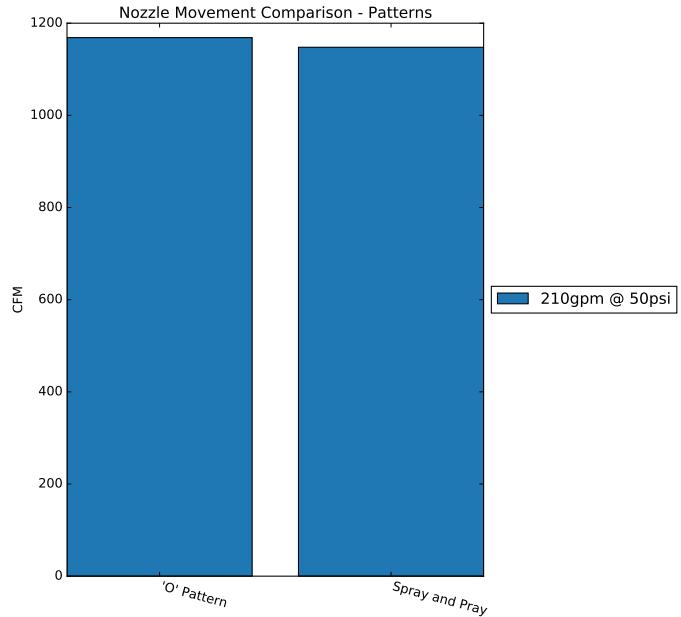


Figure 4.31: Figure showing common pattern compared to no discernible pattern for an interior 1.5” smooth bore nozzle with a 1” tip.

Because the results very clearly showed little to no difference in air entrainment from varying nozzle movements across multiple nozzle types and settings, a single nozzle movement pattern ('O') was utilized for the remainder of the experiments conducted.

Air entrainment is dependent on the distance of the nozzle to the ventilation opening.

One of the preliminary experiments conducted was the setback comparison tests in which a 1.5 in. combination nozzle at two different pressures (100 psi and 50 psi) was utilized in a fixed pattern at varying distances from the ventilation opening. The nozzle was moved back from the opening at intervals 3, 6, 9, 12, and 15 ft. to see the effect on air entrainment in the hose stream.

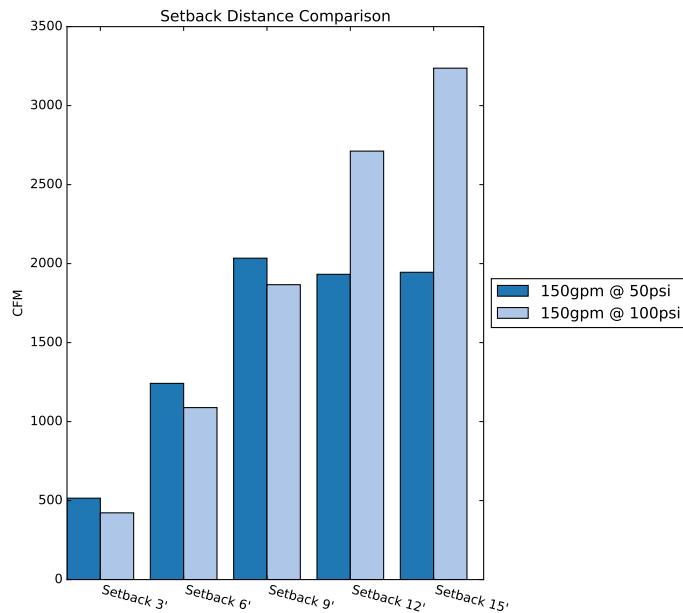


Figure 4.32: 1.5" Combination Nozzle, Setback Distance Comparison

With a fixed nozzle movement, the tests showed that increasing the distance between the tip of the nozzle and the ventilation opening increased the entrainment in the hose stream. The further the nozzle from the vent allowed for a more broken and ‘wider’ stream, which in turn, encompassed more of the opening.

5 Water Distribution Experiments

The goal of the water distribution experiments was to quantify the impact that changing a nozzle, changing flow pressure, or changing flow position had on water dispersion within a compartment. Eighty-eight water flow tests were conducted at the UL Headquarters in Northbrook, IL in a purpose built compartment with an attached hallway and movable staircase. Water flow patterns were determined by collecting the water in 48 discrete collection bins. A detailed description of the water collection is in Section 5.1.2.

5.1 Experimental Configuration

5.1.1 Test Apparatus

The main portion of test compartment had interior (finished) dimensions of 14 ft 8 in. by 10 ft 5 in with an 8 ft ceiling. To account for water collection apparatus the entire compartment was 7 ft 11 in above the floor of the lab floor (see Figure 5.1). The overall size of the compartment was designed to reflect that of one found in a typical resident structure but was also bound by the dimensions of the water collection apparatus (Section 5.1.2). The compartment was wood frame construction with 2 in. by 4 in. studs and track set to 16 in. centers with a interior height measuring 8 ft 1 1/8 in. rough. The walls and ceiling were lined with 1/2 in. durarock cement board atop 1/2 in. plywood. The ceiling joists were 2 in. by 6 in. set to 16 in. on center.



Figure 5.1: Water Distribution Test Structure and ADD Apparatus

The compartment featured two ventilation openings, one doorway measuring 3 ft by 6 ft 8 in. which opened to the interior hallway, and one window measuring 2 ft by 4 ft which opened to the exterior of the compartment. A movable staircase and landing was constructed to provide access to either the interior hallway of the compartment or provide a simulation of a first floor exterior attack. The hallway was 6 ft by 8 ft and the stairway landing was 4 ft by 6 ft 8 in. Detailed dimension drawings of the compartment are included in Figures 5.2 and 5.3

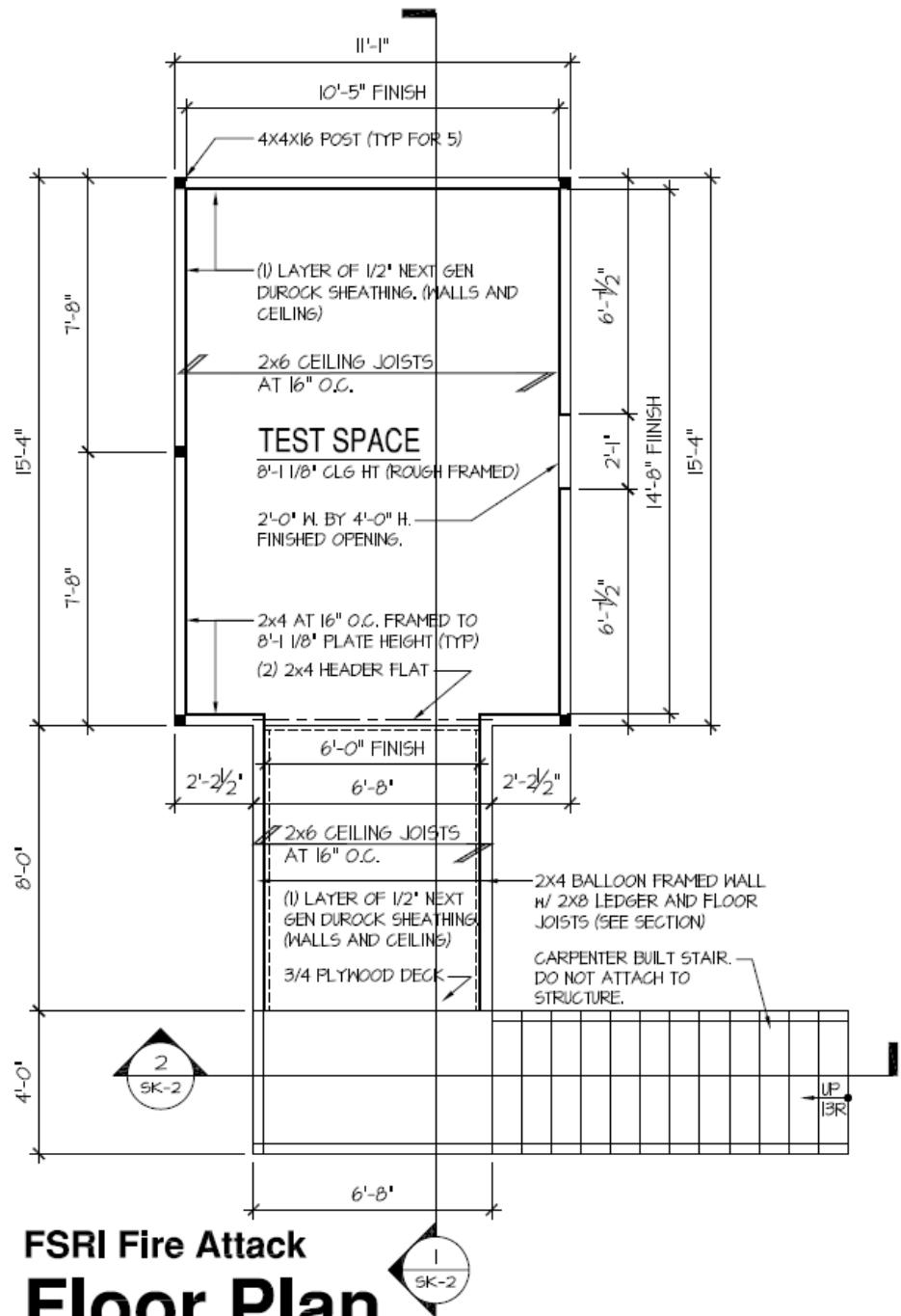
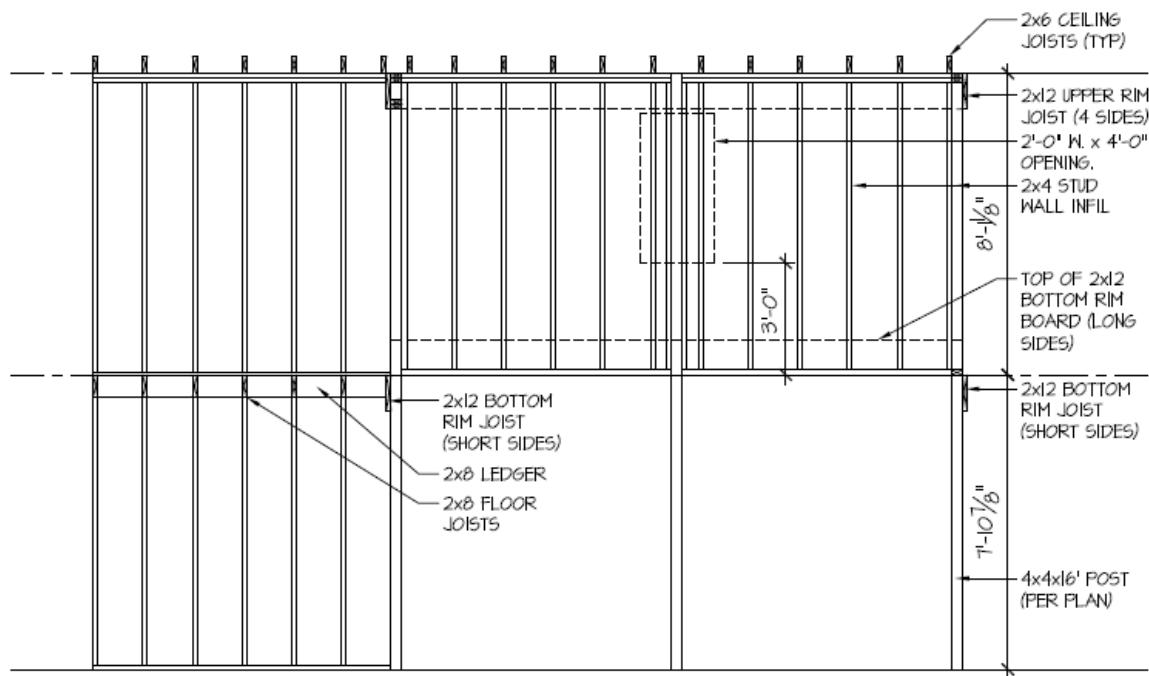
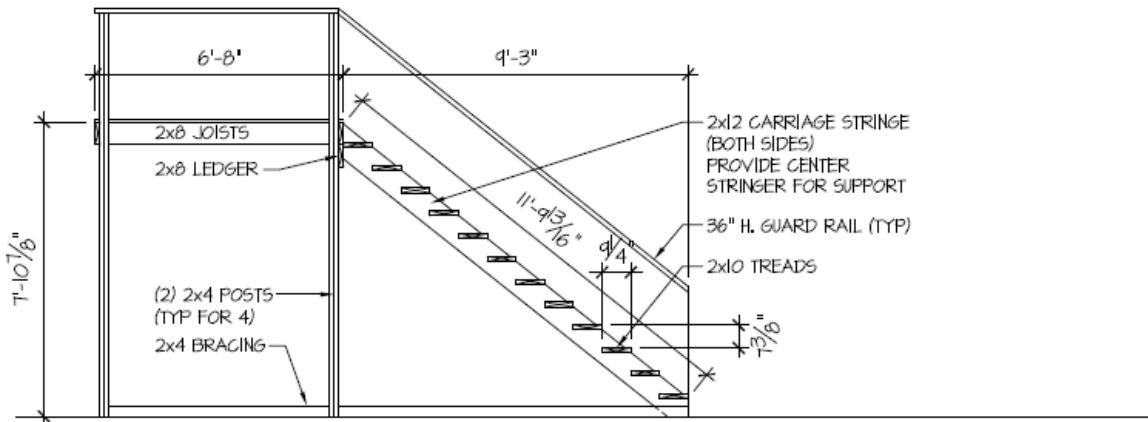


Figure 5.2: ADD Plan View



Room Section - 1

SCALE: 1/4"=1'-0"



Stair Section - 2

SCALE: 1/4"=1'-0"

Figure 5.3: ADD Section View

A unique feature of this compartment was that there was no floor constructed. The test compartment instead sat directly over 48, 20 in by 20 in stainless steel collection bins. Instead of water accumulating on the floor, it would flow into the distinct collection bins to determine accumulation. Potential gaps between the collection bins were covered by flashing which was folded to divert the water evenly in each bin, to best ensure adequate distribution results. The gaps between the outer collection bins and the walls of the structure were also covered with flashing to ensure all water directed into the structure was collected in the appropriate bins. The interior layout of the floor bins and use of flashing can be seen in Figure 5.4.

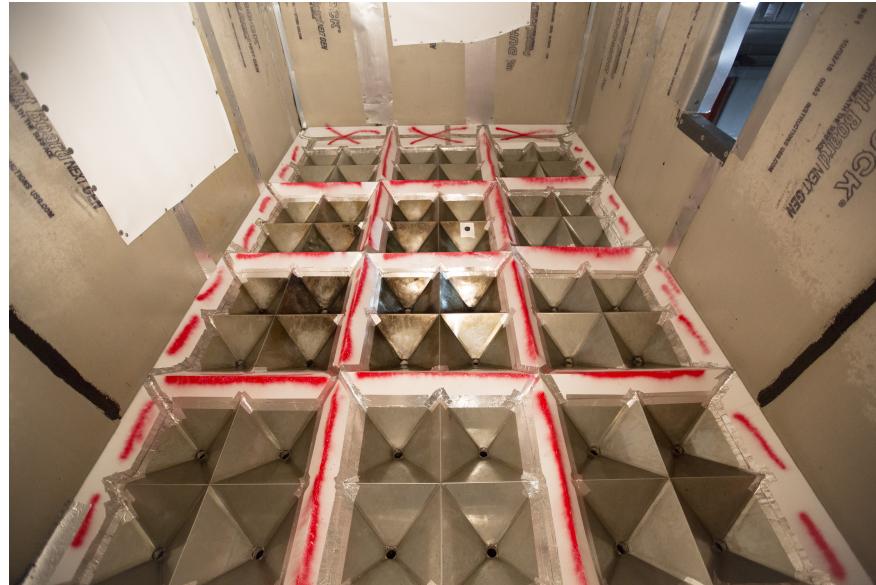


Figure 5.4: Layout of Structure Floor with 48 Collection Bins and Connected Flashing

5.1.2 Instrumentation and Uncertainty

To measure the water distribution throughout the compartment, a fire sprinkler spray density measurement instrument known as the Actual Delivered Density (ADD) apparatus was used. This device was connected to the 48 collection bins that comprised the floor of the test structure. The ADD apparatus is comprised of one main array and two satellite arrays of heavy steel framework. The main array consists of 32 water barrels and water pan collection assemblies while each satellite array contains 8 barrels and collection assemblies (see Figure 5.5). All barrels are of 30-gallon capacity and are connected by a 2 in. diameter hose to a 20 in. by 20 in. inverted square pyramid shaped stainless steel water collection pan above. In total, there are 48 total collection pans/barrels. Differential pressure transducers connect to the bottom of each water collection barrel via flexible tubing. The water level in a given barrel is determined by the head pressure measured by the transducer. The water collection rate is calculated based the change in head pressure over time. As Figure 5.6 shows, collection assemblies were arranged into 2×2 arrays. Each collection barrel is uniquely numbered so that water flow data can be mapped to specific position. The barrels are connected to a pneumatic drain valve which could be actuated to drain each barrel at the conclusion of an experiment.

Prior to testing, data was collected to estimate the uncertainty associated with the water distribution measurements performed using the ADD apparatus. Each water collection assembly was filled to capacity while recording pressure transducer measurements as well as data from a calibrated turbine flowmeter (with less than 1 % measurement uncertainty). Although the design of each water collection assembly is the same, the measurement performance across the entire apparatus varied. Overall, the 48 water collection assemblies reported an average accuracy of ± 2.4 gallons. This represents an uncertainty in total volume of ± 8 % at full scale (30 gal).



(a) Collection Barrels

(b) Collection Pans

Figure 5.5: ADD Collection Assembly

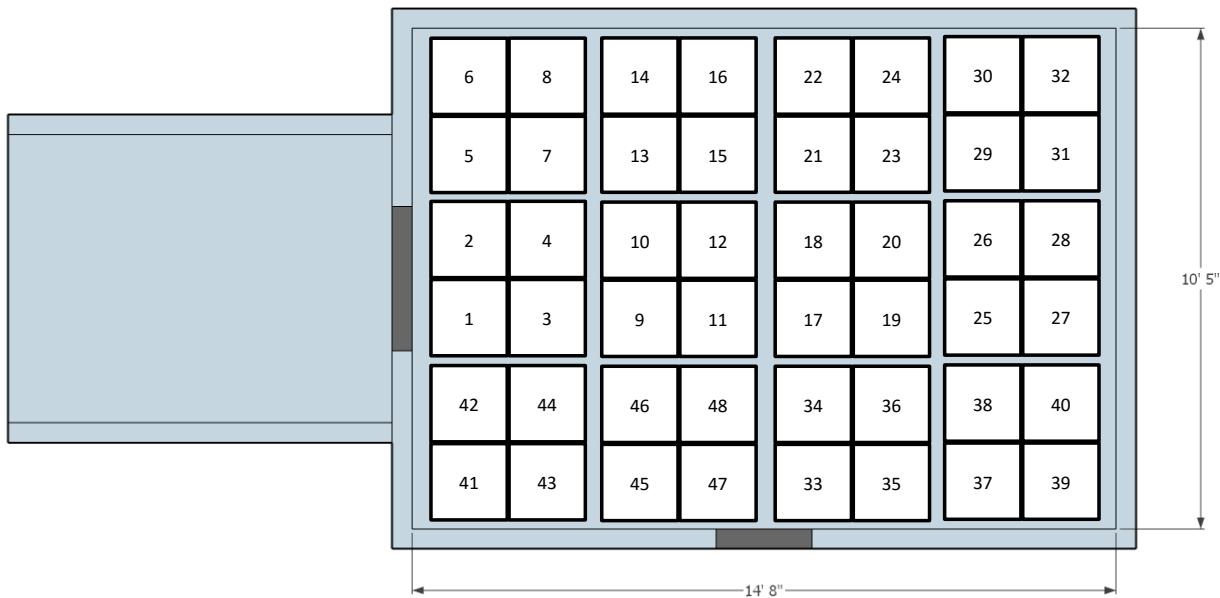


Figure 5.6: Bin Numbers and Locations

5.1.3 Experimental Equipment

To ensure the data collected were applicable to the majority of the fire service, a representative set of nozzles types, specified flows/pressures, and hose sizes were used. These test variables are similar to those discussed in the air entrainment experiments and are shown in Table 5.1.

5.2 Experiments Conducted

The water distribution experiments consisted of 88 tests that incorporated both interior and exterior fire attack utilizing the various nozzles and flow configurations. In each test, water flowed for approximately 1 min. in duration. The duration was dictated by the size of the collection barrels in the ADD apparatus. Each collection barrel was a total of 30 gallons. If a barrel overflowed, there would be an inability to

Table 5.1: Details of Nozzles Used

Line Size	Nozzle Type	Tip (in)	Nozzle Pressure (psi)	Approximate Flow Rate (gpm)
1 3/4 in.	Smooth Bore	1	50	210
	Smooth Bore	15/16	50	180
	Smooth Bore	7/8	50	150
	Combination		100	100
	Combination		100	150
	Combination		75	150
	Combination		50	150
2 1/2 in.	Smooth Bore	1 1/8	50	260
	Smooth Bore	1 1/4	50	320
	Combination		100	250
	Combination		75	250
	Combination		50	250

determine the correct distribution of water flow. At the start of each test, there was an initial amount of water in the bottom of the barrel to ensure the sensors were able to record the water received during the testing. The total water in each barrel was determined by subtracting the initial water volume in each barrel from the final value.

5.2.1 Interior Tests

The interior tests were designed to simulate a fire on the same floor as the attack crew. Suppression operations were conducted from the doorway adjoining the hallway to the test compartment. At this location, hose stream time, nozzle direction and spray pattern were varied and the water distribution within the compartment was measured. The four nozzle directions, max angle, mid ceiling, minimum angle ceiling, and at wall are shown in Figure 5.7. The max angle position was defined to be the steepest angle the nozzle could be without the stream being impacted by the soffit of the doorway. The mid ceiling position set the stream to hit the middle of the ceiling along the 14 ft 8 in. dimension. The minimum ceiling angle was defined to be the smallest angle the nozzle could be set such that the stream still completely hit the ceiling. The fourth position, the wall position, was defined to have the stream hit the vertical midpoint of the wall adjacent to the doorway. Table 5.2 lists the interior tests conducted.

Table 5.2: Interior Fire Attack Distribution Experiments

Hose Stream Type	Nozzle Direction	Nozzle Movement	Nozzle Pressure (psi)	Flow Rate (gpm)
Straight Stream	Max Angle	O	100	150
Straight Stream	Max Angle	Fixed	100	150
Straight Stream	Mid Ceiling	Fixed	100	125
Straight Stream	Mid Ceiling	O	100	125
Straight Stream	Mid Ceiling	Z	100	125
Straight Stream	Mid Ceiling	T	100	125
Straight Stream	Mid Ceiling	Inverted U	100	125
Straight Stream	Mid Ceiling	Fixed	100	150
Straight Stream	Mid Ceiling	O	100	150
Straight Stream	Mid Ceiling	Fixed	75	150
Straight Stream	Mid Ceiling	O	75	150
Straight Stream	Mid Ceiling	Fixed	50	150
Straight Stream	Mid Ceiling	O	50	150
Straight Stream	At Wall	Fixed	100	150
Straight Stream	At Wall	O	100	150
Fog	Mid Ceiling	Fixed	100	125
Fog	Mid Ceiling	Fixed	100	150
Fog	Mid Ceiling	O	100	150
Fog	Mid Ceiling	Fixed	75	150
Fog	Mid Ceiling	O	75	150
Fog	Mid Ceiling	Fixed	50	150
Fog	Mid Ceiling	O	50	150
Fog	Mid Ceiling	O	100	125
15/16 Smooth Bore	Max Angle	Fixed	50	180
15/16 Smooth Bore	Max Angle	O	50	180
15/16 Smooth Bore	At Wall	Fixed	50	180
15/16 Smooth Bore	At Wall	O	50	180
15/16 Smooth Bore	Mid Ceiling	Fixed	50	180
15/16 Smooth Bore	Mid Ceiling	O	50	180

Interior Attack

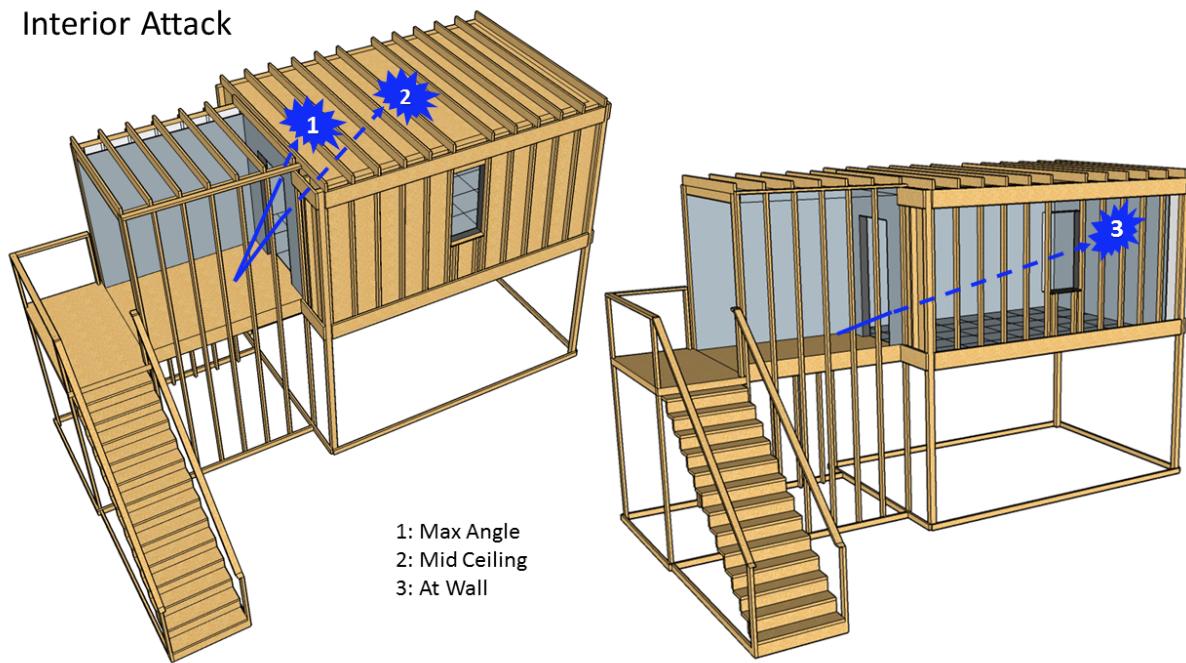


Figure 5.7: Nozzle Direction, Interior Attack

5.2.2 Exterior Tests

The exterior testing included two attack positions; one attack was from the fire floor and the second was from the floor below the fire. These are referred to as first floor and second floor attacks. The movable staircase allowed for the variation between first floor and second floor suppression through the same window vent. The exterior tests simulated a single room of fire in which an exterior attack was used. Similar to the interior testing, the nozzle type, the nozzle direction and application pattern were varied for comparison. The differences in first floor and second floor attacks can be seen in Figures 5.8 and 5.9.

There are four nozzle positions for the first floor exterior tests: max angle, mid ceiling, min angle ceiling, and min angle wall. The max angle position was defined as the steepest angle the nozzle could be positioned at without the window soffit impacting the hose stream. The mid ceiling position was defined by the hose stream aimed at the center of the compartment in the 10 ft 5 in dimension. The min angle ceiling position is defined by the shallowest angle such the hose stream did not directly contact the wall. The min angle wall is similar to the mid angle ceiling except it was defined as the angle where the hose stream would impact the wall as close to the ceiling without the stream contacting the ceiling directly.

There are five nozzle positions for the second floor exterior tests: max angle, mid ceiling, min angle ceiling, min angle wall, max angle sill. The first four positions were the same as the first floor exterior attack except that the starting position of the nozzle changed to be one story below the window vent. The fifth nozzle position, max angle sill was defined to the angle such that stream was as close to the window sill without the stream being impacted by the sill.

The exterior tests are shown in Table 5.3.

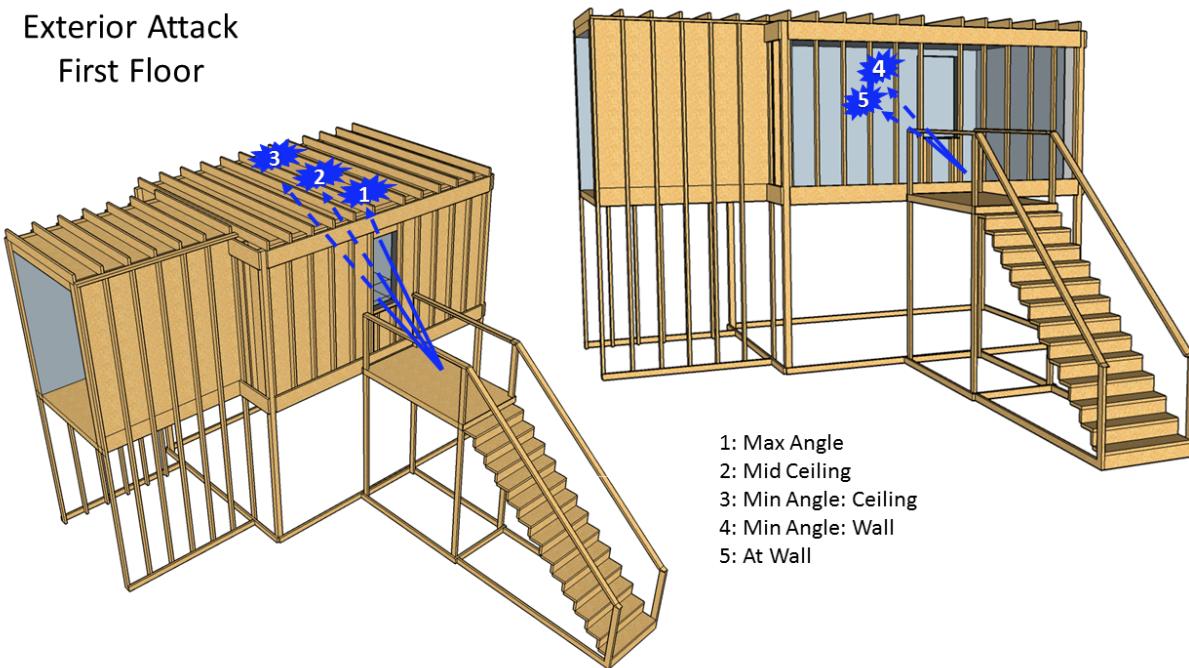


Figure 5.8: Nozzle Direction, Exterior 1st Floor Attack

**Exterior Attack
Second Floor**

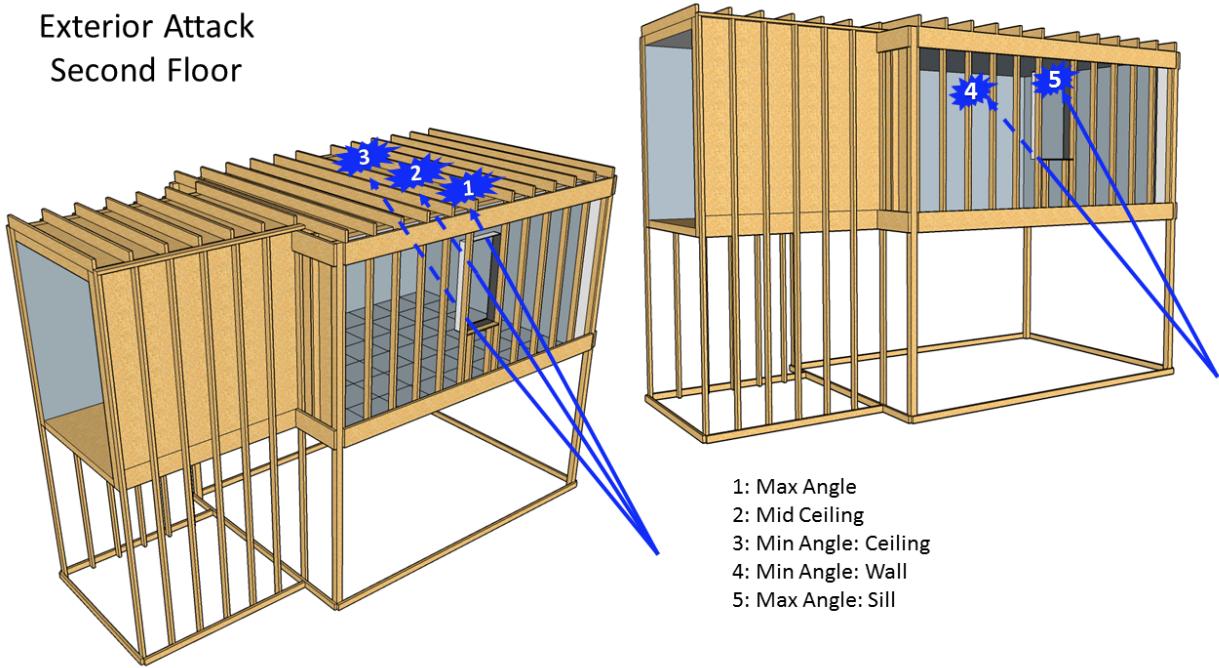


Figure 5.9: Nozzle Direction, Exterior 2nd Floor Attack

Table 5.3: Exterior Fire Attack Distribution Experiments

Floor Position	Hose Stream Type	Nozzle Movement	Nozzle Direction	Nozzle Pressure (psi)	Flow Rate (gpm)
First	Straight Stream	Fixed	Max Angle	100	150
First	Straight Stream	Fixed	Max Angle	100	150
First	Straight Stream	Fixed	Max Angle	100	150
First	Straight Stream	Fixed	Max Angle	100	150
First	Straight Stream	Fixed	Max Angle	100	150
First	Straight Stream	Fixed	Max Angle	100	150
First	Straight Stream	Fixed	Max Angle	50	150
First	Straight Stream	Fixed	Max Angle	75	60
First	Straight Stream	Fixed	Max Angle	50	185
First	Straight Stream	Fixed	Max Angle	25	130
First	Straight Stream	Fixed	Max Angle	100	250
First	Straight Stream	Sweeping	Max Angle	100	150
First	Straight Stream	Wide Sweep	Max Angle	100	150
First	Straight Stream	Fixed	Mid Ceiling	100	150
First	Straight Stream	Fixed	Min Angle: Ceiling	100	150
First	Straight Stream	Fixed	Min Angle:Ceiling	100	250
First	Straight Stream	Fixed	Min Angle: Wall	100	150
First	Straight Stream	Fixed	At Wall	100	150
First	15/16 Smooth Bore	Fixed	Max Angle	50	180
First	15/16 Smooth Bore	Sweeping	Max Angle	50	180
First	15/16 Smooth Bore	Fixed	Max Angle	50	180
First	15/16 Smooth Bore	Fixed	Max Angle	30	150
First	15/16 Smooth Bore	Fixed	Max Angle	15	130
First	15/16 Smooth Bore	Fixed	Max Angle	10	100
First	15/16 Smooth Bore	Fixed	Mid Ceiling	50	180
First	15/16 Smooth Bore	Fixed	Min Angle: Ceiling	50	180
First	15/16 Smooth Bore	Fixed	Min Angle: Wall	50	180
First	15/16 Smooth Bore	Fixed	At Wall	50	180
First	7/8 Smooth Bore	Fixed	Max Angle	50	150
First	1 Smooth Bore	Fixed	Max Angle	50	210
First	1 1/4 Smooth Bore	Fixed	Max Angle	50	260
First	Fog	Fixed	Max Angle	100	150
First	Fog	Comb (SS then Fog O)	Max Angle	100	150
Second	Straight Stream	Fixed	Max Angle	100	150
Second	Straight Stream	Sweeping	Max Angle	100	150
Second	Straight Stream	Wide Sweep	Max Angle	100	150
Second	Straight Stream	Fixed	Mid Ceiling	100	150
Second	Straight Stream	Fixed	Min Angle: Ceiling	100	150
Second	Straight Stream	Fixed	Min Angle: Wall	100	150
Second	Straight Stream	Fixed	Max Angle: Sill	100	150
Second	15/16 Smooth Bore	Fixed	Max Angle	50	180
Second	15/16 Smooth Bore	Sweeping	Max Angle	50	180
Second	15/16 Smooth Bore	Fixed	Mid Ceiling	50	180
Second	15/16 Smooth Bore	Fixed	Min Angle: Ceiling	50	180
Second	15/16 Smooth Bore	Fixed	Min Angle: Wall	50	180
Second	7/8 Smooth Bore	Fixed	Max Angle	50	150
Second	1 Smooth Bore	Fixed	Max Angle	50	210
Second	Fog	Fixed	Max Angle	100	150
Second	Fog	Comb (Fixed then O)	Max Angle	100	150

5.3 Analysis & Results

The intent of the water flow testing was to determine the location of the water within the compartment as a function of several common fire service equipment configurations and application locations. Recall, the location of the water within the compartment was achieved using the ADD device (Section 5.1.2). To ensure that differences between water distributions within the compartment could be quantified, it was important to confirm the repeatability of the experimental setup. Four tests utilizing a straight stream nozzle flowing 150 gpm at 100 psi from the exterior first floor position directed into the structure with a maximum angle were conducted to determine the variance in results. The total water in each of the 48 collection bins for the four replicate tests is shown in Figure 5.10. In the bar chart, bins with less than 8 gal. are colored blue, with more than 8 gal. but less than 16 gal. are colored green, with more than 16 gal. but less than 24 gal. are colored yellow, and bins with more than 24 gal. are colored red.

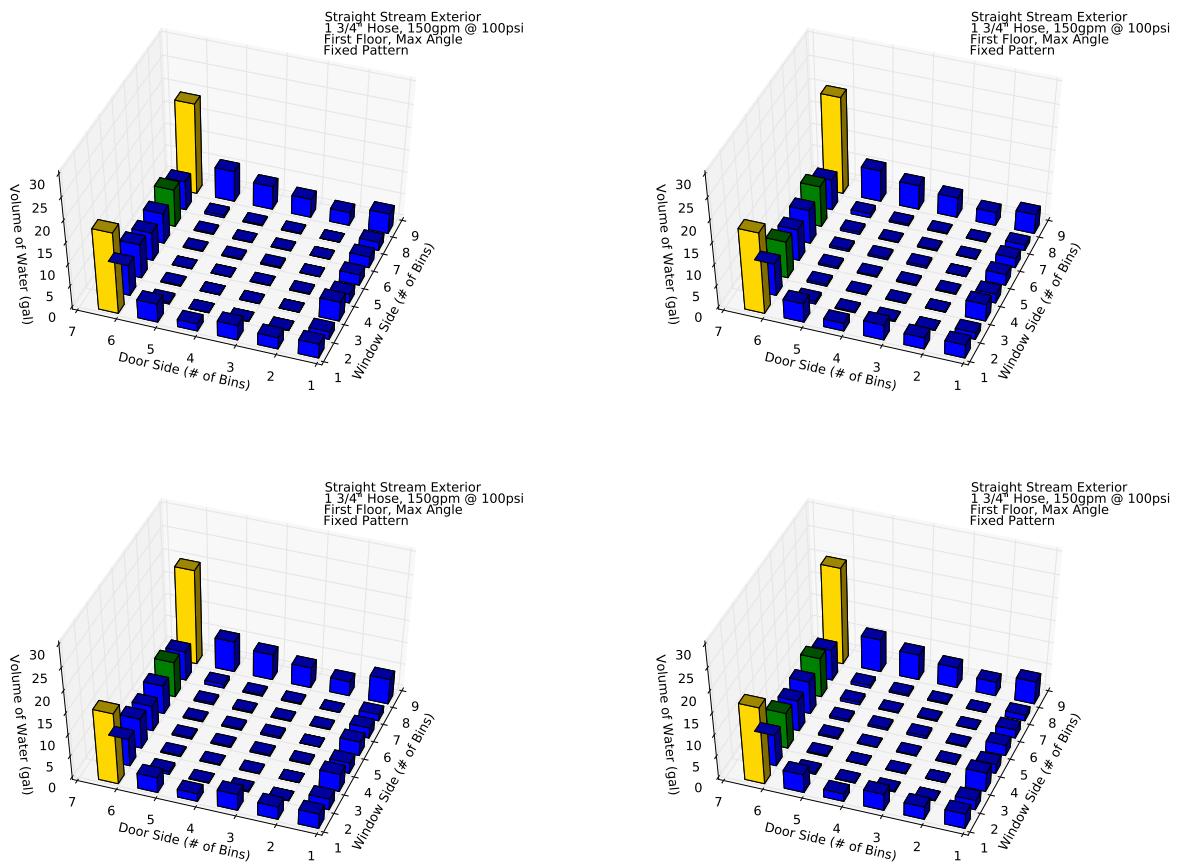


Figure 5.10: Water volume in each collection bin for a fixed exterior straight stream nozzle flowing 150 gpm at 100 psi from the first floor position directed into the structure with a maximum angle. The four bar charts are replicate tests of the same configuration

Qualitatively, the array of bars in each chart in Figure 5.10 look similar to one another. However, to better compare the tests, a statistical approach known as an analysis of variance (ANOVA), was performed. Specifically, the Kruskal-Wallis one-way ANOVA test was applied. The goal of this analysis was to quantify whether samples (in this case the flow rate of water in each bin) originate from the same distribution (are the tests similar or different). The Kruskal-Wallis analysis was selected because there is no prior assumption that the data is normally distributed. While this statistical analysis can compare n number of

data sets and identify if the data sets are statistically different, a limitation in all ANOVAs is the inability to identify which data sets are statistically different. The result of the ANOVA is a p-value. If the p-value is less than 0.05, the experiments being compared are statistically different. If the p-value is large, the experiments being compared are not statistically different.

For the straight stream experiments shown in Figure 5.10, two Kruskal-Wallis ANOVA tests were applied; one was based on average flow rate of water into each collection bin and the other was based on total volume of water recorded in each bin. The resulting p-values were 0.822 and 0.627 for average flow rate and total volume respectively. The high p-values mean that the 4 straight stream flow patterns cannot be distinguished from one another. In other words, these experiments can be considered as repeatable.

Confirmation of repeatability, allowed for the exploration of additional comparisons within the data. The three main comparisons were varying the hose stream type, varying the nozzle position, and varying the flow pressure. The hose stream comparisons were designed to quantify the impact on water distribution from using a straight stream, smooth bore, or a narrow fog pattern. For the hose stream type comparisons, 6 configurations were analyzed. Within each configuration set, the nozzle direction, nozzle movement, and nozzle pressure/flow rate were fixed. Table 5.4 shows the results from the ANOVA test based on flow rate and total volume for each of the configurations tested.

Table 5.4: Assessment of Variation of Hose Stream Types

Configuration	# of Tests	P Value Rate	Different	P Value Volume	Different
Interior, Mid Ceiling, Fixed Pattern	3	6.6E-07	✓	2.3E-05	✓
Interior, Mid Ceiling, 'O' Pattern	3	0.008	✓	0.008	✓
First Floor Exterior, Max Angle, Fixed Pattern	3	0.046	✓	0.100	
Second Floor Exterior, Max Angle, Fixed Pattern	3	0.064		0.004	✓
First Floor Exterior, Max Angle, Sweep Pattern	2	0.383		0.337	
Second Floor Exterior, Max Angle, Sweep Pattern	2	0.433		0.524	

The results of the statistical analysis identified that 4 of the 6 hose stream comparisons showed statistical difference in either the flow rate comparison, total volume comparison or both. In the case of the interior tests, both the fixed pattern and 'o' pattern showed statistical differences in both tests (Figures 5.11 and 5.12). Comparison of the three streams in Figure 5.11, shows that the fog stream had significantly lower volume of water at the edge bins along the wall opposite the doorway. For the interior test with the 'o' pattern, the p-test values indicate that the data are different. The volume data in Figure 5.12, show that patterns along the wall opposite the doorway are similar. The smooth bore had water distributed along the window wall and wall opposite the window compared to the other two hose streams which had the water more concentrated along the wall opposite the doorway; leading to the statistical difference.

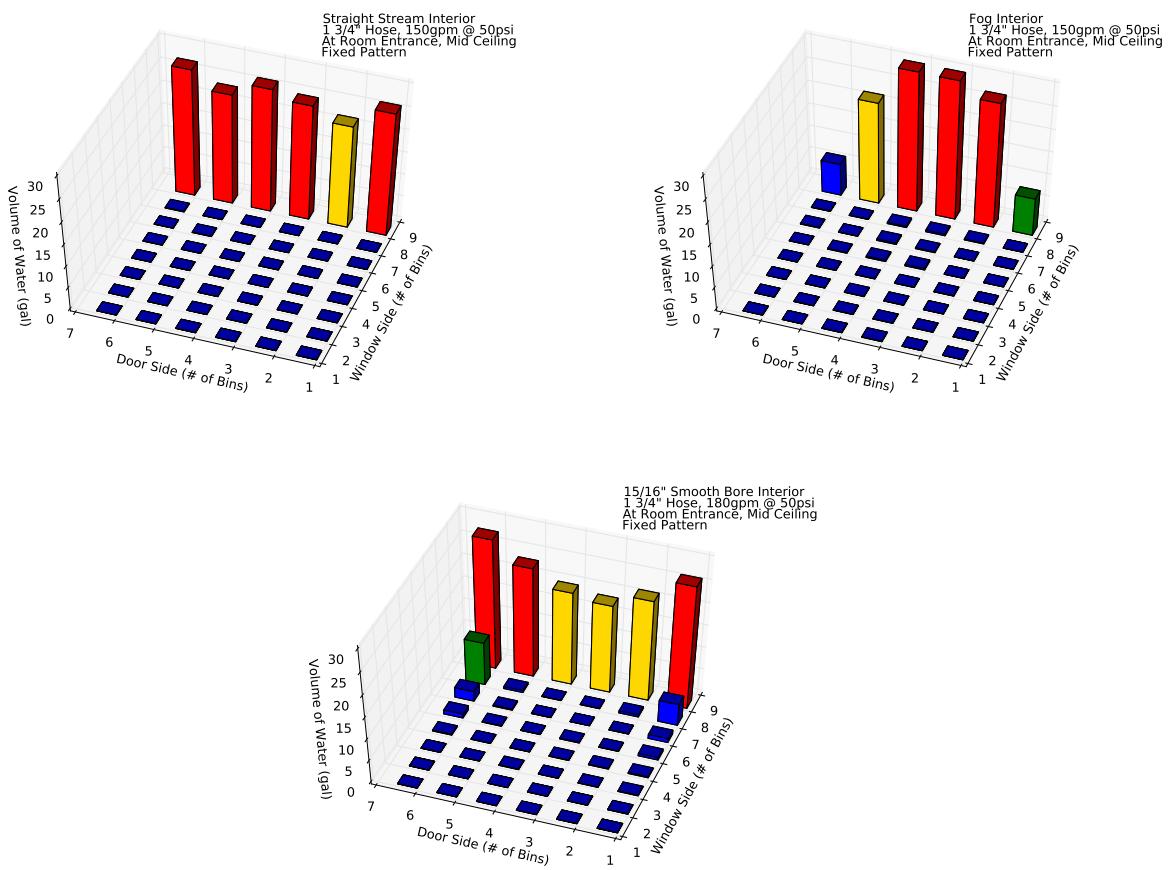


Figure 5.11: Water volume in each collection bin for interior fixed pattern flow at the mid-ceiling position for a straight stream (upper left), fog (upper right), and smooth bore (bottom middle) nozzle

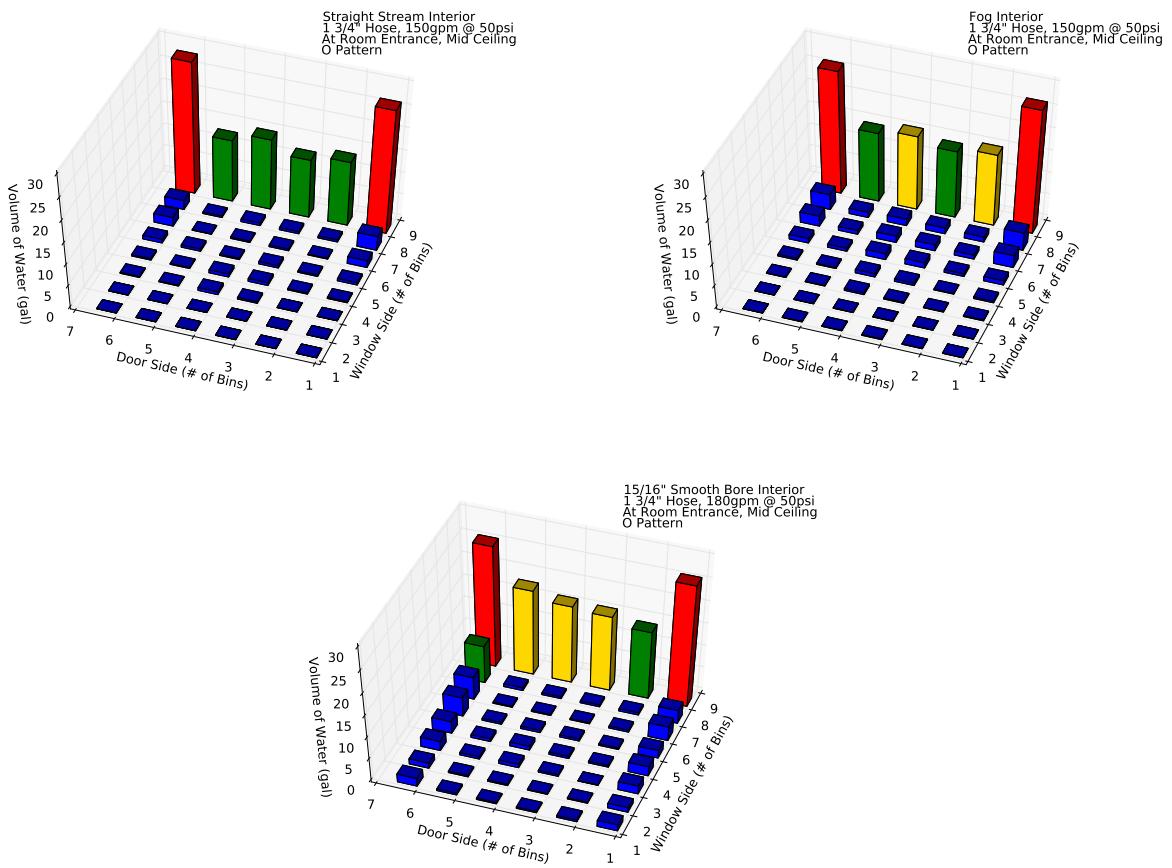


Figure 5.12: Water volume in each collection bin for interior 'O' pattern flow at the mid-ceiling position for a straight stream (upper left), fog (upper right), and smooth bore (bottom middle) nozzle

The statistical tests for the exterior, fixed pattern experiments at the max angle indicated that the first floor tests had a different flow rate distribution and the second floor tests had different total volume distribution. In both the fixed pattern first and second floor tests, the straight stream and smooth bore nozzles showed similar total volume distributions (Figures 5.13 and 5.14). Similar to the interior tests, the fog nozzle shows a different pattern, most noticeably in Figure 5.14.

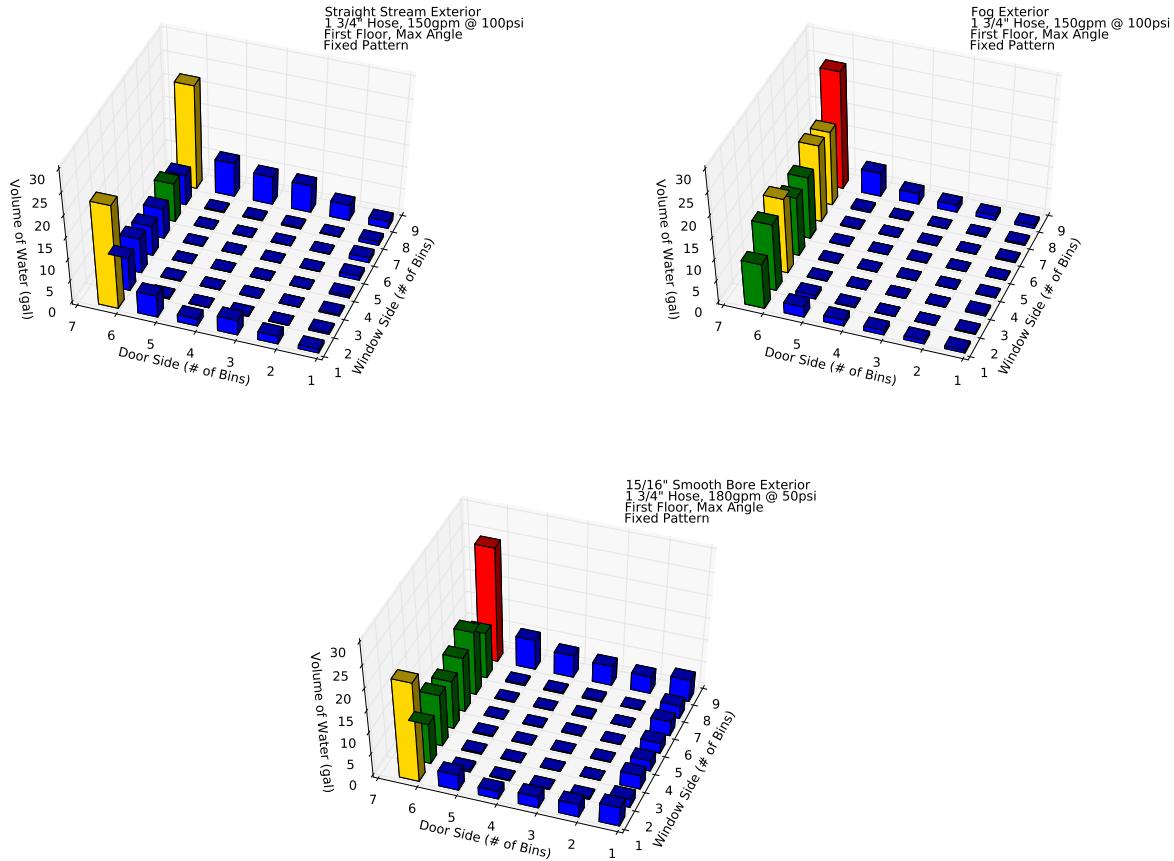


Figure 5.13: Water volume in each collection bin for exterior first floor fixed pattern flow at the max angle position for a straight stream (upper left), fog (upper right), and smooth bore (bottom middle) nozzle

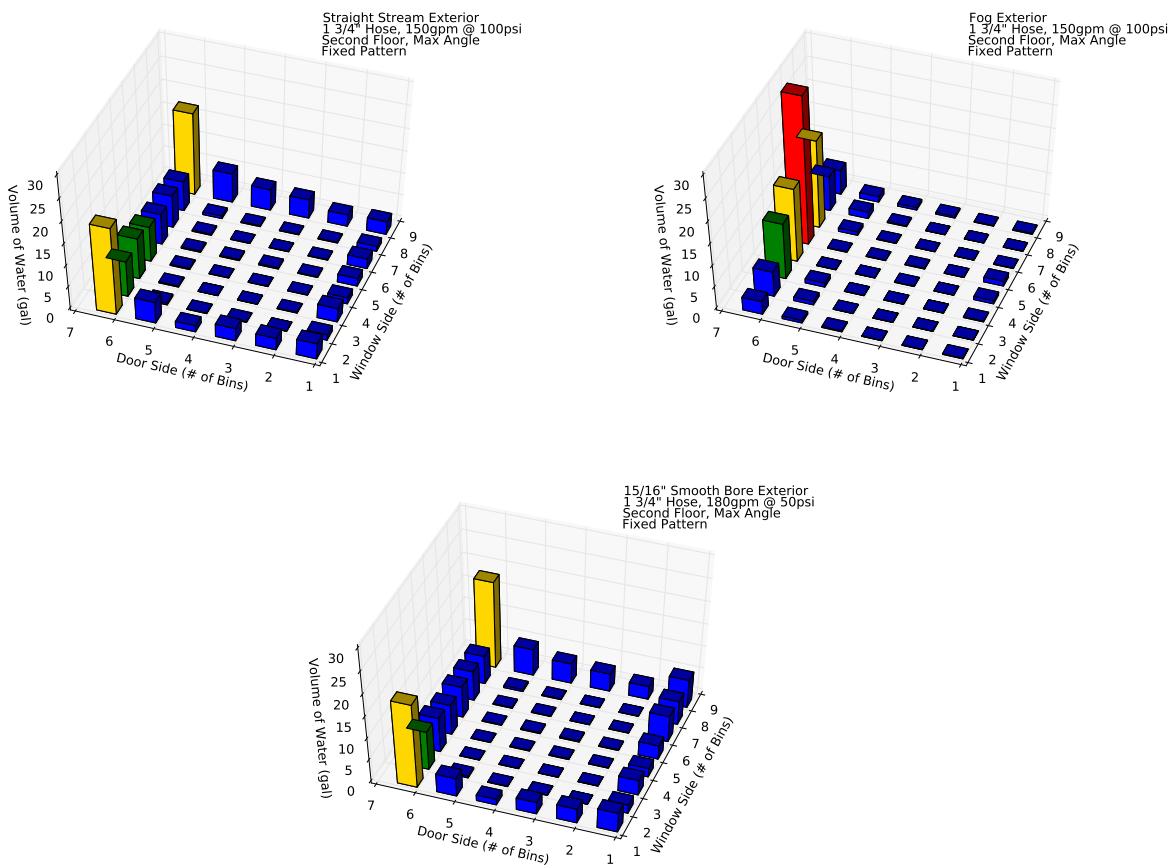


Figure 5.14: Water volume in each collection bin for exterior second floor fixed pattern flow at the max angle position for a straight stream (upper left), fog (upper right), and smooth bore (bottom middle) nozzle

Note that for the exterior water flow experiments with a sweep pattern, only a straight stream and smooth bore hose stream are compared. The stream from a fog pattern would typically encompass the ventilation opening, depending on the size of the opening and the distance from the opening. In these experiments, the fog stream enclosed the window, therefore only a fixed pattern was studied. The results from the statistical tests in Table 5.4, indicate that the straight stream and smooth bore are likely similar in both rate and volume. Figures 5.15 and 5.16 confirm the similarity in the total water distribution.

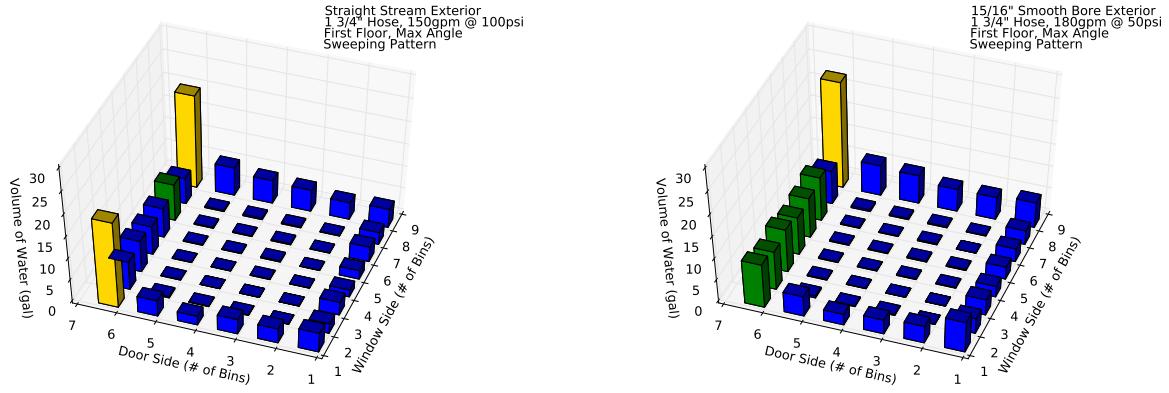


Figure 5.15: Water volume in each collection bin for exterior first floor sweeping pattern flow at the max angle position for a straight stream (left) and smooth bore (right) nozzle

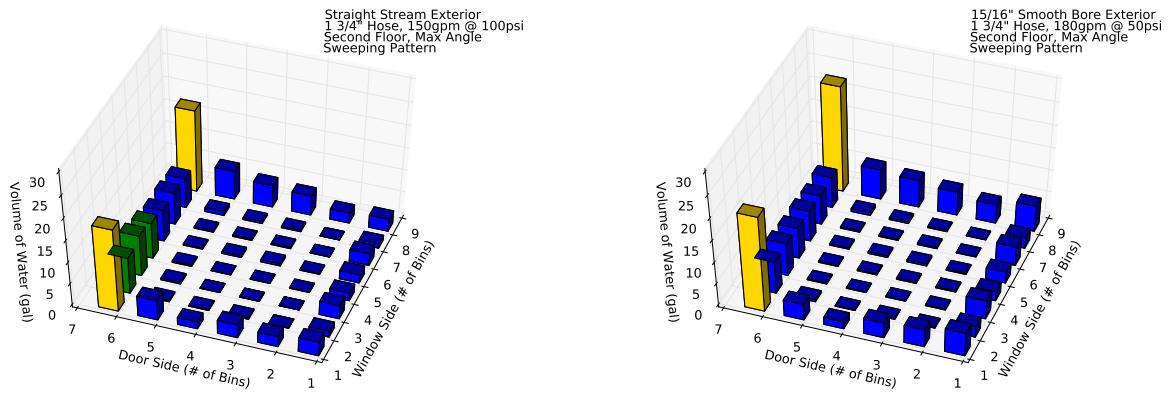


Figure 5.16: Water volume in each collection bin for exterior second floor sweeping pattern flow at the max angle position for a straight stream (left) and smooth bore (right) nozzle

The second comparison was to quantify the impact of nozzle direction on water distribution within the compartment. Referring back to Figures 5.7, 5.8, and 5.9 there are 3, 5, and 5 nozzle directions for the interior experiments, the exterior first floor experiments, and the exterior second floor experiments, respectively. Table 5.5 shows the p-test values average flow rate per collection bin and total volume per collection bin for the nozzle direction comparison experiments. In all comparisons, there was enough variation in the flow rate and volume data for the results to be statistically different.

Table 5.5: Assessment of Variation of Nozzle Directions

Configuration	# of Tests	P Value Rate	Different	P Value Volume	Different
Interior, Smooth Bore, Fixed Pattern	3	3.2E-04	✓	2.2E-04	✓
Interior, Straight Stream, Fixed Pattern	3	3.0E-09	✓	2.0E-08	✓
Interior, Smooth Bore, 'O' Pattern	3	2.0E-04	✓	7.8E-05	✓
Interior, Straight Stream, 'O' Pattern	3	3.6E-04	✓	6.0E-04	✓
First Floor Exterior, Straight Stream	5	2.8E-08	✓	5.6E-08	✓
First Floor Exterior, Smooth Bore	5	1.0E-06	✓	3.8E-06	✓
Second Floor Exterior, Straight Stream	5	2.3E-09	✓	2.7E-09	✓
Second Floor Exterior, Smooth Bore	4	3.1E-06	✓	6.9E-07	✓

For the interior tests, there were three nozzle directions examined: at wall, mid ceiling, and max angle (Figure 5.7). The fixed pattern smooth bore and straight stream tests (Figures 5.17 and 5.25) both show variation in the data (Table 5.5) that is visualized in the total volume bar charts. Specifically, the max angle position for both hose stream types resulted in spread along the perimeter of the compartment compared to localized water along the wall opposite the doorway. The 'o' pattern smooth bore and straight stream tests show are similar to the fixed pattern. The mid ceiling and wall position show water concentrated along the wall opposite the doorway while the max angle shows water distributed around the perimeter. The ANOVA tests also show that there is statistical difference between the position for the moving hose stream at the three positions.

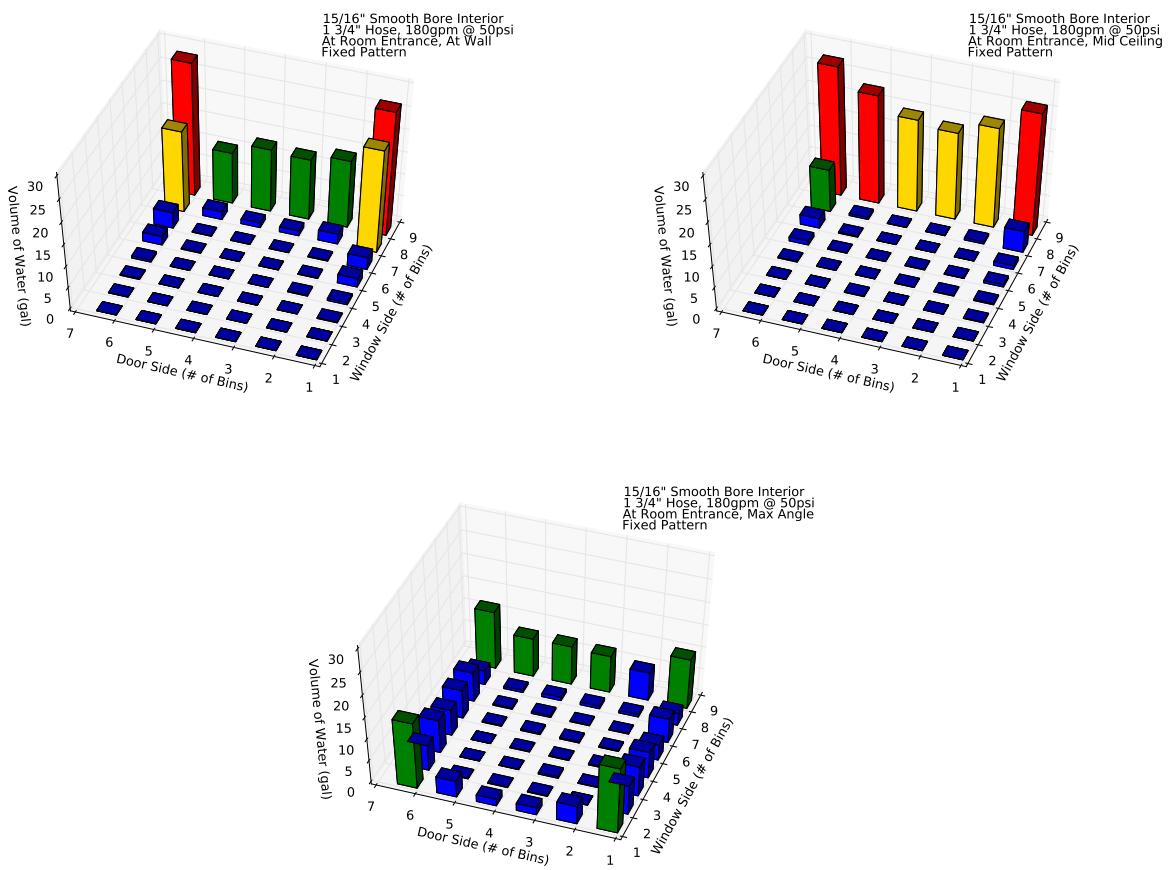


Figure 5.17: Water volume in each collection bin for an interior smooth bore stream with a fixed pattern at three nozzle positions: at wall (top left), mid ceiling (top right) and max angle (bottom)

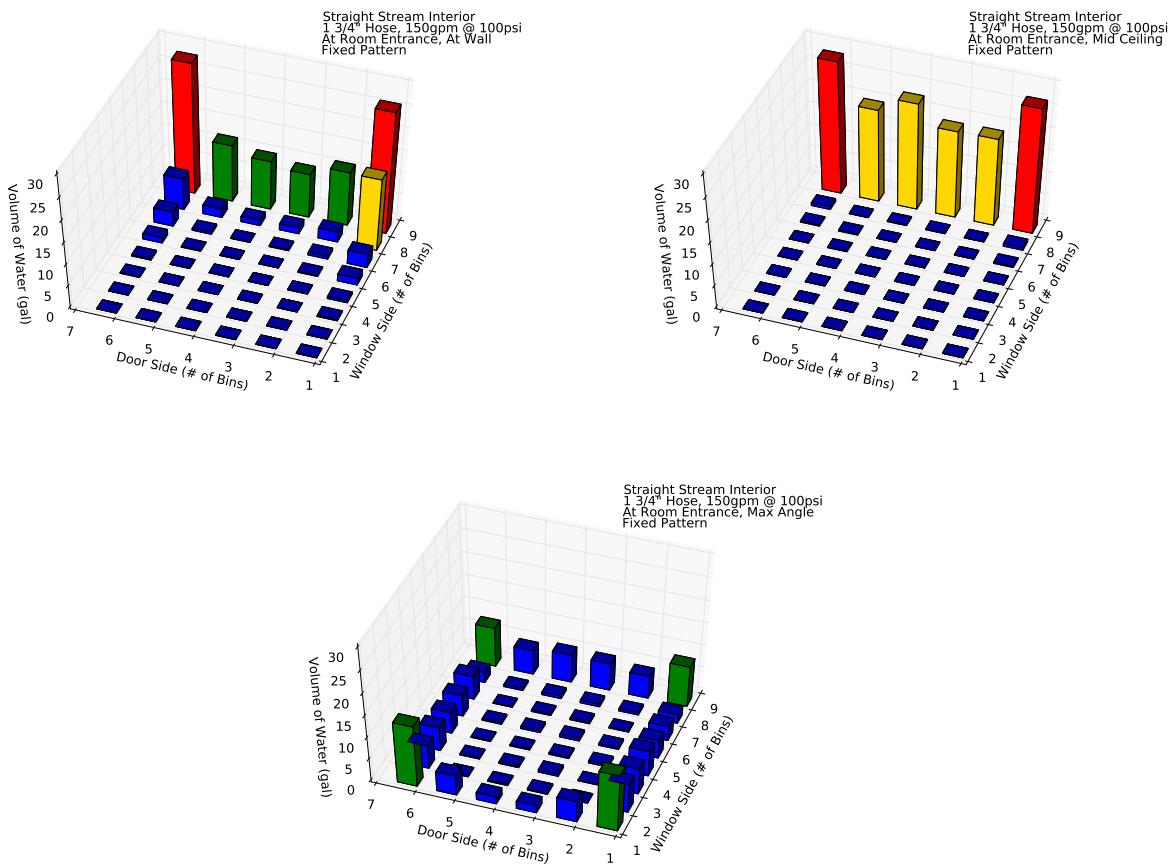


Figure 5.18: Water volume in each collection bin for an interior straight stream with a fixed pattern at three nozzle positions: at wall (top left), mid ceiling (top right) and max angle (bottom)

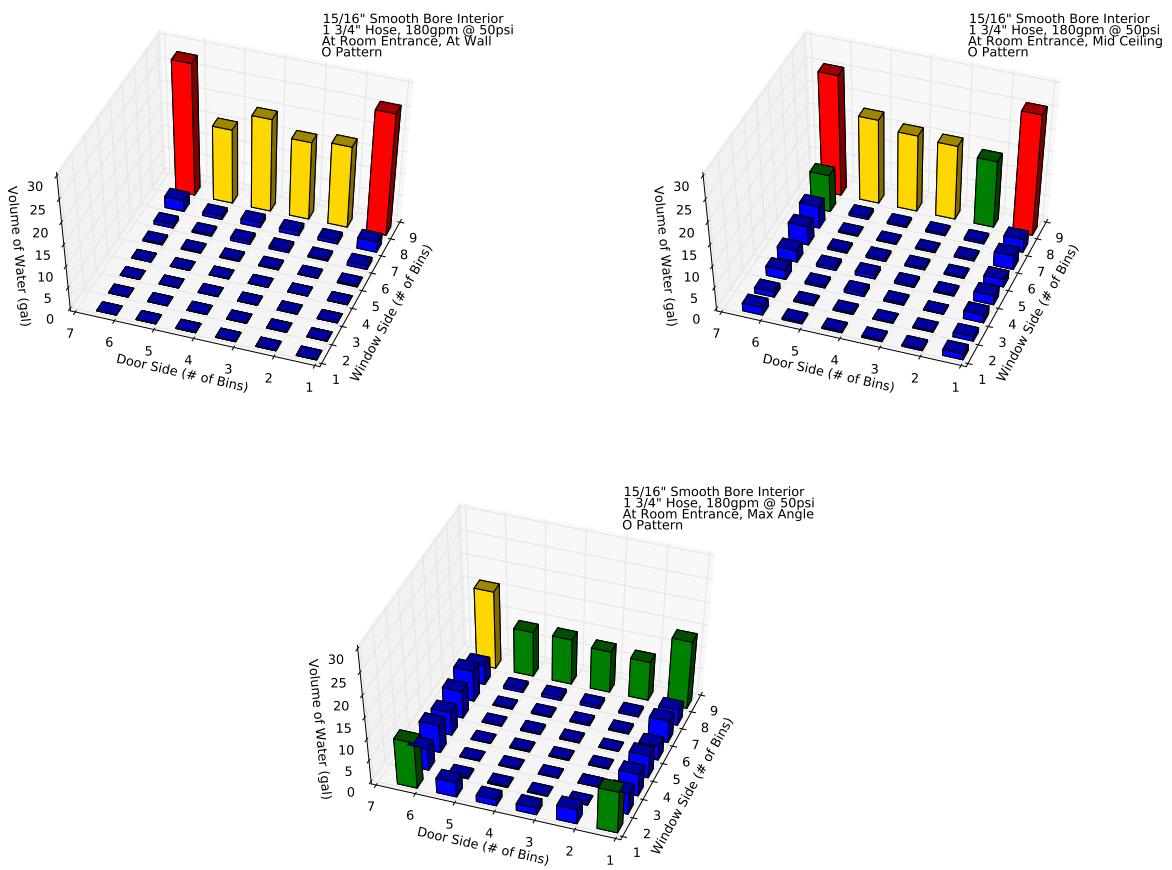


Figure 5.19: FWater volume in each collection bin for an interior smooth bore stream with an 'o' pattern at three nozzle positions: at wall (top left), mid ceiling (top right) and max angle (bottom)

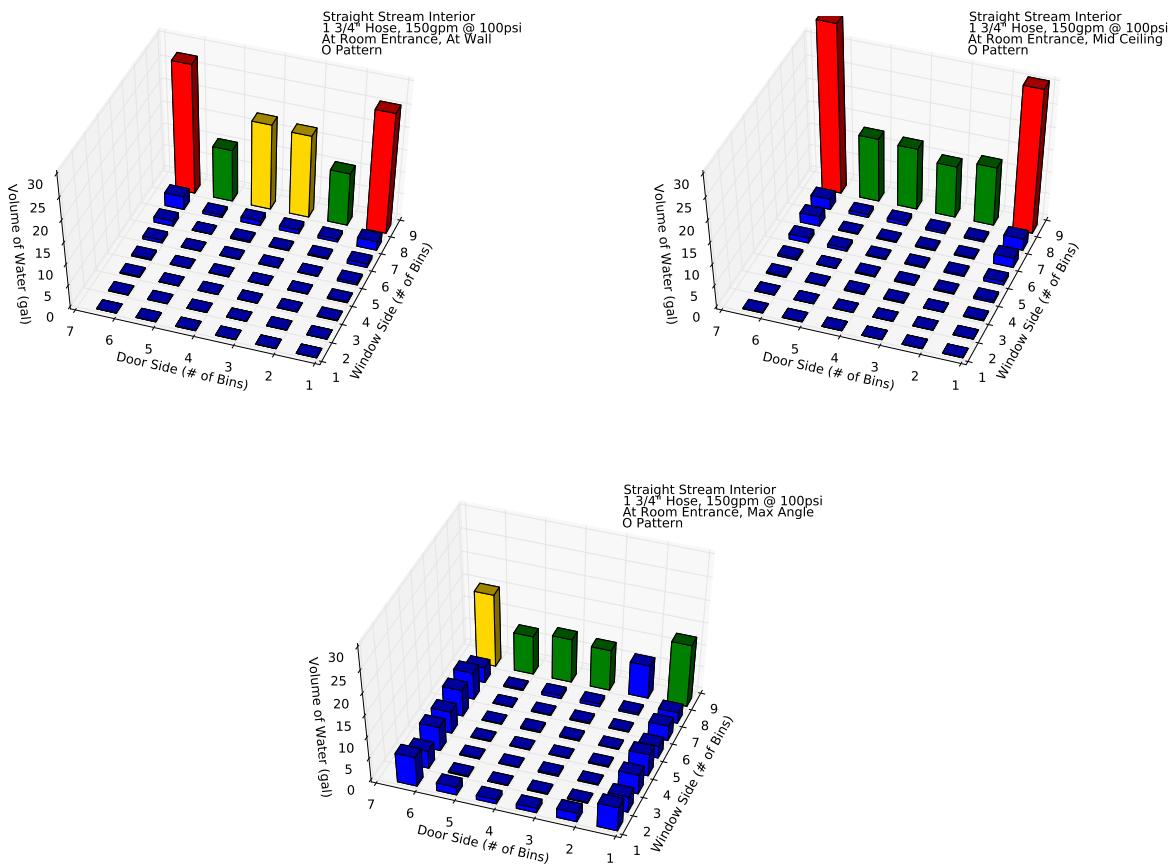


Figure 5.20: Water volume in each collection bin for an interior straight stream with an 'o' pattern at three nozzle positions: at wall (top left), mid ceiling (top right) and max angle (bottom)

The first floor exterior experiments used 5 different nozzle directions: max angle, mid ceiling, min angle ceiling, min angle wall, and at wall. The statistical analysis indicated that the 5 nozzle direction results are not the same in terms of flow rate and volume for both the smooth bore and straight stream experiments. Figure 5.21 shows the water volume distribution for the 5 positions for the smooth bore stream while Figure 5.22 shows the water volume distributions for the straight stream. For both streams, the mid ceiling and min angle ceiling positions indicate that the majority of the water accumulated in the bins along the wall opposite the window. The two wall positions and the max angle position show a broader distribution of water within in the compartment with the max angle having the most disperse distribution.

The smooth bore and straight stream second floor exterior experiments were similar to the first floor exterior experiments in that changing nozzle position produced flow rate and volume data was different as a function of position. Figures 5.23 and 5.24 show the results of the water volume distribution for 4 smooth bore positions and 5 straight stream positions. Like all of the prior position data presented, the max angle shows that the most prominent water distribution with water filling the compartment perimeter buckets, noticeably different than the wall or ceiling positions. The one exception here is the straight stream sill experiment shows a flatter overall distribution.

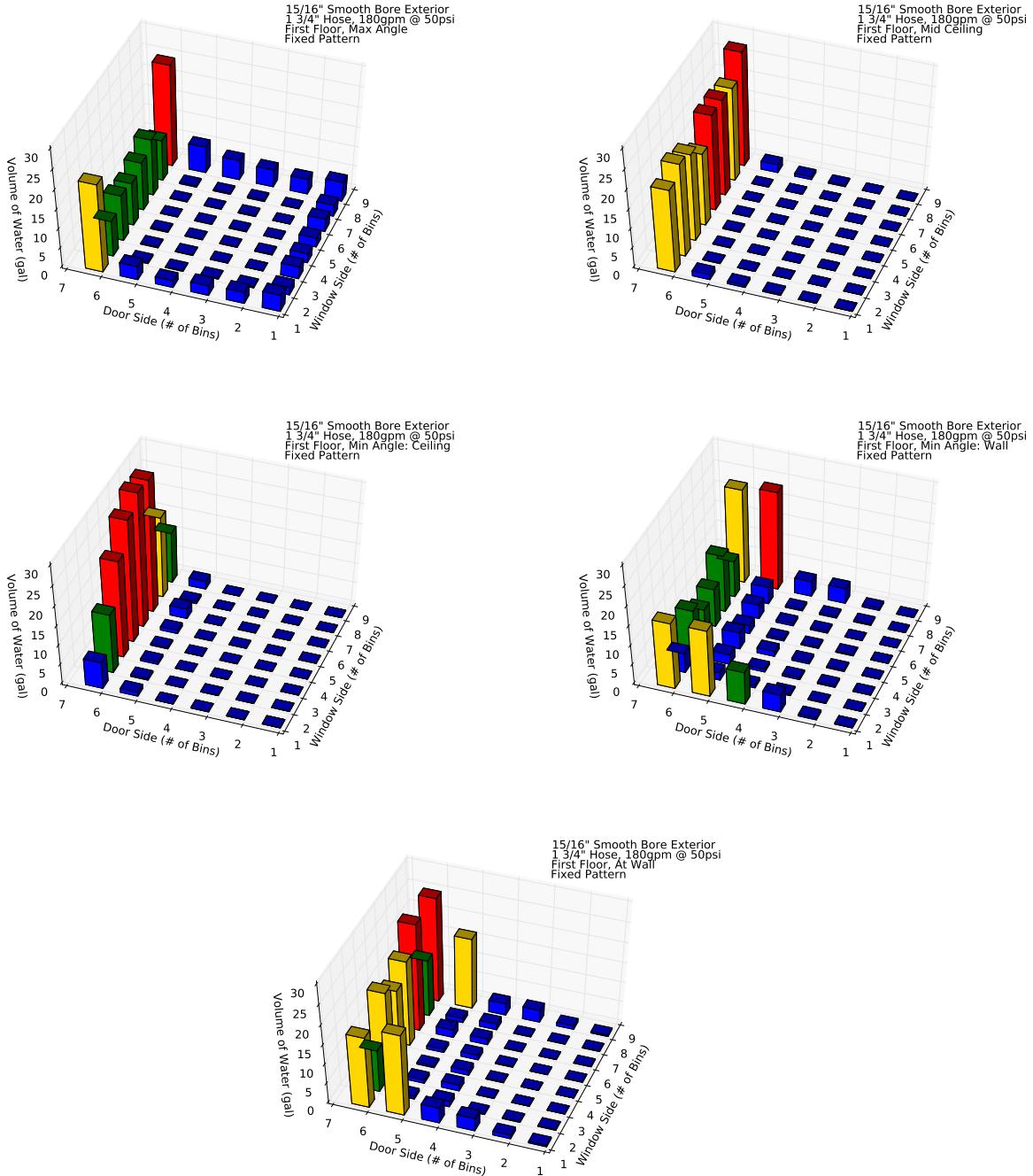


Figure 5.21: Water volume in each collection bin for a first floor exterior smooth bore stream with a fixed pattern at five nozzle positions: max angle (top left), mid ceiling (top right), min angle ceiling (middle left), min angle at wall (middle right), and at wall (bottom)

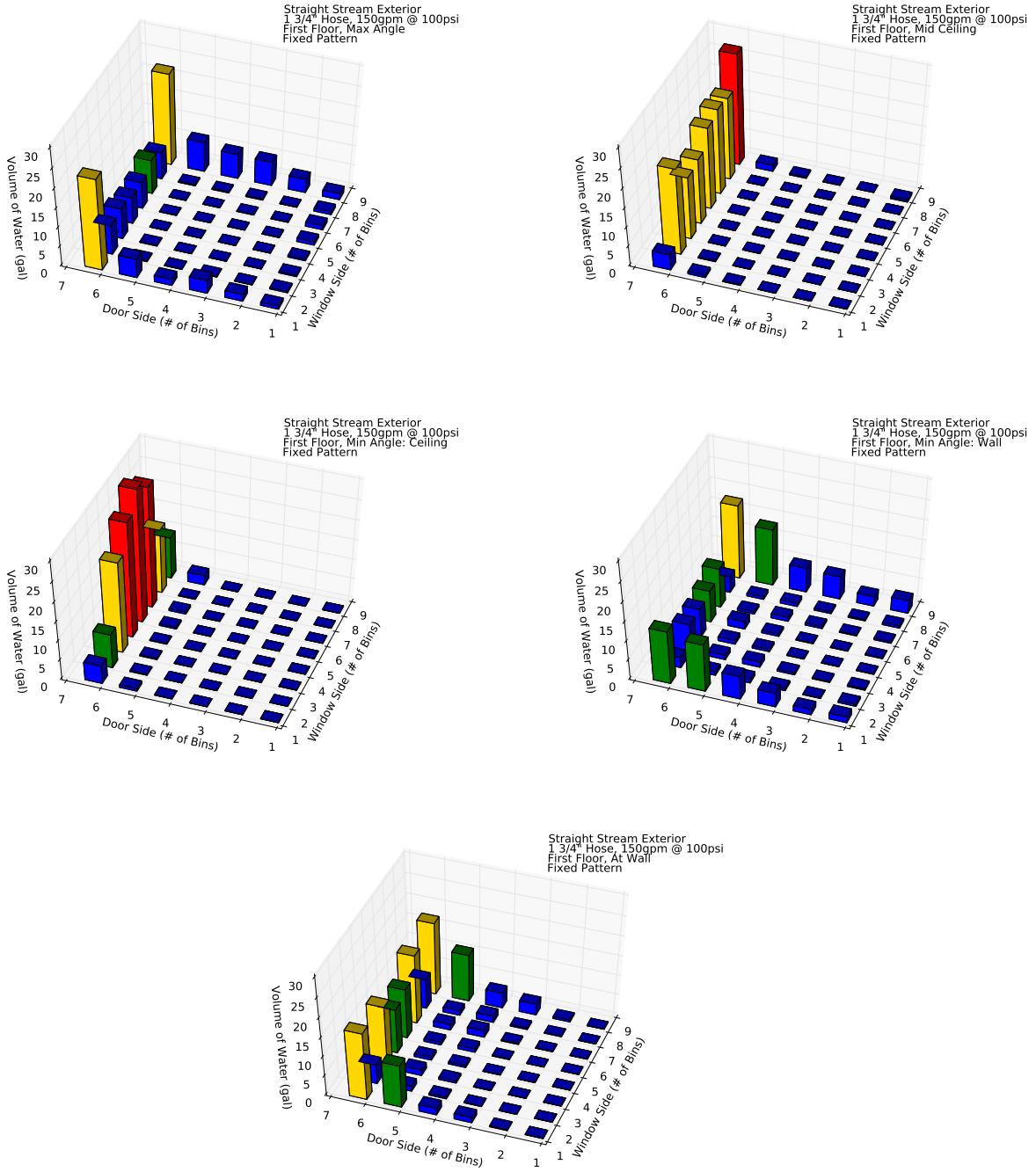


Figure 5.22: Water volume in each collection bin for a first floor exterior straight stream with a fixed pattern at five nozzle positions: max angle (top left), mid ceiling (top right), min angle ceiling (middle left), min angle at wall (middle right), and at wall (bottom)

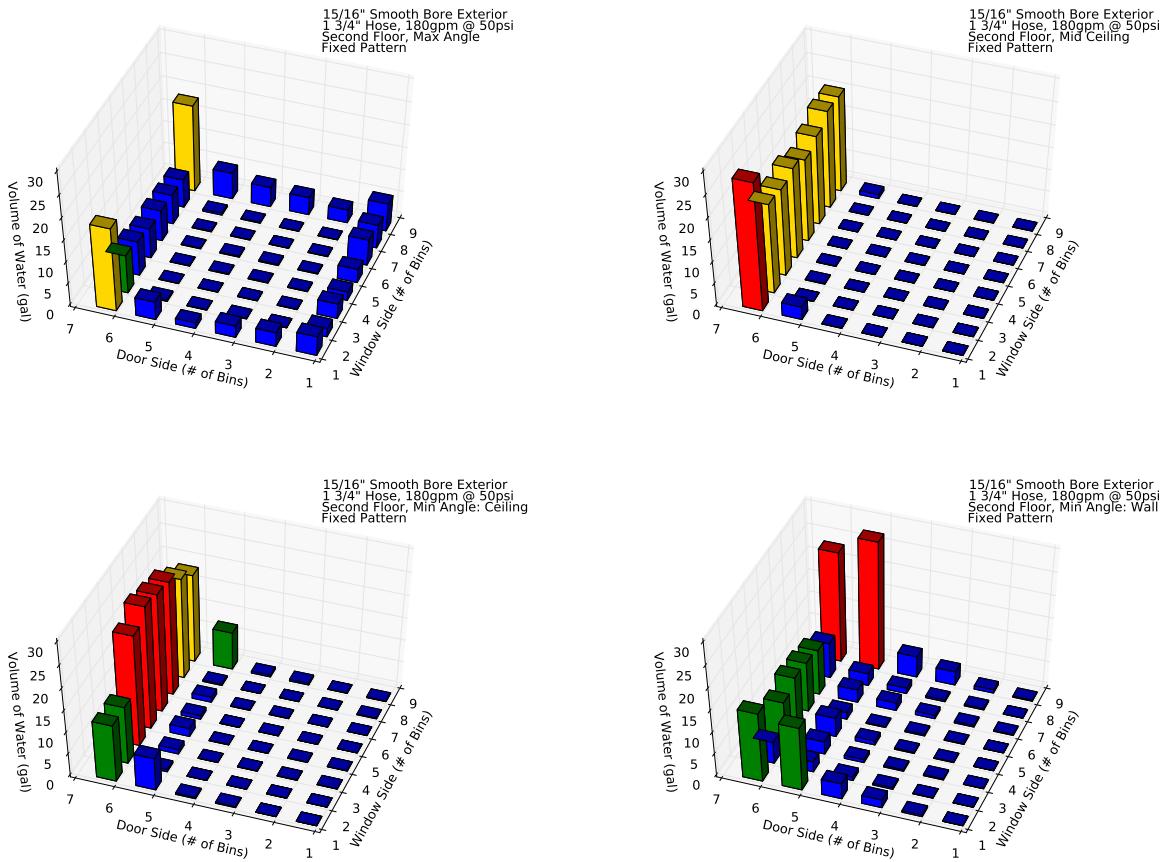


Figure 5.23: Water volume in each collection bin for a second floor exterior smooth bore stream with a fixed pattern at four nozzle positions: max angle (top left), mid ceiling (top right), min angle ceiling (bottom left), and min angle wall (bottom left)

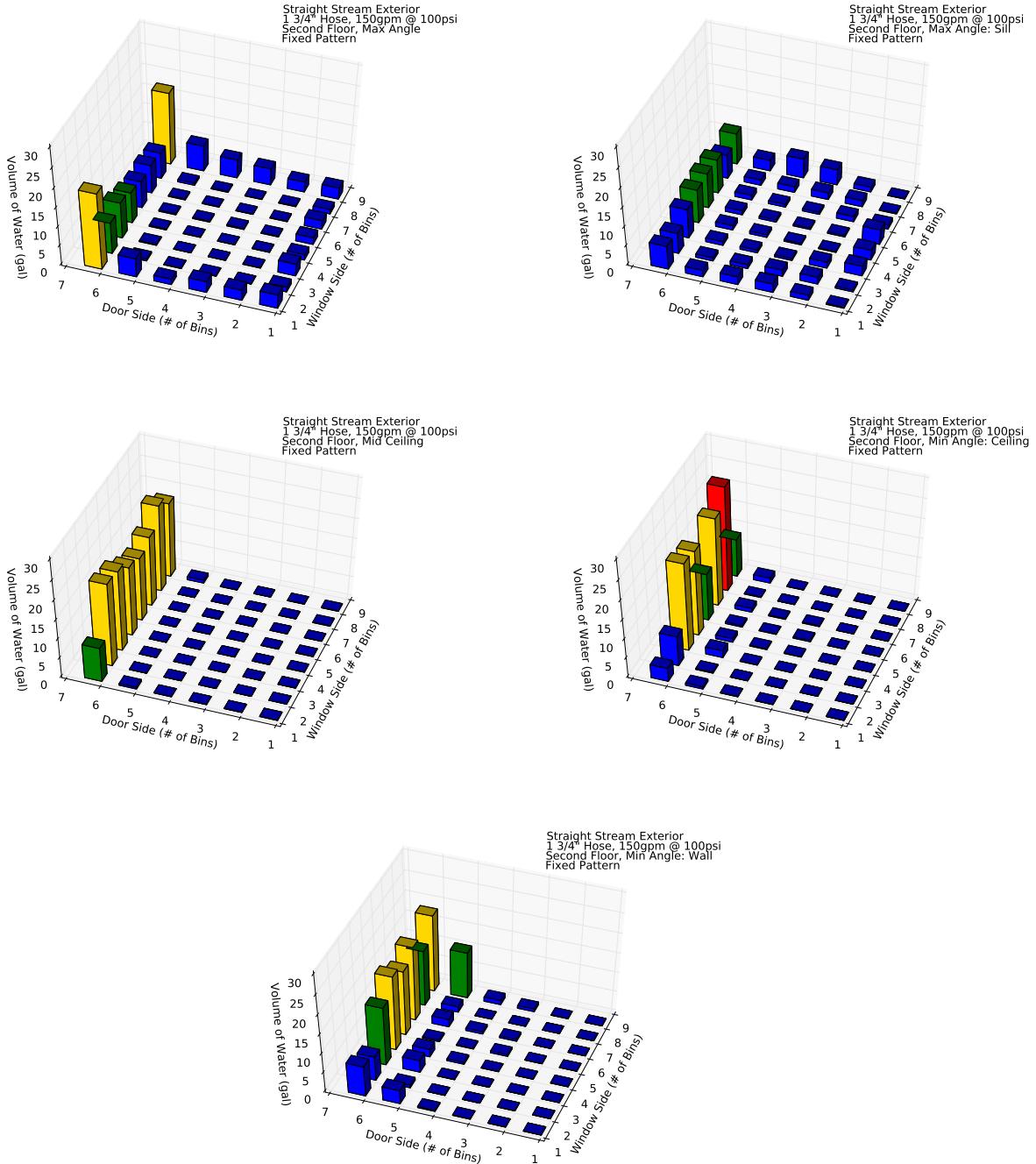


Figure 5.24: Water volume in each collection bin for a second floor exterior straight stream with a fixed pattern at five nozzle positions: max angle (top left), max angle still (top right), mid ceiling (middle left), min angle ceiling (middle right), and min angle wall (bottom)

The third comparison was to quantify the impact of nozzle pressure on water distribution within the compartment.

Table 5.6: Assessment of Variation of Nozzle Pressure

Configuration	# of Tests	P Value Rate	Different	P Value Volume	Different
Interior, Straight Stream, Mid Ceiling	3	0.277		0.031	✓
Interior, Fog Stream, Mid Ceiling	3	0.198		0.028	✓
First Floor Exterior, Straight Stream, Max Angle	4	0.850		0.591	
First Floor Exterior, Smooth Bore, Max Angle	4	0.360		0.129	
First Floor Exterior Smooth Bore, Vary Tip Size	3	0.205		0.166	

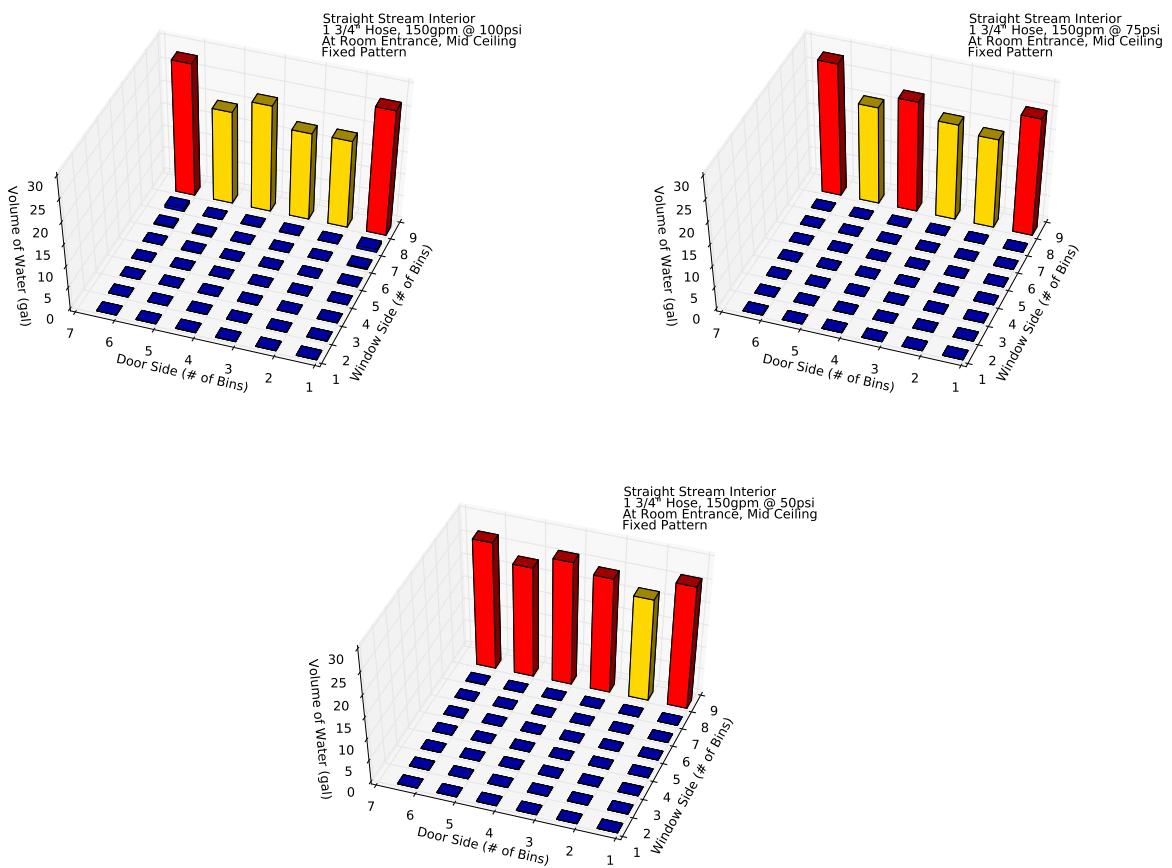


Figure 5.25: Figures showing distribution differences in varying nozzle pressures during a straight stream attack with a fixed pattern.

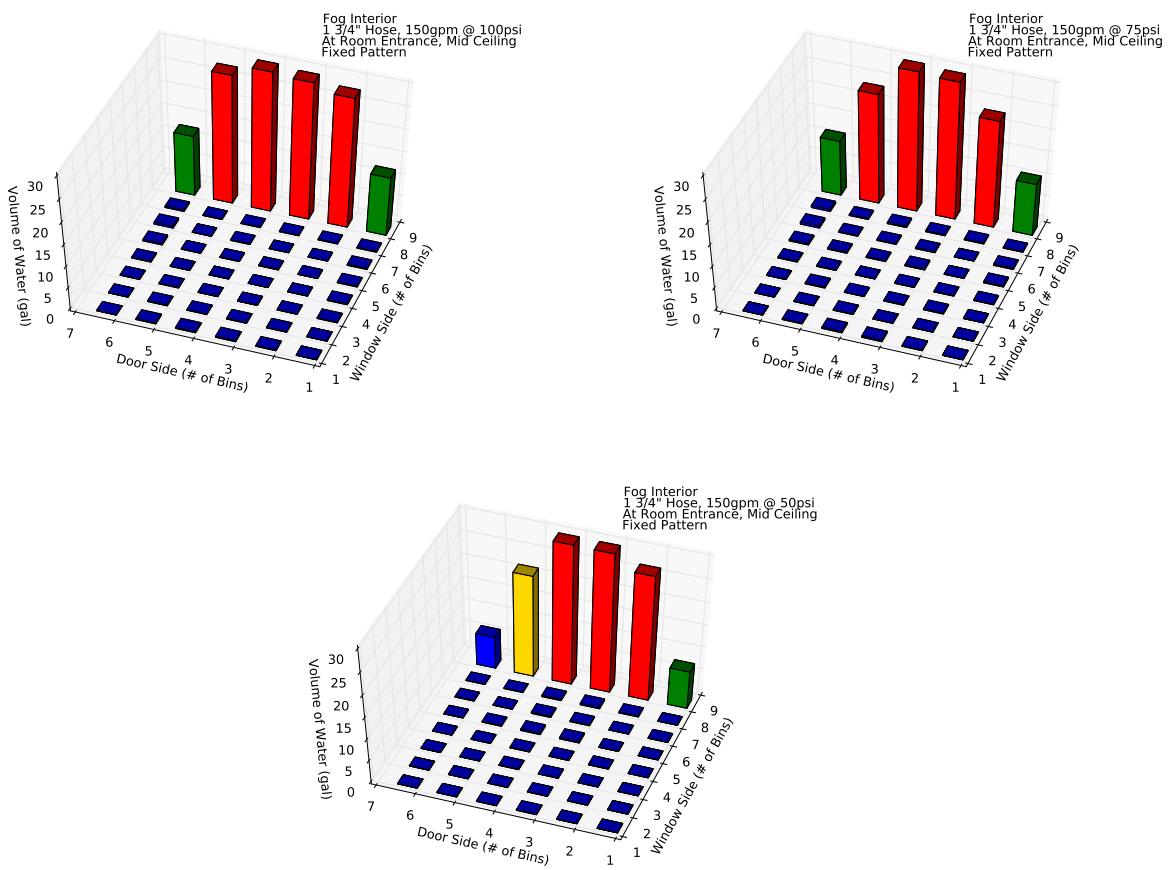


Figure 5.26: Figures showing distribution differences in varying nozzle pressures during a fog attack with a fixed pattern.

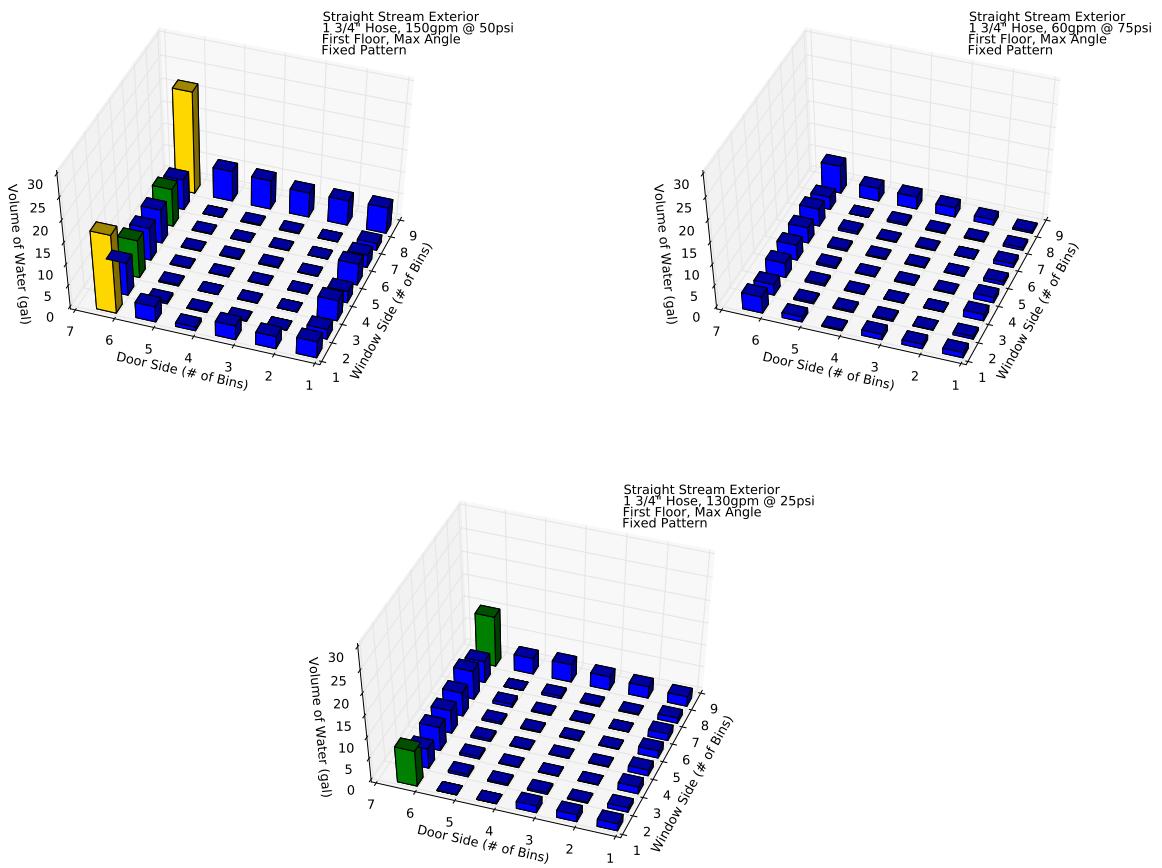


Figure 5.27: Figures showing distribution differences in varying nozzle pressures during an exterior first floor straight stream attack with a fixed pattern.

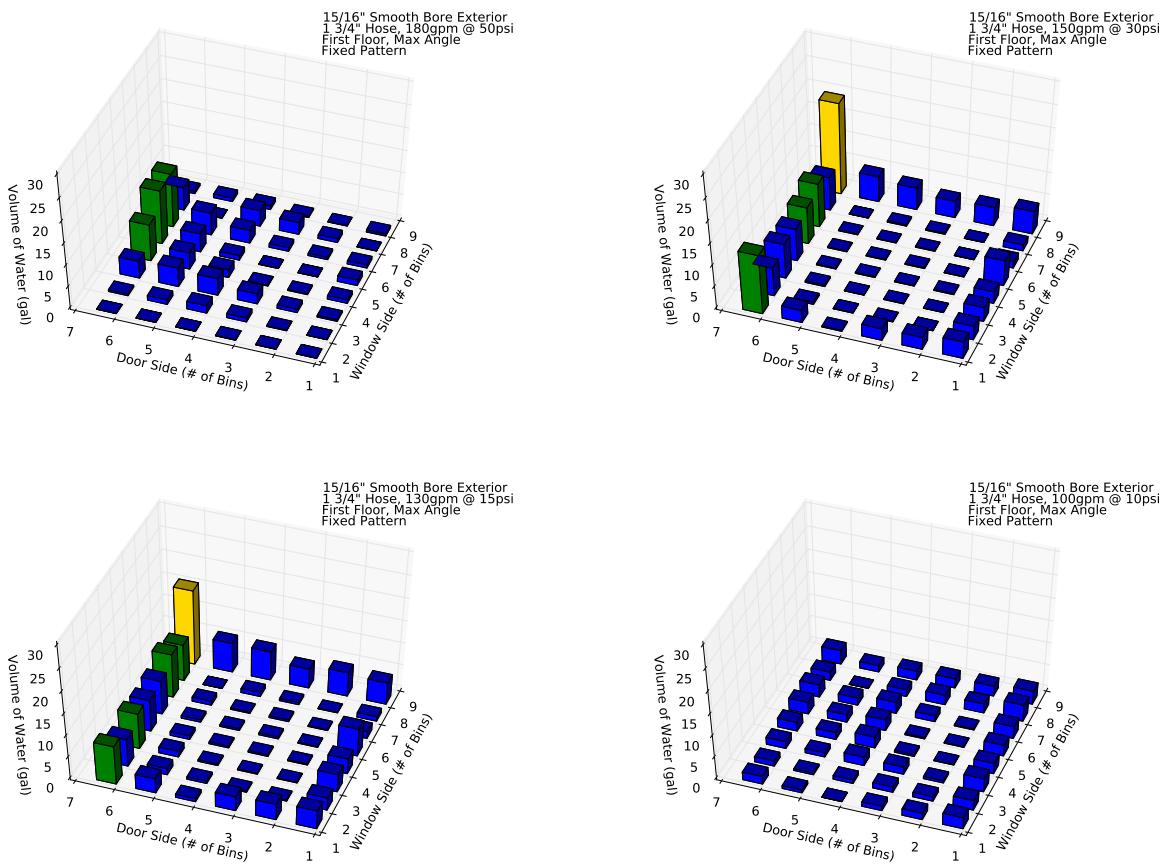


Figure 5.28: Figures showing distribution differences in varying nozzle pressures during an exterior first floor smooth bore attack with a fixed pattern.

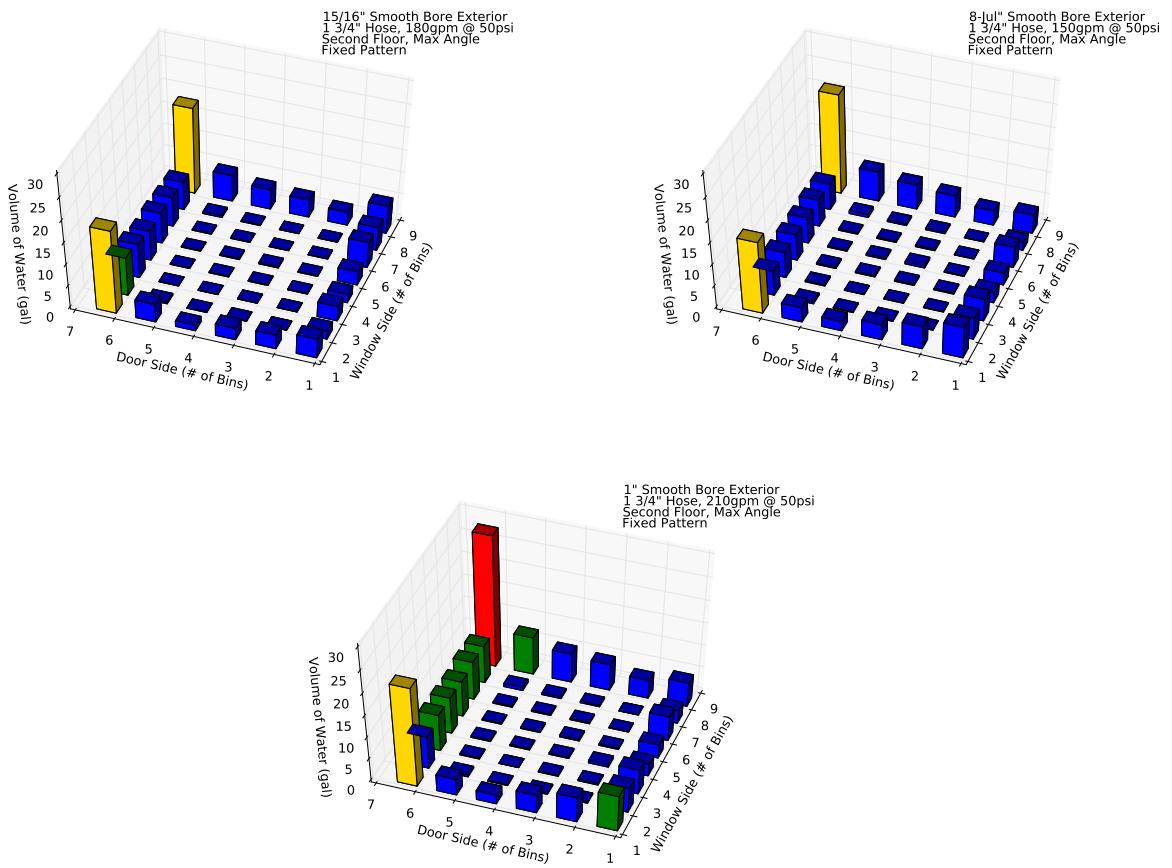


Figure 5.29: Figures showing distribution differences in varying nozzle flow rates by increasing the tip size during an exterior second floor smooth bore attack with a fixed pattern.

Applying water from the exterior or from a distance via the interior will adequately coat the surfaces of a compartment (walls and ceiling) while applying little water to the center of the room.

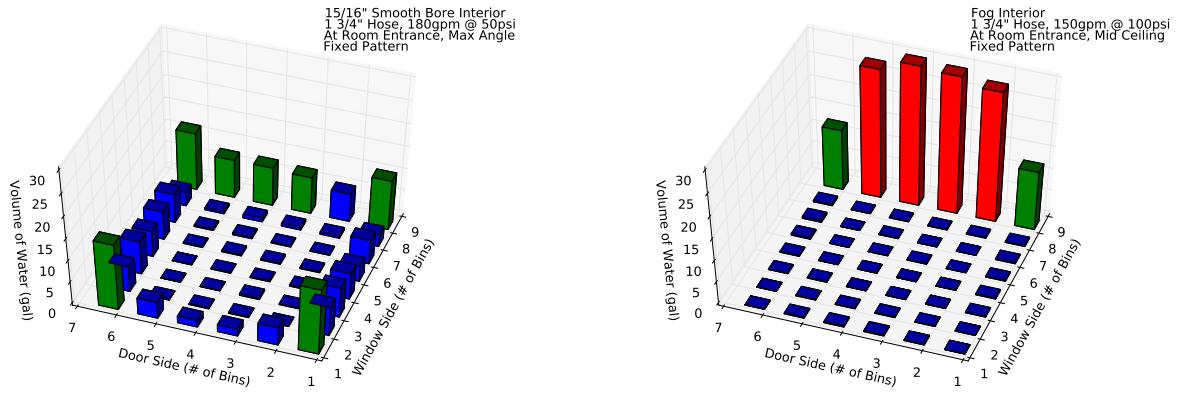


Figure 5.30: Figures showing lack of adequate coverage to the center of the room from an interior attack.

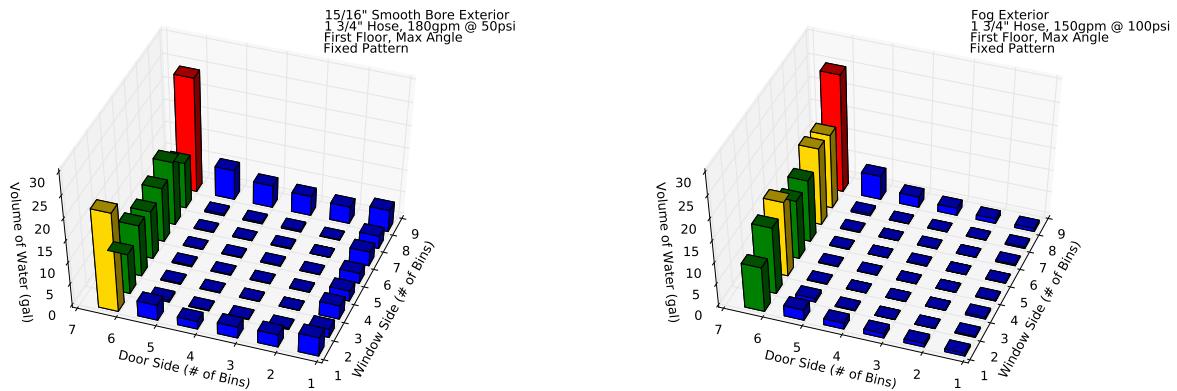


Figure 5.31: Figures showing lack of adequate coverage to the center of the room from an exterior attack.

From both the fire tests as well as the non-fire tests, it is evident that little to no water makes it into the center of the room given an attack featuring the nozzle directed at either the ceiling or the side walls of the compartment.

6 Future Research Needs

Part I of the Fire Attack Study was intended to provide preliminary results and insight into the amount of air entrained by hose streams using differing nozzles and configurations in addition to determining where water is distributed within compartments. These tests have built upon the work conducted by Knapp et. al of the Rockland County, NY Fire Training Academy who conducted early experiments to attempt to quantify the amount of air entrained by suppression operations. Because the testing scope was limited to certain geometries for both air entrainment and water distribution, a future study analyzing different sized structures (including a varying ceiling height and design) in addition to differing compartmentation versus open concepts would be beneficial to further the understanding.

7 Summary

The first part to the Fire Attack study in which testing was conducted to analyze and quantify both the air entrainment in hose streams and the water distribution in compartments has provided results to further the understanding of fire suppression operations. As previous research has shown, ventilation, flow paths, and exterior streams have opened the eyes of many individuals to the complexity of the modern fire environment and led to questions regarding traditions and tactics that have been used for decades. The ability to conduct experiments examining these methods utilizing common equipment in representative structures to provide the fire service with credible scientific information is invaluable. By examining these components to fire suppression operations individually and without fire involvement, baseline knowledge for how hose streams move air within structures and where water is distributed can be singled out. This allows for a better understanding of hose streams before utilizing them under fire conditions. All of this information can then be incorporated into the development of new strategies and tactics to create a safer and more efficient fire ground.

For both the air entrainment and water distribution testing, differences were evaluated by varying the application method, hose stream type, nozzle movements, pressures/flow rates, and stream locations and elevation angles. After conducting over 150 tests and compiling the data with both the FSRI team and our technical panel, the results were summarized as follows:

Air Entrainment -

- Air entrainment is dependent on hose stream type. (smooth bore, straight stream, fog)
- Air entrainment is dependent on structure size, compartmentalization, and ventilation configurations.
- Increases in nozzle movement increase overall air entrainment.
- Different nozzle movement patterns have little effect on overall air entrainment. (O, T, Z, inverted U)
- Air entrainment, either into or out of the structure, is dependent on the horizontal distance of the nozzle to the ventilation opening.

Water Distribution -

- Water distribution is dependent on hose stream type. (smooth bore, straight stream, fog)
- Water distribution is dependent on stream elevation angle within a compartment.
- Varying water pressure at the nozzle and flow rate can affect the total amount of water applied to a given area; however, the distribution location can remain constant.
- Deflecting the hose stream off the ceiling or opposite wall of a compartment can coat the surfaces while applying little water to the center of the room.

The conclusions from these experiments helped to guide the design of the 30+ full-scale residential fire experiments in addition to the acquired structure testing. Stay tuned to the remainder of the Fire Attack study for the details and analysis on the full-scale fire experiments, both in the laboratory and in the field. The results from the fire experiments will be constructed into tactical considerations to share with the fire service worldwide.

A Air Entrainment Figures

A.1 Manufacturer Comparison

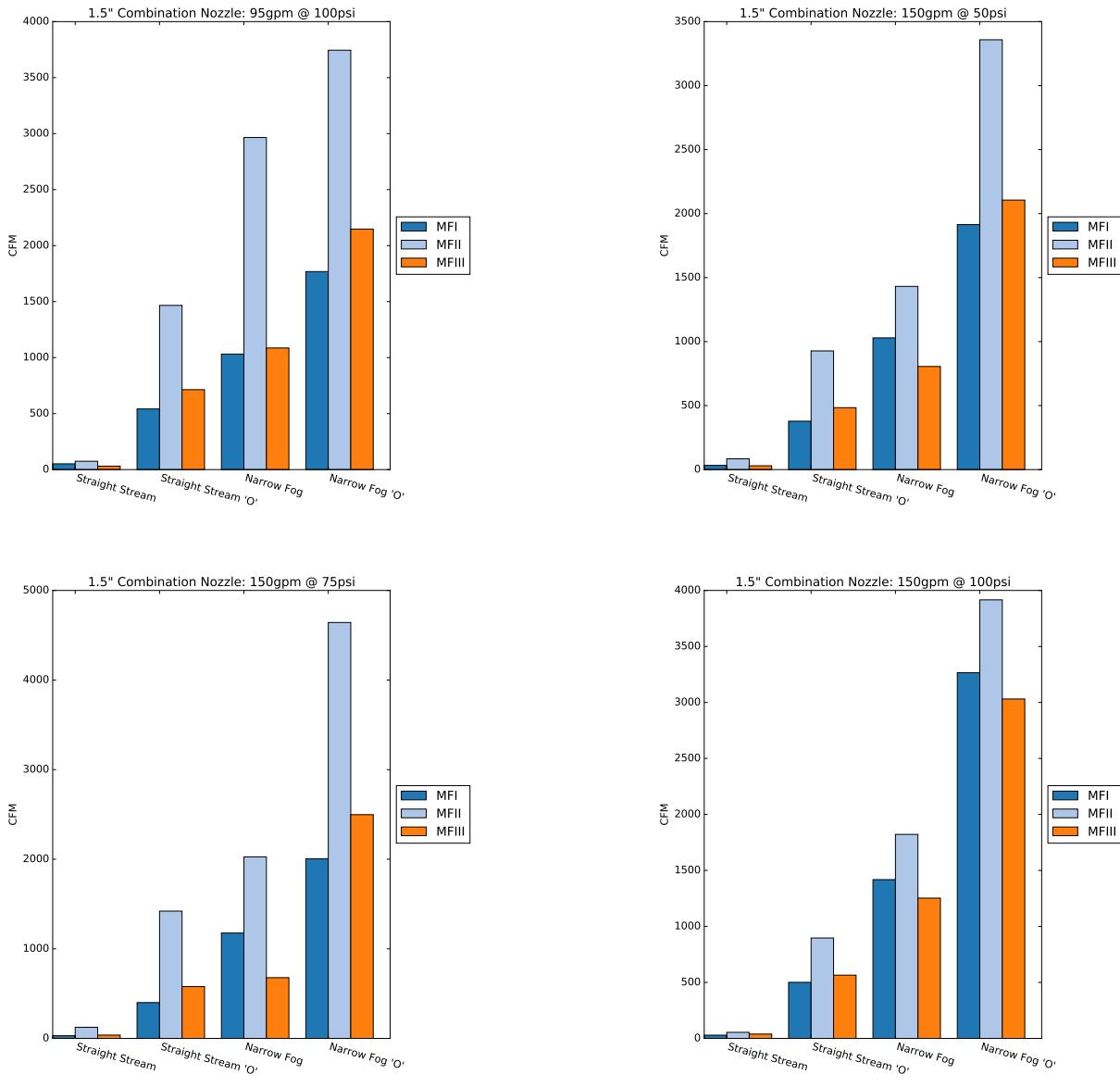


Figure A.1: Figures showing manufacturer comparison of interior air entrainment results for 1.5 in combination nozzles.

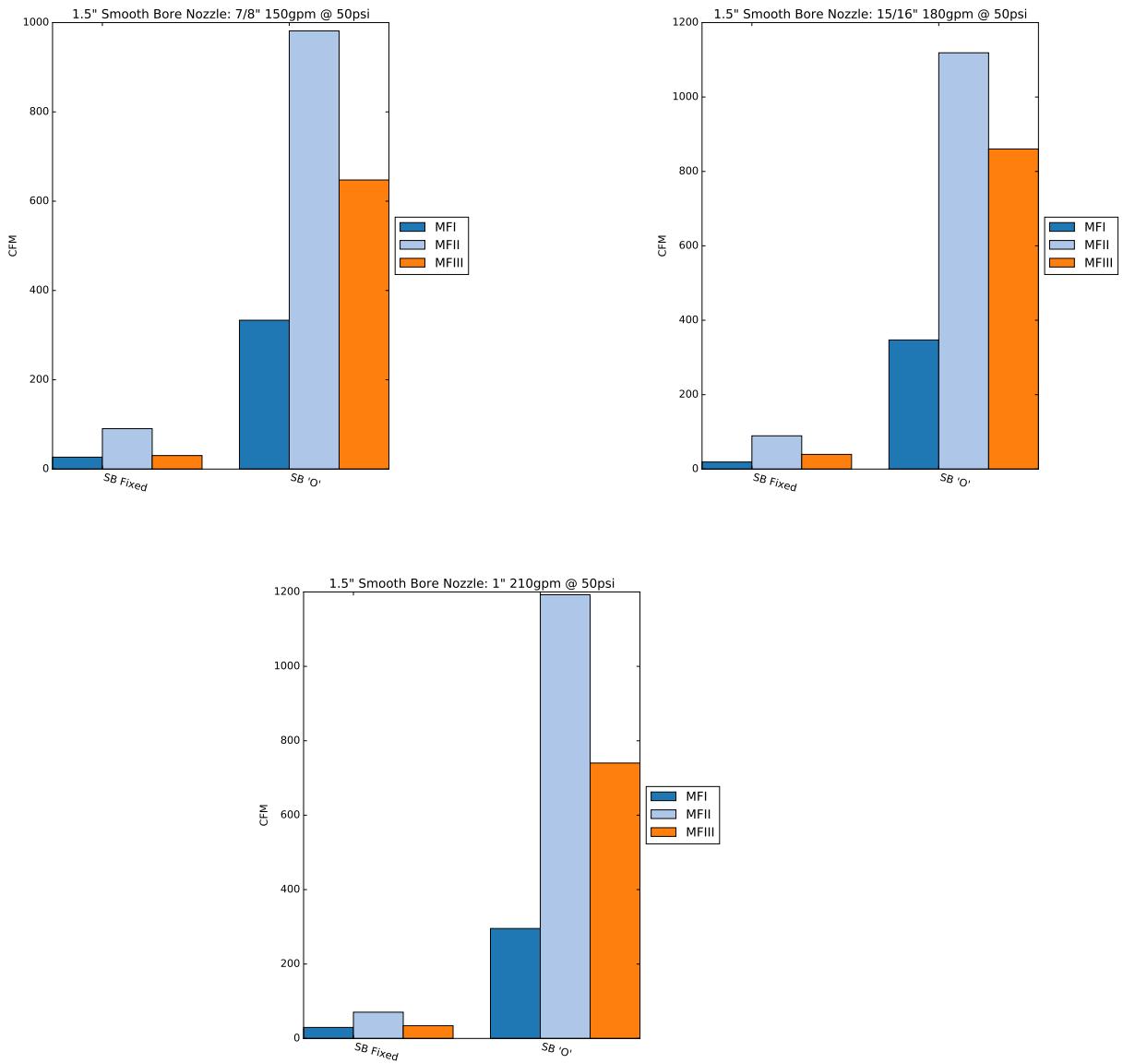


Figure A.2: Figures showing manufacturer comparison of interior air entrainment results for 1.5 in smooth bore nozzles.

A.2 Total Air Entrainment

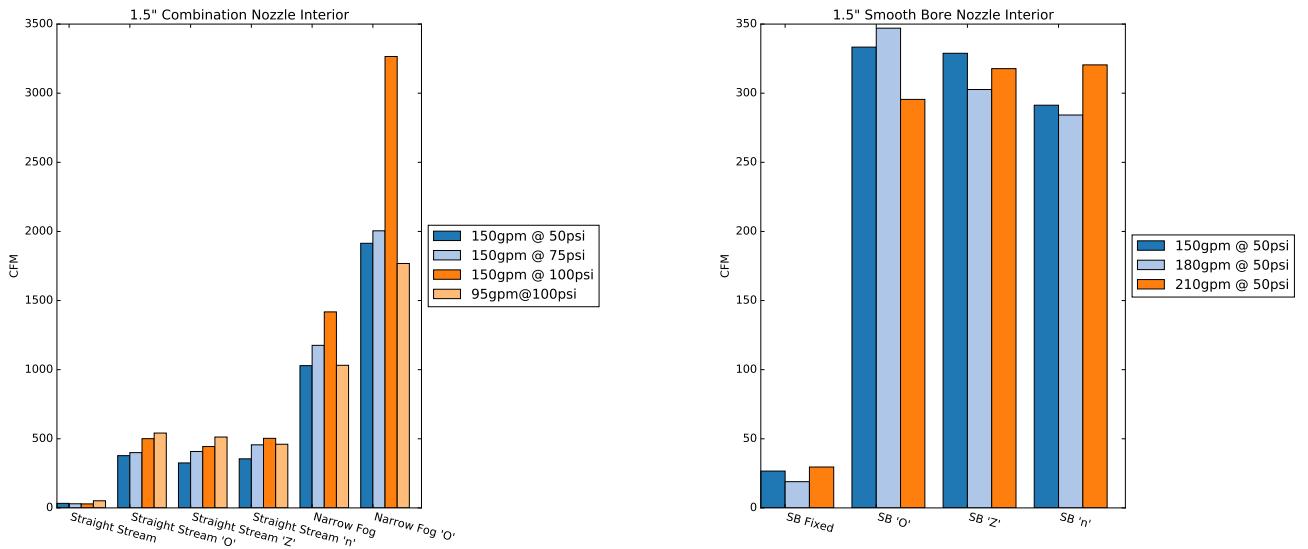


Figure A.3: Figures showing total interior air entrainment results for 1.5 in. nozzles

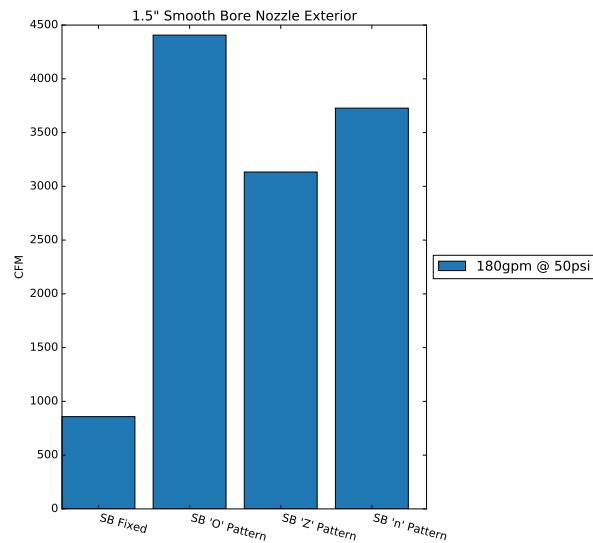


Figure A.4: Figure showing total exterior air entrainment results for 1.5 in. smooth bore nozzle

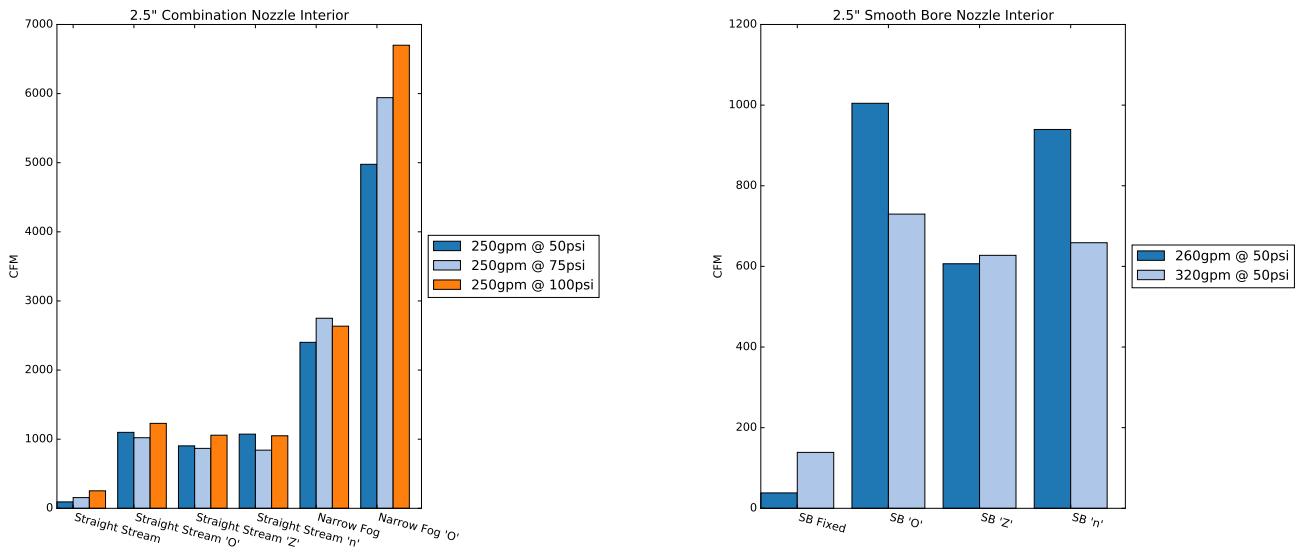


Figure A.5: Figures showing total interior air entrainment results for 2.5 in. nozzles

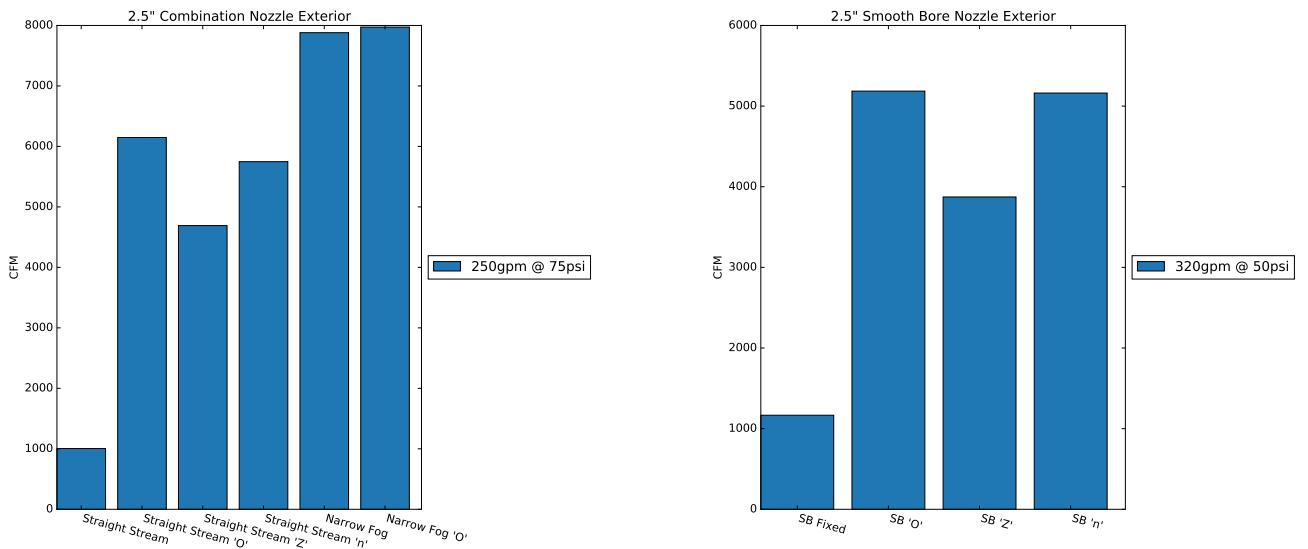


Figure A.6: Figures showing total exterior air entrainment results for 2.5 in. nozzles

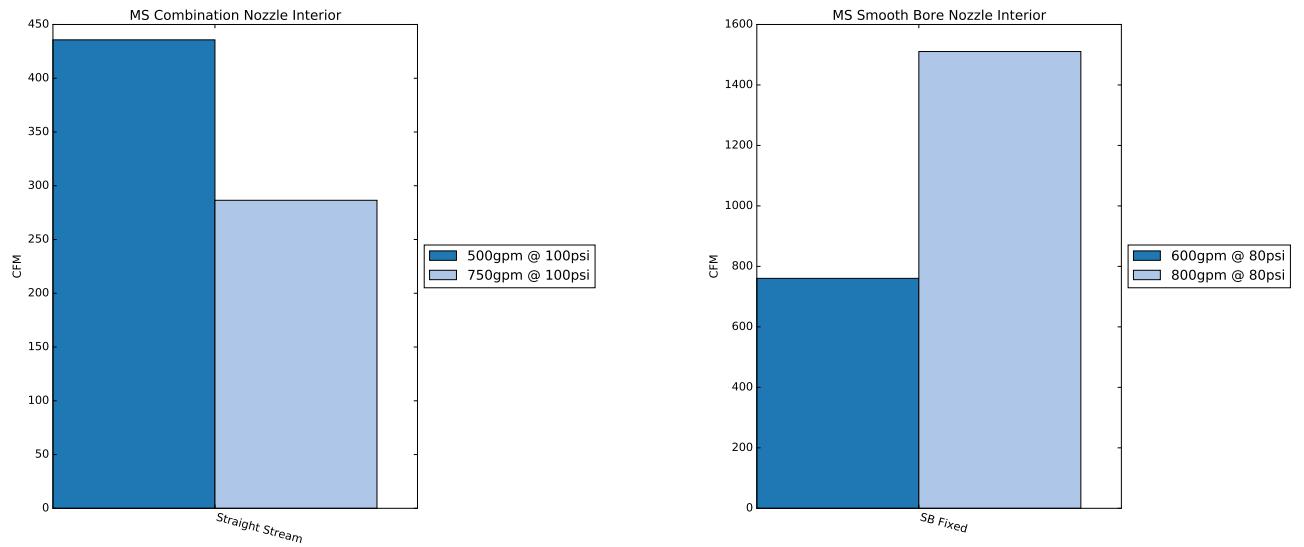


Figure A.7: Figures showing total interior air entrainment results for master stream nozzles

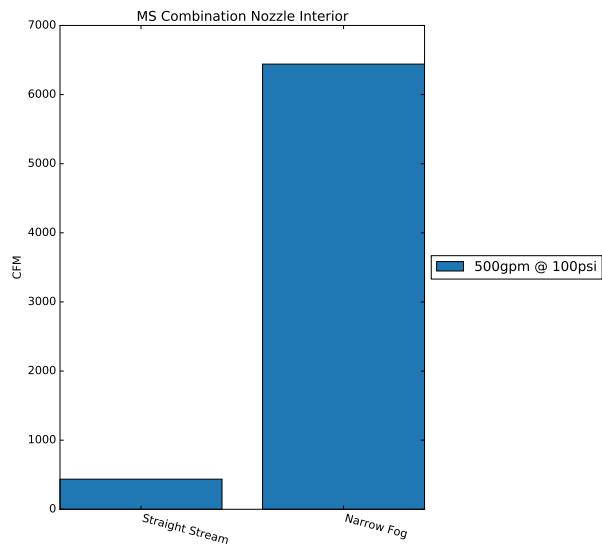


Figure A.8: Figure showing total interior air entrainment results for combination master stream nozzle

Portable Monitor Nozzle Type	Interior SS/SB	Interior Fog	Exterior SS/SB)
Combination Nozzle (500 gpm @ 75 psi)	11582 CFM	53919 CFM	26523 CFM
Smooth Bore Nozzle (1 3/8" tip, 500 gpm @ 80 psi)	6768 CFM	N/A	31572 CFM

Table A.1: Portable Monitor Entrainment Results

A.3 Ventilation Configuration

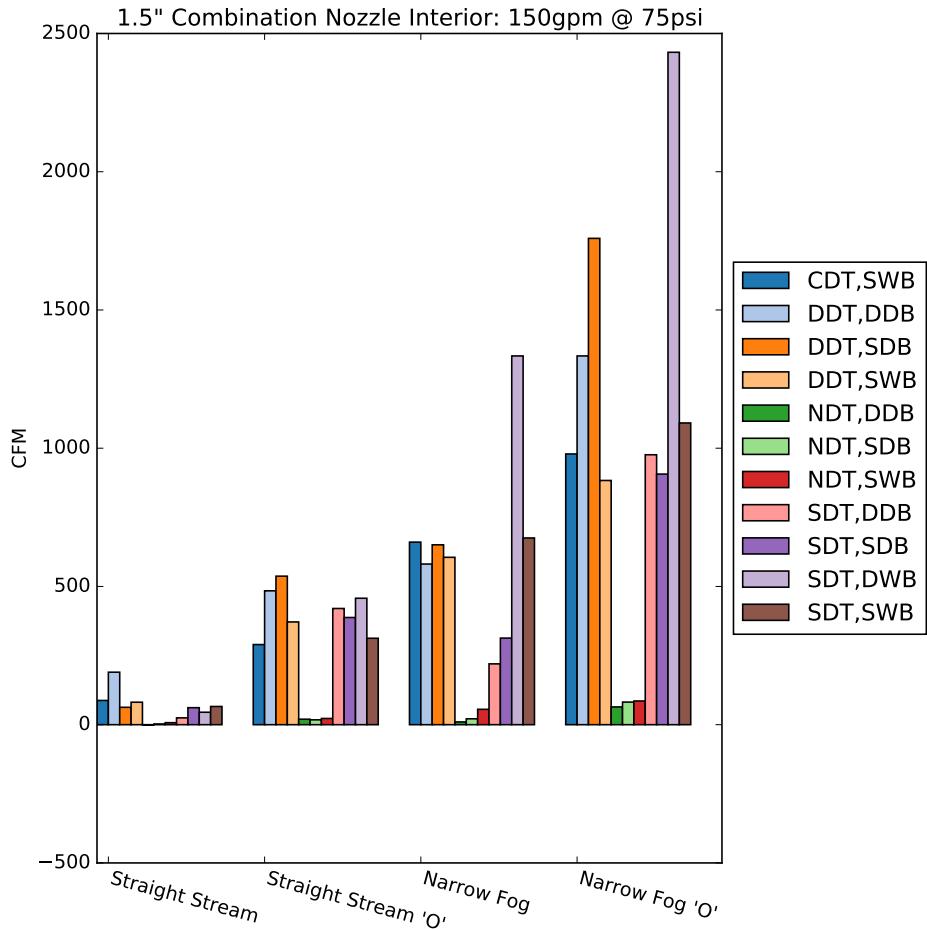


Figure A.9: Figure showing interior air entrainment results for varying vent configurations with a 1.5 in. combination nozzle

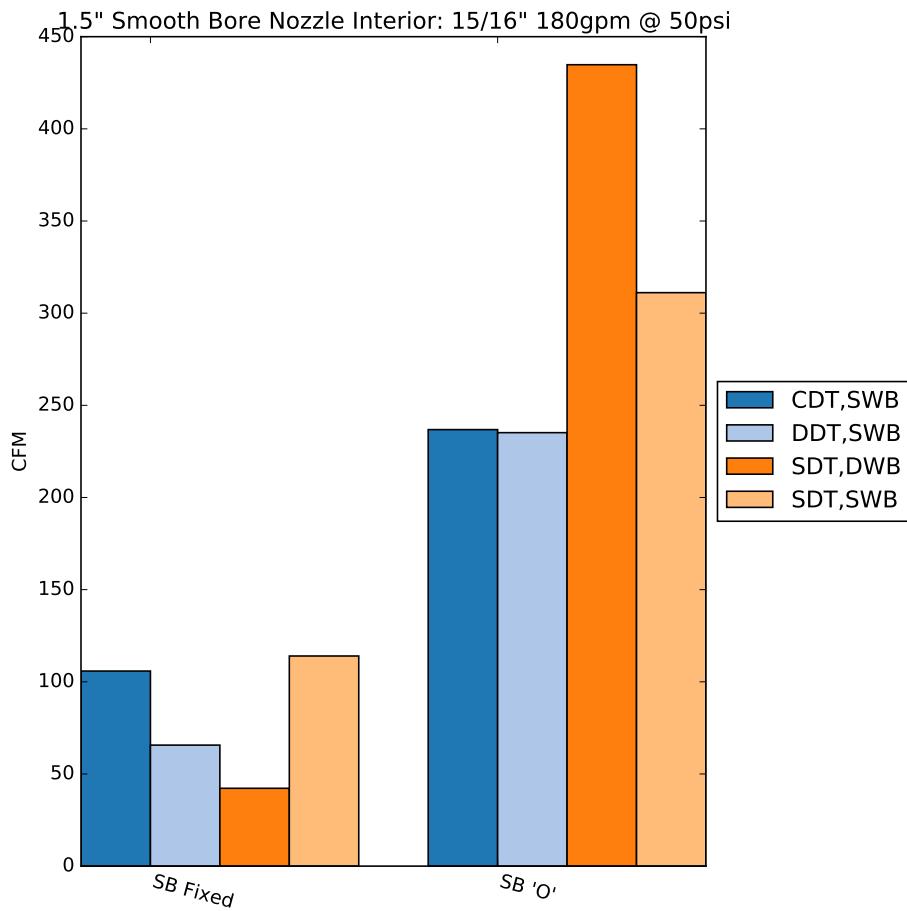


Figure A.10: Figure showing interior air entrainment results for varying vent configurations with a 1.5 in. smooth bore nozzle

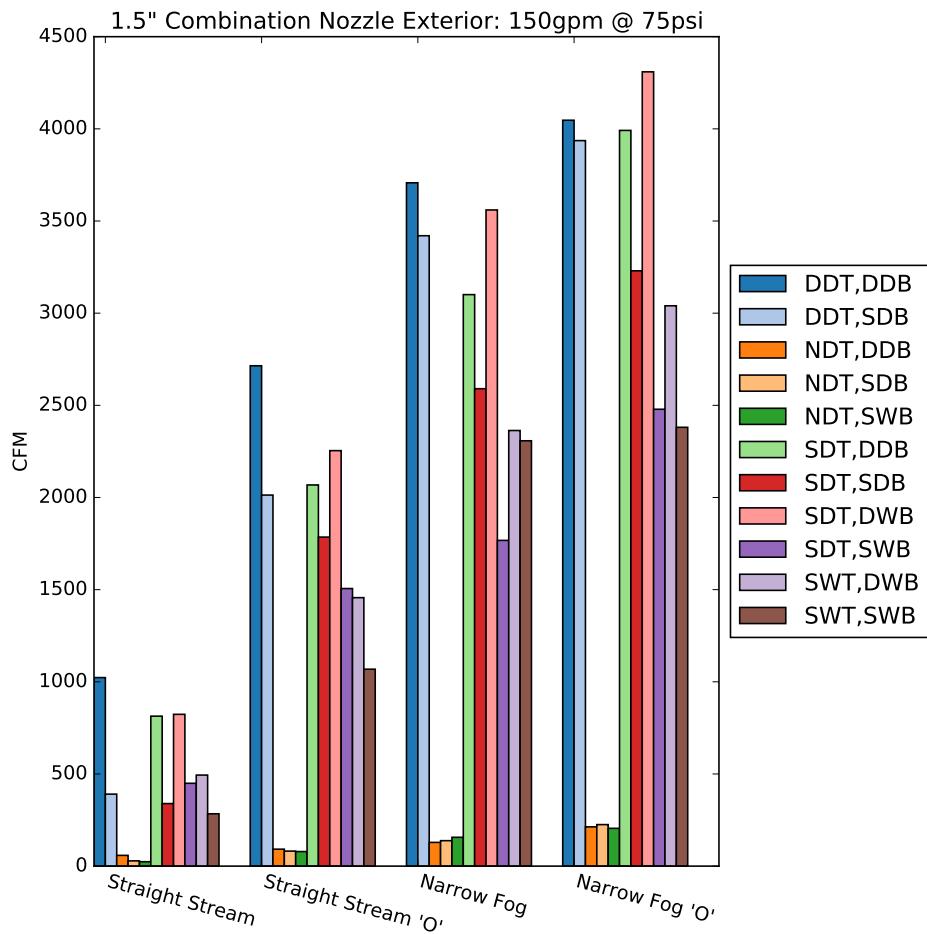


Figure A.11: Figure showing exterior air entrainment results for varying vent configurations with a 1.5 in. combination nozzle

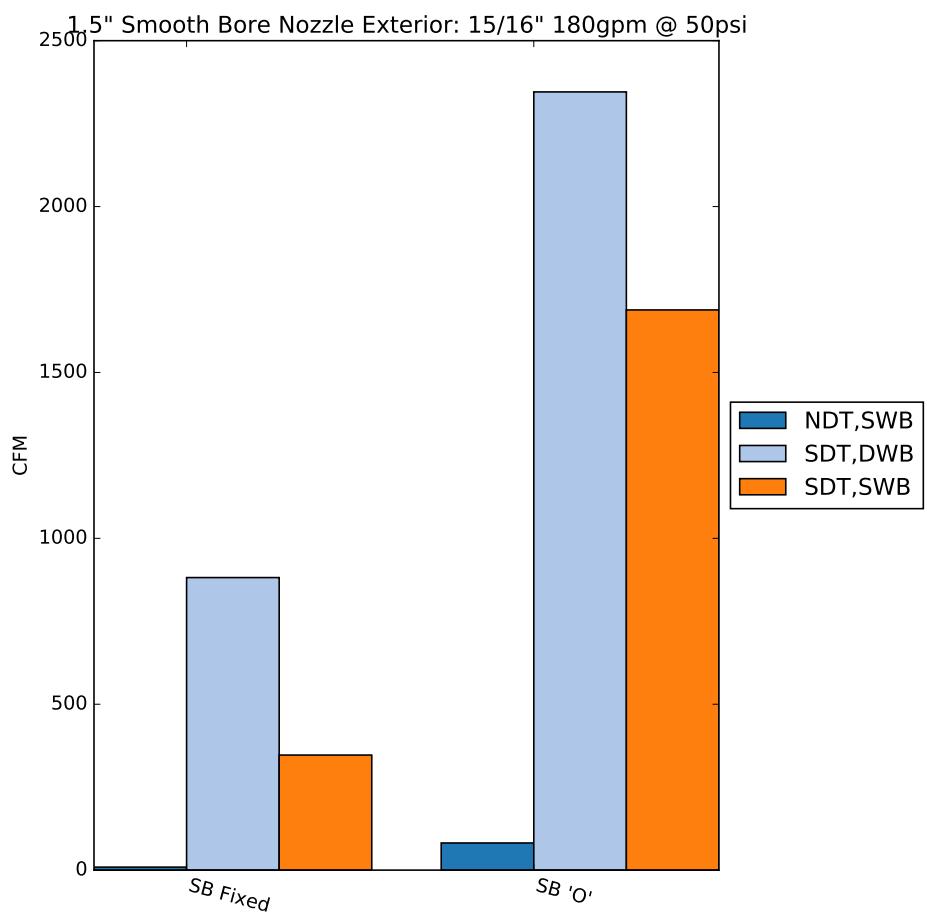


Figure A.12: Figure showing exterior air entrainment results for varying vent configurations with a 1.5 in. smooth bore nozzle

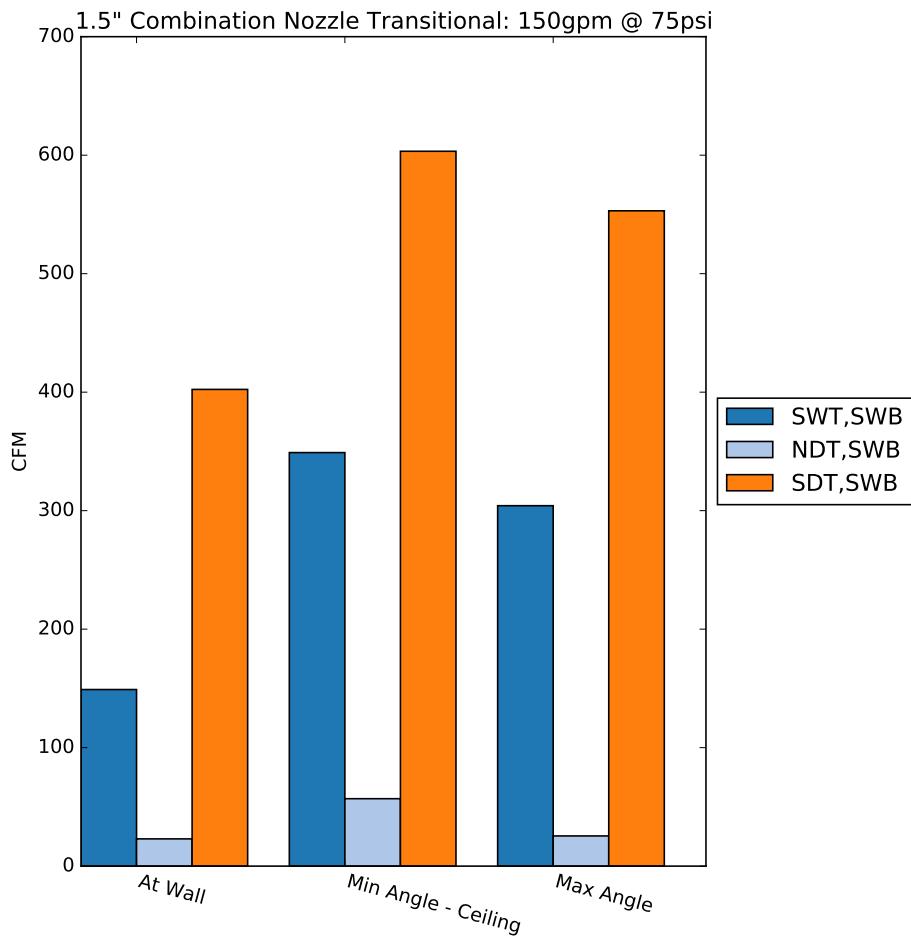


Figure A.13: Figure showing transitional air entrainment results for varying vent configurations with a 1.5 in. combination nozzle

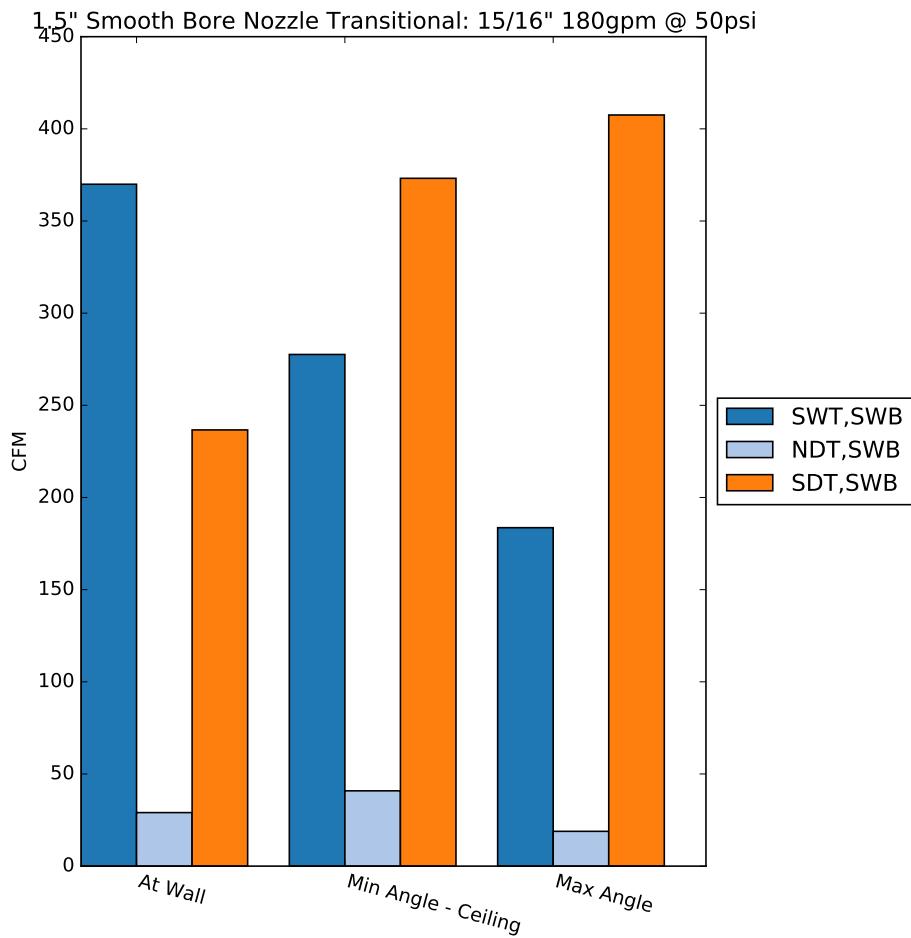


Figure A.14: Figure showing transitional air entrainment results for varying vent configurations with a 1.5 in. smooth bore nozzle

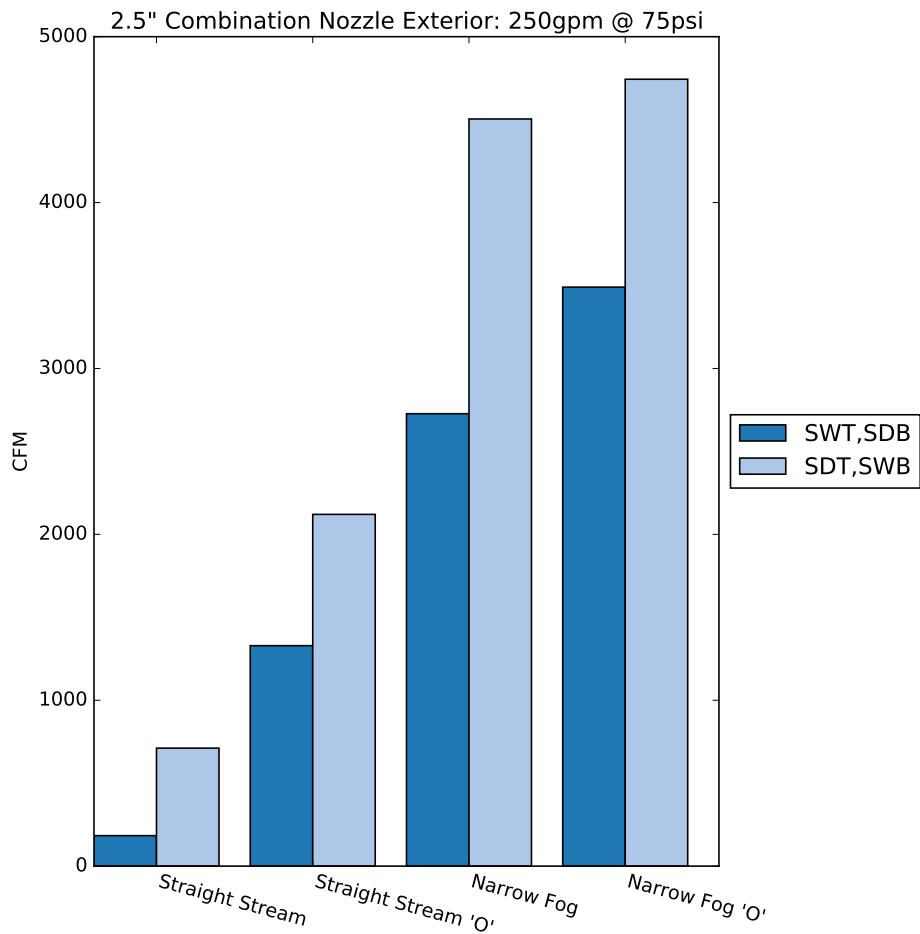


Figure A.15: Figure showing exterior air entrainment results for varying vent configurations with a 2.5 in. combination nozzle

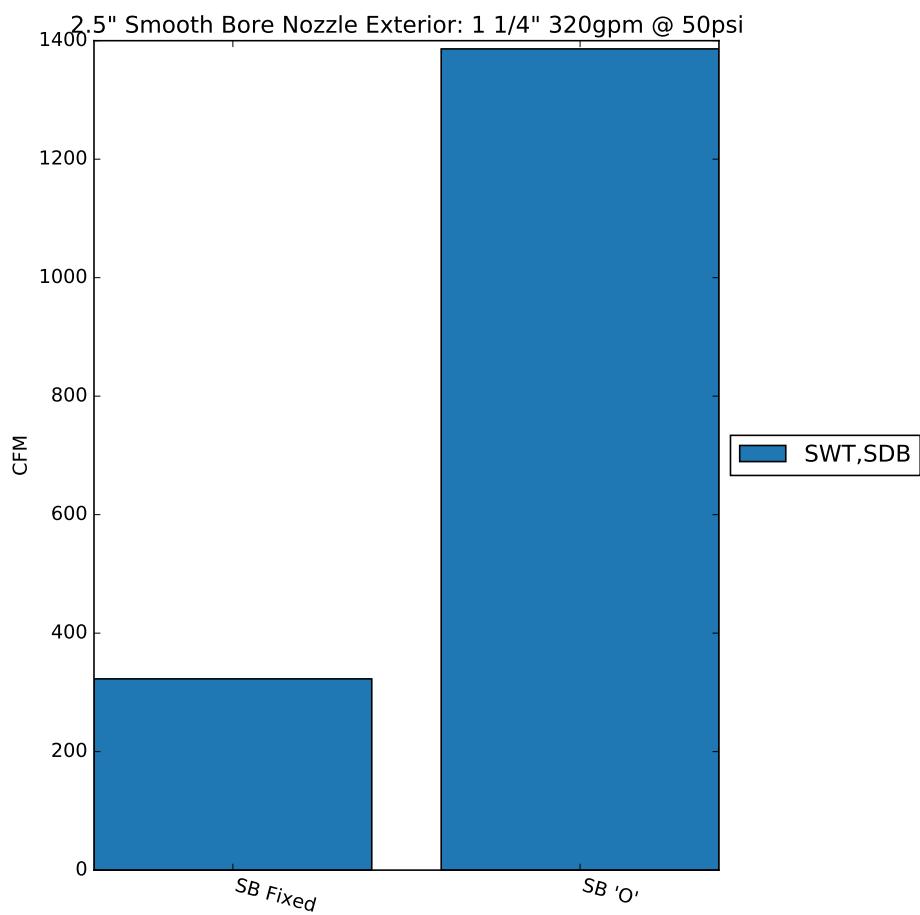


Figure A.16: Figure showing exterior air entrainment results for varying vent configurations with a 2.5 in. smooth bore nozzle

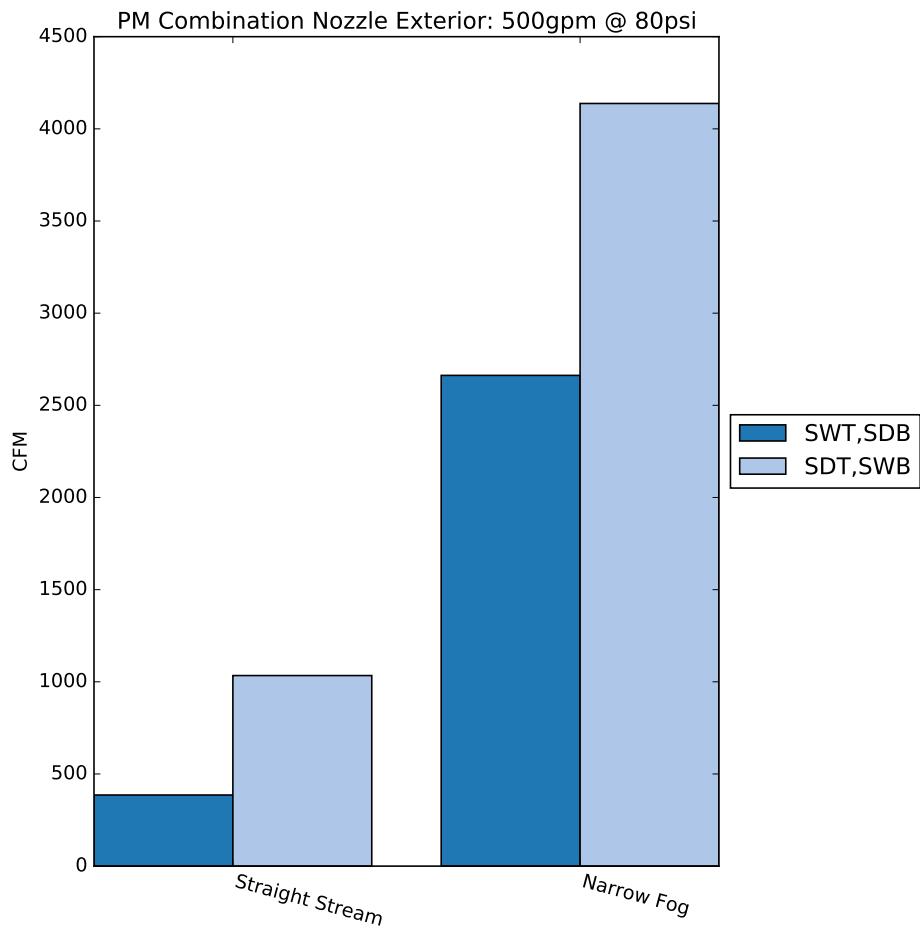


Figure A.17: Figure showing exterior air entrainment results for varying vent configurations with a portable monitor combination nozzle

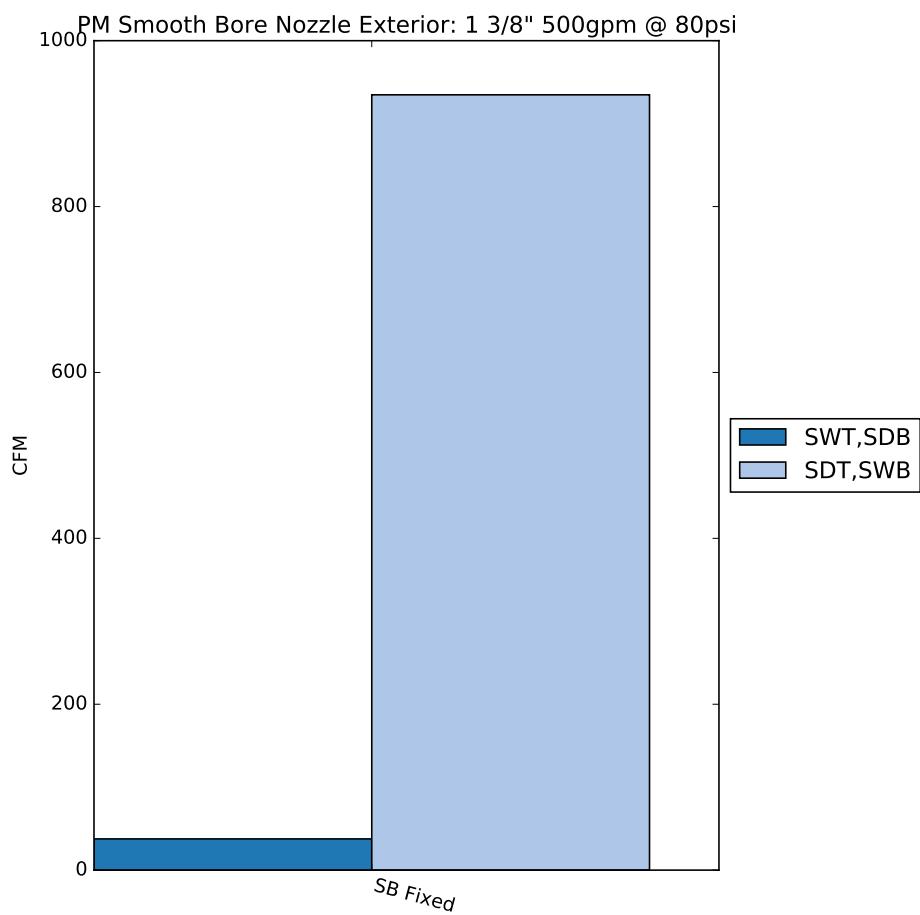


Figure A.18: Figure showing exterior air entrainment results for varying vent configurations with a portable monitor smooth bore nozzle

A.4 Room Configuration

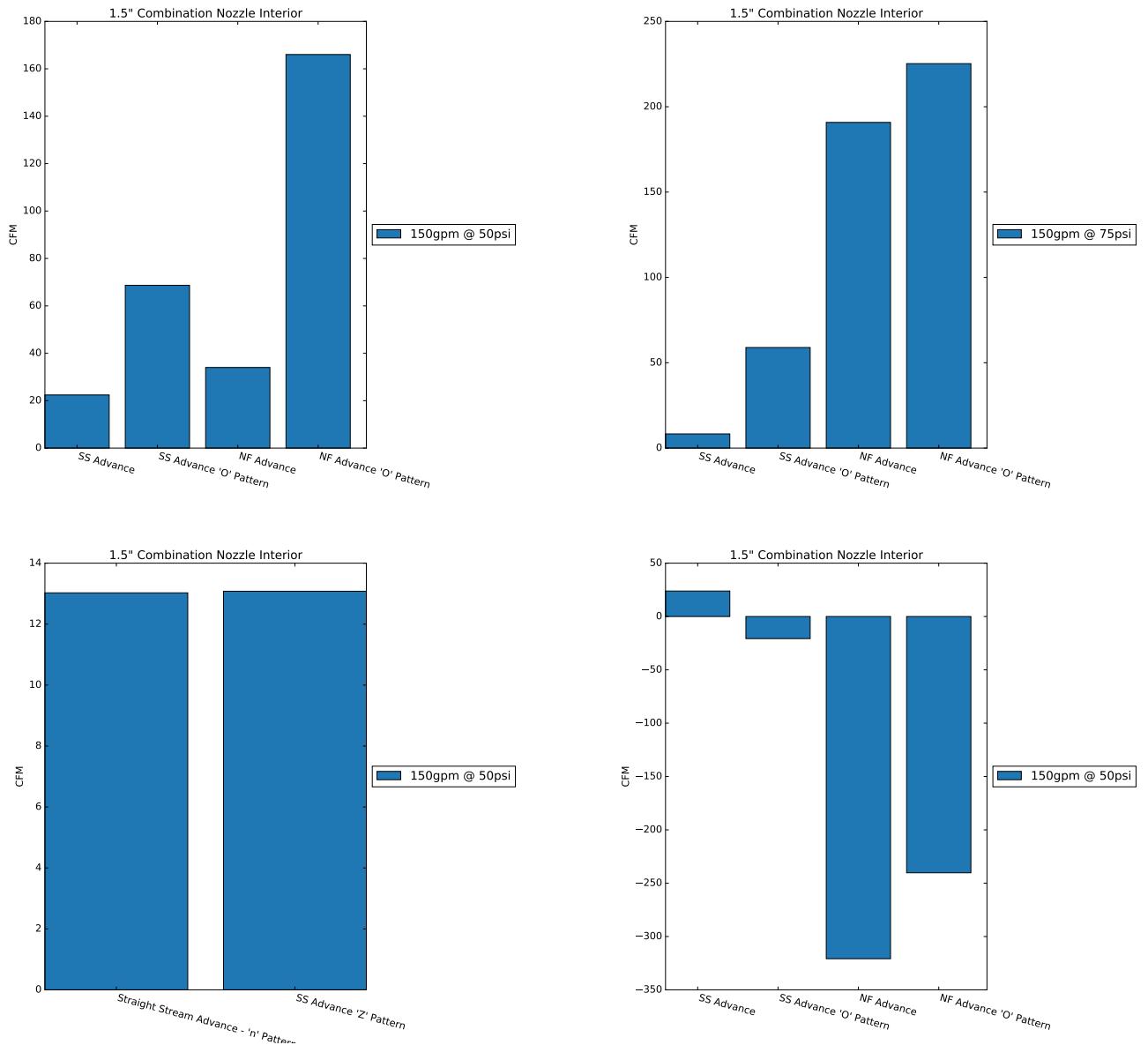


Figure A.19: Figures showing the interior air entrainment results for 1.5 in combination nozzles in the room configuration.

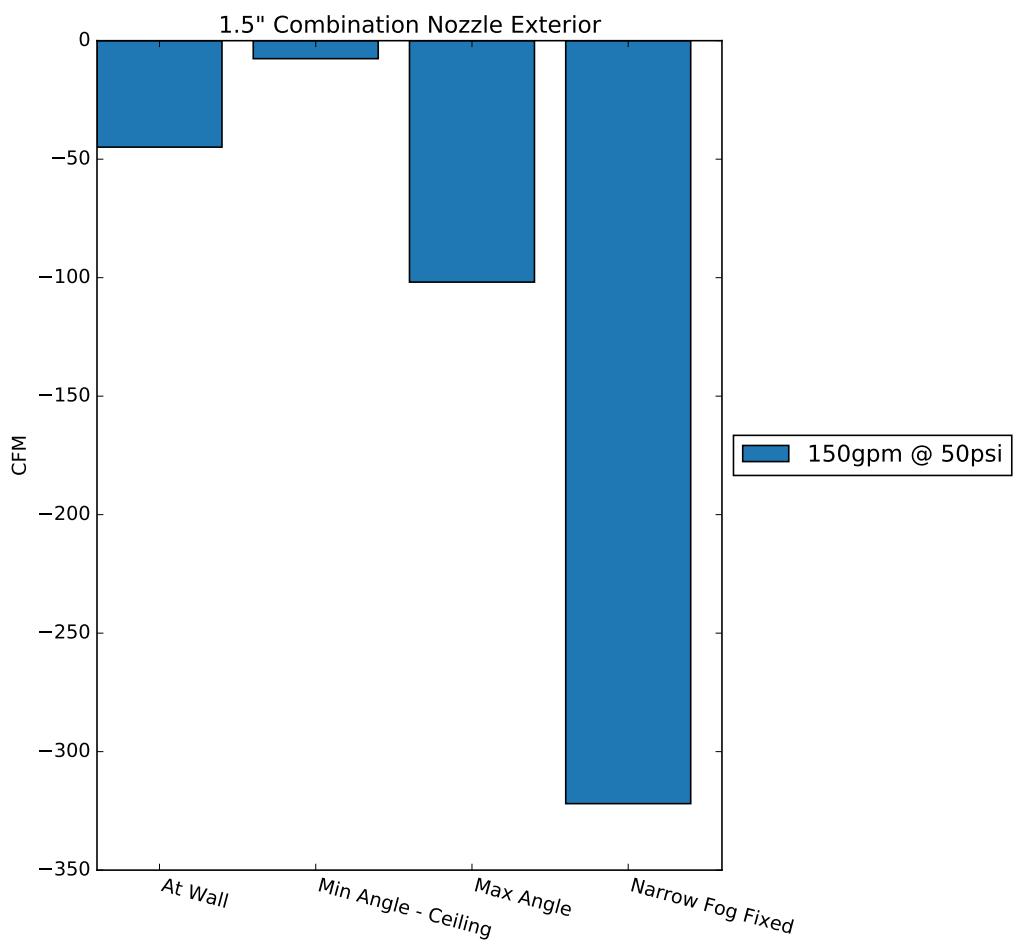


Figure A.20: Figure showing the exterior air entrainment results for 1.5 in. combination nozzles in the room configuration.

B Water Distribution Figures

B.1 Second Floor Exterior Tests

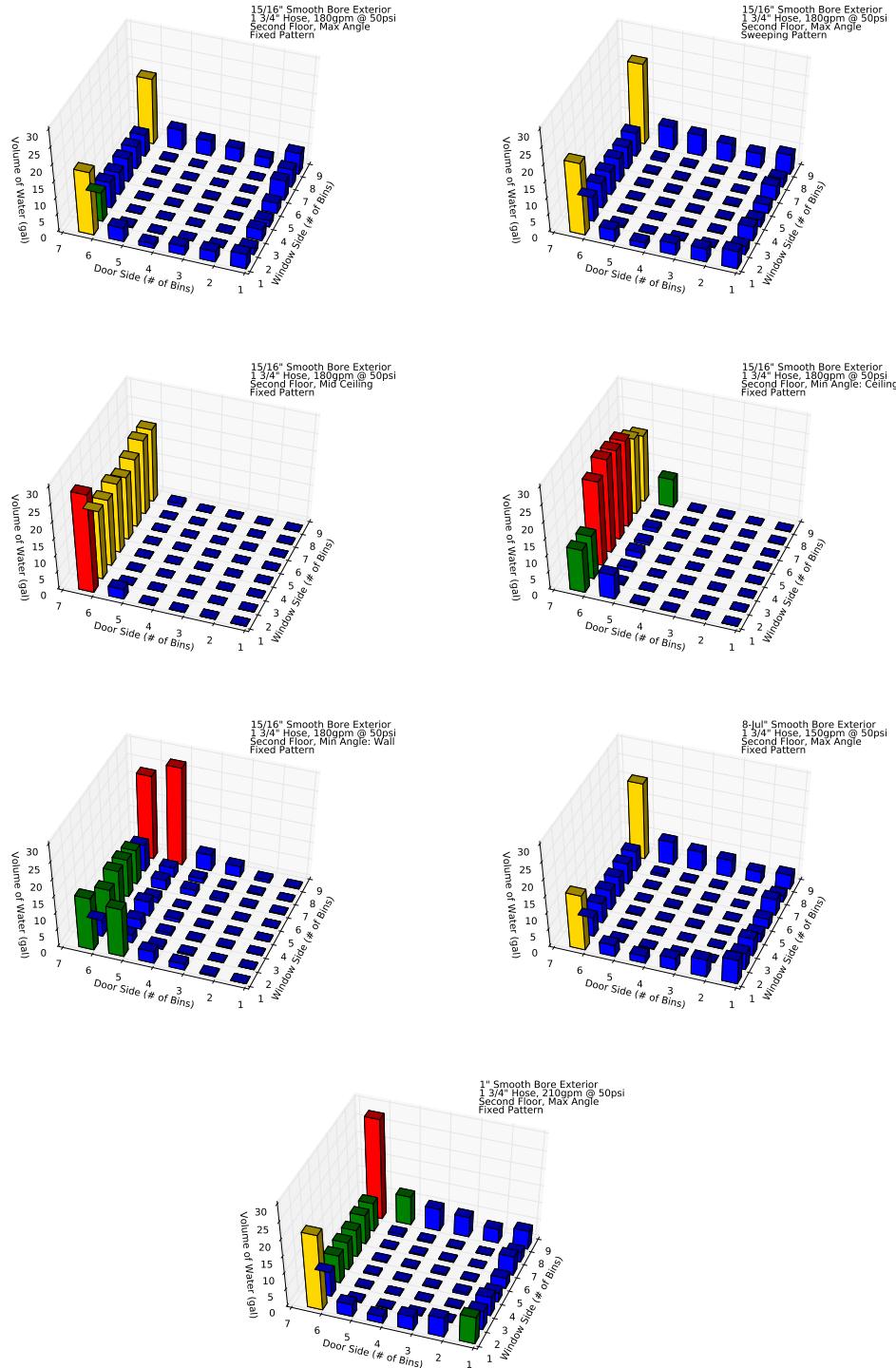


Figure B.1: Smooth Bore Second Floor Exterior

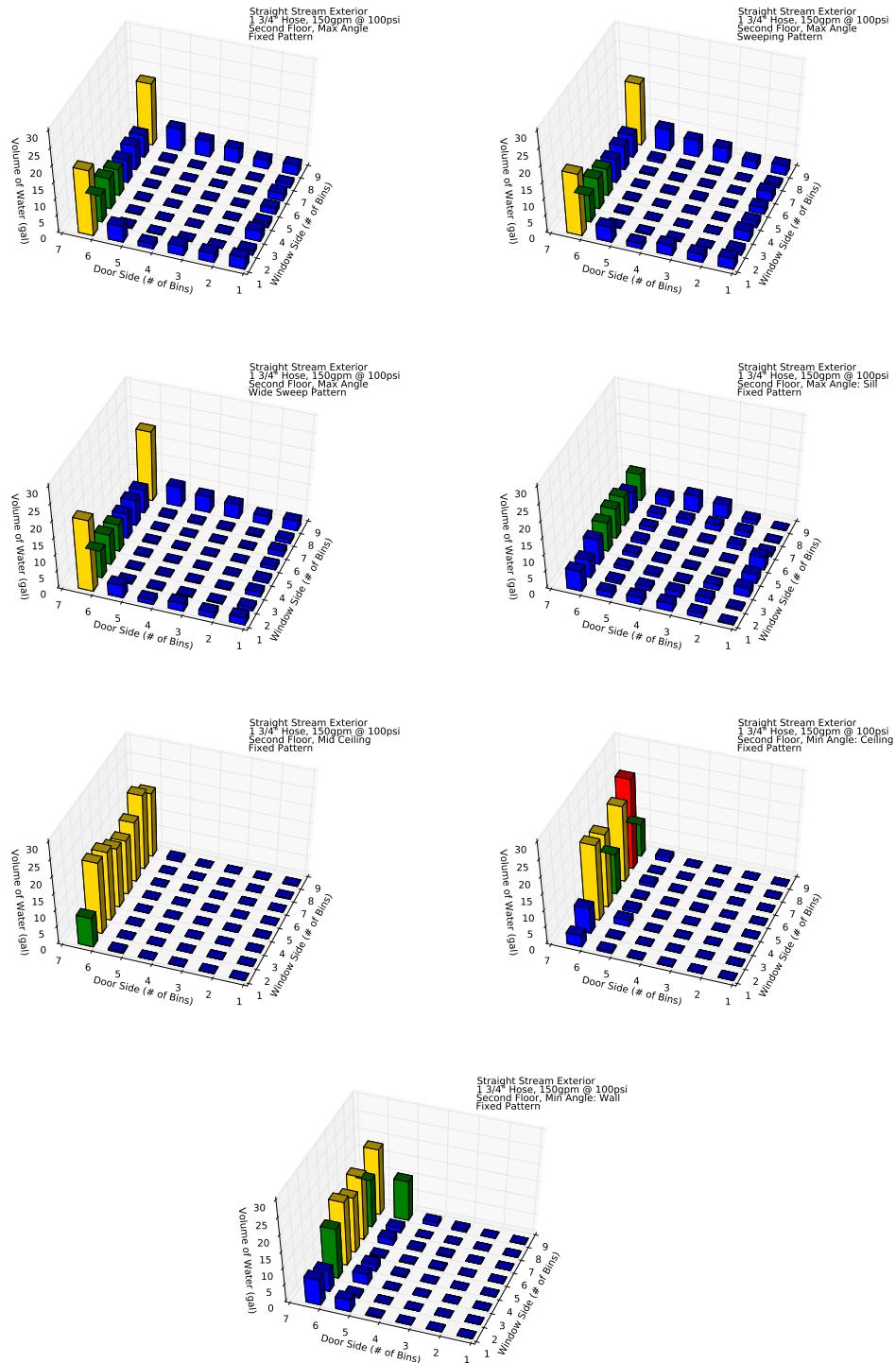


Figure B.2: Straight Stream Second Floor Exterior

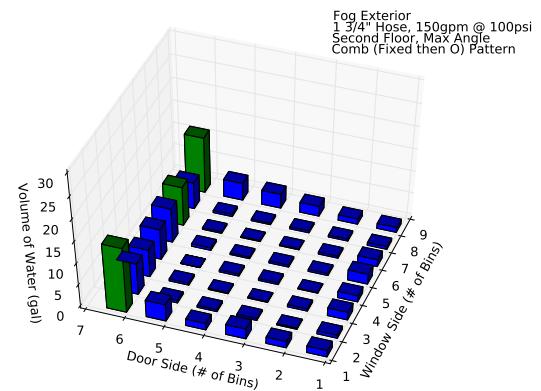
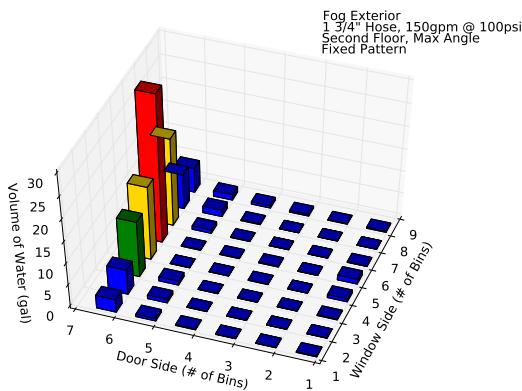


Figure B.3: Fog Stream Second Floor Exterior

B.2 First Floor Exterior Tests

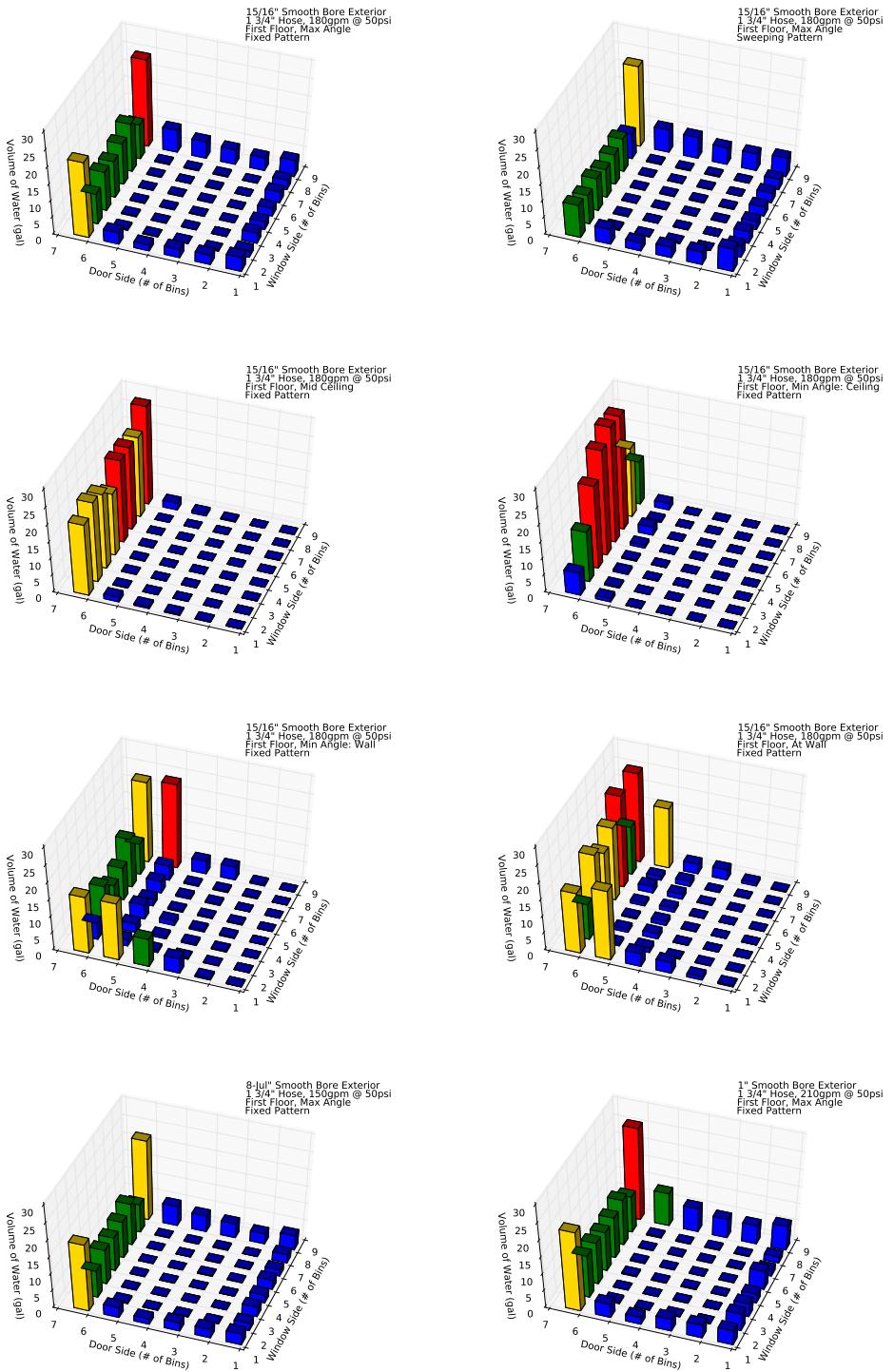


Figure B.4: Smooth Bore First Floor Exterior

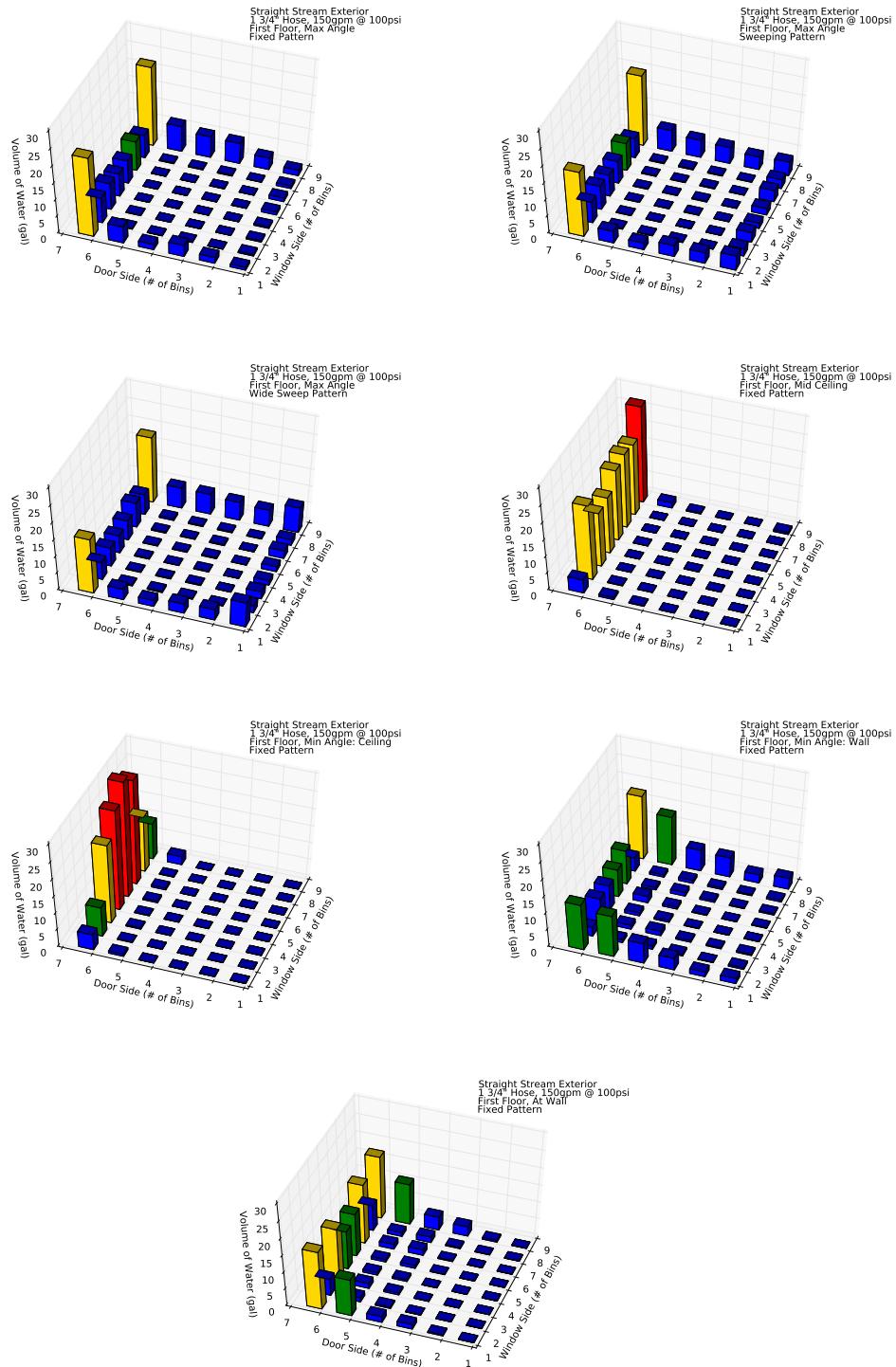


Figure B.5: Straight Stream First Floor Exterior

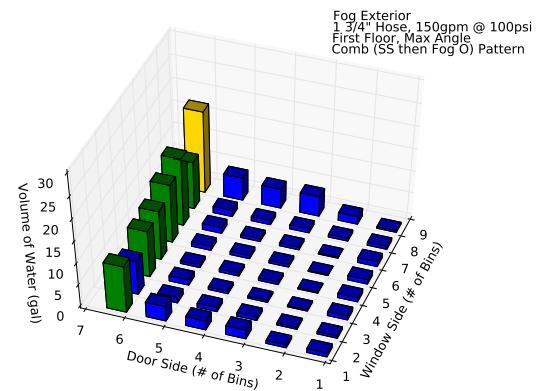
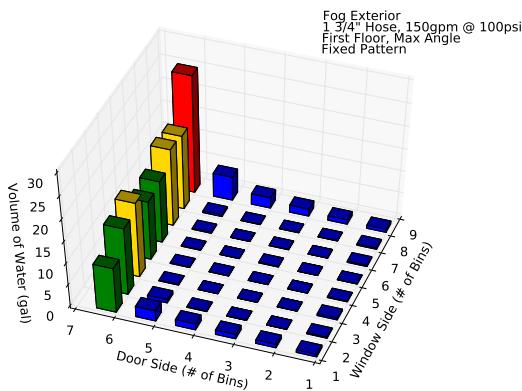


Figure B.6: Fog Stream First Floor Exterior

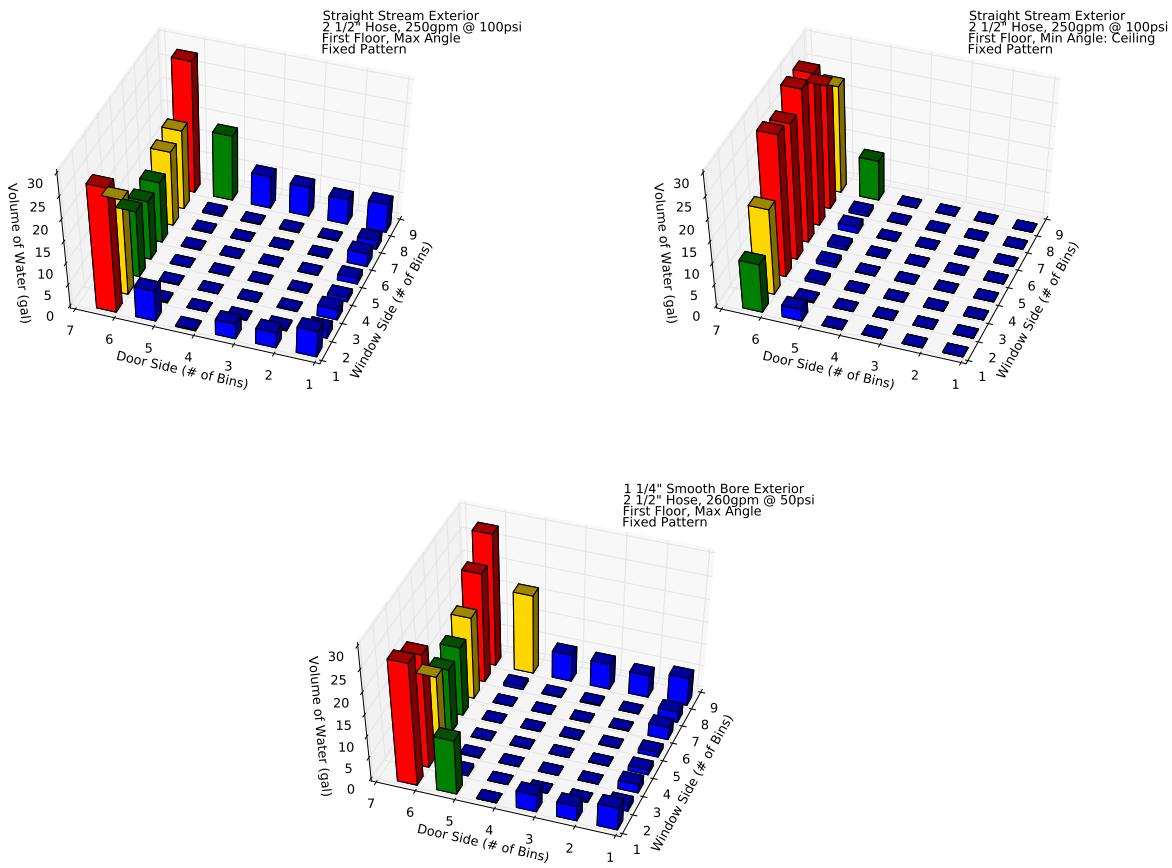


Figure B.7: Straight Stream vs. Smooth Bore, 2 1/2" Hose, First Floor, Exterior

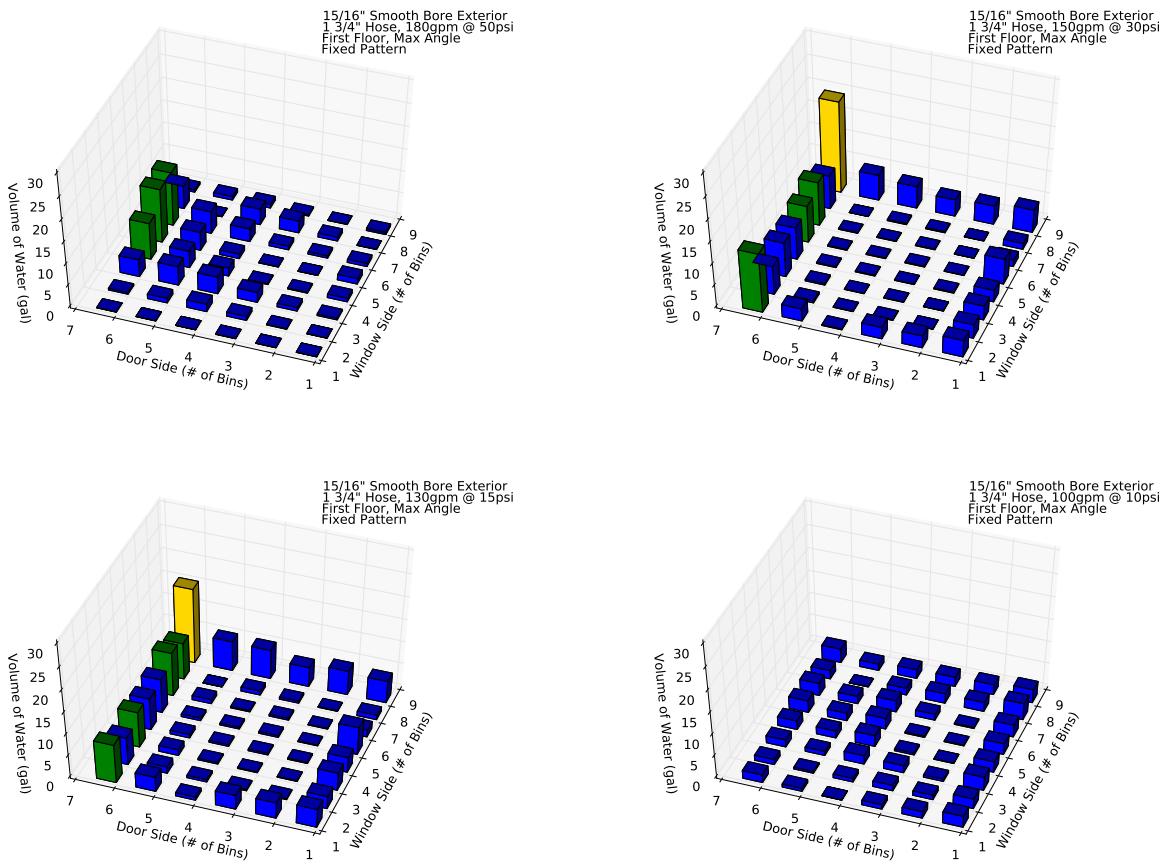


Figure B.8: Smooth Bore Adjusted Pressures/Varied Flow Rates, First Floor Exterior

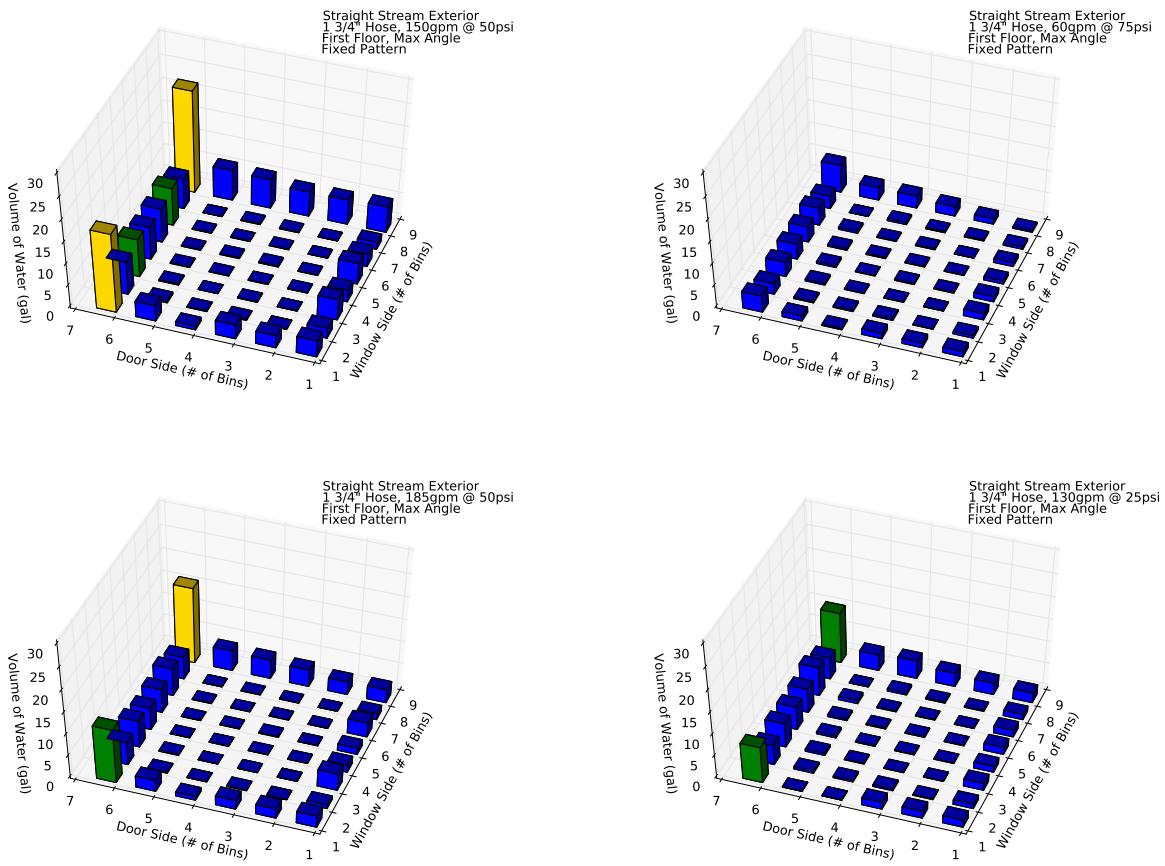


Figure B.9: Straight Stream Adjusted Pressures/Varied Flow Rates, First Floor Exterior

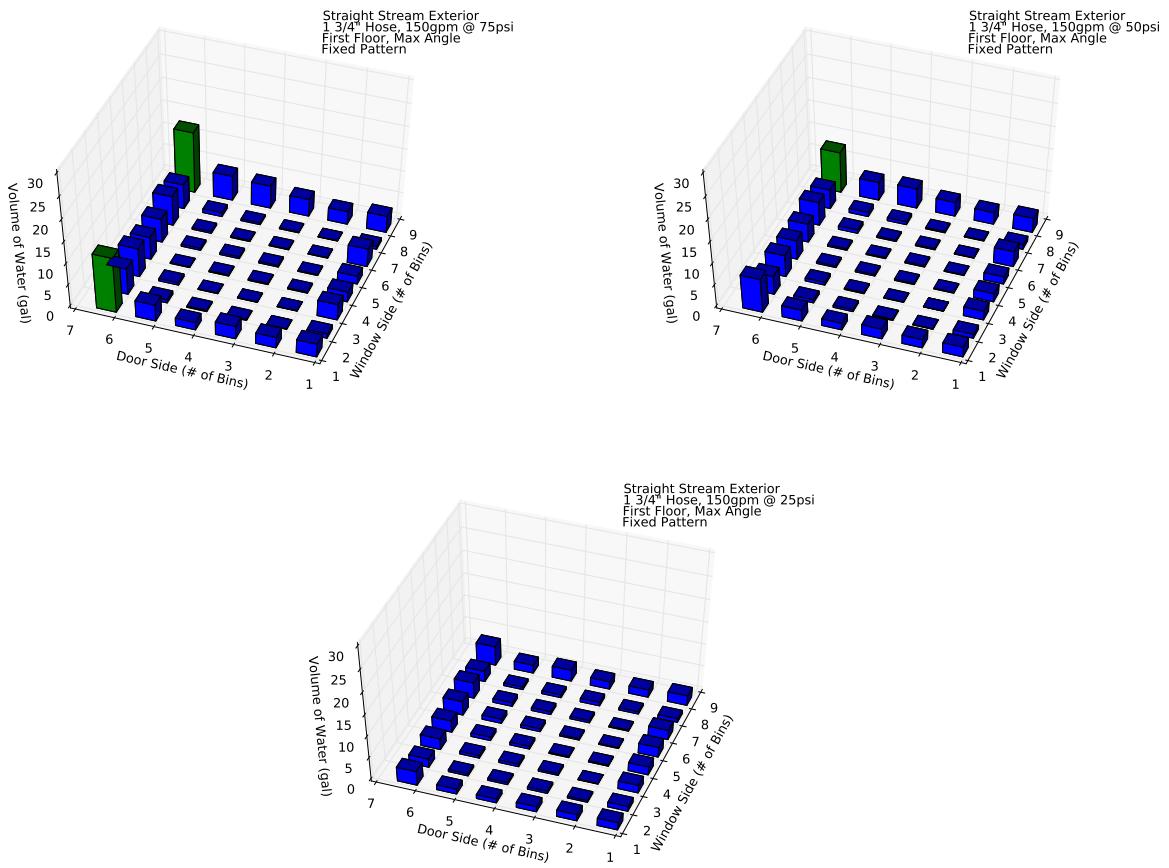


Figure B.10: Straight Stream Adjusted Pressures/Constant Flow Rates, First Floor Exterior

B.3 Interior Tests

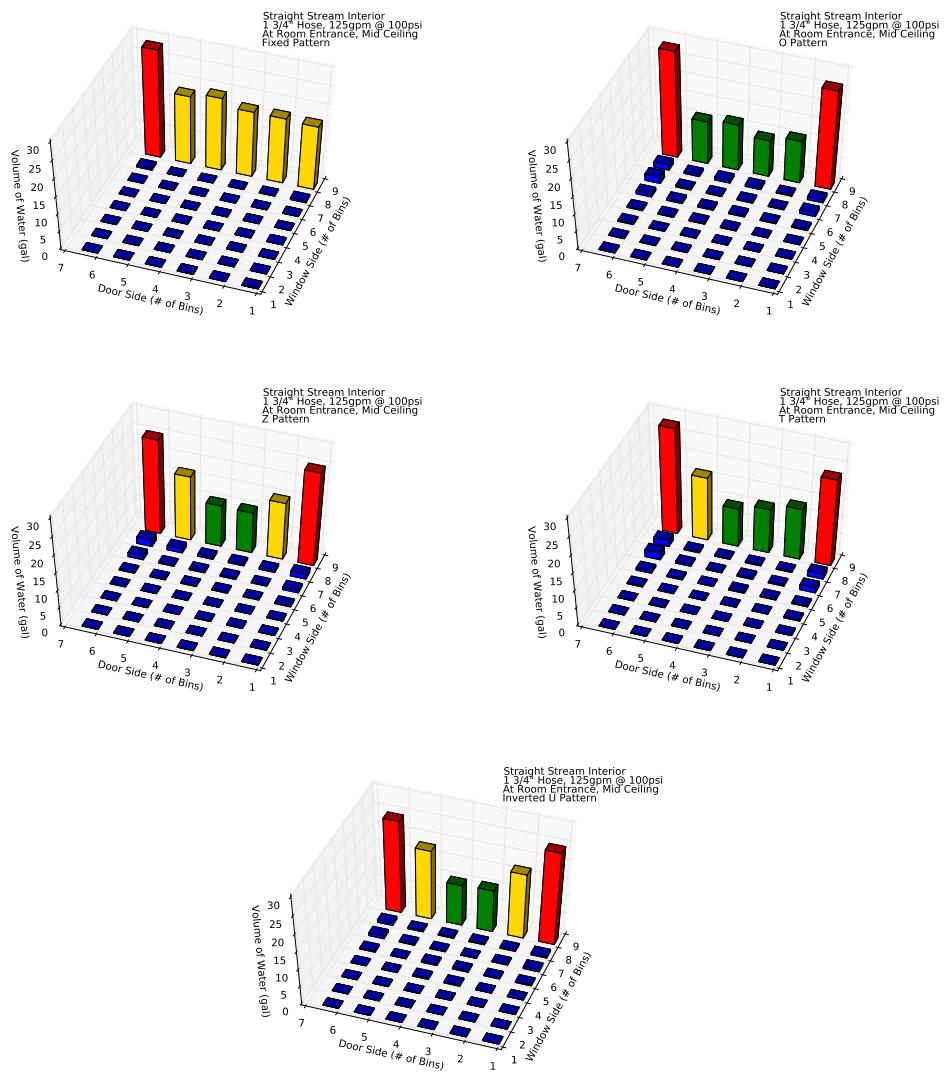


Figure B.11: Straight Stream Varied Nozzle Movements, First Floor Interior

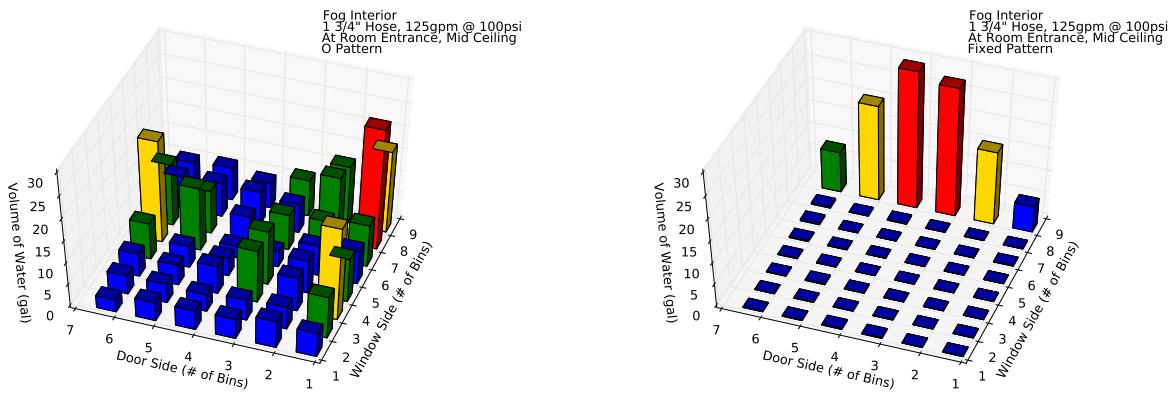


Figure B.12: Fog Stream Fixed vs. Moving, First Floor Interior

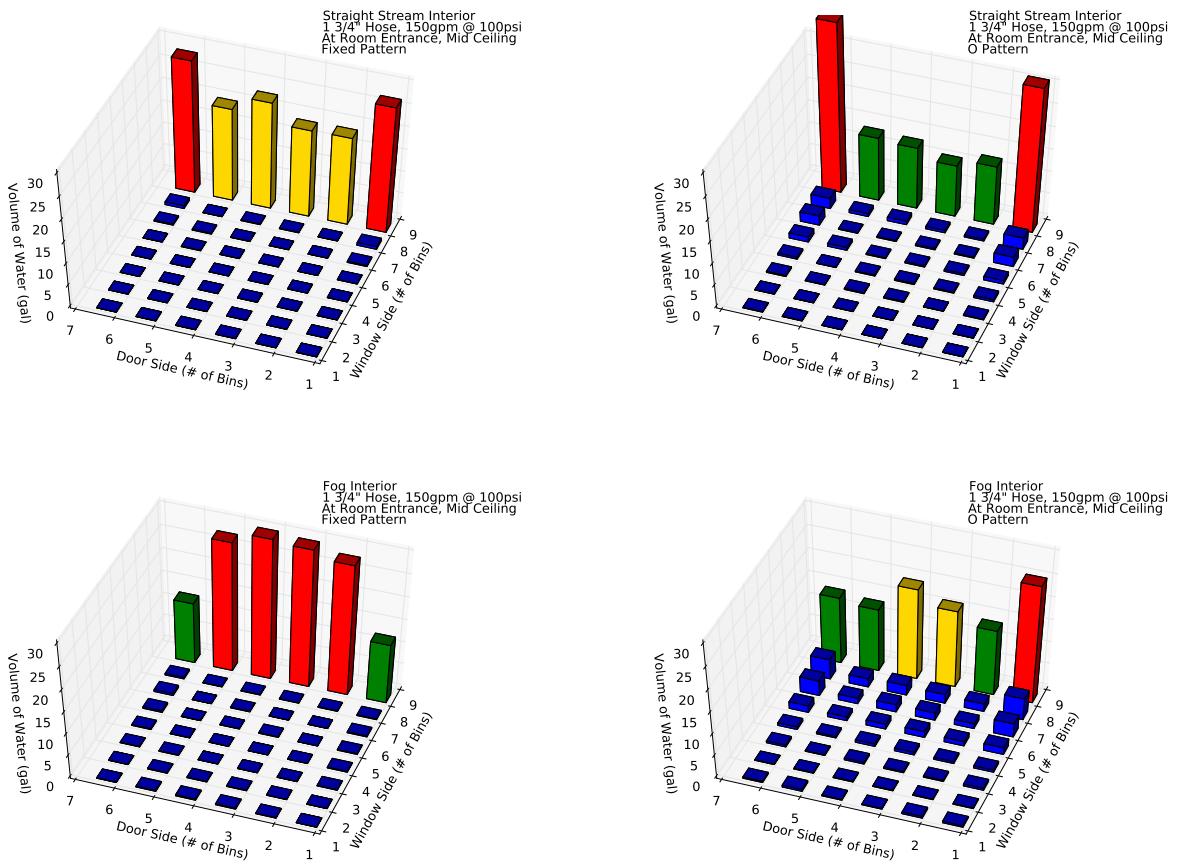


Figure B.13: Straight Stream vs. Fog 100 psi, First Floor Interior

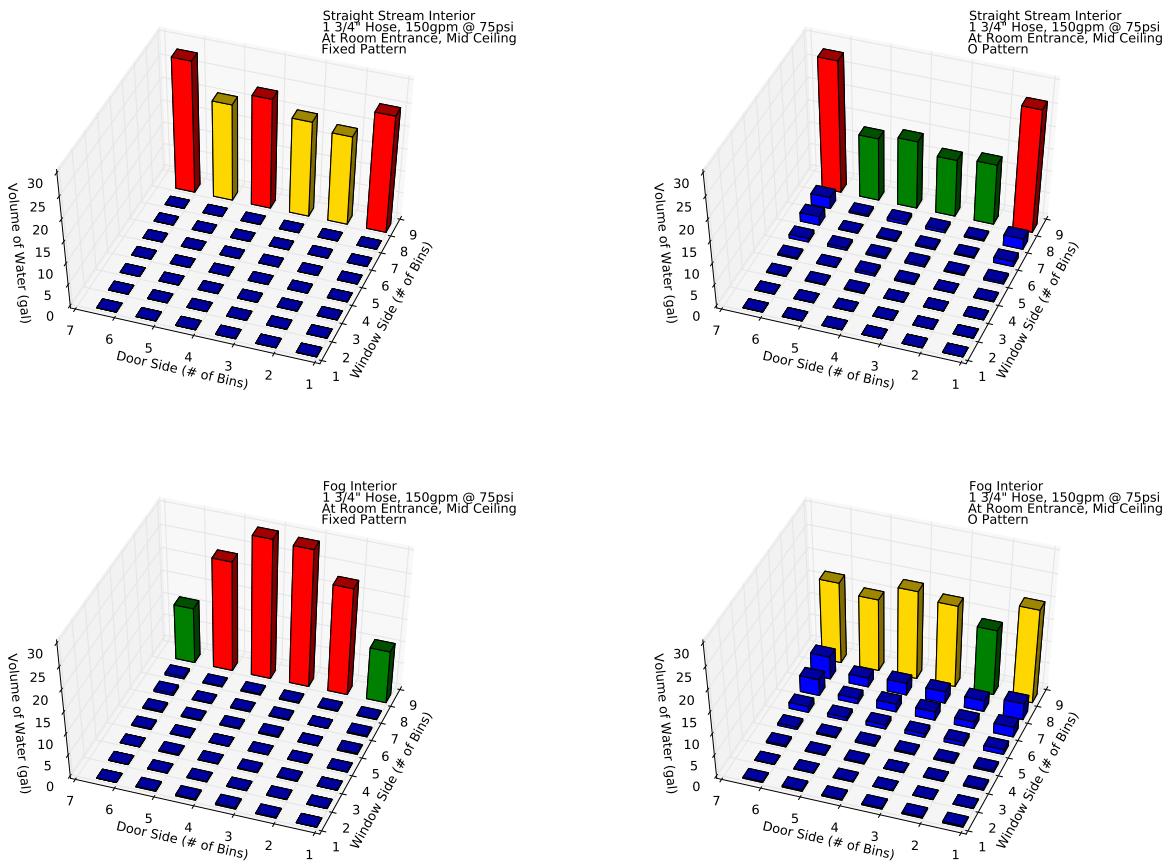


Figure B.14: Straight Stream vs. Fog 75 psi, First Floor Interior

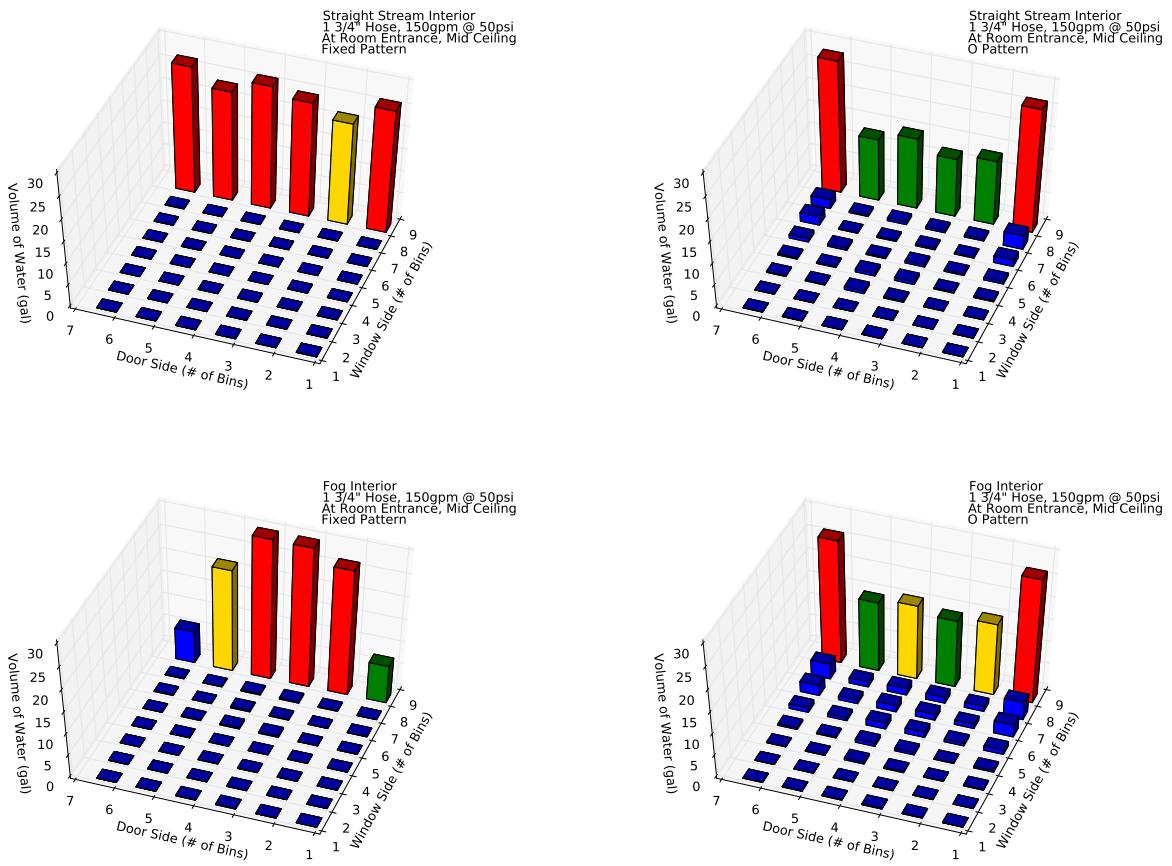


Figure B.15: Straight Stream vs. Fog 50 psi, First Floor Interior

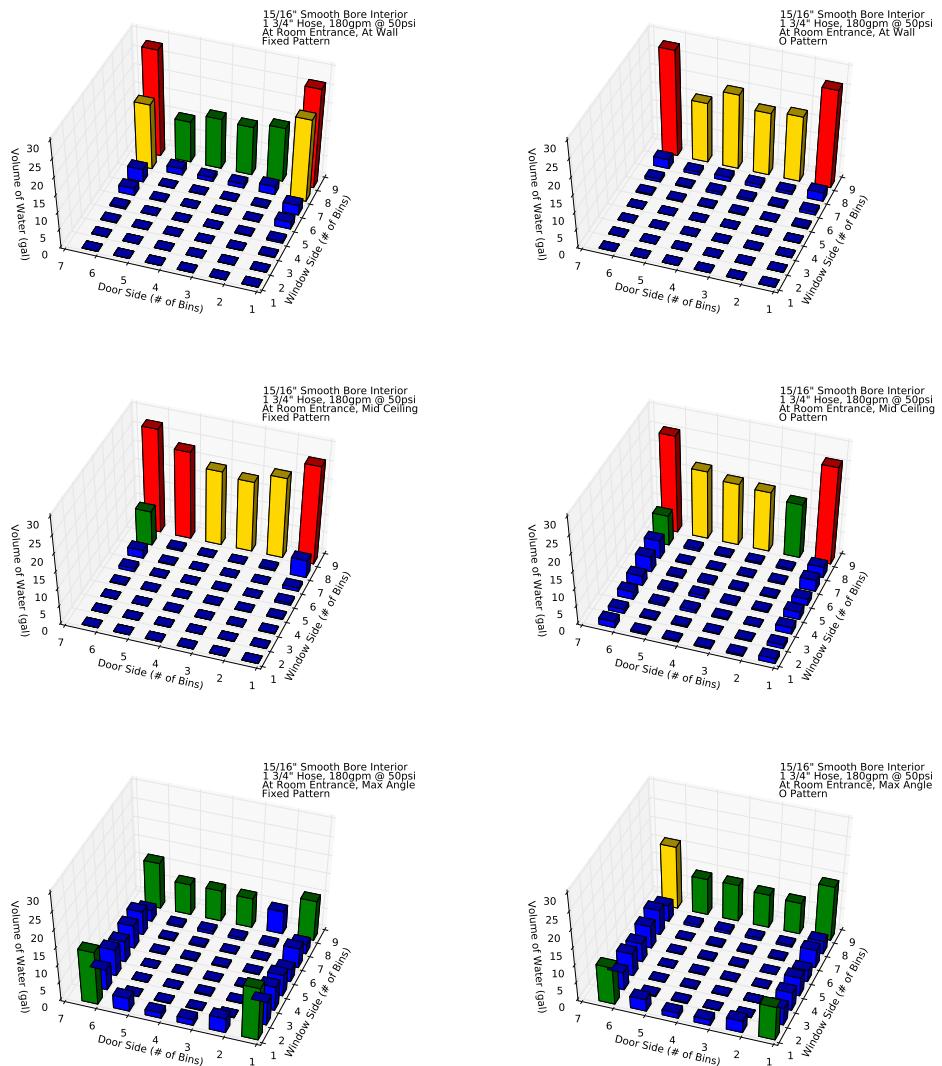


Figure B.16: Smooth Bore Varied Elevation Angle, First Floor Interior

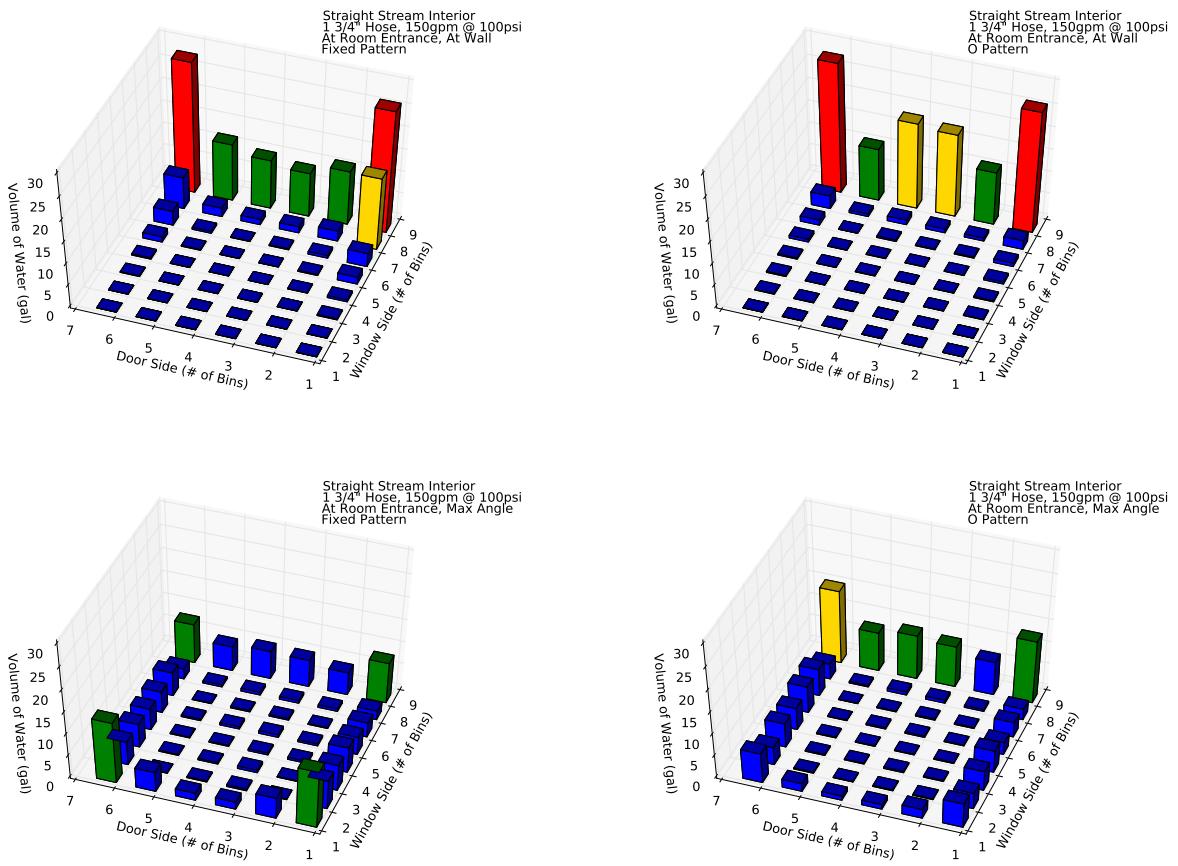


Figure B.17: Straight Stream Varied Elevation Angle, First Floor Interior