

Heating Circuit

Small heating circuits are used in many applications. For example, in manufacturing processes they heat up reactive fluids. Figure 1 illustrates a typical heating device for this model. The device consists of an electrically resistive layer deposited on a glass plate, which causes Joule heating when a voltage is applied to the circuit. The layer's properties determine the amount of heat produced.

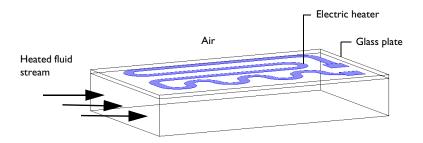


Figure 1: Geometry of a heating device.

In this particular model, you must observe three important design considerations:

- · Noninvasive heating
- Minimal deflection of the heating device
- Avoidance of overheating the process fluid

The heater must also work without failure. You achieve the first and second requirements by inserting a glass plate between the heating circuit and the fluid; it acts as a conducting separator. Glass is an ideal material for both of these purposes because it is nonreactive and has a low coefficient of thermal expansion.

You must also avoid overheating due to the risk of self-ignition of the reactive fluid stream. Ignition is also the main reason for separating the electrical circuit from direct contact with the fluid. The heating device is tailored for each application, making virtual prototyping very important for manufacturers.

For heating circuits in general, detachment of the resistive layer often determines the failure rate. This is caused by excessive thermally induced interfacial stresses. Once the layer is detached it gets locally overheated, which accelerates the detachment. Finally, in the worst case, the circuit might overheat and burn. From this perspective, it is also important to study the interfacial tension due to the differences in temperature as well as the different thermal-expansion coefficients of the resistive layer and the substrate. The geometric shape of the layer is a key parameter to design circuits for proper functioning. You can investigate all of the abovementioned aspects by modeling the circuit.

This multiphysics example simulates the electrical heat generation, the heat transfer, and the mechanical stresses and deformations of a heating circuit device. The model uses the Heat Transfer in Solids interface of the Heat Transfer Module in combination with the Electric Currents, Layered Shell interface from the AC/DC Module and the Solid Mechanics interface from the Structural Mechanics Module.

Note: This model requires the AC/DC Module, Heat Transfer Module, and Structural Mechanics Module.

Model Definition

Figure 2 shows a drawing of the modeled heating circuit.

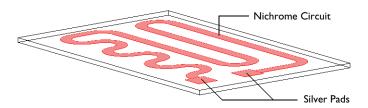


Figure 2: Drawing of the heating circuit deposited on a glass plate.

The device consists of a serpentine-shaped Nichrome resistive layer, $10~\mu m$ thick and 5 mm wide, deposited on a glass plate. At each end, it has a silver contact pad measuring 10~mm-by-10~mm-by- $10~\mu m$. When the circuit is in use, the deposited side of the glass plate is in contact with surrounding air, and the back side is in contact with the heated fluid. Assume that the edges and sides of the glass plate are thermally insulated.

Table 1 gives the resistor's dimensions.

TABLE I: DIMENSIONS.

ОВЈЕСТ	LENGTH	WIDTH	THICKNESS
Glass Plate	130 mm	80 mm	2 mm
Pads and Circuit	-	-	10 μm

During operation the resistive layer produces heat. Model the electrically generated heat using the Electric Currents, Layered Shell interface from the AC/DC Module. An electric potential of 12 V is applied to the pads. In the model, you achieve this effect by setting the potential at one edge of the first pad to 12 V and that of one edge of the other pad to 0 V.

To model the heat transfer in the thin conducting layer, use the Thin Layer feature from the Heat Transfer in Solids interface. The heat rate per unit area (measured in W/m^2) produced inside the thin layer is given by

$$q_{\text{prod}} = dQ_{\text{DC}}$$
 (1)

where $Q_{DC} = \mathbf{J} \cdot \mathbf{E} = \sigma |\nabla_t V|^2 (W/m^3)$ is the power density. The generated heat appears as an inward heat flux at the surface of the glass plate.

At steady state, the resistive layer dissipates the heat it generates in two ways: on its up side to the surrounding air (at 293 K), and on its down side to the glass plate. The glass plate is similarly cooled in two ways: on its circuit side by air, and on its back side by a process fluid (353 K). You model the heat fluxes to the surroundings using heat transfer coefficients, h. For the heat transfer to air, $h = 5 \text{ W/(m}^2 \cdot \text{K)}$, representing natural convection. On the glass plate's back side, $h = 20 \text{ W/(m}^2 \cdot \text{K)}$, representing convective heat transfer to the fluid. The sides of the glass plate are insulated.

The model simulates thermal expansion using static structural-mechanics analyses. It uses the Solid Mechanics interface for both the glass plate and the circuit layer. The stresses in the circuit layer are modeled using a thin layer approximation by adding a Thin Layer feature. The equations of these two interfaces are described in the Structural Mechanics Module User's Guide. The stresses are set to zero at 293 K. The displacements in the Solid Mechanics interface are constrained in such a way that the plate can freely deform while its rigid body motions are suppressed through appropriate constraints.

Table 2 summarizes the material properties used in the model.

TABLE 2: MATERIAL PROPERTIES.

MATERIAL	E [GPa]	ν	α [I/K]	k [W/(m·K)]	ρ [kg/m ³]	C_p [J/(kg·K)]
Silver	83	0.37	1.89e-5	420	10500	230
Nichrome	213	0.33	le-5	15	9000	20
Glass	73.I	0.17	5.5e-7	1.38	2203	703

Results and Discussion

Figure 3 shows the heat that the resistive layer generates.

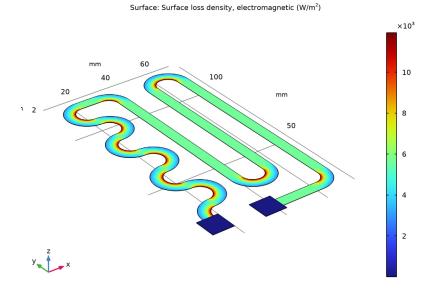


Figure 3: Stationary heat generation in the resistive layer when 12 V is applied.

The highest heating power occurs at the inner corners of the curves due to the higher current density at these spots. The total generated heat, as calculated by integration, is approximately 13.8 W.

Figure 4 shows the temperature of the resistive layer and the glass plate at steady state.

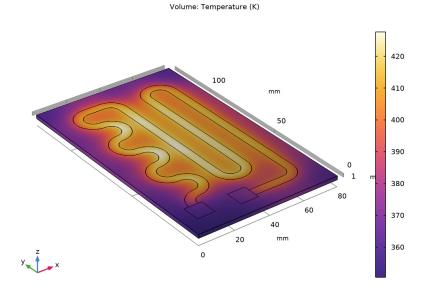


Figure 4: Temperature distribution in the heating device at steady state.

The highest temperature is approximately 428 K, and it appears in the central section of the circuit layer. It is interesting to see that the differences in temperature between the fluid side and the circuit side of the glass plate are quite small because the plate is very thin. Using boundary integration, the integral heat flux on the fluid side evaluates to approximately 8.5 W. This means that the device transfers the majority of the heat it generates — 8.5 W out of 13.8 W — to the fluid, which is good from a design perspective, although the thermal resistance of the glass plate results in some losses.

The temperature rise also induces thermal stresses due the materials' different coefficients of thermal expansion. As a result, mechanical stresses and deformations arise in the layer

and in the glass plate. Figure 5 shows the equivalent stress distribution in the device and the resulting deformations. During operation, the glass plate bends toward the air side.

Volume: von Mises stress (MPa)

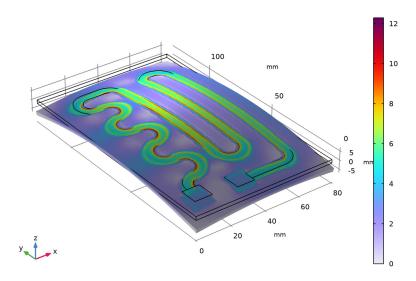


Figure 5: The thermally induced von Mises stress plotted with the deformation.

The highest equivalent stress, approximately 13 MPa, occurs at the inner corners of the curves of the Nichrome circuit. The yield stress for high quality glass is roughly 250 MPa, and for Nichrome it is 360 MPa. This means that the individual objects remain structurally intact for the simulated heating power loads.

You must also consider stresses in the interface between the resistive layer and the glass plate. Assume that the yield stress of the surface adhesion in the interface is in the region of 50 MPa — a value significantly lower than the yield stresses of the other materials in the device. If the equivalent stress increases above this value, the resistive layer locally detaches from the glass. Once it has detached, heat transfer is locally impeded, which can lead to overheating of the resistive layer and eventually cause the device to fail.

Figure 6 displays the effective forces acting on the adhesive layer during heater operation. As the figure shows, the device experiences a maximum interfacial stress that is an order of magnitude smaller than the yield stress. This means that the device is well designed in terms of adhesive stress.

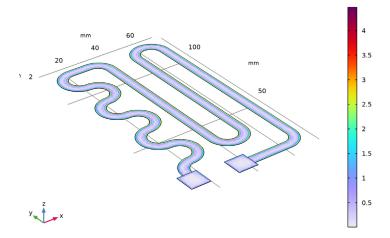


Figure 6: The effective forces at the interface between the resistive layer and the glass plate.

Finally, study the warping of the device, that is, its deviation from a plane surface, shown in Figure 7.

Surface: Warping displacement, normal component (mm) Surface: Average displacement magnitude (mm)

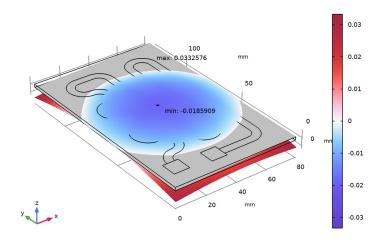


Figure 7: Warping displacement on the fluid side of the glass plate.

The maximum deviation from being a planar surface, is approximately $33 \mu m$. For high-precision applications, such as semiconductor processing, this might be a significant value that limits the device's operating temperature.

Application Library path: ACDC_Module/Electromagnetic_Heating/heating_circuit

Modeling Instructions

From the File menu, choose New.

NEW

In the New window, click Model Wizard.

MODEL WIZARD

- I In the Model Wizard window, click **1** 3D.
- 2 In the Select Physics tree, select Structural Mechanics>Thermal-Structure Interaction>
 Thermal Stress, Solid.
- 3 Click Add.
- 4 In the Select Physics tree, select AC/DC>Electric Fields and Currents> Electric Currents in Layered Shells (ecis).
- 5 Click Add.
- 6 Click Study.
- 7 In the Select Study tree, select General Studies>Stationary.
- 8 Click M Done.

GEOMETRY I

The Thermal Stress interface includes Heat Transfer in Solids and Solid Mechanics. In the volume, these two interfaces solve for temperature and displacement, respectively. In the shell representing the circuit, the temperature, the electrical potential and displacement are solved by Heat Transfer In Solids, Electric Currents, Layered Shell, and Solid Mechanics interfaces, respectively.

GLOBAL DEFINITIONS

Parameters 1

- I In the Model Builder window, under Global Definitions click Parameters I.
- 2 In the Settings window for Parameters, locate the Parameters section.
- **3** In the table, enter the following settings:

Name	Expression	Value	Description
V_in	12[V]	12 V	Input voltage
d_layer	10[um]	IE-5 m	Layer thickness
sigma_silver	6.3e7[S/m]	6.3E7 S/m	Electric conductivity of silver
sigma_nichrome	9.3e5[S/m]	9.3E5 S/m	Electric conductivity of nichrome
T_air	20[degC]	293.15 K	Air temperature
h_air	5[W/(m^2*K)]	5 W/(m²·K)	Heat transfer film coefficient, air
T_fluid	353[K]	353 K	Fluid temperature
h_fluid	20[W/(m^2*K)]	20 W/(m ² ·K)	Heat transfer film coefficient, fluid

GEOMETRY I

- I In the Model Builder window, under Component I (compl) click Geometry I.
- 2 In the Settings window for Geometry, locate the Units section.
- 3 From the Length unit list, choose mm.

Block I (blk I)

- I In the Geometry toolbar, click Block.
- 2 In the Settings window for Block, locate the Size and Shape section.
- 3 In the Width text field, type 80.
- 4 In the Depth text field, type 130.
- 5 In the Height text field, type 2.
- 6 Click | Build Selected.

Work Plane I (wbl)

- I In the Geometry toolbar, click Work Plane.
- 2 In the Settings window for Work Plane, locate the Plane Definition section.

- 3 In the z-coordinate text field, type 2.
- 4 Click A Go to Plane Geometry.

Work Plane I (wp I)>Plane Geometry

Click the **Zoom Extents** button in the **Graphics** toolbar.

Work Plane I (wpl)>Square I (sql)

- I In the Work Plane toolbar, click Square.
- 2 In the Settings window for Square, locate the Size section.
- 3 In the Side length text field, type 10.
- 4 Locate the **Position** section. In the xw text field, type 7.
- 5 In the yw text field, type 10.
- 6 Click **Build Selected**.
- 7 Right-click Square I (sql) and choose Duplicate.

Work Plane I (wp I)>Square 2 (sq2)

- I In the Model Builder window, click Square 2 (sq2).
- 2 In the Settings window for Square, locate the Position section.
- 3 In the xw text field, type 30.
- 4 In the yw text field, type 8.
- 5 Click | Build Selected.

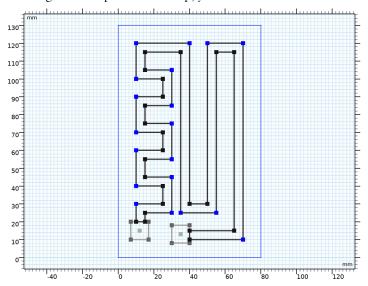
Work Plane I (wpl)>Polygon I (poll)

- I In the Work Plane toolbar, click / Polygon.
- 2 In the Settings window for Polygon, locate the Coordinates section.
- 3 From the Data source list, choose File.
- 4 Click **Browse**.
- **5** Browse to the model's Application Libraries folder and double-click the file heating_circuit_polygon.txt.
- 6 Click Pauld Selected.

Work Plane I (wpl)>Fillet I (fill)

I In the Work Plane toolbar, click **[Fillet**.

2 On the object **poll**, select Points 2–8, 23–29, 34, 36, 37, 41, and 42 only. It might be easier to select the points by using the Selection List window. To open this window, in the Home toolbar click Windows and choose Selection List. (If you are running the cross-platform desktop, you find **Windows** in the main menu.)



- 3 In the Settings window for Fillet, locate the Radius section.
- 4 In the Radius text field, type 10.
- 5 Click | Build Selected.

Work Plane I (wb I)>Fillet 2 (fil2)

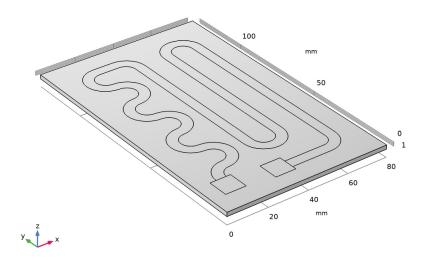
- I In the Work Plane toolbar, click Fillet.
- 2 On the object fill, select Points 6–12, 26–31, 37, 40, 43, 46, 49, and 50 only.
- 3 In the Settings window for Fillet, locate the Radius section.
- 4 In the Radius text field, type 5.
- 5 In the Work Plane toolbar, click **Build All**.

Form Union (fin)

I In the Home toolbar, click 📳 Build All.

The geometry should look like the figure below.

2 In the Model Builder window, under Component I (compl)>Geometry I click Form Union (fin).



DEFINITIONS

Add a selection that you can use later when applying boundary conditions and shell physics settings.

Circuit

- I In the **Definitions** toolbar, click **\(\big|_{\text{a}} \) Explicit**.
- 2 In the Settings window for Explicit, type Circuit in the Label text field.
- 3 Locate the Input Entities section. From the Geometric entity level list, choose Boundary.
- 4 Select Boundaries 6–8 only.

Before creating the materials for use in this model, it is a good idea to specify which boundaries are to be modeled as conducting shells. Using this information, COMSOL Multiphysics can detect which material properties are needed.

HEAT TRANSFER IN SOLIDS (HT)

Thin Layer I

- I In the Model Builder window, under Component I (compl) right-click Heat Transfer in Solids (ht) and choose Thin Structures>Thin Layer.
- 2 In the Settings window for Thin Layer, locate the Boundary Selection section.
- **3** From the **Selection** list, choose **Circuit**.
- 4 Locate the Layer Model section. From the Layer type list, choose Thermally thin approximation.

ELECTRIC CURRENTS IN LAYERED SHELLS (ECIS)

- I In the Model Builder window, under Component I (compl) click Electric Currents in Layered Shells (ecis).
- 2 In the Settings window for Electric Currents in Layered Shells, locate the **Boundary Selection** section.
- 3 From the Selection list, choose Circuit.

Conductive Shell I

- I In the Model Builder window, under Component I (compl)> Electric Currents in Layered Shells (ecis) click Conductive Shell I.
- 2 In the Settings window for Conductive Shell, locate the Constitutive Relation D-E section.
- 3 From the ε_r list, choose User defined.

Use Thin Layer in the Solid Mechanics interface.

SOLID MECHANICS (SOLID)

In the Model Builder window, under Component I (compl) click Solid Mechanics (solid).

Thin Layer 1

- I In the Physics toolbar, click **Boundaries** and choose Thin Layer.
- 2 In the Settings window for Thin Layer, locate the Boundary Selection section.
- **3** From the **Selection** list, choose **Circuit**.
- 4 Locate the Boundary Properties section. From the Thin layer type list, choose Layered.

To model the thermal effects in the thin layers, add a Thermal Expansion, Thin Layer multiphysics coupling.

MULTIPHYSICS

Thermal Expansion, Thin Layer I (tetl1)

In the Physics toolbar, click Multiphysics Couplings and choose Boundary> Thermal Expansion, Thin Layer.

Now set up the materials.

ADD MATERIAL

- I In the Home toolbar, click **Add Material** to open the Add Material window.
- 2 Go to the Add Material window.
- 3 In the tree, select Built-in>Silica glass.
- 4 Click Add to Component in the window toolbar.
- 5 In the Home toolbar, click **‡ Add Material** to close the **Add Material** window.

MATERIALS

Silver Layer

- I In the Model Builder window, under Component I (compl) right-click Materials and choose Layers>Single Layer Material.
- 2 In the Settings window for Material, type Silver Layer in the Label text field.
- 3 Locate the Geometric Entity Selection section. From the Selection list, choose Circuit.
- **4** Locate the **Orientation and Position** section. From the **Position** list, choose **Bottom side on boundary**.
- **5** Locate the **Material Contents** section. In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Heat capacity at constant pressure	Ср	230	J/(kg·K)	Basic
Young's modulus	E	83e9	Pa	Young's modulus and Poisson's ratio
Poisson's ratio	nu	0.37	I	Young's modulus and Poisson's ratio
Density	rho	10500	kg/m³	Basic

Property	Variable	Value	Unit	Property group
Thermal conductivity	k_iso ; kii = k_iso, kij = 0	420	W/(m·K)	Basic
Electrical conductivity	sigma_iso; sigmaii = sigma_iso, sigmaij = 0	sigma_si lver	S/m	Basic
Coefficient of thermal expansion	alpha_iso; alphaii = alpha_iso, alphaij = 0	18.9e-6	I/K	Basic
Thickness	lth	d_layer	m	Shell

Nichrome Layer

- I Right-click Materials and choose Layers>Single Layer Material.
- **2** Select Boundary 7 only.
- 3 In the Settings window for Material, type Nichrome Layer in the Label text field.
- 4 Locate the Orientation and Position section. From the Position list, choose Bottom side on boundary.
- **5** Locate the **Material Contents** section. In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Heat capacity at constant pressure	Ср	20	J/(kg·K)	Basic
Young's modulus	E	213e9	Pa	Young's modulus and Poisson's ratio
Poisson's ratio	nu	0.33	I	Young's modulus and Poisson's ratio
Density	rho	9000	kg/m³	Basic
Thermal conductivity	k_iso ; kii = k_iso, kij = 0	15	W/(m·K)	Basic

Property	Variable	Value	Unit	Property group
Electrical conductivity	sigma_iso; sigmaii = sigma_iso, sigmaij = 0	sigma_nic hrome	S/m	Basic
Coefficient of thermal expansion	alpha_iso; alphaii = alpha_iso, alphaij = 0	10e-6	I/K	Basic
Thickness	lth	d_layer	m	Shell

ELECTRIC CURRENTS IN LAYERED SHELLS (ECIS)

In the Model Builder window, under Component I (compl) click Electric Currents in Layered Shells (ecis).

Ground I

- I In the Physics toolbar, click Edges and choose Ground.
- 2 Select Edge 43 only.

Electric Potential I

- I In the Physics toolbar, click Edges and choose Electric Potential.
- 2 Select Edge 10 only.
- 3 In the Settings window for Electric Potential, locate the Electric Potential section.
- **4** In the V_0 text field, type V_i n.

Continuity I

- I In the Physics toolbar, click Edges and choose Continuity.
- 2 In the Settings window for Continuity, locate the Layer Selection section.
- 3 From the Source list, choose Silver Layer (mat2).
- 4 From the Destination list, choose Nichrome Layer (mat3).

With the materials defined, set up the remaining physics of the model. In the next section, the resistive loss within the circuit is defined as a heat source for the thermal stress physics. The resistive loss is calculated automatically within the **Electric Currents, Layered Shell** interface. Add the coupling feature **Electromagnetic Heating** to take the resistive loss into account.

MULTIPHYSICS

Electromagnetic Heating, Layered Shell I (ehls I)

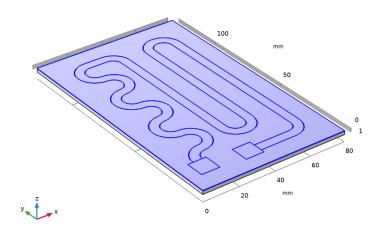
In the Physics toolbar, click Authorites Couplings and choose Boundary> Electromagnetic Heating, Layered Shell.

HEAT TRANSFER IN SOLIDS (HT)

In the Model Builder window, under Component I (compl) click Heat Transfer in Solids (ht).

Heat Flux I

- I In the Physics toolbar, click **Boundaries** and choose **Heat Flux**.
- 2 Select Boundaries 4 and 6–8 only.



- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 From the Flux type list, choose Convective heat flux.
- **5** In the *h* text field, type h_air.
- **6** In the $T_{\rm ext}$ text field, type T_air.

Heat Flux 2

- I In the Physics toolbar, click Boundaries and choose Heat Flux.
- 2 Select Boundary 3 only.
- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 From the Flux type list, choose Convective heat flux.

- **5** In the *h* text field, type h_fluid.
- **6** In the T_{ext} text field, type T_fluid.

SOLID MECHANICS (SOLID)

In order for the problem to be well posed, the glass plate must be constrained so that it does not have any possible rigid body translations or rotations. The constraints must be such that no stresses are induced by inhibited thermal expansion.

I In the Model Builder window, under Component I (compl) click Solid Mechanics (solid).

Rigid Motion Suppression I

In the Physics toolbar, click **Domains** and choose Rigid Motion Suppression.

The absolute value of the maximum or minimum displacement is not important in itself, since it is just a function of how the rigid body constraints are applied. Instead, you want to see how much the boundary deviates from being planar. Use the **Warpage** feature to display that.

Warpage I

- I In the Physics toolbar, click Boundaries and choose Warpage.
- 2 Select Boundary 3 only.

MESH I

Free Triangular I

- I In the Mesh toolbar, click \times More Generators and choose Free Triangular.
- 2 Select Boundaries 4 and 6-8 only.

Size 1

- I Right-click Free Triangular I and choose Size.
- 2 In the Settings window for Size, locate the Geometric Entity Selection section.
- 3 From the Selection list, choose Circuit.
- **4** Locate the **Element Size** section. Click the **Custom** button.
- 5 Locate the Element Size Parameters section.
- 6 Select the Maximum element size check box. In the associated text field, type 2.

Swebt I

In the Mesh toolbar, click A Swept.

Distribution I

I Right-click Swept I and choose Distribution.

- 2 In the Settings window for Distribution, locate the Distribution section.
- **3** In the **Number of elements** text field, type **3**.
- 4 Click III Build All.

STUDY I

In order to improve the solver's performance, scale the degrees of freedom in Solid Mechanics to 1e-3.

Solution I (soll)

- I In the Study toolbar, click Show Default Solver.
- 2 In the Model Builder window, expand the Solution I (soll) node.
- 3 In the Model Builder window, expand the Study I>Solver Configurations> Solution I (soll)>Dependent Variables I node, then click Displacement field (compl.u).
- 4 In the Settings window for Field, locate the Scaling section.
- 5 From the Method list, choose Manual.
- 6 In the Scale text field, type 1e-3.
- 7 In the Study toolbar, click **Compute**.

RESULTS

The first default plot shows the von Mises stress and the deformation of the device (Figure 5). The third default plot shows the temperature distribution in the volume of the full 3D geometry (Figure 4). Two plots are also generated to visualize the electric potential and the von Mises stress on the circuit layer.

Volume 1

- I In the Model Builder window, expand the Results>Stress (solid) node, then click Volume 1.
- 2 In the Settings window for Volume, locate the Expression section.
- 3 From the Unit list, choose MPa.
- 4 In the Stress (solid) toolbar, click Plot.

Volume 1

- I In the Model Builder window, expand the Results>Stress, Thin Layer (solid) node, then click Volume 1.
- 2 In the Settings window for Volume, locate the Expression section.
- 3 From the Unit list, choose MPa.
- 4 In the Stress, Thin Layer (solid) toolbar, click Plot.

Domain

In the Model Builder window, expand the Results>Temperature (ht) node.

Study I/Solution I (soll)

- I In the Model Builder window, expand the Results>Datasets node.
- 2 Right-click Results>Datasets>Study I/Solution I (soll) and choose Duplicate.

Selection

- I In the Model Builder window, right-click Study I/Solution I (2) (sol1) and choose Selection.
- 2 In the Settings window for Selection, locate the Geometric Entity Selection section.
- 3 From the Geometric entity level list, choose Boundary.
- 4 From the Selection list, choose Circuit.

To generate Figure 3 follow the steps below.

Surface Losses

- I In the Home toolbar, click Add Plot Group and choose 3D Plot Group.
- 2 In the Settings window for 3D Plot Group, type Surface Losses in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study I/Solution I (2) (soll).

Surface I

- I In the Surface Losses toolbar, click Surface.
- 2 In the Settings window for Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)> Electric Currents in Layered Shells>Heating and losses>ecis.Qsh Surface loss density, electromagnetic W/m².
- 3 In the Surface Losses toolbar, click **Plot**.
- **4** Click the **Scene Light** button in the **Graphics** toolbar.
- 5 Click the **Zoom Extents** button in the **Graphics** toolbar.

The following steps generate a plot of the norm of the surface traction vector in the surface plane (see Figure 6):

Interface Stress

- I In the Home toolbar, click Add Plot Group and choose 3D Plot Group.
- 2 In the Settings window for 3D Plot Group, type Interface Stress in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study I/Solution I (2) (soll).

Surface I

- I In the Interface Stress toolbar, click Surface.
- 2 In the Settings window for Surface, locate the Expression section.
- 3 In the Expression text field, type sqrt(solid.Tax^2+solid.Tay^2).
- 4 From the Unit list, choose MPa.
- 5 Locate the Coloring and Style section. Click Change Color Table.
- 6 In the Color Table dialog box, select Rainbow>Prism in the tree.
- 7 Click OK.
- 8 In the Interface Stress toolbar, click Plot.

Finally, to obtain Figure 7, proceed as follows:

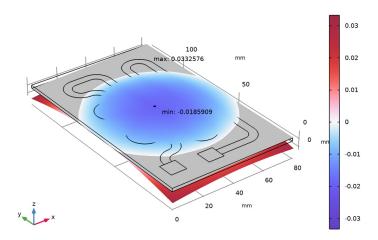
ADD PREDEFINED PLOT

- I In the Home toolbar, click Add Predefined Plot to open the Add Predefined Plot window.
- 2 Go to the Add Predefined Plot window.
- 3 In the tree, select Study I/Solution I (I) (soll)>Solid Mechanics>Warpage (wrpl).
- 4 Click Add Plot in the window toolbar.
- 5 In the Home toolbar, click Add Predefined Plot to close the Add Predefined Plot window.

RESULTS

Warpage (wrp1)

Surface: Warping displacement, normal component (mm) Surface: Average displacement magnitude (mm)



To calculate the values for the total generated heat and the integrated heat flux on the fluid side, perform a boundary integration:

Surface Integration 1

- I In the Results toolbar, click 8.85 More Derived Values and choose Integration> Surface Integration.
- 2 Select Boundary 3 only.
- 3 In the Settings window for Surface Integration, click Replace Expression in the upper-right corner of the Expressions section. From the menu, choose Component I (compl)> Heat Transfer in Solids>Boundary fluxes>ht.q0 - Inward heat flux - W/m2.
- 4 Click **= Evaluate**.

TABLE I

I Go to the Table I window.

The result should be close to 8.5 W.

RESULTS

Surface Integration 2

- I In the Results toolbar, click 8.85 More Derived Values and choose Integration> Surface Integration.
- 2 In the Settings window for Surface Integration, locate the Selection section.
- 3 From the Selection list, choose Circuit.
- 4 Click Replace Expression in the upper-right corner of the Expressions section. From the menu, choose Component I (compl)>Electric Currents in Layered Shells> Heating and losses>ecis.Qsh - Surface loss density, electromagnetic - W/m2.
- 5 Click **= Evaluate**.

TABLE 2

I Go to the Table 2 window.

The result should be close to 13.8 W.