

# Stress Corrosion

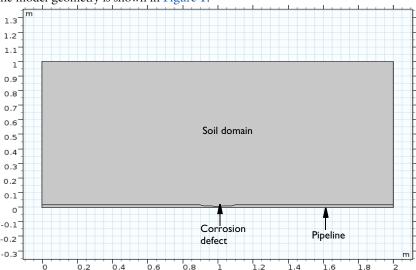
# Introduction

Steel pipelines are often subjected to complex stress/strain conditions in oil and gas industry. In addition to stress from internal pressure, pipelines are subjected to significant longitudinal strain due to surrounding soil movement. As a result of the changed surface energies at the pipe surface, the resulting stresses may have an effect on the pipe corrosion rate. The intercoupled effects of elastic and plastic deformation on pipeline corrosion is demonstrated in this model example.

The elasto-plastic stress simulations are performed here using a small strain plasticity model and von-Mises yielding criterion. Iron dissolution (anodic) and hydrogen evolution (cathodic) are considered as electrochemical reactions, using kinetic expressions that account for the effect of elasto-plastic deformations.

The example is based on a paper by L. Y. Xu and Y. F. Cheng (Ref. 1). The model is built in two parts. In the first part, the stationary effect of the elasto-plastic stress on corrosion is investigated by varying the longitudinal strain using a parametric study. In the second part, a transient simulation is performed to investigate the intercoupled effects of a dissolving, and hence dynamically varying, corrosion defect depth on a pipe, subject to a constant strain.

**Note:** This model requires the Structural Mechanics, or the MEMS Module, with the addition of either the Nonlinear Structural Materials or the Geomechanics Module.



The model geometry is shown in Figure 1.

Figure 1: The model geometry consists of a pipeline with corrosion defect and surrounding soil domain.

The model geometry consists of high strength alloy steel pipeline and surrounding soil domain. The pipeline length is 2 m and wall thickness is 19.1 mm. The corrosion defect on the exterior side of the pipeline is elliptical in shape with a length of 200 mm and a depth of 11.46 mm. The electrolyte conductivity of soil domain in 0.096 S/m.

# **ELASTOPLASTIC STRESS**

An elastoplastic stress simulation is performed over pipeline domain using the small strain plasticity model. The user defined isotropic hardening model is used where the hardening function,  $\sigma_{vhard}$ , is defined as:

$$\sigma_{\text{yhard}} = \sigma_{\text{exp}} \left( \varepsilon_{\text{p}} + \frac{\sigma_{\text{e}}}{E} \right) - \sigma_{\text{ys}}$$

where  $\sigma_{\rm exp}$  is the experimental stress-strain curve,  $\varepsilon_{\rm p}$  is the plastic deformation,  $\sigma_e$  is the von Mises stress, E is the Young's modulus (207·10<sup>9</sup> Pa), and  $\sigma_{\rm ys}$  is the yield strength of high strength alloy steel(806·10<sup>6</sup> Pa).

The experimental stress-strain curve used in the model is prescribed in terms of a piecewise cubic interpolation function and is taken from Ref. 2.

#### **ELECTROCHEMICAL REACTIONS**

The iron dissolution (anodic) and hydrogen evolution (cathodic) reactions are the two electrochemical reactions that occur at the corrosion defect surface of pipelines. The rest of pipeline surfaces are assumed to be electrochemically inactive.

An anodic Tafel expression is used to model the iron dissolution reaction, with a local anodic current density defined as

$$i_{a} = i_{0, a} 10^{\frac{\eta_{a}}{\overline{A}_{a}}}$$

where  $i_{0,a}$  is the exchange current density (2.353·10<sup>-3</sup> A/m<sup>2</sup>),  $A_a$  is the Tafel slope (0.118 V) and the overpotential  $\eta_a$  for the anodic reaction is calculated from

$$\eta_a = \phi_s - \phi_l - E_{eq,a}$$

The equilibrium potential for the anodic reaction is calculated from

$$E_{\rm eq,a} = E_{\rm eq0,a} - \frac{\Delta P_{\rm m} V_{\rm m}}{zF} - \frac{TR}{zF} \ln \left( \frac{v\alpha}{N_0} \varepsilon_p + 1 \right)$$

where  $E_{\rm eq0,a}$  is the standard equilibrium potential for the anodic reaction ( $-0.859~\rm V$ ),  $\Delta P_m$  is the excess pressure to elastic deformation ( $2.687\cdot10^8~\rm Pa$ ),  $V_{\rm m}$  is the molar volume of steel ( $7.13\cdot10^{-6}~\rm m^3/mol$ ), z is the charge number for steel (2), F is the Faraday's constant, T is the absolute temperature ( $298.15~\rm K$ ), R is the ideal gas constant, vis an orientation dependent factor (0.45),  $\alpha$  is a coefficient ( $1.67\cdot10^{15}~\rm m^{-2}$ ) and  $N_0$  is the initial dislocation density ( $1\cdot10^{12}~\rm m^{-2}$ ).

A cathodic Tafel expression is used to model the hydrogen evolution reaction, this sets the local cathodic current density to

$$i_{\rm c} = i_{\rm 0, c} 10^{\frac{\eta_{\rm c}}{A_{\rm c}}}$$

where  $i_{0,c}$  is the exchange current density,  $A_c$  is the Tafel slope (-0.207 V) and the overpotential  $\eta_c$  (SI unit: V) for the cathodic reaction is calculated from

$$\eta_{c} = \phi_{s} - \phi_{l} - E_{eq0,c}$$

where  $E_{
m eq0,c}$  is the standard equilibrium potential for the cathodic reaction (-0.644 V)

The exchange current density for the cathodic reaction is calculated from

$$i_{0, c} = i_{0, c, ref} 10^{\frac{\sigma_e V_m}{6F(-A_c)}}$$

where  $i_{0,c,ref}$  is the reference exchange current density for the cathodic reaction in the absence of external stress/strain  $(1.457 \cdot 10^{-2} \text{ A/m}^2)$ .

#### **DEFORMED GEOMETRY**

In the second part of the model, dissolution of iron from the corrosion defect is modeled using deformed geometry. The dissolution of iron causes the electrode boundary to move, with a velocity in the normal direction, v (SI unit: m/s), according to

$$v = \frac{i_a}{2F} \frac{M}{\rho}$$

where  $i_a$  (SI unit: A/m<sup>2</sup>) is the anodic current density, M is the molar mass (55.845 g/mol) and  $\rho$  the density (7870 kg/m<sup>3</sup>) of the iron.

Solve the model in a time-dependent study, simulating the corrosion for 20 years of exposure.

#### Results and Discussion

Figure 2 shows the electrolyte potential distribution (V) over the soil domain and the von Mises stress distribution (MPa) over the pipe domain, as indicated by the color bars for a prescribed displacement of 4 mm in the x direction. It can be seen that the local stresses are significantly higher near the corrosion defect than that at the rest of the

pipeline. A nonuniform electrolyte potential distribution near the corrosion defect is also evident in Figure 2, as indicated by a semi-circular area.

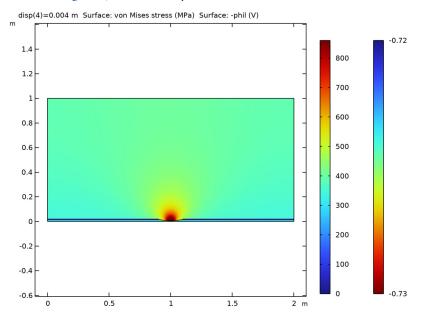


Figure 2: The electrolyte potential distribution over the soil domain and the von Mises stress distribution over the pipeline domain for a prescribed displacement of 4 mm.

Figure 3 shows the von Mises stress distribution along the length of the corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm, respectively. The von Mises stress increases with an increase in the tensile strain and it is found to be maximum at the center of corrosion defect. For the tensile strain of 2 mm, 3 mm and 4 mm, it is observed that the local stress, particularly at the center of corrosion defect, exceeds the yield strength of high strength alloy steel (806·10<sup>6</sup> Pa). This results in the plastic deformation at the center of corrosion defect while deformation in the remaining

area of corrosion defect remains in the elastic range. For the lower tensile strain of 1 mm, the entire corrosion defect is observed to be in the elastic deformation range.

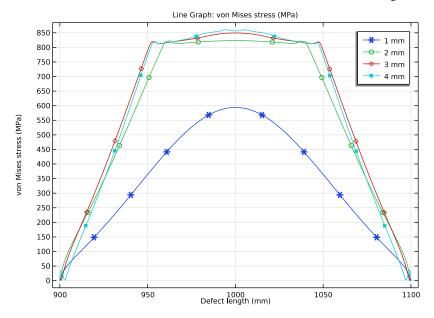


Figure 3: The von Mises stress distribution along the length of the corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm.

Figure 4 shows the corrosion potential distribution along the length of the corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm. For lower tensile strain of 1 mm, the variation in the corrosion potential is found to be uniform along the length of the corrosion defect. However, for higher tensile strains of 2 mm, 3 mm and 4 mm, the variation in the corrosion potential is nonuniform with the more negative

corrosion potential at the center of the corrosion defect than that at both the sides of the corrosion defect.

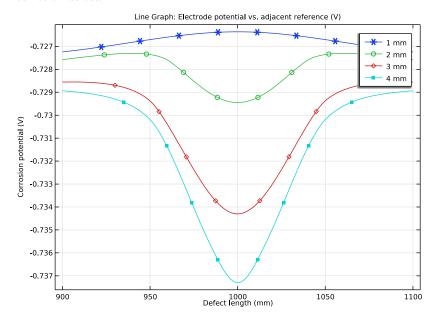


Figure 4: The corrosion potential distribution along the length of the corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm.

Figure 5 shows the anodic current density distribution along the length of corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm. For lower tensile strain of 1 mm, the variation in the anodic current density is found to be uniform along the length of the corrosion defect, similar to the corrosion potential behavior. However, for higher tensile strains of 2 mm, 3 mm and 4 mm, the variation in the anodic current density is significantly nonuniform, particularly at the center of the corrosion defect. It can be seen that the anodic current density increases significantly at the center of the corrosion defect whereas it decreases slightly at both the sides of the corrosion defect for higher tensile strains. The increase in the anodic current density for tensile strains of 2 mm, 3 mm and 4 mm is attributed to the plastic deformation observed at the center of the corrosion defect (see Figure 3).

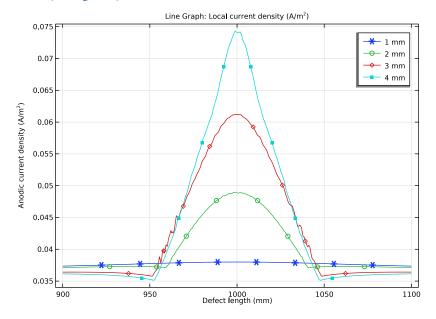


Figure 5: The anodic current density distribution along the length of the corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm.

Figure 6 shows the cathodic current density distribution along the length of the corrosion defect for prescribed displacements of 1 mm, 2 mm, 3 mm, and 4 mm. It can be seen that the cathodic current density increases negatively with an increase in the tensile strain and it is found to be the most negative at the center of the corrosion defect. The nonuniformity in the cathodic current density is also found to increase with an increase in the tensile

strain. Thus, the cathodic current density distribution is found to be the most nonuniform for a tensile strain of 4 mm.

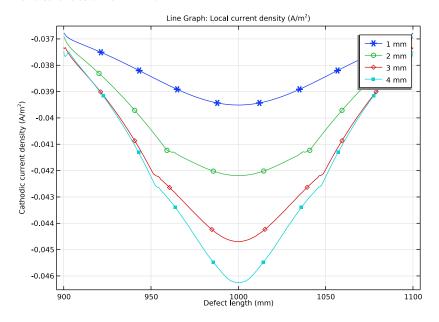


Figure 6: The cathodic current density distribution along the length of the corrosion defect for prescribed displacements of  $1\ mm,\ 2\ mm,\ 3\ mm,\ and\ 4\ mm.$ 

Figure 7 shows the corrosion defect profile at time t = 0 a and 20 a. It can be seen that after 20 years, the depth of the corrosion defect is increased particularly at the center of the corrosion defect.

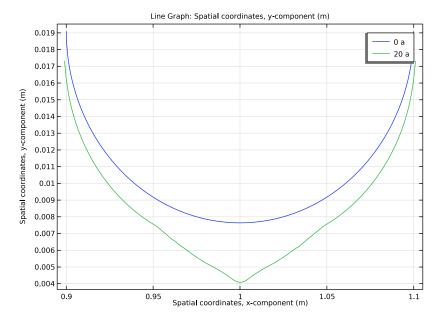


Figure 7: The corrosion defect profile at time t = 0 a and 20 a.

Figure 8 shows the von Mises stress distribution along the length of the corrosion defect at time t = 0 a and 20 a. It can be seen that after 20 years, the von Mises stress is higher at the center of the corrosion defect than that at both the sides of the corrosion defect.

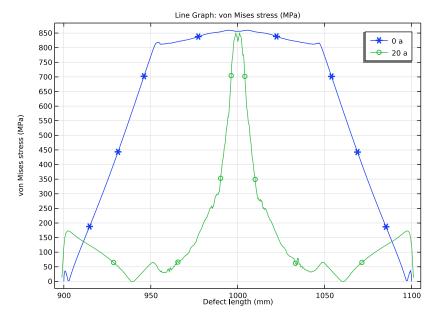


Figure 8: The von Mises stress distribution along the length of the corrosion defect at time t =0 a and 20 a.

Figure 9 shows the corrosion potential distribution along the length of the corrosion defect at time t = 0 a and 20 a. It can be seen that after 20 years, the corrosion potential is more negative throughout the length of the corrosion defect.

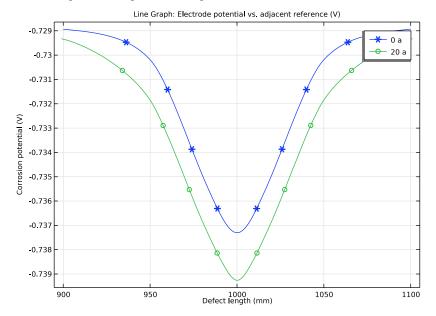


Figure 9: The corrosion potential distribution along the length of the corrosion defect at time t = 0 a and 20 a.

Figure 10 shows the anodic current density distribution along the length of corrosion defect at time t = 0 a and 20 a. It can be seen that after 20 years, the anodic current density is marginally higher at the center of the corrosion defect when compared with that at time t = 0 a.

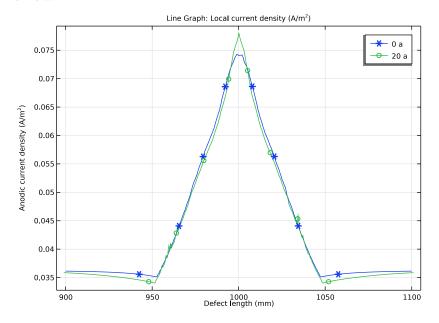


Figure 10: The anodic current density distribution along the length of the corrosion defect at time t = 0 a and 20 a.

Figure 11 shows the cathodic current density distribution along the length of the corrosion defect at time t = 0 a and 20 a. It can be seen that after 20 years, the cathodic current density is more negative at the center of the corrosion defect than that at both the sides of the corrosion defect. The cathodic current density is also found to be marginally more negative at the center of the corrosion defect when compared with that at time t =0 a.

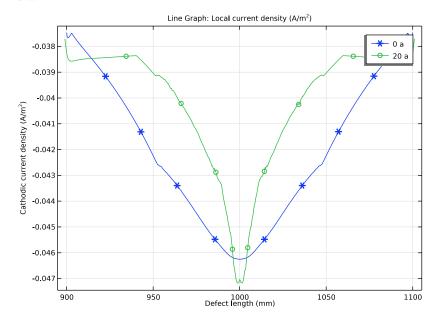


Figure 11: The cathodic current density distribution along the length of the corrosion defect at time t = 0 a and 20 a.

# Notes About the COMSOL Implementation

The model is implemented using the Solid Mechanics interface and the Secondary Current Distribution interface. In the first study, the Solid Mechanics model does not depend upon the results of the Secondary Current Distribution model, and we use a sequential solver set up with a Parametric Sweep to study the impact of elastoplastic deformations on electrochemical reactions. In the second part of the model, a transient analysis is performed using Deformed Geometry to analyze the effect of varying depth, due to dissolution, on stress as well as corrosion.

# References

1. L.Y. Xu and Y.F. Cheng, "Development of a finite element model for simulation and prediction of mechanoelectrochemical effect of pipeline corrosion," Corrosion Science, vol. 73, pp. 150-160, 2013.

2. L. Xu, Assessment of corrosion defects on high-strength steel pipelines, PhD thesis, Department of mechanical and manufacturing engineering, University of Calgary, Alberta, August 2013.

Application Library path: Corrosion Module/General Corrosion/ stress corrosion

# Modeling Instructions

From the File menu, choose New.

## NEW

In the New window, click Model Wizard.

#### MODEL WIZARD

- I In the Model Wizard window, click **2** 2D.
- 2 In the Select Physics tree, select Structural Mechanics>Solid Mechanics (solid).
- 3 Click Add.
- 4 In the Select Physics tree, select Electrochemistry> Primary and Secondary Current Distribution>Secondary Current Distribution (cd).
- 5 Click Add.
- 6 Click 🔵 Study.
- 7 In the Select Study tree, select General Studies>Stationary.
- 8 Click M Done.

## GEOMETRY I

Draw the pipe geometry with a corrosion defect and a surrounding soil domain.

Rectangle I (rI)

- I In the Geometry toolbar, click Rectangle.
- 2 In the Settings window for Rectangle, locate the Size and Shape section.
- 3 In the Width text field, type 2.
- 4 In the **Height** text field, type 19.1[mm].

Ellipse I (el)

- I In the **Geometry** toolbar, click Ellipse.
- 2 In the Settings window for Ellipse, locate the Size and Shape section.
- 3 In the a-semiaxis text field, type 100[mm].
- 4 In the b-semiaxis text field, type 11.46[mm].
- **5** Locate the **Position** section. In the **x** text field, type 1.
- 6 In the y text field, type 19.1[mm].

Difference I (dif1)

- I In the Geometry toolbar, click Booleans and Partitions and choose Difference.
- 2 Select the object rI only.
- 3 In the Settings window for Difference, locate the Difference section.
- 4 Click to select the Activate Selection toggle button for Objects to subtract.
- **5** Select the object **e1** only.

Rectangle 2 (r2)

- I In the Geometry toolbar, click Rectangle.
- 2 In the Settings window for Rectangle, locate the Size and Shape section.
- 3 In the Width text field, type 2.
- 4 Click Build All Objects.
- 5 Click the **Zoom Extents** button in the **Graphics** toolbar.

Your geometry should look like that in Figure 1.

#### GLOBAL DEFINITIONS

Parameters 1

Load the model parameters.

- I In the Model Builder window, under Global Definitions click Parameters I.
- 2 In the Settings window for Parameters, locate the Parameters section.
- 3 Click Load from File.
- **4** Browse to the model's Application Libraries folder and double-click the file stress\_corrosion\_parameters.txt.

#### DEFINITIONS

Load the model variables.

Variables 1

- I In the Model Builder window, expand the Component I (compl)>Definitions node.
- 2 Right-click **Definitions** and choose **Variables**.
- 3 In the Settings window for Variables, locate the Variables section.
- 4 Click Load from File.
- **5** Browse to the model's Application Libraries folder and double-click the file stress\_corrosion\_variables.txt.

Interpolation I (int I)

Load the stress strain interpolation data from a text file.

- I In the Home toolbar, click f(x) Functions and choose Local>Interpolation.
- 2 In the Settings window for Interpolation, locate the Definition section.
- **3** In the **Function name** text field, type stress\_strain\_curve.
- 4 Click **Load from File**.
- **5** Browse to the model's Application Libraries folder and double-click the file stress\_corrosion\_stress\_strain\_curve\_interpolation.txt.
- 6 Locate the Interpolation and Extrapolation section. From the Interpolation list, choose Piecewise cubic.
- 7 Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	1

**8** In the **Function** table, enter the following settings:

Function	Unit
stress_strain_curve	MPa

# SOLID MECHANICS (SOLID)

Start setting up the physics. First, set the elastoplastic deformation at the Linear Elastic Material node by adding a Plasticity node.

- I In the Model Builder window, under Component I (compl) click Solid Mechanics (solid).
- 2 In the Settings window for Solid Mechanics, locate the Domain Selection section.
- 3 In the list, select 2.
- 4 Click Remove from Selection.

**5** Select Domain 1 only.

Linear Elastic Material I

In the Model Builder window, under Component I (compl)>Solid Mechanics (solid) click Linear Elastic Material I.

# Plasticity 1

- I In the Physics toolbar, click \_\_\_ Attributes and choose Plasticity.
- 2 In the Settings window for Plasticity, locate the Plasticity Model section.
- 3 Find the Isotropic hardening model subsection. From the list, choose Hardening function.

#### MATERIALS

Now, add a high-strength alloy steel material for the pipe and set the values for initial yield stress, hardening function, Young's modulus, and Poisson's ratio.

#### ADD MATERIAL

- I In the Home toolbar, click **Add Material** to open the Add Material window.
- 2 Go to the Add Material window.
- 3 In the tree, select Built-in>High-strength alloy steel.
- 4 Click Add to Component in the window toolbar.
- 5 In the Home toolbar, click Radd Material to close the Add Material window.

# MATERIALS

High-strength alloy steel (mat I)

- I In the Settings window for Material, locate the Geometric Entity Selection section.
- 2 In the list, select 2.
- 3 Click Remove from Selection.
- 4 Select Domain 1 only.
- **5** Locate the **Material Contents** section. In the table, set the following property values:

Property	Variable	Value	Unit	Property group
Initial yield stress	sigmags	806[MPa]	Pa	Elastoplastic material model
Hardening function	sigmagh	hardening	Pa	Elastoplastic material model

Property	Variable	Value	Unit	Property group
Young's modulus	E	207[GPa]	Pa	Young's modulus and Poisson's ratio
Poisson's ratio	nu	0.33	I	Young's modulus and Poisson's ratio

# SOLID MECHANICS (SOLID)

Next, set the initial value for the displacement field and then proceed to the setup of boundary conditions for the Solid Mechanics interface.

#### Initial Values 1

- I In the Model Builder window, under Component I (compl)>Solid Mechanics (solid) click Initial Values I.
- 2 In the Settings window for Initial Values, locate the Initial Values section.
- **3** Specify the **u** vector as

0.0001*X	Х
0	Υ

#### Fixed Constraint I

- I In the Physics toolbar, click Boundaries and choose Fixed Constraint.
- 2 Select Boundary 1 only.

# Prescribed Displacement I

- I In the Physics toolbar, click Boundaries and choose Prescribed Displacement.
- **2** Select Boundary 7 only.
- 3 In the Settings window for Prescribed Displacement, locate the Prescribed Displacement section.
- 4 From the Displacement in x direction list, choose Prescribed.
- **5** In the  $u_{0x}$  text field, type disp.

# Prescribed Displacement 2

- I In the Physics toolbar, click Boundaries and choose Prescribed Displacement.
- 2 Select Boundary 1 only.
- 3 In the Settings window for Prescribed Displacement, locate the Prescribed Displacement section.
- 4 From the Displacement in x direction list, choose Prescribed.

#### Fixed Constraint 2

- I In the Physics toolbar, click Points and choose Fixed Constraint.
- **2** Select Point 1 only.

# SECONDARY CURRENT DISTRIBUTION (CD)

Now, set up the physics for the electrochemical reactions. First, set the electrolyte conductivity, the initial value for the electrolyte potential, and then both the anodic and cathodic reactions at the corrosion defect surface of the pipe.

# Electrolyte I

- I In the Model Builder window, under Component I (compl)>
  Secondary Current Distribution (cd) click Electrolyte I.
- 2 In the Settings window for Electrolyte, locate the Electrolyte section.
- **3** From the  $\sigma_l$  list, choose **User defined**. In the associated text field, type sigmal.

#### Initial Values 1

- I In the Model Builder window, click Initial Values I.
- 2 In the Settings window for Initial Values, locate the Initial Values section.
- 3 In the phil text field, type (Eeq0a+Eeq0c)/2.

#### Current Conductor I

- I In the Physics toolbar, click **Domains** and choose **Current Conductor**.
- **2** Select Domain 1 only.
- 3 In the Settings window for Current Conductor, locate the Electrode section.
- **4** From the  $\sigma_s$  list, choose **User defined**. In the associated text field, type sigmas.

# Internal Electrode Surface I

- I In the Physics toolbar, click Boundaries and choose Internal Electrode Surface.
- 2 Select Boundaries 4, 6, 9, and 10 only.

# Electrode Reaction I

- I In the Model Builder window, click Electrode Reaction I.
- 2 In the Settings window for Electrode Reaction, locate the Equilibrium Potential section.
- 3 In the  $E_{\rm eq}$  text field, type Eeqa.
- 4 Locate the Electrode Kinetics section. From the Kinetics expression type list, choose Anodic Tafel equation.
- **5** In the  $i_0$  text field, type i0a.

**6** In the  $A_a$  text field, type ba.

Internal Electrode Surface I

In the Model Builder window, click Internal Electrode Surface 1.

# Electrode Reaction 2

- I In the Physics toolbar, click Attributes and choose Electrode Reaction.
- 2 In the Settings window for Electrode Reaction, locate the Equilibrium Potential section.
- **3** In the  $E_{\rm eq}$  text field, type Eeq0c.
- 4 Locate the Electrode Kinetics section. From the Kinetics expression type list, choose Cathodic Tafel equation.
- **5** In the  $i_0$  text field, type ic.
- **6** In the  $A_c$  text field, type bc.

# Electric Ground 1

- I In the Physics toolbar, click Boundaries and choose Electric Ground.
- 2 Select Boundary 1 only.

#### MESH I

Set a finer mesh near the corrosion defect surface of pipe.

# Free Triangular I

In the Mesh toolbar, click Free Triangular.

# Size 1

- I Right-click Free Triangular I and choose Size.
- 2 In the Settings window for Size, locate the Geometric Entity Selection section.
- 3 From the Geometric entity level list, choose Domain.
- **4** Select Domain 1 only.
- **5** Locate the **Element Size** section. Click the **Custom** button.
- 6 Locate the Element Size Parameters section.
- 7 Select the Maximum element size check box. In the associated text field, type 0.01.

# Size 2

- I In the Model Builder window, right-click Free Triangular I and choose Size.
- 2 In the Settings window for Size, locate the Geometric Entity Selection section.
- 3 From the Geometric entity level list, choose Boundary.
- 4 Select Boundaries 9 and 10 only.

- **5** Locate the **Element Size** section. Click the **Custom** button.
- 6 Locate the Element Size Parameters section.
- 7 Select the Maximum element size check box. In the associated text field, type 0.001.
- 8 Click **Build All**.

# STUDY: STATIONARY PARAMETRIC

Next, set the solver settings. Since the Solid Mechanics interface is independent of the electrochemical reactions, use a sequential solver setup with a parametric sweep.

- I In the Model Builder window, click Study I.
- 2 In the Settings window for Study, type Study: Stationary Parametric in the Label text field.

# Parametric Sweep

- I In the Study toolbar, click Parametric Sweep.
- 2 In the Settings window for Parametric Sweep, locate the Study Settings section.
- 3 Click + Add.
- **4** In the table, enter the following settings:

Parameter name	Parameter value list	Parameter unit
disp (Displacement)	0.001 0.002 0.003 0.004	m

# Steb 1: Stationary

- I In the Model Builder window, click Step I: Stationary.
- 2 In the Settings window for Stationary, locate the Physics and Variables Selection section.
- 3 In the table, clear the Solve for check box for Secondary Current Distribution (cd).

# Step 2: Stationary 2

- I In the Study toolbar, click Study Steps and choose Stationary>Stationary.
- 2 In the Settings window for Stationary, locate the Physics and Variables Selection section.
- 3 In the table, clear the Solve for check box for Solid Mechanics (solid).

# Solution I (soll)

Lower the relative tolerance for the **Secondary Current Distribution** study step.

- 2 In the Model Builder window, expand the Solution I (soll) node, then click Stationary Solver 2.

- 3 In the Settings window for Stationary Solver, locate the General section.
- 4 In the Relative tolerance text field, type 0.00001.
- 5 In the Model Builder window, click Study: Stationary Parametric.
- 6 In the Settings window for Study, locate the Study Settings section.
- 7 Clear the Generate default plots check box.

The model is now ready to be solved.

8 In the Study toolbar, click **Compute**.

#### RESULTS

Corrosion Potential and von Mises Stress

- I In the Home toolbar, click Add Plot Group and choose 2D Plot Group.
- 2 In the Settings window for 2D Plot Group, type Corrosion Potential and von Mises Stress in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study: Stationary Parametric/ Parametric Solutions I (sol3).

Surface I

- I In the Corrosion Potential and von Mises Stress toolbar, click Surface.
- 2 In the Settings window for Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)>Solid Mechanics> Stress>solid.misesGp - von Mises stress - N/m2.
- 3 Locate the Expression section. From the Unit list, choose MPa.

Corrosion Potential and von Mises Stress

In the Model Builder window, click Corrosion Potential and von Mises Stress.

Surface 2

- I In the Corrosion Potential and von Mises Stress toolbar, click
- 2 In the Settings window for Surface, locate the Expression section.
- **3** In the **Expression** text field, type -phil.
- 4 Click to expand the Range section. Select the Manual color range check box.
- 5 In the Minimum text field, type -0.733.
- 6 In the Maximum text field, type -0.724.
- 7 Locate the Coloring and Style section. From the Color table transformation list, choose Reverse.

- 8 In the Corrosion Potential and von Mises Stress toolbar, click Plot.
- **9** Click the **Zoom Extents** button in the **Graphics** toolbar.

The plot should like the one in Figure 2. Zoom in on a region close to the corrosion defect using the **Zoom Box** button in the **Graphics** window.

von Mises Stress, Parametric

Plot the von Mises stress along the corrosion defect for different values of prescribed displacements.

- I In the Home toolbar, click Add Plot Group and choose ID Plot Group.
- 2 In the **Settings** window for **ID Plot Group**, type von Mises Stress, Parametric in the **Label** text field.
- 3 Locate the Data section. From the Dataset list, choose Study: Stationary Parametric/ Parametric Solutions 1 (sol3).
- 4 Locate the Plot Settings section.
- 5 Select the x-axis label check box. In the associated text field, type Defect length (mm).

Line Graph I

- I In the von Mises Stress, Parametric toolbar, click Line Graph.
- 2 Select Boundaries 9 and 10 only.
- 3 In the Settings window for Line Graph, click Replace Expression in the upper-right corner of the y-Axis Data section. From the menu, choose Component I (compl)> Solid Mechanics>Stress>solid.misesGp von Mises stress N/m².
- 4 Locate the y-Axis Data section. From the Unit list, choose MPa.
- 5 Locate the x-Axis Data section. From the Parameter list, choose Expression.
- **6** In the **Expression** text field, type x.
- 7 From the **Unit** list, choose **mm**.
- **8** Click to expand the **Coloring and Style** section. Find the **Line markers** subsection. From the **Marker** list, choose **Cycle**.
- **9** From the **Positioning** list, choose **Interpolated**.
- 10 Click to expand the Legends section. Select the Show legends check box.
- II From the Legends list, choose Evaluated.
- 12 In the Legend text field, type eval(disp, mm) mm.
- 13 In the von Mises Stress, Parametric toolbar, click Plot.

The plot should look like Figure 3.

von Mises Stress, Parametric

Now, plot the corrosion potential along the defect length for different prescribed displacements.

I In the Model Builder window, right-click von Mises Stress, Parametric and choose Duplicate.

Corrosion Potential, Parametric

- I In the Model Builder window, under Results click von Mises Stress, Parametric I.
- 2 In the Settings window for ID Plot Group, type Corrosion Potential, Parametric in the Label text field.
- 3 Locate the Plot Settings section.
- 4 Select the y-axis label check box. In the associated text field, type Corrosion potential (V).

Line Grabh I

- I In the Model Builder window, expand the Corrosion Potential, Parametric node, then click Line Graph 1.
- 2 In the Settings window for Line Graph, click Replace Expression in the upper-right corner of the y-Axis Data section. From the menu, choose Component I (compl)> Secondary Current Distribution>cd.Evsref - Electrode potential vs. adjacent reference - V.
- 3 In the Corrosion Potential, Parametric toolbar, click Plot. The plot should look like Figure 4.

Corrosion Potential, Parametric

Plot the anodic current density along the corrosion defect.

I In the Model Builder window, right-click Corrosion Potential, Parametric and choose Duplicate.

Anodic Current Density, Parametric

- I In the Model Builder window, under Results click Corrosion Potential, Parametric I.
- 2 In the Settings window for ID Plot Group, type Anodic Current Density, Parametric in the Label text field.
- 3 Locate the Plot Settings section. In the y-axis label text field, type Anodic current density (A/m<sup>2</sup>).

Line Grabh I

I In the Model Builder window, expand the Anodic Current Density, Parametric node, then click Line Graph 1.

- 2 In the Settings window for Line Graph, click Replace Expression in the upper-right corner of the y-Axis Data section. From the menu, choose Component I (compl)> Secondary Current Distribution>Electrode kinetics>cd.iloc\_erl Local current density A/m².
- 3 In the Anodic Current Density, Parametric toolbar, click Plot.

  The plot should look like Figure 5.

Anodic Current Density, Parametric

Plot the cathodic current density along the corrosion defect.

I In the Model Builder window, right-click Anodic Current Density, Parametric and choose Duplicate.

Cathodic Current Density, Parametric

- I In the Model Builder window, under Results click Anodic Current Density, Parametric I.
- 2 In the Settings window for ID Plot Group, type Cathodic Current Density, Parametric in the Label text field.
- 3 Locate the **Plot Settings** section. In the **y-axis label** text field, type Cathodic current density (A/m<sup>2</sup>).

Line Graph I

- I In the Model Builder window, expand the Cathodic Current Density, Parametric node, then click Line Graph I.
- 2 In the Settings window for Line Graph, click Replace Expression in the upper-right corner of the y-Axis Data section. From the menu, choose Component I (compl)> Secondary Current Distribution>Electrode kinetics>cd.iloc\_er2 Local current density A/m².
- 3 In the Cathodic Current Density, Parametric toolbar, click Plot.
  The plot should look like Figure 6.

# COMPONENT I (COMPI)

In the second part of the model, we add a Deformed Geometry node to investigate the impact of deformation due to dissolution on the stress distribution and hence on the corrosion.

Deforming Domain I

- I In the Physics toolbar, click • Deformed Geometry and choose Free Deformation.
- 2 In the Settings window for Deforming Domain, locate the Smoothing section.
- **3** From the Mesh smoothing type list, choose Hyperelastic.

# SECONDARY CURRENT DISTRIBUTION (CD)

Next, add a dissolving-depositing species to capture dissolution at the electrode surface.

Internal Electrode Surface I

- I In the Model Builder window, under Component I (compl)> Secondary Current Distribution (cd) click Internal Electrode Surface 1.
- 2 In the Settings window for Internal Electrode Surface, click to expand the Dissolving-**Depositing Species** section.
- 3 Click + Add.
- **4** In the table, enter the following settings:

Species	Density (kg/m^3)	Molar mass (kg/mol)
s1	rho_Fe	M_Fe

Electrode Reaction I

- I In the Model Builder window, click Electrode Reaction I.
- 2 In the Settings window for Electrode Reaction, locate the Stoichiometric Coefficients section.
- 3 In the Stoichiometric coefficients for dissolving-depositing species: table, enter the following settings:

Species	Stoichiometric coefficient (I)
sl	1

# MULTIPHYSICS

Next, set multiphysics features for deformed geometry.

Nondeforming Boundary I (ndbdg1)

- I In the Physics toolbar, click Multiphysics Couplings and choose Boundary> Nondeforming Boundary.
- 2 In the Settings window for Nondeforming Boundary, locate the Boundary Selection section.
- 3 From the Selection list, choose All boundaries.
- 4 Locate the Nondeforming Boundary section. From the Boundary condition list, choose Zero normal displacement.

Deforming Electrode Surface I (desdg1)

I In the Physics toolbar, click Multiphysics Couplings and choose Boundary> **Deforming Electrode Surface.** 

- 2 In the Settings window for Deforming Electrode Surface, locate the Boundary Selection section.
- 3 From the Selection list, choose All boundaries.

# STUDY: STATIONARY PARAMETRIC

Before setting up a transient study, disable the appropriate nodes in the Stationary Parametric study for completeness.

# Step 1: Stationary

- I In the Model Builder window, under Study: Stationary Parametric click Step 1: Stationary.
- 2 In the Settings window for Stationary, locate the Physics and Variables Selection section.
- **3** In the table, enter the following settings:

Physics interface	Solve for	Equation form
Deformed geometry (Component I)		Automatic

**4** In the table, enter the following settings:

Multiphysics couplings	Solve for	Equation form
Nondeforming Boundary I (ndbdgI)		Automatic (Stationary)
Deforming Electrode Surface I (desdg1)		Automatic (Stationary)

# Step 2: Stationary 2

- I In the Model Builder window, click Step 2: Stationary 2.
- 2 In the Settings window for Stationary, locate the Physics and Variables Selection section.
- **3** In the table, enter the following settings:

Physics interface	Solve for	Equation form
Deformed geometry (Component I)		Automatic

**4** In the table, enter the following settings:

Multiphysics couplings	Solve for	Equation form
Nondeforming Boundary I (ndbdgI)		Automatic (Stationary)
Deforming Electrode Surface I (desdg1)		Automatic (Stationary)

#### ROOT

Finally, add a new time-dependent study to capture the deformation.

#### ADD STUDY

- I In the Home toolbar, click Add Study to open the Add Study window.
- 2 Go to the Add Study window.
- 3 Find the Studies subsection. In the Select Study tree, select General Studies> Time Dependent.
- 4 Click Add Study in the window toolbar.
- 5 In the Home toolbar, click Add Study to close the Add Study window.

#### STUDY 2

## Step 1: Time Dependent

- I In the Settings window for Time Dependent, locate the Study Settings section.
- 2 From the Time unit list, choose a.
- 3 In the Output times text field, type range (0, 1, 20).
- 4 Click to expand the Values of Dependent Variables section. Find the **Initial values of variables solved for subsection.** From the **Settings** list, choose User controlled.
- **5** From the **Method** list, choose **Solution**.
- 6 From the Study list, choose Study: Stationary Parametric, Stationary 2.
- 7 From the Solution list, choose Parametric Solutions I (sol3).
- 8 In the Model Builder window, click Study 2.
- 9 In the Settings window for Study, type Study: Transient, Deformed Geometry in the **Label** text field.
- 10 Locate the Study Settings section. Clear the Generate default plots check box.

#### Solution 8 (sol8)

- 2 In the Model Builder window, expand the Solution 8 (sol8) node.
- 3 In the Model Builder window, expand the Study: Transient, Deformed Geometry> Solver Configurations>Solution 8 (sol8)>Time-Dependent Solver I node, then click Fully Coupled 1.
- 4 In the Settings window for Fully Coupled, click to expand the Method and Termination section.

- 5 In the Maximum number of iterations text field, type 12.
- 6 In the Study toolbar, click **Compute**.

#### RESULTS

Corrosion Defect Profile

Now, plot the corrosion defect profile for the first and last time steps.

- I In the Home toolbar, click Add Plot Group and choose ID Plot Group.
- 2 In the Settings window for ID Plot Group, type Corrosion Defect Profile in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study: Transient, Deformed Geometry/Solution 8 (sol8).
- 4 From the Time selection list, choose From list.
- 5 In the Times (a) list, choose 0 and 20.

Line Graph 1

- I In the Corrosion Defect Profile toolbar, click Line Graph.
- 2 Select Boundaries 9 and 10 only.
- 3 In the Settings window for Line Graph, locate the y-Axis Data section.
- **4** In the **Expression** text field, type **y**.
- 5 Locate the x-Axis Data section. From the Parameter list, choose Expression.
- 6 In the Expression text field, type x.
- 7 Locate the Legends section. Select the Show legends check box.

The plot should look like Figure 7.

von Mises Stress, Parametric

Plot the von Mises stress along the corrosion defect for the first and last time steps.

In the Model Builder window, under Results right-click von Mises Stress, Parametric and choose Duplicate.

von Mises Stress, Deformed Geometry

- I In the Model Builder window, under Results click von Mises Stress, Parametric I.
- 2 In the Settings window for ID Plot Group, type von Mises Stress, Deformed Geometry in the Label text field.

- 3 Locate the Data section. From the Dataset list, choose Study: Transient, Deformed Geometry/Solution 8 (sol8).
- 4 From the Time selection list, choose From list.
- 5 In the Times (a) list, choose 0 and 20.

Line Graph 1

- I In the Model Builder window, expand the von Mises Stress, Deformed Geometry node, then click Line Graph 1.
- 2 In the Settings window for Line Graph, locate the Legends section.
- 3 From the Legends list, choose Automatic.
- 4 In the von Mises Stress, Deformed Geometry toolbar, click Plot. The plot should look like Figure 8.

Corrosion Potential, Parametric

Plot the corrosion potential along the corrosion defect for the first and last time steps.

In the Model Builder window, under Results right-click Corrosion Potential, Parametric and choose **Duplicate**.

Corrosion Potential, Deformed Geometry

- I In the Model Builder window, under Results click Corrosion Potential, Parametric I.
- 2 In the Settings window for ID Plot Group, type Corrosion Potential, Deformed Geometry in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study: Transient, Deformed Geometry/Solution 8 (sol8).
- **4** From the **Time selection** list, choose **From list**.
- 5 In the Times (a) list, choose 0 and 20.

Line Graph 1

- I In the Model Builder window, expand the Corrosion Potential, Deformed Geometry node, then click Line Graph 1.
- 2 In the Settings window for Line Graph, locate the Legends section.
- 3 From the Legends list, choose Automatic.
- 4 In the Corrosion Potential, Deformed Geometry toolbar, click **Toolbar** Plot.

The plot should look like Figure 9.

Anodic Current Density, Parametric

Plot the anodic current density along the corrosion defect for the first and last time steps.

In the Model Builder window, under Results right-click Anodic Current Density, Parametric and choose Duplicate.

Anodic Current Density, Deformed Geometry

- I In the Model Builder window, under Results click Anodic Current Density, Parametric I.
- 2 In the **Settings** window for **ID Plot Group**, type Anodic Current Density, Deformed Geometry in the **Label** text field.
- 3 Locate the Data section. From the Dataset list, choose Study: Transient, Deformed Geometry/Solution 8 (sol8).
- 4 From the Time selection list, choose From list.
- 5 In the Times (a) list, choose 0 and 20.

Line Graph 1

- I In the Model Builder window, expand the Anodic Current Density, Deformed Geometry node, then click Line Graph I.
- 2 In the Settings window for Line Graph, locate the Legends section.
- 3 From the Legends list, choose Automatic.
- 4 In the Anodic Current Density, Deformed Geometry toolbar, click Plot.

  The plot should look like Figure 10.

Cathodic Current Density, Parametric

Plot the cathodic current density along the corrosion defect for the first and last time steps.

In the Model Builder window, under Results right-click Cathodic Current Density, Parametric and choose Duplicate.

Cathodic Current Density, Deformed Geometry

- I In the Model Builder window, under Results click Cathodic Current Density, Parametric I.
- 2 In the Settings window for ID Plot Group, type Cathodic Current Density, Deformed Geometry in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study: Transient, Deformed Geometry/Solution 8 (sol8).
- 4 From the Time selection list, choose From list.
- 5 In the Times (a) list, choose 0 and 20.

Line Graph 1

I In the Model Builder window, expand the Cathodic Current Density, Deformed Geometry node, then click Line Graph I.

- 2 In the Settings window for Line Graph, locate the Legends section.
- 3 From the Legends list, choose Automatic.
- The plot should look like Figure 11.