



# Postbuckling Analysis of a Hinged Cylindrical Shell

## Introduction

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Buckling is a phenomenon that can cause sudden failure of a structure.

A linear buckling analysis predicts the critical buckling load. Such an analysis, however, does not give any information about what happens at loads higher than the critical load. Tracing the solution after the critical load is called a *postbuckling analysis*.

A linear buckling analysis also often overpredicts the load-carrying capacity of the structure.

In order to accurately determine the critical buckling load or predict the postbuckling behavior, you can use the nonlinear solver and ramp up the applied load to compute the structure deformation. The buckling load can then be based on when a certain, not acceptable, deformation is reached.

Once the critical buckling load has been reached, it can happen that the structure undergoes a sudden large deformation into a new stable configuration. This is known as a snap-through phenomenon. A snap-through process cannot be simulated using prescribed load in a standard nonlinear static solver because the problem becomes numerically singular. Physically speaking, it is a highly transient problem as the structure “jumps” from one state to another. For simple cases with a single point load, it is often possible to replace the point load with a prescribed displacement and then measure the reaction force instead.

For more general problems, the postbuckling solution must however be tracked using more sophisticated methods, as shown in this example.

Figure 1 shows the variation of load versus the displacement for such a difficult case. It illustrates the possible computational problem by using either a load control (path A) or a displacement control (path B).

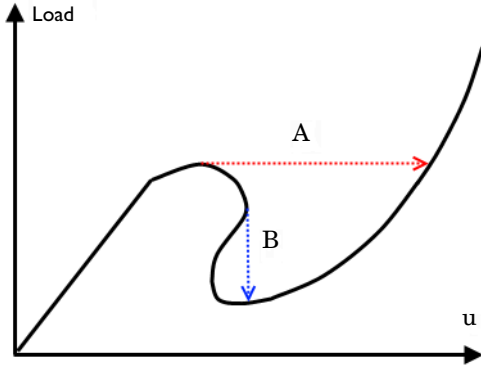


Figure 1: Load versus displacement in snap-through buckling.

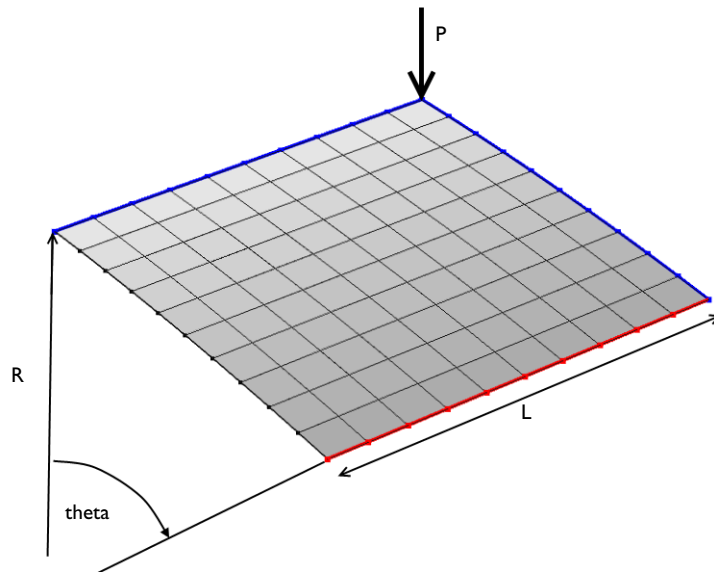
The shell structure in this example has a behavior similar to this.

### Model Definition

The model studied here is a benchmark for a hinged cylindrical panel subjected to a point load at its center; see Ref. 1.

- The radius of the cylinder is  $R = 2.54$  m and all edges have a length of  $2L = 0.508$  m. The angular span of the panel is thus 0.2 radians. The panel thickness is  $th = 6.35$  mm.
- The straight edges are hinged.
- In the study, the variation of the panel center vertical displacement with respect to the change of the applied load is of interest.

Due to the double symmetry, only one quarter of the geometry is modeled as shown in [Figure 2](#). The blue lines show the symmetry edge conditions, while the red line shows the location of the hinged edge condition.

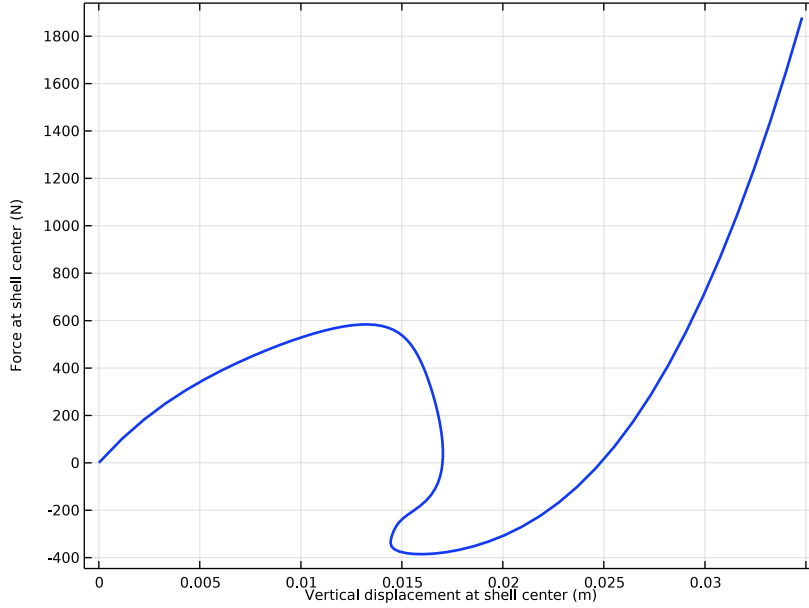


*Figure 2: Problem description.*

In general, you should be careful when using symmetry in buckling problems, because nonsymmetric solutions may exist.

## Results

In [Figure 3](#) you can see the applied load as a function of the panel center displacement. The figure shows clearly a nonunique solution for a given applied load (between -400 N to 600 N) or a given displacement (between 14.4 mm and 17 mm).



*Figure 3: Applied load versus panel center displacement.*

As shown in [Table 1](#), the results agree well with the target data from [Ref. 1](#).

TABLE 1: COMPARISON BETWEEN TARGET AND COMPUTED DATA.

Applied Load (N)	Displacement target (mm)	Displacement computed (mm)	Difference (%)
155.1	1.846	1.871	1.35
574.2	11.904	12.054	1.24
485.1	15.501	15.561	0.38
24.9	17.008	17.029	0.12
-300.3	14.520	14.538	0.12
-381.3	16.961	16.8	0.94
-1.8	24.824	24.808	0.06
1469.4	33.388	33.339	0.14

## Notes About the COMSOL Implementation

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The main feature of this model is that a limit point instability occurs at the buckling load. Neither a load control, nor a point displacement control, would be able to track the jump between the stable solution paths (see [Figure 1](#)). To solve this type of problem you can use different approaches:

- Find a proper parameter that increases monotonically. Then, use a **Global Equation** node where the load is made a function of this monotonically increasing parameter. This is the approach used in this example.. In this case, a good such parameter is the average of the displacement in the direction of the applied force. You use a nonlocal average coupling to measure the displacement and then add a global equation to compute the appropriate point load for each prescribed parameter value. There is no general way to determine which controlling parameter to use, so it is necessary to use some physical insight.
- Use an arc length method. The Application Library example [Postbuckling Analysis Using an Incremental Arc Length Method](#) demonstrates this approach. It is useful if you cannot find a suitable monotonically increasing control parameter.

## Reference

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1. K.Y. Sze, X.H. Liua, and S.H. Lob, “Popular Benchmark Problems for Geometric Nonlinear Analysis of Shells,” *Finite Element in Analysis and Design*, vol. 40, issue 11, pp. 1551–1569, 2004.

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**Application Library path:** Structural\_Mechanics\_Module/  
Verification\_Examples/postbuckling\_shell


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## Modeling Instructions


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From the **File** menu, choose **New**.

### NEW

In the **New** window, click  **Model Wizard**.

### MODEL WIZARD

I In the **Model Wizard** window, click  **3D**.

- 2 In the **Select Physics** tree, select **Structural Mechanics>Shell (shell)**.
- 3 Click **Add**.
- 4 Click  **Study**.
- 5 In the **Select Study** tree, select **General Studies>Stationary**.
- 6 Click  **Done**.

## GLOBAL DEFINITIONS



### *Parameters I*

- 1 In the **Model Builder** window, under **Global Definitions** click **Parameters I**.
- 2 In the **Settings** window for **Parameters**, locate the **Parameters** section.
- 3 In the table, enter the following settings:


Name	Expression	Value	Description
R	2540[mm]	2.54 m	Panel radius
L	254[mm]	0.254 m	Panel length
thic	6.35[mm]	0.00635 m	Panel thickness
theta	0.1[rad]	0.1 rad	Panel section angle
E0	3.103[GPa]	3.103E9 Pa	Young's modulus
nu0	0.3	0.3	Poisson's ratio
disp	0	0	Displacement parameter

## GEOMETRY I

### *Work Plane I (wp1)*

- 1 In the **Geometry** toolbar, click  **Work Plane**.
- 2 In the **Settings** window for **Work Plane**, locate the **Plane Definition** section.
- 3 From the **Plane** list, choose **xz-plane**.
- 4 Click  **Go to Plane Geometry**.

### *Work Plane I (wp1)>Line Segment I (ls1)*

- 1 In the **Work Plane** toolbar, click  **More Primitives** and choose **Line Segment**.
- 2 In the **Settings** window for **Line Segment**, locate the **Starting Point** section.
- 3 From the **Specify** list, choose **Coordinates**.
- 4 Locate the **Endpoint** section. From the **Specify** list, choose **Coordinates**.
- 5 Locate the **Starting Point** section. In the **yw** text field, type R.

6 Locate the **Endpoint** section. In the **xw** text field, type L and **yw** to R.

7 Click  **Build Selected**.

*Revolve I (revl)*

1 In the **Model Builder** window, right-click **Geometry 1** and choose **Revolve**.

2 In the **Settings** window for **Revolve**, locate the **Revolution Angles** section.

3 Click the **Angles** button.


4 In the **End angle** text field, type theta.

5 Locate the **Revolution Axis** section. Find the **Direction of revolution axis** subsection. In the **xw** text field, type 1.

6 In the **yw** text field, type 0.

7 Click  **Build Selected**.

**DEFINITIONS**

Click the  **Zoom Extents** button in the **Graphics** toolbar.

*Average I (aveop1)*

1 In the **Definitions** toolbar, click  **Nonlocal Couplings** and choose **Average**.

2 In the **Settings** window for **Average**, locate the **Source Selection** section.

3 From the **Geometric entity level** list, choose **Boundary**.

4 Select Boundary 1 only.

*Integration I (intop1)*


1 In the **Definitions** toolbar, click  **Nonlocal Couplings** and choose **Integration**.

2 In the **Settings** window for **Integration**, locate the **Source Selection** section.

3 From the **Geometric entity level** list, choose **Point**.

4 Select Point 4 only.

*Variables I*

1 In the **Definitions** toolbar, click  **Local Variables**.

2 In the **Settings** window for **Variables**, locate the **Variables** section.

3 In the table, enter the following settings:

Name	Expression	Unit
w_center	-intop1(w)	m



## SHELL (SHELL)


### Thickness and Offset 1

- 1 In the **Model Builder** window, under **Component 1 (comp1)>Shell (shell)** click **Thickness and Offset 1**.
- 2 In the **Settings** window for **Thickness and Offset**, locate the **Thickness and Offset** section.
- 3 In the  $d_0$  text field, type **thic**.

### Symmetry 1

- 1 In the **Physics** toolbar, click  **Edges** and choose **Symmetry**.
- 2 Select Edge 3 only.

### Symmetry 2

- 1 In the **Physics** toolbar, click  **Edges** and choose **Symmetry**.
- 2 Select Edge 4 only.
- 3 In the **Settings** window for **Symmetry**, locate the **Coordinate System Selection** section.
- 4 From the **Coordinate system** list, choose **Global coordinate system**.
- 5 Locate the **Symmetry** section. From the **Symmetry plane normal** list, choose **First axis**.

### Pinned 1

- 1 In the **Physics** toolbar, click  **Edges** and choose **Pinned**.
- 2 Select Edge 2 only.


### Point Load 1

- 1 In the **Physics** toolbar, click  **Points** and choose **Point Load**.
- 2 Select Point 4 only.


Apply 1/4th of the total load because of the double symmetry used in this model.

- 3 In the **Settings** window for **Point Load**, locate the **Force** section.
- 4 Specify the  $\mathbf{F}_P$  vector as





0	x
0	y
-P/4	z

- 5 Click the  **Show More Options** button in the **Model Builder** toolbar.
- 6 In the **Show More Options** dialog box, in the tree, select the check box for the node **Physics>Equation-Based Contributions**.
- 7 Click **OK**.

### Global Equations I

- 1 In the **Physics** toolbar, click  **Global** and choose **Global Equations**.
- 2 In the **Settings** window for **Global Equations**, locate the **Global Equations** section.
- 3 In the table, enter the following settings:

Name	$f(u, ut, utt, t)$ (I)	Initial value ( $u_0$ ) (I)	Initial value ( $u_{t0}$ ) (I/s)	Description
P	aveop1(-w)-disp	0	0	Force at shell center

- 4 Locate the **Units** section. Click  **Select Dependent Variable Quantity**.
- 5 In the **Physical Quantity** dialog box, type force in the text field.
- 6 Click  **Filter**.
- 7 In the tree, select **General>Force (N)**.
- 8 Click **OK**.
- 9 In the **Settings** window for **Global Equations**, locate the **Units** section.
- 10 Click  **Select Source Term Quantity**.
- 11 In the **Physical Quantity** dialog box, type displacement in the text field.
- 12 Click  **Filter**.
- 13 In the tree, select **General>Displacement (m)**.
- 14 Click **OK**.

### MATERIALS

#### Material I (matI)

- 1 In the **Model Builder** window, under **Component I (comp1)** right-click **Materials** and choose **Blank Material**.
- 2 In the **Settings** window for **Material**, locate the **Material Contents** section.
- 3 In the table, enter the following settings:


Property	Variable	Value	Unit	Property group
Young's modulus	E	E0	Pa	Young's modulus and Poisson's ratio
Poisson's ratio	nu	nu0	I	Young's modulus and Poisson's ratio
Density	rho	0	kg/m <sup>3</sup>	Basic

**MESH I**

*Mapped I*

- 1 In the **Mesh** toolbar, click  **More Generators** and choose **Mapped**.
- 2 Select Boundary 1 only.


*Distribution I*

- 1 Right-click **Mapped I** and choose **Distribution**.
- 2 Select Edges 1 and 2 only.
- 3 In the **Settings** window for **Distribution**, locate the **Distribution** section.
- 4 In the **Number of elements** text field, type 10.
- 5 Click  **Build Selected**.

**STUDY I**

*Step 1: Stationary*

Set up an auxiliary continuation sweep for the **disp** parameter.


- 1 In the **Model Builder** window, under **Study I** click **Step 1: Stationary**.
- 2 In the **Settings** window for **Stationary**, click to expand the **Study Extensions** section.
- 3 Select the **Auxiliary sweep** check box.
- 4 Click  **Add**.
- 5 In the table, enter the following settings:


Parameter name	Parameter value list
disp (Displacement parameter)	range ( 0 , 2e - 4 , 1 )

- 6 Locate the **Study Settings** section. Select the **Include geometric nonlinearity** check box.  
Sometimes it is not straightforward to guess the maximum value of the parameter used. You can then instead set a stop condition for the parametric solver based on something that is known.
- 7 In the **Model Builder** window, click **Study I**.
- 8 In the **Settings** window for **Study**, type Postbuckling Study in the **Label** text field.


*Solution I (sol1)*

- 1 In the **Study** toolbar, click  **Show Default Solver**.
- 2 In the **Model Builder** window, expand the **Solution I (sol1)** node.

- 3 In the **Model Builder** window, expand the **Postbuckling Study>Solver Configurations>Solution 1 (sol1)>Stationary Solver 1** node.
- 4 Right-click **Postbuckling Study>Solver Configurations>Solution 1 (sol1)>Stationary Solver 1>Parametric 1** and choose **Stop Condition**.
- 5 In the **Settings** window for **Stop Condition**, locate the **Stop Expressions** section.
- 6 Click  **Add**.
- 7 In the table, enter the following settings:


Stop expression	Stop if	Active	Description
comp1.w_center>0.035	True ( $\geq 1$ )		Stop expression 1

Specify that the solution is to be stored just before the stop condition is reached.

- 8 Locate the **Output at Stop** section. From the **Add solution** list, choose **Step before stop**.
- 9 Clear the **Add warning** check box.
- 10 In the **Model Builder** window, under **Postbuckling Study>Solver Configurations>Solution 1 (sol1)** click **Stationary Solver 1**.
- 11 In the **Settings** window for **Stationary Solver**, click to expand the **Output** section.
- 12 Clear the **Reaction forces** check box.
- 13 Click  **Compute**.

## RESULTS

### *Evaluation Group: Force vs. Displacement*


- 1 In the **Results** toolbar, click  **Evaluation Group**.
- 2 In the **Settings** window for **Evaluation Group**, type Evaluation Group: Force vs. Displacement in the **Label** text field.

### *Point Evaluation 1*


- 1 Right-click **Evaluation Group: Force vs. Displacement** and choose **Point Evaluation**.
- 2 Select Point 4 only.
- 3 In the **Settings** window for **Point Evaluation**, locate the **Expressions** section.
- 4 In the table, enter the following settings:

Expression	Unit	Description
w_center	m	Vertical displacement at shell center
P	N	Force at shell center


#### *Evaluation Group: Force vs. Displacement*

- 1 In the **Model Builder** window, click **Evaluation Group: Force vs. Displacement**.
- 2 In the **Settings** window for **Evaluation Group**, click to expand the **Format** section.
- 3 From the **Include parameters** list, choose **Off**.
- 4 In the **Evaluation Group: Force vs. Displacement** toolbar, click  **Evaluate**.

#### *Force vs. Displacement*

- 1 In the **Home** toolbar, click  **Add Plot Group** and choose **ID Plot Group**.
- 2 In the **Settings** window for **ID Plot Group**, type Force vs. Displacement in the **Label** text field.
- 3 Locate the **Plot Settings** section.
- 4 Select the **x-axis label** check box. In the associated text field, type Vertical displacement at shell center (m).
- 5 Select the **y-axis label** check box. In the associated text field, type Force at shell center (N).

#### *Table Graph 1*

- 1 Right-click **Force vs. Displacement** and choose **Table Graph**.
- 2 In the **Settings** window for **Table Graph**, locate the **Data** section.
- 3 From the **Source** list, choose **Evaluation group**.
- 4 In the **Force vs. Displacement** toolbar, click  **Plot**.

