

# Carburization and Quenching of a Steel Gear

In this model, a steel gear is first carburized in a carbon rich atmosphere. Diffusion of carbon into the surface lowers the martensite start temperature, and thereby delays the onset of transformation. Quenching of the carburized gear is then performed. The quenching simulation includes heat transport in the gear, phase transformations, and computation of residual stresses.

# Model Definition

A 2D spur gear is used to build a model for the carburization and quenching processes. The spur gear has a pitch diameter of 100 mm and twenty teeth, see Figure 1. Because of symmetries, half a gear segment is included in the model, and corresponding boundary conditions are applied. The 2D model is meant to represent a center cut of the spur gear. A generalized plane strain assumption is used.

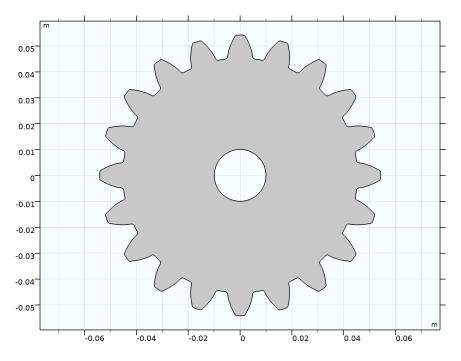


Figure 1: The 2D spur gear.

Figure 2 shows the geometry of the gear segment. During carburization, flux of carbon is possible along the tooth surface and along the center hole (dashed, blue lines). Along the symmetry planes, there is zero carbon flux. During quenching, the rollers shown in the figure indicate applied displacement symmetry boundary conditions. Heat flux to the surrounding quenching oil is possible though the tooth surface, and along the center hole (dashed, blue lines).

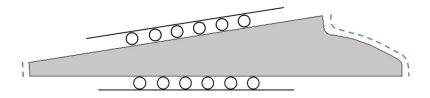


Figure 2: Boundary condition regions: Rollers indicate displacement symmetry boundary conditions. The dashed lines in blue indicate boundaries on which flux boundary conditions are applied.

# MATERIAL PROPERTIES

The material properties of the gear are temperature-dependent, and also depend on phase composition. The Austenite Decomposition physics interface automatically averages these properties into effective properties that define a compound material. The compound material is used in the thermal and mechanical analyses.

# CARBURIZATION ANALYSIS

The process of carburization involves heating a steel component and exposing it to a carbon rich environment, such as carbon monoxide. When done correctly, carburization followed by quenching can produce compressive stresses at the surface of a component, which is beneficial from a fatigue standpoint. In this model, it is assumed that the carbon content of the austenite is c=0.2%, and that the so-called carbon potential of the surrounding atmosphere is  $c_{\rm env}=0.75\%$ . A simple carburization process is modeled using the transient Fick's law:

$$\frac{\partial c}{\partial t} + (-D_{c} \nabla^{2} c) = 0$$

where the diffusion constant is  $D_{\rm c} = 2 \cdot 10^{-7} \, {\rm cm}^2/{\rm s}$ .

**Boundary Conditions** 

Diffusion of carbon from the surrounding environment occurs through a boundary flux of the form

$$\mathbf{n} \cdot (D_c \nabla c) = k_c (c_{\text{env}} - c)$$

with the assumed mass transfer coefficient  $k_c = 2 \cdot 10^{-5}$  cm/s. The carburization process is taken to occur over a period of twelve hours, during which carbon diffuses from the surface and into the material.

#### PHASE TRANSFORMATION ANALYSIS

In this analysis, it is assumed that austenite decomposes into martensite only. This phase transformation is displacive and described by the Koistinen-Marburger model. The model states that the amount of martensite formed at the expense of austenite depends on the fraction of available austenite, and under-cooling below the so-called martensite start temperature  $M_s$ . On differential form, the model is given by

$$\dot{\xi}^{\mathbf{d}} = -\xi^{\mathbf{s}} \beta \dot{T}$$

where the rate at which the destination phase (martensite) forms is proportional to the temperature rate and the instantaneous fraction of the source phase (austenite), through a the Koistinen–Marburger coefficient  $\beta$ . The start temperature  $M_s$  depends on the carbon content. Here a simple linear relationship is assumed:

$$M_s = (560 - 470 \times c)^{\circ} \text{C}$$

where the carbon concentration is c. The Koistinen–Marburger coefficient is given as  $\beta$ =0.011/K. Note that the start temperature decreases with increasing carbon content, which means that martensite may well begin to form inside the surface of the gear, as a result of the carburization.

# THERMAL ANALYSIS

The heat transport in the bar is described by the heat equation:

$$\rho C_p \frac{\partial T}{\partial t} + \nabla \cdot (-k \nabla T) = 0$$

where T is the temperature, k represents the thermal conductivity,  $\rho$  denotes the density,  $C_p$  denotes the specific heat capacity. In the equation above, the effect of latent heat of phase transformation has been neglected. The thermal conductivity, the density, and the specific heat capacity are in general temperature dependent, and in the presence of metallurgical phase transformations, they also depend on the current phase composition.

# Material Properties

The densities, specific heat capacities and heat conductivities of austenite and martensite are given in Table 1. It is assumed that densities are not temperature dependent.

TABLE I: TEMPERATURE-DEPENDENT THERMAL MATERIAL PROPERTIES.

Temperature (°C)	$\rho$ (kg/m <sup>3</sup> )	C <sub>p</sub> (J/(kg·K))	<b>k (</b> W/(m·K))
Austenite			
0	7930	520	15
300		560	20
600		590	22
900		620	25
Martensite			
0	7850	480	44
300		570	38
600		640	30
900		650	24

# **Boundary Conditions**

The quenching oil is not modeled explicitly, but it is replaced by a temperature-dependent heat-transfer coefficient h that is used to prescribe a heat flux as

$$q_0 = h(T)(T_{\text{ext}} - T)$$

where  $T_{\rm ext}$  = 80°C is the temperature of the quenching oil. The heat-transfer properties of the quenching oil are shown in Table 2.

TABLE 2: HEAT-TRANSFER COEFFICIENT OF THE QUENCHING OIL.

Temperature (°C)	h (W/(m <sup>2</sup> ·K))
0	200
300	200
500	2800
650	750
1300	750

#### MECHANICAL ANALYSIS

The quenching process is time dependent, but from a structural-mechanics point of view it is quasi static, and modeled as such. Stresses and strains are computed using material properties of the compound material defined by the phase composition and the constitutive behavior of the individual phases, here austenite and martensite.

# Material Properties

As in the thermal analysis, the mechanical analysis involves material properties that are temperature as well as phase composition dependent. In this model, the elastoplastic behavior of austenite and martensite is taken to be linear elastic with linear hardening. The properties for austenite and martensite are shown in Table 3. The linear elastic behavior is given by the Young's moduli (E) and Poisson's ratios (v) of the phases, and the plastic behavior is given by initial yield stresses ( $\sigma_{vs0}$ ) and isotropic hardening moduli (h). In this model, the elastic behavior of austenite and martensite is assumed equal. Note that the secant coefficients of thermal expansion ( $\alpha$ ) are not averaged into a compound material property, but are instead used to compute the thermal strain tensor of each metallurgical phase. The thermal strain tensors are averaged into a thermal strain of the compound material.

TABLE 3: TEMPERATURE-DEPENDENT MECHANICAL MATERIAL PROPERTIES.

Temperature (°C)	E (GPa)	ν	$\sigma_{ys0}$ (MPa)	h (GPa)	α (I/K)
Austenite					
0	210	0.3	200	1	22·10 <sup>-6</sup>
300	180		135	15	
600	165		40	П	
900	120		36	0.6	
Martensite					14·10 <sup>-6</sup>
0	210	0.3	1600	I	
300	180		1500	15	
600	165		1400	П	
900	120		100	0.6	

To complete the description of the phase properties, a volume reference temperature  $T_{\rm ref}$ has to be defined for the phases. In this model, the heating stage (austenitization) is not considered explicitly, so the volume reference temperature is set to the austenitization temperature (900°C). This means that the gear is strain free at this temperature.

# Boundary Conditions and Constraints

Because of symmetries, displacement boundary conditions are applied according to Figure 2, where the rollers indicate that displacements normal to the surface are prescribed to be zero. The gear segment is modeled using generalized plane strain to allow for out-of-plane strains. Only normal out-of-plane strains are allowed.

# Initial Strains from Heating and Austenitization

To account for the strains that follow from thermal expansion and austenitization of the (unknown) base phase composition, an initial strain is applied. The initial strain is given by

$$\varepsilon_0 = 5 \cdot 10^{-3} \cdot \left( \begin{array}{c} 1 \ 0 \ 0 \\ 0 \ 1 \ 0 \\ 0 \ 0 \ 1 \end{array} \right)$$

# Transformation Induced Plasticity (TRIP)

In general, phase transformations occur while the material is subjected to a mechanical stress. This gives rise to so-called transformation induced plasticity, or TRIP. In essence, an inelastic straining of the material results from stresses that are below the yield stress, and would not cause plastic flow in a classical plasticity sense. In this model, the TRIP effect is included in the transformation from austenite to martensite. Two parameters are required to describe the effect: the parameter  $K_{\mathrm{S} \to \mathrm{d}}^{\mathrm{TRIP}}$  and the saturation function  $\Phi$ . For the present model, the default parameter value is used, and the Desalos saturation function is used.

#### Phase Plasticity

During a quenching process, each phase may undergo plastic straining. By default, the equivalent plastic strain of the individual phases follows that of the compound material. That is to say, the equivalent plastic strain of a given phase in the Austenite Decomposition interface is equal to the equivalent plastic strain of a Plasticity node under Solid Mechanics. This equivalence is established through the Phase Transformation Strain multiphysics coupling. For the vanishing austenite, this is a reasonable modeling assumption. However, for phases that appear gradually and devoid of prior plastic straining, this assumption is questionable. This deficiency can be remedied by allowing for plastic recovery of the destination phase. In this model, the plastic recovery option is therefore used for the martensite. In the computation of an initial yield stress for the compound material, a linear averaging between phases is often adequate as long as the phases are of similar hardness. In the case where one phase is significantly harder than the others, this averaging scheme can be amended by giving the hard phase stronger influence on the compound material behavior. To this end, the description by Geijselaers (Ref. 1) is used to modify the weighting of the martensite initial yield stress.

During carburization, the amount of carbon in the austenite increases because of diffusion into the surface of the gear. After the carburization period of twelve hours, the mass percent of carbon at the surface has almost saturated to the surrounding level, see Figure 3. The influence of the carburization process is mainly affecting the surfaces of the gear, while the interior remains at its initial carbon content.

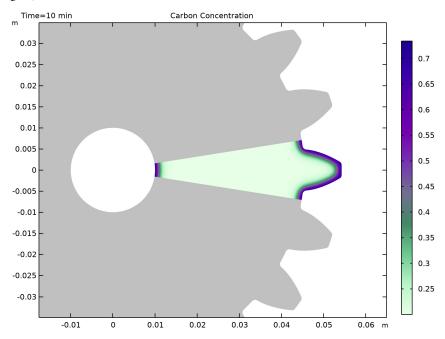


Figure 3: Carbon content in the gear after carburization.

One reason for performing the carburization is to alter the phase transformation characteristics by changing the carbon content. Figure 4 shows how the martensite start temperature has been affected by the carburization process. In the vicinity of the surfaces, where the carbon content is the highest, the martensite start temperature is lower than in the interior. During cooling, it is therefore likely that austenite on the inside of the gear transforms to martensite before the surface does.

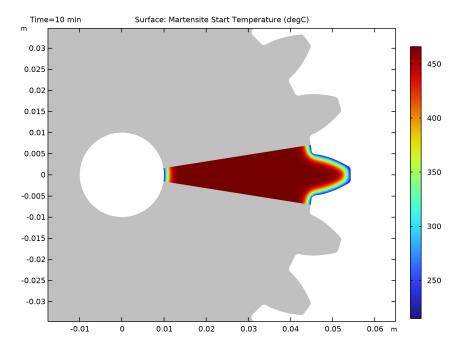


Figure 4: Computed martensite start temperature resulting from the carburization.

During quenching, the austenite is cooled, and the onset of martensitic transformation is determined by the computed start temperatures. From a fatigue standpoint, it is well known that residual compressive stresses are beneficial. During service, gear teeth will experience high cycle fatigue loading, and a critical location is often near the root of each gear tooth, where tensile stresses may cause fatigue. In Figure 5, the second principal stress is displayed. High compressive stresses appear at the root of the tooth, and the entire gear tooth surface experiences compressive stresses.

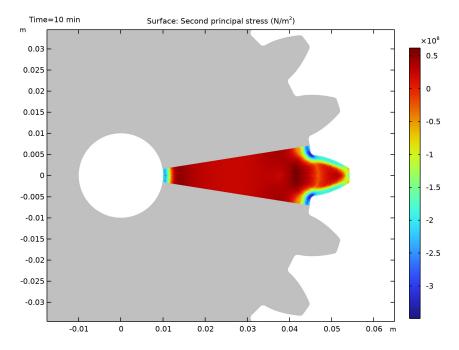


Figure 5: Residual stress state in the gear after quenching.

# Reference

1. H.J.M. Geijselaers, Numerical simulation of stresses due to solid state transformations: The simulation of laser hardening, doctoral dissertation, Univ. of Twente, Enschede, 2003.

Application Library path: Metal\_Processing\_Module/Steel\_Quenching/ carburization\_and\_quenching\_of\_a\_steel\_gear

# Modeling Instructions

From the File menu, choose New.

#### NEW

In the New window, click Model Wizard.

# MODEL WIZARD

- I In the Model Wizard window, click **2** 2D.
- 2 In the Select Physics tree, select Heat Transfer>Metal Processing>Steel Quenching.
- 3 Click Add.
- 4 In the Select Physics tree, select Heat Transfer>Metal Processing>Carburization (carb).
- 5 Click Add.
- 6 Click Study.
- 7 In the Select Study tree, select General Studies>Time Dependent.
- 8 Click **Done**.

# **GLOBAL DEFINITIONS**

#### Parameters 1

- I In the Model Builder window, under Global Definitions click Parameters I.
- 2 In the Settings window for Parameters, locate the Parameters section.
- **3** In the table, enter the following settings:

Name	Expression	Value	Description
cenv	0.75	0.75	Carbon potential
c0	0.2	0.2	Initial carbon concentration
Dc	2e-7[cm^2/s]	2E-II m <sup>2</sup> /s	Carbon diffusion coefficient
kc	2e-5[cm/s]	2E-7 m/s	Mass transfer coefficient

# PART LIBRARIES

- I In the Home toolbar, click Windows and choose Part Libraries.
- 2 In the Model Builder window, under Component I (compl) click Geometry I.
- 3 In the Part Libraries window, select Multibody Dynamics Module>2D>External Gears> spur\_gear\_2d in the tree.
- 4 Click Add to Geometry.

#### **GEOMETRY I**

Spur Gear (2D) I (bil)

- I In the Model Builder window, under Component I (compl)>Geometry I click Spur Gear (2D) I (pil).
- 2 In the Settings window for Part Instance, click **Build All Objects**.

Square I (sql)

- I In the Geometry toolbar, click Square.
- 2 In the Settings window for Square, locate the Size section.
- 3 In the Side length text field, type 0.06.

Square 2 (sq2)

- I In the Geometry toolbar, click Square.
- 2 In the Settings window for Square, locate the Size section.
- 3 In the Side length text field, type 0.06.
- **4** Locate the **Rotation Angle** section. In the **Rotation** text field, type 9.

Intersection I (intl)

- I In the Geometry toolbar, click Booleans and Partitions and choose Intersection.
- 2 Select the objects pil and sql only.

Difference I (dif1)

- I In the Geometry toolbar, click Booleans and Partitions and choose Difference.
- 2 Select the object intl only.
- 3 In the Settings window for Difference, locate the Difference section.
- 4 Click to select the **Activate Selection** toggle button for **Objects to subtract**.
- **5** Select the object **sq2** only.
- 6 Click **Build All Objects**.

# CARBURIZATION (CARB)

- I In the Model Builder window, under Component I (compl) click Carburization (carb).
- 2 In the Settings window for Carburization, locate the Carburizing Cycle section.
- 3 From the Carbon potential model list, choose User defined.
- **4** In the  $c_{pot}$  text field, type cenv.

Carbon Flux I

In the Physics toolbar, click — Boundaries and choose Carbon Flux.

# Carburization I

- I In the Model Builder window, click Carburization I.
- 2 In the Settings window for Carburization, locate the Carbon Diffusion section.
- **3** In the  $D_0$  text field, type Dc.
- 4 From the Diffusion coefficient list, choose User defined.
- **5** In the *D* text field, type Dc.

#### Initial Values 1

- I In the Model Builder window, click Initial Values I.
- 2 In the Settings window for Initial Values, locate the Initial Values section.
- **3** In the c text field, type c0.

# Carbon Flux I

- I In the Model Builder window, click Carbon Flux I.
- 2 Select Boundaries 3–8 only.
- 3 In the Settings window for Carbon Flux, locate the Carbon Mass Transfer section.
- 4 From the Mass transfer coefficient list, choose User defined.
- **5** In the *b* text field, type kc.

#### MESH I

- I In the Model Builder window, under Component I (compl) click Mesh I.
- 2 In the Settings window for Mesh, locate the Sequence Type section.
- **3** From the list, choose **User-controlled mesh**.

#### Size

- I In the Model Builder window, under Component I (compl)>Mesh I click Size.
- 2 In the Settings window for Size, locate the Element Size section.
- 3 From the Predefined list, choose Extra fine.

# Size 1

- I In the Model Builder window, right-click Mesh I and choose Size.
- 2 Drag and drop Size I below Size.
- 3 In the Settings window for Size, locate the Element Size section.
- 4 Click the **Custom** button.
- 5 Locate the Element Size Parameters section.
- 6 Select the Maximum element size check box. In the associated text field, type 0.3[mm].

- 7 Locate the Geometric Entity Selection section. From the Geometric entity level list, choose Boundary.
- **8** Select Boundaries 3–8 only.
- 9 Click III Build All.

#### CARBURIZATION

- I In the Model Builder window, click Study I.
- 2 In the Settings window for Study, type Carburization in the Label text field.

# Step 1: Time Dependent

- I In the Model Builder window, under Carburization click Step 1: Time Dependent.
- 2 In the Settings window for Time Dependent, locate the Study Settings section.
- **3** From the **Time unit** list, choose **h**.
- 4 In the Output times text field, type range (0,0.1,12).
- 5 Locate the Physics and Variables Selection section. In the table, clear the Solve for check boxes for Heat Transfer in Solids (ht), Solid Mechanics (solid), and Austenite Decomposition (audc).
- 6 In the table, clear the Solve for check boxes for Phase Transformation Latent Heat I (IhtI) and Phase Transformation Strain I (ptstrl).
- 7 In the Home toolbar, click **Compute**.

#### **GLOBAL DEFINITIONS**

Interpolation | (int |)

- I In the Home toolbar, click f(x) Functions and choose Global>Interpolation.
- 2 In the Settings window for Interpolation, locate the Definition section.
- 3 In the Function name text field, type htc.
- 4 Click **Load from File**.
- **5** Browse to the model's Application Libraries folder and double-click the file carburization\_and\_quenching\_of\_a\_steel\_gear\_htc.txt.
- **6** Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	degC

7 In the **Function** table, enter the following settings:

Function	Unit
htc	W/(m^2*K)

Analytic I (an I)

- I In the Home toolbar, click f(x) Functions and choose Global>Analytic.
- 2 In the Settings window for Analytic, type Ms in the Function name text field.
- 3 Locate the **Definition** section. In the **Expression** text field, type 560-470\*carb.c.
- 4 In the Arguments text field, type carb.c.
- **5** Locate the **Units** section. In the table, enter the following settings:

Argument	Unit
carb.c	1

6 In the Function text field, type degC.

Interpolation 2 (int2)

- I In the Home toolbar, click f(x) Functions and choose Global>Interpolation.
- 2 In the Settings window for Interpolation, locate the Definition section.
- 3 In the Function name text field, type EYoung.
- 4 Click **Load from File**.
- **5** Browse to the model's Application Libraries folder and double-click the file carburization\_and\_quenching\_of\_a\_steel\_gear\_EYoung.txt.
- **6** Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	degC

7 In the Function table, enter the following settings:

Function	Unit
EYoung	GPa

# **HEAT TRANSFER IN SOLIDS (HT)**

Initial Values 1

I In the Model Builder window, under Component I (compl)>Heat Transfer in Solids (ht) click Initial Values I.

- 2 In the Settings window for Initial Values, locate the Initial Values section.
- 3 In the T text field, type 900[degC].

# Symmetry I

- I In the Physics toolbar, click Boundaries and choose Symmetry.
- 2 Select Boundaries 1 and 2 only.

# Heat Flux 1

- I In the Physics toolbar, click 
  Boundaries and choose Heat Flux.
- 2 Select Boundaries 3–8 only.
- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 From the Flux type list, choose Convective heat flux.
- **5** In the h text field, type htc(T).
- **6** In the  $T_{\rm ext}$  text field, type 80[degC].

# SOLID MECHANICS (SOLID)

- I In the Model Builder window, under Component I (compl) click Solid Mechanics (solid).
- 2 In the Settings window for Solid Mechanics, locate the 2D Approximation section.
- 3 From the list, choose Generalized plane strain.
- 4 Clear the Enable out-of-plane bending check box.

# Linear Elastic Material I

In the Model Builder window, under Component I (compl)>Solid Mechanics (solid) click Linear Elastic Material I.

# Plasticity 1

- I In the Physics toolbar, click Attributes and choose Plasticity.
- 2 In the Settings window for Plasticity, locate the Plasticity Model section.
- 3 Find the Isotropic hardening model subsection. From the list, choose Hardening function.

#### Linear Elastic Material I

In the Model Builder window, click Linear Elastic Material 1.

# Initial Stress and Strain I

- I In the Physics toolbar, click Attributes and choose Initial Stress and Strain.
- 2 In the Settings window for Initial Stress and Strain, locate the Initial Stress and Strain section.

**3** In the  $\varepsilon_0$  table, enter the following settings:

0.005	0	0
0	0.005	0
0	0	0.005

# Symmetry I

- I In the Physics toolbar, click Boundaries and choose Symmetry.
- 2 Select Boundaries 1 and 2 only.

Disable phases and phase transformations that are not present in the analysis.

# AUSTENITE DECOMPOSITION (AUDC)

Austenite to Bainite, Austenite to Ferrite, Austenite to Pearlite, Bainite, Ferrite, Pearlite

- I In the Model Builder window, under Component I (compl)>Austenite Decomposition (audc), Ctrl-click to select Ferrite, Pearlite, Bainite, Austenite to Ferrite,

  Austenite to Pearlite, and Austenite to Bainite.
- 2 Right-click and choose Disable.

#### Austenite

- I In the Model Builder window, click Austenite.
- 2 In the Settings window for Metallurgical Phase, locate the Model Input section.

# SHARED PROPERTIES

# Model Input 1

- I In the Model Builder window, under Component I (compl)>Definitions>Shared Properties click Model Input I.
- 2 In the Settings window for Model Input, locate the Definition section.
- 3 In the text field, type 900 [degC].

# AUSTENITE DECOMPOSITION (AUDC)

- I In the Model Builder window, under Component I (compl) click Austenite Decomposition (audc).
- 2 In the Settings window for Austenite Decomposition, locate the Material Properties section.
- **3** Click **Create Compound Material** in the upper-right corner of the section.

- 4 Locate the Heat Transfer section. Clear the Enable phase transformation latent heat check box.
- 5 Locate the Solid Mechanics section. Select the Enable phase plasticity check box.

- I In the Model Builder window, under Component I (compl)> Austenite Decomposition (audc) click Austenite.
- 2 In the Settings window for Metallurgical Phase, locate the Phase Material section.
- 3 Click Create Phase Material in the upper-right corner of the section.
- 4 Locate the Mechanical Properties section. From the Isotropic hardening model list, choose Linear

# Martensite

- I In the Model Builder window, click Martensite.
- 2 In the Settings window for Metallurgical Phase, locate the Phase Material section.
- 3 Click Create Phase Material in the upper-right corner of the section.
- **4** Locate the **Mechanical Properties** section. From the  $g(\xi)$  list, choose **Geijselaers**.
- 5 From the Soft phase list, choose Austenite.
- 6 From the Isotropic hardening model list, choose Linear.

# Austenite to Martensite

- I In the Model Builder window, click Austenite to Martensite.
- 2 In the Settings window for Phase Transformation, locate the Phase Transformation section.
- 3 In the  $M_s$  text field, type Ms(carb.c).
- 4 Locate the Phase Transformation Strain section. Select the Transformation induced plasticity check box.
- **5** From the  $\Phi$  list, choose **Desalos**.
- 6 Select the Plastic recovery for destination phase check box.

#### **GLOBAL DEFINITIONS**

Austenite (audcphase I mat)

In the Model Builder window, expand the Global Definitions>Materials node.

Interpolation I (int I)

I In the Model Builder window, expand the Austenite (audcphase I mat) node.

- 2 Right-click Global Definitions>Materials>Austenite (audcphase | mat)>Basic (def) and choose Functions>Interpolation.
- 3 In the Settings window for Interpolation, locate the Definition section.
- 4 In the Function name text field, type k.
- 5 Click Load from File.
- **6** Browse to the model's Application Libraries folder and double-click the file carburization\_and\_quenching\_of\_a\_steel\_gear\_kAustenite.txt.
- 7 Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	degC

**8** In the **Function** table, enter the following settings:

Function	Unit
k	W/(m*K)

Austenite (audcphase I mat)

- I In the Model Builder window, under Global Definitions>Materials> Austenite (audcphase I mat) click Basic (def).
- 2 In the Settings window for Basic, locate the Model Inputs section.
- 3 Click + Select Quantity.
- 4 In the Physical Quantity dialog box, select General>Temperature (K) in the tree.
- 5 Click OK.

Interpolation 2 (int2)

- I In the Home toolbar, click f(x) Functions and choose Global>Interpolation.
- 2 In the Settings window for Interpolation, locate the Definition section.
- 3 In the Function name text field, type Cp.
- 4 Click Load from File.
- **5** Browse to the model's Application Libraries folder and double-click the file carburization\_and\_quenching\_of\_a\_steel\_gear\_CpAustenite.txt.
- **6** Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	degC

7 In the **Function** table, enter the following settings:

Function	Unit			
Ср	J/(kg*K)			

Austenite (audcphase I mat)

- I In the Model Builder window, under Global Definitions>Materials> Austenite (audcphase I mat) click Basic (def).
- 2 In the Settings window for Basic, locate the Output Properties section.
- **3** In the table, enter the following settings:

Property	Variable	Expression	Unit	Size
Thermal conductivity	k_iso ; kii = k_iso, kij = 0	k(T)	W/(m·K)	3×3
Density	rho	7930	kg/m³	lxl
Heat capacity at constant pressure	Ср	Cp(T)	J/(kg·K)	lxl

- 4 In the Model Builder window, under Global Definitions>Materials> Austenite (audcphase I mat) click Thermal expansion (ThermalExpansion).
- 5 In the Settings window for Thermal Expansion, locate the Output Properties section.
- **6** In the table, enter the following settings:

Property	Variable	Expression	Unit	Size
Coefficient of thermal expansion	alpha_iso; alphaii = alpha_iso, alphaij = 0	2.2e-5	I/K	3×3

- 7 In the Model Builder window, under Global Definitions>Materials> Austenite (audcphase I mat) click Young's modulus and Poisson's ratio (Enu).
- 8 In the Settings window for Young's Modulus and Poisson's Ratio, locate the Model Inputs section.
- 9 Click + Select Quantity.
- 10 In the Physical Quantity dialog box, select General>Temperature (K) in the tree.
- II Click OK.
- 12 In the Settings window for Young's Modulus and Poisson's Ratio, locate the **Output Properties** section.

**I3** In the table, enter the following settings:

Property	Variable	Expression	Unit	Size
Young's modulus	E	EYoung(T)	Pa	lxl
Poisson's ratio	nu	0.3	I	lxl

14 In the Model Builder window, under Global Definitions>Materials> Austenite (audcphase I mat) click Elastoplastic material model (Elastoplastic Model).

15 In the Settings window for Elastoplastic Material Model, locate the Model Inputs section.

16 Click + Select Quantity.

17 In the Physical Quantity dialog box, select General>Temperature (K) in the tree.

18 Click OK.

Interpolation | (int |)

- I In the Home toolbar, click f(x) Functions and choose Global>Interpolation.
- 2 In the Settings window for Interpolation, locate the Definition section.
- 3 In the Function name text field, type sY.
- 4 Click Load from File.
- **5** Browse to the model's Application Libraries folder and double-click the file carburization and quenching of a steel gear sYAustenite.txt.
- **6** Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	degC

7 In the **Function** table, enter the following settings:

Function	Unit
sY	MPa

Interpolation 2 (int2)

- I In the Home toolbar, click f(x) Functions and choose Global>Interpolation.
- 2 In the Settings window for Interpolation, locate the Definition section.
- 3 In the Function name text field, type h.
- 4 Click Load from File.
- **5** Browse to the model's Application Libraries folder and double-click the file carburization\_and\_quenching\_of\_a\_steel\_gear\_hardeningAustenite.txt.

**6** Locate the **Units** section. In the **Argument** table, enter the following settings:

Argument	Unit
t	degC

7 In the **Function** table, enter the following settings:

Function	Unit
h	GPa

Austenite (audchhase I mat)

- I In the Model Builder window, under Global Definitions>Materials> Austenite (audcphase I mat) click Elastoplastic material model (ElastoplasticModel).
- 2 In the Settings window for Elastoplastic Material Model, locate the Output Properties section.
- **3** In the table, enter the following settings:

Property	Variable	Expression	Unit	Size
Initial yield stress	sigmags	sY(T)	Pa	lxl
Isotropic tangent modulus	Et	h(T)	Pa	lxl

Repeat the definitions of material properties for martensite.

# ADD STUDY

- I In the Home toolbar, click Add Study to open the Add Study window.
- 2 Go to the Add Study window.
- 3 Find the Studies subsection. In the Select Study tree, select General Studies> Time Dependent.
- 4 Click Add Study in the window toolbar.
- 5 In the Home toolbar, click Add Study to close the Add Study window.

# QUENCHING

- I In the Model Builder window, click Study 2.
- 2 In the Settings window for Study, type Quenching in the Label text field.

# Step 1: Time Dependent

- I In the Model Builder window, under Quenching click Step 1: Time Dependent.
- 2 In the Settings window for Time Dependent, locate the Study Settings section.

- **3** From the **Time unit** list, choose **min**.
- 4 In the Output times text field, type range (0,0.1,10).
- 5 From the Tolerance list, choose User controlled.
- 6 In the Relative tolerance text field, type 0.001.
- 7 Locate the Physics and Variables Selection section. In the table, clear the Solve for check box for Carburization (carb).
- 8 Click to expand the Values of Dependent Variables section. Find the Values of variables not solved for subsection. From the Settings list, choose User controlled.
- **9** From the **Method** list, choose **Solution**.
- 10 From the Study list, choose Carburization, Time Dependent.
- II From the Time (h) list, choose Last.
- 12 In the Home toolbar, click **Compute**.

#### RESULTS

# Mirror 2D I

- I In the Results toolbar, click More Datasets and choose Mirror 2D.
- 2 In the Settings window for Mirror 2D, locate the Data section.
- 3 From the Dataset list, choose Quenching/Solution 2 (sol2).
- 4 Locate the Axis Data section. From the Axis entry method list, choose Point and direction.
- **5** Find the **Direction** subsection. In the **Y** text field, type **0**.
- 6 In the X text field, type 1.

# Sector 2D I

- I In the Results toolbar, click More Datasets and choose Sector 2D.
- 2 In the Settings window for Sector 2D, locate the Data section.
- 3 From the Dataset list, choose Mirror 2D 1.
- 4 Locate the Symmetry section. In the Number of sectors text field, type 20.

# Carbon Concentration (carb)

- I In the Model Builder window, expand the Results>Carbon Concentration (carb) node, then click Carbon Concentration (carb).
- 2 In the Settings window for 2D Plot Group, locate the Data section.
- 3 From the Dataset list, choose Mirror 2D 1.

**4** Locate the **Plot Settings** section. Clear the **Plot dataset edges** check box.

# Surface 2

- I Right-click Carbon Concentration (carb) and choose Surface. Create a backdrop depicting the whole spur gear.
- 2 Drag and drop Surface 2 above Surface 1.
- 3 In the Settings window for Surface, locate the Data section.
- 4 From the Dataset list, choose Sector 2D 1.
- **5** Click to expand the **Title** section. From the **Title type** list, choose **None**.
- 6 Locate the Coloring and Style section. From the Coloring list, choose Uniform.
- 7 From the Color list, choose Gray.

# Martensite Start Temperature

- I In the Home toolbar, click **Add Plot Group** and choose **2D Plot Group**.
- 2 In the Settings window for 2D Plot Group, locate the Data section.
- 3 From the Dataset list, choose Mirror 2D 1.
- 4 In the Label text field, type Martensite Start Temperature.
- **5** Locate the **Plot Settings** section. Clear the **Plot dataset edges** check box.

# Surface I

- I Right-click Martensite Start Temperature and choose Surface.
- 2 In the Settings window for Surface, locate the Data section.
- 3 From the Dataset list, choose Sector 2D 1.
- 4 Locate the Coloring and Style section. From the Coloring list, choose Uniform.
- 5 From the Color list, choose Gray.
- **6** Locate the **Title** section. From the **Title type** list, choose **None**.

# Surface 2

- I In the Model Builder window, right-click Martensite Start Temperature and choose Surface.
- 2 In the Settings window for Surface, locate the Expression section.
- 3 In the Expression text field, type Ms (carb.c).
- 4 From the Unit list, choose degC.

- 5 Select the **Description** check box. In the associated text field, type Martensite Start Temperature.
- 6 In the Martensite Start Temperature toolbar, click  **Plot**.

# Residual Stress

- I In the Home toolbar, click Add Plot Group and choose 2D Plot Group.
- 2 In the Settings window for 2D Plot Group, type Residual Stress in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Mirror 2D 1.
- 4 Locate the Plot Settings section. Clear the Plot dataset edges check box.

# Surface I

- I Right-click Residual Stress and choose Surface.
- 2 In the Settings window for Surface, locate the Data section.
- 3 From the Dataset list, choose Sector 2D 1.
- 4 Locate the Coloring and Style section. From the Coloring list, choose Uniform.
- 5 From the Color list, choose Gray.
- **6** Locate the **Title** section. From the **Title type** list, choose **None**.

# Surface 2

- I In the Model Builder window, right-click Residual Stress and choose Surface.
- 2 In the Settings window for Surface, locate the Expression section.
- **3** In the **Expression** text field, type solid.sp2Gp.
- 4 In the Residual Stress toolbar, click  **Plot**.