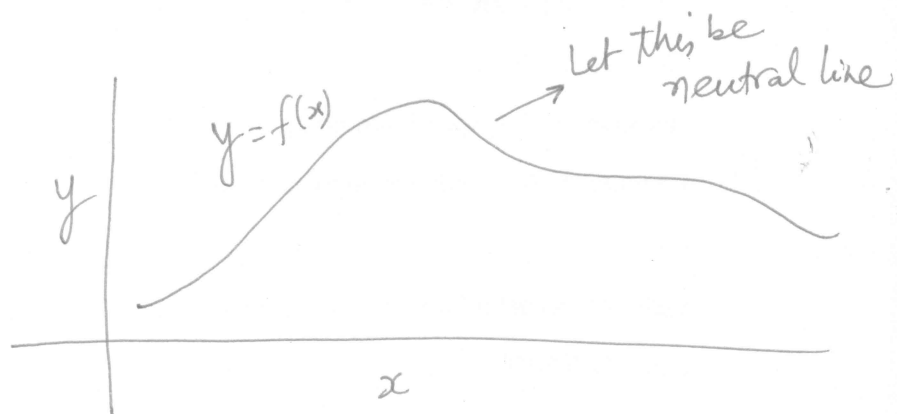


Euler Bernoulli beam theory

We know from bending of beams that

$$EI \frac{1}{R} = M(x), \quad R \text{ is the radius of curvature of neutral line.}$$

$$\text{then, } \frac{1}{R} = \frac{d^2y/dx^2}{\left(1 + \left(\frac{dy}{dx}\right)^2\right)^{3/2}}$$



If the deflection is such that $\frac{dy}{dx} \approx 0$

$$\Rightarrow \frac{1}{R} \approx \frac{d^2y}{dx^2}$$

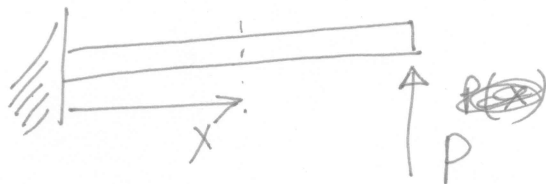
Also, $\frac{dy}{dx}$ denotes rotation of cross-section

$$\text{So, } \boxed{EI \frac{d^2y}{dx^2} = M(x)}$$

this is Euler Bernoulli beam theory!

If $M(x)$ is known, then two more boundary conditions needed to solve the above equation!

One simple example of a cantilever



In this case, $M(x) = P(L-x)$

Hence, $EI \frac{d^2 y}{dx^2} = P(L-x)$

Integrating twice

$$\Rightarrow EI y(x) = PL \frac{x^2}{2} - \frac{Px^3}{6} + Cx + d$$

To obtain 'C' & 'd'

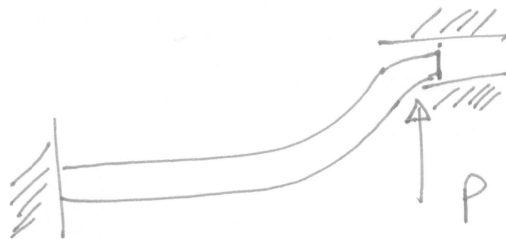
we apply, $y(0) = 0 \Rightarrow d = 0$

$$\frac{dy}{dx}(0) = 0 \Rightarrow C = 0$$

$$\text{So, } y(x) = \frac{PLx^2}{2EI} \left(1 - \frac{x}{3L} \right)$$

$$\boxed{y(L) = \frac{PL^3}{3EI}}$$

Another case.



In this case, we are apply force 'P' at the other end but the beam is not allowed to rotate at this end

$\Rightarrow M(L) \neq 0$ is an additional unknown!!

$$M(x) = M(L) + P(L-x)$$

The three boundary conditions are: -

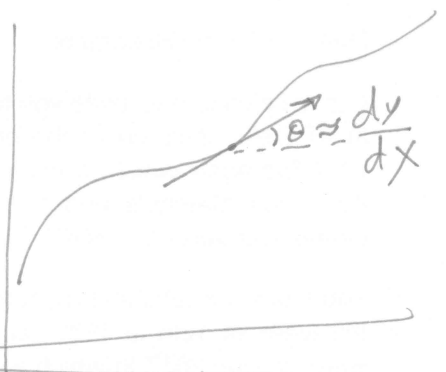
$$y(0) = 0, \quad \frac{dy}{dx}(0) = 0$$

$$\frac{dy}{dx}(L) = 0$$

* Euler bernouli theory holds only when $\frac{dy}{dx} \approx 0$

$$\text{So, } \frac{dy}{dx} = \tan \theta \approx \theta \quad (\text{slope of neutral line})$$

* Furthermore, we assume that the slope of neutral axis coincides with the cross-sectional normal \Rightarrow



$$\boxed{\text{rotation of cross-section} = \frac{dy}{dx}}$$

\rightarrow this assumption is relaxed in case of Timoshenko beam theory.

\rightarrow We ~~assume~~ that ~~deflection~~ also take into account the effect of shear force on deflection of a beam!

Hence,

$$\frac{dy}{dx} = \text{slope due to bending} + \text{slope due to shear}$$

(shear angle)

We further assume that $\frac{dy}{dx}$ is very small!

$$\frac{dy}{dx} \approx 0$$

$$\Rightarrow \frac{dy}{dx} \approx \text{rotation due to bending} + \text{rotation due to shear force}$$

$$\approx \theta_b + \theta_s$$

* θ_b is such that $EI \frac{d\theta_b}{dx} = M(x)$

→ θ_b is also the rotation of a cross-section! We will simply call it " θ "

→ θ_s is shear strain $= \frac{V}{KGA}$

So, the Timoshenko beam equation is

$$\boxed{\begin{aligned} EI \frac{d\theta}{dx} &= M(x) \\ \frac{dy}{dx} &= \theta + \frac{V(x)}{KGA} \end{aligned}}$$

→ System of two equations in unknowns 'y' (transverse deflection) and ' θ ' (cross-section rotation)

→ Unlike Euler Bernoulli theory, $\frac{dy}{dx} \neq \theta$ here!!

Cantilever problem using Timoshenko beam theory!



$$EI \frac{d\theta}{dx} = M(x)$$

$$\frac{dy}{dx} = \theta + \frac{V(x)}{kGA}$$

$$\boxed{\begin{aligned} M(x) &= P(L-x) \\ V(x) &= P \end{aligned}}$$

~~So~~ Since, bending moment and

shear force profile are known completely

\Rightarrow 2 more boundary conditions needed!

They are

$$\boxed{\begin{aligned} y(0) &= 0 \\ \theta(0) &= 0 \end{aligned}}$$

TBT.

Notice the change in boundary condition!
in Euler Bernoulli theory, we had

$$\boxed{\begin{aligned} y(0) &= 0 \\ \frac{dy}{dx}(0) &= 0 \end{aligned}}$$

EBT.