

Data / /

$$\text{wavelength} = \frac{c}{f} \rightarrow \text{Frequency}$$

$\lambda \rightarrow$

5. Horn Antenna
6. Vivaldi Antenna
7. Telescopes.

Other Antennas:-

1. NFC Antenna
2. Fractal Antenna
3. Wearable Antenna.

4 nec 2

Numeric Electromagnetic Code

C EMCA Ex. 1

1. Configure a linear wire antenna so as to operate at $f = 400 \text{ MHz}$,

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{4 \times 10^8} = \frac{3}{4} \text{ m}$$

$$= \frac{3}{4} \cancel{\lambda} = 0.75 \text{ m}$$

) Symbols

odd value greater than λ

$$\lambda = 0.75 \text{ m}$$

Type Tag Segs $x_1 \quad y_1 \quad z_1$ $x_2 \quad y_2 \quad z_2$ Radius
 Wire 1 27 0 0 -1/2 0 0 +1/2 0.0001m

2) Geometry

Wires

3) Source / load

Type	Tag	seg	(opt)	Real	Imag	Magn	Phase
voltage- src	1	14	00	1	0	1	0

22
↑
Middle of previous seg.

4) Freq / Ground

Frequency \rightarrow 400MHz From question

Environment \rightarrow Free-space

Run button Green color. Upper right side.

Select. Far field

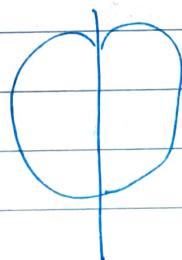
Resolution 5

Click generate.

Omni directional pattern.

E Non-directional pattern in given plane
& directional pattern in its orthogonal plane

Dipole Antenna



Mono pole \rightarrow



Variable Name

1. It can be only one word.
2. It can use only letters, numbers and the underscore (-) character.
3. It can't begin with a number.

`input()` function → Store value in form of string.

len() function

In python, one data type can change one data type to another data type.

EMA Practical - 2 27/01/2023

Title:- Performance comparison of half wave dipole versus, quarterwave monopole antenna.

$$c = 3 \times 10^8 \text{ m/s}$$

$$f = 500 \text{ MHz} = 500 \times 10^6$$

$$\lambda = \frac{c}{f} = \frac{3}{5} = 0.6$$

$$\lambda = 0.6 \text{ m}$$

$$\lambda = \text{lambda}/2$$

Geometry

Type	Tag	Segs	x_1	y_1	z_1	x_2	y_2	z_2	Radius
Wire	1	21	0	0	-1/2	0	0	1/2	0.0001

Source / Load

Type	Seg	opt	Real	Imag	Magn	Phase
Vtg source	II	oo	01	00	01	0

Environment - Free-space.

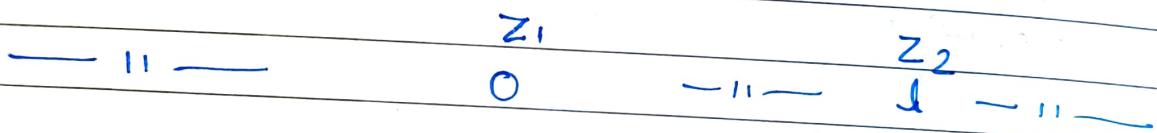
For halfwave dipole - at $f = 500\text{MHz}$.

- ① Gain = 2.17 dB
- ② HPBW = Half power beamwidth = 80 deg
- ③ Impedance = $80.5 + j46.4 \Omega$

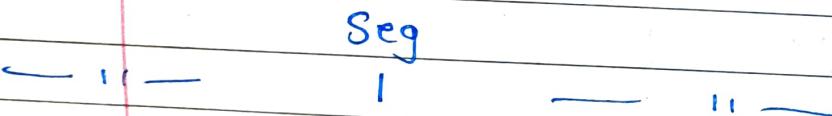
For quarterwave monopole

$$l = \lambda_{\text{free}}/4$$

Geometry.



Source / Load



Freqn. / Gnd

Environment - perfect ground

For quarterpole dipole at 500 MHz

- ① Gain = 5.18 dB
- ② HPBW = 40 deg
- ③ Impedance = $40.3 + j23.6 \Omega$

Expt. 3

DOMS
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Study of effect of variation of length of linear wire antenna on radiation pattern and associated parameters.

Symbols

$$\lambda = 1$$

$$L = \lambda/4$$

$$\lambda = \frac{C}{f}$$

$$f = \frac{C}{\lambda} = \frac{3 \times 10^8}{1} = 300 \text{ MHz}$$

Geometry

$$\lambda = 1 \text{ m}$$

Type	Tag	Segs	x_1	y_1	z_1	x_2	y_2	z_2	Radius
wire	1	27	0	0	-1/2	0	0	1/2	0.0001
<i>Serial no. of wire</i>									

Source/Load

Type	Tag	Segs	(opt)	Real	Imag	Magn	Phase	f
rtg-SRC	1	14	00	1	0	1	0	

Freq/ Ground

$$\text{Frequency} = 300 \text{ MHz}$$

Environment = Freespace

Far - field ~~region~~. pattern

$$\left[\begin{array}{|c|c|c|} \hline a_{11} & a_{12} & a_{13} \\ \hline a_{21} & a_{22} & a_{23} \\ \hline a_{31} & a_{32} & a_{33} \\ \hline \end{array} \right] \quad \left[\begin{array}{|c|} \hline b_1 \\ \hline b_2 \\ \hline b_3 \\ \hline \end{array} \right]$$

Observation Table:-

Sr. No.	Length of Linear wire antenna	HPBW		Gain (in dB)
		Theoretical	Practical	
1.	$\lambda/4$	87dg	90dg	1.85dB
2.	$\lambda/2$	78dg	80dg	2.17dB
3.	$3\lambda/4$	64dg	60dg	2.8dB
4.	λ	47.8dg	50dg	3.49dB
5.	1.25λ	---	30dg	5.09dB

$\downarrow \text{HPBW} = \text{Directivity} \uparrow$

$$\text{Gain} =$$

$$\eta G = e \cdot d.$$

$$\frac{\text{Efficiency}}{\text{of antenna}} \times \frac{\text{Directivity}}{\text{of antenna}}$$

Restrict length of λ upto 1λ .

\therefore there will not be any sidelobes.

Q.6) Why log periodic antenna is so called?

In case of log periodic antenna, the electric properties of the antenna are varying periodically with respect to logarithm of freqn (log f). Hence it is so called.

Q.7) The normalised field pattern of a certain antenna is given by $E(\theta) = \sin \theta$ for $0 \leq \theta \leq \pi$, where θ is in radians. Compute 3dB beamwidth for this antenna.

EXPT 4

Title:- Principle of pattern multiplication.

Aim:- To understand & verify principle of pattern multiplication for a given antenna array configuration.

Software used:-

~~Matlab~~ Scilab.

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Theory:-

Statement of principle of pattern multiplication

Case 1 : An array of 4 isotropic point sources fed with equal amplitude & equal phase separated by $d = \lambda/2$.

Step 1 to 5.

Case 2 :- An array of 4 equal amplitude & opposite phase separated by $d = \lambda/2$.
Step 1 to 5.

O/p :- program print. Case 1 & Case 2
O/p print (plot). Both.

Conclusion:- Take batch 3.

for Case 1:-

// Principle of Pattern Multiplication.

clear;

clc;

lambda = 1;

d = lambda/2;

beta = (2 * %pi) / lambda ;

delta = 0; // defining Delta as a phase of difference between dipoles.

phi = 0: 0.01: 2 * %pi; // Variation of the theta from 0 to 360 degrees.

subplot (2, 2, 1);

EP = cos (%pi/2 * (cos(phi)));

polarplot (phi, abs(EP)); // plot of single element pattern.

title ('ELEMENT ELEMENT PATTERN');

AF = cos(%pi * (cos(phi) + delta)) // Expression for an Array Factor

subplot (2, 2, 2);

polarplot (phi, abs(AF)); // plot of Array pattern.

title ('ARRAY FACTOR PATTERN');

subplot (2, 2, 3.5);

polarplot (phi, abs(EP) .* abs(AF));

// plot of Total Field Pattern of Array.

title ('TOTAL ARRAY PATTERN');

for case 2

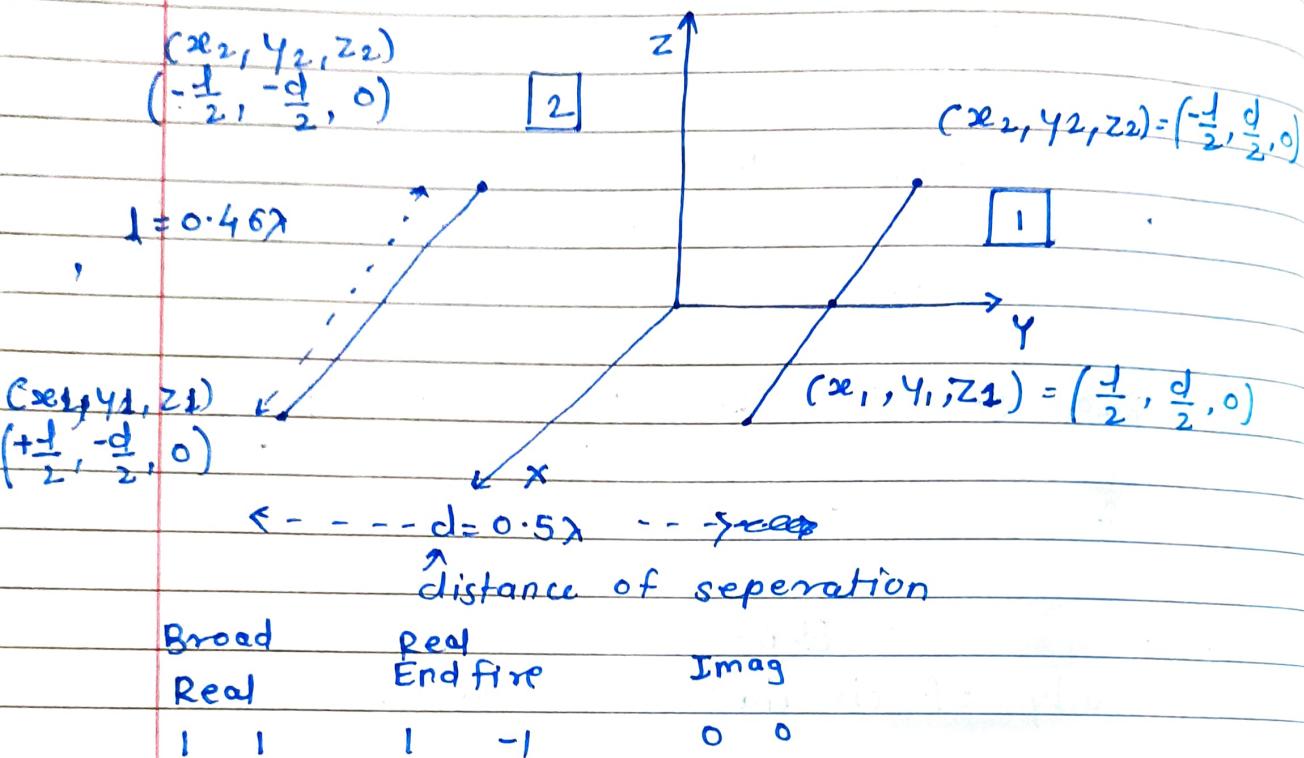
just change

$EP = \sin(\frac{\pi}{2} * (\cos(\phi)))$;

EMA EXPT 5

Title:- Performance comparison of broadside array and endfire array.

Two element antenna array.



*End fire *

Symbols:- $\lambda_{\text{ambda}} = 1$

$$L = 0.5 \times 0.46 \times \lambda_{\text{ambda}}$$

$$d = 0.5 \times \lambda_{\text{ambda}}$$

Geometry:

Type	Tag	Segs	x_1	y_1	z_1	x_2	y_2	z_2	Radius
Wire	1	2	$\frac{d}{2}$	$\frac{d}{2}$	0	$-\frac{d}{2}$	$\frac{d}{2}$	0	0.001
Wire	2	2	$\frac{d}{2}$	$-\frac{d}{2}$	0	$-\frac{d}{2}$	$-\frac{d}{2}$	0	0.001

Source / Load

Type	Tag	Seg.	(opt)	Real	Imag	Magn	Phase
vtg-src	1	14	00	1	0	1	0
vtg-src	2	14	00	-1	0	1	0

Time varying excitation

Freq / Ground

$$f = 300 \text{ MHz}$$

Environment

Free space.

* For Broadside *

Remain all settings are same only change in
Source & Load:-

Type	Tag	Sig	(opt)	Real	Imag	Magn	Phase
Vtg-Src	1	14	00	1	0	1	0
Vtg-Src	2	14	00	1	0	1	0

Expt 7

Study of circular loop antenna.

10/3/2022

Types of Loop antenna.

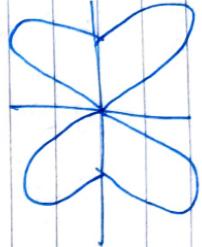
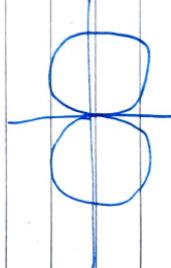
Electrically small

$$D < \frac{\lambda}{10}$$

Electrically large

$$D > \lambda$$

$$C_2 = \frac{C}{\lambda} = \frac{\pi D}{\lambda} < 0.314 \quad C_2 = \frac{C}{\lambda} = \frac{\pi D}{\lambda} > 3.14$$



For single turn small loop antenna.

$$R_x = 20 \cdot \pi^2 \left(\frac{C}{\lambda} \right)^4$$

where $C = 2 \cdot \pi$ is circumference of loop antenna

For N turns

$$R_x = 20 \cdot \pi^2 N^2 \left(\frac{C}{\lambda} \right)^4$$

for large loop ($C \gg 314 \lambda$) Antenna

$$R_x = 60 \cdot \pi^2 \left(\frac{C}{\lambda} \right)$$

Symbols:-

$$\lambda_{\text{m}} = 1 \quad f = 300 \text{ MHz}$$

$$D = \lambda_{\text{m}}/10$$

Geometry

Type	Tag	Segs	Arc-rad	Angl-1	Angl-2	Wire-rad
Arc	1	50	D/2	0	360	0.0001

Source / load

Type	Tag	Seg (opt)	Real	Imag	Magn	Phase
Vtgsrc	1	1	0.0	1	0	1

$$\text{Freq / Gnd} \\ F = 300 \text{ MHz}$$

Free-space.

Far-field pattern.

Observation Table

Sr.No.	Loop Diameter (D)	Max. Gain (in dBi).
1.	$\lambda/10$	1.55
2.	$\lambda/8$	1.47
3.	$\lambda/4$	2.53
4.	$\lambda/2$	3.85
5.	λ	4.14

Comparison of different circular loop antenna.

Case i) - Let D (D) = $\lambda/10$

Structure (Hide pattern) 3D pattern (Multicolor)
 fig. Loop antenna structure and 3d radiation pattern.

Vertical plane Horizontal plane.

fig. 2D vertical & hori field patterns of loop antenna.

Very Very Important

Cartesian

Differential in length

$$dL = dx a_x + dy a_y + dz a_z$$

Differential surface.

$$\begin{aligned} dS_x &= dy dz a_x \\ dS_y &= dx dz a_y \\ dS_z &= dx dy a_z \end{aligned}$$

Differential Volume

$$dV = dx dy dz$$

Cylindrical

$$\begin{aligned} dL &= d\sigma a_\theta \\ &\quad + r d\phi a_\phi + dz a_z \end{aligned}$$

— || —

Spherical

$$\begin{aligned} dL &= dr a_r + r d\theta a_\theta \\ &\quad + r \sin \theta d\phi a_\phi \end{aligned}$$

— || —

$$\begin{aligned} dS_r &= r^2 \sin \theta d\theta d\phi a_r \\ dS_\theta &= r s \sin \theta dr d\phi a_\theta \\ dS_\phi &= r dr \sin \theta d\phi a_\phi \end{aligned}$$

— || —

$$dV = r^2 \sin \theta dr d\theta d\phi$$

17/3/2023

Expt. 8

Study of Principle of superposition for calculation of Electric Field Intensity due to 'N' point charges

EQ.1) Calculate the electric field intensity at point $A(1,1,1)$ due to three point charges each of magnitude 1nC , 5nC , 4nC located at $(2,1,1)$; $(1,5,1)$ and $(2,2,2)$ respectively.

Initial $Q_1 = 1\text{nC}$ - - -

$(2,1,1)$

$\overrightarrow{R_1}$

Final

$Q_2 = 5\text{nC}$ - - - $\overrightarrow{R_2}$ - - - $A(1,1,1)$.

$(1,5,1)$

$\overrightarrow{R_3}$

$Q_3 = 4\text{nC}$ - - - $\overrightarrow{R_3}$
 $(2,2,2)$

$$\bar{E}_1 = \frac{q_1}{4\pi \cdot \epsilon_0 R_1^2} \cdot \bar{a}_{R_1}$$

But here,

$$\bar{R}_1 = (1-2)\bar{a}_x + (1-1)\bar{a}_y + (1-1)\bar{a}_z$$

$$|\bar{R}_1| = \sqrt{(-1)^2} = 1$$

$$\bar{a}_{R_1} = \frac{\bar{R}_1}{|\bar{R}_1|} = \frac{-\bar{a}_x}{1} = -\bar{a}_x$$

Now, $\bar{E}_1 = 8.98 (-\bar{a}_x) \text{ V/m}$

$$\bar{E}_1 = \frac{1 \times 10^{-9}}{4\pi \times (8.854 \times 10^{-12}) \times 1} \bar{a}_x$$

$$\boxed{\bar{E}_1 = 8.98 (-\bar{a}_x) \text{ V/m}}$$

$$\boxed{* \quad \bar{E}_1 = -8.98 \bar{a}_x \text{ V/m}}$$

$$\bar{E}_2 = \frac{q_2}{4\pi \cdot \epsilon_0 R_2^2} \cdot \bar{a}_{R_2}$$

But here,

$$\bar{R}_2 = (1-1)\bar{a}_x + (1-5)\bar{a}_y + (1-1)\bar{a}_z$$

$$= -4\bar{a}_y$$

$$|\bar{R}_2| = \sqrt{(-4)^2} = 4$$

$$\bar{a}_{R_2} = 4 \quad \bar{a}_{R_2} = \frac{\bar{R}_2}{|\bar{R}_2|} = \frac{-\bar{a}_y}{4} = -\frac{1}{4}\bar{a}_y - \bar{a}_y$$

$$\bar{E}_2 = \frac{5 \times 10^{-9}}{4\pi \times (8.854 \times 10^{-12}) \times (4)^2} (-\bar{a}_y)$$

$$\boxed{\bar{E}_2 = -2.808 \bar{a}_y \text{ V/m}}$$

$$\bar{E}_3 = \frac{Q_3}{4\pi \epsilon_0 R^2} \bar{a}_{R_3}$$

But here,

$$\begin{aligned} \bar{R}_3 &= (1-2)\bar{a}_x + (1-2)\bar{a}_y + (1-2)\bar{a}_z \\ &= -\bar{a}_x - \bar{a}_y - \bar{a}_z \end{aligned}$$

$$|\bar{R}_3| = \sqrt{(-1)^2 + (1)^2 + (1)^2} = \sqrt{3}$$

$$\bar{a}_{R_3} = \frac{\bar{R}_3}{|\bar{R}_3|} = \frac{-\bar{a}_x - \bar{a}_y - \bar{a}_z}{\sqrt{3}} =$$

$$\begin{aligned} \bar{E}_3 &= \frac{4 \times 10^{-9}}{4\pi \times (8.854 \times 10^{-12}) \cdot (\sqrt{3})^2} \cdot -\bar{a}_x - \bar{a}_y - \bar{a}_z \\ &= 11.983 \cdot \frac{-\bar{a}_x - \bar{a}_y - \bar{a}_z}{\sqrt{3}} \end{aligned}$$

$$\boxed{\cancel{E_3 = -6(\bar{a}_x + \bar{a}_y + \bar{a}_z) \text{ V/m}}}$$

$$\boxed{\bar{E}_3 = -6.9187(\bar{a}_x + \bar{a}_y + \bar{a}_z) \text{ V/m}}$$

$$= -6.9187\bar{a}_x - 6.9187\bar{a}_y - 6.9187\bar{a}_z \text{ V/m}$$

$$|\vec{E}_1| = \sqrt{(8.98)^2} = 8.98 \text{ V/m}$$

$$|\vec{E}_2| = \sqrt{(-2.808)^2} = 2.808 \text{ V/m}$$

$$|\vec{E}_3| = \sqrt{(-6.9187)^2 + (-6.9187)^2 + (-6.9187)^2} = 11.983 \text{ V/m}$$

By principle of Superposition.

$$\vec{E} = \vec{E}_1 + \vec{E}_2 + \vec{E}_3$$

$$\vec{E} = (8.98 + 2.808 + 11.983) \text{ V/m}$$

$$\boxed{\vec{E} = 23.771 \text{ V/m}}$$

//Program for Electric Field Intensity due to ^{N point} charges

clc; clear all;

N = input ('Enter the number of point charges : ');

p = input ('Enter the coordinates of a point at which
- E is to be calculated in the form [x, y, z] : ');

epso = input ('Enter the value of permittivity of
the medium : ');

E > 0;

for M=1:N

q = input ('Enter the magnitude of a point charge : ');

T = input ('Enter the point at which charge is
located as [x y z] : ');

R = norm (p - T);

EN = q / (4 * pi * eps0 * R * R);

E = E + EN

end

disp ('The Resultant Electric Field Intensity is', E, 'V/m');

EMA Expt. 6

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5 element Yagi Uda antenna:-

Symbols:-

$$Act = 0.48 \times \lambda$$

$$Ref = 0.525 \times \lambda$$

$$Dir_1 = 0.42 \times \lambda$$

$$Dir_2 = 0.4 \times \lambda$$

$$Dir_3 = 0.37 \times \lambda$$

$$S_1 = 0.2 \times \lambda$$

$$S_2 = 0.3 \times \lambda$$

$$S_3 = 0.55 \times \lambda$$

$$S_4 = 0.8 \times \lambda$$

$$H = \lambda$$

where $\lambda = 0.75$. for $f = 400 \text{ MHz}$

Geometry

Type	Tag	Segs	X_1	Y_1	Z_1	X_2	Y_2	Z_2	Radius
Wire	1	21	0	$-Act/2$	H	0	$Act/2$	H	0.0001
—	2	21	$+S_1$	$-Ref/2$	H	S_1	$Ref/2$	H	—
—	3	21	$-S_2$	$-Dir_1/2$	H	S_2	$Dir_1/2$	H	—
—	4	21	$-S_3$	$-Dir_2/2$	H	S_3	$Dir_2/2$	H	—
—	5	21	$-S_4$	$-Dir_3/2$	H	S_4	$Dir_3/2$	H	—

Source / Load

Type	Tag	Seg	(opt)	Real	Img	Magn	Phase
Vtg-src	I	II	00	1	0	1	0

Freq / Gnd

$$F = 400 \text{ MHz}$$

Environment

→ Free Space.

Far field pattern.

3 element Yagi-Uda antenna:-

Symbols:-

$$\lambda = 0.75$$

$$A_{ct} = 0.48 \times \lambda$$

$$R_{ef} = 0.525 \times \lambda$$

$$D_{ir} = 0.42 \times \lambda$$

$$S_1 = 0.2 \times \lambda$$

$$S_2 = 0.3 \times \lambda$$

$$H = \lambda$$

Geometry

Type	Tag	Seg	X_1	Y_1	Z_1	X_2	Y_2	Z_2	Radius
Wire	1	21	0	$-A_{ct}/2$	z	0	$A_{ct}/2$	H	0.0001
- -	2	21	S_1	$-R_{ef}/2$	z	S_1	$R_{ef}/2$	H	0.0001
- -	3	21	$-S_2$	$-D_{ir}/2$	z	$-S_2$	$-D_{ir}/2$	H	0.0001

Source / Load

Type	Tag	Seg	(opt)	Real	Img	Mag	Phase
Vtg-Src	1	11	00	1	0	1	0

Freq / Gnd

$$F = 400 \text{ MHz}$$

Environment

Free space

Far field pattern.