

NPTEL ONLINE CERTIFICATION COURSES

DIGITAL CONTROL IN SMPCs AND FPGA-BASED PROTOTYPING

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Module 04: Modeling Techniques and Mode Validation using MATLAB

Lecture 32: Discrete Time Modeling with Closed Current Loop

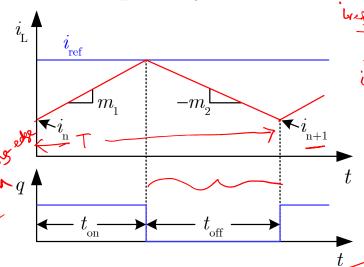




CONCEPTS COVERED

- Discrete-time modeling analog current loop
- Current loop stability under mixed-signal CMC
- Current-loop stability under fully digital CMC
- Need for going closed-loop stability analysis

Fixed Frequency Analog Peak CMC – Current Loop Stability $ton = d \top$



 $i_{
m n+1}=i_{
m ref}-\underline{m_{
m 2}t_{
m off}}$ 4

 $i_{\rm n}=i_{\rm ref}-m_{\rm 1}t_{\rm on}$

(a) Under fixed-frequency modulation $t_{\rm on}=dT; ~~t_{\rm off}=\left(1-d\right)T$

$$i_{\mathbf{n}+1} = i_{\mathbf{ref}} - m_2 \left(1 - d\right) T$$

$$i_{\text{ref}} - m_{_{1}} dT$$

$$\Rightarrow dT = \left(\frac{i_{\text{ref}} - i_{\text{n}}}{m_{\text{n}}}\right)$$

[For details, refer to Lecture~23, NPTEL "Control and Tuning Methods ..." course (Link)





Current Loop Stability Analysis (contd...)

Thus,
$$i_{n+1} = i_{ref} + m_2 \underbrace{\left(\frac{i_{ref} - i_n}{m_1}\right)}_{-m_2} - m_2 T = -\left(\frac{m_2}{m_1}\right) i_n + \left(1 + \frac{m_2}{m_1}\right) i_{ref} - m_2 T$$

Perturbed current dynamics becomes

$$\tilde{i}_{n+1} = -\left(\frac{m_2}{m_1}\right) \tilde{i}_n + \left(1 + \frac{m_2}{m_1}\right) \tilde{i}_{ref}$$

Passumptions:

Perturbed current dynamics becomes

$$\tilde{i}_{\mathrm{n}+1} = - \left(\frac{m_{\mathrm{2}}}{m_{\mathrm{1}}} \right) \tilde{i}_{\mathrm{n}} + \left(1 + \frac{m_{\mathrm{2}}}{m_{\mathrm{1}}} \right) \tilde{i}_{\mathrm{ref}}$$

- Assumptions:
 - Perturbations in slopes are neglected
 - Nonlinear perturbed (product) terms are neglected

[For details, refer to Lecture~23, NPTEL "Control and Tuning Methods ..." course (Link)



Current Loop Stability Analysis (contd...) stability due to the perturbation in in For constant reference, $\tilde{i}_{\rm ref}=0;$ For inner loop stability,

Thus,
$$\tilde{i}_{\mathrm{n+1}} = \left(-\left(\frac{m_{\mathrm{2}}}{m_{\mathrm{1}}} \right) \tilde{i}_{\mathrm{n}} \right)$$

$\sigma_{\rm s} > 0$		
$\frac{1}{2}\left(\frac{1}{2}\right)\left(\frac{1}{2}+\frac{m_{1}}{m_{1}}\right)=0$	$\left \frac{m_{_{2}}}{m_{_{1}}}\right <$	1

Slope	Buck Converter	Boost Converter
$m_{_{\! 1}}$ \smile	$\frac{V_{ m in}-V_{ m o}}{L}$	$rac{V_{ m in}}{L}$
$m^{}_2$	$rac{V_{ m o}}{L}$	$rac{V_{ m o}-V_{ m in}}{L}$

[For details, refer to Lecture~23, NPTEL "Control and Tuning Methods ..." course (Link)





Current Loop Stability Analysis (contd...)

■ <u>Buck Converter</u>:

$$\begin{aligned} \left| \frac{m_2}{m_1} \right| &= \left| \frac{V_{\text{o}}}{V_{\text{in}} - V_{\text{o}}} \right| = \frac{V_{\text{o}}}{V_{\text{in}} - V_{\text{o}}} \quad \text{(Since } 0 < V_{\text{o}} < V_{\text{in}} \text{)} \\ & \therefore \frac{V_{\text{o}}}{V_{\text{in}} - V_{\text{o}}} < 1 \\ & \Rightarrow \frac{V_{\text{o}}}{V_{\text{in}}} < \frac{1}{2} \\ & \Rightarrow D < 0.5 \end{aligned}$$

[For details, refer to Lecture~23, NPTEL "Control and Tuning Methods ..." course (Link)



Current Loop Stability Analysis (contd...)

■ <u>Boost Converter</u>:

$$\frac{m_{_2}}{m_{_1}} = \frac{V_{_o} - V_{_{\mathrm{in}}}}{V_{_{\mathrm{in}}}}$$

$$\therefore \frac{V_o - V_{\text{in}}}{V_{\text{in}}} < 1$$

$$\Rightarrow V_{_{o}} < 2V_{_{
m in}}$$

$$\Rightarrow D < 0.5$$

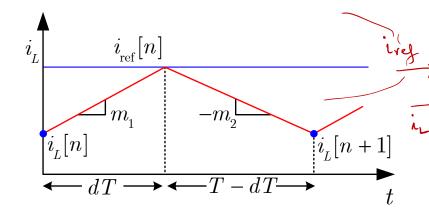


[For details, refer to Lecture~23, NPTEL "Control and Tuning Methods ..." course (Link)





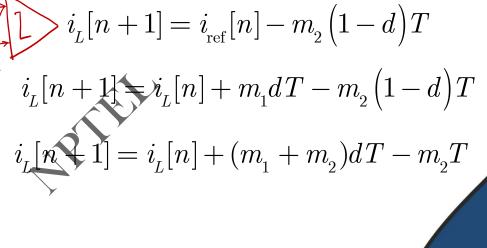
Fixed Frequency Mixed Signal Peak CMC - Current Loop Stability



$$dT = \frac{i_{\text{ref}}[n] - i_{\!\scriptscriptstyle L}[n]}{m_{\!\scriptscriptstyle 1}}$$

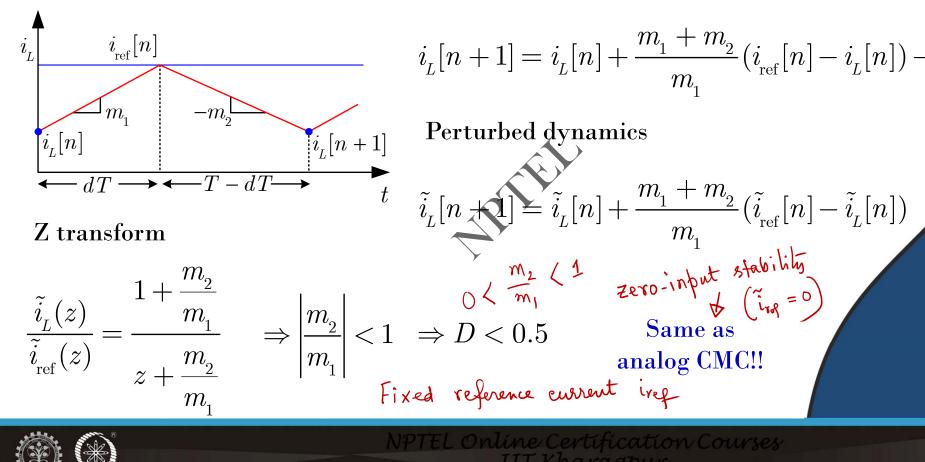
$$\Rightarrow i_{\!\scriptscriptstyle L}[n+1] = i_{\!\scriptscriptstyle L}[n] + \frac{m_{\!\scriptscriptstyle 1} + m_{\!\scriptscriptstyle 2}}{m_{\!\scriptscriptstyle 1}} (i_{\!\scriptscriptstyle \mathrm{ref}}[n] - i_{\!\scriptscriptstyle L}[n]) - m_{\!\scriptscriptstyle 2} T$$





 $i_{ref}[n] = i_{L}[n] + m_{1}dT$

Fixed Frequency Mixed Signal Peak CMC - Current Loop Stability

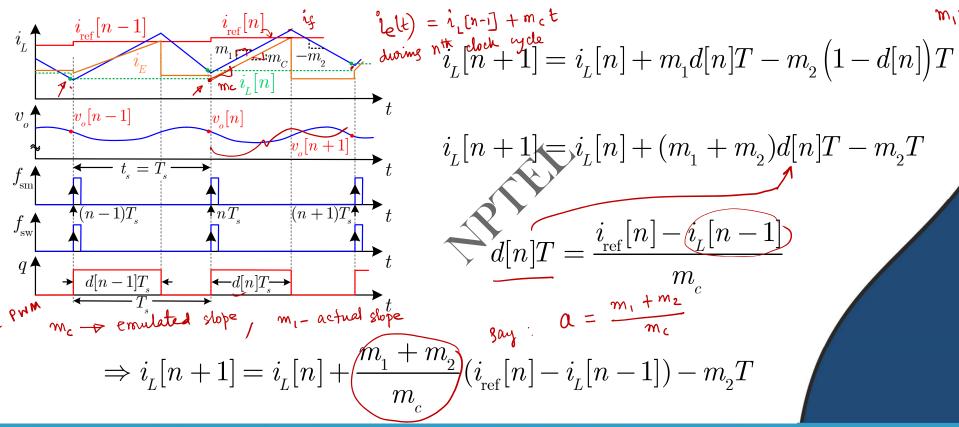


$$i_{\!{}_{\!L}}[n+1] = i_{\!{}_{\!L}}[n] + \frac{m_{\!{}_{\!1}} + m_{\!{}_{\!2}}}{m_{\!{}_{\!1}}} (i_{\!{}_{\mathrm{ref}}}[n] - i_{\!{}_{\!L}}[n]) - m_{\!{}_{\!2}}T$$

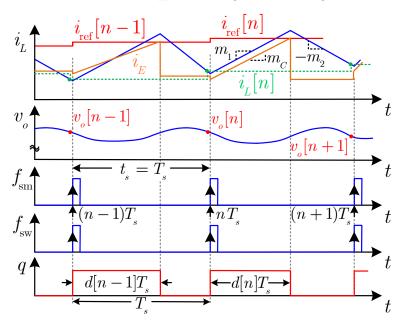
$$\frac{\tilde{i}_L(z)}{\tilde{i}_{\text{ref}}(z)} = \frac{1 + \frac{m_2}{m_1}}{z + \frac{m_2}{m_1}}$$

$$\Rightarrow \left| \frac{m_2}{m_1} \right| < 1 \quad \Rightarrow D < 0.5$$









$$i_{\!\scriptscriptstyle L}[n+1] = i_{\!\scriptscriptstyle L}[n] + \frac{m_{\!\scriptscriptstyle 1} + m_{\!\scriptscriptstyle 2}}{m_{\!\scriptscriptstyle c}} (i_{\!\scriptscriptstyle \mathrm{ref}}[n] - i_{\!\scriptscriptstyle L}[n-1]) - m_{\!\scriptscriptstyle 2} T$$

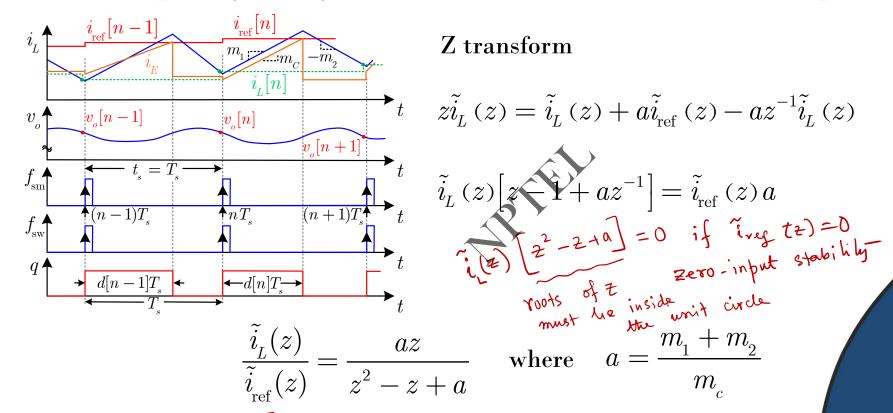
Perturbed dynamics

$$\underbrace{\tilde{i}_L[n+1]}_{\tilde{l}_L[n]} = \underbrace{\tilde{i}_L[n]}_{\tilde{l}_L[n]} + \underbrace{m_1 + m_2}_{m_c} (\tilde{i}_{\text{ref}}[n] - \tilde{i}_L[n-1])$$

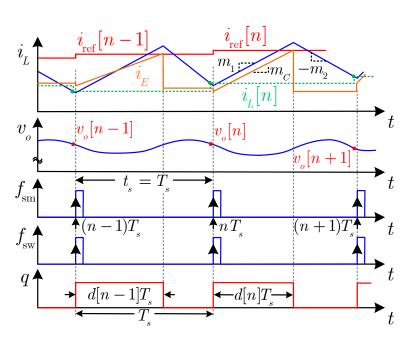
Apply Z transform

$$z\tilde{i}_{L}(z) = \tilde{i}_{L}(z) + a\tilde{i}_{ref}(z) - az^{-1}\tilde{i}_{L}(z)$$









$$\frac{\tilde{i}_{_L}(z)}{\tilde{i}_{_{\mathrm{ref}}}(z)} = \frac{az}{\underline{z^2 - z + \underline{a}}} \qquad \text{where} \quad a = \frac{m_1 + m_2}{m_c}$$

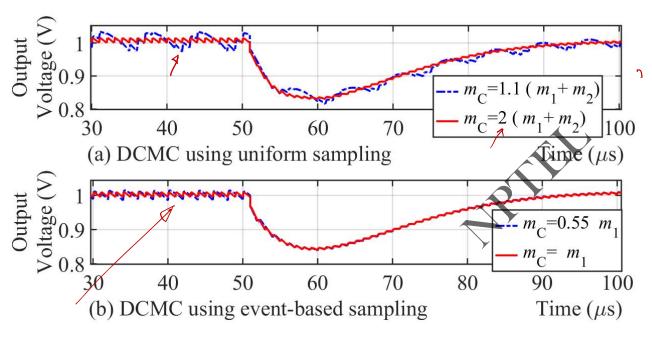
For current-loop stability $a < 1 \Rightarrow \frac{m_1 + m_2}{m_c} < 1$

 $m_c > m_1 + m_2$

[S. Kapat, "Beyond Stability and Performance Limits in Digital Current Mode Control ...", IEEE APEC, 2021]







$$m_c > m_1 + m_2$$

Need to study closed-

loop stability!!

• Detailed system

model needed

[S. Kapat, "Beyond Stability and Performance Limits in Digital Current Mode Control ...", *IEEE APEC*, 2021]



CONCLUSION

- Discrete-time modeling analog current loop
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