## Nodal Analysis Laboratory I

Patrycja Nazim, Adrian Król, Kamil Chaj

### 1 Aim of exercise

The aim of our exercise was to experimentally verify the nodal analysis in RLC circuits. We have achieved it by measuring the voltages on different nodes of the chosen circuits using a dedicated evaluation board and vector voltmeter. The obtained measurement results are compared with analytical calculations.

Apart from the values of potentials in individual nodes of the circuits being measured, we calculated the currents flowing through pointed elements.

### 2 Course of measurements

First step of our measurements was connecting evaluation board(fig.1) to laboratory computer via USB and starting Vector Voltage Meter software. Next we connected both INPUT1 and CON1 to OUTPUT using BNC cables and splitter, last we connected oscilloscope probe to INPUT2 connector. Now with all preparation finished we started voltage measurements of each node in Circuit A(fig.4). Then we disconnected BNC cable connected to CON1 and connected it to CON2 and repeated the same measurements for Circuit B(fig.5)

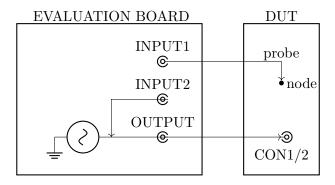


Figure 1: measurements schematic

# 3 Nodal analysis - method

Method which we are going to use to solve these circuits is known as "Nodal Analysis by Inspection". In this method we need to construct 3 matrices: **i** - current vector, **u** - voltage vector(unknown), **G** - conductance matrix, with sizes respectively  $N \times 1$ ,  $N \times 1$ ,  $N - 1 \times N - 1$ .

Size of conductance matrix is always smaller then number of nodes in the circuit by one because in nodal analysis one node is connected to ground as reference node.

$$\mathbf{Gu} = \mathbf{i}$$

$$\begin{bmatrix} G_{11} & -G_{12} & -G_{13} \\ -G_{21} & G_{22} & -G_{23} \\ -G_{31} & -G_{32} & G_{33} \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

Where  $G_{11}$ ,  $G_{22}$ ,  $G_{33}$  are sums of conductance of each branch connected to the node  $G_{12} = G_{21}$ ,  $G_{13} = G_{31}$ ,  $G_{32} = G_{23}$  are sums of conductance of branches between nodes  $I_1$ ,  $I_2$ ,  $I_3$  are sums of current sources entering or exiting node and  $U_1$ ,  $U_2$ ,  $U_3$  are unknown voltages that we are trying to find.

With simple matrix operation we obtain equation

$$\mathbf{u} = \mathbf{G}^{-1}\mathbf{i}$$

which can be easily calculated

### 4 Theoretical calculations

All calculation are made in Python with NumPy library. Source code for all calculation can be found in the Appendix

Before starting any calculation we modified original circuits' schematics by replacing BNC connectors with AC voltage source and drawing connection between ground(fig. 2a, fig. 3)

for both circuits amplitude of Voltage source is 0.192V and calculations are made for frequencies 1kHz, 5kHz and 9kHz

#### 4.1 Circuit A

In our calculations voltages in nodes 1, 3 and 4 are named  $U_1, U_3, U_4$  and reference node is the same node that was ground in original circuit schematic. Lone voltage source must be transfigured in order to solve this circuit by nodal analysis, after source transfiguration circuit looks like this fig. 2b

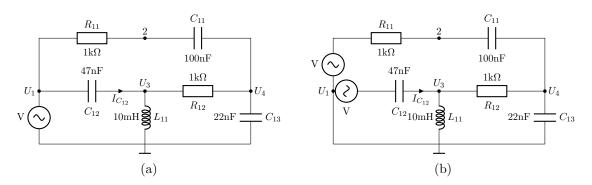


Figure 2: theoretical circuit A

following rules of Nodal Analysis by Inspection (Sec. 3) we obtain  $\mathbf{G}\mathbf{u} = \mathbf{i}$  equation

$$\begin{bmatrix} G_{R_{11}+C_{11}} + G_{C_{12}} & -G_{C_{12}} & -G_{R_{11}+C_{11}} \\ -G_{C_{12}} & G_{C_{12}} + G_{L_{11}} + G_{R_{12}} & -G_{R_{12}} \\ -G_{R_{11}} - G_{C_{11}} & -G_{C_{12}} & G_{R_{11}+C_{11}} + G_{R_{12}} + G_{C_{12}} \end{bmatrix} \begin{bmatrix} U_1 \\ U_3 \\ U_4 \end{bmatrix} = \begin{bmatrix} \frac{-V}{Z_{R_{11}+C_{11}}} + \frac{-V}{Z_{C_{12}}} \\ \frac{V}{Z_{C_{12}}} \\ \frac{V}{Z_{R_{11}+C_{11}}} \end{bmatrix}$$

after solving above equation we can easily calculate current of the capacitor  $C_{12}$ 

$$I_{C_{12}} = \frac{U_3 - U_2}{Z_{C_{12}}}$$

all that is left to do is computing

#### results of calculations

source code in the Appendix. A

|                      |              | !!      | !WRONG               | RESULTS     | <u>I THINI</u> | <u> </u>             |             |          |
|----------------------|--------------|---------|----------------------|-------------|----------------|----------------------|-------------|----------|
| $1000.0~\mathrm{Hz}$ | Magnitude    | Phase   | $5000.0~\mathrm{Hz}$ | Magnitude   | Phase          | $9000.0~\mathrm{Hz}$ | Magnitude   | Phase    |
| Node 1               | 0.192        | 180     | Node 1               | 0.192       | -180           | Node 1               | 0.192       | 180      |
| Node 3               | 1.22663e-18  | 135     | Node 3               | 2.86098e-17 | 104.036        | Node 3               | 5.72196e-17 | -165.964 |
| Node 4               | 0            | 0       | Node 4               | 1.43049e-17 | 14.0362        | Node 4               | 2.08167e-17 | -90      |
| I of $C_{-}12$       | 5.66995 e-05 | -1.5708 | I of $C_{-12}$       | 0.000283497 | -1.5708        | I of $C_{-12}$       | 0.000510295 | -1.5708  |

### 4.2 Circuit B

Following similar steps as in Circuit A, voltages in notes 2, 3 and 4 are named  $U_2, U_3, U_4$  and reference node is the same node that was ground in original circuit schematic. There is no lone voltage source so source transfiguration is not necessary.

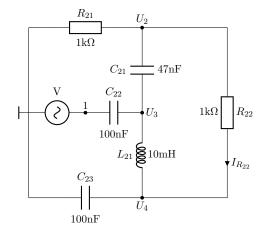


Figure 3: theoretical circuit B

following rules of Nodal Analysis by Inspection (Sec. 3) we obtain Gu = i equation

$$\begin{bmatrix} G_{R_{21}} + G_{R_{22}} + G_{C_{21}} & -G_{C_{21}} & -G_{R_{22}} \\ -G_{C_{21}} & G_{C_{21}} + G_{C_{22}} + G_{L_{21}} & G_{L_{21}} \\ -G_{R_{22}} & -G_{L_{21}} & G_{R_{22}} + G_{C_{23}} + G_{L_{21}} \end{bmatrix} \begin{bmatrix} U_2 \\ U_3 \\ U_4 \end{bmatrix} = \begin{bmatrix} 0 \\ \frac{V}{Z_{C_{22}}} \\ 0 \end{bmatrix}$$

after solving above equation we can easily calculate current of the capacitor  $R_{22}$ 

$$I_{R_{22}} = \frac{U_4 - U_2}{Z_{R_{22}}}$$

and these are the results

#### 4.2.1 Results of calculations

Source code in the Appendix B

| $1000.0~\mathrm{Hz}$ | Magnitude      | Phase    | $5000.0~\mathrm{Hz}$ | Magnitude   | Phase    | $9000.0~\mathrm{Hz}$ | Magnitude   | Phase   |
|----------------------|----------------|----------|----------------------|-------------|----------|----------------------|-------------|---------|
| Node 2               | 0.0442579      | 28.1037  | Node 2               | 0.0521098   | -53.9736 | Node 2               | 0.16282     | 63.622  |
| Node 3               | 0.0837746      | 22.3054  | Node 3               | 0.0534524   | 86.6776  | Node 3               | 0.219774    | 20.3532 |
| Node 4               | 0.0867875      | 20.4605  | Node 4               | 0.206963    | -12.1633 | Node 4               | 0.0750914   | -122.05 |
| I of $R_22$          | 4.33246 e - 05 | -2.92078 | I of $R_22$          | 0.000171674 | 3.13307  | I of $R_22$          | 0.000237659 | 1.07918 |

## 5 Real measurements

Following steps of measurements described in Section 2 we obtain measurements for each circuit

### 5.1 Circuit A

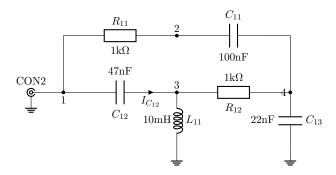


Figure 4: circuit A

Current  $I_{C_{12}}$  is measured indirectly using measured voltage and impedance of the component

$$I_{C_{12}} = \frac{U_1 - U_3}{Z_{C_{12}}}$$

where  $U_3$  is voltage in node 3,  $U_1$  is voltage in node 1 and  $Z_{C_{12}}$  is impedance of capacitor  $C_{12}$ 

| Circuit A |              |               |           |  |
|-----------|--------------|---------------|-----------|--|
| Freq      | Channel 1[V] | Channel 2 [V] | Angle [°] |  |
|           | n            | ode 1         |           |  |
| 1kHz      | 0.192        | 0.192         | 0         |  |
| 5kHz      | 0.192        | 0.192         | -0.1      |  |
| 9kHz      | 0.192        | 0.192         | -0.1      |  |
|           | n            | ode 2         |           |  |
| 1kHz      | 0.192        | 0.145         | -19.3     |  |
| 5kHz      | 0.192        | 0.59          | 9.3       |  |
| 9kHz      | 0.192        | 0.236         | -9.7      |  |
|           | n            | ode 3         |           |  |
| 1kHz      | 0.192        | 0.008         | 140.7     |  |
| 5kHz      | 0.192        | 0.154         | 136.1     |  |
| 9kHz      | 0.192        | 0.376         | 30        |  |
| node 4    |              |               |           |  |
| 1kHz      | 0.192        | 0.072         | 38.6      |  |
| 5kHz      | 0.192        | 0.082         | 42.1      |  |
| 9kHz      | 0.192        | 0.231         | -11.8     |  |
| (a)       |              |               |           |  |

| freq | $I_{C_{12}}[\mathrm{I}]$ | angle[°] |
|------|--------------------------|----------|
| 1kHz | 0.198                    | 178.5°   |
| 5kHz | $7.543 \cdot 10^{-5}$    | 1.5°     |
| 9kHz | $9.954 \cdot 10^{-5}$    | -36.9°   |
|      | (b)                      |          |

Table 1: evaluation board measurements for Circuit A

## 5.2 Circuit B

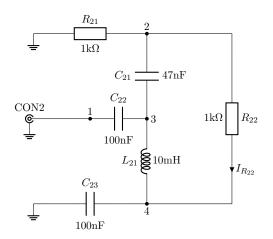


Figure 5: circuit B

Current  $I_{R_{22}}$  is measured indirectly using measured voltage and impedance of the component

$$I_{R_{22}} = \frac{U_4 - U_2}{Z_{R_{22}}}$$

where  $U_4$  is voltage in node 4,  $U_2$  is voltage in node 2 and  $Z_{R_{22}}$  is impedance of resistor  $R_{22}$ 

| Circuit B |              |               |           |  |
|-----------|--------------|---------------|-----------|--|
| Freq      | Channel 1[V] | Channel 2 [V] | Angle [°] |  |
| rreq      |              |               | Angle     |  |
|           | n            | ode 1         |           |  |
| 1kHz      | 0.192        | 0.192         | 0         |  |
| 5kHz      | 0.192        | 0.192         | -0.1      |  |
| 9kHz      | 0.192        | 0.192         | 0         |  |
|           | n            | ode 2         |           |  |
| 1kHz      | 0.192        | 0.044         | 28.7      |  |
| 5kHz      | 0.192        | 0.044         | -35.7     |  |
| 9kHz      | 0.192        | 0.156         | 69.7      |  |
|           | n            | ode 3         |           |  |
| 1kHz      | 0.192        | 0.084         | 23.3      |  |
| 5kHz      | 0.192        | 0.055         | 62.4      |  |
| 9kHz      | 0.192        | 0.22          | 24.4      |  |
| node 4    |              |               |           |  |
| 1kHz      | 0.192        | 0.086         | 21.2      |  |
| 5kHz      | 0.192        | 0.18          | -11.8     |  |
| 9kHz      | 0.192        | 0.09          | -113.8    |  |
|           |              |               |           |  |

(a)

| freq | $I_{R_{22}}[I]$       | Angle[°] |
|------|-----------------------|----------|
| 1kHz | $4.379 \cdot 10^{-5}$ | 28.83    |
| 5kHz | $1.407 \cdot 10^{-4}$ | 175.48   |
| 9kHz | $2.456 \cdot 10^{-4}$ | 68.44    |
|      | (b)                   |          |

Table 2: evaluation board measurements for Circuit B

# 6 Comparison

Results of measurements are in general similar to results of nodal analysis. In most cases at least first significant digit of amplitude is the same in both results and phase shifts are within few percent of error, for some applications it can be not satisfying, but roughly both results are comparable. In order to verify how precise nodal analysis is more data and more precise measuring equipment are needed

# 7 Summery

Nodal analysis broadly speaking is good method to evaluate values in a circuit, but in terms of precision as stated in Section 6 for some applications evaluation can be not good enough.

# Appendix

### A Source code circuit A

```
import numpy as np
from tabulate import tabulate
def get_V(f):
    w=2*np.pi*f
    Zr=1e3 #Zr1 == Zr2
    Zc1=1/(complex(0,100e-9)*w)
    Zc2=1/(complex(0,47e-9)*w)
    Zc3=1/(complex(0,22e-9)*w)
    Z1=complex(0,10e-3)*w
    V = 0.192
    G1 = 1/Zc2 + 1/(Zc1+Zr)
    G3 = 1/Zr + 1/Zc2 + 1/Z1
    G4 = 1/Zc3 + 1/(Zc1+Zr) + 1/Zr
    G13 = -1/Zc2
    G14 = -1/(Zr+Zc1)
    G34 = -1/Zr
    I1 = - V/(Zr+Zc1) - V/Zc2
    I3 = V/Zc2
    I4 = V/(Zr+Zc1)
    G = np.array([[G1, G13, G14],
                [G13, G3, G34],
                [G14, G34, G4]])
    I = np.array([[I1]],
                [I3],
                [I4]])
    V = np.matmul(np.linalg.inv(G), I)
    VP = np.angle(V, True)
    VA = np.abs(V)
    IC12 = (V[0]-V[1])/Zc2
    VA = np.append(VA, np.abs(IC12))
    VP = np.append(VP, np.angle(IC12))
    headers = [str(f)+' Hz' , 'Magnitude', 'Phase']
    first_col = ['Node 1', 'Node 3', 'Node 4', 'I of C_12']
    table1 = np.column_stack((first_col, VA, VP))
    print(tabulate(table1, headers=headers, tablefmt="latex"))
    return(V, VA, VP)
(V1, VA1, VP1)=get_V(1e3)
(V5, VA5, VP5)=get_V(5e3)
(V9, VA9, VP9)=get_V(9e3)
```

### B Source code circuit B

```
import numpy as np
from tabulate import tabulate
def get_V(f):
    w=2*np.pi*f
    Zr=1e3
    Zc1=1/(complex(0,47e-9)*w)
    Zc2=1/(complex(0,100e-9)*w)
    Zc3=1/(complex(0,100e-9)*w)
    Z1=complex(0,10e-3)*w
    V = 0.192
    G2 = 2/Zr + 1/Zc1
    G3 = 1/Zc1 + 1/Zc2 + 1/Z1
    G4 = 1/Zc3 + 1/Z1 + 1/Zr
    G23 = -1/Zc1
    G24 = -1/Zr
    G34 = -1/Z1
    I1 = 0
    I2 = V / (Zc2)
    I3 = 0
    G = np.array([[G2, G23, G24],
                [G23, G3, G34],
                [G24, G34, G4]])
    I = np.array([[I1],
                [I2],
                [I3]])
    V = np.matmul(np.linalg.inv(G), I)
    VP = np.angle(V, True)
    VA = np.abs(V)
    IR22 = (V[0]-V[2])/Zr
    VA = np.append(VA, np.abs(IR22))
    VP = np.append(VP, np.angle(IR22))
    headers = [str(f)+' Hz', 'Magnitude', 'Phase']
    first_col = ['Node 2', 'Node 3', 'Node 4', 'I of R_22']
    table1 = np.column_stack((first_col, VA, VP))
    print(tabulate(table1, headers=headers,tablefmt='latex'))
    return(V, VA, VP)
(V1, VA1, VP1)=get_V(1e3)
(V5, VA5, VP5)=get_V(5e3)
(V9, VA9, VP9)=get_V(9e3)
```