

HERITAGE INSTITUTE OF TECHNOLOGY  
KOLKATA

Electrical System Design Report

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Paper Name - Electrical System Design

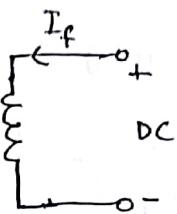
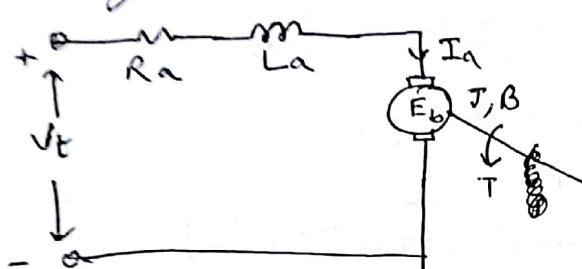
Paper Code - ELEC 4221

## speed control of Separately Excited DC Motor using armature voltage control in Simulink

In case of separately excited DC Motor, field and armature coils are electrically isolated. Field coil is excited by independent ~~with~~ DC voltage source, while armature has its own variable supply.

### Mathematical Model and Control Theory

The electrical circuit of the armature and field winding are shown



### Parameters of separately excited DC Motor

$R_a$  = Armature Resistance

$L_a$  = Armature Self Inductance

$I_a$  = Armature Current

$I_f$  = Field current

$E_b$  = Back emf in armature

$V$  = Applied voltage

$T$  = Torque developed by Motor

$\theta$  = Angular displacement of motor shaft

$J$  = Equivalent moment of inertia of motor shaft & load referred to motor

$B$  = Equivalent coefficient of friction of motor shaft and load referred to motor

DC Motors are generally used in the linear range of the magnetization curve. Therefore, air gap flux  $\phi$  is proportional to field current  $I_f$  & if  $\Rightarrow \phi = K_f I_f$  ... (i) where  $K_f$  is constant

The torque  $T$  developed by the motor is proportional to armature current and air gap flux, i.e.,  $T \propto \phi I_a \Rightarrow T = K_t \phi I_a$  ... (2)

Therefore  $T = K_t I_a$  where  $K_t$  is motor constant ... (2)

In armature controlled DC motor, field current is kept constant, so from equation (i) ...  $T_m = K_t I_a$  ... (iii)

where  $K_t$  = motor torque constant

The motor back emf being proportional to speed ( $\theta$ ) is given by  $e_b = K_b \frac{d\theta}{dt}$  ... (iv)  $K_b$  = back emf constant

The differential equation of armature circuit is

$$L_a \frac{di_a}{dt} + R_a i_a + e_b = e_a \dots (v)$$

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The torque equation is

$$J \frac{d^2\theta}{dt^2} + f_o \frac{d\theta}{dt} = T_m = K_T i_a \dots (vi)$$

Taking Laplace transformation of equation (iii) to (v)  
assuming zero initial condition, we get,

$$E_b(s) = K_b s \theta(s) \dots (vii)$$

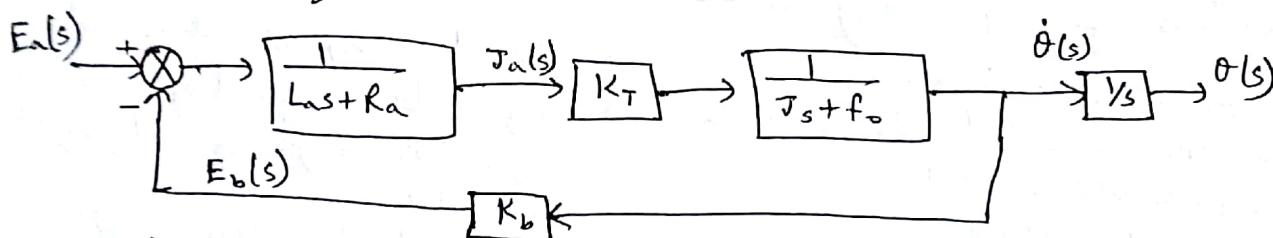
$$(L_a s + R_a) I_a(s) = E_a(s) - E_b(s) \dots (viii)$$

$$(J s^2 + f_o s) \theta(s) = T_m(s) = K_T I_a(s) \dots (ix)$$

Thus, transfer function is given by,

$$G(s) = \frac{\theta(s)}{E_a(s)} = \frac{K_T}{s[(R_a + L_a s)(J s + f_o) + K_T K_b]} \dots (x)$$

Block diagram :-



Speed  $\dot{\theta}(s)$  is in rad/s unit (equivalent to  $\omega$ )

$$\omega = \frac{2\pi N(\text{rpm})}{60} \quad \therefore N(\text{rpm}) = \left(\frac{30}{\pi}\right) \omega \text{ rad/s}$$

Field controlled DC Motor is open loop while armature controlled DC Motor is closed loop system and thus preferred. For small size motor, field control is advantageous because only a low power servo amplifier is required while armature current is not large. For large size motor, it is easier to use armature control scheme. Further in armature controlled motor, back emf contributes additional damping over and above load friction.

$$E_a(s) \rightarrow \frac{R_T}{s[(R_a + L_a s)(J s + f_o) + K_T K_b]} \rightarrow \dot{\theta}(s)$$

From this simplified equation of transfer function, the armature

inductance is very small in practice, hence the transfer function of DC motor speed to input voltage can be

simplified as follows,  $\text{in}(s) = \frac{\theta(s)}{E_a(s)} = \frac{K_m}{ns+1}$  ...

where,  $K_m = \frac{K}{R_a B + K_b K_T}$  is the motor gain

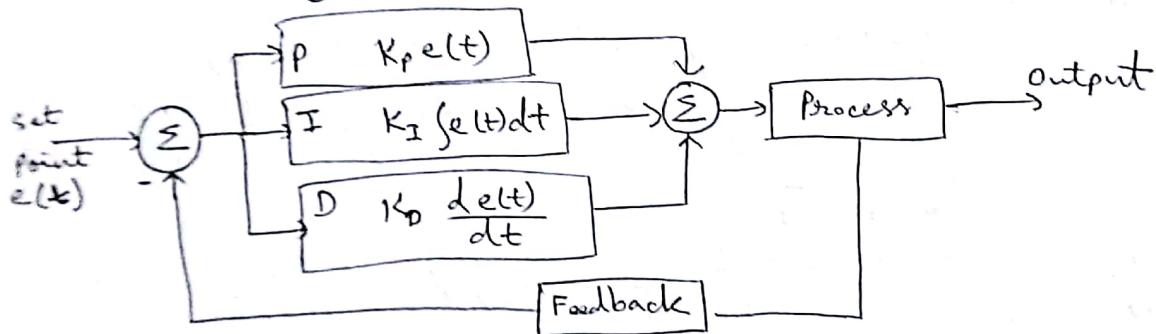
and  $n = \frac{R_a T}{R_a B + K_b K_T}$  is motor time constant

### Proportional-Integral-Derivative Controller Addition to circuit

A PID controller /Proportional-Integral-Derivative controller is a generic control loop feedback mechanism widely used in industrial control systems.

A PID controller calculates an "error" value as the difference between a measured process variable and a desired set point. The controller attempts to minimize the error by adjusting the process control inputs. In this section, the method to obtain the controller of a process is described using PID scheme. The transfer function of PID controller has form like

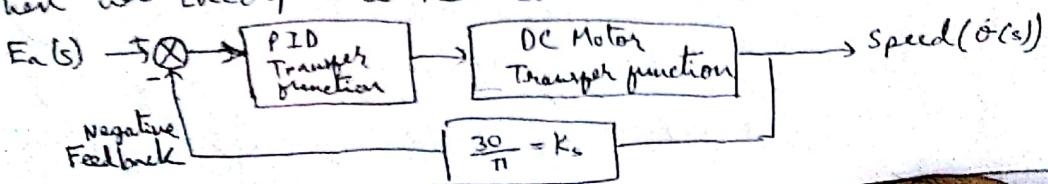
$$G(s) = K_p + \frac{K_i}{s} + K_d s$$



In our case, we know  $W (\text{rad/s}) = \frac{2\pi N}{60} (\text{rpm})$

$$\begin{aligned} \text{Transfer function of PID} &= P + \frac{I}{s} + \frac{DN}{s+N} = \frac{Ps(s+N) + I(s+N) + DNs^2}{s(s+N)} \\ &= \frac{s^2 DN + sI + NI + Ps^2 + PsN}{s^2 + Ns} \end{aligned}$$

When we incorporate PID controller in our circuit



So, our DC Motor TF is  $\frac{K_T}{s[(R_L+sL_a)(J_S+f_o)+K_T K_b]}$

and PID Transfer equation derivation continues to,

$$PID(s) = \frac{s^2 DN + sI + NI}{s^2 + NS} + \frac{s^2 P + PsN}{s^2 + NS} = \frac{(DN+P)s^2 + (I+PN)s + NI}{s^2 + NS}$$

On adding DC Motor & PID controller

$$\begin{aligned} G(s) &= \frac{K_T(DN+P)s^2 + K_T(I+PN)s + K_T NI}{s^3 + NS^2 [(R_L+sL_a)(J_S+f_o) + K_T K_b]} \\ &= \frac{(DNK_T+PK_T)s^2 + (K_T I + PN K_T)s + K_T NI}{s^5 JL_a + s^4 (f_o L_a + JR_a + NJL_a) + s^3 (f_o R_a + K_T K_b + NJR_a + NF_o L_a)} \\ &\quad + s^2 (NF_o R_a + NK_T K_b) \quad \dots (7) \end{aligned}$$

Now we are considering the feedback loop also,

$$\text{Overall TF} = \frac{G(s)}{1 + G(s)H(s)} \text{ (for negative feedback)}$$

$G(s)$  = Forward TF derived in eqn (7)

$H(s)$  = feedback TF =  $K_s$

We assume  $JL_a = 8 \times 10^{-4} \approx 0$ , so overall TF will look like

$$\frac{G(s)}{1 + G(s)H(s)} = \frac{\overset{A}{(DNK_T+PK_T)s^2} + \overset{B}{(K_T J + PN K_T)s} + \overset{C}{K_T NI}}{s^4(f_o L_a + JR_a + NJL_a) + s^3(f_o R_a + K_T K_b + NJR_a + NF_o L_a) + s^2(NF_o R_a + NK_T K_b + DNK_T K_s + PK_T K_s)s + s(K_T I K_s + PN K_T K_s) + K_T K_s NI} \quad \overset{D}{\cancel{JL_a}} \quad \overset{E}{\cancel{JR_a}} \quad \overset{F}{\cancel{NJK_b}} \quad \overset{G}{\cancel{DNK_T K_s}} \quad \overset{H}{\cancel{PK_T K_s}}$$

$$\frac{Y(s)}{U(s)} = \frac{As^2 + Bs + C}{Ds^4 + Es^3 + Fs^2 + Gs + H} = \frac{Y(s)}{X_1(s)} \frac{X_1(s)}{U(s)}$$

$$\frac{X_1(s)}{U(s)} = \frac{1}{s^4 D + s^3 E + s^2 F + s G + H}$$

$$s^4 D X_1(s) + s^3 E X_1(s) + s^2 F X_1(s) + s G X_1(s) + H X_1(s) = U(s) \quad \dots (a)$$

$$L[X_1(t)] = x_1(s)$$

$$x_2(t) = \dot{x}_1(t)$$

$$x_3(t) = \ddot{x}_1(t) = \ddot{x}_2(t)$$

$$x_4(t) = \dot{x}_3(t) = \dot{x}_2(t)$$

$$y(t) = A \ddot{x}_1(t) + B \dot{x}_2(t) + C x_3(t)$$

$$\ddot{x}_1(t) + \left(\frac{E}{D}\right) \ddot{x}_2(t) + \left(\frac{F}{D}\right) \dot{x}_3(t) + \left(\frac{G}{D}\right) x_3(t) + \left(\frac{H}{D}\right) x_2(t) = \frac{1}{D} u(t)$$

$$\dot{x}_4(t) = -\frac{E}{D} x_4(t) - \frac{F}{D} x_3(t) - \frac{G}{D} x_2(t) - \frac{H}{D} x_1(t) + \frac{1}{D} u(t)$$

State Equation  $\dot{x} = [A_1]x + [B_1]v$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -F/D \\ -T/P & -Cn/P & -F/D & -E/D \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1/D \end{bmatrix} v$$

$$y = [c \ B \ A \ 0] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + [0] v$$

Parameters taken for building model

Rating:- 5 HP, 1750 RPM, Field voltage = 300 V

$$\text{Calculated rated torque} = \frac{5 \text{ HP}}{1750 \text{ RPM}} = 20.3536 \text{ Nm}$$

= Load Torque

Armature Resistance ( $R_a$ ) = 11.2 Ω

Armature Inductance ( $L_a$ ) = 0.1215 H

Field Resistance ( $R_f$ ) = 281.03 Ω

Field Inductance ( $L_f$ ) = 156 H

Field Armature Mutual Inductance ( $L_{af}$ ) = 1.976 H

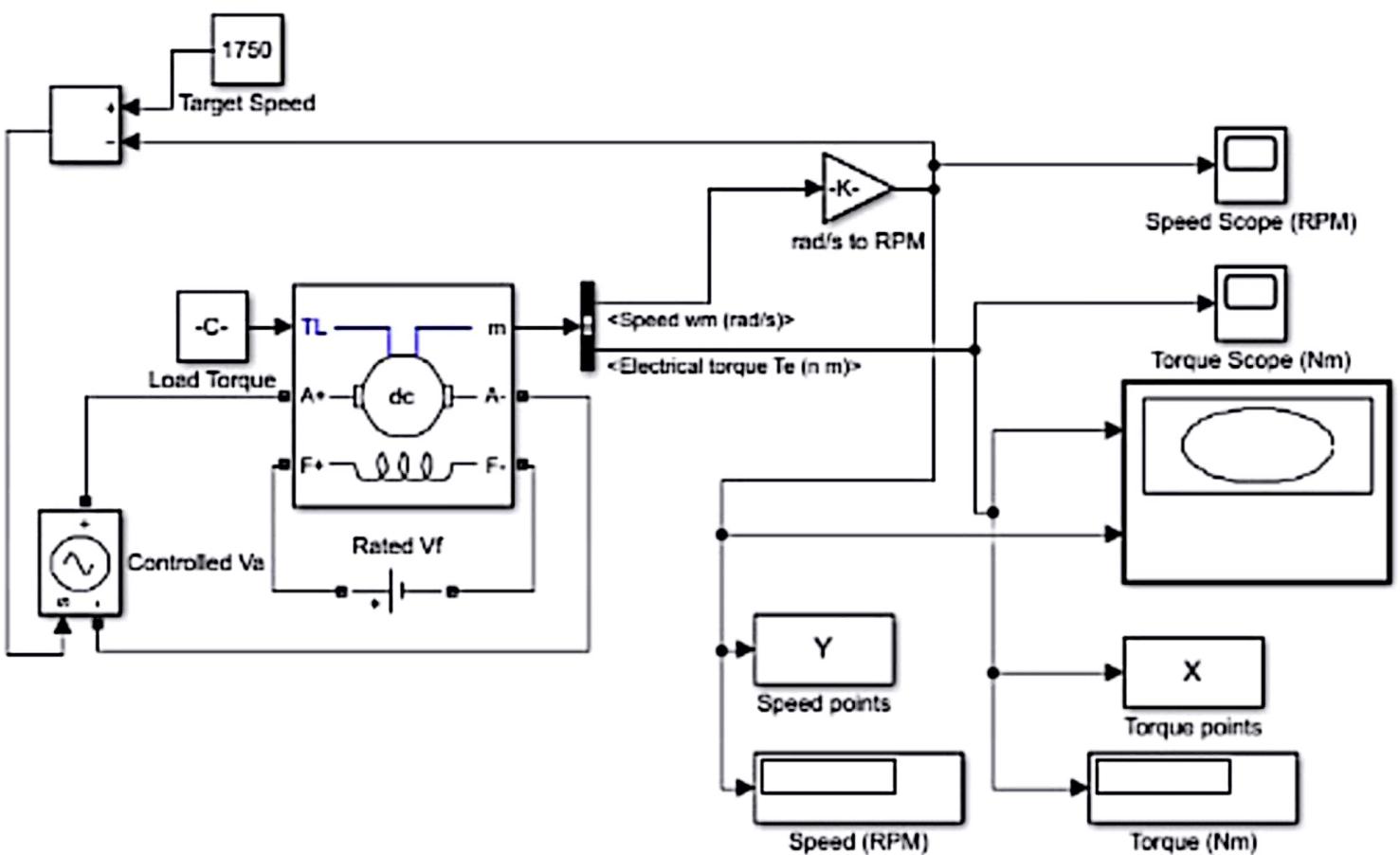
Total inertia  $J = 0.02215 \text{ kgm}^2$

Viscous friction coefficient  $B_m = 0.002953 \text{ Nms}$

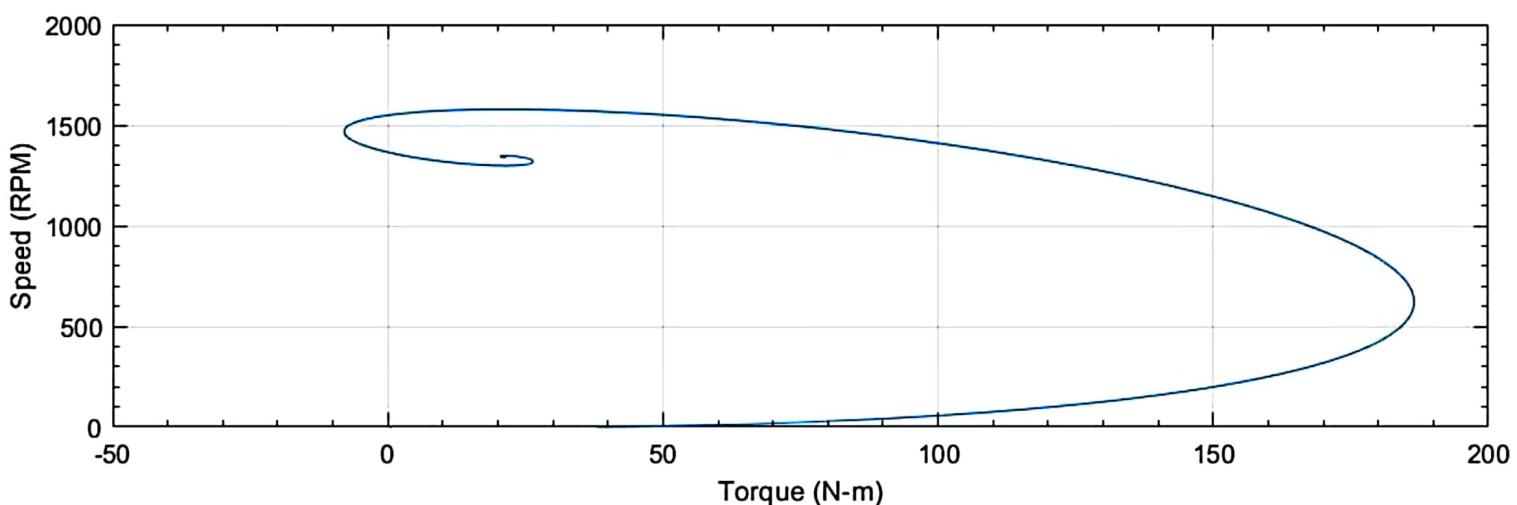
Coulomb friction Torque  $T_f = 0.576 \text{ Nm}$

rad/s to RPM gain = 9.5493

Target speed = 1750 rpm

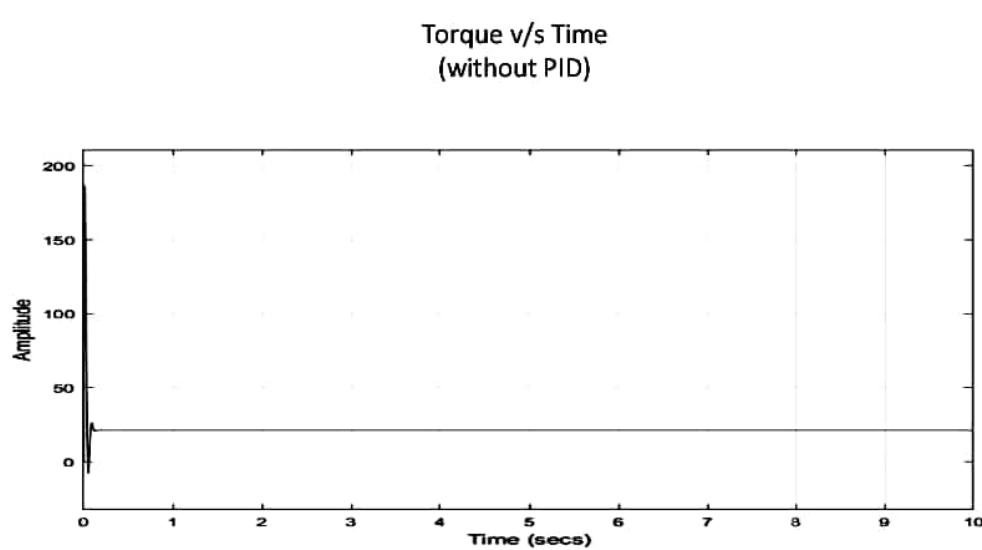
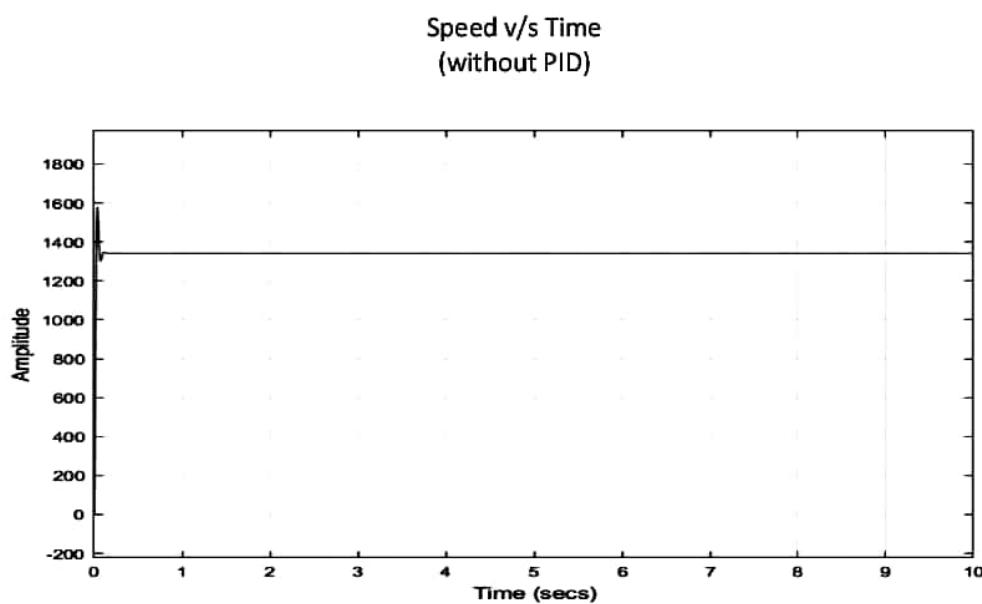


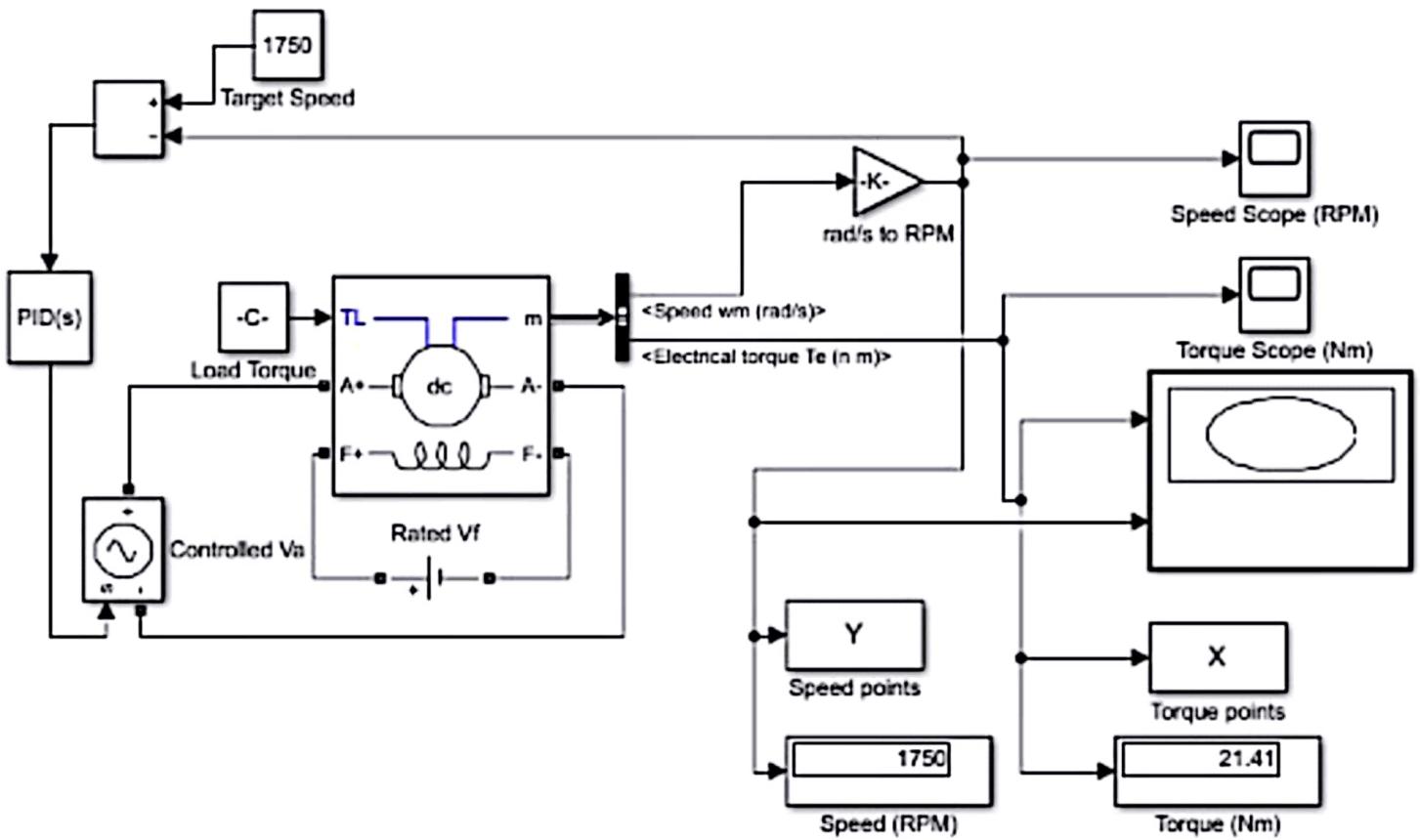
# Circuit without PID Controller



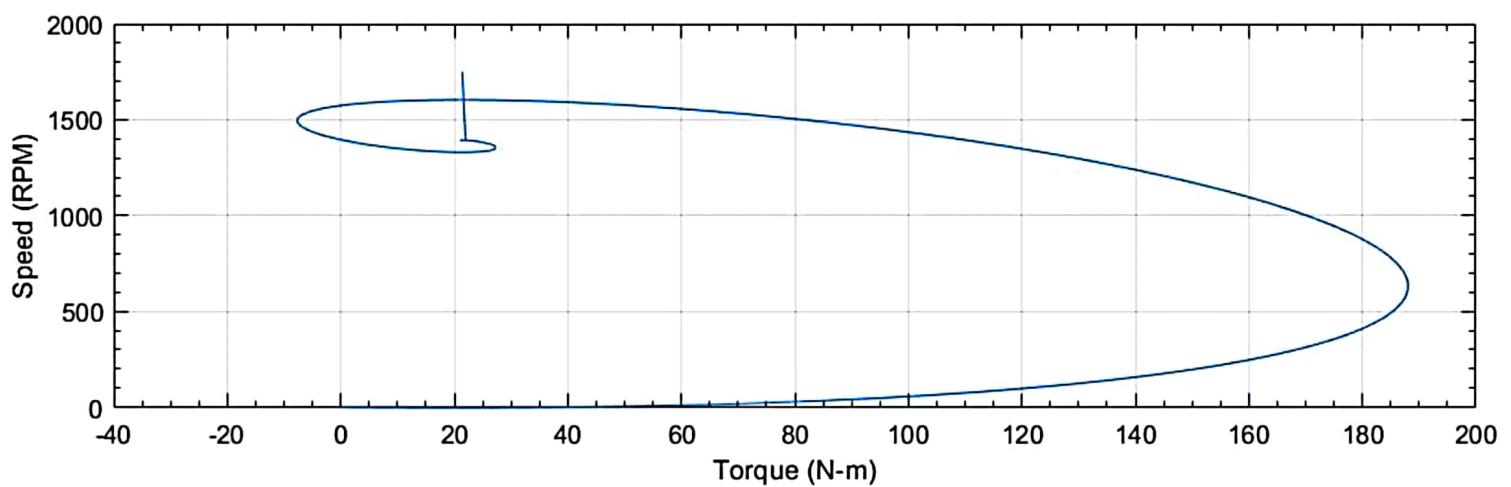
# Output without PID Controller

Without PID



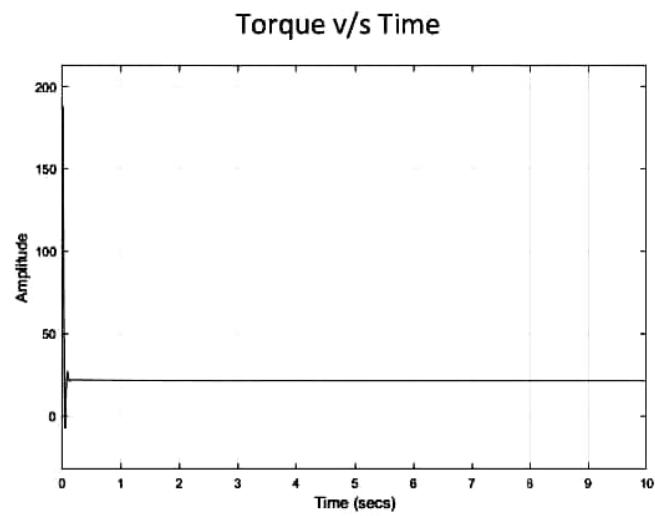
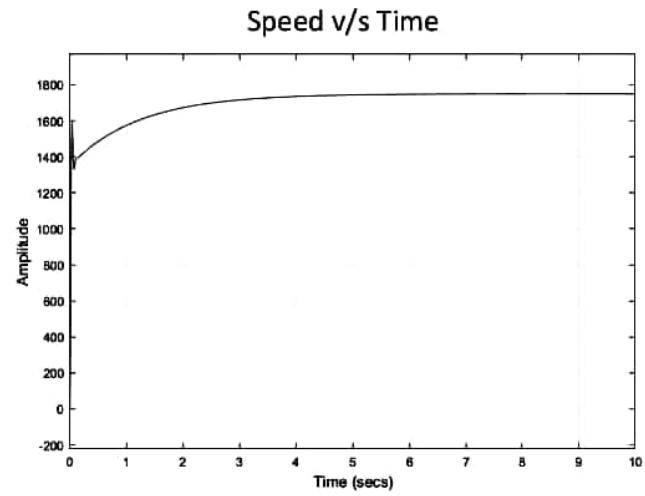


# Circuit with PID Controller



# Output with PID Controller

With PID



Power System DesignDistribution System Design of Ideal City (Block A)Step I

Survey of model town

Dividing roads into small segments

Identify load position

We will calculate load street light load

and we are putting street light hundred meter apart

We are going to collect and organize data in following format :-

Road segment No

Road length in map (cm)

Actual road length (m)

Road width in map (cm)

Actual road width (m)

Lighting wattage (W)

Lighting type (both side for each entry)

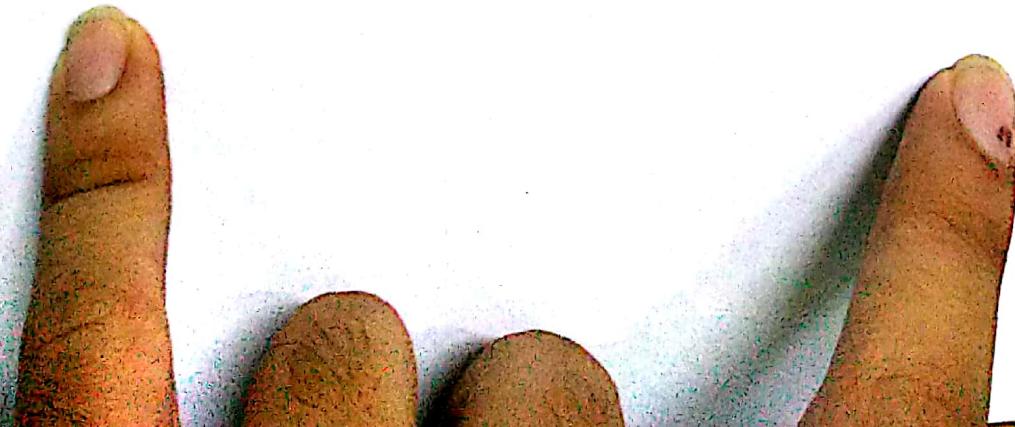
Number of light

Total wattage (kW)

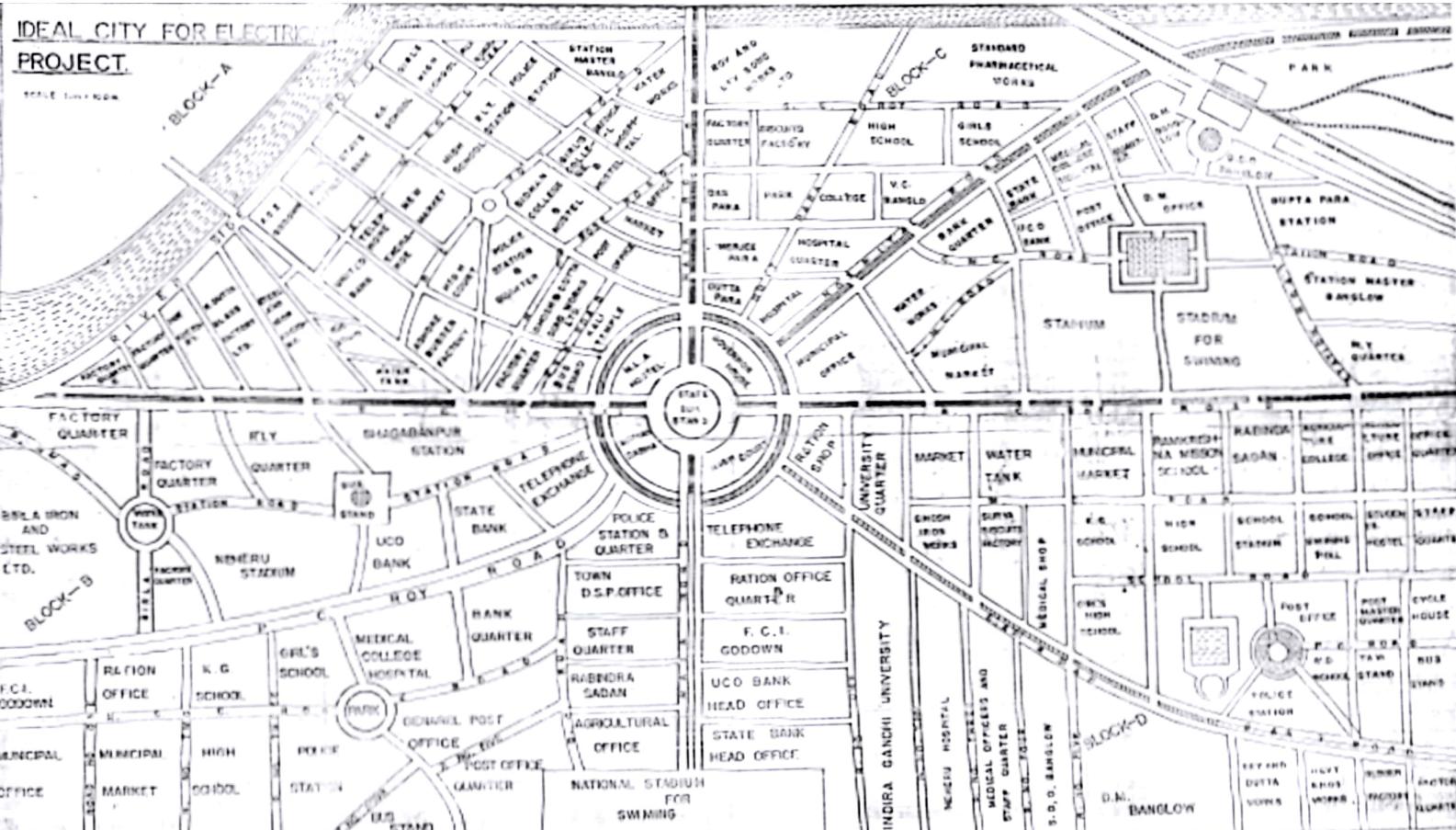
And the total road length in actual is 35514 meters

Number of lights used - 708 pieces

Total wattage in kW = 141.6



## IDEAL CITY FOR ELECTRICAL PROJECT.



### Distribution System Design Of Ideal City (Block - A)

STEP - I								
Survey of Model Town. Divide the rods into small segments. Identify load position.								
Calculate total street light load. Put street light 100 meter apart and								
<b>STREET LIGHT LOAD</b>								
Road segment no.	Road length in map (cm)	Actual road length (m)	Road width in map(cm)	Actual road width (m)	Lighting wattage (W)	Lighting Type	No. of light	Total Wattage (KW)
1	4.9	490	0.5	50	200	Both Side	10	2
2	30	3000	0.5	50	200	Both Side	60	12
3	3	300	0.5	50	200	Both Side	6	1.2
4	5	500	0.5	50	200	Both Side	10	2
5	7	700	0.5	50	200	Both Side	14	2.8
6	9.5	950	0.5	50	200	Both Side	19	3.8
7	12	1200	0.5	50	200	Both Side	24	4.8
8	1	100	0.5	50	200	Both Side	2	0.4
9	3	300	0.5	50	200	Both Side	6	1.2
10	4.2	420	0.5	50	200	Both Side	8	1.6
11	15.5	1550	0.5	50	200	Both Side	31	6.2
12	17	1700	0.5	50	200	Both Side	34	6.8
13	4.7	470	0.5	50	200	Both Side	9	1.8
14	4.5	450	0.5	50	200	Both Side	9	1.8
15	4.7	470	0.5	50	200	Both Side	9	1.8
16	4.7	470	0.5	50	200	Both Side	9	1.8
17	3.2	320	0.5	50	200	Both Side	6	1.2
18	4.9	490	0.5	50	200	Both Side	10	2
19	4.5	450	0.5	50	200	Both Side	9	1.8
20	4.2	420	0.5	50	200	Both Side	8	1.6
21	5	500	0.5	50	200	Both Side	10	2
22	5.3	530	0.5	50	200	Both Side	11	2.2
23	5.5	550	0.5	50	200	Both Side	11	2.2
24	8.5	850	0.5	50	200	Both Side	17	3.4
25	13.2	1320	0.5	50	200	Both Side	26	5.2
26	3.3	330	0.5	50	200	Both Side	7	1.4
27	9.5	950	0.5	50	200	Both Side	19	3.8
28	9	900	0.5	50	200	Both Side	18	3.6
29	2	200	0.5	50	200	Both Side	4	0.8
30	2.5	250	0.5	50	200	Both Side	5	1
31	7.7	770	0.5	50	200	Both Side	15	3
32	2	200	0.5	50	200	Both Side	4	0.8
33	8	800	0.5	50	200	Both Side	16	3.2
34	6.5	650	0.5	50	200	Both Side	13	2.6
35	3.5	350	0.5	50	200	Both Side	7	1.4
36	11.5	1150	0.5	50	200	Both Side	23	4.6
37	5	500	0.5	50	200	Both Side	10	2
38	5	500	0.5	50	200	Both Side	10	2
39	8.5	850	0.5	50	200	Both Side	17	3.4
40	5	500	0.5	50	200	Both Side	10	2
41	3.5	350	0.5	50	200	Both Side	7	1.4
42	4.5	450	0.5	50	200	Both Side	9	1.8
43	16.5	1650	0.5	50	200	Both Side	33	6.6
44	20	2000	0.5	50	200	Both Side	40	8
45	33.5	3350	0.5	50	200	Both Side	67	13.4
46	3.14	314	0.5	50	200	Both Side	6	1.2
<b>Total</b>		<b>35,514.00</b>					<b>708</b>	<b>141.6</b>

## Step II Estimation of different types of loads

Each flat load to be computed as:

Item	Watt/unit	Qty	Total wattage
Tube light	40	4	160
Bulb	60	5	300
Fan	80	3	240
TV	120	2	240
Refrigerator	350	1	350

$$\text{Each flat total load} = \frac{1290 \text{ W}}{\text{load}} = 1.29 \text{ kW}$$

### Domestic Load Description:

Type of Building	Flat/Building	Total No of Building	Total no of flat	Load/ building (kW)	Total Building load (kW)
2-Storied	4	300	1200	5.16	1548
3-Storied	6	120	720	7.74	928.8
Multi Storied	10	50	500	12.9	645
Station master bungalow					15
MLA Hostel					26
			2420 (Total flats)		3162.8 (Total load)

∴ Total 3162.8 kW domestic load in 2420 flats

### Commercial load calculation:

Item	Load (kW)
United Bank	15
State Bank	15
Police Station 1	100
Police Station 2	100
Market	40
New Market	40
Post office	5

Total Commercial load is 491 kW

Item	Load (kW)
Bus Stand 1	3
Bus Stand 2	3
High Court	40
Office	10
FCL Ord.	30
Kali Temple	10
Medical college	50
Telecom executive	30

## Industrial Load Calculation:

Item	Load (kW)
Steel & iron factory	150
Ashok rubber factory	100
Ink Factory	50
K Dutta Glass Factory	100
Ghosh & Dutta Works Ltd	75
Total	475

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## Public Load Calculation:

Item	Load (kW)
High School	30
Girls School	30
K.G. School	8
Railway Station	40
Bidhan College & Hospital	50
Girls College & Hostel	50
Water Works	1670
Water Tank	850
Total	2728

## Capacity Calculation of Water Works:

Water consumption / head / day = 20 ltr (assume)

$$\begin{aligned} \text{Total population} &= (\text{Total no of flats} \times \text{person per flat}) + \text{outsiders per day} \\ &= 2420 \times 6 + 30\% (2420 \times 6) = 18876 \end{aligned}$$

$$\text{Total water consumption} = 18876 \times 20 = 377520 \text{ ltr/day}$$

$$\text{Total water generation} = 377520 + 10\% (\text{wastage}) = 415272 \text{ ltr/day}$$

$$\text{Supply time} = 5 \text{ hr/day} \quad \text{Pump size} = 3000 \text{ ltr/day} \quad \text{Motor size} = 420 \text{ kW}$$

$$\text{No of pump} = \frac{\text{Total water consumption}}{\text{Pump Capacity} \times \text{Supply time}} = 6$$

$$\text{Total power consumption} = 2520 \text{ kW}$$

$$\text{Power consumption for filling water} = (420 \times 2 + 10) = 850 \text{ kW}$$

$$\text{Therefore actual power consumption} = 2520 - 850 = 1670 \text{ kW}$$

## Each Area Load (LT)

Domestic load	3163 kW
Street light load	142 kW
Public load	208 kW
Commercial load	491 kW
Industrial load	0
Total	4003 kW

$$\text{Total connected load (HT+LT)} = 6998 \text{ kW}$$

## Each Area Load (HT)

Public Load	2520 kW
Commercial load	0 kW
Industrial load	475 kW
Total	2995 kW

<b>SL. NO.</b>	<b>Load Type</b>		<b>Qty</b>	<b>Power consumtion(k W Each)</b>
1	<i>DOMESTIC</i>	<i>Multistorried building</i>	50	
2	<i>DOMESTIC</i>	<i>3- Storried building</i>	120	
3	<i>DOMESTIC</i>	<i>2- Storried building</i>	300	
4	<i>DOMESTIC</i>	<i>Station master banglo</i>	1	
5	<i>DOMESTIC</i>	<i>M.L.A. HOSTEL</i>	1	
6	<i>PUBLIC</i>	<i>Water works</i>	1	
7	<i>PUBLIC</i>	<i>Water tank</i>	1	
8	<i>PUBLIC</i>	<i>Railway station</i>	1	40
9	<i>PUBLIC</i>	<i>High school</i>	1	30
10	<i>PUBLIC</i>	<i>Girl's school</i>	1	30
11	<i>PUBLIC</i>	<i>K.G. SCHOOL</i>	2	4
12	<i>COMMERCIAL</i>	<i>United bank</i>	1	15
13	<i>COMMERCIAL</i>	<i>State bank</i>	1	15
14	<i>COMMERCIAL</i>	<i>Police station</i>	1	10
15	<i>COMMERCIAL</i>	<i>Market</i>	2	40
16	<i>COMMERCIAL</i>	<i>Post office</i>	2	5
17	<i>COMMERCIAL</i>	<i>bus stand</i>	1	3
18	<i>COMMERCIAL</i>	<i>High court</i>	1	40
19	<i>COMMERCIAL</i>	<i>High school</i>	1	20
20	<i>COMMERCIAL</i>	<i>FCI Godown</i>	1	30
21	<i>COMMERCIAL</i>	<i>Kali Temple</i>	1	10
22	<i>COMMERCIAL</i>	<i>Telephone exchange</i>	1	30
23	<i>INDUSTRIAL</i>	<i>Steel and iron factory</i>	1	150
24	<i>INDUSTRIAL</i>	<i>Ashoke rubber factory</i>	1	100
25	<i>INDUSTRIAL</i>	<i>Ink factory</i>	1	50
26	<i>INDUSTRIAL</i>	<i>K.Dutta glass factory Ltd.</i>	1	100
27	<i>INDUSTRIAL</i>	<i>Ghosh &amp; duttasons Works Ltd.</i>	1	75

Step III

Area II

Loop A

Total connected load in kw	
Domestic load	1981
street light load	78
Public load	954
Commercial load	148
Industrial load	300
Total	3461

Loop B	
Total connected Load in kw	
Domestic load	= 1285 <del>kw</del>
street light load	= 63
Public load	= 1770
Commercial load	= 168
Industrial load	= 175
Total	3462

Now we can see from attached chart, the estimated demand factor of different loads of summer & winter (hourly basis for 24 hrs of the day in step of 4 hrs)

Calculating effective load on hourly basis for different loops (for summer & winter) :

For loop A summer

	Duration (hrs)						
Total connected load	6-10	10-14	14-18	18-20	20-22	22-02	02-06

For loop A winter

	Duration (hrs)						
Total connected load	5.30-9.30	9.30-13.30	13.30-17.30	17.30- -19.30	19.30- -21.30	21.30- -1.30	1.30- -5.30

For loop B winter

	Duration (hrs)						
Total connected load	5.30- -9.30	9.30- -13.30	13.30- -17.30	17.30- -19.30	19.30- -21.30	21.30- -1.30	1.30- -5.30

Division of Loops :					
Loop No.	Domestic Load (KW)	Street Light Load (KW)	Public Load (KW)	Commercial Load (KW)	Industrial Load (KW)
Loop - A [o]	50	78.2	850	3	50
Loop - A [o]	50		4	30	100
Loop - A [o]	77.4		30	15	150
Loop - A [o]	108.2		30	5	
Loop - A [o]	195.8		40	30	
Loop - A [o]	115.9			15	
Loop - A [o]	149.2			40	
Loop - A [o]	154			10	
Loop - A [o]	193				
Loop - A [o]	87.6				
Loop - A [o]	90.1				
Loop - A [o]	51.6				
Loop - A [o]	51.6				
Loop - A [o]	51.6				
Loop - A [o]	82.6				
Loop - A [o]	51.6				
Loop - A [o]	30.8				
Loop - A [o]	90.1				
Loop - A [o]	51.6				
Loop - A [o]	77.4				
Loop - A [o]	40				
Loop - A [o]	115.9				
Loop - A [o]	15				
<b>TOTAL</b>	<b>1981</b>	<b>78.2</b>	<b>954</b>	<b>148</b>	<b>300</b>
Loop No.	Domestic Load (KW)	Street Light Load (KW)	Public Load (KW)	Commercial Load (KW)	Industrial Load (KW)
Loop - B [*]	159.8	63.4	1670	50	75
Loop - B [*]	61.8		50	5	100
Loop - B [*]	157.3		50	40	
Loop - B [*]	229.2			10	
Loop - B [*]	201.2			10	
Loop - B [*]	50			10	
Loop - B [*]	118.3			3	
Loop - B [*]	26			40	
Loop - B [*]	50				
Loop - B [*]	164.7				
Loop - B [*]	67				
<b>TOTAL</b>	<b>1285.3</b>	<b>63.4</b>	<b>1770</b>	<b>168</b>	<b>175</b>
Note:	Highlited Cells are HT Load				

II) Calculate effective load on hourly basis for different loops (for summer & winter)							
For Loop - A Summer							
Type of load	Total connected Load (KW)	Duration (hrs)					
		06 -- 10	10 -- 14	14 -- 18	18 -- 20	20 -- 22	22 -- 02
Domestic	1981	693.35	495.25	495.25	1485.75	1485.75	495.25
Street Light	78.2	0	0	0	78.2	78.2	78.2
Public	954	343.44	763.2	524.7	238.5	190.8	143.1
Commercial	148	51.8	103.6	106.56	106.56	59.2	44.4
Industrial	300	240	255	255	255	210	180
<b>Total</b>		<b>1,328.59</b>	<b>1,617.05</b>	<b>1,381.51</b>	<b>2,164.01</b>	<b>2,023.95</b>	<b>940.95</b>
For Loop - A Winter							
Type of load	Total connected Load (KW)	Duration (hrs)					
		5.30 - 9.30	9.30 - 13.30	13.30 - 17.30	17.30 - 19.30	19.30 - 21.30	21.30 - 1.30
Domestic	1981	495.25	297.15	297.15	1386.7	990.5	198.1
Street Light	78.2	0	0	0	78.2	78.2	78.2
Public	954	143.1	763.2	381.6	95.4	95.4	95.4
Commercial	148	37	88.8	96.2	66.6	37	14.8
Industrial	300	195	240	240	210	180	150
<b>Total</b>		<b>870.35</b>	<b>1,389.15</b>	<b>1,014.95</b>	<b>1,836.90</b>	<b>1,381.10</b>	<b>536.50</b>
For Loop - B Summer							
Type of load	Total connected Load (KW)	Duration (hrs)					
		06 -- 10	10 -- 14	14 -- 18	18 -- 20	20 -- 22	22 -- 02
Domestic	1285.3	449.855	321.325	321.325	963.975	963.975	321.325
Street Light	63.4	0	0	0	63.4	63.4	63.4
Public	1770	637.2	1416	973.5	442.5	354	265.5
Commercial	168	58.8	117.6	120.96	120.96	67.2	50.4
Industrial	175	140	148.75	148.75	148.75	122.5	105
<b>Total</b>		<b>1,285.86</b>	<b>2,003.68</b>	<b>1,564.54</b>	<b>1,739.59</b>	<b>1,571.08</b>	<b>805.63</b>
For Loop - B Winter							
Type of load	Total connected Load (KW)	Duration (hrs)					
		5.30 - 9.30	9.30 - 13.30	13.30 - 17.30	17.30 - 19.30	19.30 - 21.30	21.30 - 1.30
Domestic	1285.3	321.325	192.795	192.795	899.71	642.65	128.53
Street Light	63.4	0	0	0	63.4	63.4	63.4
Public	1770	265.5	1416	708	177	177	177
Commercial	168	42	100.8	109.2	75.6	42	16.8
Industrial	175	113.75	140	140	122.5	105	87.5
<b>Total</b>		<b>742.58</b>	<b>1,849.60</b>	<b>1,150.00</b>	<b>1,338.21</b>	<b>1,030.05</b>	<b>473.23</b>

## Transformer Selection:

	Loop A	Loop B
Maximum Demand (kW)	2164	2004
Maximum Demand (kVA, pf=0.8)	2546	2357
Maximum Demand (taking 50% extra for power loss and future extension)	3819	3536
HT load (kW)	1150	1845
HT Load (kVA, pf=0.85)	1353	2171
LT load (kVA)	2466	1365
Transformer rating (kVA)	500	500
No of Transformer (500 kVA)	5	4

## Load distribution in Transformers

Transformer Number	T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	T <sub>6</sub>	T <sub>7</sub>	T <sub>8</sub>	T <sub>9</sub>
Total connected load	431.4	436.3	459.1	435.5	406.7	381.7	413.5	367.1	391
connected load details	50	149.2	115.9	51.6	30	40	3	50	229.2
	50	3	154	4	90.1	67	10	154.8	50
	77.4	129	30	30	40	164.7	118.3	157.3	50
	103.2	15	5	51.6	82.6	50	26		61.8
	145.3	90.1	87.6	40	30	10	201.2		
		50	51.6	15	51.6	50	5		
			15	10	51.6		40		
				115.9	30.8		10		
				40					
				77.4					

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Step 4 : Determination of load centre is required for power system distribution optimization. It has been done statistically.

Determine that a distribution system operates most optimally when electrical loads are considered as masses and supply transformer is placed at the C.G. of the designated loop determined as;

$$X = \frac{\sum P_i X_i}{\sum P_i} \quad \& \quad Y = \frac{\sum P_i Y_i}{\sum P_i}$$

where,  $P_i$  =  $i$ th load

$X_i, Y_i$  = corresponding distance from reference axes  $X$  &  $Y$

LOAD CENTER CALCULATION FOR LT LOAD:										
Transformer	P(kW)	Xi(cm)	Yi(cm)	PXi	Pyi	current (A)	X(cm)	Y(cm)	TOTAL AMP(A)	PRIMARY CURRENT (A)
T1	50.00	4.00	2.00	200.00	100.00	81.84	7.33	2.70	706.08	26.64
	50.00	4.60	4.00	230.00	200.00	81.84				
	77.40	6.50	0.60	503.10	46.44	126.68				
	108.20	7.80	1.50	843.96	162.30	177.09				
	145.80	9.50	4.50	1385.10	656.10	238.63				
T2	149.20	15.60	2.50	2327.52	373.00	244.20	15.08	3.96	714.10	26.94
	3.00	15.00	3.70	45.00	11.10	4.91				
	129.00	13.40	5.70	1728.60	735.30	211.14				
	15.00	15.70	5.90	235.50	88.50	24.55				
	90.10	17.90	4.50	1612.79	405.45	147.47				
T3	50.00	12.60	2.30	630.00	115.00	81.84	11.43	10.38	751.41	28.35
	115.90	9.20	9.00	1066.28	1043.10	189.69				
	154.00	9.90	9.60	1524.60	1478.40	252.05				
	30.00	11.00	11.10	330.00	333.00	49.10				
	5.00	12.70	13.30	63.50	66.50	8.18				
T4	87.60	14.80	9.80	1296.48	858.48	143.38	22.96	17.06	712.79	26.89
	51.60	14.20	15.30	732.72	789.48	84.45				
	15.00	15.50	13.20	232.50	198.00	24.55				
	51.60	16.10	17.80	830.76	918.48	84.45				
	4.00	17.00	15.50	68.00	62.00	6.55				
T5	30.00	18.90	18.00	567.00	540.00	49.10	19.28	11.84	665.65	25.11
	51.60	21.90	17.60	1130.04	908.16	84.45				
	40.00	23.50	19.40	940.00	776.00	65.47				
	15.00	28.00	19.00	420.00	285.00	24.55				
	10.00	26.40	19.50	264.00	195.00	16.37				
T6	115.90	25.90	16.70	3001.81	1935.53	189.69	23.46	4.97	624.73	23.57
	40.00	22.20	17.20	888.00	688.00	65.47				
	77.40	24.40	14.50	1888.56	1122.30	126.68				
	30.00	20.20	15.00	606.00	450.00	49.10				
	90.10	21.70	12.50	1955.17	1126.25	147.47				
T7	40.00	18.20	12.70	728.00	508.00	65.47	27.05	6.61	676.78	25.53
	82.60	20.10	9.90	1660.26	817.74	135.19				
	30.00	17.80	8.00	534.00	240.00	49.10				
	51.60	16.30	10.50	841.08	541.80	84.45				
	51.60	18.00	12.80	928.80	660.48	84.45				
T8	30.80	19.10	15.30	588.28	471.24	50.41	27.57	13.57	600.84	22.67
	40.00	21.00	7.70	840.00	308.00	65.47				
	67.00	21.70	8.80	1453.90	589.60	109.66				
	164.70	23.50	3.00	3870.45	494.10	269.57				
	50.00	26.50	6.20	1325.00	310.00	81.84				
T9	10.00	23.60	7.60	236.00	76.00	16.37	21.79	12.94	639.95	24.14
	50.00	24.60	2.40	1230.00	120.00	81.84				
	3.00	22.60	1.30	67.80	3.90	4.91				
	10.00	23.90	4.00	239.00	40.00	16.37				
	118.30	25.30	6.30	2992.99	745.29	193.62				
T10	26.00	26.80	3.20	696.80	83.20	42.55	27.57	13.57	600.84	22.67
	201.20	27.80	6.60	5593.36	1327.92	329.31				
	5.00	25.00	7.90	125.00	39.50	8.18				
	40.00	29.40	9.40	1176.00	376.00	65.47				
	10.00	29.30	11.80	293.00	118.00	16.37				
T11	50.00	25.40	14.60	1270.00	730.00	81.84	27.57	13.57	600.84	22.67
	159.80	29.30	14.80	4682.14	2365.04	261.55				
	157.30	26.50	12.00	4168.45	1887.60	257.45				
T12	229.20	20.30	12.80	4652.76	2933.76	375.13	21.79	12.94	639.95	24.14
	50.00	23.00	12.60	1150.00	630.00	81.84				
	50.00	25.20	14.20	1260.00	710.00	81.84				
	61.80	23.60	12.70	1458.48	784.86	101.15				

LOAD CENTER CALCULATION FOR HT LOAD:										
Transformer & HT Load	P(kW)	Xi(cm)	Yi(cm)	PXi	Pyi	current(A)	X(cm)	Y(cm)	11kv, TOTAL AMP(A)	132kv, PRIMARY CURRENT (A)
T1	425.00	7.33	2.70	3115.25	1147.56	26.24				
T2	425.00	15.08	3.96	6409.01	1683.59	26.24				
T3	425.00	11.43	10.38	4856.42	4412.89	26.24				
T4	425.00	22.96	17.06	9757.11	7251.32	26.24				
T5	425.00	19.28	11.84	8194.43	5032.19	26.24				
HT Load	50.00	6.20	5.50	310.00	275.00	3.09				
HT Load	100.00	7.80	7.30	780.00	730.00	6.17				
HT Load	150.00	11.90	4.50	1785.00	675.00	9.26				
HT Load	850.00	19.50	0.70	16575.00	595.00	52.49				
T6	425.00	23.46	4.97	9971.24	2112.97	26.24				
T7	425.00	32.05	6.61	13619.99	2809.84	26.24				
T8	425.00	32.57	13.57	13841.84	5768.52	26.24				
T9	425.00	26.79	12.94	11387.22	5498.50	26.24				
HT Load	100.00	20.60	2.40	2060.00	240.00	6.17				
HT Load	75.00	27.00	6.30	2025.00	472.50	4.63				
HT Load	1670.00	28.00	18.80	46760.00	31396.00	103.12				
Therefore rating of the transmission transformer =							4.63	MVA		

Conductor Selection :											Current rating (Amps)			
Feeder Specification:	Code Name	Size	Standard (A/St)	Dia (Inch)				Weight per 1000 ft (lbs)			Content %	Rated Strength (lbs)	Resistance ohm / 1000 ft	
				Individual (A/L)	Wire (STL)	Steel Core	Complete Cable	A/L	Stl	Total			DC @ 20 °C	AC @ 75 °C
LT feeder	Stilt	715.5	24/7	0.1727	0.1151	0.3453	1.036	675.2	246.5	921.8	73.23	26.77	25500	0.0239
for all HT load service line	Turkey	6	6/1	.0661	.0661	.0661	.198	24.5	11.6	36.1	67.90	32.10	1190	.641
HT feeder	Waxwing	266.8	18/1	0.1217	0.1217	0.1217	0.609	250.3	39.2	289.5	86.45	13.55	6,880	0.0643
LT distribution size justification :														
	Current (A)	Length (cm)	Resistance (ohm / 1000 ft)	Resistance (ohm)	Voltage Drop (%)									
Loop of T1	238.63	2.3	0.0294	0.02219	0.0128									
		1.5	0.0294	0.01447	0									

### Step V : Calculation of All Day Efficiency (Summer)

Duration (hrs)	06-10	10-14	14-18	18-20	20-22	22-02	02-06
Total load demand (kw)	150.99	107.85	107.85	313.55	323.55	107.85	107.85
Loop demand x hrs (kwh)	603.96	431.40	431.4	1294.20	647.10	431.40	431.4
kVA load demand	710.54	507.53	507.53	1522.59	761.29	507.53	507.53
Fractional loading (X)	1.42	1.02	1.02	3.05	1.52	1.02	1.02
Cu loss (kw)	50.49	25.76	25.76	231.83	57.96	25.76	25.76
Cu loss (kwh)	201.95	103.03	103.03	927.31	115.91	103.03	103.03

Total output (kwh) → 4270.86

Total Cu loss (kwh) → 1657.31

All day efficiency of Transformer ( $T_1$ ) = 72.04%.

### Calculation of All Day Efficiency (Winter)

Duration (hrs)	06-10	10-14	14-18	18-20	20-22	22-02	02-06
Total load demand (kw)	107.85	64.71	64.71	301.98	215.7	43.14	43.14
Loop demand x hrs (kwh)	431.40	258.84	258.84	1207.92	431.4	172.56	172.56
kVA load demand	507.53	304.52	304.52	1421.08	507.53	203.01	203.01
Fractional loading (X)	1.02	0.61	0.61	2.84	1.02	0.41	0.41
Cu loss (kw)	25.76	9.27	9.27	201.95	25.76	4.12	4.12
Cu loss (kwh)	103.03	37.09	37.09	807.79	51.52	16.49	16.49
Total output (kwh)	→ 2933.52						
Total Cu loss (kwh)	→ 1069.50						

All Day Efficiency of Transformer ( $T_1$ ) → 73.28%

M Str	3 Str	2 Str							Domestic Load (KW)	Street Light Load (KW)	Public Load (KW)	Commercial Load (KW)	Industrial Load (KW)	
3	1		46.4	LOOP =	3,336.50	3,355.00	6,691.50	6,833.50	L-A=O	50				
3	1		46.4		1670	850		(164.90)	L-A=O	50				
		15	77.4		50	3			L-A=O	77.4				
4	15	108.2			159.8	129			L-A=O	108.2			50	
4	8	16	195.8		50	154			L-A=O	195.8			100	
5	15	115.9			157.3	115.9			L-A=O	115.9			150	
10	14	149.2			50	150			L-A=O	149.2				
		20	154.0		229.2	149.2			L-A=O	154				
10			129.0		10	196.8			L-A=O	193				
	2	14	87.6		40	100			L-A=O				3	
5	10	90.1			5	108.2			L-A=O	87.6	850	30		
	10	51.6			201.2	50			L-A=O	90.1			15	
	10	51.6			26	77.4			L-A=O	51.6			5	
		10	51.6		118.3	50			L-A=O				30	
		16	82.6		10	50			L-A=O	51.6				
		10	51.6		3	15			L-A=O				15	
4		30.8			75	90.1			L-A=O	51.6			40	
5	10	90.1			50	30			L-A=O	82.6				
	10	51.6			50	40			L-A=O	51.6				
	15	77.4			10	82.6			L-A=O				4	
5	15	115.9			164.7	30			L-A=O	30.8				
2	10	67.0			67	90.1			L-A=O				30	
10	17	164.7			40	40			L-A=O	90.1				
3	1	46.4			100	77.4			L-A=O				30	
	2	8	56.7			10			L-A=O	51.6				
5	10	17	229.2			115.9			L-A=O	77.4			40	
	8		61.6			50			L-A=O	40			10	
5	2	15	157.3			40			L-A=O	115.9				
3	5	16	159.8			51.6			L-A=O	15				
14		4	201.2			30			L-A=O					
	10	8	118.3			51.6			L-A=O		78.2			
50	120	300	3117.0			4			<b>3461.2</b>	1981	78.2	954	148	300
						30.8			L-B=*		63.4			
						51.6			L-B=*				1670	
						15			L-B=*				50	
						51.6			L-B=*	159.8				
						5			L-B=*	61.8			50	
						51.6			L-B=*	157.3				
						30			L-B=*				50	
						87.6			L-B=*	229.2				
									L-B=*				5	
									L-B=*				40	
									L-B=*				10	
									L-B=*	201.2				
									L-B=*					75
									L-B=*					
									L-B=*					
									L-B=*	118.3				
									L-B=*	26				
									L-B=*	50				3
									L-B=*	164.7				
									L-B=*	67				40
									<b>3461.7</b>	1285.3	63.4	1770	168	175