

# Numerical Study of Microstructural Evolution of IN625 During Pulsed Laser Welding

Paper ID: ICAM-2026-1234

Rakibul Islam Kanak<sup>1</sup>    Badhon Kumar<sup>1</sup>

<sup>1</sup>Department of Mechanical Engineering  
Bangladesh University of Engineering and Technology

15th International Conference on Mechanical Engineering (ICME) 2025  
December 17-18, 2025  
BUET, Dhaka, Bangladesh



# Outline

**1** Introduction

**2** Methodology

**3** Model Validation

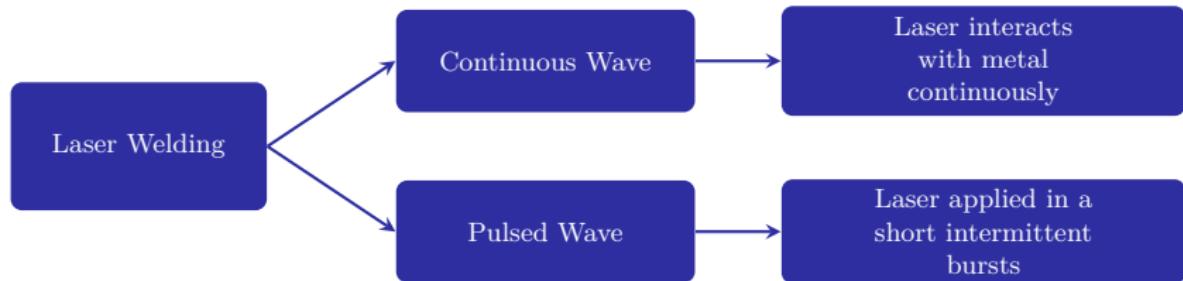
**4** Results

**5** Conclusion

# Introduction

## Laser Welding

One of the most preferred welding techniques due to excellent precision and high energy density – produces excellent quality joints.



# Our work

## Why Pulsed Laser welding

It enables finer control of heat input and melt-pool dynamics – thus controlling the cooling rate and grain growth.

## Why Nickel Based Alloy

They have excellent properties like low density yet high toughness, bio-compatibility, and excellent resistance to creep, corrosion, and high temperatures

## Our Work

This work utilizes a **Cellular Automata (CA)** based microstructural simulation to establish *predictive process-structure relationships*, directly informing the optimization of weld quality in the alloy **Inconel 625**.

# Mathematical modeling

## Thermo-fluid Transport Equation

$$\begin{aligned}\nabla \cdot (\mathbf{u}) &= 0 \\ \rho \left[ \frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u} \mathbf{u}) \right] &= \nabla \cdot (\mu \nabla \mathbf{u}) - \nabla p + \rho \beta (T - T_0) \mathbf{g} - \mu \frac{180}{\lambda^2} \frac{f_s^2}{(1 - f_s)^3} \mathbf{u} \\ \rho c_p \left[ \frac{\partial T}{\partial t} + \nabla \cdot (\mathbf{u} T) \right] &= \nabla \cdot (k \nabla T) + \rho L_f \frac{\partial f_s}{\partial t} + Q\end{aligned}$$

## Gaussian Heat Source

$$Q(x, y, z) = \frac{2\eta P}{r_{xy}^2 d \pi^{3/2}} \exp \left( - \left( \frac{2(x - x_0)^2}{r_{xy}^2} + \frac{2(y - y_0)^2}{r_{xy}^2} + \frac{2(z - z_0)^2}{d^2} \right) \right)$$

## Heterogeneous Nucleation

$$f(\Delta T) = \frac{1}{\Delta T_\sigma \sqrt{2\pi}} \exp \left( -\frac{1}{2} \left( \frac{\Delta T_\mu - \Delta T}{\Delta T_\sigma} \right)^2 \right)$$

# Model Validation

The numerical model was validated using experimental data from the *NIST Additive Manufacturing Benchmark 2018 Challenge* across 3 distinct welding conditions:

Case	Power (W)	Speed (mm/s)
A	137.9	400
B	179.2	800
C	179.2	1200

## Validation Metrics

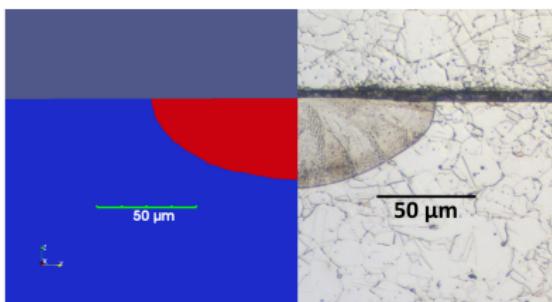
- Melt pool geometry
- Cooling rates
- Microstructure predictions

**Table:** Welding Process Parameters

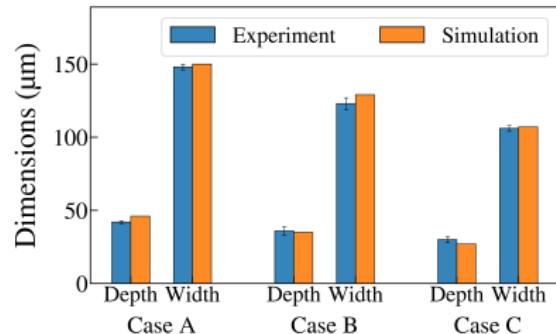
\* *NIST AM Bench* is an international benchmark series for validating computational models against standardized additive manufacturing experiments.

# Thermo-Fluid Validation

The thermo-fluid model was validated by comparing predicted melt pool dimensions (depth and width) against experimental measurements through qualitative and quantitative analysis.

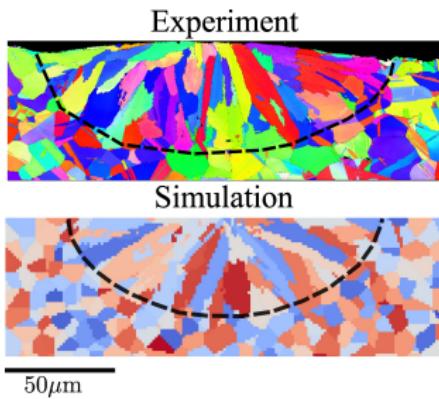


(a) Qualitative comparison of melt pool morphology for case B

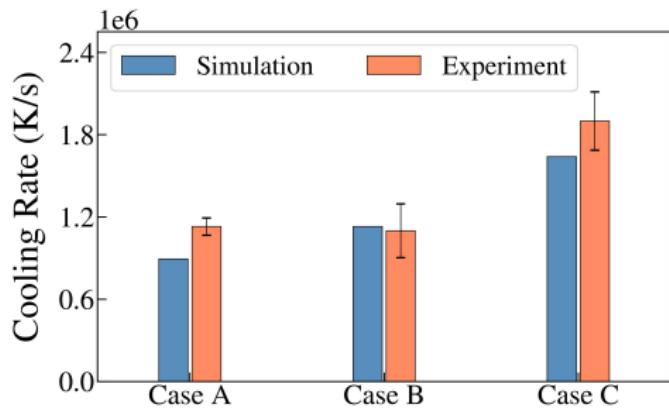


(b) Quantitative validation of melt pool dimensions for all 3 cases

# Microstructure Validation



(a) Qualitative comparison of grain structure (Case B)



(b) Quantitative validation of grain dimensions

# Pulse Laser Setup

- Four pulsed welding cases: 2, 8, 20, and 50 kHz
- AMMT Case B parameters with 0.5 duty cycle
- Peak power doubled to maintain equivalent average power

# Results

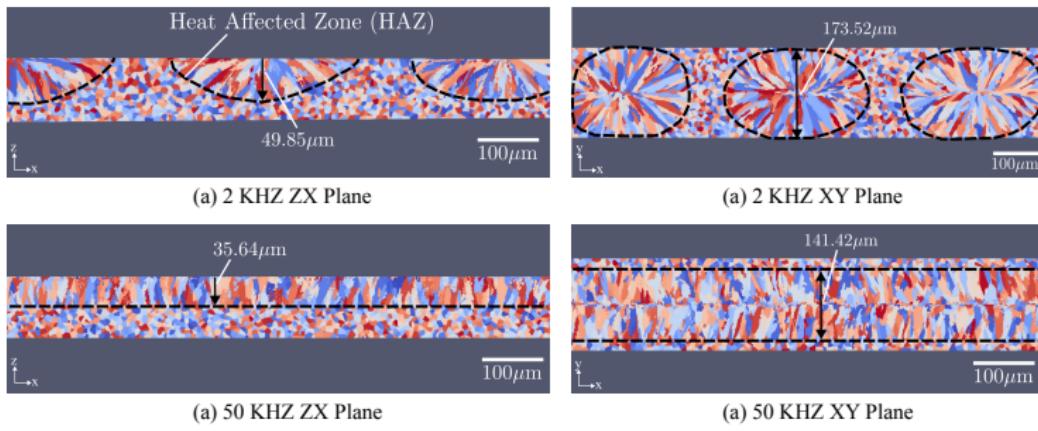


Figure: Caption

# Results

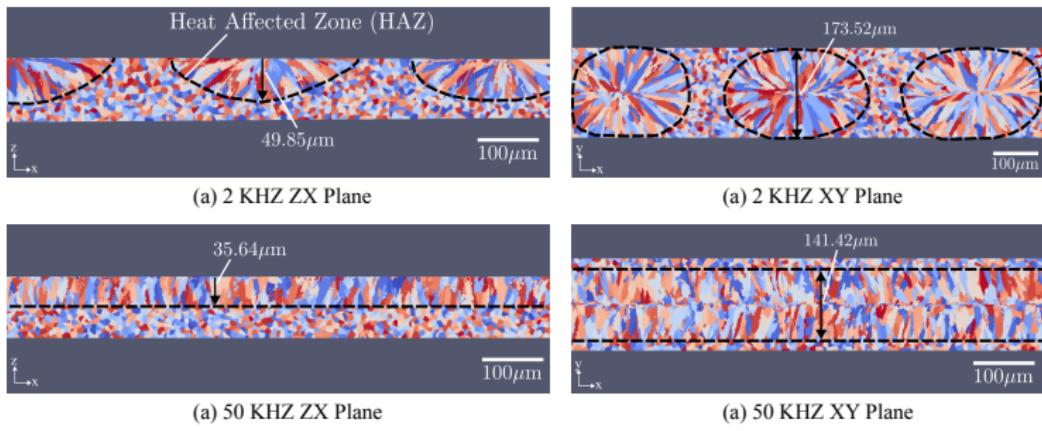


Figure: Caption

# Conclusion