# ENPM 808M: Homework #3

Due on Wednesday, October 14, 2015

 $Dr.\ William\ Levine\ 4:00\ PM$ 

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By definition, skew matrices have the following property:

$$S + S^T = 0 (1)$$

We have

$$e^A = I + A + \frac{1}{2}A^2 + \frac{1}{3!}A^3 + \dots$$
 (2)

$$\implies e^S = I + S + \frac{1}{2}S^2 + \frac{1}{3!}S^3 + \dots$$
 (3)

$$\implies (e^S)^T = \left(I + S + \frac{1}{2}S^2 + \frac{1}{3!}S^3 + \dots\right)^T \tag{4}$$

$$\implies (e^S)^T = e^{S^T} \tag{5}$$

Now, given  $S \in so(3)$ , we get from above

$$(e^S)^T = e^{S^T} (6)$$

Thus, we have

$$e^S \times e^{S^T} = e^{S + S^T} = e^0 = I$$
 (7)

Now, let  $e^S = R$  which gives us

$$RR^T = I (8)$$

which is possible only when sum of the squares of each row = 1, which is a property of  $R \in SO(3)$ . This however gives us two possible determinant values for R, namely +1 or -1.

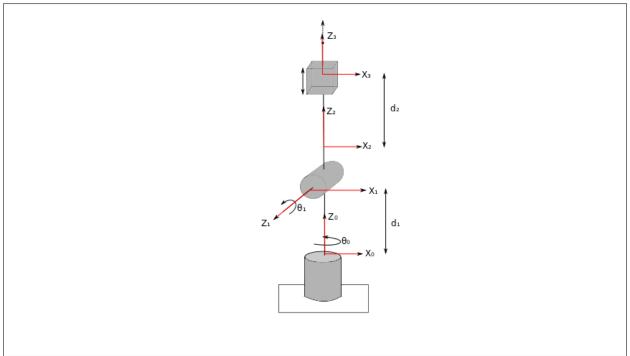
We also have

$$det(e^S) = e^{Tr(S)} = e^0 = 1 (9)$$

Thus, both conditions for  $R \in SO(3)$  are met, namely

- 1.  $RR^T = 1$
- 2. det(R) = 1

Thus,  $R = e^S \in SO(3)$ .



Choice of Axes - DH Convention

From given figure, we form DH Parameters as:

Link (i)	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	90	$d_1$	$\theta_1$
2	0	90	0	$\theta_2$
3	0	0	$\mathbf{d_2}$	0

where **bold** indicates a variable parameter value.

We now have the following transformation matrices:

$$T_1 = \begin{bmatrix} c_1 & 0 & s_1 & 0 \\ s_1 & 0 & -c_1 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
 (10)

$$T_{1} = \begin{bmatrix} c_{1} & 0 & s_{1} & 0 \\ s_{1} & 0 & -c_{1} & 0 \\ 0 & 1 & 0 & d_{1} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{2} = \begin{bmatrix} c_{2} & 0 & -s_{2} & 0 \\ s_{2} & 0 & c_{2} & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$(10)$$

$$T_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \tag{12}$$

Taking products, we get:

$$T_1 T_2 = \begin{bmatrix} c_1 c_2 & -s_1 & -s_2 c_1 & 0 \\ s_1 c_2 & c_1 & -s_2 s_1 & 0 \\ s_2 & 0 & c_2 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
 (13)

$$T_1 T_2 T_3 = \begin{bmatrix} c_1 c_2 & -s_1 & -s_2 c_1 & -s_2 c_1 d_2 \\ s_1 c_2 & c_1 & -s_2 s_1 & -s_2 s_1 d_2 \\ s_2 & 0 & c_2 & c_2 d_2 + d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$(14)$$

From above matrices, we get:

$$O_0 = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}^T \tag{15}$$

$$O_1 = \begin{bmatrix} 0 & 0 & d_1 \end{bmatrix}^T \tag{16}$$

$$O_2 = \begin{bmatrix} 0 & 0 & d_1 \end{bmatrix}^T \tag{17}$$

$$O_3 = \begin{bmatrix} -s_2 c_1 d_2 & -s_2 s_1 d_2 & c_2 d_2 + d_1 \end{bmatrix}^T$$
(18)

Also, we have:

$$Z_0 = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}^T \tag{19}$$

$$Z_1 = \begin{bmatrix} s_1 & -c_1 & 0 \end{bmatrix}^T \tag{20}$$

$$Z_2 = \begin{bmatrix} -s_2 c_1 & -s_2 s_1 & c_2 \end{bmatrix}^T \tag{21}$$

$$Z_3 = \begin{bmatrix} -s_2c_1 & -s_2s_1 & c_2 \end{bmatrix}^T \tag{22}$$

From the figure, we have revolute joints at joints 1 and 2 and joint 3 as prismatic joint. This gives us:

$$J_1 = \begin{bmatrix} Z_0 \times (O_3 - O_0) \\ Z_0 \end{bmatrix} \tag{23}$$

$$J_2 = \begin{bmatrix} Z_1 \times (O_3 - O_1) \\ Z_1 \end{bmatrix} \tag{24}$$

$$J_3 = \begin{bmatrix} Z_2 \\ 0 \end{bmatrix} \tag{25}$$

$$J = \begin{bmatrix} J_1 & J_2 & J_3 \end{bmatrix} \tag{26}$$

We need to calculate  $J_{11}$ , which is the upper half of the matrix J. Thus,

$$J_{11} = \begin{bmatrix} Z_0 \times (O_3 - O_0) & \underline{Z_1 \times (O_3 - O_1)} & Z_2 \end{bmatrix}$$
 (27)

For  $Z_0 \times (O_3 - O_0)$ , we have

$$(O_3 - O_0) = \begin{bmatrix} -s_2 c_1 d_2 \\ -s_2 s_1 d_2 \\ c_2 d_2 + d_1 \end{bmatrix}$$
(28)

$$Z_0 \times (O_3 - O_0) = S(Z_0)(O_3 - O_0)$$
(29)

$$= \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \times \begin{bmatrix} -s_2 c_1 d_2 \\ -s_2 s_1 d_2 \\ c_2 d_2 + d_1 \end{bmatrix}$$
(30)

$$\implies \begin{bmatrix} s_2 s_1 d_2 \\ -s_2 c_1 d_2 \\ 0 \end{bmatrix} \tag{31}$$

For  $\underline{Z_1 \times (O_3 - O_1)}$ , we have

$$(O_3 - O_1) = \begin{bmatrix} -s_2 c_1 d_2 \\ -s_2 s_1 d_2 \\ c_2 d_2 \end{bmatrix}$$
(32)

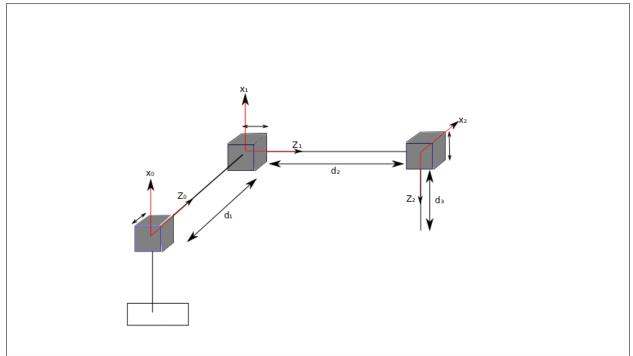
$$Z_1 \times (O_3 - O_1) = S(Z_1)(O_3 - O_1) \tag{33}$$

$$= \begin{bmatrix} 0 & 0 & -c_1 \\ 0 & 0 & -s_1 \\ c_1 & s_1 & 0 \end{bmatrix} \times \begin{bmatrix} -s_2 c_1 d_2 \\ -s_2 s_1 d_2 \\ c_2 d_2 \end{bmatrix}$$
(34)

$$\implies \begin{bmatrix} -c_1c_2d_2 \\ -s1c_2d_2 \\ -s_2d_2 \end{bmatrix} \tag{35}$$

Combining results above, we get

$$J_{11} = \begin{bmatrix} s_2 s_1 d_2 & -c_1 c_2 d_2 & -s_2 c_1 \\ -s_2 c_1 d_2 & -s_1 c_2 d_2 & -s_2 s_1 \\ 0 & -s_2 d_2 & c_2 \end{bmatrix}$$
(36)



Choice of Axes - DH Convention

From given figure, we form DH Parameters as:

Link (i)	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	-90	$d_1$	0
2	0	-90	$\mathbf{d_2}$	90
3	0	0	$d_3$	0

where **bold** indicates a variable parameter value.

We now have the following transformation matrices:

$$T_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
 (37)

$$T_2 = \begin{bmatrix} 0 & 0 & -1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & -1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
 (38)

$$T_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
 (39)

Taking products, we get:

$$T_1 T_2 = \begin{bmatrix} 0 & 0 & -1 & 0 \\ 0 & -1 & 0 & d_2 \\ -1 & 0 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
 (40)

$$T_1 T_2 = \begin{bmatrix} 0 & 0 & -1 & 0 \\ 0 & -1 & 0 & d_2 \\ -1 & 0 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_1 T_2 T_3 = \begin{bmatrix} 0 & 0 & -1 & d_3 \\ 0 & -1 & 0 & d_2 \\ -1 & 0 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$(40)$$

For a prismatic joint, we have

$$J_i = \begin{bmatrix} Z_{i-1} \\ 0 \end{bmatrix} \tag{42}$$

$$J = \begin{bmatrix} J_1 & J_2 & J_3 & \dots \end{bmatrix} \tag{43}$$

We thus have:

$$Z_0 = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}^T \tag{44}$$

$$Z_1 = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix}^T \tag{45}$$

$$Z_2 = \begin{bmatrix} -1 & 0 & 0 \end{bmatrix}^T \tag{46}$$

$$\therefore J = \begin{bmatrix} Z_0 & Z_1 & Z_2 \\ 0 & 0 & 0 \end{bmatrix} \tag{47}$$

We can see that J is a  $6 \times 3$  matrix. So, the maximum rank possible is 3. Since, the actual rank of J is the maximum possible rank, we can say that there are no singular configurations.

From Equation 4.87 in the textbook, we have the following:

$$B(\alpha) = \begin{bmatrix} c_{\phi}s_{\theta} & -s_{\phi} & 0\\ s_{\phi}s_{\theta} & c_{\phi} & 0\\ c_{\theta} & 0 & 1 \end{bmatrix}$$

$$(49)$$

Taking the determinant of  $B(\alpha)$  we get

$$det(B(\alpha)) = (c_{\phi}s_{\theta})(c_{\phi})(1) + (-s_{\phi})(0)(c_{\theta}) + (0)(s_{\phi}s_{\theta})(0) - (0)(c_{\phi})(c_{\theta}) - (-s_{\phi})(s_{\phi}s_{\theta})(1) - (c_{\phi}s_{\theta})(0)(0)$$

$$(50)$$

$$\Rightarrow det(B(\alpha)) = (c_{\phi}s_{\theta})(c_{\phi}) - (-s_{\phi})(s_{\phi}s_{\theta})$$

$$(51)$$

$$\Rightarrow det(B(\alpha)) = c_{\phi}^{2}s_{\theta} + s_{\phi}^{2}s_{\theta}$$

$$(52)$$

$$\Rightarrow det(B(\alpha)) = s_{\theta}$$

$$(53)$$

Now, given that  $s_{\theta} \neq 0$ ,  $det(B(\alpha)) = k$  where k is some non-zero value. Thus  $B(\alpha)$  is invertible if  $s_{\theta} \neq 0$