



A single-ion focused 393nm laser for photon generation and qubit control

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Abstract

I swear I did something

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Chapter 1

Introduction

Quantum computing has been a rapidly increasing field of interest, which is probably due to the fact that it represents the next step in technology advancement. Classical computers are limited in solving some particular problems that scale exponentially, and therefore a new approach is needed. Quantum computing can exploit particular features of quantum mechanics that have no classical counterparts, this allows for a speed up for a certain class of problems such as factorizing numbers [1], or searching in a database [2]. Moreover, simulating nature at its quantum level is a hard task for classical computer, while quantum computers are naturally prone to simulate quantum dynamics.

A set of criteria exists to assess the viability of a realistic implementation of a quantum computer [3], several platforms have been proposed and implemented trying to satisfy these criteria. Ion trapping has already fulfilled all criteria experimentally and it shows great potential for a possible large scale quantum computer. The idea is simple, qubits are encoded in the electronic state of single trapped ion in a Paul trap. Manipulation can be done with laser pulses and by placing a cavity, an ion trap gains network abilities.

However, still a lot of challenges needs to be addressed for a quantum computer to outperform a classical one. Due to the incredible delicate nature of qubits, they are subject to decoherence which harms the successfullness and computational power of quantum computers. Therefore, scaling the number of qubit has been proven to be a difficult engineeristic challenge. Several solutions are possible: the number of qubits can scale; the dimension of qubits can decrease; or qubits can be linked together. The last solution is the approach at the base of quantum networks. The idea is to link several quantum computers to create a cluster of nodes that can work jointly. The task of building a quantum network is not trivial, there are fundamental differences with a classical link. Although the medium can be the same, such as optical fiber, a quantum network must have additional abilities, such as distributing entanglement, or transmitting quantum states. In addition to scaling quantum computers, quantum networks allow for more secure transmission of information [4], and improve some measurements [5].

It is in this context that this thesis arises. Currently there is an ongoing project of building a three node quantum network between two buildings on the campus of the University of Innsbruck. The third node is located in IQOQI, where the thesis took place. Here an ion trap is used as node of the network and it is connected to the other traps via a 400m fiber link. A 393nm lasers is responsible for the generation of the transmitted photons via a cavity enhanced Raman process [6]. At the time of this thesis' start, the 393nm laser was shining on every ion in the trap. In this case, if an ion string were to

be loaded, the light would couple to every ions and there would be no control over the single ion-photon pair. An addressing setup enables the generation of single photons from individual ions which opens up several possibilities in computer-network interfacing: multi-ion-multi-photon states can be generated, qubits can be used for different purposes, network bandwidth can be improved.

To overcome this limitation, an optical setup for the 393nm laser had to be built with the purpose of focusing the light to a single ion in a string. Moreover the setup should have the ability to steer the beam on a fast scale $\sim \mu\text{s}$ and focus it on a different ion. The goal of this thesis was to design and build such a system. The setup is per se not complex, but the design is critical, ions separation is typical in the order of μm , which means the light should be focused down to $1 - 2 \mu\text{m}$, at the limits of the optical elements involved. The steering part is achieved with an acousto-optical deflector (AOD), such device deflects the laser light on microsecond timescales proportionally to the applied input frequency allowing to control remotely the beam pointing of the system.

(To improve) Once completed, the system will allow to manipulate single ions in a string. The same laser can manipulate ions in two different ways: we already mentioned the most important: the triggering of the photon's generation; but, by driving in the laser in a different regime, it is also possible to implement a single qubit gate. This is used to implement quantum operations that are the base for some experiments. For instance, the characterization and beam shape probing experiment performed in this thesis is built on top of such quantum operation.

This work is presented in the following way: Chapter 2 is devoted to the theoretical background necessary to understand the rest of the work. Here the foundations of quantum computing and networking are laid down, along with the basic concepts of ion trapping, and Gaussian beams; Chapter 3 presents the existing experimental setup, i.e. the already built and working blocks of the experiment where the setup designed in this thesis has been added; Chapter 4 is the core of the thesis, here the final design made with the software Zemax and simulations of different aspects of the project are introduced and presented; Chapter 5 contains all the experimental results obtained. It is divided in two parts: First, the setup was built on a spare optical table, here we had the freedom to test different key properties of the performance of the system and decide whether or not it was satisfactory. After having the certainty that the system will work, the setup was transferred and aligned on the main experiment where limited access did not allow for easy performance testing. Here, different and more advanced experimental quantum optics methods had to be used to check if the system was working properly. The description and discussion of these results are in the second part of chapter 5. Lastly, in chapter 6 a conclusion with a summery and a future outlook is given.

Chapter 2

Theoretical framework

Quantum computing is based on a general framework that does not depend on the physical platform. Here, important concepts such as qubit, and quantum operations are described from a theoretical point of view, before showing how we can realize them with trapped ions. The same goes with quantum networking, the concept and the realization can be treated separately and they will be described in this chapter. Furthermore, in this chapter we will take a look into Gaussian beams and their properties. Since that is the shape emitted by laser, it is important to understand their characteristic and how to manipulate them. Lastly, Acousto-optical interactions are introduced and studied to give an idea of how AODs work and how they can be used to steer a laser beam.

2.1 Quantum logic with trapped ions

2.1.1 Quantum computer and quantum gates

The concepts of quantum computing are borrowed and extended from classical computational theory. In the classical case, information is mostly represented in terms of binary digits, the so called bit, essentially mapping information to a base-2 number. Information processing is done with gates acting on those numbers. The idea of quantum computer is still to encode information in a binary form, but due to the nature of quantum mechanics, a quantum bit (in short qubit) gains new features that can be exploited to perform different kind of operations.

A qubit is formally a normalized wave function that can be written as superposition of two orthogonal states indicated usually with $|0\rangle$ and $|1\rangle$:

$$|\psi\rangle = \alpha|0\rangle + \beta|1\rangle, \quad (2.1.1)$$

where α, β are probability amplitudes, two complex numbers that satisfy the relationship $|\alpha|^2 + |\beta|^2 = 1$. At first glance, the advantage of qubits seems obvious, while one classical bit can store only one bit of information, a qubit can be in any linear combination, i.e. α and β can be chosen freely and any information can be represented. Although, the reality is different, due to rules of quantum mechanics, α and β cannot be directly accessed, which means that we can get only a limited amount of information out of a qubit. The outcome of measuring a qubit will give the value 0 with a probability of $|\alpha|^2$ and 1 with a

probability of $|\beta^2|$.

Qubits also have a geometrical representation that can be useful, equation (2.1.1) depends on 4 real numbers, however since ψ is normalized, we can rewrite the expression as

$$|\psi\rangle = e^{i\gamma} \left(\cos \frac{\theta}{2} |0\rangle + e^{i\varphi} \sin \frac{\theta}{2} |1\rangle \right). \quad (2.1.2)$$

the global phase factor $e^{i\gamma}$ can be left out, as it does not influence the measurement outcome. This leaves us with only two real number: θ and φ . A qubit is therefore representable with only these two numbers that we can chose to represent geometrically with normalized spherical coordinates. The so called Bloch sphere is depicted in figure 2.1.1, every point on its surface represents a different state of the qubit. Here qubit manipulation can be visualized as trajectories on the surface. The drawback of this representation is that it is limited to only one qubit, so it loses usefulness when dealing with multiple qubits.



Figure 2.1.1: The Bloch sphere. The states $|0\rangle$ and $|1\rangle$ are at the poles of the sphere, every other point of the surface represents a superpositions of these states. A quantum gate can be seen as trajectory on the surface mapping one state to another.

An alternative way of dealing with qubits is via matrices. We can assign to the states $|0\rangle$ and $|1\rangle$ the following:

$$|0\rangle = \begin{pmatrix} 1 \\ 0 \end{pmatrix} \quad |1\rangle = \begin{pmatrix} 0 \\ 1 \end{pmatrix} \implies |\psi\rangle = \begin{pmatrix} \alpha \\ \beta \end{pmatrix}. \quad (2.1.3)$$

In this representation, rotations of qubits are calculated using 2×2 unitary matrices. These kind of operations are named *quantum gates* and they are the building blocks of quantum computing. Quantum algorithm can be written as a sequence of quantum gates and it is therefore important to understand them. For a single qubit any gate can be written as combination of two operations [7]

$$U_z(\theta) = \begin{pmatrix} e^{-i\frac{\theta}{2}} & 0 \\ 0 & e^{i\frac{\theta}{2}} \end{pmatrix} \quad U_\varphi(\theta) = \begin{pmatrix} \cos \frac{\theta}{2} & -ie^{-i\varphi} \sin \frac{\theta}{2} \\ -ie^{i\theta} \sin \frac{\theta}{2} & \cos \frac{\theta}{2} \end{pmatrix}. \quad (2.1.4)$$

These two matrices can be seen as two different rotations in the Bloch sphere, U_z is a rotation around the z axis by the amount θ , while U_φ is a rotation on the $x - y$ plane around an axis tilted by φ . Important examples are the Hadamard gate H , which creates a superposition of one qubit starting from the state $|0\rangle$, or $|1\rangle$, and the phase shift gate R_ϕ that shift the phase:

$$H = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 & 1 \\ 1 & -1 \end{pmatrix} \quad R_\phi = \begin{pmatrix} 1 & 0 \\ 0 & e^{i\phi} \end{pmatrix}. \quad (2.1.5)$$

As we have seen, a single qubit has already the advantage of superposition compared to classical case. When considering multiple qubits, we gain even more quantum mechanical features like entanglement. This phenomenon does not have a classical analogy and it is an extremely useful tools in quantum information.

In general a state with N qubits is written as tensor product of the single qubit states ψ_i

$$|\psi_N\rangle = |\psi_1\rangle \otimes |\psi_2\rangle \otimes \cdots \otimes |\psi_N\rangle \equiv |\psi_1\psi_2 \dots \psi_N\rangle. \quad (2.1.6)$$

If we had to write out explicitly all the probability coefficients of ψ_N , we would need 2^N complex numbers. It is clear then why classical computer cannot keep up. N bits can only give N^2 different combinations, while the Hilbert space of qubits is exponentially larger. Now, let us consider only 2 qubits, a particular case would be

$$|\psi\rangle = \frac{1}{\sqrt{2}} (|00\rangle + |11\rangle). \quad (2.1.7)$$

If a measurement is made on one of the two qubit and, for instance, the outcome is 0, the wave function collapses to the state $|00\rangle$, collapsing also the state of the other qubit, even if no operation has been directly performed on it. Next you measure the the second qubit and the outcome will be 0 with unit probability. Viceversa, if the outcome if the first measurement was 1, the state collapses to $|11\rangle$ and the outcome of the second measurement is always 1. The two qubits are correlated, but this correlations is stronger than the classical one.

Gates that involve multiple qubits are written as $2^N \times 2^N$ unitary matrices, a famous example is the controlled not (CNOT) gate

$$\text{CNOT} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \end{pmatrix}. \quad (2.1.8)$$

It can be shown [8] that the examples of this section: H gate, phase gate, and CNOT gate form a universal set of quantum gates, i.e. a sequence of these gates approximates every other quantum gate.

2.1.2 Ion qubits and laser-ion interactions

Qubits can be encoded in any pair of orthogonal states. In the case of an ion it is possible to take two internal electronic states. The choices are multiple: an optical qubit is implemented in an optical transition, an hyperfine qubit is between two hyperfine states,

and a Zeeman qubit can be realized with two magnetically separated levels. We will take the choice of an optical qubit, in this case lasers provide an easy way to manipulate the population of the two level and therefore to manipulate the state of the qubit, implementing quantum gates in an almost straightforward way. As long as the chosen levels are well separated, and the light is near resonant to the transition, it is possible to describe the system with the basic 2-level atom scheme interacting with classical light. This assumption can be explained as follow, the wavelength of transitions in an atom, are typically in the optical regime: hundreds of nanometers, which is order of magnitude greater than the typical atom dimension. Thus, the electric field can be considered constant over the atom size. This allows to expand the electric field in Taylor series and remove every spatial dependent term in the so called dipole approximation.

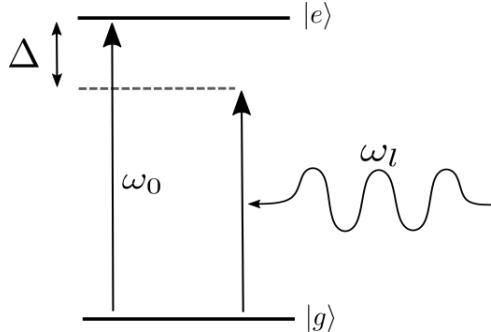


Figure 2.1.2: 2-level atom scheme, the ground and excited states are denoted as $|g\rangle$, and $|e\rangle$. ω_l is the laser frequency, which is detuned by $\Delta \equiv \omega - \omega_0$ from the transition frequency ω_0 .

Consider the system in figure 2.1.2, the Hamiltonian of the atomic part can be written as:

$$H_a = \hbar\omega_0 |e\rangle \langle e|, \quad (2.1.9)$$

where ω_0 is the frequency difference between the ground and excited state, the energy of the ground state has also been set to 0. The Hamiltonian of the interaction between light and atom can be written as [9]

$$H_{int} = -d \cdot E \quad (2.1.10)$$

where the electric field will be treated classically and the dipole approximation is assumed. This means

$$E(t) = \hat{\varepsilon} E_0 \cos(\omega t + \varphi) = \hat{\varepsilon} \frac{E_0}{2} (e^{-i(\omega t + \varphi)} + e^{i(\omega t + \varphi)}), \quad (2.1.11)$$

where ε is a the unit polarization vector. The next step is to work out the dipole operator, this can be done by applying the identity $|g\rangle \langle g| + |e\rangle \langle e|$ on both sides of d . Due to parity arguments [9], only the non diagonal terms are non vanishing, giving

$$d = \langle g|d|e\rangle (|g\rangle \langle e| + |e\rangle \langle g|) \equiv \langle g|d|e\rangle (\sigma + \sigma^\dagger). \quad (2.1.12)$$

Combining the last three equations yields

$$H_{int} = -\langle g|\hat{d}|e\rangle \frac{E_0}{2} (\sigma e^{i(\omega t + \varphi)} + \sigma^\dagger e^{-i(\omega t + \varphi)} + \sigma e^{-i(\omega t + \varphi)} + \sigma^\dagger e^{i(\omega t + \varphi)}) \quad (2.1.13)$$

A rotating wave approximation is used now, essentially σ (σ^\dagger) evolves in time as $\propto e^{-i\omega_0 t}$

($\propto e^{i\omega_0 t}$), therefore we can drop the fast oscillating terms in the last equation and keeping only those that depends on time as $\propto e^{\pm i(\omega - \omega_0)t}$. The validity of this approximation is given by the facts that ω and ω_0 are in the optical regime, thus they oscillate extremely fast and average to zero, the interesting slow dynamic is given only by their difference, aka detuning. With this final approximation we arrive at the final form of the interaction Hamiltonian

$$H_{int} = \frac{\hbar\Omega}{2}(\sigma e^{i(\omega t + \varphi)} + \sigma^\dagger e^{-i(\omega t + \varphi)}), \quad (2.1.14)$$

where we defined the Rabi frequency $\Omega \equiv -\langle g|\hat{e}d|e\rangle E_0/\hbar$. The Rabi frequency depends linearly with the applied electrical field and hence its square is proportional to the intensity of the field $\Omega^2 \propto I$. It also provides a convenient way to describe the coupling strength between the atom and the electric field. To summarize, the final system Hamiltonian is

$$H = H_a + H_{int} = \hbar\omega_0 |e\rangle\langle e| + \frac{\hbar\Omega}{2}(\sigma e^{i(\omega t + \varphi)} + \sigma^\dagger e^{-i(\omega t + \varphi)}). \quad (2.1.15)$$

This Hamiltonian depends explicitly on time, which could lead to unnecessary complications if we want to solve the dynamics. To eliminate the time dependence, we can go in the rotating frame with the unitary transformation $U = e^{i\omega t|e\rangle\langle e|}$, the Hamiltonian in this frame is

$$\tilde{H} = -\hbar\Delta |e\rangle\langle e| + \frac{\hbar\Omega}{2}(e^{i\varphi}\sigma + e^{-i\varphi}\sigma^\dagger) \quad (2.1.16)$$

The time dependence is now gone, and the unitary evolution matrix can be calculated as

$$U(t) = \exp\left\{-\frac{i}{\hbar}\tilde{H}t\right\} = \begin{pmatrix} \cos\left(\frac{\tilde{\Omega}t}{2}\right) + i\frac{\Delta}{\tilde{\Omega}}\sin\left(\frac{\tilde{\Omega}t}{2}\right) & -ie^{i\varphi}\frac{\Omega}{\tilde{\Omega}}\sin\left(\frac{\tilde{\Omega}t}{2}\right) \\ -ie^{-i\varphi}\frac{\Omega}{\tilde{\Omega}}\sin\left(\frac{\tilde{\Omega}t}{2}\right) & \cos\left(\frac{\tilde{\Omega}t}{2}\right) - i\frac{\Delta}{\tilde{\Omega}}\sin\left(\frac{\tilde{\Omega}t}{2}\right) \end{pmatrix}. \quad (2.1.17)$$

Where $\tilde{\Omega} = \sqrt{\Delta^2 + \Omega^2}$ is the generalized Rabi frequency. With this matrix we can calculate all the dynamic we need. In the case of zero detuning $\Delta = 0$, we also notice that the matrix is the same as equation (2.1.4). Thus, a laser pulse can implement such qubit rotation, the other rotation can be performed in the same way, but with a different laser regime. We will explore this possibility later in the AC Stark shift.

As example, let us take the atom in the ground state $|\psi\rangle = |0\rangle$ and apply the unitary evolution (2.1.17). The probability to be in the excited state becomes

$$\mathbb{P}\{|1\rangle\}(t) = |\langle 1|U(t)|0\rangle|^2 = \frac{\Omega^2}{\Omega^2 + \Delta^2} \sin^2\left(\frac{\tilde{\Omega}t}{2}\right) \quad (2.1.18)$$

This equation is plotted in figure 2.1.3. For $\Delta = 0$, we get a cosine behaviour, the so called Rabi oscillations. An electron constantly shined will jump between the two levels at a frequency Ω . Detuning damps the amplitude of such oscillations and increases the oscillation frequency. Rabi oscillations are an important tool in quantum information, by sending laser pulses it is possible to prepare the state in any superposition, e.g. with a $\pi/2$ pulse ($\Omega t = \pi/2$) the resulting state will be $(|0\rangle - i|1\rangle)/\sqrt{2}$, with a π pulse ($(\Omega t = \pi)$) the population is completely transferred to another level $|0\rangle \rightarrow |1\rangle$. These pulses can be used to implement the Hadamard gate of equation (2.1.5).



Figure 2.1.3: Rabi flops for different detuning Δ

Rabi oscillations can be observed with near resonant light, in the off-resonant regime, oscillations are suppressed, but the light shifts the energy levels. The shift δ can be calculated by finding the eigenvalues of the Hamiltonian (2.1.16). It can be easily written in matrix form and diagonalized, we find that there are two eigenstates $|+\rangle$ and $|-\rangle$ called dressed states with eigenvalues

$$E_{\pm} = -\frac{\hbar\Delta}{2} \pm \frac{\hbar}{2}\sqrt{\Delta^2 + \Omega^2}. \quad (2.1.19)$$

In the limit $\Delta \gg \Omega$, dressed states tend to the bare states $|+\rangle \rightarrow |e\rangle, |-\rangle \rightarrow |g\rangle$, and the energies becomes

$$E_{\pm} \rightarrow -\frac{\hbar\Omega}{2} \pm \frac{\hbar\Omega}{2} \pm \frac{\hbar\Omega^2}{4\Delta} \implies \delta = \pm \frac{\Omega^2}{4\Delta}. \quad (2.1.20)$$

The effective Hamiltonian for the off-resonant regime can be derived following a Markovian approximation [10]

$$H_{eff} = \frac{1}{\hbar\Delta} [\sigma, \sigma^\dagger] = \frac{\hbar\delta}{2} \sigma_z \quad (2.1.21)$$

The corresponding evolution is

$$U(t) = \exp \left\{ -\frac{i}{\hbar} H_{eff} t \right\} = \begin{pmatrix} \exp \left\{ i \frac{\delta}{2} t \right\} & 0 \\ 0 & \exp \left\{ i \frac{\delta}{2} t \right\} \end{pmatrix}. \quad (2.1.22)$$

This matrix implements the quantum gate from equation (2.1.4). Furthermore, Ac stark shift can also implement the phase gate (2.1.5), the trick is to shift the energy of a transition the shares only one level with qubit transition. From the prospective of the qubit, only one level is shifted and the other level remains unaltered, thus one of the two matrix element of equation (2.1.22) is 1.

2.2 Quantum networking with trapped ions

2.2.1 General introduction

Quantum networks can serve different purposes, either transmission of quantum information at long distances, or interconnections of quantum processors for qubits scaling. The topology of these configurations changes, but the constituent elements are the same: a node, where quantum information is prepared, manipulated, and stored; and a link that connects node and where information is transmitted. Links are typically realized with optical fibers, photons can carry quantum information over long distance with very high speed. Instead, nodes can be realized in a variety of ways: trapped ions [11], neutral atoms [12], atomic ensembles [13]. Nodes and links are connected through an interface that converts deterministically a stationary qubit in a node to a flying qubit over the network. In the next section we will explore how an interface can be realized by placing an ion based quantum memory in a optical cavity. Here we will examine some properties needed for a quantum network to work.

In the case of quantum information transmission, a fundamental property of quantum network is the ability of transmitting faithfully any state between nodes. For long distances this requires the use of amplifiers or repeaters that boost the signal as it gets attenuated during the transmission. However, due to the no-cloning theorem [14], qubits cannot be copied. A workaround of this problem is to send multiple qubits and purify the entanglement along the transmission with extra qubits and quantum nodes between the endpoints [15].

To create a cluster of quantum nodes, another property of quantum network is necessary: entanglement distribution allows to entangle qubits located in different quantum nodes. A protocol to distributed entanglement can be realized with photon interference on a beam splitter. Consider the case of figure 2.2.1. Two nodes each with a qubit

$$|\psi_A\rangle = a|0\rangle_A + b|1\rangle_A \quad |\psi_B\rangle = c|0\rangle_B + d|1\rangle_B. \quad (2.2.1)$$

With the use of an interface each qubit is entangled to a photon. The photonic qubit can have different implementations, for this protocol however it is not important and we will indicate them as $|H\rangle, |V\rangle$. The states ready for transmission are

$$|\psi_A\rangle = a|0\rangle_A|H\rangle_A + b|1\rangle_A|V\rangle_A \quad |\psi_B\rangle = c|0\rangle_B|H\rangle_B + d|1\rangle_B|V\rangle_B. \quad (2.2.2)$$

The total system is described as the product state of the two subsystem:

$$|\psi_A\rangle \otimes |\psi_B\rangle = (a|0\rangle_A|H\rangle_A + b|1\rangle_A|V\rangle_A) \otimes (c|0\rangle_B|H\rangle_B + d|1\rangle_B|V\rangle_B). \quad (2.2.3)$$

When the photons arrive at the beam splitter there are four possible outcomes and two distinguishable events: either the two detectors click at the same time or only one detector clicks twice. In the second case, one photon was transmitted and the other reflected, the final state is proportional to $|0\rangle_A|1\rangle_B + |1\rangle_A|0\rangle_B$, which in the case of indistinguishable photons is just a product state. More interesting is the case when a coincidence on both detector occurs. The final state is projected into

$$|\psi\rangle = ac|0\rangle_A|0\rangle_B + bd|1\rangle_A|1\rangle_B, \quad (2.2.4)$$

leading to the two qubits to be entangled with each other. This protocol is probabilistic, but the success of entanglement can be heralded after a coincidence measure.

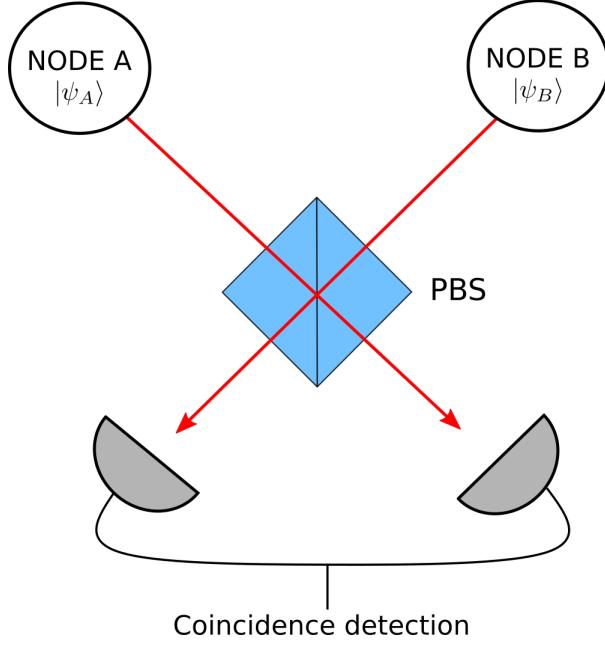


Figure 2.2.1: Remote qubits entanglement protocol.

2.2.2 Cavity QED

Trapped ions can become quantum nodes of a quantum network by placing them in a cavity. Ions emits photon by spontaneous emission, or stimulated emission. The problem with spontaneous emission is that the photonic channel of emission is random and in free space. To realize a quantum interface, photon should be produced almost deterministically in defined mode. The trick is to use a cavity tuned to one particular transition, such that the probability of a photon to be emitted in the cavity mode is greatly enhanced. In this section we describe a simple model of a two-level system in a cavity, the derivation is similar to section 2.1.2, with the difference that in a cavity the electric field is quantized. Using the mode operator a, a^\dagger the electric field inside a cavity can be written as:

$$E = A(f(r)a + f^*(r)a^\dagger) \quad (2.2.5)$$

where A is an amplitude, and $f(r)$ is the spatial mode profile [16]. The interaction between the field and the cavity is obtained as from $H_{int} = -d \cdot E$, following a rotating wave approximation the result is

$$H_{int} = \hbar g(\sigma a^\dagger + \sigma^\dagger a), \quad (2.2.6)$$

where $g = A \langle g|d|e \rangle f(r)$ is called cavity coupling constant. It is analogous to the Rabi frequency, it gives an idea of the coupling between the cavity field and the 2-level atom. An important dependence of g can be found by considering that $f(r)$ is inversely proportional to the volume of the cavity V , i.e.

$$g \propto \langle g|d|e \rangle \sqrt{\frac{\omega}{2\epsilon_0 \hbar V}}. \quad (2.2.7)$$

The coupling therefore, increases with decreasing cavity volume and viceversa. The total system Hamiltonian includes also the atomic part, and a single mode optical field. It takes the name of Jaynes-Cummings Hamiltonian and it is written as [17]

$$H = \hbar\omega_0 |e\rangle\langle e| + \hbar\omega a^\dagger a + \hbar g(\sigma a^\dagger + \sigma^\dagger a). \quad (2.2.8)$$

States now are a product state of the atomic part and the photon number $|g, n\rangle, |e, n\rangle$. They are however not the eigenstates of the Jaynes-Cumming Hamiltonian. It can be seen that this Hamiltonian is block diagonal, which means that each 2×2 block can be diagonalized, the dressed states found after diagonalization are similar to the semiclassical model. Moreover, also the dynamics is analogue to the semiclassical case, Rabi oscillations are still present with quantized Rabi frequency given by $\Omega_n = \sqrt{4(n+1)g^2 + \Delta^2}$. The presence of a cavity makes dynamics more interesting, especially when considering spontaneous emission and interaction with cavity modes. For a mathematical description, we need to introduce dissipative process that do not follow an Hermitian evolution. This is done heuristically by adding terms in the Heisenberg equation

$$\frac{d\rho}{dt} = \frac{1}{i\hbar}[H, \rho] + \mathcal{L}(\rho). \quad (2.2.9)$$

This equation is usually referred to as master equation in Lindblad form, where ρ is the density matrix of system. The superoperator $\mathcal{L}(\rho)$ contains phenomena not included in the Hamiltonian. In our case, we are most interested in two process: spontaneous emission in a free space field mode, and decay in one cavity mode and out of the cavity. The first is quantified with the decay rate Γ , while the latter is characterized by the decay rate κ . The functional dependence of these two terms goes as [9]

$$\mathcal{L}(\rho) = \Gamma\mathcal{D}(\sigma)\rho + \kappa\mathcal{D}(a)\rho. \quad (2.2.10)$$

A good approximation of the model is given in the *strong coupling* regime $g \ll \Gamma, \kappa$, where damping due to dissipative process is slow and dynamics is mainly driven coherently by the coupling atom-cavity g . The decay rate κ depends exclusively on the cavity parameters as [16]

$$\kappa = \frac{c\pi}{FL}, \quad (2.2.11)$$

where F is the cavity finesse, and L the length. In the design of the experiment one must play and compromise with these three parameters in order to reach a good coupling ion-cavity but also being able to send photons out of the cavity.

2.3 Basics of ion trapping

2.3.1 Linear Paul trap

In order to trap a charged atom, a three dimensional trapping potential ϕ is needed. However it follows directly from Maxwell equation $\nabla^2\phi = 0$ that the potential must be antitrapping at least in one direction. There are two workarounds for this problem: the first one introduces magnetic fields to trap particles in some directions, this takes the name of Penning trap. The second solution is the so called Paul trap, and it is what we are going to describe in this section. The idea is to introduce a time varying potential, such

that the antitrapping direction is constantly switching between two different dimension. If the switching is timed correctly, the particle will not have the time to escape but will always encounter a potential barrier. The shape of the trap can be adapted to load more ions in different geometries. For instance, a linear Paul trap is elongated in one direction where the trapping confinement is weaker, such that loaded ions will align in a single long string. This kind of trap is depicted in figure 2.3.1.



Figure 2.3.1: A linear Paul trap. U is the voltage applied to the electrodes trapping in the z direction, while in the $x - y$ plane trapping is achieved with a radio frequency signal. r_0 is the distance from the central axis to the RF electrodes.

The confinement in the $x - y$ plane is provided by 4 electrodes, two of which are grounded and the other two are connected to a radio frequency source. This design is similar to a mass filter, with the difference of additional endcaps electrodes in the z direction that plug the trap and confine also in axial direction.

The potential inside the trap can be described for the $x - y$ plan independently from the z direction. In the case of a linear Paul trap the radial potential is [18]:

$$\phi = \frac{\Phi_0}{2r_0^2} (x^2 - y^2), \quad (2.3.1)$$

with the amplitude that consists of a static part U and a dynamical one $\Phi_0 = U + V \cos(\Omega_{RF}t)$. The study of the particle's motion with mass m and charge e inside the trap can be done with classical physics, Newton's second law in this case is

$$m\ddot{x} = -q \frac{\partial \phi}{\partial x} = -\frac{ex}{r_0^2} (U + V \cos(\Omega_{RF}t)), \quad (2.3.2)$$

and similarly for \ddot{y} . This equation can be written in the form of Mathieu equation by defining two parameters:

$$a_x = \frac{4eU}{\Omega_{RF}^2 r_0^2 m}, \quad q_x = \frac{2eV}{\Omega_{RF}^2 r_0^2 m} \implies \ddot{x} + \frac{\Omega_{RF}}{4} (a_x + 2q_x \cos(\Omega_{RF}t)) x = 0 \quad (2.3.3)$$

and with a change of variable $\tau = \frac{\Omega_{RF}t}{2}$ we end up with

$$\frac{\partial^2 x}{\partial \tau^2} + (a_x + 2q_x \cos(2\tau)) x = 0 \quad (2.3.4)$$

This kind of equations have stable solutions that can be found in a recursive way with Floquet theorem [19]. However, the problem is simplified by performing the so called secular approximation, which consists of separating the motion in a slow changing position:

\bar{x} called *secular motion*, and in a rapid oscillation: ξ , called *micromotion*. The behaviour of micromotion is dictated by the force due to the potential at the position \bar{x} , and the secular motion will follow a time average of the potential $\langle \phi(t) \rangle$ eliminating therefore the effect of micromotion. In this case, equation (2.3.4) can be solved in the limit $a_x \ll q_x \ll 1$

$$x(t) = x_0 \cos(\omega_x t + \phi_x) \left[1 + \frac{q_x}{2} \cos(\Omega_{RF} t) \right]. \quad (2.3.5)$$

Where we recognize a slowly varying oscillation with amplitude modulated by a faster oscillation. The approximation is valid only in the case $\omega_x \ll \Omega_{RF}$. The frequency ω_x is given in the solution as

$$\omega_x = \frac{\Omega_{RF}}{2} \sqrt{a_x + \frac{q_x^2}{2}}. \quad (2.3.6)$$

By imposing real solution, the stability diagram of the trap can be found. It is depicted in figure 2.3.2. The other spatial dimension can be treated in the same way and the results are the same. Important to notice is that a consequence of the secular approximation is that the potential can be approximated, the ion in the trap sees therefore a pseudo potential which is harmonic. Deviations from harmonicity are possible and they are mainly due to stray fields. Extra electrodes can be added to the trap design to compensate for such deviations.



Figure 2.3.2: Stability diagram for a linear Paul trap, taken from [19]. The coefficient β_x, β_y can be calculated numerically from a_x and q_x

2.3.2 Ion strings

We have seen that the potential inside the trap can be described as an harmonic potential. What we are interested in, is the ion separation between N ions loaded in the trap. This will give us an idea of how narrowly the beam should be focused and will set an appropriate problem spatial scale.

Let us consider the z direction where the ions are weakly confined and will form a string. The potential can be approximated as harmonic and hence given by

$$V = \sum_{i=0}^N \frac{1}{2} M \omega^2 z_i^2 + \sum_{i \neq j}^N \frac{Z^2 e^2}{8\pi\epsilon_0} \frac{1}{|z_i - z_j|} \quad (2.3.7)$$

The equilibrium position can be found at the minima of the potential, i.e. where the first derivative zeros

$$\frac{\partial V}{\partial z_i} = 0 \implies u_i - \sum_{j=1}^{i-1} \frac{1}{(u_i - u_j)^2} + \sum_{j=i+1}^N \frac{1}{(u_i - u_j)^2} = 0, \quad (2.3.8)$$

where we defined the dimensionless quantity $u_i = z_i/l$ and $l^3 = \frac{Z^2 e^2}{4\pi\epsilon_0 M \omega^2}$. The last equations can be solved analytically only for 2 or 3 ions. In fact, for the case $N = 2$ we simply get the system

$$\begin{cases} u_1 + \frac{1}{(u_1 - u_2)^2} = 0 \\ u_2 - \frac{1}{(u_1 - u_2)^2} = 0 \end{cases} \implies u_1 = -u_2, \quad u_1 = \left(\frac{1}{2}\right)^{2/3} \simeq 0.629 \quad (2.3.9)$$

For calcium-40 ions in a Paul trap with axial confinement of $\omega = 1$ MHz, we have $l \simeq 4.45 \times 10^{-6}$ m, which means that 2 ions are separated by $\simeq 5.6 \mu\text{m}$. In the case of more ions the separation is lesser with the same confinement, but it is also possible to lower the axial frequency and increase the separation between the ions such that also in the case of several ions, the distance between them is still in the order of several μm . This size is accessible with current focusing optics and it is above the diffraction limit.

For more ions, a numerical approach has to be used, [20] reports values of u_i up to $N = 10$, and gives an empirical formula of the minimum separation

$$u_{min}(N) \simeq \frac{2.018}{N^{0.559}}, \quad (2.3.10)$$

Although, numerical solution are preferred and can be computed fast.

2.3.3 Doppler cooling and detection

Ion trapping was treated here classically, because ions, when trapped, are still hot and follow classical mechanics. In order to reach the quantum regime, they must be cooled down. Several techniques are available for cooling, but the most popular and more frequently used is doppler cooling. The idea comes from neutral atoms and can be applied to ions as well: a laser interacts with a particular transition, exchanging a photon and therefore giving a momentum kick $\Delta p = \hbar \mathbf{k}$ in a particular direction to the ion. The absorbed photon is given back through spontaneous emission in a random direction, giving another kick to the ion. Over many cycles of absorption and emission, the random kick due to emission will average to zero, while the kick given by the laser will accumulate slowing down and cooling the ion in the direction of the laser.

The difference with neutral atoms is that an ion is confined inside a trap rotating at frequency ω . Hence, even the simple 2-level system gains new transitions called sidebands.

Some consideration must be put into the relative strength of the decay rate Γ with respect to the sidebands. For describing the Doppler cooling we assume that the ion is weakly confined $\omega \ll \Omega$. The intuitive picture is that the rate of spontaneous emission in this case is much faster than the time scale over which the trap changes potential. Therefore, the trap can be considered static and has no effect on the cooling.

In order to describe spontaneous emission, we use the master equation (2.2.9), in the case of spontaneous emission, the superoperator is given by [21]

$$\mathcal{L}(\rho) = \frac{\Gamma}{2} (2\sigma\rho\sigma^\dagger - \{\sigma^\dagger\sigma, \rho\}). \quad (2.3.11)$$

Γ is the decay rate from the excited state to the ground state. The actual value is found in perturbation theory with Fermi's golden rule []

$$\Gamma = \frac{\omega_0^3}{3\pi\varepsilon_0\hbar c^3} |\langle e|d|g\rangle|^2 \quad (2.3.12)$$

The master equation (2.2.9) can be explicitly written for every component of the density matrix ρ , in the rotating frame they are called optical equations and they are

$$\frac{d\rho_{ee}}{dt} = -i\frac{\Omega}{2}(\rho_{eg} - \rho_{ge}) - \Gamma\rho_{ee} \quad (2.3.13)$$

$$\frac{d\rho_{gg}}{dt} = i\frac{\Omega}{2}(\rho_{eg} - \rho_{ge}) + \Gamma\rho_{ee} \quad (2.3.14)$$

$$\frac{d\rho_{ge}}{dt} = -\left(\frac{\Gamma}{2} + i\Delta\right)\rho_{ge} - i\frac{\Omega}{2}(\rho_{ee} - \rho_{gg}) \quad (2.3.15)$$

$$\frac{d\rho_{eg}}{dt} = -\left(\frac{\Gamma}{2} - i\Delta\right)\rho_{eg} + i\frac{\Omega}{2}(\rho_{ee} - \rho_{gg}) \quad (2.3.16)$$

The most interesting solution is the population of the excited level ρ_{ee} in the steady state case, i.e. when the system reached equilibrium. In this case we look at $\rho_{ee}(t \rightarrow \infty)$, the solution of equation (2.3.13) is

$$\rho_{ee}(t \rightarrow \infty) = \frac{\Omega^2/\Gamma^2}{1 + \left(2\frac{\Delta-\mathbf{k}\cdot\mathbf{v}}{\Gamma}\right)^2 + 2\frac{\Omega^2}{\Gamma^2}} \quad (2.3.17)$$

The force exerted on the ions, due to the radiative pressure, is proportional to this population as

$$F = \hbar k\Gamma\rho_{ee} \simeq F_0 + \frac{dF}{dv}v = \hbar k\Gamma \frac{\Omega^2}{\Gamma^2 + 4\Delta^2} + F_0 \frac{8k\Delta}{\Gamma^2 + 4\Delta^2}v \quad (2.3.18)$$

where we assumed low velocities $v \simeq 0$ and thus linearized the equation. The effect of the constant term in the force is just to displace the ion from its central position. Instead, the linear term acts as a viscous friction that cools the ions with a rate of $\dot{E}_c = \langle Fv \rangle$. If on one side spontaneous emission allows for Doppler cooling, it also sets the lower limit. The small fluctuations in the Brownian motion leads to diffusion which heats the ion at a rate of

$$\dot{E}_h = \frac{1}{m} \frac{d}{dt} \langle p^2 \rangle = \frac{1}{m} (\hbar k)^2 \Gamma \langle \rho_{ee}(v) \rangle. \quad (2.3.19)$$



Figure 2.3.3: Λ type scheme. Two ground states $|g_1\rangle$ and $|g_2\rangle$ are stable or metastable, while the excited level $|e\rangle$ is short lived. Qubit is encoded in the two ground states while laser fluorescence and laser cooling is done on the $|g_1\rangle \rightarrow |e\rangle$ transition.

At equilibrium, the heating rate equals the cooling rate giving the lowest temperature achievable

$$\dot{E}_h + \dot{E}_c = 0 \implies k_B T = -\frac{\hbar\Gamma}{4} \left(\frac{\Gamma}{2\Delta} + \frac{2\Delta}{\Gamma} \right). \quad (2.3.20)$$

From here it is clear that by choosing the appropriated detuning, it is possible to reach the lowest temperature

$$T_{min} = \frac{\hbar\Gamma}{2k_B}, \quad \text{for } \Delta = -\frac{\Gamma}{2} \quad (2.3.21)$$

The achieved temperatures with Doppler cooling are enough to perform standard measurements. To go further down in temperature, sideband cooling is used, here particular sideband transition are excited to reduce the phonon number of the ions inside the trap.

With the same interaction of Doppler cooling, state detection can also be performed by means of laser induced fluorescence. Consider the Λ scheme in figure 2.3.3, the qubit is encoded in the level $|g_1\rangle$ and $|g_2\rangle$. To distinguish in which state the electron is, the transition $|g_1\rangle \rightarrow |e\rangle$ is excited. In the case the electron is in $|g_1\rangle$, the electron undergoes Rabi flops and scatters photons that can be collected and measured. If the electron is $|g_2\rangle$, no photons will be emitted and therefore no light is collected. The difference between these bright and dark states is clear and detection can be performed efficiently with near perfect efficiency.

In the real case, one must take into consideration also all the other levels. In fact, an electron from the excited state $|e\rangle$ can have multiple decay channels to other states and repumping becomes necessary.

2.4 Laser beam

2.4.1 Gaussian beams

Lasers emit light in the shape of Gaussian beams, so it is import to understand what Gaussian beams are and their characteristics. In this chapter we will take a closer look into such beams and introduce important quantities to characterize a Gaussian beam.



Figure 2.4.1: Normalized Gaussian profile. Different ways of measuring the width of the profile are displayed geometrically.

From a theoretical point of view, Gaussian beams are solution of the Helmholtz equation $(\nabla^2 + k^2)U(r) = 0$, with k being the wavevector. Such equation is a time independent variant of the wave equation that follows directly from Maxwell equations. A paraxial approximation is often used, i.e. we assume that the amplitude $A(r)$ of the wave is slowly varying, this means that the envelope of the wave is approximately constant on a length of λ and we can write the complex electric field as $U(r) = A(r)e^{-ikz}$. If we can consider a wave propagating in the z direction, we can find a solution in the form of [22]:

$$U(r) = A_0 \frac{W_0}{W(z)} \exp \left\{ -\frac{x^2 + y^2}{W^2(z)} \right\} \exp \left\{ -ikz - ik \frac{x^2 + y^2}{2R(z)} + i \arctan(z/z_0) \right\}. \quad (2.4.1)$$

These solutions are called Gaussian beams, they are characterized by an amplitude A , a width $W(z)$, Rayleigh range z_0 , and a curvature radius $R(z)$. Let us take a look at the features that arise from these beams. The optical power can be calculate by taking the square of the complex amplitude

$$I(r) = |U(r)|^2 = I_0 \left(\frac{W_0}{W(z)} \right)^2 \exp \left\{ \frac{2x^2 + 2y^2}{W^2(z)} \right\} \quad I_0 = |A_0|^2. \quad (2.4.2)$$

It is clear from here why the beam is called Gaussian. For a fixed z , the beam shape is the one of a two dimensional beam profile, i.e. the sections in the $x - y$ plane of a Gaussian beams are Gaussian shaped distribution. If we further take a cross section in the $x - y$ plane, we end up with a one dimensional Gaussian distribution. This shape is shown in figure 2.4.1, along with some important parameters. It is important to understand how to characterize the width of a Gaussian shape, as it provides a quantitative way of



Figure 2.4.2: Width profile of a Gaussian beam. The beam is focused at the position z_0 , here it assumes the minimum width W_0 , also referred to as waist.

measuring a laser beam width and its focus spot. A common way to define the width of a Gaussian distribution is according to the standard deviation σ , in this case the shape is given by $Ae^{-\frac{x^2}{2\sigma^2}}$, but for the intensity of a Gaussian beam, $W(z)$ is a much more used value. $W(z)$ is defined as the point at which the irradiance I has fallen to $1/e^2 = 13.5\%$ of its maximum value. The relationship between these two quantities is easily found: $W(z) = 2\sigma$.

Another common parameter to characterize the width of a Gaussian is the full width half maximum (FWHM), this can be found to be related to W as: $W = 0.84 \cdot \text{FWHM}$. All these methods are equivalent and are different only from a prefactor, so for the rest of the section, we can stick to $W(z)$ and study its behaviour. Always from Helmholtz equation [22], the profile of $W(z)$ is found to be

$$W(z) = W_0 \sqrt{1 + \left(\frac{z}{z_0}\right)^2} \quad W_0 = \sqrt{\frac{\lambda z_0}{\pi}}. \quad (2.4.3)$$

This equation is plotted in figure (2.4.2). There are several important features that can be seen. First of all, the width reaches a minimum in $z = 0$ at a value of W_0 , this is called focus of the beam and its width is the waist of the beam. Before and after the focus, the beam profile diverges almost linearly with an angle given by $\theta = W_0/z_0$, which means the smaller the focus, the greater it diverges. This property will become important later in the work, because it provides one limit on the focus spot. In fact, the optical aperture of the trap is limited by the electrodes, and a too diverging beam can potentially clip on one electrode causing aberrations and scattered light in the whole trap. The Rayleigh range z_0 also has a geometrical interpretation, it represents the point where the beam width is exactly $\sqrt{2}W_0$, along with θ this is a useful way to characterize how fast a beam diverges.

In real experiments, all of these beam quantities can be manipulated with a lens. A Gaussian beam can therefore be shaped at will using optical elements. In order to study such reshaping, let us consider a thin spherical lens with focal length f , and radius of curvature R_l placed at position z . The effect of the lens on the beam is to give an extra phase factor to equation (2.4.1) equals to $k(x^2 + y^2)/2f$ [23]. We can match the phase of the incoming and emerging waves

$$kz + k\frac{x^2 + y^2}{2R} - \zeta - k\frac{x^2 + y^2}{2f} = kz + k\frac{x^2 + y^2}{2R'} - \zeta \implies \frac{1}{R'} = \frac{1}{R} - \frac{1}{f}. \quad (2.4.4)$$

The effect of the lens is now clear, it changes the radius of curvature to R' according to the previous equation. Moreover, the width of the beam at the lens is not altered $W = W'$. Using these last two facts, we can determine all the parameters of the outgoing wave. The most important for us is the new waist W'_0

$$W'_0 = MW_0 \quad M = \frac{M_r}{\sqrt{q + r^2}} \quad M_r = \left| \frac{f}{z - f} \right| \quad r = \frac{z_0}{z - f}. \quad (2.4.5)$$

M is the magnification factor which provides an easy way to describe the change of the beam. For a better understanding of this last result, let us consider a less general example. We can place the lens at the focus $z = 0$, and have a collimated beam $z_0 \rightarrow +\infty$. In this case the new waist is

$$W'_0 = \frac{W_0}{\sqrt{1 + (z_0/f)^2}} \simeq W_0 \frac{f}{z_0} = \frac{\lambda f}{\pi W_0} \quad (2.4.6)$$

where the approximation comes from taking $z_0 \gg f$. There are three parameters we can act on to achieve the smallest focus spot. The wavelength λ , the shorter the better. The focal length of the lens f must be as small as possible, and the waist of the incoming beam W_0 as big as possible. Usually the wavelength is fixed in an optical system, so the best way to achieve a small focus is to collimate the beam as large as possible, the limit is given by the diameter D of the lens. Hence, in the best case we have $D = 2W_0$ which means the waist is

$$W_0 = \frac{2\lambda}{\pi} \frac{f}{D}. \quad (2.4.7)$$

A system focused to this limit is said to be diffraction limited. Indeed, if the size of the collimated beam is yet increased, the lens becomes a finite size aperture and diffraction effects will appear at the image plane.

2.4.2 Beam steering via AOD's

Acousto-optical deflectors are a common practical devices to steer a laser beam. Their working principle is based on the Acousto-optical effect. A crystal is strained due to an acoustic wave. A piezo is used to create vibrations that propagate in the crystal, and it is absorbed on the opposite facet of the crystal. Vibrations compress and stretch the medium creating a pattern. Due to the different density of the crystal medium at different position, the refractive index is modified creating a grating that can be used to deflects light.

As a simple model, let us consider a rectangular crystal like in figure 2.4.3. The acoustic wave creates a sinusoidal pattern with frequency Ω_s and wavevector q , for the refractive index $n(x, t)$

$$n(x, t) = n - \Delta n_0 \cos(\Omega_s t - qx), \quad (2.4.8)$$

where n is the refractive index of the unperturbed medium, Δn_0 is the amplitude of the perturbation. Δn_0 is proportional to the square root of the sound intensity.

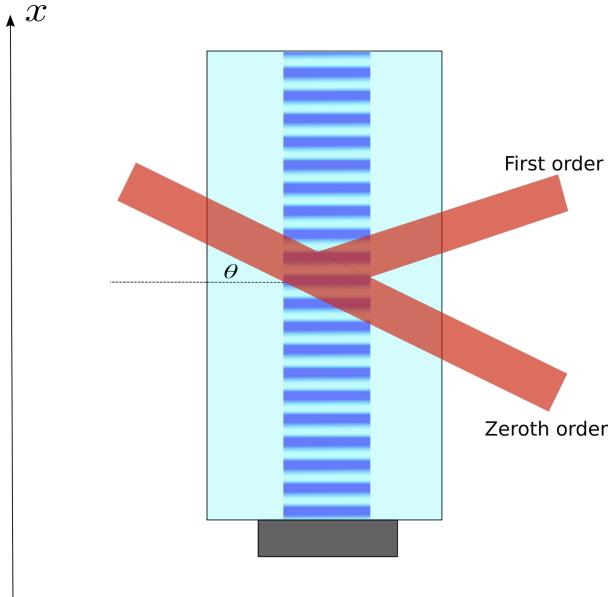


Figure 2.4.3: AOD.

The reflected wave can be calculated by dividing the crystal in thin layers, each with his refractive index $n(x)$. The total reflection is given by all the contributions $\frac{dr}{dx}$ of every layer, we can therefore integrate over a length L as follow:

$$r = \int_{L/2}^{L/2} e^{i2kx \sin \theta} \frac{dr}{dx} dx \quad (2.4.9)$$

The included phase takes into consideration the different phase of the input beam when different layers are met. The integral can be solved with a change of variable

$$\frac{dr}{dx} = \frac{dr}{dn} \frac{dn}{dx} = \frac{dr}{dn} q \Delta n_0 \sin(\Omega_s t - qx), \quad (2.4.10)$$

The sine function can be written as exponential and now the integral contains only exponential functions which are trivial to calculate. At the end we obtain two contributes for the reflected wave r :

$$r = r_+ + r_- \quad r_{\pm} = \pm i r_0 \text{sinc} \left[(2k \sin \theta \mp q) \frac{L}{2\pi} \right] e^{\pm i \Omega_s t} \quad (2.4.11)$$

These two terms are the plus and minus first order diffraction, an acousto-optical device can be operated symmetrically entering either with a positive angle or with a negative one. Since the maths and the physics is the same, we will focus only on the positive term, called upshifted Bragg diffraction. The sinc function peaks sharply when its argument is 0, i.e. at $2k \sin \theta = q$, and then quickly decreases as the angle is changed. Hence, the input beam must enter with a particular angle in order to diffract. The condition to be satisfied is usually called Bragg condition, and can be written as a function of the wavelengths as

$$\sin \theta = \frac{\lambda}{2\Lambda_s} \quad \Lambda_s = \frac{2\pi}{q}. \quad (2.4.12)$$

If the condition is not perfectly matched, some light will not be diffracted and will be

transmitted unaltered through the device. The ratio of the transmitted and diffracted light is called diffraction efficiency and gives an idea of how well an acousto-optical device is performing.

From equation (2.4.11) we can notice that an extra phase factor proportional to $\Omega_s t$ is added to the reflected wave. Thus, if the incoming wave is oscillating at $\propto e^{i\omega t}$, the diffracted wave will oscillate as $\propto r_+ e^{i\omega t} \implies \propto e^{i(\omega + \Omega_s)t}$. The frequency of the diffracted wave ω_r is therefore shifted by the frequency of the acoustic vibration as

$$\omega_r = \omega + \Omega_s. \quad (2.4.13)$$

This fact already suggests an application for acousto devices: they can be used as tuning device to shift the frequency of a laser. This kind of devices are called acousto-optical modulator (AOM). However, it is not the only application, we can also use the same device to deflect a beam. The idea is to change the deflection angle θ by changing the frequency Ω_s applied to the crystal. Assume that the angle θ is small enough to approximate $\sin \theta \sim \theta$, the Bragg condition can be written as

$$\theta \simeq \frac{\lambda}{2v_s} f, \quad (2.4.14)$$

where v_s is the speed of sound and f the frequency of the signal. We can already see that if we change the frequency f , the deflection angle θ changes proportionally. Although the Bragg condition (2.4.12) is not satisfied anymore, we can work with small enough angles that the diffraction efficiency remain above a certain thresholds. The bandwidth is defined as the possible scanning angles, if B is the frequency bandwidth in which the diffraction efficiency stay above a certain number (50% for instance). Then, the range of scannability is

$$\Delta\theta = \frac{\lambda B}{2v_s} \quad (2.4.15)$$

there are several ways to engineer such device to increase bandwidth and keep the Bragg condition verified, for example the transducer is replaced by a phase array of transducers that tilt the acoustic beam [1].

Chapter 3

Existing experimental system

The work developed in this thesis lies on top of an existing experiment. In this chapter we are going to describe the essential parts of the already existing setup on top of which the addressing system has been build. Calcium-40 ions are used in the experiment, the implementation of several techniques for trapping and manipulating these ions are discussed. Furthermore, the addressing setup utilizes 393 nm light, the laser emitting this light was already installed and used, thus that setup is presented. The experiment can be controlled remotely via computers, an overview of how it is implemented and how it works is also given.

3.1 Ion trap and key techniques

3.1.1 Calcium Ions

In choosing the appropriate ion to trap, one looks first of all for simplicity, which means choosing an element with one single electron in the most outer orbital. This fact limits the choice to the second group of the periodic table, many of these elements have been successfully trapped: beryllium [24], barium [25], strontium [26], and calcium [27]. The latter has been chosen for this experiment, as calcium has transitions easily accessible with commercial diode and titanium-sapphire lasers. The most abundant isotope of calcium is calcium-40, which is a common choice, but not the only one [28]. Nevertheless, $^{40}\text{Ca}^+$ ions were our choice. In figure 3.1.1 the level scheme of the only electron in the outer shell is presented. A single ground state is present $S_{1/2}$ with no hyperfine structure as $^{40}\text{Ca}^+$ does not possess a nuclear spin. There are two short lived excited states (~ 7 ns): $P_{1/2}$, and $P_{3/2}$ which are accessible with dipole transitions. These states have different decay channels, for $P_{1/2}$ the branching ratios are 6% to $D_{3/2}$, and 94% back to the ground state. For $P_{3/2}$ there is a probability of 5.3% to decay to $D_{5/2}$, 0.6% to go to $D_{3/2}$ and 94% to return to $S_{1/2}$. Due to the short lifetimes of these two states, they are suitable for laser cooling and state detection, while the states $D_{3/2}$ and $D_{5/2}$ are metastable (~ 1 s) since accessible with electric quadrupole transition. Since the lifetime of the D states are much greater than typical coherence time, they can encode a stable qubit and manipulated without worrying about dissipative process. Table 3.1.1 summarizes details about the different transitions, and what they are used for. A more detailed description and implementation is discussed in the next section.

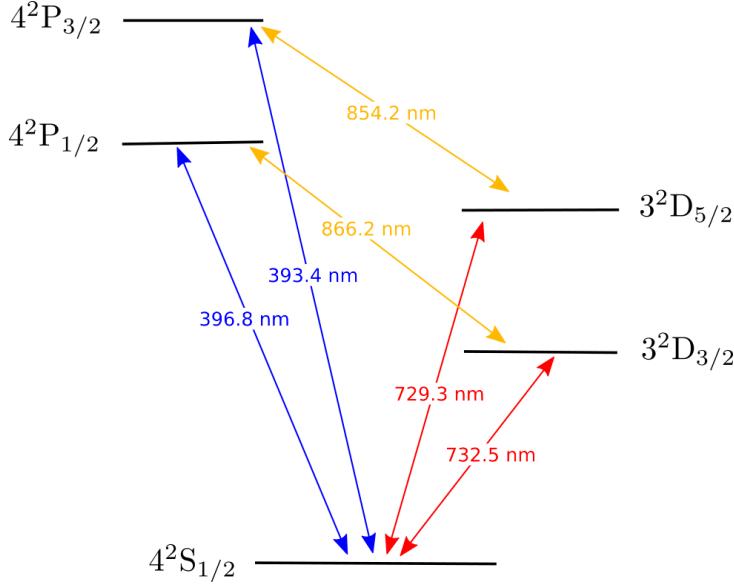


Figure 3.1.1: Level scheme of $^{40}\text{Ca}^+$ with main transitions highlighted. Blue transitions are dipole transitions suitable for cooling, imaging and photon detection. Red transitions are dipole forbidden, but accessible with electric quadrupole, they are used to encode qubits. Orange transition are usually repumped. In addition, the 854 nm transition is tuned in resonance with the cavity for photon generation purposes. From more and precise value see table 3.1.1

Transition	wavelength (nm)	Decay rate Γ	Lifetime τ	Main use
$S_{1/2} \rightarrow P_{1/2}$	396.847	$2\pi \times 20.8$ MHz	7.7 ns	Cooling and imaging
$S_{1/2} \rightarrow P_{3/2}$	393.366	$2\pi \times 21.4$ MHz	7.4 ns	Photon generation
$S_{1/2} \rightarrow D_{3/2}$	732.389	$2\pi \times 0.132$ Hz	1.080 s	-
$S_{1/2} \rightarrow D_{5/2}$	729.147	$2\pi \times 0.136$ Hz	1.045 s	Qubit
$P_{1/2} \rightarrow D_{3/2}$	866.214	$2\pi \times 1.70$ MHz	94.3 ns	Repumping
$P_{3/2} \rightarrow D_{5/2}$	854.209	$2\pi \times 1.34$ MHz	101 ns	Cavity photon
$P_{3/2} \rightarrow D_{3/2}$	849.802	$2\pi \times 1.52$ MHz	902 ns	Repumping

Table 3.1.1: Transitions in $^{40}\text{Ca}^+$ and current use in the experiment. Values are taken from [20, 29]

3.1.2 Trapping, cooling, and state readout

Our trap is a linear 3D RF Paul trap as depicted in figure (), the picture of the real trap is displayed in figure 3.1.2. The trap consists of 4 orthogonal electrodes with blade shape for RF confinement in the radial direction. In the axial direction confinement is achieved with two tip electrodes that forms the endcaps. Everything is made in titanium, it is covered in gold and the trap itself is mounted vertically on a Shappire holder. The endcaps are 5 mm apart, and they are usually kept at a voltage in the order of 500-1000V, which means an axial frequency of $\omega_z \sim 2\pi \times 0.7 - 1$ MHz. The four blades are 0.8 mm from the center of the trap and driven with an RF of ~ 24 MHz. Due to the high power delivered to this blades (~ -4 dBm), the RF signal has to be impedance matched with the trap, this



Figure 3.1.2: Photo of the mounted trap, a pair of compensation electrodes and the mirrors of the cavity are also visible.

is done with an helical resonator. The trap also includes three pairs of compensations electrodes that can be used to compensate micromotion. Loading of ions is done with an atomic oven, calcium is heated a directed towards the trap, in the trap the atoms undergo 2-stage photon ionization. The first laser 375 nm, excite one electron to a very high excited state, the second laser 422 nm, brings the electron to free space ionizing the atom. Such two stage process allows to filter for isotopes and ionize only ^{40}Ca . Loading usually takes minutes or tens of minutes depending on the number of ions one wants to load. Storing time can be in the order of days, especially when a single ion is loaded.

Once loaded, ions are laser cooled with 397 nm light on the transition $S_{1/2} \rightarrow P_{1/2}$ detuned at $-\Gamma/2$. An additional repumper on the transition $P_{1/2} \rightarrow D_{3/2}$ is also used to avoid for the electron being stuck in the $D_{3/2}$ state. For typical experiment a stage of doppler cooling is always included, this lasts from 1 millisecond up to tens of milliseconds.

With the same Doppler cooling light, imaging can also be done. The light shines on the ions exciting the transition $S_{1/2} \rightarrow P_{1/2}$ driving the electron to the excited states which then decay spontaneously emitting a photons. Photon are collected with a custom objective with NA of ~ 0.3 , which means an efficiency of 2.5 % over the solid angle 4π . The objective focuses the collected photons 1.5 meters away where a CCD camera (Andor iXon Ultra 897) is placed. The geometrical path of the imaging is displayed in figure 3.1.3, this setup has a magnification factor of ~ 18.6 . The same objective is also used for the addressing setup built within this thesis. Therefore, the imaging optical path must be partially shared with the newly built addressing. In depth overview of objective is therefore given in section 4.2.

State read out is possible with this kind of imaging, with the difference of using a photonmultiplier tube (PMT) for counting photons instead of a camera. Consider a qubit encoded in the states $S_{1/2} \rightarrow D_{5/2}$, if the imaging laser is switched on, the electron will be projected either to the $S_{1/2}$ level or in the $D_{5/2}$. In the first case, photons are scattered from the ion and collected on the PMT, in the second case the electron is shelved and will not scatter any photon. Hence, the two cases are distinguishable by counting statistics.

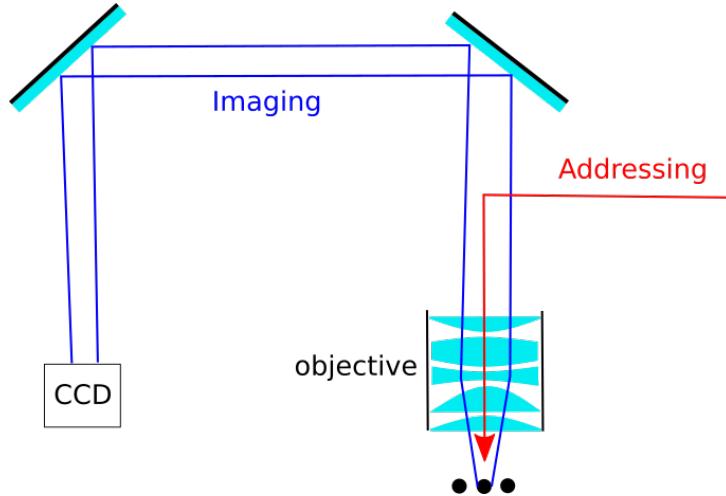


Figure 3.1.3: Top view of the imaging optical path, the objective collimates and focuses the scatter photons onto the CCD camera. The addressing setup must share part of this path, as the same objective is used for focusing.

An histogram can be constructed with the number of photon measured, and a properly set threshold differentiates between bright and dark states. Typical detection times are in the order of milliseconds.

3.1.3 Photon generation

By placing a cavity around the trap, photon generation is enabled. The cavity mediated Raman process is responsible for this phenomenon. It can be explained starting from a three level atom like in figure 3.1.4. The electron is initially in the ground state $|0\rangle$, a laser pulse excites the transition $S_{1/2} \rightarrow D_{3/2}$ detuned properly to eliminate the population in the $|e\rangle$ level. Among the decay channels of the electron, the decay $P_{3/2} \rightarrow D_{5/2}$ is enhanced due to the presence of the cavity and therefore the coupling g between the ion and the cavity mode. The electron will more likely decay to the $D_{5/2}$ state emitting a photon inside the cavity. Thus the process can be described as $|0\rangle_i |0\rangle_p \rightarrow |1\rangle_i |1\rangle_p$ where the subscript i indicates the ion and p the photon number in the cavity. The detuning is set such as $\Delta \gg \Omega, g$, in this regime the whole process can be described as a single transition with effective Rabi frequency of [16]

$$\Omega_{eff} = \frac{\Omega g}{2\Delta}. \quad (3.1.1)$$

It is equivalent of a classical Raman process driven with two laser pulses on the two different transitions, but in this case the second laser is substituted by the vacuum standing wave of the cavity. In order to avoid decay in other channels, one must be sure that Ω_{eff} is larger than the effective decay rate of other spontaneous emission $\Omega_{eff} \gg \Gamma_{eff}$. Moreover, the photon should leave the cavity after the transfer is complete, this is ensured by $\Omega_{eff} > \kappa$.

In the real case the electronic states are also shifted due to a magnetic field generated by a permanent magnet perpendicular to the cavity axis and at 45° with respect to the trap axis. This is done in the optics of achieving ion-photon entanglement, since in that case multiple Zeeman levels should be addressed. The situation is therefore further

complicated and the polarization of the laser field should be taken into consideration. In figure (), the Zeeman structure of $^{40}\text{Ca}^+$ is depicted. One can start from the state $|\text{S}_{1/2}, m_j = -1/2\rangle$. From here three choices of polarization can be taken: σ^- , π , σ^+ , for each choice three Raman transition are possible, the most favorable in the case of the magnetic field orthogonal to the cavity axis is [6]

$$|\text{S}_{1/2}, -1/2\rangle \rightarrow |\text{P}_{3/2}, -3/2\rangle \rightarrow |\text{D}_{5/2}, -5/2\rangle. \quad (3.1.2)$$

In this case the transitions strengths, i.e. the projection on the laser polarization onto the dipole moment, and the same projection onto the cavity axis are maximized.

The generated photon from this process can be entangled with the ion state by driving this Raman transition with a bichromatic beam. This means that the laser pulse drives two transitions at the same time, for example the one that ends up in $|\text{D}_{5/2}, -5/2\rangle$ and $|\text{D}_{5/2}, -3/2\rangle$. In this instance, the generated photon will be a superposition of σ^+ and π polarization. With respect to the cavity it means vertical and horizontal polarization. The final state of the bichromatic transition is therefore

$$|\psi\rangle = |\text{D}_{5/2}, -5/2\rangle |H\rangle + |\text{D}_{5/2}, -3/2\rangle |V\rangle. \quad (3.1.3)$$

In the real experiment the designed cavity is near concentric with a length of 19.9 mm, and radii of curvature of 9.98 mm. The cavity length is actively stabilized with a PDH type feedback which locks the mirrors position to a 806nm laser. One mirror of the cavity is highly reflective $T_1 = 2.2$ ppm, while the other is more transmissive $T_2 = 97$. This asymmetry of the mirrors allows for the produced photons to exit one from one side in most cases and subsequently coupled to a fiber. The probability to get a photon out of the cavity from the designed mirror can be determined from the transmission and losses of the cavity, the maximum achievable is $P_{max} = 0.83$. The maximum g factor achievable with this geometry is $g = 2\pi \times 1.53$ MHz. The Finesse of the cavity for the TEM₀₀ mode is 54000. The other cavity parameters are $\kappa = 2\pi \times 70$ kHz, and $\gamma = 2\pi \times 11.45$ MHz for the P_{3/2} state. With these numbers the preferred strong regime is not reached, but nonetheless, it is still possible to produce photons and collect them out of the cavity.

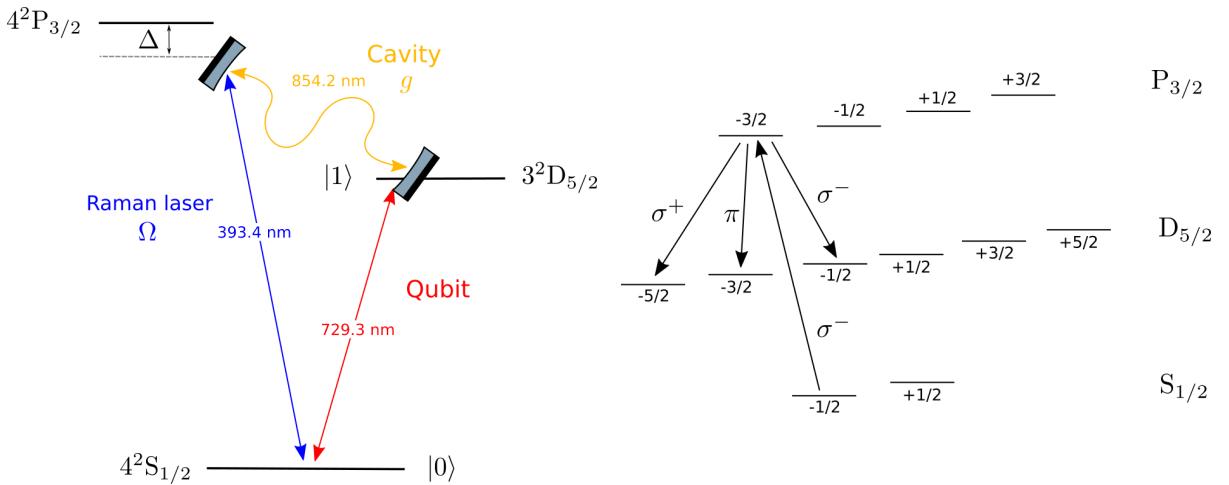


Figure 3.1.4: Roba

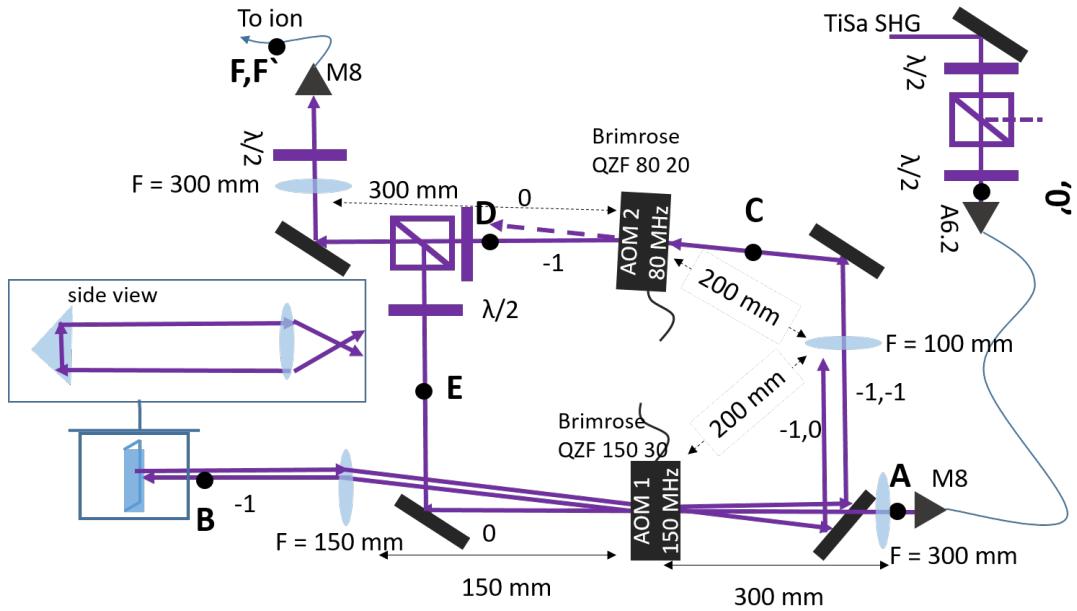


Figure 3.2.1: 393 nm optical setup.

3.2 393 nm laser

The laser used to drive the Raman transition is 393 nm. This light is obtained from a titanium-sapphire laser from MSquared. The laser is optically pumped with 8 W of light at 532 nm coming from a Lighthouse Photonics Sprout laser. The active Ti:Sa crystal is contained in a cavity in a bow tie configuration, together with an optical diode, etalon, birefringent mirror, and tunable cavity mirror for frequency tuning and stabilization. The fundamental mode is at 786 nm with tunability ranging from 725 nm to 875 nm that can be controlled remotely on the computer. The laser can also be locked to a wavemeter and tuned with it. The fundamental light is frequency doubled to 393 nm via a MSquared ECD-X external cavity resonant doubler accessory module. Blue light can be obtained with up to 1 W of power. Before reaching the ion trap, 393 nm light is sent through the setup in figure 3.2.1. There are two AOM's in the setup, AOM1 from Brimrose with a working frequency of 150 MHz, AOM2 is still from Brimrose and works at 80 MHz. There are two paths for the light: a resonant one which gets resonant light from the laser, and send it directly to the ion trap. The second path is the detuned one, the main purpose is to red detune the laser light in order to excite the Raman transition. This path goes through both AOM's, the first AOM1 is in double pass configuration and shift the light by 300 MHz. Diffracted light in the -1 order is sent through and reflected back again in the same AOM by a prism. Diffracted light from AOM1 is sent to the second AOM used in single pass configuration which further shift the light by 80 MHz. The diffracted light (-1 order), from AOM2, is coupled to a fiber that brings it to the ion trap. The detuned beam therefore reaches the ion with a -380 MHz detuning which can be modulated within the bandwidths of both AOM's. The zeroth order of AOM2 is blocked to avoid that this light is coupled to the fiber and end in the trap. Lenses in the setup have the purpose to focus the waist of the beam in the AOM's aperture avoiding unwanted beam steering and therefore losing coupling to the

fiber. AOM2 is also used to generate a bichromatic field, simply by driving this AOM with a multifrequency signal.

This particular setup had to be altered after the installation of the addressing setup, minor adjustment had to be made in order to compensate for an additional frequency shift due to the AOD in the addressing setup. AOM2 was switched from -1 order to +1 order, and driving frequency were changed to 180 MHz for AOM1 and 70 MHz for AOM2.

3.3 Experiment control

Complex experiments require control over a large network of AOM's and other devices. Furthermore, laser pulse coherence is also fundamental in some sequential experiment. The need of fast and coherent pulse control is fulfilled by an electronic system that can be controlled with a software on a computer where every device connected to the network can be controlled. The experiment control network is sketched in figure 3.3.1. On the computer TrICS software is installed, this computer is connected to a BUS system with a NIDAQ card. Direct Digital Synthesizers (DDS) used to generate radio frequency signal for AOM's are connected to the BUS system through an optocoupler to avoid ground loops. Therefore, the computer can send electric signal over the BUS to specific DDS allowing for direct control. The computer is also connected via ethernet to a Pulse Box, and through another NIDAQ card to the same box. The card sends and receive trigger signals, while over the ethernet, sequences are uploaded. The pulse box contains DDS and and FPGA, thus it has the capabilities of generating short and coherent TTL pulses (μ s) that can send to TTL switches placed between a DDS, the source of the signal, and an AOM. The Pulse Box contains fast switching DDS, this means that the frequency of such DDS can be changed quickly, unlike the DDS on the BUS. The whole system runs with two separated clocks, one at 10 MHz, and another one at 1.2 GHz.

With this system, a laser pulse can be controlled in frequency, amplitude, and length. Frequency and amplitude are set in the DDS by sending a signal over the BUS system to the appropriate DDS channel. The length of the pulse can be controlled precisely by the Pulse Box. Moreover, the Pulse Box also has pulse shaping possibilities.

In a typical experiment, a sequence of pulses is programmed in python on the computer. When the experiment is run, the computer uploads the sequence to the FPGA inside the Pulse Box. Next, the computer updates the DDS on the BUS with the appropriate values for the experiment, sends a trigger signal to the Pulse Box and the Pulse Box generates and sends all the signals for the sequence. When the experiment is done, the Pulse box sends another trigger back to the computer, which proceeds to prepare for the next measurement point, it updates the values of the BUS DDS, reupload the code to the Pulse Box, sends a trigger to start the sequence and the loop is repeated.

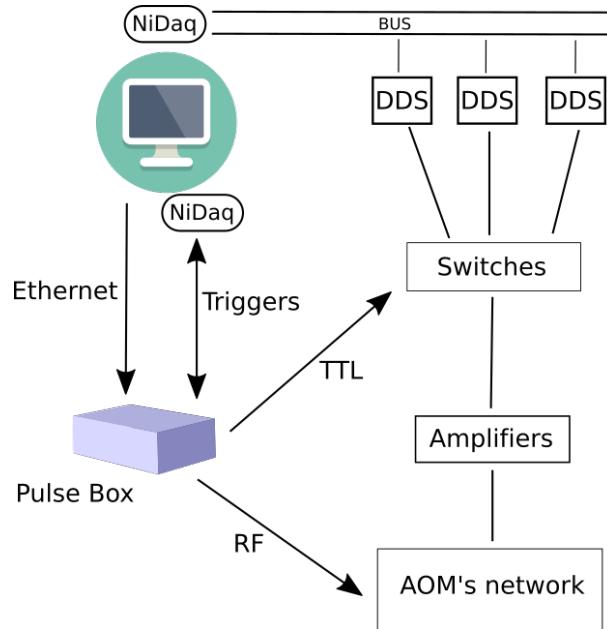


Figure 3.3.1: Schematic of the experimental control



Figure 3.3.2: Trics software

Chapter 4

Design and simulation of the addressing setup

The purpose of this thesis work was to design and build the addressing setup for the already existing experiment. In this chapter we discuss the design and the implementation of such setup. The design is a crucial part of the work, there are several requirements that have to be met in order to achieve the proper needed functionality. In the first section, the requirements are presented together with an overview of the design idea. In the setup an objective was already present, and the choice of an AOD was already made. Hence, we discuss this components as given. The rest of the setup was simulated with the software Zemax, which was used to find the optimal optical components and their placement.

4.1 Addressing system overview and requirements

Addressing systems have already been developed and employed in experiments successfully. Different techniques are available: the main idea is to focus a laser beam tighter than ion-ion separation and steer it. In Innsbruck calcium ions have been addressed in this way, where the steering was achieved with an AOD [30]; Beam has also been steered with micro-electromechanical systems (MEMS) mirrors [31]. Another idea is to send a normal beam illuminating all the ions, but hiding those who are not addressed. This was done with Ytterbium atoms where by means of a inhomogeneous magnetic field the transition frequencies were shifted shielding selected ions [32].

Our choice was to implement the already successful idea of Innsbruck with an AOD and improve it. The advantage of AODs is to have a fast switching time in the order of μs , that is used for fast switching between ions. A problem with the implementation of [30] is however the fact that the AOD is placed right before the beam expander, this limits the addressing range, as the beam is likely to clip when it is steered on the edge of the AOD's bandwidth. This is the main problem that the new designed system, here implemented, wanted to address: exploiting the full capabilities of the AOD while maintaining a very tight focus. Therefore, there are mainly two aspects to keep in mind, the focus spot and the addressing range. However the priority was the focus spot as a large addressing range is not essential.

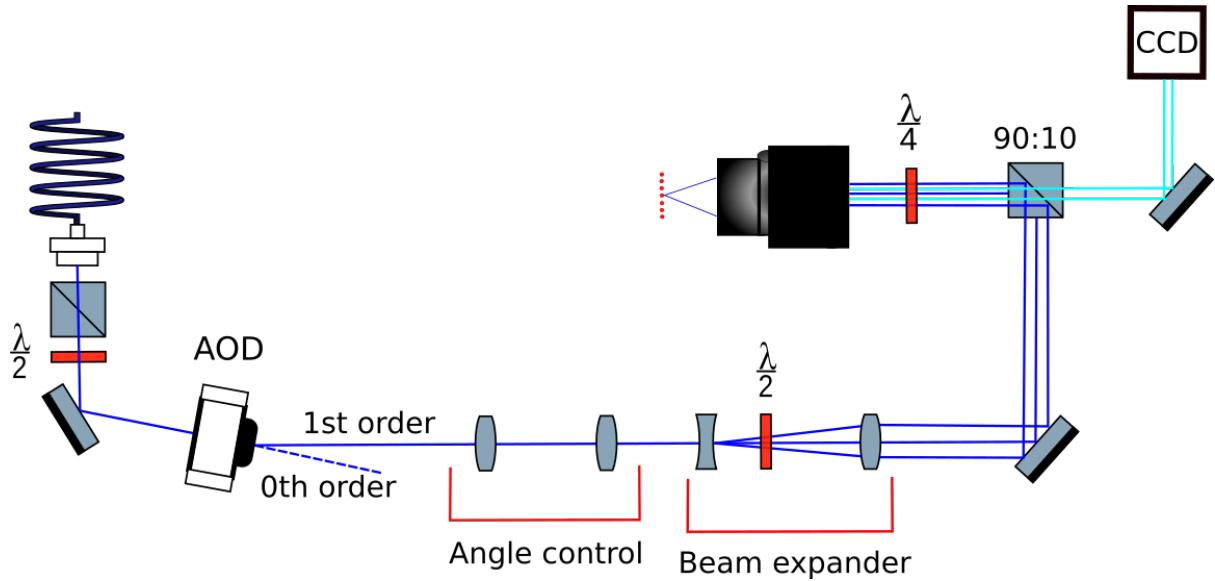
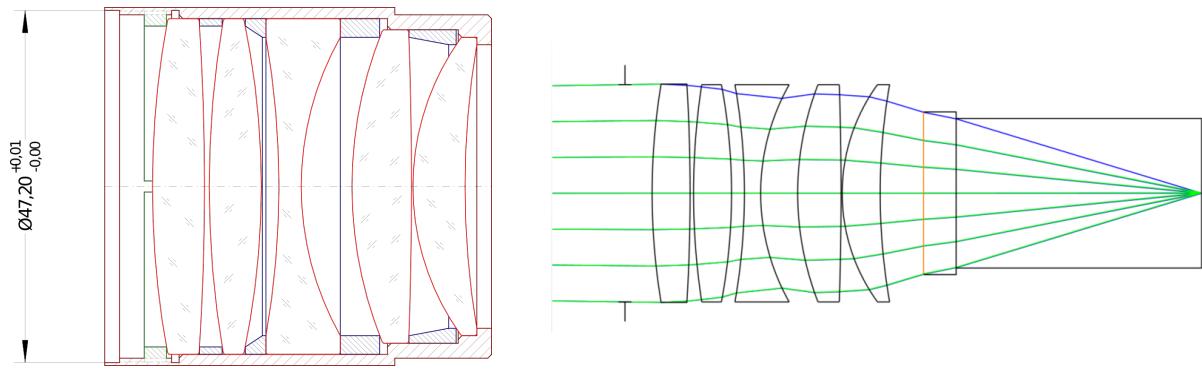


Figure 4.1.1: Scheme of the setup. Light comes from a fiber, polarization is cleaned, and then sent thorough the AOD. 1st order diffracted light is refocused into a beam expander, where the beam is broadened before being focus by the objective. Light blue lines represents 393 nm light coming from the ions into the imaging setup.

The addressing setup should be able to address single ions in a string in order to generate single photons out of single ions via the already discussed Raman process. Ion separations, in the case of $^{40}\text{Ca}^+$, has been derived in section 2.3.2, for a trap frequency of 1 MHz is $5.6 \mu\text{m}$. The setup must therefore be able to focus tightly a laser beam down to 1-2 μm . As seen in section 2.4.1, a tighter focus can obtained with a shorter wavelength, a bigger lens, or with shorter focal length. The focusing lens, a.k.a the objective, is shared with the imaging setup, and thus it is given, the focal length is therefore a constant in the problem. The wavelength is also a constant, as the Raman process happens only at 393 nm. This gives only one possibility left to tighten the focus, i.e. by making the beam as broad as possible at the objective input surface. Beam expansion can be achieved with a Galilean telescope, it take two lenses to form such Telescope, a concave Lenses to diverge a collimated beam and a convex lens to collimate the diverging beam. The combinations of these two lenses takes a collimated beam and expands it to another collimated beam. This expansion part is one of the two essential part of the addressing setup. The other part is related to addressing range. Not only, we want to focus the beam to a single ion, but we want to move the beam as well, such that it focuses on a different ion. Therefore, there is a requirement also on the range that can be addressed. This depends on the number of ions and their spacing, a good aim is to address tens of ions, this requires the ability to move the focus in one direction by $150\text{-}200 \mu\text{m}$. Beam steering is possible with the use of an AOD, the detailed working principle of this device has been discussed in section 2.4.2. Basically the angle of the output beam of the AOD changes as the driving frequency changes. However, the AOD must be placed far behind the objective to leave space for the beam expander, this implies a need to control and redirect the angle of the AOD's output beam to send it to the beam expander and later in the objective without any clipping. This task is accomplished with a pair of converging lenses, they refocus the collimated beam into the beam expander, beam then becomes wider, reaches the objective and it is focused on the ion. It is important to get the right lenses at the right distances,

the objective has 5 different lenses inside and it works slightly differently from a normal lens. For instance, it does not focus collimated blue light, but red. This means that the beam expander should not collimate completely the beam but rather expand it and leave it diverging, so that the objective can focus it at the right position. The setup displayed in figure 4.1.1 also contains polarization optics. As discussed in section 3.1.3, Zeeman transitions are polarization sensitive, thus polarization control is required. The AOD is polarization sensitive, which means it requires a certain input polarization and outputs another particular polarization, that is the reason why half wave plate are before and after, and additional quarter wave plate is inserted before the objective to obtain circular polarized light. This placements means having a bigger plate than standard, but if placed before in the optical path, the mirror and the beam splitter could alter the polarization. Moreover, the quarter wave plate is zeroth order and custom made, in order to have a greater polarization stability. The choice of using a beam splitter is also peculiar, to separate light at different wavelength it is common choice to use a dichroic mirror, however the light in the imaging path is 397 nm, very close to the 393 nm light of the addressing setup. This would have meant using a very narrow dichroic, the alternative was to use a 90:10 beam splitter, where 90 % of the light is transmitted and only 10 % of the light is reflected. The addressing therefore loses 90 % of the power on this splitter, but that is not a problem, since it is always possible to get more light out of the laser. Furthermore, this light is focused so tightly that even a small amount of light can excite the ions. On the other end, it is not really possible to get more scattered light from the ions, so 397 nm light and the imaging setup must be as efficient as possible, with 10 % of losses, ions are still visible on the camera and on the PMT.

4.2 Objective and AOD



(a) Section of the custom objective, red parts are the lenses, while the rest is the housing.

(b) Zemax simulation of the objective. On the right, viewport and the vacuum chamber are also present.

Figure 4.2.1

The objective used to focus the light was already present in the system and had to be taken as it is. It is a custom objective by Sill optics placed outside vacuum, the section is in figure 4.2.1a. It contains 5 lenses inside a mechanical housing, the aperture is about 47 mm large in diameter. This objective has different purposes, it was designed keeping in mind: imaging of ions, addressing with red light and addressing of blue light. The objective has

to perform all three of this jobs fairly well, which means it has light transmission $>90\%$, every lenses is AR coated, numerical aperture of $NA = 0.3$. Moreover, it is telecentric, which means that the focus spot should move perpendicularly to the optical axis if the beam is steered. Lastly it was also designed to take into consideration the fact that it is placed out of vacuum, the light after the objective has to go through a 6 mm fused silica viewport before entering the vacuum and after further 40 mm encounters the ions. The focal length of the objective is 54.07 mm at 729nm. The objective is also mounted on a 3 dimensional translational stage to allow for imaging and addressing calibration.

The AOD is from Gooch & Housego, model 4120-3. It has a specified central frequency of 120 MHz, with 50 MHz, bandwidth, so the driving frequency ranges from 95 to 145 MHz with a maximum RF power of 0.3 W. Therefore, the angle of deflection should be $\pm 0.86^\circ$ ($\pm 0.86^\circ$). In this bandwidth the diffraction efficiency should remain above 75 % and have an average of 83 %. Further light is lost as much as 3% of due to insertion losses. The active aperture measures 3×3 mm, and the polarization has to be horizontal when entering the AOD, while it gets rotated during diffraction, as the specified output polarization is vertical.

4.3 Design simulation

The setup in figure 4.1.1 has been simulated with the software Zemax. The simulation had the purpose of assessing the performance of the setup, i.e. checking the viability of the setup and see if it meets all requirements. It was also used to find the best lenses for building the setup and the best placement. Not everything was simulated, bu only the essential parts. This includes the four lenses, the objective, the viewport and the vacuum chamber. As there is no option to simulate an AOD, it was not taken in consideration, instead the simulation started at the output of the AOD as described below. Mirrors and beam splitters also do not alter drastically the optical path and therefore there was no need to simulate them.

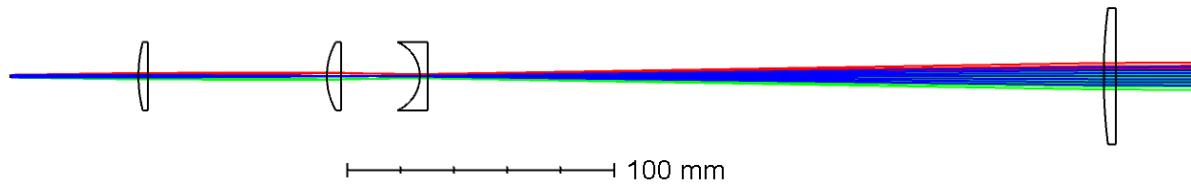


Figure 4.3.1: Zemax simulation of the setup. Rays propagate from left to right, only the four lenses are displayed, objective and image plane are far on the right. Different colors indicate different fields at different angle

The simulations start by specifying the input fields, these represent the physical light beam. To account for the different angled beams at the output of the AOD, three different fields has been simulated. One is along the optical axis, while the other two are angled corresponding to the extrema of the AOD bandwidth, so $\pm 0.86^\circ$. Therefore the propagation of these beams represents three different situations of beam direction and should also give an idea of the behaviour in between the extrema. Next, the four lenses of the setup were inserted in Zemax, initially with variable radius and thickness. The Zemax file of the objective came from the company which designed it and was simply

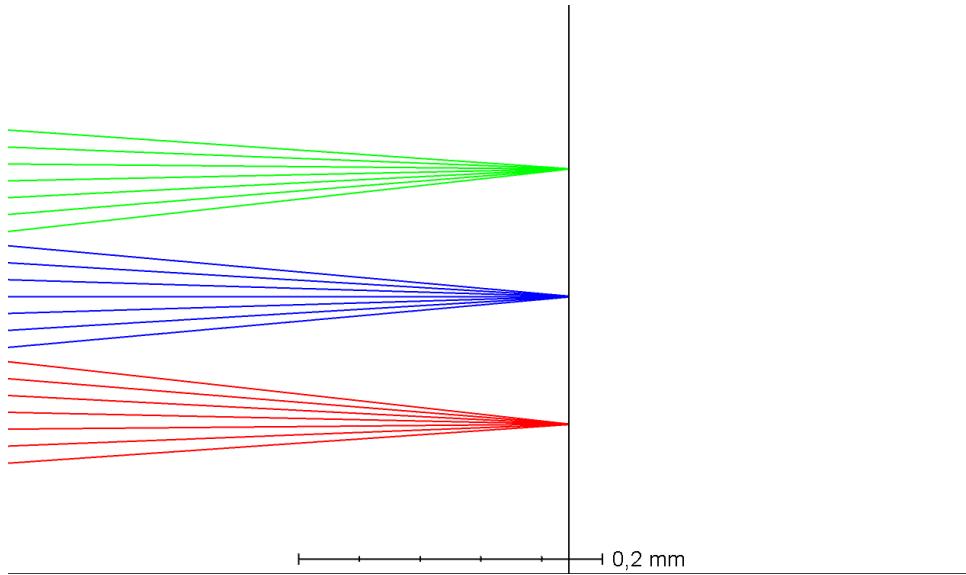


Figure 4.3.2: Zemax simulation at the image plane, where the ions are. The three colors are three different fields with different angles that are focus at different position along the ion string. The full addressing range here displayed is about 168 μm .

imported in the project. After the objective the 6mm viewport glass was included and then vacuum for 38.6 mm, which is the distance between the outer facet of the glass and the ion axis. The image plane was therefore set here. The distance between the last lens of the objective and the viewport was unknown, but a good estimation¹ allowed to progress with the simulation. They physical simulation in the software was carried out with the tool Physical Optics Propagation (POP). POP works by propagating a wavefront represented by an array of discrete points. The array is propagated through every optical component and free space. This method can be used to simulate coherent Gaussian beam with high precision as well as wave phenomena such as diffraction and aberrations. The initial value given to the propagator was the waist of the collimated beam out of the AOD. Since the beam going to the AOD comes from a fiber collimator, the value specified was taken from the datasheet of the fiber collimator, namely Scäfter + Kirchhoff 60FC-M8-33 [33]. Therefore, the specified waist was 0.72 mm.

The first step of the simulation work was to find the appropriate lens to build the setup. The thickness and the radius of the lenses was optimized trying to achieve the best focus spot while maintaining a good addressing range. Once obtained the desired situation, the lenses were found with the Zemax tool *Stock Lens Matching*. Basically the tool compares the simulated lenses with those in a catalogue from different companies and find the closest match. We opted to rely on the provider Thorlabs, so the search was limited to this company. Found lenses were in order from left to right LA-1059, LA-1131, LA-4252, and LA-1725 and can be seen in figure 4.3.1. Once the desired lenses were found, their Zemax files provided by the company were imported in the project and further optimization was carried on.

The second step was to optimize the lenses position always in view of finding the best focus spot while keeping a good addressing range. This was done using the optimising tools

¹A posteriori, this assumption was not well suited and lead to some errors in the test setup. The correct value could be found by simulating the imaging setup and optimizing this distance to get the focus onto the camera.

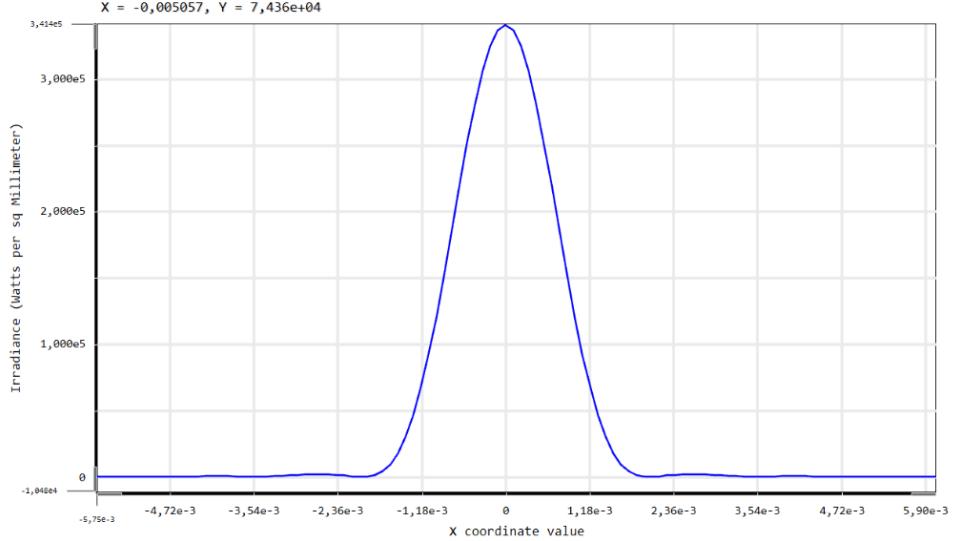


Figure 4.3.3: POP of the central field at the ion position, x cross section is displayed.

of Zemax and the merit function. The software can perform multivariate analysis and minimize the focus spot depending on all the assigned variables, which in this case were the distance between the lenses. The final results can be seen in figure (), the addressing range is $168 \mu\text{m}$, while the waist is $1.3 \mu\text{m}$.

Another important parameter for the performance of the setup is the addressing error. In the case of the beam focused on one ion, the addressing error is the leaking light on the neighbours ions. It can be a problem in the case of aberrations that produce bumps on the side of the main Gaussian peak. Especially in the case of diffraction limited system, the profile of the beam is a sinc function that can have more local maxima around the central peak. To estimate the addressing error, two ions are placed next to each other at $5.6 \mu\text{m}$, and the respective addressing beam has been simulated. The intensity profile has been plotted in figure 4.3.4 and addressing error is calculated as $I_1(x_2)/I_1(x_1)$, where I_1 is the intensity profile of the beam focused on the left ion and x_1, x_2 are the positions of the two ions. From the simulations we get $I_1(x_2)/I_1(x_1) \simeq 9 \times 10^{-4}$.

Another aspect that was simulated is the beam profile inside the trap. Optical access to the trap is limited and a tightly focus beam also has a large divergence, which could lead to clipping on the trap's blades or compensation electrodes scattering light all around the trap and thus creating problems. In figure 4.3.6 the top view of the trap is plotted. The blue line represents the radius $W(z)$ from equation 2.4.3 of the addressing beam in the case of a waist W_0 of $1 \mu\text{m}$. There is no apparent clipping, and the main problem seems to be the compensations electrodes. Since the the beam is Gaussian, there is always a clipping part. To determine the fraction of power lost due to clipping on the compensation electrodes, we can calculated the transmitted power through the electrodes:

$$P_t = \int_{-\infty}^{\infty} dy \int_{-x_c/2}^{x_c/2} dx P(z), \quad (4.3.1)$$

where $P(z)$ is the power of the Gaussian beam, and x_c is the horizontal position of the compensation electrode. The integral can be computed numerically at position z of the electrodes. The result is plotted in figure 4.3.5, where the lost power $1 - P_t$ is plotted as a function of the waist W_0 .

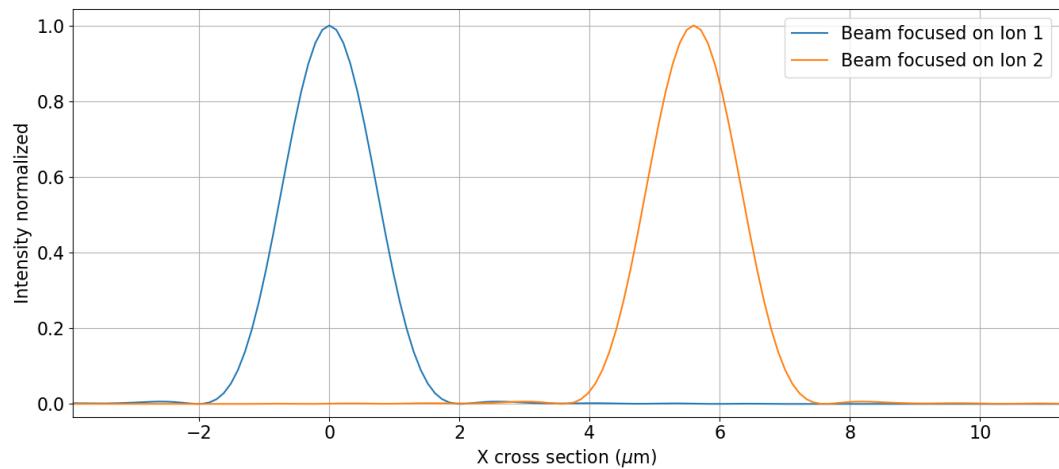


Figure 4.3.4: Beam focused at two different positions, where ions have their equilibrium position. From estimation of the addressing error can be made.

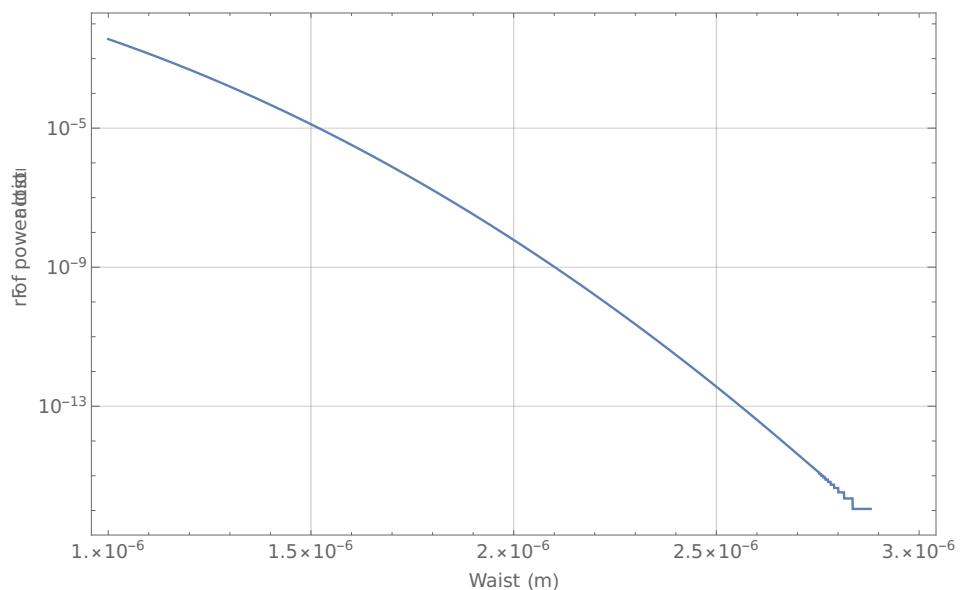


Figure 4.3.5: Losses on the compensation electrodes as a function of the beam waist

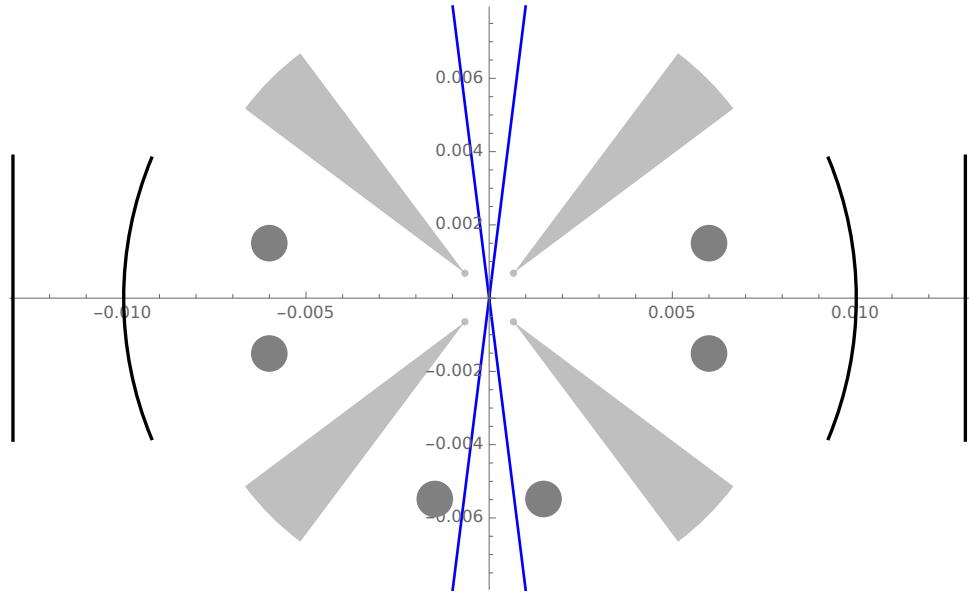


Figure 4.3.6: Top view of the trap and addressing beam. Grey circles are the compensation electrodes, blue is the radius $1/e^2$ of the beam, while the black arches representes the mirrors of the cavity.

4.4 Physical implementation

Once the simulations gave satisfactory results, a test setup was built. The idea of building first a test setup on a different optical table from the main experiment was to check if the system was working as intended, and asses its performance. Due to physical access problems, in the final system there is no space to place a beam profiler, or a polarimeter, and after the objective there is no access to the vacuum and the trap. While on another table everything could be checked and tested to make sure everything was working as expected. The results of the measurements obtained on this test setup are presented in the next chapter.

Afterwards, the real system was built. The building process was tricky, as the system is particularly sensitive to aberrations. Furthermore, there was not much room for alignment errors, since the trap and ion have to be hit perfectly. For this reason the alignment was essential. In order to make sure the addressing beam would hit the ion, a counter propagating red beam was send in the opposite direction, starting from the ion back to the objective and back to the addressing path. Since the lenses of the addressing are antireflecting coated for 393 nm, the reflection of the red beam was visible and it was possible to align every optical component. The photo of the final system is in figure 4.4.1. Here the collimating lens is mounted on a 3D translation stage with Newport screws for fine tuning calibration of the focus position. Manual screw has been later replaced with remote controlled one always from Newport, model PZA12. An iris is also used to block the zeroth order beam from the AOD. Moreover, The AOD is placed on a rotational mount that allows to tilt it in two directions. One direction was used to find the Bragg angle to achieve maximum diffraction, and the other can be used to tilt the axis over which the AOD sweeps. This can be used to compensate for an ion string which is not exactly parallel to the AOD sweeping direction.

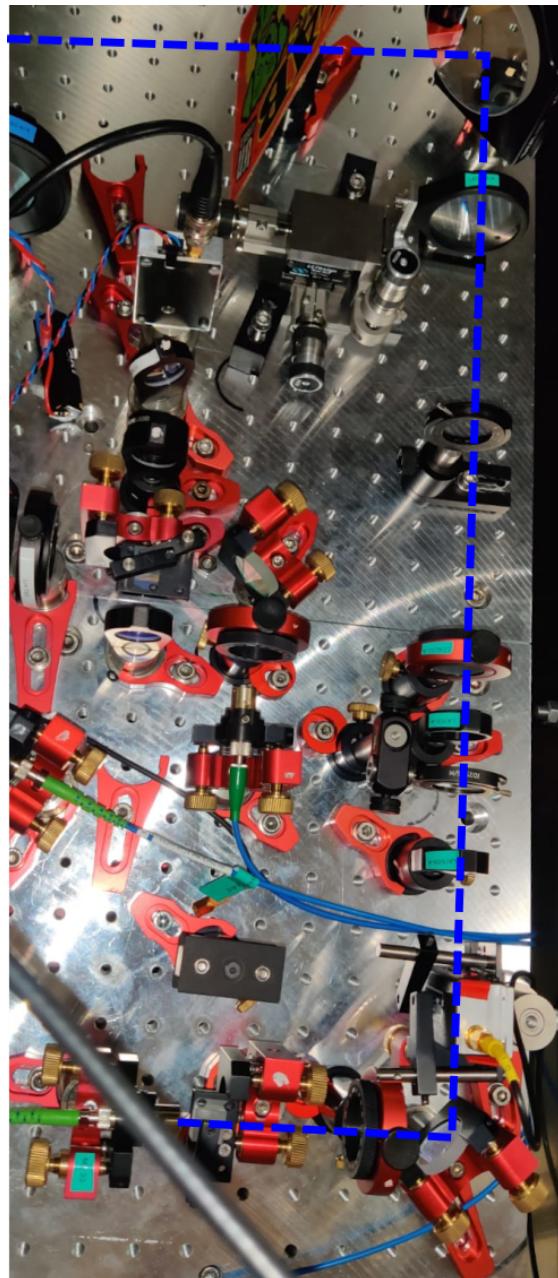


Figure 4.4.1: Photo of the final setup. The blue dashed line is the beam path starting from bottom left at the fiber collimator, all the way to the top where a mirror deflects the beam to send it to the beam splitter.

Chapter 5

Experimental results

This chapter collects all the experimental results obtained during the thesis. Apart from the AOD characterization, there are two main sections. The first one contains the measurements carried out on the test setup done to asses the performance of the system. Here, polarization, stability, and focus spot has been checked. In particular, two methods have been used to measure μm focus spot: razor blade scans, and small pixel size camera. The other section comprises more advanced quantum optic experiments realized with ions and the final installed system. Ramsey spectroscopy was used to check addressing error and focus spot. Moreover, photons have been generated from one single ion with adjacent unperturbed ions.

5.1 AOD

The AOD is the core element of the setup, it is therefore essential to characterize it. The two main parameters we are interested in are the diffraction efficiency and the response time. For the diffraction efficiency we measure the total output power of the light P_{tot} and then the power of the first diffracted order P_1 . Diffraction efficiency is defined as the ratio between the two.

$$\text{DE} = \frac{P_1}{P_{tot}}. \quad (5.1.1)$$

Before measuring the diffraction, the optimal RF power to drive the AOD has been found. This was done by measuring the power at the central frequency of the AOD and maximizing the light in the first diffracted order. Power measurements of the light were done with a Thorlabs PM100D, and the AOD was driven with a signal generator. The optimal RF power was found to be 0.11 W, and for the rest of the measurements it was kept as that value. Furthermore, the input polarization was optimized with a half wave plate, always trying to maximize the power of the diffracted light. In figure 5.1.1 the plot of the diffraction efficiency as a function of the RF frequency is displayed. Within a bandwidth of 50 MHz from 105 MHz to 155 MHz, we can see that more than 70 % of the light is in the first diffracted order as expected from the datasheet, even though the bandwidth looks shifted with respect to the nominal central frequency of 120 MHz. The response time is the time that it takes for the light to move when the RF frequency is changed. In order to perform this measurement, a voltage controlled oscillator (VCO) was used to generate the RF signal. The VCO was supplied a square wave that jumped

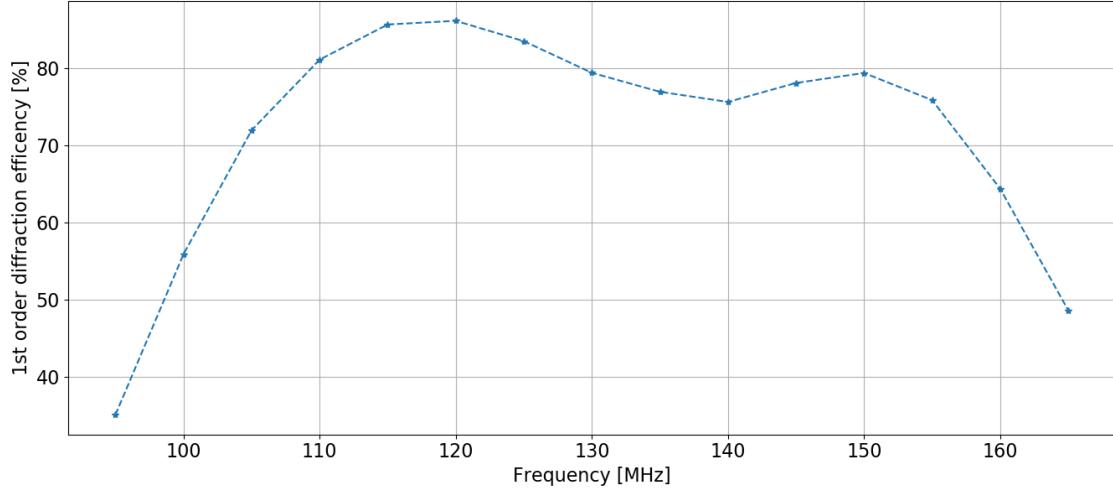


Figure 5.1.1: Diffraction efficiency of the AOD as a function of the RF driving frequency.

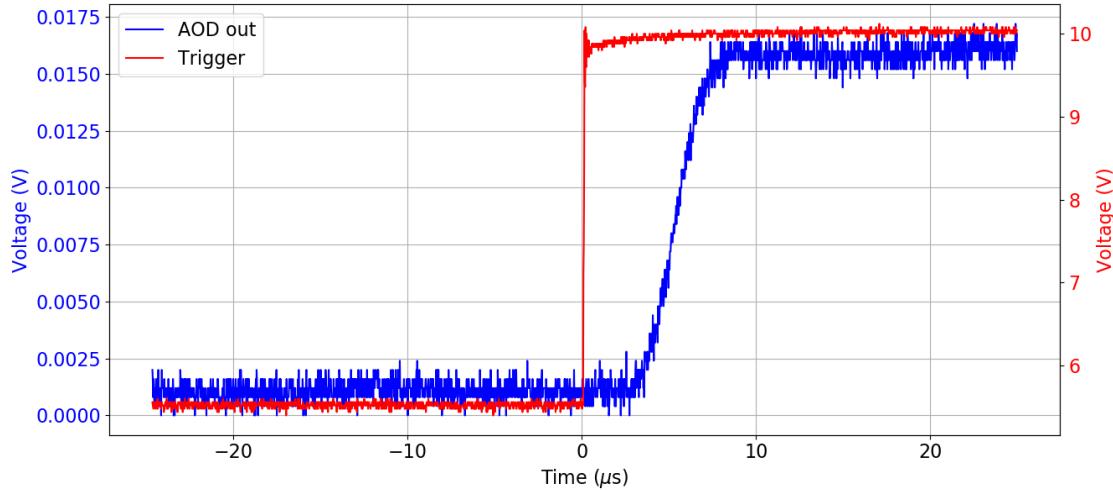


Figure 5.1.2: Response time of the AOD, plotted are the photodiode signal in blue on the left y axis, and the VCO voltage is in red on the right axis.

between two voltages corresponding to two different frequencies. The blue light was measured with a photodiode. The photodiode was aligned with the light at one particular frequency, such that when the light moves, the beam would not hit the chip and the signal generated changes. In figure 5.1.2, the signal of the photodiode, together with the supplied VCO signal are plotted. Response time is $\sim 7 - 8 \mu\text{s}$, in this time the light completely move from one angle to another one.

5.2 Full test setup characterization

The test setup was built on a spare optical table with a spare objective. The layout of the setup was as close as possible to the final version, so the system in figure 4.1.1 was replicated. The most important assessment was the focus spot, i.e. we tried to measure the waist of the beam and check if it was within requirements. This is measured in two

different ways: first we used a technique called Knife-edge, where the beam is scanned with a razor blade; then we also tried to measure it directly with a camera equipped with $1.6 \mu\text{m}$ pixel size.

Other than the waist size, we also measured stability of the system and the polarization capabilities.

5.2.1 Waist: Knife-Edge method

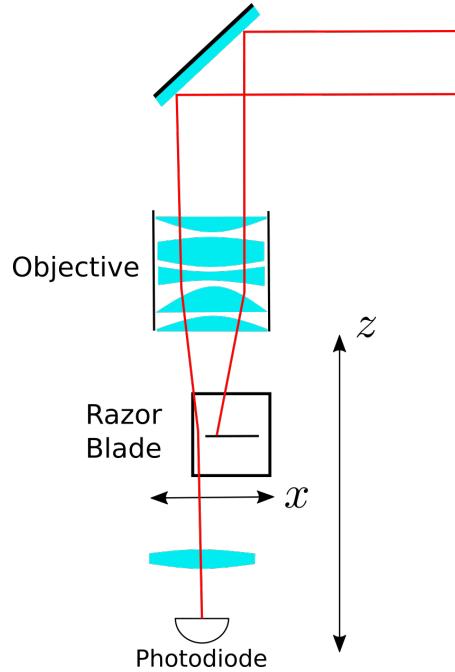


Figure 5.2.1: Scheme of the razor scan.

Measuring a micrometer waist is not easy task, the first approach we tried consists of mounting a razor blade on a translational stage. The stage is then moved in the x direction cutting the beam perpendicularly such that the blade is scanning the beam profile. The setup used is showed in figure 5.2.1, after the objective the blade is present, and since the beam is quickly diverging after the focus, a lens is used to refocus the light into a photodiode. A filter was also inserted in order to not saturate the photodiode. In the z direction the stage was controlled with a manual screw with resolution of $1 \mu\text{m}$. While in the x direction, the stage had to be moved with sub-micrometer precision, so the screw was a piezo actuator controlled by custom software. The same software also controlled a multimeter that measured the voltage of the photodiode. To get the whole profile of the beam, i.e. $W(z)$, the measurement procedure was as follow

- Position blade at appropriate z coordinate
- Scanning beam in x direction with blade
- Beam width extrapolation
- Shift z direction

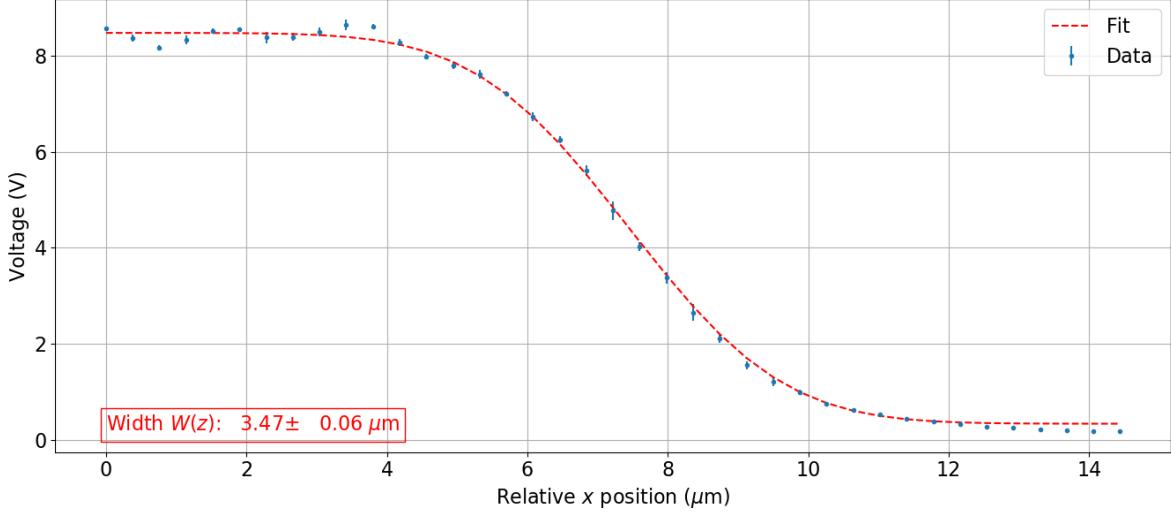


Figure 5.2.2: Example of razor scan

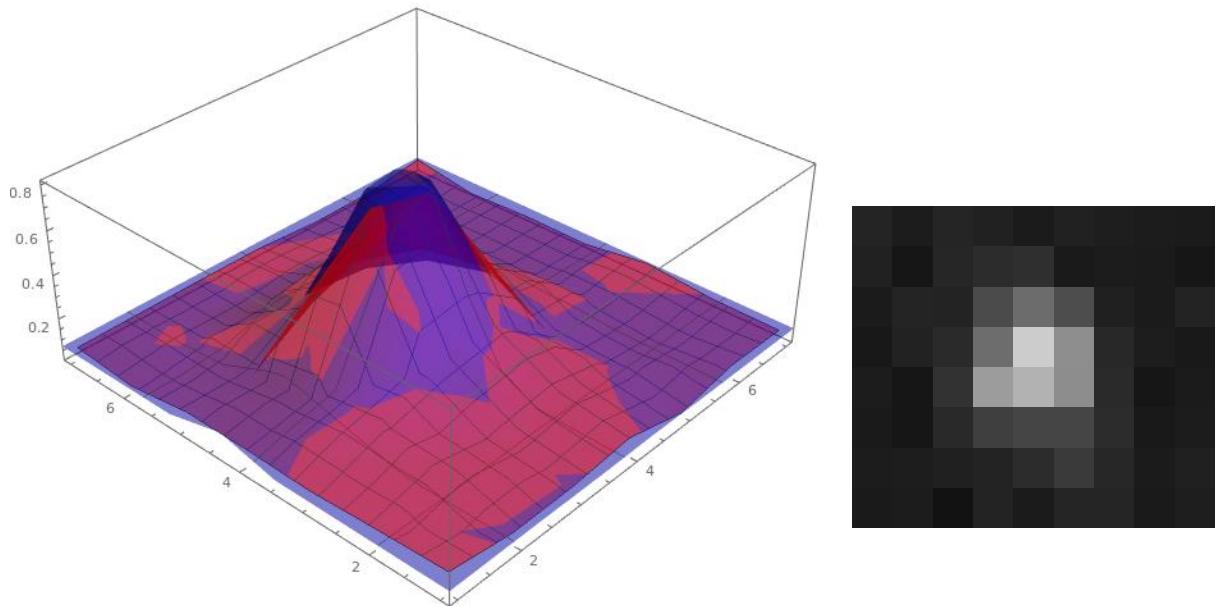
And the procedure is repeated for sufficient values of z to scan at least few Rayleigh ranges. The beam width can be calculated from the scans by fitting the data with [34]

$$P(x, z) = \frac{P_0}{2} \operatorname{erfc} \left[\frac{\sqrt{2}(x - x_0)}{W(z)} \right]. \quad (5.2.1)$$

Where the fitting parameters are P_0 , x_0 , and the width $W(z)$. An example of scan is in figure 5.2.2. The errorbars comes from statistical average, every data point is a mean over 5 measurement, and the error is the standard deviation. The fit in this case gave a width of $3.47 \pm 0.06 \mu\text{m}$, the smallest width obtained with this method. Unfortunately, it is broader than the initial expectations. Furthermore, the profile $W(z)$ did not look symmetric and could not be fitted with equation (2.4.3). A possible explanation is that this method is not suitable for measuring micrometer waists with a razor blade, the roughness of the surface could limit the result. In comparison, authors of [35] have used, instead of a common razor blade, a glass substrate etched with an effective knife-edge feature.

5.2.2 Waist: Camera

Since the Knife-Edge method did not demonstrate particularly effective, if not to give an upper bound to the waist, a more direct approach has been subsequently adopted. We look directly into the beam with a camera from IDS model UI-1490LE-M-GL. This particular camera has a pixel size of $1.6 \mu\text{m}$, with no pixel-pixel distance. It should therefore be suitable to measure a focus spot better than the razor blade. A μm focus should hit one single pixel, and if aligned between two pixels, a Gaussian profile could also be fitted. In addition, unlike the Knife-Edge technique, a camera provides 2-dimensional information about the beam shape and can be exploited to look for aberrations in the system. The setup is almost the same as figure 5.2.1, but the camera now replaces the razor blade, and there is no need for scanning in the x direction, as the z is enough to reconstruct the profile $W(z)$. An additional gradient filter was used to optimize the light reaching the



(a) Fitted data from the camera. In red color, the normalized pixel value is displayed, while the blue curve is a fitted 2D Gaussian. On the axis there is the pixel number

(b) Original photo from the camera.

Figure 5.2.3

camera in order to not saturate it and get a visible signal. The measurement procedure is also similar to the Knife-Edge case. For every desired z displacement, a photo with the camera is taken, post processed, and then the camera is displaced to the new z coordinate. Post processing is done by fitting the pixel values with a 2-dimensional Gaussian

$$P = A \exp \left\{ -\frac{(x - x_0)^2}{2\sigma_x^2} \right\} \exp \left\{ -\frac{(y - y_0)^2}{2\sigma_y^2} \right\}. \quad (5.2.2)$$

The fit parameters are A, x_0, y_0, σ_x , and σ_y . From the standard deviation σ_x and σ_y the width $W(z)$ in the x and y direction can be determined as $W_x = 2 \cdot 1.6 \cdot \sigma_x$ and respectively $W_y = 2 \cdot 1.6 \cdot \sigma_y$, where $1.6 \mu\text{m}$ is the pixel size. In figure 5.2.3, an example of the measurement taken is displayed. The full profiles $W_x(z)$ and $W_y(z)$ can be found in figure 5.2.4. Even here anomalies can be noticed. The profile is asymmetric and does not follow equation 2.4.3, however a width $< 2.5 \mu\text{m}$ has been measured. There could be some reasons behind this result, in some camera pictures some aberrations were visible. Moreover, some estimation error lead to non ideal placement of the lenses. Nonetheless, the smallest measured waist was satisfactory and enough for proceeding with the installation and doing more advanced experiments. But first few more characteristics of the system had to be tested, namely polarization and stability.

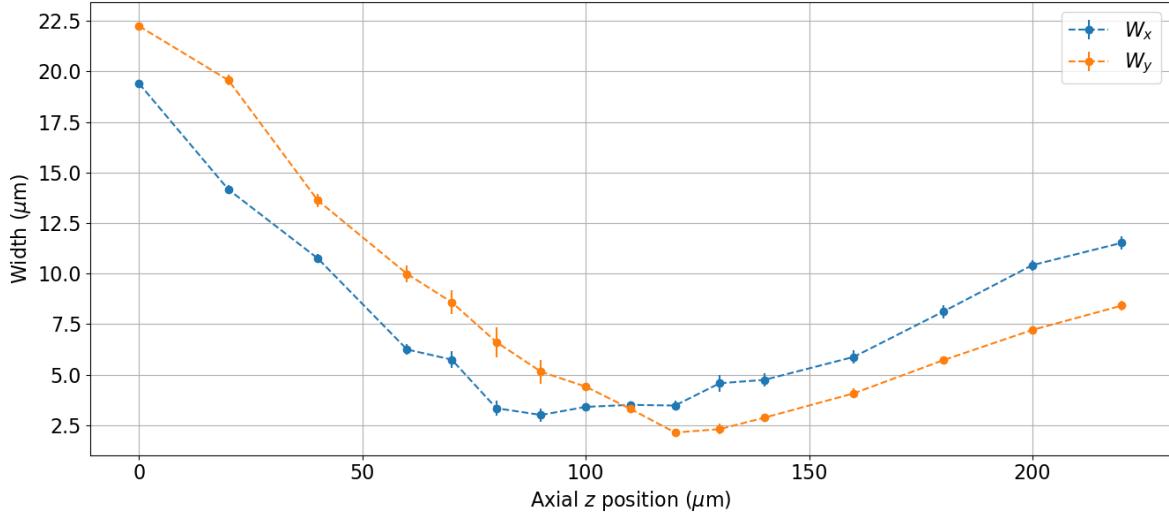


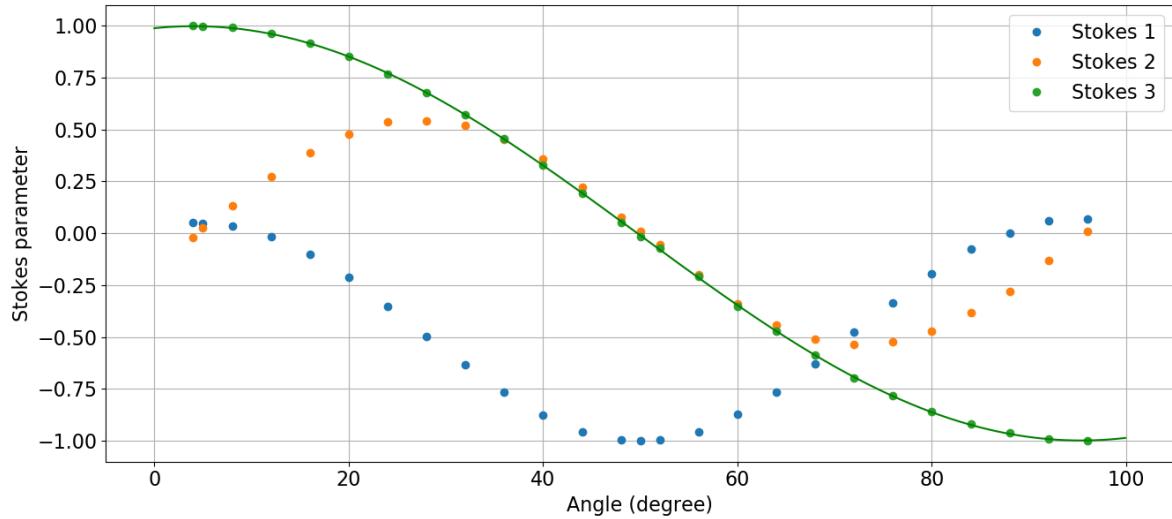
Figure 5.2.4: Profile of the Gaussian beam

5.2.3 Polarization

As discussed in the design section, polarization is an important component of the Raman process, thus the polarization capabilities of the system had to be tested. The goal is to achieve vertical, horizontal, left circular, and right circular polarization at the ion position. Polarization can be changed with two plates: a half wave plate after the AOD, and a quarter wave plate right before the objective, see figure 4.1.1. In order to characterize the polarization, the three Stokes parameters [36] has been measured with a polarimeter from Scäfter + Kirchhoff series SK010PA. Stokes parameters quantify the type of polarization of an electric field. Linear polarized light (vertical and horizontal) has all Stokes parameters set to 0, apart from the first one. Instead, the third parameter, when the others are zero, contains information about circular polarized light which goes from right to left. By rotating a plate and fitting a sine function to the appropriate Stokes parameter, it is possible to gain insights on the appropriate angle to set in order to obtain the desired polarization.

The first step was to characterize the $\lambda/2$ plate alone, the main result from this characterization is that horizontal polarization can be achieved with an angle of $267.2 \pm 0.1^\circ$, and vertical is achieved with an angle of $312.5 \pm 0.1^\circ$ obtained from fitting a sine on the first Stokes parameter. From the same fit, the semiperiod of the polarization is $45.3 \pm 0.6^\circ$. As the mirror can change the polarization, the same characterization has been done after the mirror finding that the polarization is altered unless it is either horizontal or vertical. However the main result was obtained when the $\lambda/4$ was characterized. With every plate inserted, two measurements were made. In the first one the $\lambda/2$ was set to 267° to get horizontal polarization, and the angle of the $\lambda/4$ scanned. This result is presented in figure 5.2.5. The third Stokes parameter is fitted with a sine function to get the angles at which the polarization is right and left circular. The right circular polarization is obtained at the maximum of the curve, while the left corresponds to the minimum. Moreover, when the third Stokes parameter is zero, the polarization results linear. The results are shown in table 5.2.1. The second measurement also scanned the angle of the $\lambda/4$ plate, but this time the $\lambda/2$ was set to 312° such that the polarization before the $\lambda/4$ plate was vertical. In figure 5.2.6 the data is displayed. Again, to get the angle for the different polarizations,

Polarization	$\lambda/2$ ($^{\circ}$)	$\lambda/4$ ($^{\circ}$)
Horizontal	267.2 ± 0.1	49.7 ± 0.1
Vertical	312.5 ± 0.1	48.1 ± 0.1
Right circular	267.2 ± 0.1	4 ± 0.1
Right circular	312.5 ± 0.1	93.1 ± 0.1
Left circular	267.2 ± 0.1	95.4 ± 0.1
Left circular	312.5 ± 0.1	3.1 ± 0.1

Table 5.2.1: Angles**Figure 5.2.5:** Polarization after the objective as a function of the $\lambda/4$ angle with $\lambda/2$ set to horizontal (267°). Green line is a sine function fit.

a sine function was fitted to the third Stokes parameter. The results yielded by the fit are summarized in table 5.2.1.

5.2.4 Stability

In the future the addressing system will be used for long experiments, it is therefore imperative to know the stability of the system in terms of polarization and beam pointing. This means knowing over the course of hours or days if the setup needs to be calibrated. Let us start with polarization stability, the polarization was measured with a polarimeter from Scäfter + Kirchhoff series SK010PA after the objective. The polarization was set to be right circular: $\lambda/2$ set to 267° , and $\lambda/4$ set to 4° . We recorded the three Stokes parameters for a total of one hour, this data is plotted in figure 5.2.7. To the third parameter, 0.998 has been subtracted during the plot such that it would fit with the others. It can be seen that the polarization is stable over a period of one hour.

Beam pointing stability regards the stability of the focus position, which could drift in any direction for any reason. To test the stability, we recorded the position of the focus for a period of one hour with the camera IDS model UI-1490LE-M-GL. The camera was positioned at the focus with the same setup discussed in section 5.2.2, and then a video

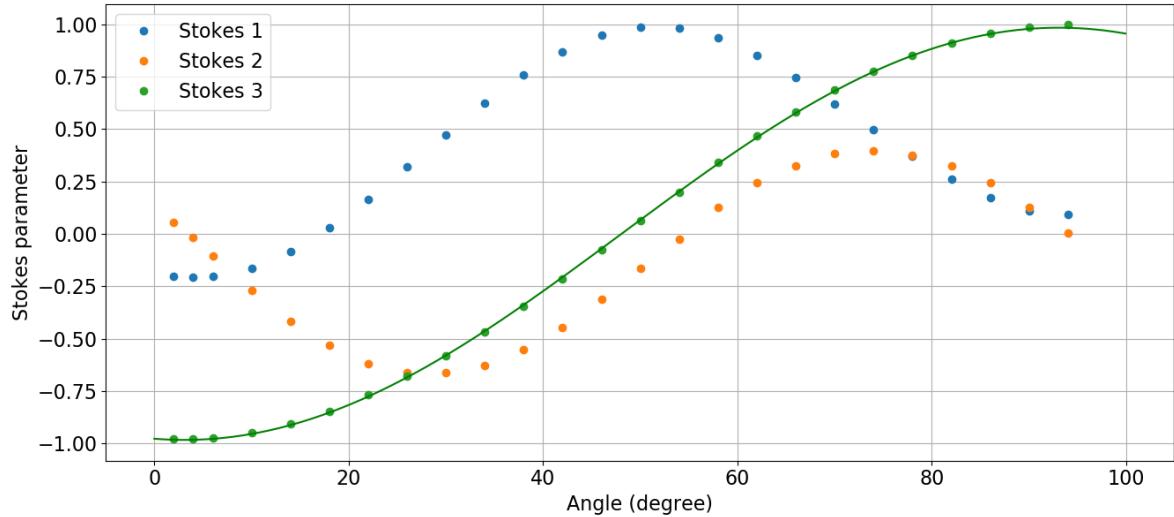


Figure 5.2.6: Polarization after the objective as a function of the $\lambda/4$ angle with $\lambda/2$ set to vertical (314°). Green line is a sine function fit.

was recorded. The video was later analyzed by tracking the the brightest pixel over time. In figure 5.2.8 we can see the horizontal x and vertical y position of such pixel. In the horizontal directions, fluctuations of one single pixel can be noticed, which could be a result of the light hitting between two pixels. In the vertical direction over it looks like the fluctuations are on the order of two pixels, if one consider one pixel a normal fluctuation, then the position might have shifted by one pixel over this period. This means that the focus position is stable within $1.6 \mu\text{m}/\text{hour}$.

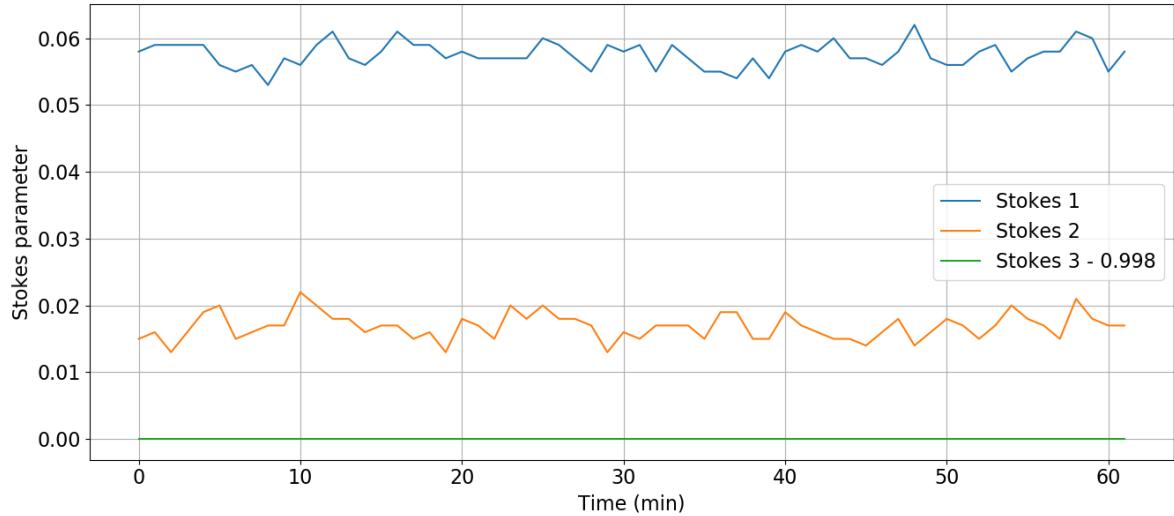


Figure 5.2.7: Right circular polarization stability over a period of one hour.

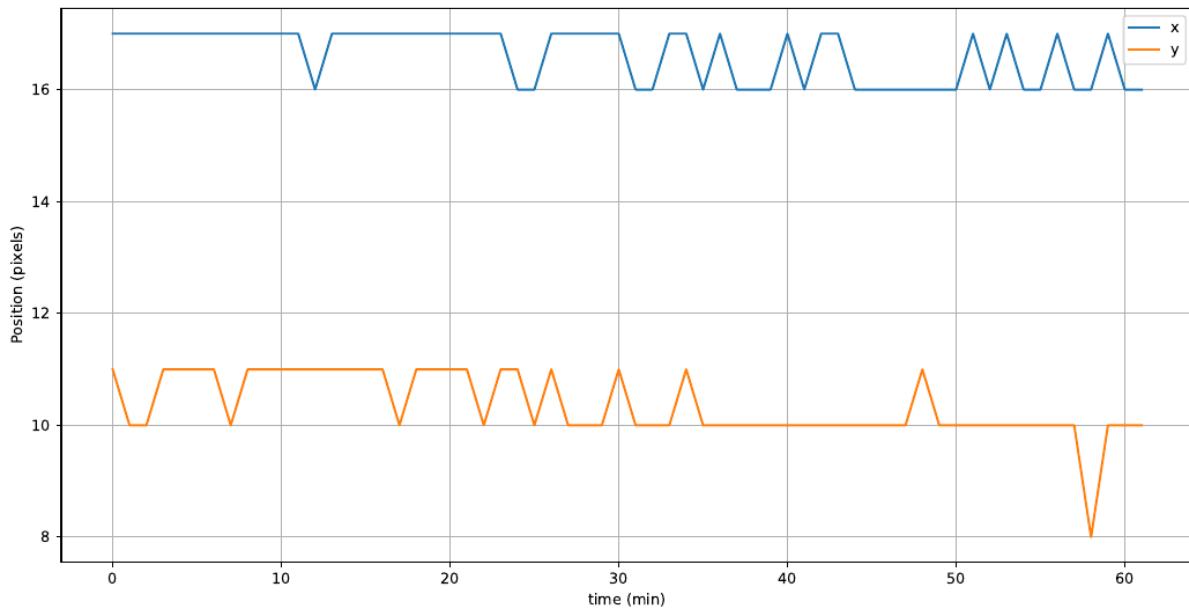


Figure 5.2.8: Beam pointing stability over a period of one hour.

5.3 Final installed system

5.3.1 Ramsey interferometry

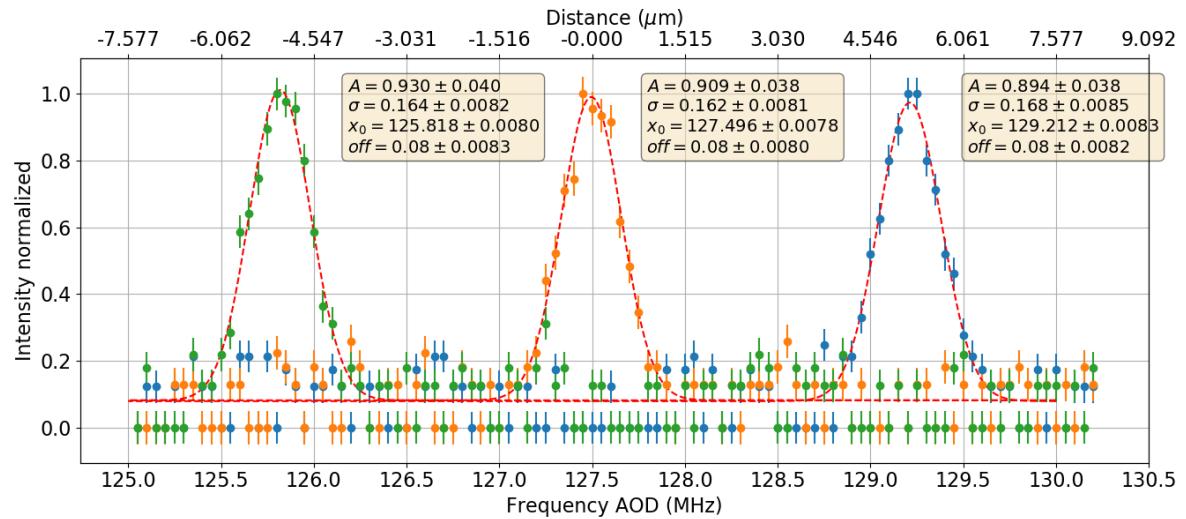


Figure 5.3.1: 3 ions scanned

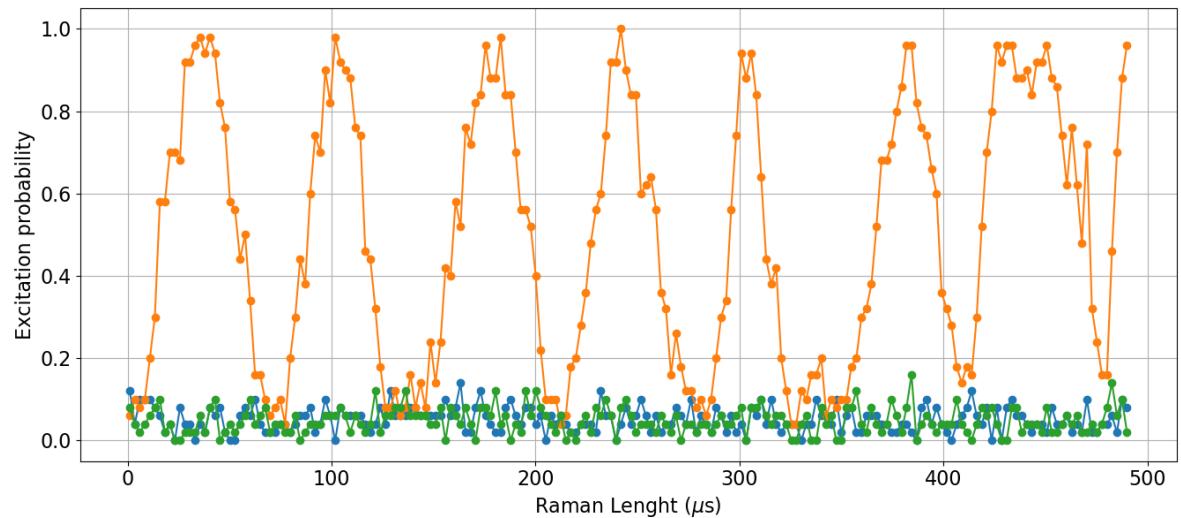


Figure 5.3.2: 393nm AC-Stark flops

5.3.2 Photons production

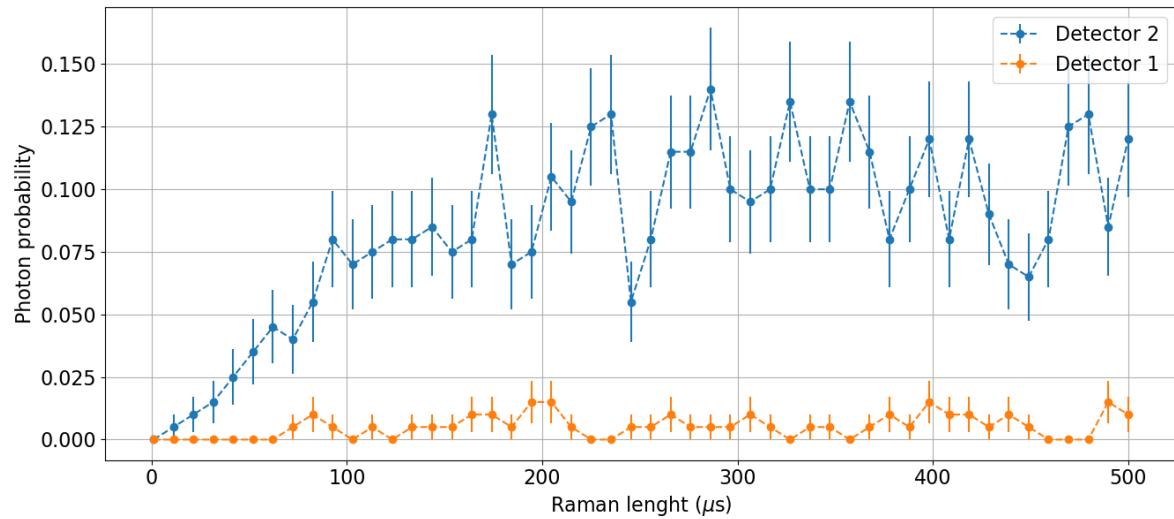


Figure 5.3.3: Generated photon efficiency

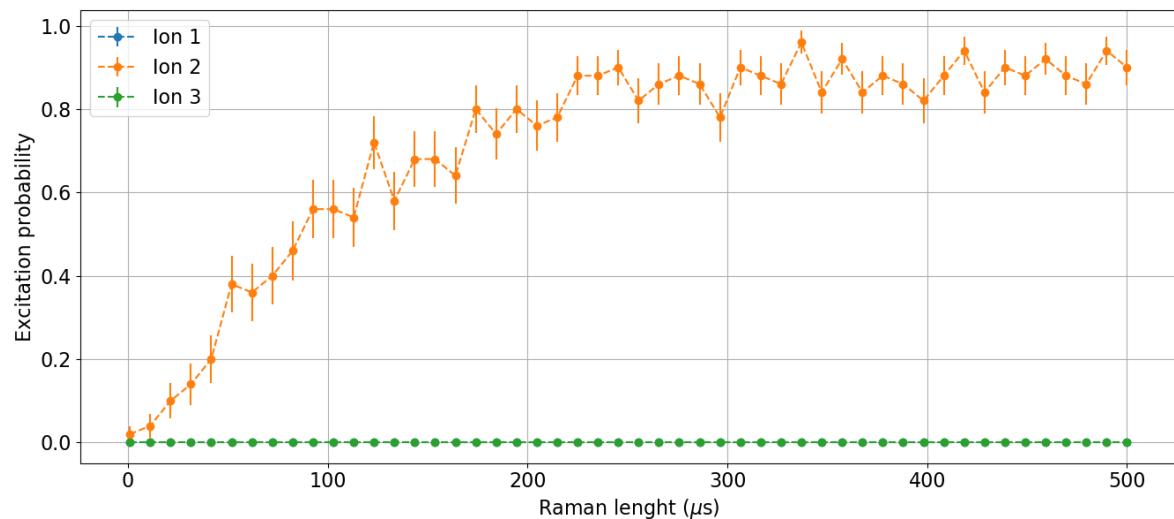


Figure 5.3.4: Excitation of ion while emitting photon

- g2 plot?

5.4 Final properties summary

Chapter 6

Conclusions and outlook

- Usual conclusions

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Appendix

- Error analysis? Maximum likelihood estimation?