

# Global Sensitivity Analysis (GSA)

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# SENSITIVITY ANALYSIS

**Sensitivity Analysis** provides a means to quantify the **relative** importance of inputs to the variability in a system response or a model output.

$$\mathcal{Q} = f(\theta_1, \dots, \theta_p)$$

- ▶  $\theta_i$ 's are uncertain
- ▶  $p$  can be large
- ▶ Higher the sensitivity index, more important is the input

**Applications:** Model verification, dimension reduction, model reliability, optimal experimental design

# H<sub>2</sub>/O<sub>2</sub> REACTION KINETICS

- Clean energy source for transportation, fuel cells

- Reaction Rate:

$$k_i(T) = A_i T^{n_i} \exp(-E_{a,i}/RT)$$

$A_i$ : Pre-exponent  $E_{a,i}$ : Activation Energy

- Initial conditions:  $P_0, T_0, \phi_0$

- **Research Interests:** Uncertainty propagation, reduction, design

- GSA plays a **critical** role!

Reaction #	Reactants	Products
$\mathcal{R}_1$	$\text{H} + \text{O}_2$	$\rightleftharpoons \text{O} + \text{OH}$
$\mathcal{R}_2$	$\text{O} + \text{H}_2$	$\rightleftharpoons \text{H} + \text{OH}$
$\mathcal{R}_3$	$\text{H}_2 + \text{OH}$	$\rightleftharpoons \text{H}_2\text{O} + \text{H}$
$\mathcal{R}_4$	$\text{OH} + \text{OH}$	$\rightleftharpoons \text{O} + \text{H}_2\text{O}$
$\mathcal{R}_5$	$\text{H}_2 + \text{M}$	$\rightleftharpoons \text{H} + \text{H} + \text{M}$
$\mathcal{R}_6$	$\text{O} + \text{O} + \text{M}$	$\rightleftharpoons \text{O}_2 + \text{M}$
$\mathcal{R}_7$	$\text{O} + \text{H} + \text{M}$	$\rightleftharpoons \text{OH} + \text{M}$
$\mathcal{R}_8$	$\text{H} + \text{OH} + \text{M}$	$\rightleftharpoons \text{H}_2\text{O} + \text{M}$
$\mathcal{R}_9$	$\text{H} + \text{O}_2 + \text{M}$	$\rightleftharpoons \text{HO}_2 + \text{M}$
$\mathcal{R}_{10}$	$\text{HO}_2 + \text{H}$	$\rightleftharpoons \text{H}_2 + \text{O}_2$
$\mathcal{R}_{11}$	$\text{HO}_2 + \text{H}$	$\rightleftharpoons \text{OH} + \text{OH}$
$\mathcal{R}_{12}$	$\text{HO}_2 + \text{O}$	$\rightleftharpoons \text{O}_2 + \text{OH}$
$\mathcal{R}_{13}$	$\text{HO}_2 + \text{OH}$	$\rightleftharpoons \text{H}_2\text{O} + \text{O}_2$
$\mathcal{R}_{14}$	$\text{HO}_2 + \text{HO}_2$	$\rightleftharpoons \text{H}_2\text{O}_2 + \text{O}_2$
$\mathcal{R}_{15}$	$\text{H}_2\text{O}_2 + \text{M}$	$\rightleftharpoons \text{OH} + \text{OH} + \text{M}$
$\mathcal{R}_{16}$	$\text{H}_2\text{O}_2 + \text{H}$	$\rightleftharpoons \text{H}_2\text{O} + \text{OH}$
$\mathcal{R}_{17}$	$\text{H}_2\text{O}_2 + \text{H}$	$\rightleftharpoons \text{HO}_2 + \text{H}_2$
$\mathcal{R}_{18}$	$\text{H}_2\text{O}_2 + \text{O}$	$\rightleftharpoons \text{OH} + \text{HO}_2$
$\mathcal{R}_{19}$	$\text{H}_2\text{O}_2 + \text{OH}$	$\rightleftharpoons \text{HO}_2 + \text{H}_2\text{O}$

[Yetter et al., 1991]



# ESTIMATION OF SENSITIVITY MEASURES

- **Sampling-based**

- ▶ Morris Screening: Trajectory-based sampling
  - ▶ Sobol' indices: Monte Carlo Sampling

- **Surrogate-based**

- ▶ Polynomial Chaos Expansion (PCE)

- **Dimension reduction:** Reduced-space Surrogates

- ▶ Derivative-based global sensitivity measures (DGSMs)
  - ▶ Active subspaces → Activity scores

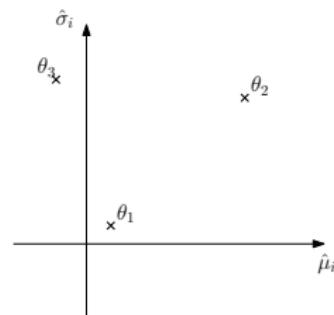
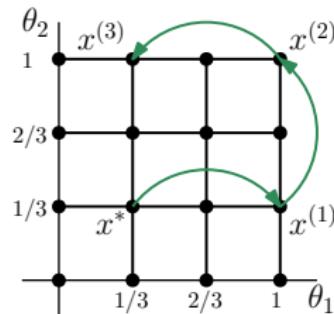
# MORRIS SCREENING

- Trajectory-based sampling approach is adopted

- Elementary effect of  $\theta_i$  at  $x^{(j)}$ :

$$d_{\theta_i}(x^{(j)}) = \frac{\mathcal{M}(x_1^{(j)}, \dots, x_i^{(j)} + \Delta, \dots, x_m^{(j)}) - \mathcal{M}(x^{(j)})}{\Delta}$$

- Mean and variance of the distribution of  $d_{\theta_i}(x^{(j)})$  is examined





# SOBOL' SENSITIVITY INDICES

- Consider the variance of  $f$ :

$$\begin{aligned}\mathbb{V}(f) &= \int (f - f_0)^2 d\boldsymbol{\theta} = \int f^2 d\boldsymbol{\theta} - f_0^2 \\ &= \underbrace{\int f_1^2 d\boldsymbol{\theta}}_{\mathbb{V}(f_1)} + \underbrace{\int f_2^2 d\boldsymbol{\theta}}_{\mathbb{V}(f_2)} + \underbrace{\int f_{12}^2 d\boldsymbol{\theta}}_{\mathbb{V}(f_{12})}\end{aligned}$$

- First-order or Main-effect index ( $S_i$ ):**

$$S_i = \frac{\mathbb{V}(f_1)}{\mathbb{V}(f)} = \frac{\overbrace{\mathbb{V}(\mathbb{E}[f|\theta_i])}^{\text{contribution due to } \theta_i}}{\mathbb{V}(f)}$$

- Total-effect index ( $S_{T_i}$ ):**

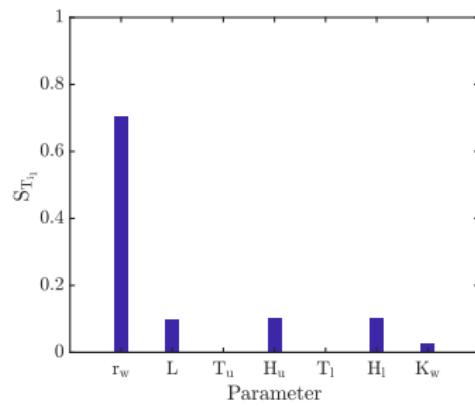
$$S_{T_i} = \frac{\mathbb{V}(f_1) + \mathbb{V}(f_{12})}{\mathbb{V}(f)} = \frac{\mathbb{V}(f) - \mathbb{V}(f_2)}{\mathbb{V}(f)} = 1 - \frac{\mathbb{V}(f_2)}{\mathbb{V}(f)} = 1 - \frac{\overbrace{\mathbb{V}(\mathbb{E}[f|\theta_{\sim i}])}^{\text{contribution due to } \theta_{\sim i}}}{\mathbb{V}(f)}$$



# THE BOREHOLE FUNCTION

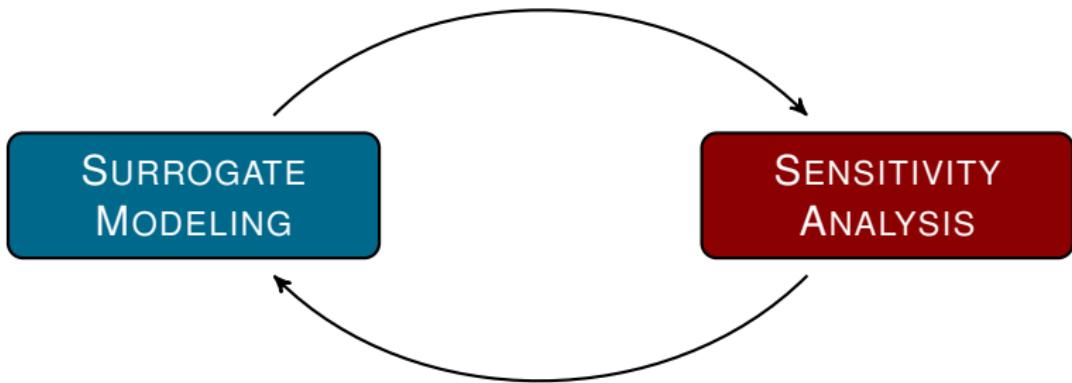
$$\begin{aligned} \mathcal{Q} &= \frac{2\pi T_u (H_u - H_l)}{\ln(r/r_w) \left[ 1 + \frac{2LT_u}{\ln(r/r_w)r_w^2 K_w} + \frac{T_u}{T_l} \right]} \\ \boldsymbol{\theta} &= [r_w \quad L \quad T_u \quad H_u \quad T_l \quad H_l \quad K_w]^T \end{aligned}$$

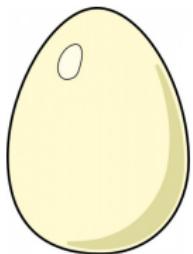
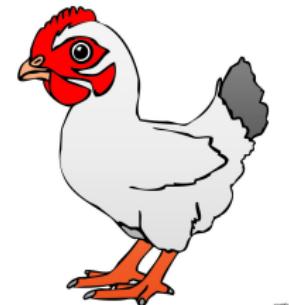
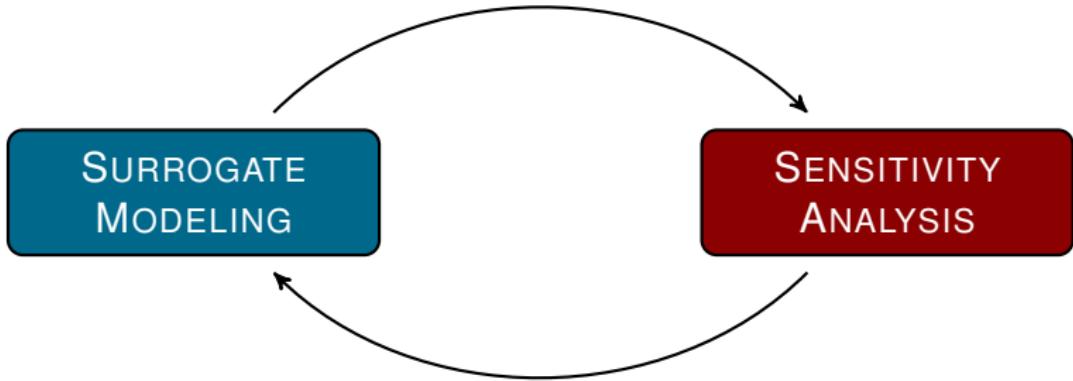
Parameter	Distribution
Borehole radius, $r_w$ (m)	$\mathcal{N}(0.1, 0.016)$
Borehole length, $L$ (m)	$\mathcal{U}[1120, 1680]$
Transmissivity, $T_u$ ( $m^2/yr$ )	$\mathcal{U}[63070, 115600]$
Potentiometric head, $H_u$ (m)	$\mathcal{U}[990, 1110]$
Transmissivity, $T_l$ ( $m^2/yr$ )	$\mathcal{U}[63, 1, 116]$
Potentiometric head, $H_l$ (m)	$\mathcal{U}[700, 820]$
Hydraulic conductivity, $K_w$ ( $m/yr$ )	$\mathcal{U}[9855, 12045]$











# DERIVATIVE-BASED GLOBAL SENSITIVITY MEASURES (DGSMs)

- DGSM for a parameter,  $\theta_i$ :

$$\mu_i = \mathbb{E} \left[ \left( \frac{\partial G(\theta)}{\partial \theta_i} \right)^2 \right]$$

[Sobol' and Kucherenko, 2009]

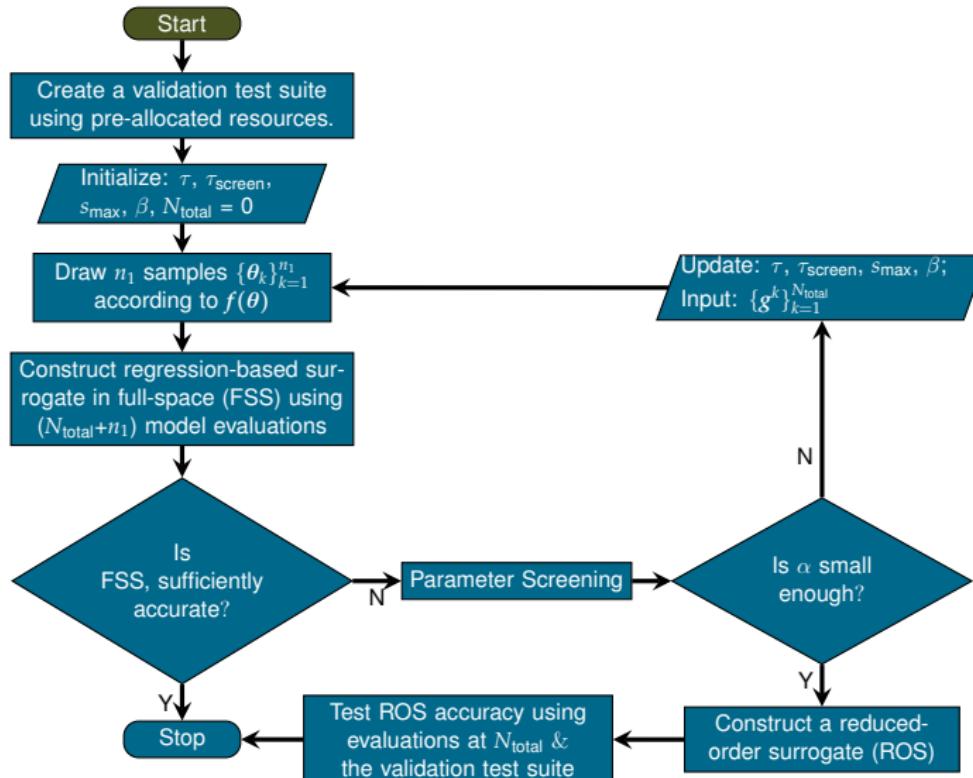
- Upper bound on  $S_{T_{i_1}}$ :

$$S_{T_i} \leq \frac{c_i \mu_i}{\mathbb{V}(G)}, c_i: \text{Poincaré Constant}$$

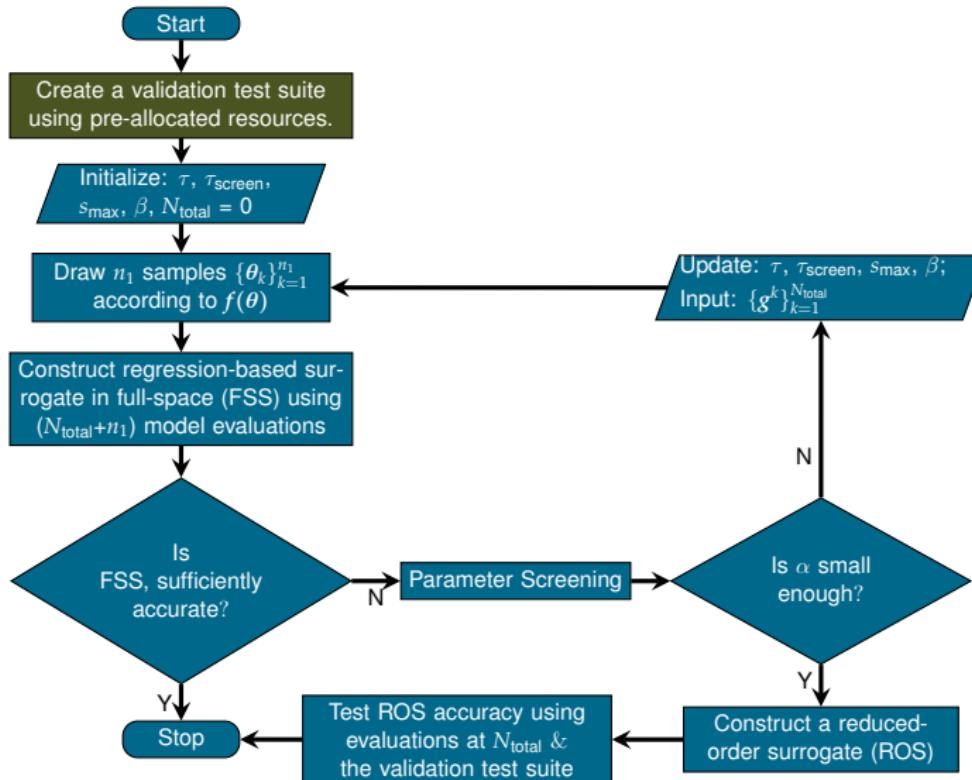
[Lamboni et al., 2013]

- Typically, fewer samples are needed to converge to the upper bound.
- **Limitation:** Need gradient information

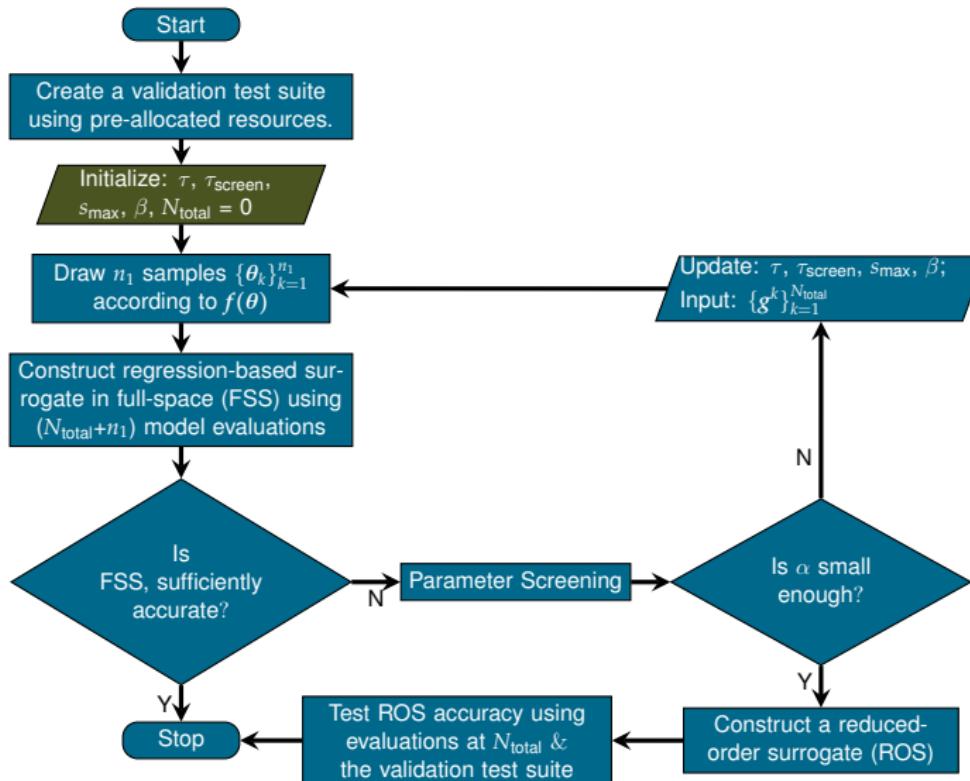
# ADAPTIVE SURROGATE CONSTRUCTION



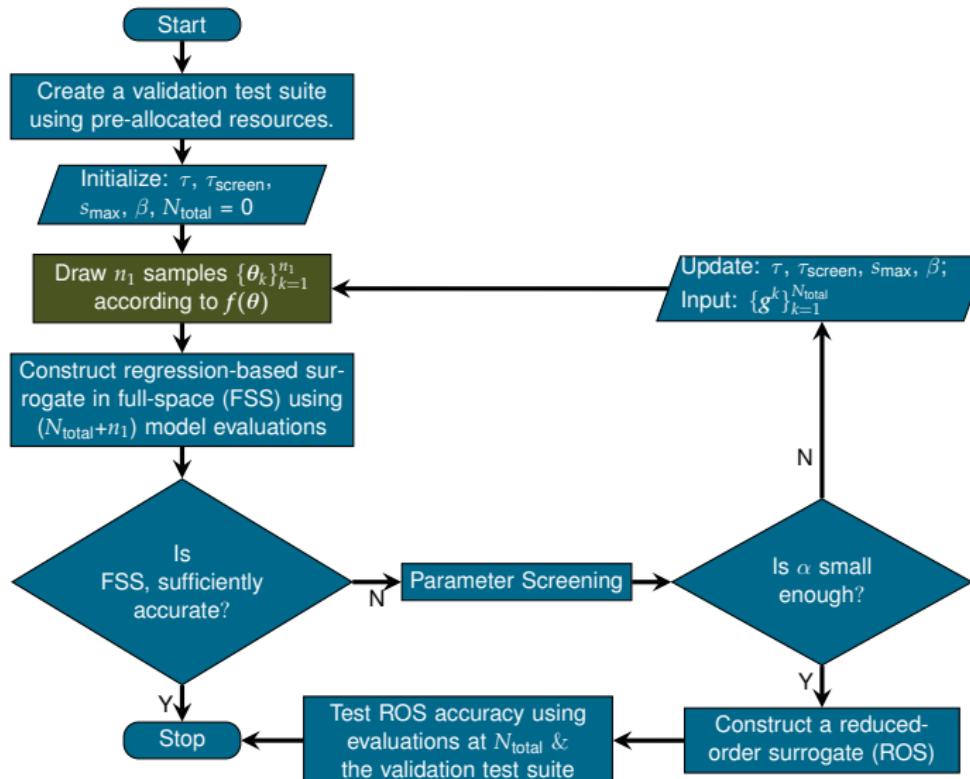
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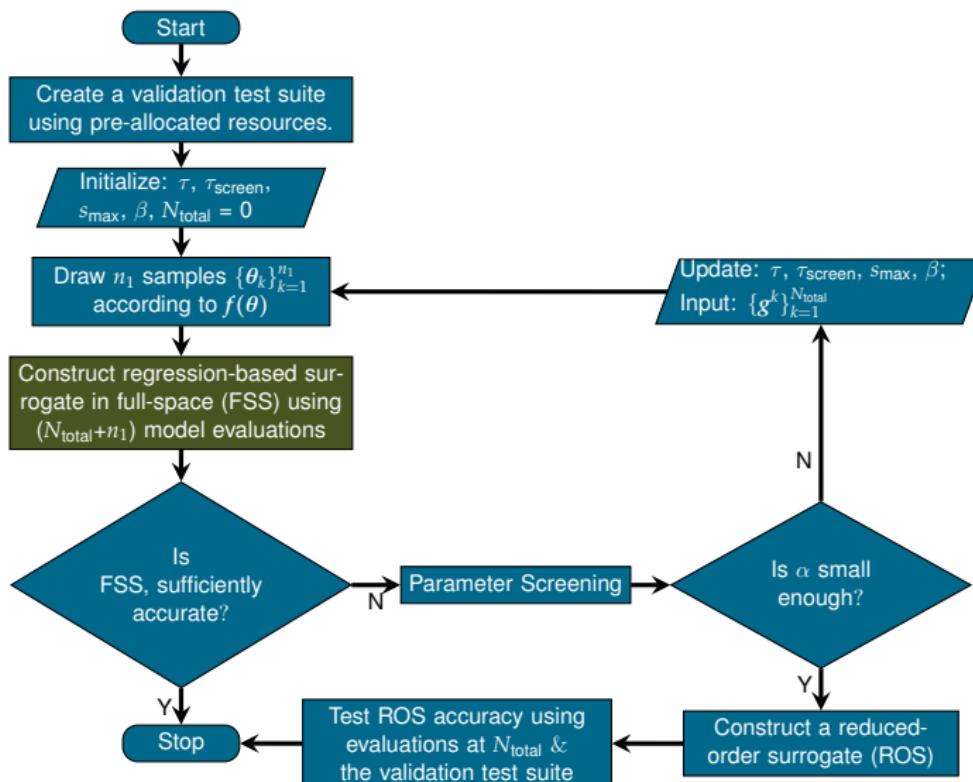
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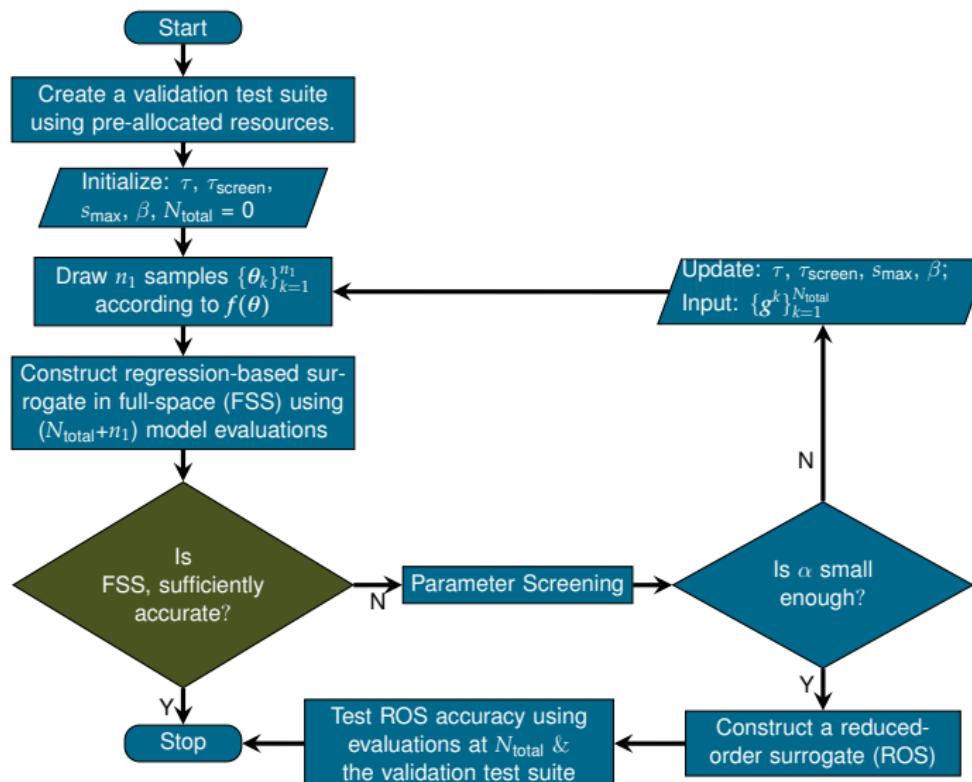
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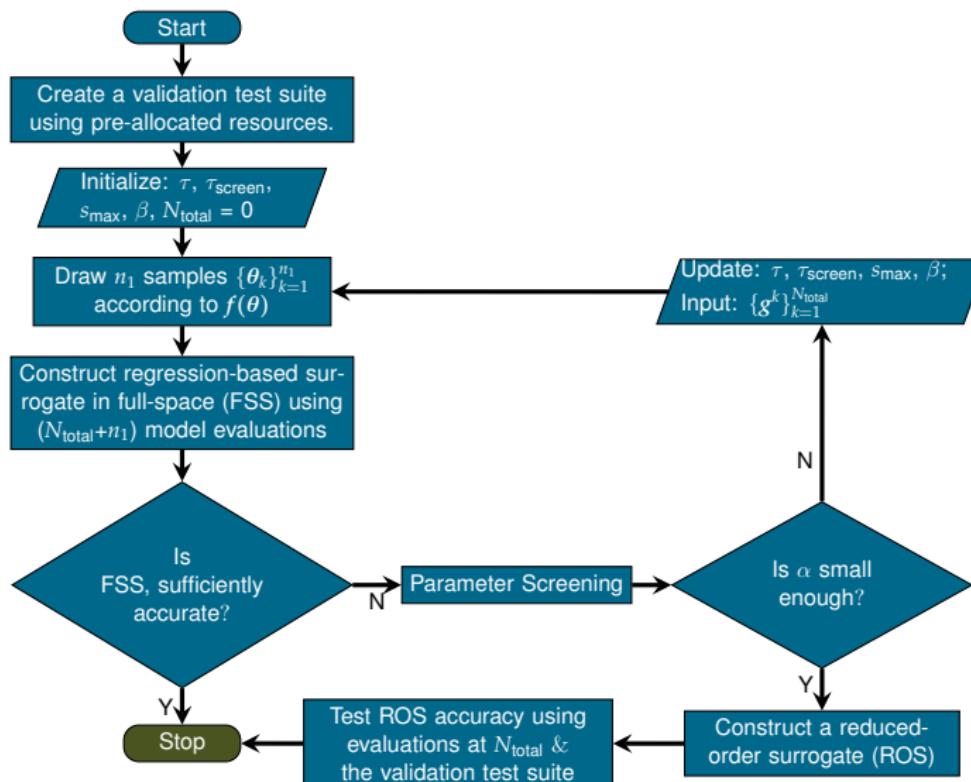
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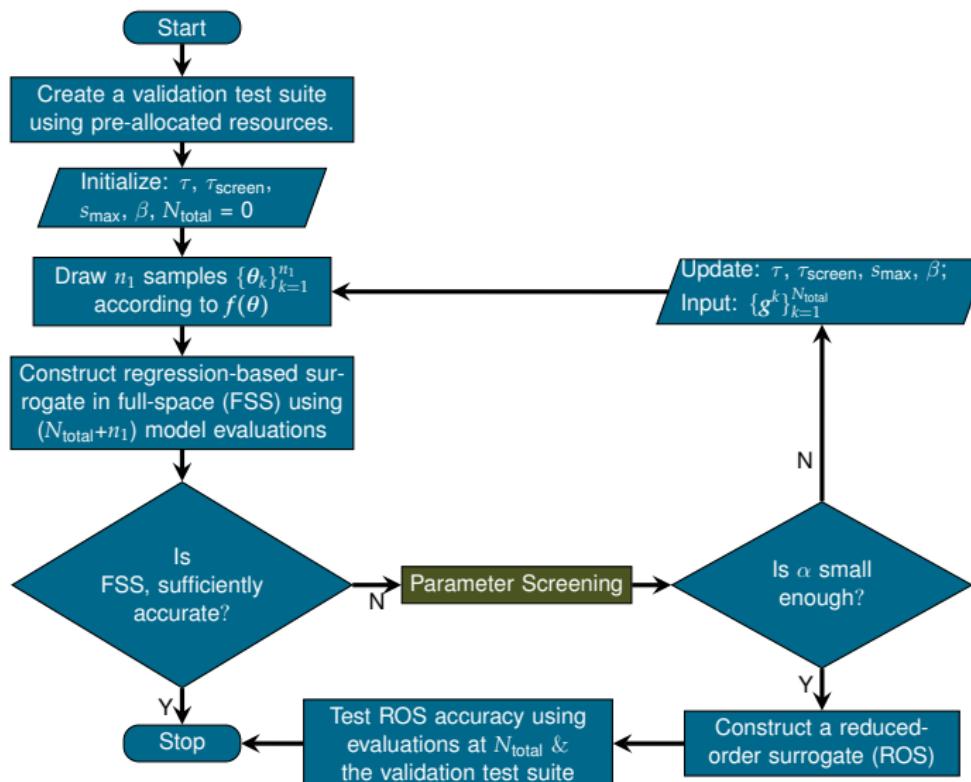
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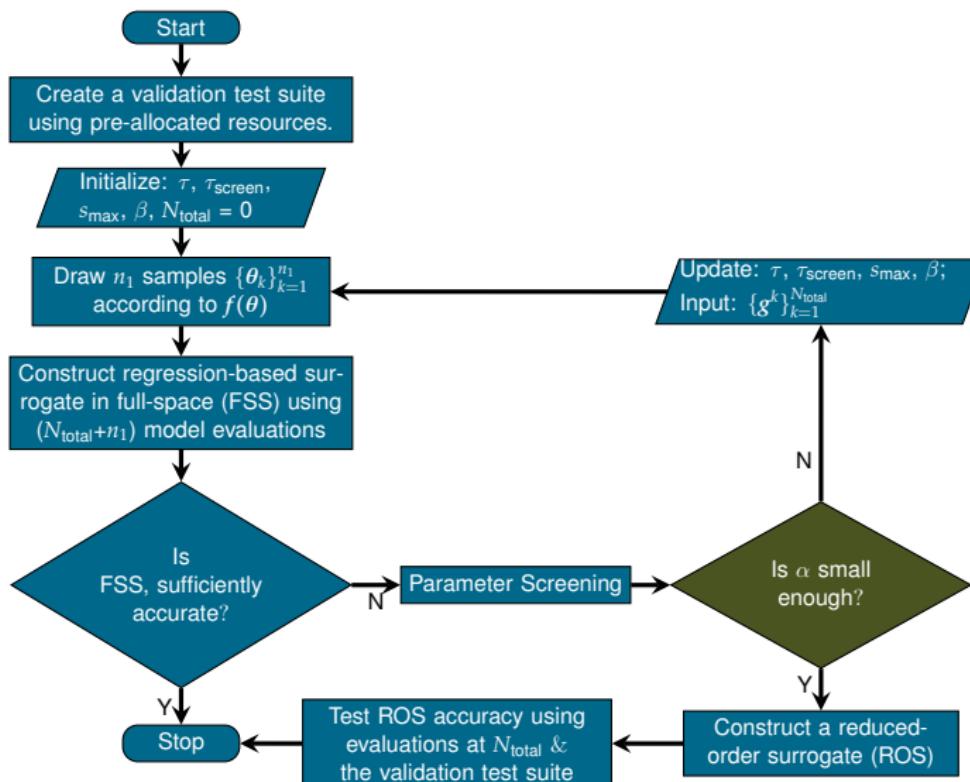
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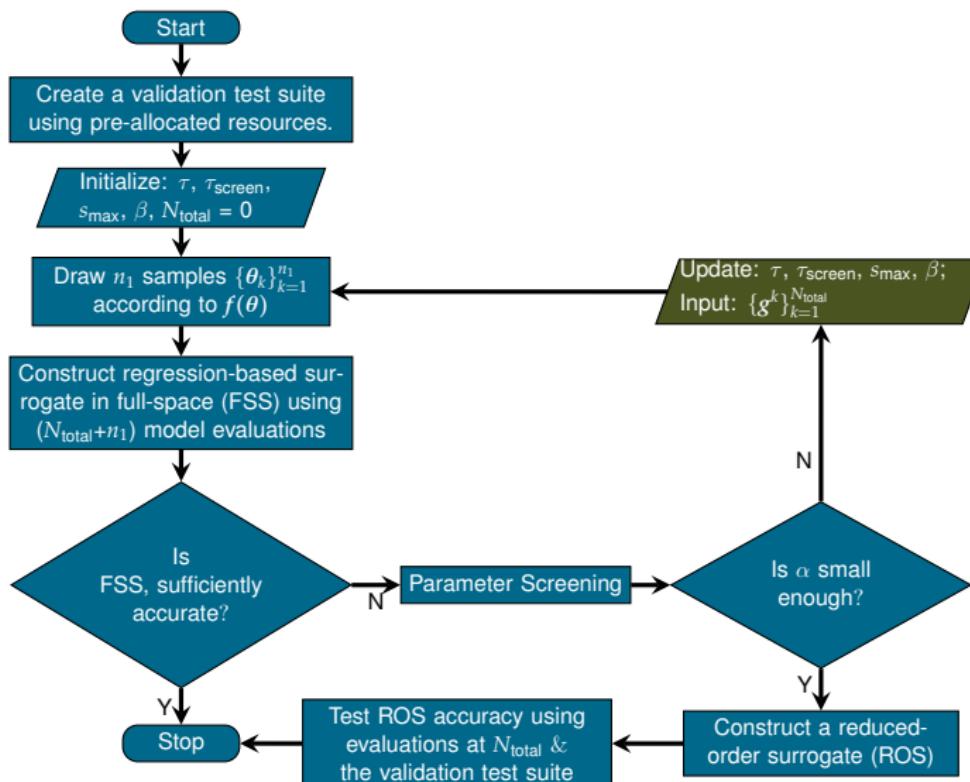
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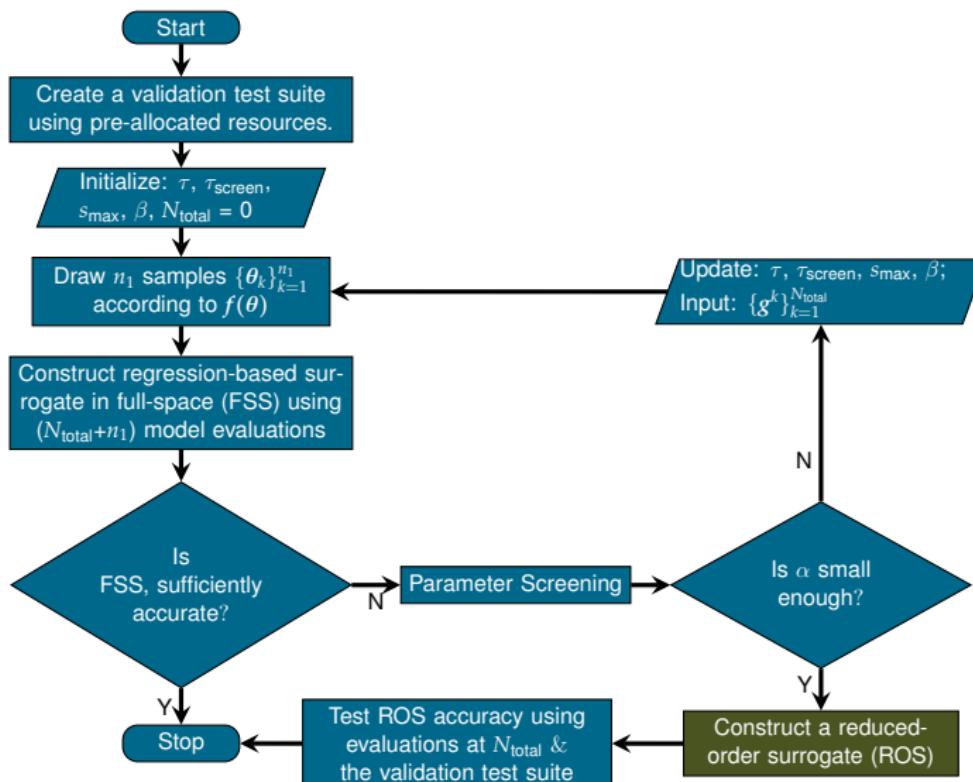
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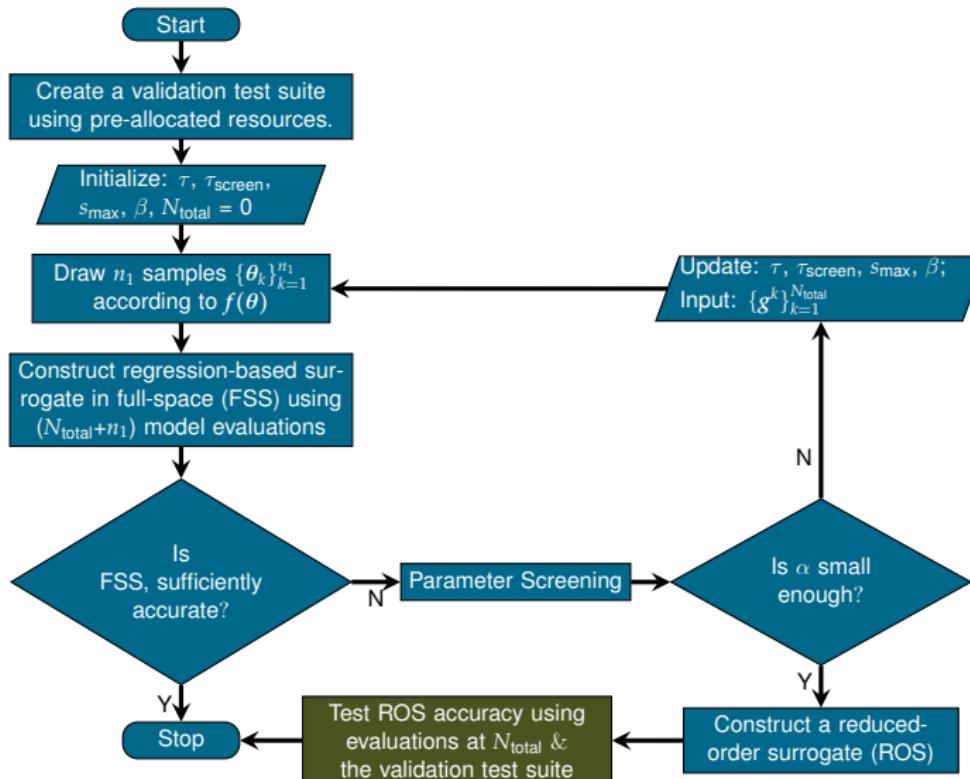
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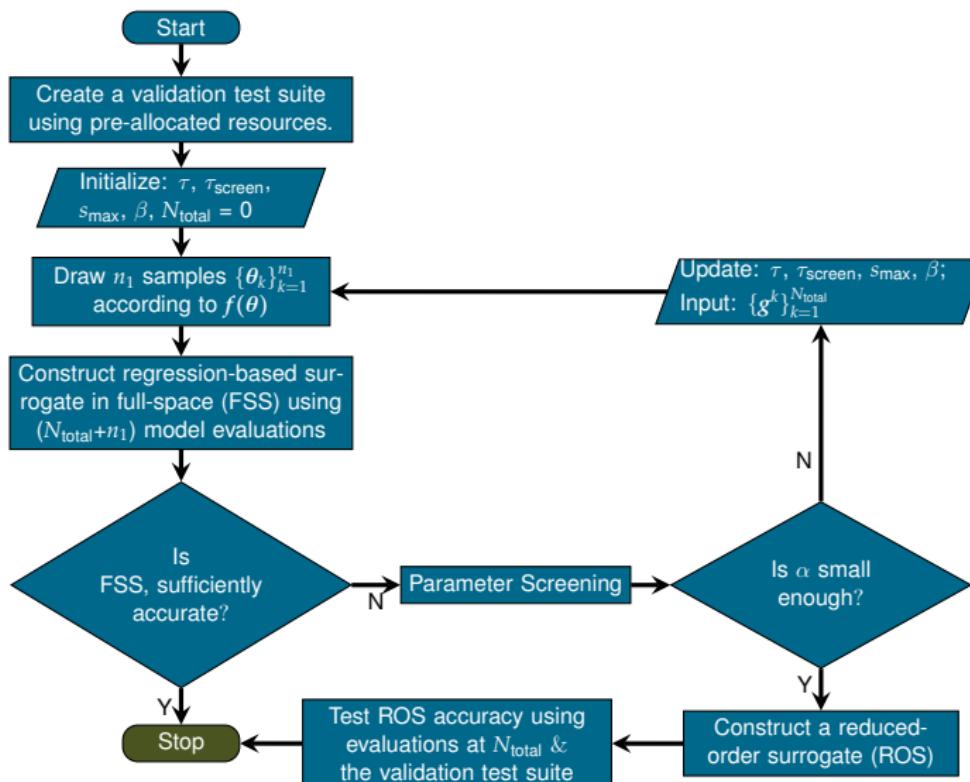
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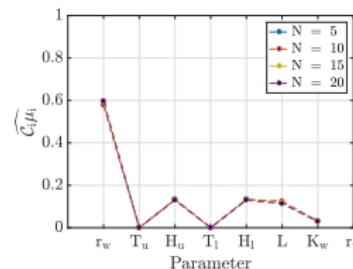
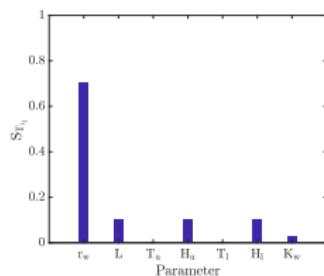


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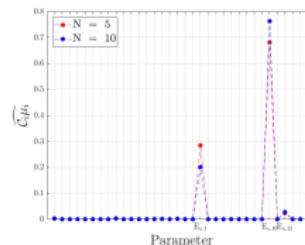
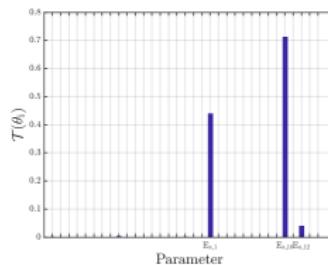


# APPLICATIONS

## ■ Borehole function



## ■ Chemical Kinetics: $\text{H}_2/\text{O}_2$ Reaction Mechanism



# ACTIVITY SCORES

- Consider a positive semi-definite matrix,  $C$ :

$$C = \int_{\Omega} (\nabla_{\xi} G)(\nabla_{\xi} G)^{\top} dP_{\xi}$$

- Eigenvalue decomposition of  $C$ :

$$C = W \Lambda W^{\top}$$

- Partition the eigenspace:

$$W = [W_1 \ W_2], \quad \Lambda = \begin{bmatrix} \Lambda_1 & \\ & \Lambda_2. \end{bmatrix}$$

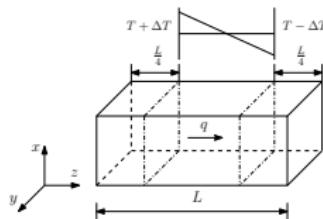
- Activity score for parameter,  $\theta_i$ :

$$\nu_{i,p}(G) = \sum_{j=1}^p \lambda_j w_{i,j}^2$$



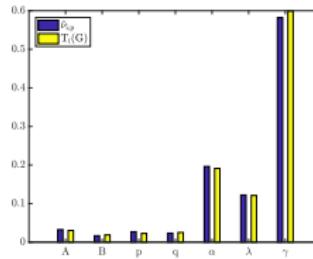
# APPLICATIONS

- Thermal transport in Si using Non-equilibrium Molecular Dynamics (NEMD)



$$\text{SW Potential, } \Phi = \sum_{i,j(i < j)} \phi_2(A, B, p, q, \alpha) + \sum_{i,j,k(i < j < k)} \phi_3(\lambda, \gamma)$$

- GSA of the SW parameters



M. Vohra, S. Mahadevan, *International Journal of Heat and Mass Transfer*, 2019

# PROBABILITY MODELS: GSA

- Variance decomposition methods assume independence

$$S_{i_c} = \frac{\mathbb{V}_{\boldsymbol{\theta}_c} [\mathbb{E}[f|\boldsymbol{\theta}_c]]}{\mathbb{V}(f)}$$

$$S_{T_{i_c}} = 1 - \frac{\mathbb{V}_{\boldsymbol{\theta}_r} [\mathbb{E}[f|\boldsymbol{\theta}_r]]}{\mathbb{V}(f)}  
\boldsymbol{\theta} : (\boldsymbol{\theta}_c, \boldsymbol{\theta}_r)$$

- Conditional expectation,  $\mathbb{E}[f|\boldsymbol{\theta}_c]$ :

$$\mathbb{E}[f|\boldsymbol{\theta}_c] = \int_{\Omega_f} f p(f|\boldsymbol{\theta}_c) df = \int_{\Omega_f} f \frac{p(\boldsymbol{\theta}_c, f)}{p(\boldsymbol{\theta}_c)} df$$



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## GAUSSIAN COPULA

$$p(\boldsymbol{\theta}_c, f) = \mathcal{C} \left( p_f \prod_{i=1}^{n(\boldsymbol{\theta}_c)} p_{\theta_i} \right)$$

## GAUSSIAN MIXTURE MODEL

$$p(f|\boldsymbol{\theta}_c) = \sum_{i=1}^{n(\boldsymbol{\theta}_c)} \lambda_i(\boldsymbol{\theta}_c) \phi(f, \boldsymbol{\mu}_i, \Sigma_i)$$

