

Steady State Error & System Type

$$\text{Recall } D(s)G(s) = \frac{K \prod_{i=1}^n (1 + T_i s)}{s^j \prod_{k=j+1}^n (1 + T_k s)}$$

where  $j$  is the system type

Example : Step input of Amplitude  $A$

$$R(s) = \frac{A}{s}$$

$$E(s) = \frac{1}{1+D(s)} R(s)$$

$$e_{ss} = \lim_{s \rightarrow 0} s E(s)$$

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{1}{1+D(s)} \cdot \frac{A}{s}$$

$$= \lim_{s \rightarrow 0} \frac{A}{1+D(s)}$$

$$= \frac{A}{1 + \lim_{s \rightarrow 0} D(s)} \quad \& \quad \lim_{s \rightarrow 0} D(s)G(s) = \begin{cases} K_p & j=0 \\ \infty & j>0 \end{cases}$$

$$\therefore e_{ss} = \begin{cases} A/(1+K_p) & j=0 \\ 0 & j \geq 1 \end{cases}$$

Ex velocity / ramp input

$$R(s) = \frac{A}{s^2}$$

$$\text{Find } e_{ss} = \lim_{s \rightarrow 0} s \frac{1}{1+D(s)} \cdot \frac{A}{s^2} \rightarrow$$

$$e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s + SDG(s)}$$

$$= \frac{A}{\lim_{s \rightarrow 0} s + \lim_{s \rightarrow 0} SDG(s)}$$

$$\lim_{s \rightarrow 0} SDG(s) = \begin{cases} \infty & j=0 \\ K_v & j=1 \\ \infty & j \geq 2 \end{cases}$$

$$\Rightarrow e_{ss} = \begin{cases} \infty & j=0 \\ 1/K_v & j=1 \\ 0 & j \geq 2 \end{cases}$$

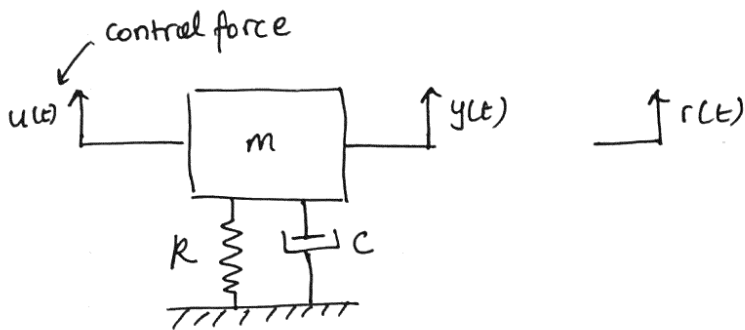
Note: The power of the denominator of the input gives the bounds for the system type that will give zero steady state error.  
for step it was  $e_{ss} = 0$  if  $j \geq 1$ , for velocity  $e_{ss} = 0$  if  $j \geq 2$

Proceeding similarly we find

Input \ type		0	1	2	3
Input	impulse	0	0	0	0
	step	$\infty \frac{1}{1+k_p}$	0	0	0
ramp	velocity	$\infty$	$1/K_v$	0	0
	parabola	$\infty$	$\infty$	$1/K_a$	0

→

## PID Controllers



$y(t) \rightarrow$  actual output position

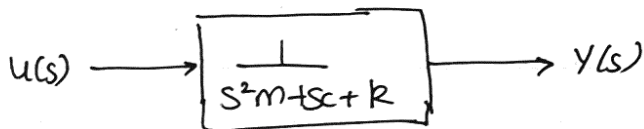
$r(t) \rightarrow$  reference or required position

Equation of motion

$$m\ddot{y} + c\dot{y} + ky = u(t)$$

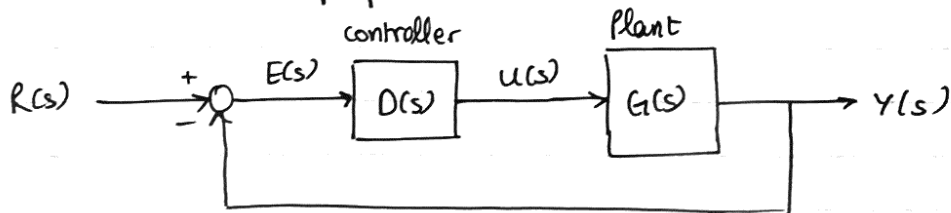
assume a quiescent system & take the Laplace transform

$$(s^2m + sc + k)Y(s) = U(s)$$



output error  $E(s) = R(s) - Y(s)$

make  $u(s)$  proportional to  $E(s)$



$\rightarrow$

Case 1 Choose  $D(s) = K_p$  a constant  
↳ Proportional

$$Y(s) = \frac{DG}{1+D(s)G(s)} R(s)$$

$$= \frac{K_p}{ms^2 + cs + K + K_p} R(s)$$

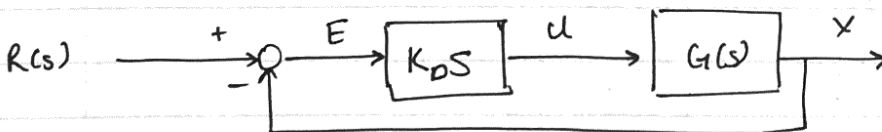
- $K_p$  acts like adding another spring
- increases  $\omega_n$
- has no effect on damping
- effects rise time  
peak time  
settling time
- no effect on overshoot

Case 2 Derivative Control

Assume the control force is proportional to the rate of change of the error.

$$u(t) = K_D \frac{de}{dt}$$

$$U(s) = K_D s E(s)$$



$$Y = \frac{K_0 s}{ms^2 + (c + K_0)s + k}$$

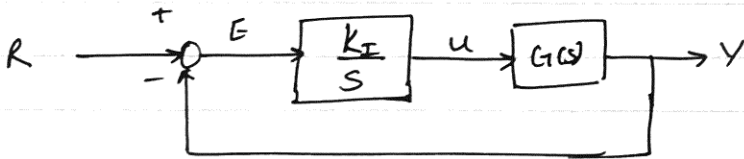
- $K_0$  increases the system damping  
 $\Rightarrow$  the effective  $\delta$  increases
- D-control removes energy from the system
- leaves  $\omega_n$  unchanged
- decreases  $\omega_d$

$K_P$  &  $K_0$  cannot destabilize the system.

### Case 3 Integral Control

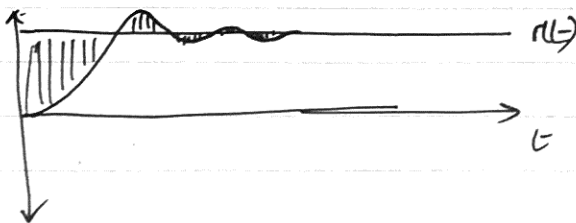
$$u(t) = K_I \int_0^t e(t) dt$$

$$U(s) = K_I \frac{E(s)}{s}$$



$$\frac{Y}{R} = \frac{DG}{1+DG} = \frac{K_I}{s(ms^2 + (s+k) + K_I)} = \frac{K_I}{ms^3 + cs^2 + ks + K_I}$$

- Adds another pole  $\Rightarrow$  can potentially destabilize the system.



- change the system to 3rd degree
- cause  $u(t) \neq 0$  even when  $e(t) = 0$  due to the integral effect.

In general all are used together as

