MAE 275 - Final

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1 Defining the System

The longitudinal linearized aircraft equations of motion can be expressed in state space form, with state variables Δu , Δw , Δq , $\Delta \theta$, Δh , as

$$A = \begin{bmatrix} X_u & X_w & 0 & -g\cos(\theta_0) & 0\\ \frac{Z_u}{1 - Z_{\dot{w}}} & \frac{Z_w}{1 - Z_{\dot{w}}} & \frac{Z_q + u_0}{1 - Z_{\dot{w}}} & -\frac{g\sin\theta_0}{1 - Z_{\dot{w}}} & 0\\ M_u + \frac{M_{\dot{w}}Z_u}{1 - Z_{\dot{w}}} & M_w + \frac{M_{\dot{w}}Z_w}{1 - Z_{\dot{w}}} & M_q + \frac{M_{\dot{w}}(Z_q + u_0)}{1 - Z_{\dot{w}}} & -\frac{M_{\dot{w}}g\sin\theta_0}{1 - Z_{\dot{w}}} & 0\\ 0 & 0 & 1 & 0 & 0\\ 0 & -1 & 0 & u_0 & 0 \end{bmatrix}$$

Relevant B, C, and D matrices can also be formed

Plugging in the data for the A-7E aircraft in a landing approach to an aircraft carrier yields

$$A = \begin{bmatrix} -5.4534e - 2 & +6.4327e - 2 & 0 & -3.2200e + 1 & 0 \\ -2.8695e - 1 & -5.2887e - 1 & +2.1800e + 2 & 0 & 0 \\ -8.2071e - 5 & -7.8112e - 3 & -3.9053e - 1 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & -1 & 0 & +2.1800e + 2 & 0 \end{bmatrix}$$

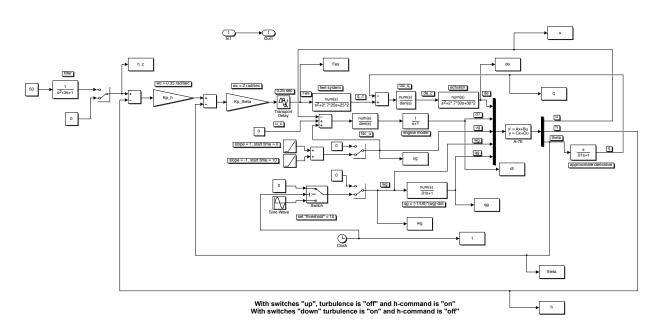


Figure 1: Final Simulink Diagram

2 Controller Design

Two controllers were designed as part of a Stability and Command Augmentation System (SCAS). These controllers were designed to control the pitch-rate and airspeed loops. The resultant controllers were:

$$\frac{q}{\delta_e} = \frac{-218.46s(s+0.4291)(s+0.1018)}{(s+100)(s^2+0.03945s+0.03717)(s^2+0.9345s+1.904)}$$

$$GC_q = -2 \times \frac{(s^2 + 0.04s + 0.04)(s^2 + s + 1.25)}{s(s+0.1)^3}$$

$$G_m = Inf \, dB$$

 $P_m = 86.7^{\circ} \, at \, 5.06 \, rad/s$
 $\omega_{BW} = 5 \, rad/s \, (-3 dB \, criterion)$
 $Unstable$

$$\frac{u}{\delta_T}\Big|_{q \to \delta_e} = \frac{0.001317(s + 5.486)(s + 0.5165)}{(s + 5.459)(s + 1)(s + 0.4842)(s + 0.1018)}$$

$$* \frac{(s^2 + 0.03252s + 0.04026)(s^2 + 1.196s + 1.248)(s^2 + 36.57s + 643.2)}{(s^2 + 0.03952s + 0.04002)(s^2 + 1.203s + 1.256)(s^2 + 36.58s + 643.6)}$$

$$GC_u = 335 \times \frac{(s+0.1)}{s(s+1.5)}$$

$$G_m = 18.3 \, \mathrm{dB} \, \mathrm{at} \, 1.21 \, \mathrm{rad/s}$$

 $P_m = 64.5^{\circ} \, \mathrm{at} \, 0.286 \, \mathrm{rad/s}$
 $\omega_{BW} = .497 \, \mathrm{rad/s} \, (-3 \, \mathrm{dB} \, \mathrm{criterion})$
 $Stable$

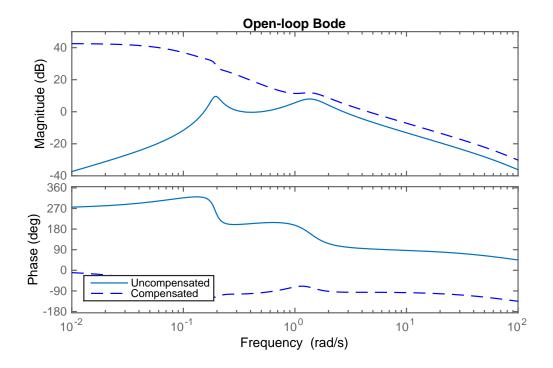


Figure 2: Open-loop Bode for Gc_q

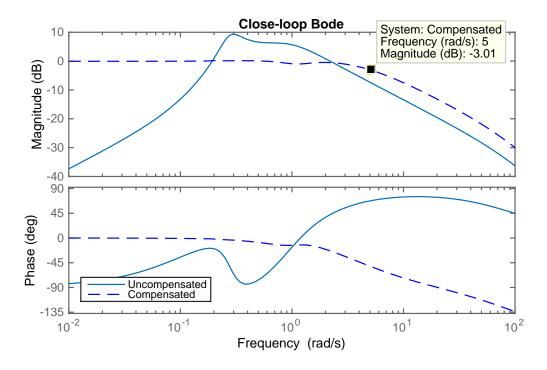


Figure 3: Close-loop Bode for Gc_q

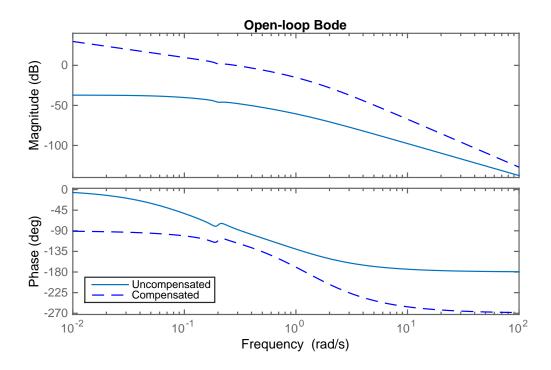


Figure 4: Open-loop Bode for Gc_u

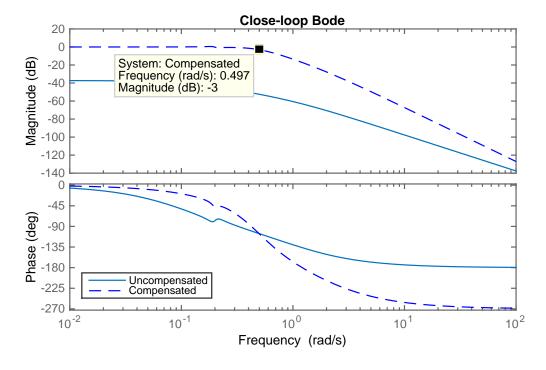


Figure 5: Close-loop Bode for Gc_u

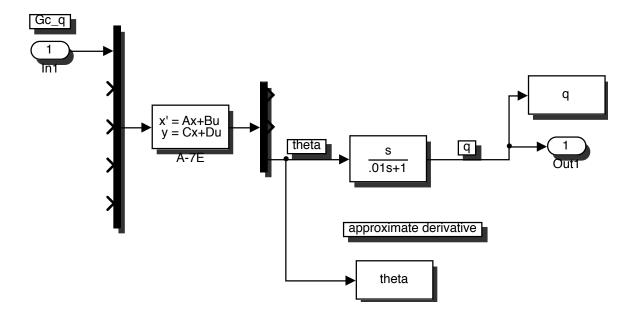


Figure 6: Simulink Diagram used to design the Pitch-rate loop

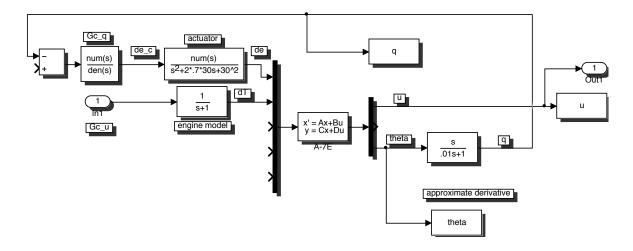


Figure 7: Simulink Diagram used to design the Airspeed loop

3 Human Pilot Model

In addition to the SCAS controllers, a pair of pilot models were used to emulate a pilot's control of altitude (through pitch attitude). The pilot models are $Y_{p_{\theta}} = K_{\theta}e^{-0.35s}$ 1/sec; $Y_{p_h} = K_h$ rad/ft. K_{θ} was chosen to give a 2 rad/sec crossover frequency in the θ -loop and K_h to give a 0.35 rad/sec crossover frequency in the h-loop. Two gains were chosen:

$$K_{\theta} = 2.04 K_h = 0.0024$$

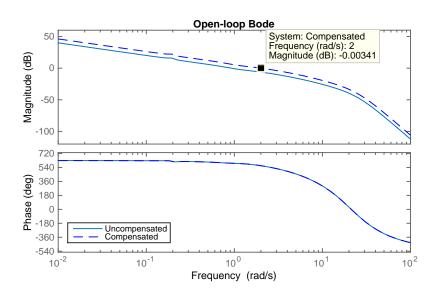


Figure 8: Open-loop Bode for Gc_u

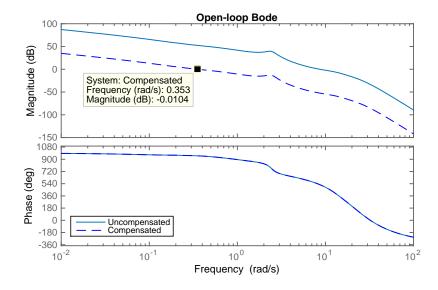


Figure 9: Open-loop Bode for Gc_u

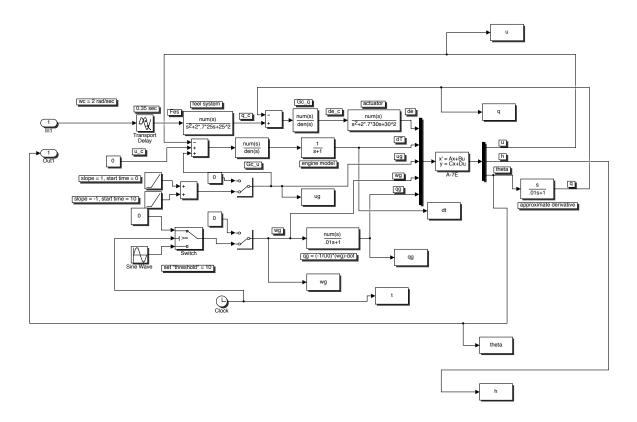


Figure 10: Simulink Diagram used to choose K_{θ}

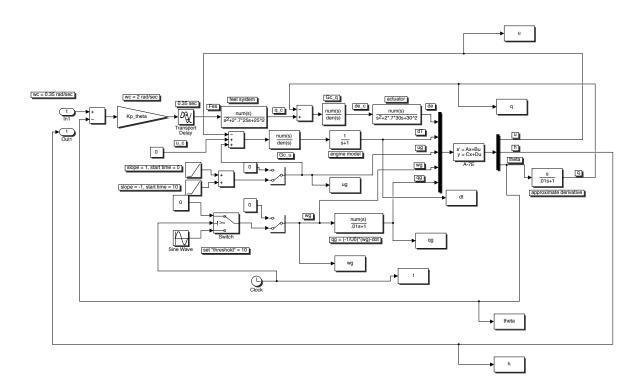


Figure 11: Simulink Diagram used to choose ${\cal K}_h$

4 Simulation Results

4.1 Step Command h_c

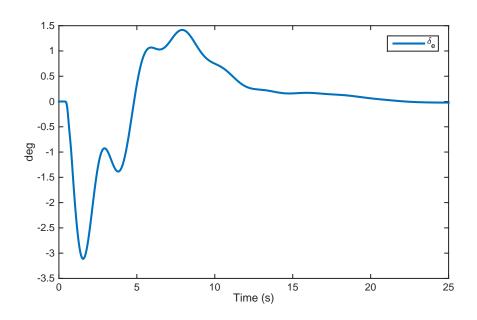


Figure 12: δ_e Response to Step Command

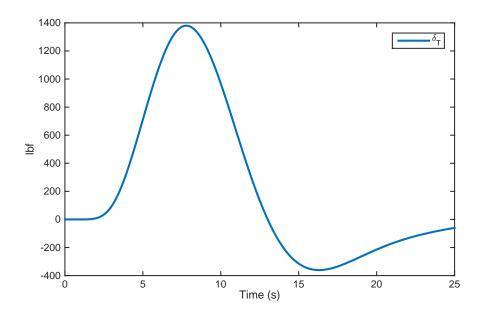


Figure 13: δ_T Response to Step Command

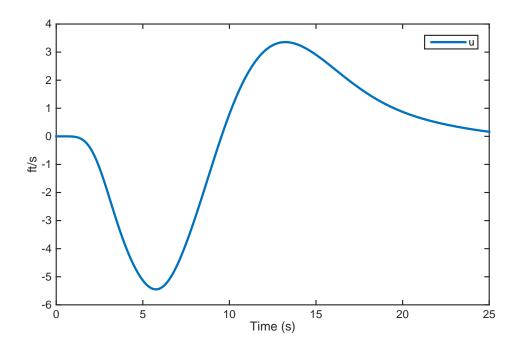


Figure 14: u Response to Step Command

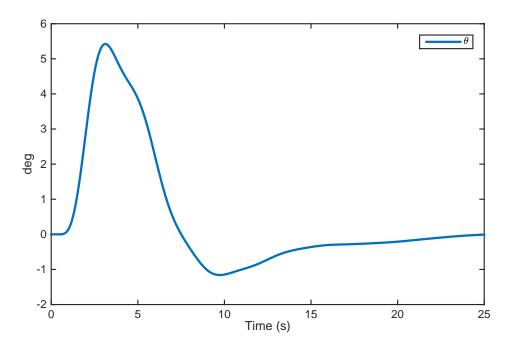


Figure 15: θ Response to Step Command

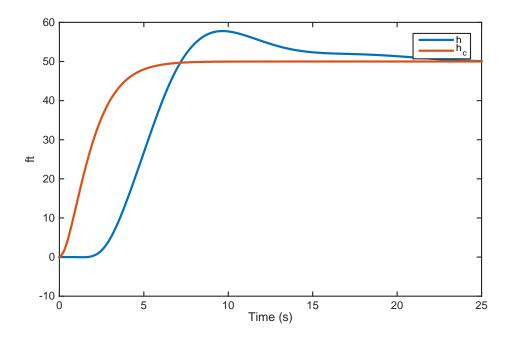


Figure 16: h Response to Step Command

4.2 Burble Response

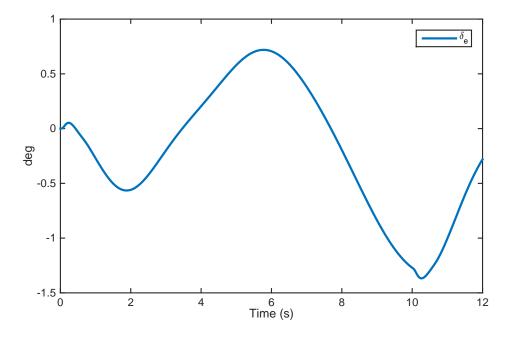


Figure 17: δ_e Response to Burble

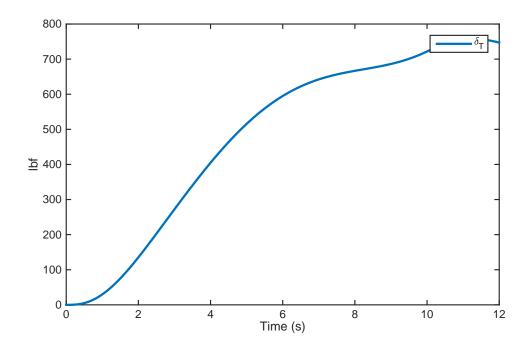


Figure 18: δ_T Response to Burble

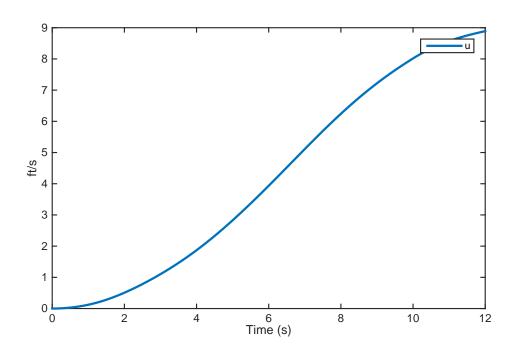


Figure 19: u Response to Burble

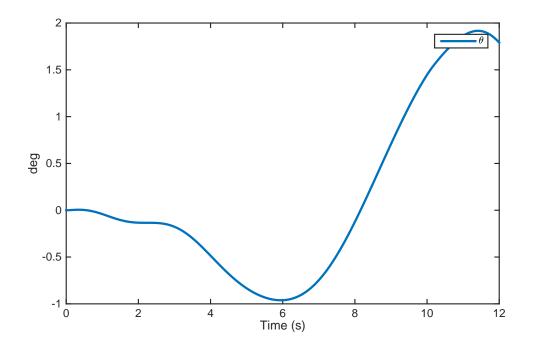


Figure 20: θ Response to Burble

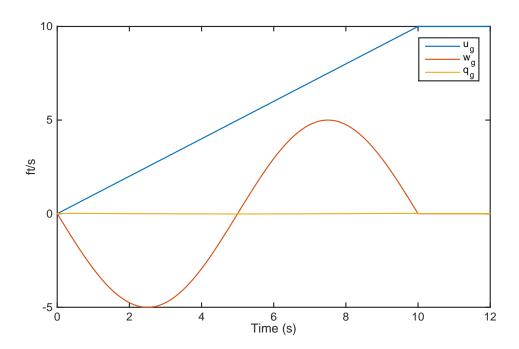


Figure 21: u_g, w_g, q_g Burble Inputs

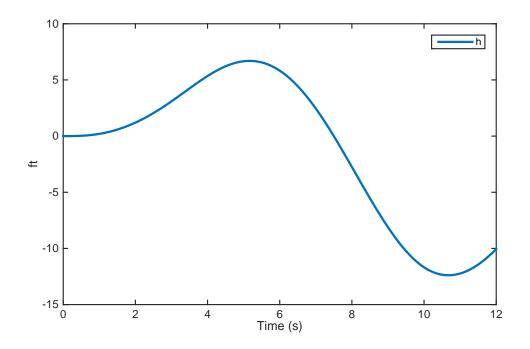


Figure 22: h Response to Burble

5 Handling Qualities

The handling qualities of the pitch-rate SCAS can be estimated using the Bandwidth/Phase-Delay boundaries explained in the handout. The bandwidth is defined as the lesser of $w_{BW_{gain}}$ and $w_{BW_{phase}}$, which is 3.09 rad/s. The phase delay, τ_p is defined

$$\tau_p = \frac{\Delta\Phi 2w_{180}}{57.3(2w_{180})} = \frac{244 - 180}{57.3(12.8)} = 0.09s$$

These values suggest Level 1 handling qualities.

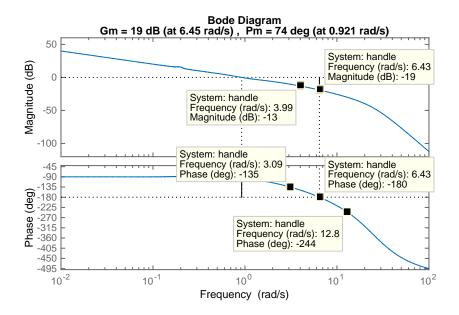


Figure 23: $\left|\frac{\theta}{F_{es}}\right|$ bode with relevant points selected

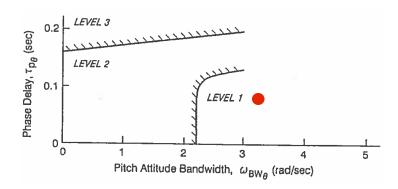


Figure 24: Handling qualities diagram with location marked