### Problem 1. Develop a very simple representation of the Hubble telescope.

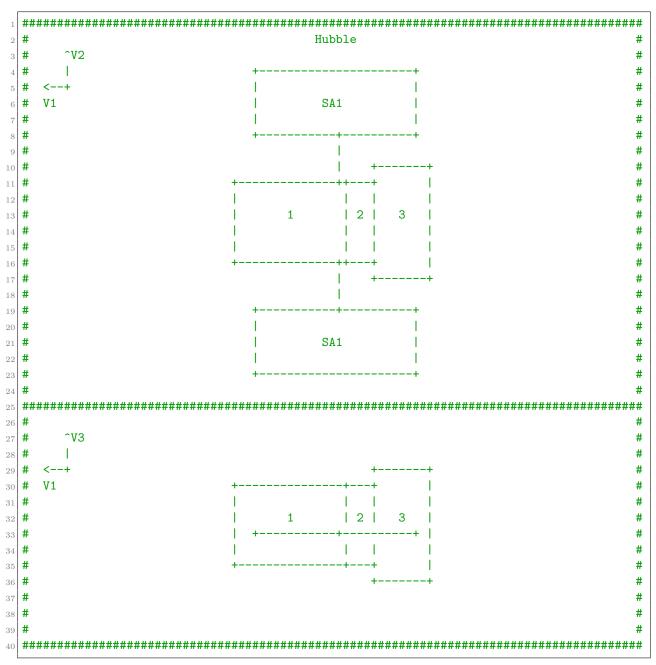


Diagram 1: Hubble ASCII Diagram. Solar panel distance from HST is exaggerated. One character is  $\approx$  20 inches.

We model both the body (3 sections) and the solar panels (2 sections) of the Hubble Space Telescope (HST). The body sections are connected as such: Section 1 is connected to Section 2, and Section 2 is connected to Section 3. The solar arrays are connected on Section 1, along the centerline, 20.75 inches  $V_1$  away from the connection point with Section 2, and the near edge of the SA is 129 inches from center of Section 1. These sections are modeled with thin walled cylinders (TWC), solid cylinders (SC), and flat plates (FP). The rough

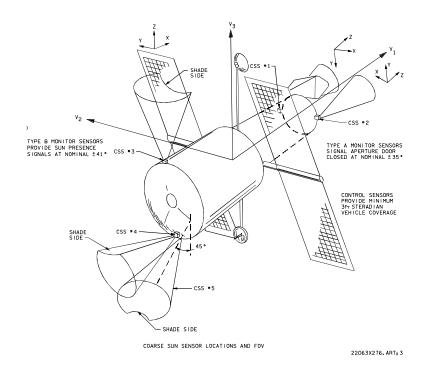


Figure 1: HST Axes Definition for  $V_1, V_2, V_3$ , CG is located at axis origin

Section	Model	$V_1$ (in)	$V_2$ (in)	Weight (lb)
Section 1				
Light Shield (LS)	-	153.2	120	_
Forward Shell (FS) (except OTA)	-	156.05	121.2	-
Total	TWC	270.75	121.2	2796
Section 2				
OTA Equipment Section	TWC	38.5	121.2	9033
Section 3				
SSM Equipment Section (SSM-ES)	-	61.25	168.16	10594
Aft Shroud (AS)	-	138.00	168.16	569
Total	SC	199.25	168.16	11163
Section 4				
Solar Arrays (SA)	FP	$476.8^{1}$	113.5	$735^{2}$

Table 1:  $^1$ : This length can be fully rotated into  $V_3$ .  $^2$ : Weight of both solar arrays.  $V_1$  and  $V_2$  indicate the measurements of the parts. All lengths taken from Hubble technical drawings [2]; all masses from [3].

layout of the sections is shown on the previous page, and the mass and length properties of each section are listed in Table 1.

# Problem 2. Use this model as a basis to write a function(s) to determine the Mass Center and Inertia Matrix for any location.

Using the radial-center of the farthest tip of Section 1 as our zero point, the center of mass is located at V = [327, 0, 0] inches. This makes since, as the model is symmetric about the  $V_2$  and  $V_3$  axes, and this value is on the boundary between Section 2 and Section 3, which is very close to where the reaction wheels are located.

The HST inertia matrix [1], was at one point measured as:

$$I = \begin{bmatrix} 36046 & -706 & 1491 \\ -706 & 86868 & 449 \\ 1491 & 449 & 93848 \end{bmatrix} kg \cdot m^2.$$

The Python script in Appendix gives the result of:

$$I = \begin{vmatrix} 35914 & 0 & 0 \\ 0 & 88215 & 0 \\ 0 & 0 & 113393 \end{vmatrix} kg \cdot m^2,$$

which has a relative error of:

$$I = \begin{bmatrix} 0 & 100 & 100 \\ 100 & -2 & 100 \\ 100 & 100 & -21 \end{bmatrix} \%.$$

Note that while our simple, 5 part model does a very good job of predicting the  $I_{V_1}$  and  $I_{V_2}$  components, the  $I_{V_3}$  component is not represented very well. This is likely due to leaving out the antenna booms, which should have the largest effect in the  $V_3$  directions. It should also be noted that, due to the symmetric nature of our model, all of the off-axis terms are missing. For the rest of the analysis, the true values for the inertia matrix will be used. See Figure 2 for the effects of rotating the solar arrays on the principle axes.

#### Problem 3. Write a function to find the current angular momentum relative to the mass center.

H increases linearly with  $\omega$ . See Appendix for the code used to create Figure 3.

## Problem 4. Choose the optimal location for a torque producing system and explain why you think is the best location.

The optimal location for a torque producing system is usually on the centerline, as near to the center of mass of the spacecraft as possible. Placing the torque producing system close the the spacecraft's center of mass minimizes the amount of undesirable resultant torque when the system is activated. In HST's case, the optimal location for a torque producing system is in the SSM-ES, see Fig. 4. The two wheels of a single SSM bay are canted off the

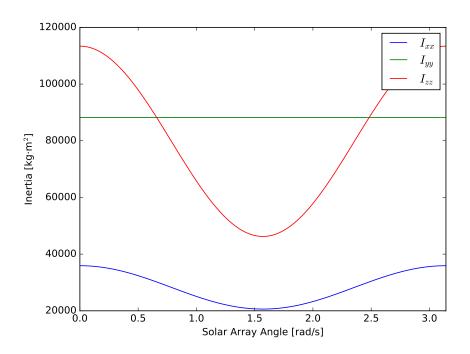


Figure 2: Inertias for principal axes for different solar array configurations

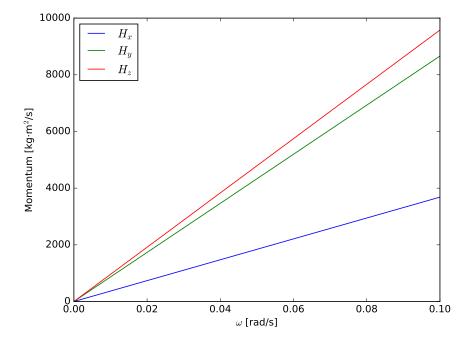


Figure 3: Effects of spin on each axis

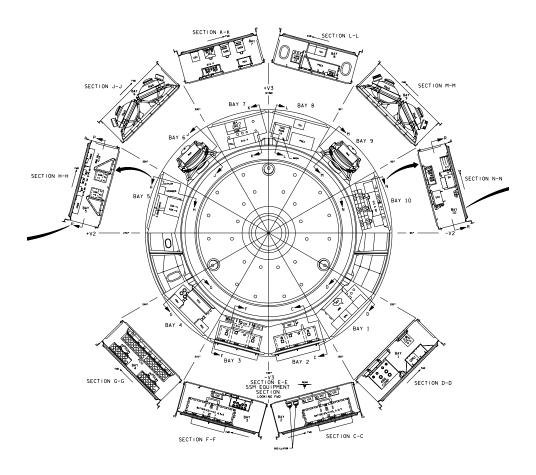


Figure 4: HST's reaction wheels are located in the SSM-ES in bays 6 and 9. The pairs were installed in at a 90° offset to protect against failures [2].

 $V_2$ - $V_3$  plane by 20°, one toward the  $+V_1$  and one toward the  $-V_1$ . I think that this is likely the best location to place the system as it's the one that was actually used, and because the engineers that placed them the reaction wheels there had much greater access to information about HST than I do.

As we do not have to worry about reaction wheels failing for the purposes of this homework, I would instead simplify the system to a single location of three reaction wheels, one of which is aligned with each axis. "Nominal dynamic torque range is 0.003 to 0.605 ft-lb (0.004 to 0.7 N·m), with a maximum wheel speed of  $\pm 3000$  rpm" for each of the four reaction wheels [2].

Problem 5. Using your previous functions, write a program to find the resulting angular acceleration produced from a given torque.

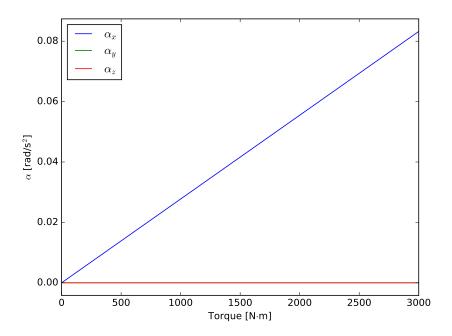


Figure 5: Angular acceleration response along all three axis from a single reaction wheel producing  $\tau_x$ , from initial conditions  $\omega = [0, 0, 0] \text{ rad/s}$ .

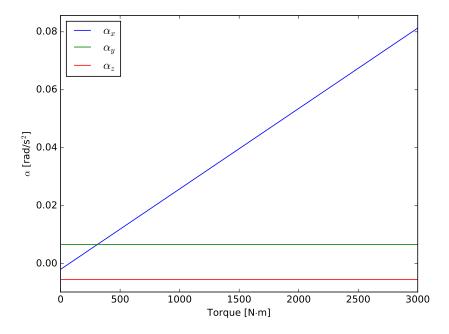


Figure 6: Angular acceleration response along all three axis from a single reaction wheel producing  $\tau_x$ , from initial conditions  $\omega = [0.1, 0.1, 0.1] \text{ rad/s}$ .

### Problem 6. Write what next steps you would take to develop a controller that keeps the craft pointed in a specific direction.

To develop a controller, we would need to:

- (a) Determine where the craft should be pointed (science requirements)
- (b) Determine where the craft is currently pointed (using sensors)
- (c) Find the difference between these two (the error)
- (d) Determine which reaction wheels need to be activated to minimize the error
- (e) Activate the reaction wheels

Once we had sensors and the ability to activate our reaction wheels, the majority of the time developing the controller would involve tuning it to perform to some specification (minimizing overshoot, minimizing response time, etc.).

#### **Bibliography**

- [1] Queen, S., "HRV GNC Peer Review, Flight Performance Analysis," Tech. rep., NASA Goddard Space Flight Center, 2004.
- [2] NASA, "Cargo Systems Manual (CSM): Hubble Space Telescope," February 13, 2002
- [3] Mattice, J., "Hubble Space Telescope Systems Engineering Case Study."

#### .1 Python Code

```
import numpy as np
2 from collections import namedtuple
3 import pandas as pd
4 import matplotlib.pyplot as plt
  # Origin is the tip of far center of the far end of Section1
  Part = namedtuple('Part', ['mass', 'v1', 'v2', 'v3'])
g | Cylinder = namedtuple('Cylinder', Part._fields + ('length', 'radius'))
| Plate = namedtuple('Plate', Part._fields + ('length', 'width'))
12 Section1 = Cylinder(mass=2796, v1=270.75/2, v2=0, v3=0, length=270.75, radius=121.2/2)
13 Section 2 = Cylinder(mass=9033, v1=Section1.length + 38.5/2, v2=0, v3=0, length=38.5,
      radius=121.2/2)
14 Section3 = Cylinder(mass=11163, v1=Section1.length + Section2.length + 199.25/2, v2=0, v3
      =0, length=199.25, radius=168.16/2)
Solar1 = Plate(mass=735/2, v1=309.25 - 20.75, v2=129 + 113.5/2, v3=0, length=476.8, width
      =113.5)
16 Solar2 = Plate(mass=735/2, v1=309.25 - 20.75, v2=-129 - 113.5/2, v3=0, length=476.8,
      width=113.5)
```

```
parts = [Section1, Section2, Section3, Solar1, Solar2]
19 r_cm = ([part.mass * np.array([part.v1, part.v2, part.v3]) for part in parts] /
          np.sum([part.mass for part in parts])).sum(axis=0)
  print(r_cm)
21
22
23
  def parallel_axis(part, inertia, r=[0, 0, 0]):
24
      # The moment of inertia about the center of mass of the body with respect
      # to an orthogonal coordinate system.
26
      Ic = inertia(part)
27
      m = part.mass
28
29
      # The distances along the three ordinates that located the new point
      # relative to the center of mass of the body.
      d = np.array([part.v1, part.v2, part.v3])
32
33
      a = d[0] - r[0]
34
      b = d[1] - r[1]
35
      c = d[2] - r[2]
36
      dMat = np.zeros((3, 3), dtype=object)
37
      dMat[0] = np.array([b**2 + c**2, -a * b, -a * c])
38
      dMat[1] = np.array([-a * b, c**2 + a**2, -b * c])
39
      dMat[2] = np.array([-a * c, -b * c, a**2 + b**2])
40
      return Ic + m * dMat
41
42
43
  def SolidCylinder(cylinder):
44
      m = cylinder.mass
45
      r = cylinder.radius
46
      h = cylinder.length
47
      I = np.array([[1/12 * m * (3 * r**2 + h**2), 0, 0],
48
                     [0, 1/12 * m * (3 * r**2 + h**2), 0],
49
                     [0, 0, 1/2 * m * r**2]])
50
      return I
51
53
  def ThinWalledCylinder(cylinder):
54
      m = cylinder.mass
      r = cylinder.radius
56
      h = cylinder.length
57
      I = np.array([[1/12 * m * (3 * 2*(r**2) + h**2), 0, 0],
                     [0, 1/12 * m * (3 * 2*(r**2) + h**2), 0],
59
                     [0, 0, 1/2 * m * 2 * (r**2)]])
      return I
61
62
  def FlatPlate(plate):
      m = plate.mass
65
      a = plate.length
66
      b = plate.width
67
      I = np.array([[1/12 * m * b**2, 0, 0],
68
                     [0, 1/12 * m * a**2, 0],
69
                     [0, 0, 1/2 * m * (a**2 + b**2)]])
70
```

```
return I
71
72
73
   def rotation_matrix(axis, theta):
74
       0.00
75
       Return the rotation matrix associated with counterclockwise rotation about
76
       the given axis by theta radians.
77
       axis = np.asarray(axis)
79
       theta = np.asarray(theta)
80
       axis = axis/np.sqrt(np.dot(axis, axis))
81
       a = np.cos(theta)
82
       b, c, d = -axis*np.sin(theta)
83
       aa, bb, cc, dd = a*a, b*b, c*c, d*d
       bc, ad, ac, ab, bd, cd = b*c, a*d, a*c, a*b, b*d, c*d
85
       return np.array([[aa+bb-cc-dd, 2*(bc+ad), 2*(bd-ac)],
86
                         [2*(bc-ad), aa+cc-bb-dd, 2*(cd+ab)],
87
                         [2*(bd+ac), 2*(cd-ab), aa+dd-bb-cc]])
88
89
90
   def TotalI(r, theta=0):
91
       I_S1 = parallel_axis(Section1, ThinWalledCylinder, r=r)
92
       I_S2 = parallel_axis(Section2, ThinWalledCylinder, r=r)
93
       I_S3 = parallel_axis(Section3, SolidCylinder, r=r)
94
       I_SA1 = parallel_axis(Solar1, FlatPlate, r=r)
95
       I_SA2 = parallel_axis(Solar2, FlatPlate, r=r)
96
97
       # Rotate if necessary
98
       I_SA1 = np.dot(rotation_matrix(np.array([0, 1, 0]), theta), I_SA1)
       I_SA2 = np.dot(rotation_matrix(np.array([0, 1, 0]), theta), I_SA2)
100
       # Convert from lb * inches^2 to kg * m^2
       I = (I_S1 + I_S2 + I_S3 + I_SA1 + I_SA2) * 0.000292639653
       return I
   truth = np.array([[36046, -706,
105
                      [ -706, 86868,
                                        4491.
106
                      [ 1491,
                                449, 93848]])
   print(truth)
108
   print(TotalI(r_cm))
109
110
   def plot1():
       plt.close('all')
113
       res = []
114
       for theta in np.linspace(0, np.pi, 100):
           res.append([theta, *TotalI(r=r_cm, theta=theta).diagonal()])
       pd.DataFrame(res).plot(x=0, y=[1, 2, 3])
       plt.legend(['$I_{xx}$', '$I_{yy}$', '$I_{zz}$'], loc='upper right')
       plt.ylabel('Inertia [kgm$^2$]')
119
       plt.xlabel('Solar Array Angle [rad/s]')
120
       plt.savefig('figure1.pdf')
   plot1()
122
123
124
```

```
def angularMomentum(w):
       ''' Using the true value for the inertia matrix.'''
126
       I = truth
127
       H = np.dot(I, w)
128
       return H
130
   def plot2():
       plt.close('all')
133
       res = []
134
       for w in np.linspace(0, 0.1, 100):
           w *= np.ones(3)
136
           res.append([w[0], *angularMomentum(w)])
       pd.DataFrame(res).plot(x=0, y=[1, 2, 3])
       plt.legend(['$H_x$', '$H_y$', '$H_z$'], loc='upper left')
139
       plt.ylabel('Momentum [kgm$^2$/s]')
140
       plt.xlabel('$\omega$ [rad/s]')
141
       plt.savefig('figure2.pdf')
142
   plot2()
143
144
145
   def estimateAlpha(torque, omega=0, I=truth):
146
       ''' Using the true value for the inertia matrix.'''
147
       alpha = np.zeros(3)
148
149
       alpha[0] = (torque[0] + (I[1][1] - I[2][2]) * omega**2) / I[0][0]
150
       alpha[1] = (torque[1] + (I[2][2] - I[0][0]) * omega**2) / I[1][1]
       alpha[2] = (torque[2] + (I[0][0] - I[1][1]) * omega**2) / I[2][2]
       return alpha
   def plot3():
156
       plt.close('all')
       res = []
158
       for torque in np.linspace(0, 3000, 100):
           torque *= np.array([1, 0, 0])
           res.append([torque[0], *estimateAlpha(torque, omega=0)])
161
       pd.DataFrame(res).plot(x=0, y=[1, 2, 3])
162
       #plt.ylim(0, .05)
163
       #plt.xlim(0, 5e-7)
164
       plt.legend(['$\\alpha_x$', '$\\alpha_y$', '$\\alpha_z$'], loc='upper left')
165
       plt.ylabel('$\\alpha$ [rad/s$^2$]')
166
       plt.xlabel('Torque [N$\cdot$m]')
167
       plt.margins(0.05)
       plt.savefig('figure3.pdf')
   plot3()
170
   def plot4():
173
174
       plt.close('all')
       res = []
       for torque in np.linspace(0, 3000, 100):
176
           torque *= np.array([1, 0, 0])
177
           res.append([torque[0], *estimateAlpha(torque, omega=0.1)])
178
```

```
pd.DataFrame(res).plot(x=0, y=[1, 2, 3])
       #plt.ylim(0, .05)
180
       #plt.xlim(0, 5e-7)
181
       plt.legend(['$\\alpha_x$', '$\\alpha_y$', '$\\alpha_z$'], loc='upper left')
182
       plt.ylabel('$\\alpha$ [rad/s$^2$]')
183
       plt.xlabel('Torque [N$\cdot$m]')
184
       plt.margins(0.05)
185
       plt.savefig('figure4.pdf')
186
187 plot4()
```