

Summary: Viortual Work & Energy Methods Unit laad method (ULU) * Derived from the principle at complementory wistual work * / ields the clisplacement (or ratation)
in the direction at an applied
wintual cenit load (moment). Po $H_{23} = 0$ Ly $\int_{X_1}^{X_2} \int_{X_1}^{X_2} \int_{X_2}^{X_3} \int_{X_3}^{X_4} \int_{X_4}^{X_4} \int_{X_4}^$ Je 3/2 3/ OP=1 -> Unit Load System 1) Real interal moment les (x1) $U_3(x,) = -\frac{P_0(1-x_i)^2}{3}$ 2) Statically adminible M3 (x1) $\hat{\mathcal{M}}_{3}(x_{1}) \begin{cases} -\partial P(L/2-x_{1}) \times_{1} < 1/2 \\ 0 \times_{1} > 1/2 \end{cases}$ $\Delta = \int_0^L \frac{\mathcal{U}_3 \, \hat{\mathcal{U}}_3}{H_{33}^2} \, dx_1 = \int_0^{\sqrt{7}} \frac{\rho_0}{2H_{23}^2} \left(1 - x_1\right)^2 \left(\frac{\zeta}{2} - x_1\right) \, dx_1$

$$\Delta = \begin{cases} (\hat{N}_{1} E_{1} + \hat{M}_{2} K_{2} + \hat{M}_{3} K_{3}) dx_{1} \\ K_{2} = (H_{33} M_{2} + H_{23} M_{3}) / \Delta H \end{cases}$$

$$K_{3} = (H_{23} M_{2} + H_{22} M_{3}) / \Delta H$$

$$\Delta H = H_{22} H_{33} - H_{23} H_{23}$$

Dunny Laad Wethod

- * Derived drom the principle at minimum complementary energy and Castigliano's 2 nd Theorem
- * Yelds the displacement (or ratation) under an applied concentrated dummy laad (or moment)

$$\frac{1}{12}$$

$$S = \lim_{\beta \to 0} \frac{\partial A}{\partial \beta} = \lim_{\beta \to 0} \frac{\partial}{\partial \beta} \left(\frac{1}{2} \frac{M_3^2}{H_{33}^2} dx, \frac{1}{2} \frac{M_3^2}{H_{33}^2} dx \right)$$

$$\Delta = \lim_{S \to 0} \left(\frac{M_3}{H_{33}} \frac{\partial M_3}{\partial S} dx \right)$$

$$M_{3} = \begin{cases} -\frac{\rho_{0}(1-x_{1})^{2}}{2} - \beta(1/2-x_{1}) & x_{1} < 1/2 \\ -\frac{\rho_{0}(1-x_{1})^{2}}{2} & x_{1} > 1/2 \end{cases}$$

$$\frac{\partial M_{3}}{\partial \beta} = \begin{cases} -\frac{\rho_{0}(1-x_{1})^{2}}{2} - \beta(1/2-x_{1}) & x_{1} < 1/2 \\ -\frac{\rho_{0}(1-x_{1})^{2}}{2} - \beta(1/2-x_{1}) & x_{2} < 1/2 \end{cases}$$

$$\Delta = \lim_{D \to \infty} \int_{0}^{1/2} \frac{1}{H_{33}^{2}} \left(-\frac{\rho_{0}(1-x_{1})^{2}}{2} - \beta(1/2-x_{1}) \right) \frac{1}{2} \left(-\frac{\rho_{0}(1-x_{1})^{2}}{2} - \frac{\rho_{0}(1-x_{1})^{2}}{2} - \frac{\rho_{0}(1-x_{1})^{2}}{2} \right) \frac{1}{2} \frac{1}{2} \left(-\frac{\rho_{0}(1-x_{1})^{2}}{2} - \frac{\rho_{0}(1-x_{1})^{2}}{2} - \frac{\rho_{0}(1-x_{1})^{2}}{2} \right) \frac{1}{2} \frac{1}{2} \left(-\frac{\rho_{0}(1-x_{1})^{2}}{2} - \frac{\rho_{0}(1-x_{1})^{2}}{2} - \frac{\rho_{0}(1-x_{1})^{2}}{2} \right) \frac{1}{2} \frac{1$$

Costigliano's 2nd Theorem

- * yields the displacement under a point load. (On ratation under a point moment).
- * Useful ter Lending reaction torces
 that lead to kinematic constraints.

$$D_R = \frac{\partial A'}{\partial R} = 0 \rightarrow Solve lor R$$

$$\Delta_{R} = 0 \quad \begin{cases} 1 & M_{3} & dx_{1} \\ 0 & \overline{2} & \overline{H_{53}} \end{cases} = \begin{cases} \frac{1}{2} & \frac{$$

$$\mathcal{U}_{3}(x_{l}) = -\frac{P_{0}(L-x_{l})^{2}}{2} + \mathcal{R}(L-x_{l})$$

$$\frac{\partial \mathcal{U}_3}{\partial \mathcal{R}} = \left(L - \times_1 \right)$$

$$\Delta_R = 0 = \left(\frac{1}{H^{C}} \left(-\frac{PO(L-x_1)^2 + R(L-x_1)}{2}\right)(L-x_1)\right) dx_1$$

$$\frac{1}{1} \frac{1}{1} - \frac{1}{1} \frac{1}{2} \frac{1}{4} + \frac{1}{1} \frac{1}{3} \frac{1}{3} = 0 \qquad R = \frac{3}{3} \frac{1}{1} \frac{1}{8} \frac{1}{8}$$

Rayleigh Ritz * Derived from the principle at minimum patential energy * Vields an approseimate soleetlen ly tening a continues pralem into one with a femile # at DDF. $\hat{u} = \sum_{i=1}^{\infty} q_i h_i(x_i, x_2, x_3)$ Shope Fenctions must ODF satisfy Rinematic B.C.s Compute q'i through $\frac{\partial 11}{\partial q_i} = 0$ $\Pi = A + \Phi$ $\frac{\lambda_{2}}{1} = \frac{P_{0} L^{2} + \lambda_{1}^{2}}{12 H_{32}}$ $\frac{\lambda_{1}}{1} = \frac{L}{1} + \frac{L}{132} + \frac{L}{12 H_{32}} + \frac{L}{12 H_{32}}$ $\frac{\lambda_{1}}{1} = \frac{L}{100} + \frac{L}{12 H_{32}} + \frac{L}{12 H_{32}}$ $\frac{\lambda_{1}}{12 H_{32}} = \frac{L}{12 H_{32}} + \frac{L}{12 H_{32}}$ $\frac{\lambda_{1}}{12 H_{32}} = \frac{L}{12 H_{32}}$ $\overline{11} = \int_{0}^{L} \left(\frac{1}{2} H_{33}^{2} + 4q^{2} + P_{0} q_{x_{1}}^{2} \right) dx_{1}$ $\overline{11} = 2 H_{33} q^{2} L + Po q L^{3}$ $\frac{\partial 11}{\partial q} = 0 = 4 H_{33} q^{2} + Po L^{3}$ 9 = - Po L'

$$A = \frac{1}{2} \int_{0}^{L} \left(S \bar{e}_{1}^{2} + H_{22}^{C} k_{2}^{2} + H_{33}^{C} k_{3}^{2} - 2H_{23}^{C} k_{2} k_{3} \right) dx_{1}$$