### Georgia Institute of Technology School of Aerospace Engineering

### AE 6115 — Fundamentals of Aerospace Structural Analysis — Spring 2021

#### Quiz No.1

Consider a cantilevered wing of length L with an asymmetric airfoil cross-section which is constant along the long direction of the wing as shown in Fig. 1. The wing is subjected to two distributed loads representing the lift and drag forces which are given by

$$p_2(x_1) = P_L \left( 1 - \left( \frac{x_1}{L} \right)^2 \right), \text{ and } p_3(x_1) = -P_D \left( 1 - \frac{x_1}{L} \right),$$
 (1)

with  $P_L$  and  $P_D$  known constants and with  $x_1 = 0$  starting at the cantilevered end. You may assume that the wing is slender and composed of a homogeneous material of Young's modulus E.

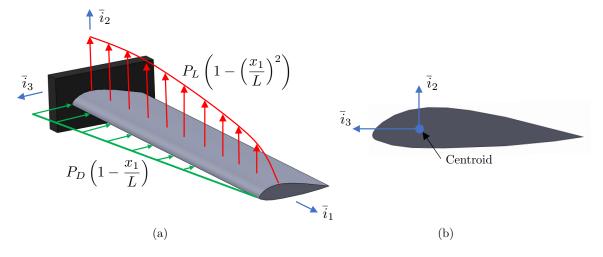
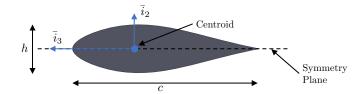


Figure 1: Cantilevered wing under applied distributed loads.

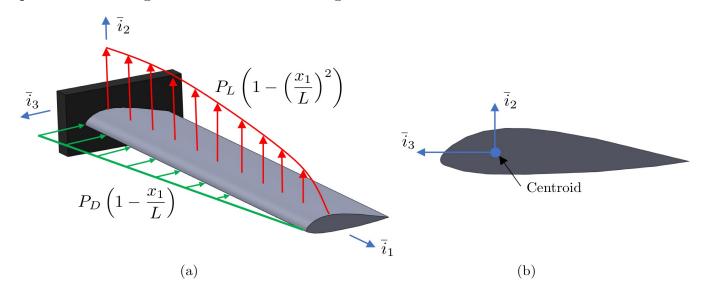
- a) Solve for the internal moment distributions  $M_2(x_1)$  and  $M_3(x_1)$  in the wing.
- b) Solve for the displacement components  $u_1(x_1, x_2, x_3)$ ,  $u_2(x_1, x_2, x_3)$ , and  $u_3(x_1, x_2, x_3)$ . **Important:** You may leave your answer in terms of any non-zero stiffnesses.
- c) **Semi-Conceptual:** Consider now a *symmetric* cross-section as shown in the figure below:

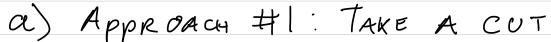


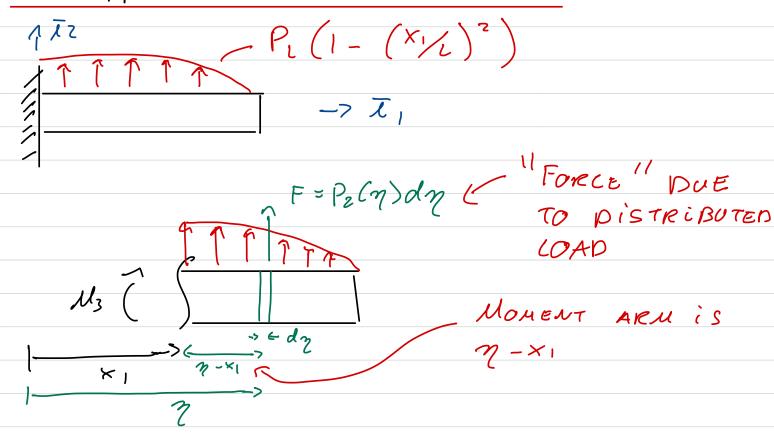
For the special case of  $P_L/P_D = 1$  and c/h = 5, find a good **estimate** for the equation of the neutral axis at the root of the beam  $(x_1 = 0)$ . Sketch the neutral axis.

**Hint:** You will have to make some estimates here about the stiffnesses of this cross-section. You may also estimate any necessary results that you did not already find in parts a) and b) above.

omposed of a nomogeneous majories of round a measure -







$$M_3 = \int_{x_1}^{L} (\eta - x_1) P_L \left( 1 - \left( \frac{\eta}{L} \right)^2 \right) d\eta$$

$$M_{3} = \int_{x_{1}}^{L} (\eta - x_{1}) P_{L} \left( 1 - \left( \frac{\eta}{L} \right)^{2} \right) d\eta$$

$$M_{3} = P_{L} \int_{x_{1}}^{L} \left( \eta - \frac{\eta}{L^{2}} - x_{1} + \frac{x_{1} \eta}{L^{2}} \right) d\eta$$

$$M_{3} = P_{L} \left[ \frac{\eta^{2} - \eta^{4} - x_{1} \eta + \frac{x_{1} \eta}{3 L^{2}} \right]_{x_{1}}^{L}$$

$$= P_{L} \left[ \frac{L^{2} - L^{2} - x_{1} L + \frac{1}{2} x_{1} L \right]$$

$$- \frac{x_{1}^{2}}{2} + \frac{x_{1}^{4}}{4 L^{2}} + \frac{x_{1}^{2} - \frac{x_{1}^{4}}{3 L^{2}}}{\frac{3}{2} L^{2}} \right]$$

$$M_3 = P_L \left( \frac{L^2 - 2x_1L}{4} + \frac{1}{2}x_1^2 - \frac{1}{12}\frac{x_1}{L^2} \right)$$

Similarely
$$M_2 = \left( \left( n - x_1 \right) P_p \left( 1 - \frac{2}{L} \right) d_p$$

$$\mathcal{M}_{2} = P_{p} \left( \left( \frac{\eta - \eta^{2} - \chi_{1} + \chi_{2} \eta}{2} \right) d\eta \right)$$

$$\mathcal{M}_{2} = \mathcal{P}_{p} \left( \left( \eta - \frac{\eta^{2}}{2} - \times_{1} + \times_{2} \eta \right) \right) d\eta$$

$$\mathcal{U}_2 = P_p \left[ \frac{n^2 - n^3 - x_1 \eta + x_1 \eta^2}{2L} \right]_{x_1}^{\zeta}$$

$$M_2 = P_0 \left( \frac{L^2 - L^2 - x_1 l + x_1 L}{2} \right)$$

$$\frac{-x_{1}^{2}+1x_{1}^{3}+x_{1}^{2}+x_{1}^{2}-(x_{1}^{3})}{2}$$

$$M_2 = P_p \left( \frac{1}{6} \frac{1^2 - 1 \times_1 L + \times_1^2}{2} - \frac{1}{6} \frac{\times_1^3}{2} \right)$$

APPROACH #2: USE BALANCELAWS

$$\frac{dM_3}{dx_1} + V_2 = -q_3(x_1) + x_{2A}p_1(x_1)$$

$$\frac{dV_2}{dx_1} = -P_2(x_1)$$

COMBIN IN G

$$\frac{d^2 M_3}{d \times 1^2} = P_2(x_1) = P_1 \left( 1 - \left( \frac{x_1}{2} \right)^2 \right)$$

$$\frac{13.C.s}{2} = \frac{2}{2} =$$

INTEGRATING:

$$\frac{\mathcal{O}M_3}{\mathcal{O}\times 1} = P_L\left(\times_1 - \frac{\times_1^3}{3L^2}\right) + C$$

Apply (1)

$$\frac{dM_3}{dx_1} = P_L\left(\frac{x_1 - \frac{x_1^3}{3L^2} - \frac{z_2}{3}L}\right)$$

$$\frac{dM_3}{dx_1} = P_L\left(x_1 - \frac{x_1^3}{3L^2} - \frac{2}{3}L\right)$$

$$M_3 = P_L \left( \frac{x_1^2}{7} - \frac{x_1^4}{12L^2} - \frac{2Lx_1}{7} \right) + C$$

$$0 = P_{L} \left( \frac{L^{2} - L^{2} - 2L^{2}}{2} \right) + C$$

$$M_3 = P_L\left(\frac{x_1^2 - x_1^4 - 2Lx_1 + 1L^2}{2}\right)$$

-> NATCHES THE SAME AS BEFORE.

SimilARELY FOR N2

$$\frac{dU_2}{dX_1} - V_3 = 0 \quad \frac{dV_3}{dX_1} = -P_3(x_1)$$

$$\frac{d^2 \mathcal{U}_2}{d \times 1^2} = -P_3(x_1) = P_D\left(1 - \frac{x_1}{\ell}\right)$$

$$\frac{B.C.^{1}S}{\omega \times_{1} = L} \qquad \frac{V_{3} = dM_{2} = 0}{\omega \times_{1}}$$

$$M_{2} = 0$$

$$\frac{dM_2}{dx_1} = P_D\left(x_1 - x_1^2\right) + C$$

$$O = P_{\mathcal{D}} \left( 1 - \frac{1}{2} \right) + C, - > C_{1} = -P_{\mathcal{D}} \frac{1}{2}$$

$$\frac{dN_2}{dx_1} = P_D\left(x_1 - \frac{x_1^2}{2\lambda} - \frac{L}{2}\right)$$

$$\mathcal{U}_2 = P_p \left( \frac{x_1^2}{2} - \frac{x_1^3}{6L} - \frac{L}{2} x_1 \right) + C_2$$

$$0 = P_0 \left( \frac{L^2}{2} - \frac{L^2}{6} - \frac{L^2}{2} \right) + C_2$$

$$-> \quad C_2 = L^2 P_0$$

$$\mathcal{U}_{2} = P_{D}\left(\frac{x_{1}^{2}}{2} - \frac{x_{1}^{3}}{6L} - \frac{L}{2}x_{1} + \frac{L^{2}}{6}\right)$$

APPROACH #3: SOLUE GOVERNING EQUATIONS.

$$H_{33} \frac{d^{4} U_{2}}{d x_{1}^{4}} + H_{23} \frac{d^{4} U_{3}}{d x_{1}^{4}} = P_{2}(x_{1})$$

$$H_{23}^{C} \frac{d^{4}U_{2}}{dx_{1}^{4}} + H_{22}^{C} \frac{d^{4}U_{3}}{dx_{1}^{4}} = P_{3}(x_{1})$$

COMBINING TO SOLVE FOR d'U2/dx,4 & d'U3/dx,4 YIELDS

$$\frac{d^4 U_2}{d x_1^4} = \frac{H_{22}}{\Delta H} p_2(x_1) - \frac{H_{23}}{\Delta H} p_3(x_1)$$

$$\frac{\mathcal{B}.\mathcal{C}s}{\frac{\partial \mathcal{U}_2}{\partial x_1} = \frac{\partial \mathcal{U}_3}{\partial x_1} = 0}$$

$$\frac{\partial^{2} U_{2}}{\partial x_{1}^{2}} = \frac{\partial^{2} U_{3}}{\partial x_{1}^{2}} = \frac{\partial^{2} U_{3}}{\partial x_{1}^{2}} = \frac{\partial^{3} U_{3}}{\partial x_{1}^{3}} = \frac{\partial^$$

$$\frac{d^{4} V_{z}}{d x_{1}^{u}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( 1 - \left( \frac{x_{1}}{L} \right)^{2} \right) + \frac{H_{zz}^{c}}{\Delta H} P_{p} \left( 1 - \frac{x_{1}}{L} \right)$$

$$\frac{d^{3} U_{z}}{d x_{1}^{3}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1} - \frac{x_{1}^{3}}{3L^{c}}}{\frac{3}{L^{c}}} \right) + \frac{H_{zz}^{c}}{\Delta H} P_{D} \left( \frac{x_{1} - \frac{x_{1}^{c}}{2L}}{\frac{2}{L^{c}}} \right) + C_{1}$$

$$\frac{d^{3} U_{z}}{d x_{1}^{3}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1} - \frac{x_{1}^{3}}{3L^{c}}}{\frac{3}{L^{c}}} \right) + \frac{H_{zz}^{c}}{\Delta H} P_{D} \left( \frac{1}{2} L \right) + C_{1}$$

$$\frac{d^{3} U_{z}}{d x_{1}^{3}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1} - \frac{x_{1}^{3}}{3L^{c}}}{\frac{3}{L^{c}}} \right) + \frac{H_{zz}^{c}}{\Delta H} P_{D} \left( \frac{x_{1} - \frac{x_{1}^{c}}{2L}}{\frac{2}{L^{c}}} \right) + C_{1}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{12L^{c}} \right) + \frac{L_{x_{1}}^{c}}{2L} - \frac{L_{x_{1}}^{c}}{2L} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{12L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{D} \left( -\frac{1}{2} L^{c} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{12L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{D} \left( -\frac{1}{2} L^{c} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{12L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{D} \left( -\frac{1}{2} L^{c} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{12L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{D} \left( -\frac{1}{2} L^{c} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{12L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{D} \left( -\frac{1}{2} L^{c} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{2L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{D} \left( -\frac{1}{2} L^{c} \right) + C_{2}$$

$$\frac{d^{2} U_{z}}{d x_{1}^{2}} = \frac{H_{zz}^{c}}{\Delta H} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{2L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{2L^{c}} \right) + \frac{L_{z}^{c}}{2L} P_{L} \left( \frac{x_{1}^{c}}{2} - \frac{x_{1}^{c}}{2L^{c}} \right) + \frac$$

$$\frac{d^{2}U_{2}}{dx_{1}^{2}} = \frac{H_{22}}{\Delta H} P_{L} \left( \frac{x_{1}^{2} - \frac{x_{1}U}{2} - \frac{2Lx_{1} + 1L^{2}}{3} + \frac{1L^{2}}{4} \right)$$

$$+ \frac{H_{2}}{\Delta H} P_{D} \left( \frac{x_{1}^{2} - \frac{x_{1}^{3}}{6L} - \frac{Lx_{1} + 1L^{2}}{2} + \frac{1L^{2}}{6L} \right)$$

Recall the Sedional constitutive equation  $\frac{d^2 u_2}{d \times l^2} = \frac{H_{23}}{\Delta H} \frac{U_2}{\Delta H} + \frac{H_{22}}{\Delta H} \frac{U_3}{\Delta H}$ 

HENCE WE HAVE ALSO FOUND

$$M_{2} = P_{p} \left( \frac{x_{1}^{2} - x_{1}^{3} - Lx_{1} + L^{2}}{2} \right)$$

$$M_{3} = P_{L} \left( \frac{x_{1}^{2} - x_{1}^{4} - 2Lx_{1} + L^{2}}{2} \right)$$

$$\frac{1}{2} \left( \frac{x_{1}^{2} - x_{1}^{4} - 2Lx_{1} + L^{2}}{2} \right)$$

-> MATCHES PREVIOUS ANSWERS!

# PART (d) SOLVE U.

## -> RECOGNIZE H23 70!

-> WITH M2 AND M3 KNOWN WE MAY SOLVE USING THE SECTIONAL CONSTITUTIVE EQUATIONS.

$$K_{2} = H_{33} \quad M_{2} + H_{23} \quad M_{3} = -\frac{d^{2}U_{3}}{dx_{1}^{2}} \quad Q \quad x_{1} = 0$$

$$\frac{\Delta H}{\Delta H} \quad \frac{\Delta H}{\Delta H} \quad \frac{d^{2}U_{2}}{dx_{1}^{2}} \quad U_{2} = u_{3} = 0$$

$$K_{3} = H_{23} \quad M_{2} + H_{22} \quad M_{3} = \frac{d^{2}U_{2}}{dx_{1}} \quad \frac{dU_{2}}{dx_{1}} = \frac{dU_{3}}{dx_{1}} = 0$$

$$\frac{\Delta H}{\Delta H} \quad \frac{\Delta H}{\Delta H} \quad \frac{d^{2}U_{2}}{dx_{1}^{2}} \quad \frac{dU_{3}}{dx_{1}} = 0$$

$$\frac{d^{2}U_{2}}{d\times^{2}} = \frac{H_{23}}{\Delta H} P_{D} \left( \frac{\times^{2} - \times^{3}}{6L} - \frac{L\times_{1} + L^{2}}{2} \right)$$

$$\frac{+ \frac{1}{122} P_{L} \left( \frac{x_{1}^{2} - x_{1}}{2 \frac{12L^{2}}{3} - \frac{2Lx_{1}}{3} + \frac{L^{2}}{4} \right)}{\frac{2}{12L^{2}}}$$

$$\frac{dU_{2}}{dx_{1}} = \frac{H_{23}^{c}}{\Delta H} P_{D} \left( \frac{x_{1}^{3} - x_{1}^{4}}{6} - \frac{Lx_{1}^{2}}{4} + \frac{L^{2}x_{1}}{6} \right)$$

$$\frac{+ \frac{1}{122} P_{L} \left( \frac{X_{1}^{3} - \frac{X_{1}^{5} - 2L^{X_{1}^{2}}}{6} + \frac{L^{2}X_{1}}{4} \right) + C_{1}}{6 + \frac{1}{6} \frac{1$$

$$U_{2} = \frac{H_{23}^{C}}{2H} P_{0} \left( \frac{x_{1}^{4}}{24} - \frac{x_{1}^{5}}{120L} - \frac{Lx_{1}^{3}}{12} + \frac{L^{2}x_{1}^{2}}{12} \right)$$

$$+\frac{H_{22}^{C}}{\Delta H}P_{L}\left(\frac{x_{1}^{4}-\frac{x_{1}^{6}}{360L^{2}}-\frac{1}{9}Lx_{1}^{3}+\frac{L^{2}x_{1}^{2}}{8}\right)+L_{2}^{2}$$

$$U_{2} = \frac{H_{23}^{C}}{\Delta H} P_{0} \left( \frac{x_{1}}{2q} - \frac{x_{1}}{120L} - \frac{Lx_{1}}{12} + \frac{L^{2}x_{1}^{2}}{12} \right) + \frac{H_{22}^{C}}{\Delta H} P_{1} \left( \frac{x_{1}^{q}}{2q} - \frac{x_{1}^{6}}{360L^{2}} - \frac{1}{q} Lx_{1}^{3} + L^{2}x_{1}^{2} \right)$$

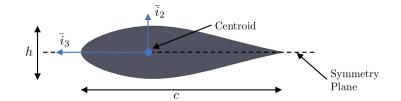
By imprection

$$U_{3} = -\frac{H_{33}}{\Delta H} P_{D} \left( \frac{x_{1}^{4} - x_{1}^{5} - Lx_{1}^{3} + L^{2}x_{1}^{2}}{24 - 120L} - \frac{Lx_{1}^{3} + L^{2}x_{1}^{2}}{12} \right)$$

$$-\frac{H_{23}^{2}}{\Delta H} P_{2} \left( \frac{x_{1}^{4} - x_{1}^{6} - Lx_{1}^{3} + L^{2}x_{1}^{2}}{360L^{2}} - \frac{L}{2} Lx_{1}^{3} + L^{2}x_{1}^{2} \right)$$

$$U_1 = -x_3 \frac{dU_3}{dx_1} - x_2 \frac{dU_2}{dx_1}$$

## PART (C)



For the special case of  $P_L/P_D = 1$  and c/h = 5, find a good **estimate** for the equation of the neutral axis at the root of the beam  $(x_1 = 0)$ . Sketch the neutral axis.

**Hint:** You will have to make some estimates here about the stiffnesses of this cross-section. You may also estimate any necessary results that you did not already find in parts a) and b) above.

$$O_1 = E\left(\frac{N_1 + x_3}{S} + \frac{H_{33}}{S} + \frac{N_2 + H_{23}}{S} + \frac{N_3}{S} + \frac{N_4}{S} + \frac{N_5}{S} + \frac$$

SINCE THE AIRFOIL IS SYMMETRIC,
H23 = 0

$$\sigma_1 = E\left(\frac{\mathcal{M}_2}{\mathcal{N}_{22}^c} \times_3 - \frac{\mathcal{M}_3}{\mathcal{N}_{23}^c} \times_2\right)$$

NOW WE ESTINATE M2, M3, H22, H33 (ASSUME WE PIP NOT SOLVE (a) or (b))

$$M_3 - P_{c.l^2}$$
,  $M_2 \sim P_{pl}^2$   
 $H_{22}^{c} \sim Ehc^3$ ,  $H_{33}^{c} \sim Eeh^3$ 

$$\sigma_1 = E \left( \frac{P_0 L^2}{E_h c^3} \times_3 - \frac{P_L L^2}{E_h^3 c} \times_2 \right)$$

$$\sigma_1 = \frac{P_L L^2}{h^3 c} \left( \frac{P_P (h)^2 x_3 - x_2}{P_L} \right) = 0$$

The neutral aseis is given by

$$\frac{*}{2} = \frac{P_L}{P_D} \left(\frac{h}{c}\right)^2 \times_3$$

Useng the given numbers

$$*$$
  $\times_3 = 1 \times_2$   $\times_2$ 

