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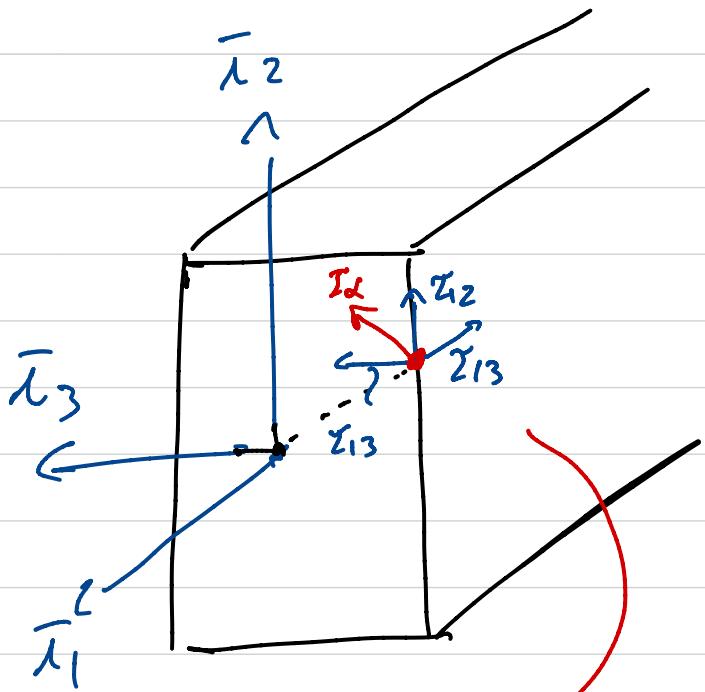
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# Torsion at bars w/ arbitrary cross-sections



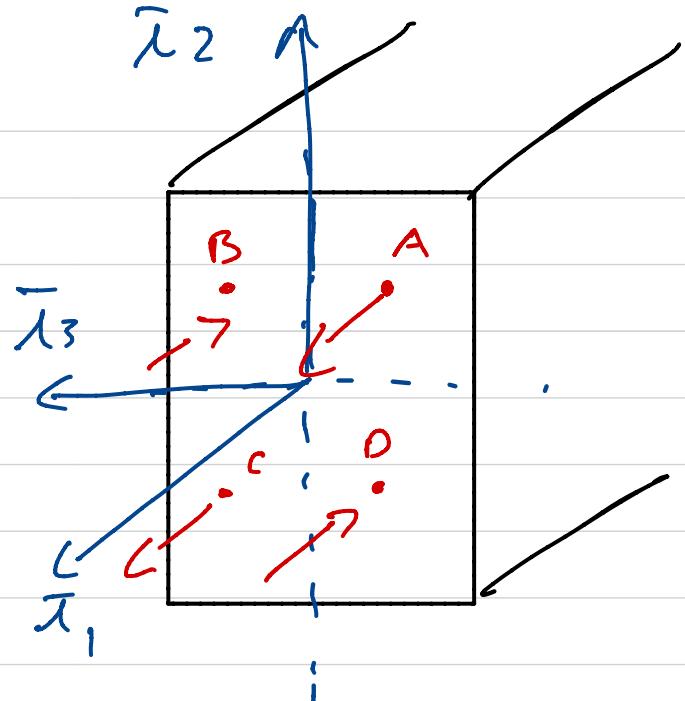
If stress is at the form

$$\begin{cases} \tau_{12} = G \cdot \gamma_1 \\ \tau_{13} = 0 \end{cases}$$

We would have a non-physical state at stress

This surface is often free, hence  $\gamma_{13} = 0$

- \* At any point along the edge of the bar's section, the shear stress must be tangent to the edge.



Due to antisymmetry  
at the loading  
about  $(\bar{x}_2, \bar{x}_1)$  planes

$$U_1^A = -U_1^B, U_1^C = U_1^D$$

About  $(\bar{x}_3, \bar{x}_1)$  plane

$$U_1^A = -U_1^D, U_1^B = -U_1^C$$

Combining

$$U_1^A = -U_1^B = U_1^C = -U_1^D$$

\* The section at loss with  
arbitrary cross-section will  
work.

# Saint - Venant's Solution

Kinematic Assumptions:

- \* Each cross-section rotates like a rigid body & warps out at plane

$$u_2 = -x_3 \phi_1(x_1)$$

$$u_3 = x_2 \phi_1(x_1)$$

$$u_1 = \psi(x_2, x_3) \cdot K_1(x_1)$$

↑ Warping Function.

- $u_1$  is proportional to  $K_1$  through  $\psi(x_2, x_3)$
- We will assume that the twist rate is constant

$$K_1 = \frac{d\phi_1}{dx_1} = \text{constant}$$

Referred to as unit torsion

## Strain

$$\epsilon_1 = \frac{\partial U_1}{\partial x_1} = \varphi(x_2, x_3) \cdot \frac{\partial K_1}{\partial x_1} = 0$$

$$\epsilon_2 = \epsilon_3 = 0, \gamma_{23} = 0$$

$$\begin{aligned}\gamma_{12} &= \frac{\partial U_1}{\partial x_2} + \frac{\partial U_2}{\partial x_1} = \left( \frac{\partial \varphi}{\partial x_2} \cdot K_1 - x_3 K_1 \right) \\ &= \left( \frac{\partial \varphi}{\partial x_2} - x_3 \right) K_1\end{aligned}$$

$$\begin{aligned}\gamma_{13} &= \frac{\partial U_1}{\partial x_3} + \frac{\partial U_3}{\partial x_1} = \left( \frac{\partial \varphi}{\partial x_3} K_1 + x_2 K_1 \right) \\ &= \left( \frac{\partial \varphi}{\partial x_3} + x_2 \right) K_1\end{aligned}$$

## Stress

$$\sigma_{12} = G \left( \frac{\partial \varphi}{\partial x_2} - x_3 \right) K_1$$

$$\sigma_{13} = G \left( \frac{\partial \varphi}{\partial x_3} + x_2 \right) K_1$$

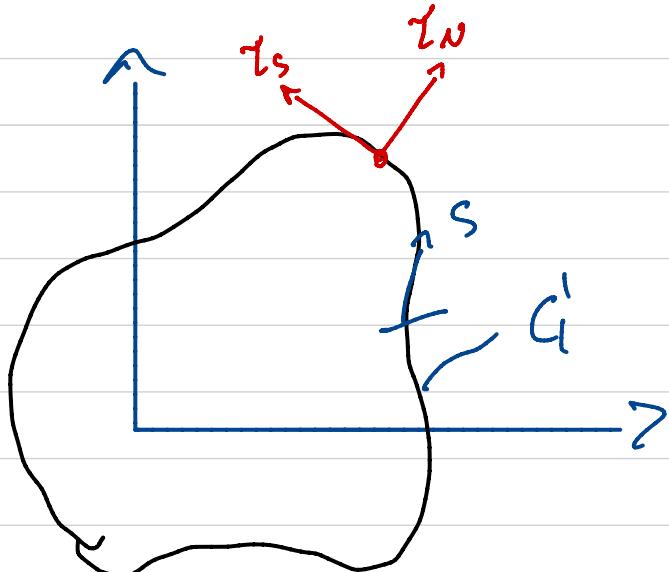
# Equilibrium & Boundary Conditions

$$\cancel{\frac{\partial \sigma_1}{\partial x_1}} + \frac{\partial \varphi_{12}}{\partial x_2} + \frac{\partial \varphi_{13}}{\partial x_3} + \cancel{\delta_1} = 0$$

$$\frac{\partial}{\partial x_2} \left[ G K_1 \left( \frac{\partial \varphi}{\partial x_2} - x_3 \right) \right]$$

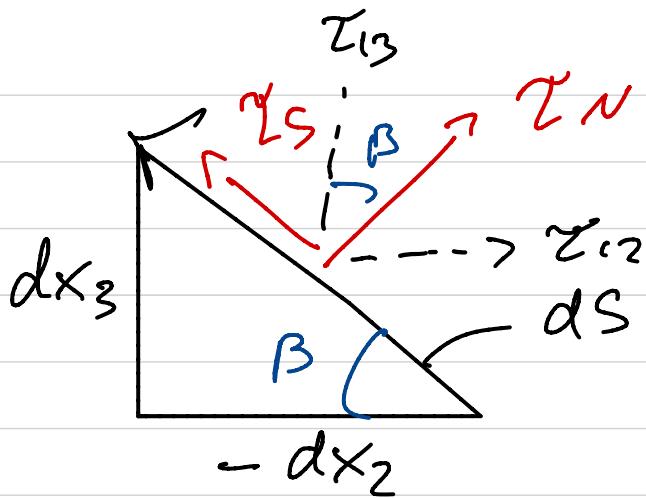
$$+ \frac{\partial}{\partial x_3} \left[ G K_1 \left( \frac{\partial \varphi}{\partial x_3} - x_2 \right) \right] = 0$$

$$\boxed{\frac{\partial^2 \varphi}{\partial x_2^2} + \frac{\partial^2 \varphi}{\partial x_3^2} = 0}$$



On the outer edge  
(curve  $C_1'$ ) we  
want

$$\varphi_n = 0$$



$$\begin{aligned}
 Z_N &= Z_{12} \sin(\beta) + Z_{13} \cos(\beta) \\
 &= Z_{12} \left( \frac{dx_3}{ds} \right) + Z_{13} \left( -\frac{dx_2}{ds} \right) = 0
 \end{aligned}$$

$$GK_1 \left[ \left( \frac{\partial \Psi}{\partial x_2} - x_3 \right) \left( \frac{dx_3}{ds} \right) \right]$$

$$- \left( \frac{\partial \Psi}{\partial x_3} + x_2 \right) \left( \frac{dx_2}{ds} \right) \right] = 0$$

$$= 0$$

Solve

$$0 = \frac{\partial^2 \Psi}{\partial x_2^2} + \frac{\partial^2 \Psi}{\partial x_3^2}, \text{ or } A$$

$$\left( \frac{\partial \Psi}{\partial x_2} - x_3 \right) \left( \frac{dx_3}{ds} \right) - \left( \frac{\partial \Psi}{\partial x_3} + x_2 \right) \left( \frac{dx_2}{ds} \right) = 0$$

on  $G_1$

# Prandtl Stress Function

Let  $\underline{\Phi}(x_2, x_3)$  be a function defined as

$$\tau_{12} = \frac{\partial \underline{\Phi}}{\partial x_3}, \quad \tau_{13} = -\frac{\partial \underline{\Phi}}{\partial x_2}$$

→ Automatically satisfies equilibrium

$$\frac{\partial \tau_{12}}{\partial x_2} + \frac{\partial \tau_{13}}{\partial x_3} = 0$$

$$\frac{\partial^2 \underline{\Phi}}{\partial x_2 \partial x_3} - \frac{\partial^2 \underline{\Phi}}{\partial x_3 \partial x_2} = 0 \quad \checkmark$$

Relates to  $\Psi(x_2, x_3)$  through

$$\tau_{12} = G K_1 \left( \frac{\partial \Psi}{\partial x_2} - x_3 \right) = \frac{\partial \underline{\Phi}}{\partial x_3}$$

$$\tau_{13} = G K_1 \left( \frac{\partial \Psi}{\partial x_3} + x_2 \right) = \frac{\partial \underline{\Phi}}{\partial x_2}$$

$$\frac{\partial \chi_{12}}{\partial x_3} = G K_1 \left( \frac{\partial^2 \Phi}{\partial x_2 \partial x_3} - 1 \right) = \frac{\partial^2 \Phi}{\partial x_3^2}$$

$$\frac{\partial \chi_{13}}{\partial x_2} = G K_1 \left( \frac{\partial^2 \Phi}{\partial x_2 \partial x_3} + 1 \right) = - \frac{\partial^2 \Phi}{\partial x_2^2}$$

Subtracting

$$-2 G K_1 = \frac{\partial^2 \Phi}{\partial x_3^2} + \frac{\partial^2 \Phi}{\partial x_2^2}$$

$\rightarrow$  Goedeberg Equation for  $\Phi$

Boundary Condition

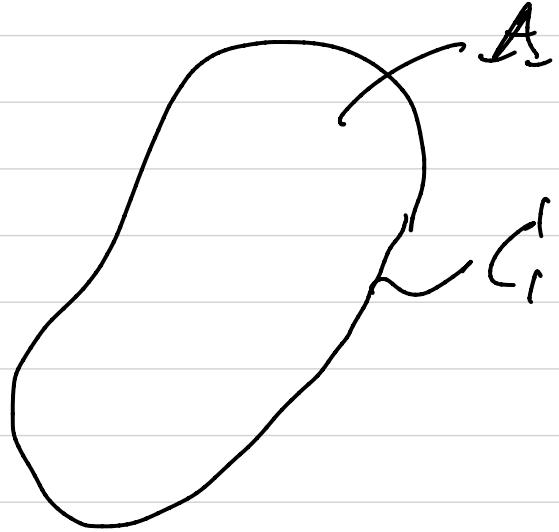
$$\mathcal{I}_N = \chi_{12} \frac{dx_3}{ds} + \chi_{13} \left( - \frac{dx_2}{ds} \right) = 0$$

$$\mathcal{I}_N = \frac{\partial \Phi}{\partial x_3} \frac{dx_3}{ds} + \frac{\partial \Phi}{\partial x_2} \frac{dx_2}{ds} = 0$$

$$\rightarrow \chi_N = \frac{\partial \Phi}{\partial s} = 0$$

$\rightarrow \Phi$  must be a constant along the edge!

→ For a solid cross-section bounded by a single curve, we may choose  $\Phi = 0$  on the boundary



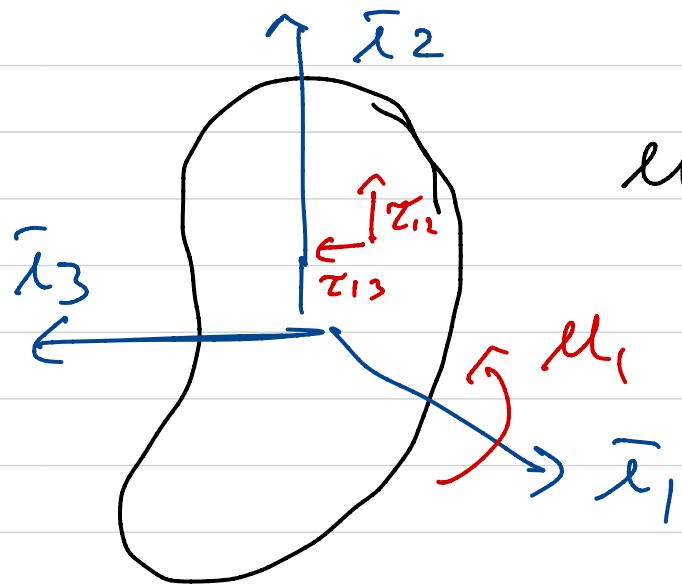
Solve

$$-2GK_1 = \frac{\partial^2 \Phi}{\partial x_2^2} + \frac{\partial^2 \Phi}{\partial x_3^2}$$

on A

$\Phi = 0$  on C\_1

# Sectional Equilibrium



$$M_1 = \int_A (x_2 \tau_{13} - x_3 \tau_{12}) dA$$

For a solid cross-section bounded by a single curve

$$M_1 = 2 \cdot \int_A \bar{\Phi} dA$$

# Summary

## Kinematics

$$d_2 = -x_3 \phi_1(x_1) \quad K_1 = \text{const!}$$

$$d_3 = x_2 \phi_1(x_1)$$

$$d_1 = q(x_2, x_3) \cdot K_1$$

$\underline{\Phi}(x_2, x_3)$  - Prandtl Stress Function

$$\gamma_{12} = \frac{\partial \underline{\Phi}}{\partial x_3}, \quad \gamma_{13} = -\frac{\partial \underline{\Phi}}{\partial x_2}$$

Solve:  $\frac{\partial^2 \underline{\Phi}}{\partial x_2^2} + \frac{\partial^2 \underline{\Phi}}{\partial x_3^2} = -2 \cdot G \cdot K_1$  on A

with  $\frac{\partial \underline{\Phi}}{\partial S} = 0$  ( $\underline{\Phi} = \text{const.}$ ) on  $G'$

Find:  $H_{11} = \frac{M_1}{K_1}$  once  $\underline{\Phi}$  is known

using  $M_1 = 2 \cdot \int_A \underline{\Phi} dA$

Knowing  $H_{11}$  we may solve  
 $\Phi_1(x_1)$  using the gauging equations.

$$\frac{d}{dx_1} \left[ H_{11} \frac{d\Phi_1}{dx_1} \right] = -q_1(x_1)$$

Solve for  $\Phi(x_2, x_3)$  from

$$Z_{12} = \frac{\partial \bar{\Phi}}{\partial x_3} = GK_1 \left( \frac{\partial \Phi}{\partial x_2} - x_3 \right)$$

$$Z_{13} = \frac{\partial \bar{\Phi}}{\partial x_2} = GK_1 \left( \frac{\partial \Phi}{\partial x_3} + x_2 \right)$$