

Technical Team

Applicant: VortexChem

Inventors: P. Shruti Sekhar , Shantanu Prakash

Chemical Formula: $C_{28}H_{22}Cl_2FNO_3$

Chemical Name: Flumethrin

Cyano(4-fluoro-3-phenoxyphenyl)methyl

3-[(Z)-2-chloro-2-(4-chlorophenyl)ethenyl]-2,2-dimethylcyclopropane-1-carboxylate

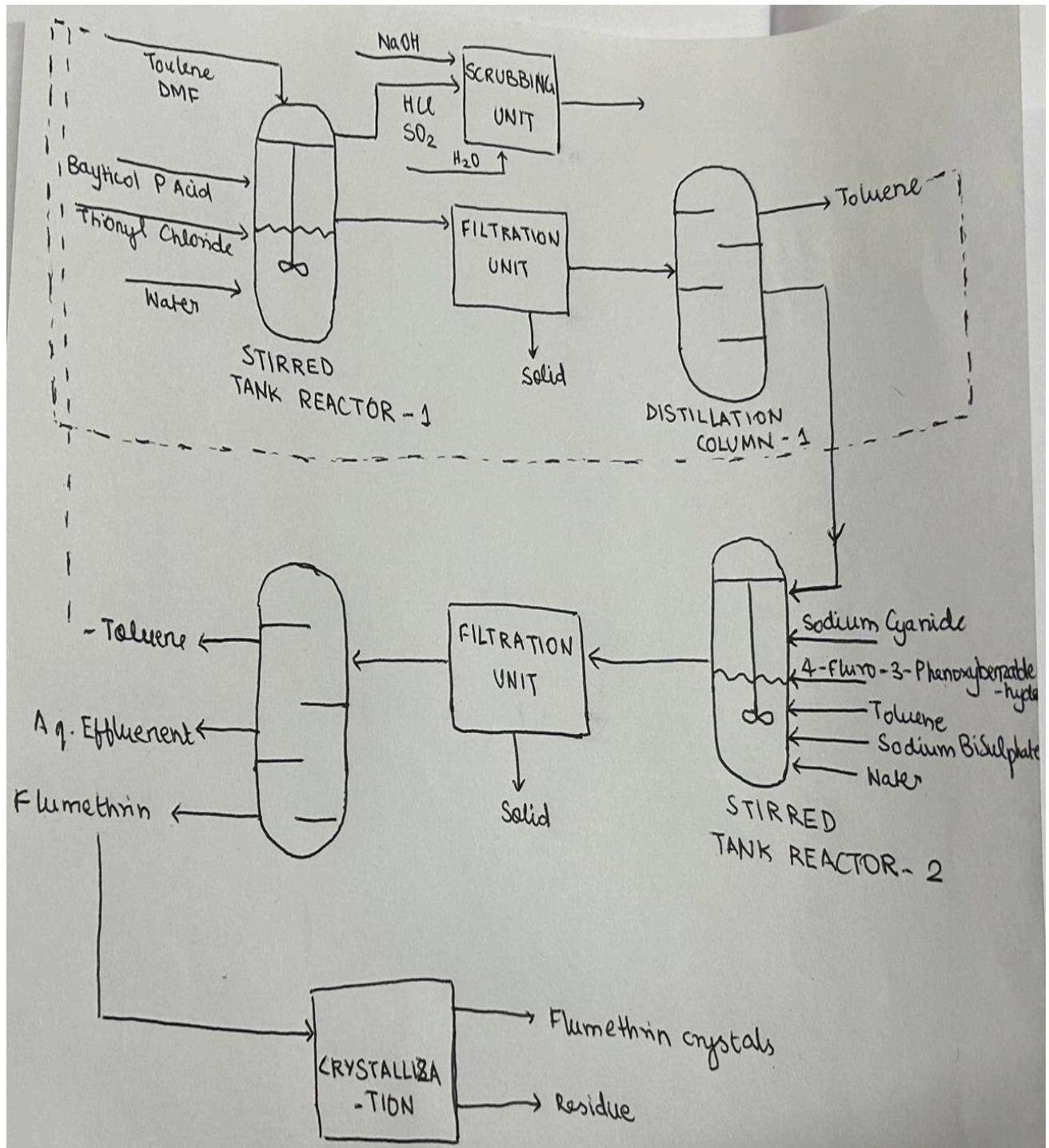
Process Title: Industrial Production of Flumethrin

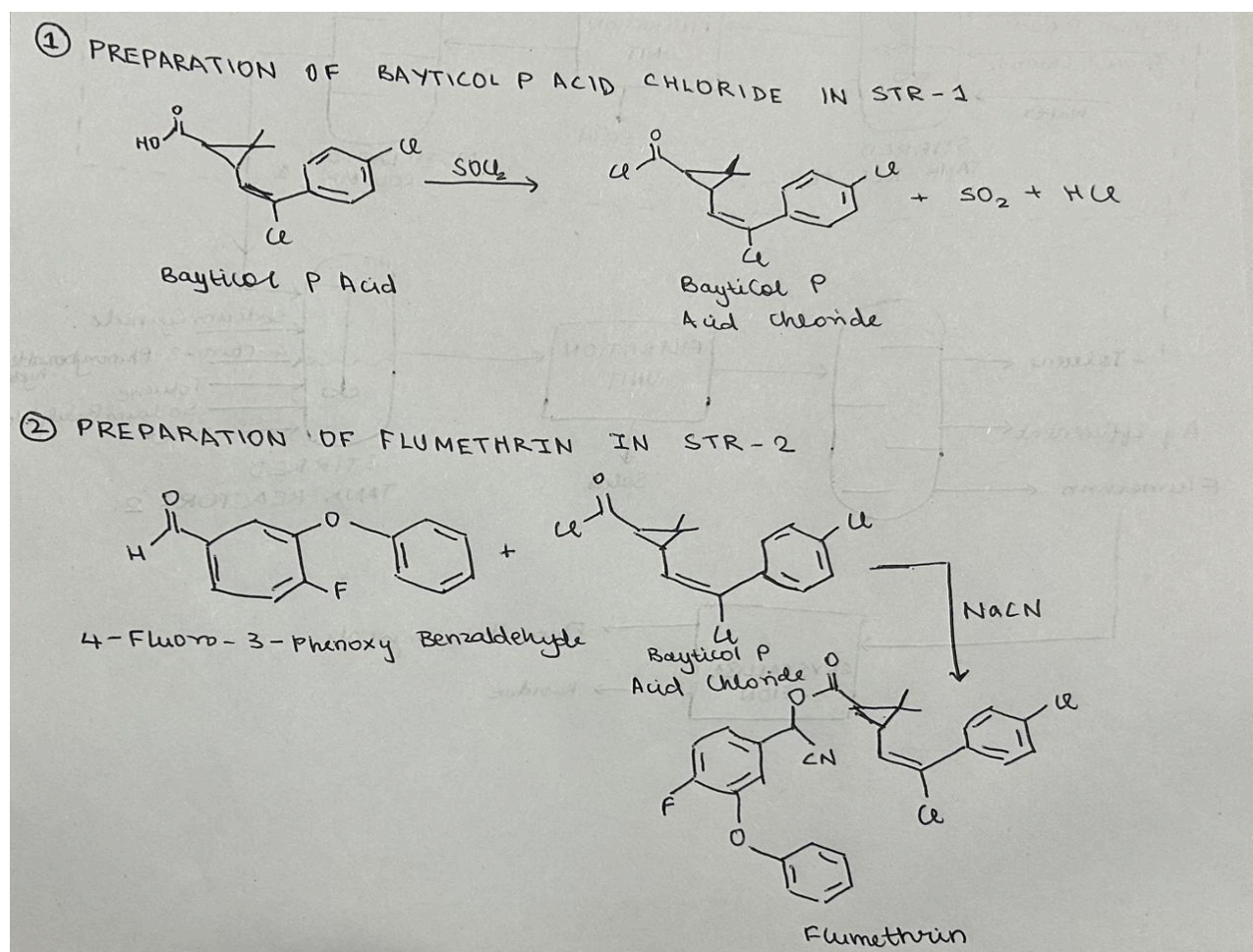
Raw materials and chemicals required: 4-Fluoro-3-Phenoxybenzaldehyde, Bayticol P Acid Chloride, Sodium Cyanide (NaCN), Thionyl Chloride, Toluene, DMF, NaOH, HCl, SO₂, Water.

Process Description:

Flumethrin is synthesized through a multi-step reaction involving chlorination, cyanation, and purification.

1. Stirred Tank Reactor-1: Bayticol P Acid reacts with Thionyl Chloride in Toluene and DMF to form the acid chloride. Water is added to control excess SOCl₂.
2. Scrubbing Unit: Acidic gases (SO₂, HCl) are neutralized using NaOH to prevent environmental release.
3. Filtration & Distillation: Solid impurities are removed, and Toluene is recovered for reuse.
4. Stirred Tank Reactor-2: The acid chloride reacts with NaCN and 4-Fluoro-3-Phenoxybenzaldehyde in Toluene to form Flumethrin.
5. Final Purification: Filtration removes residual solids, and the purified product undergoes crystallization and drying. The final product purity is ~ **98%** .

Process Flowsheet for the production of Flumethrin :

Reactions Involved:

Reaction 1 :

Reactor Type : Stirred Tank Reactor

Operating Temperature : 80 C

Product Yield : 95 %

Reaction 2 :

Reactor Type : Stirred Tank Reactor

Operating Temperature : 60 C

Product Yield : 90 %

Material Balance:

Basis : 1000 kg Flumethrin / day

Assuming a yield of 90% for Reaction - 2,

Let 'x' be the flow rate (molar) of Flumethrin exiting STR-2,

MW (Flumethrin) = 510.4 g

$$x = \frac{1000 \text{ kg}}{\text{MW}_{\text{Flumethrin}}}$$

$$x = \frac{1000 \text{ kg}}{510.4 \text{ g}} = 1.96 \text{ kmol/day}$$

$$\text{Required 4F3P} \times 0.9 (\text{yield}) = 1.96 \text{ kmol/day}$$

$$\therefore \text{4-Fluoro-3-Phenoxy Benzaldehyde} = 2.177 \text{ kmol/day} \approx 2.2 \text{ kmol/day}$$

$$\text{Required Bayticol P-Acid Chloride} = 2.2 \text{ kmol/day}$$

$$\text{Mass of 4F3P (input to STR-2)} = 2.2 \times 216.2 \frac{\text{kg}}{\text{day}} = 471 \text{ kg/day}$$

$$\text{MW (4F3P)} = 216.2 \text{ g}$$

$$\text{Mass of Bayticol P-Acid Chloride (input to STR-2)} = 2.2 \times 303.6 \frac{\text{kg}}{\text{day}} = 661 \text{ kg/day}$$

$$\text{MW (Bayticol P-Acid Chloride)} = 303.6 \text{ g}$$

$$\text{Mass of NaCN (input to STR-2)} = 2.2 \times 49 \text{ kg/day} = 108 \text{ kg/day}$$

Assuming a yield of 95% for Reaction - 1,

$$\text{Required Bayticol P-Acid} \times 0.95 (\text{yield}) = 2.2 \text{ kmol/day}$$

$$\text{Req. Bayticol P-Acid} = 2.31 \text{ kmol/day}$$

$$\text{MW (Bayticol P-Acid)} = 283.2 \text{ g}$$

$$\text{Mass of Bayticol P-Acid (Input to STR-1)} = 653 \text{ kg/day}$$

$$\text{Req SOCl}_2 = 2.31 \text{ kmol/h}$$

$$\text{Mass of SOCl}_2 = 2.31 \times 118.97 \text{ kg/h} = 276 \text{ kg/day}$$

(input to STR-1)

$$\text{MW (SOCl}_2) = 118.97 \text{ g}$$

MASS BALANCE AROUND STR-1

$$\text{Mass of HCl} = 2.2 \times 36.5 \text{ kg/h} = 80 \text{ kg/day}$$

(Output from STR-1)

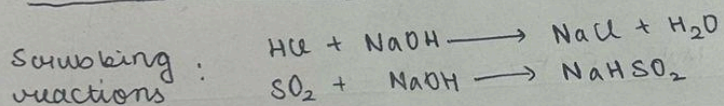
[Stoichiometric ratio of Bayticol P Acid Chloride, HCl and SO₂ is 1:1:1]

$$\text{Mass of SO}_2 = 2.2 \times 64 \text{ kg/h} = 141 \text{ kg/day}$$

(Output from STR-1)

$$\text{Mass of unreacted reactants} = 653 + 276 - 80 - 141 - 661 \frac{\text{kg}}{\text{day}} = 47 \text{ kg/day}$$

MASS BALANCE AROUND SCRUBBER



$$\text{NaOH req} = 2.2 + 2.2 \text{ kmol/day} = 4.4 \text{ kmol/day}$$

$$\text{Mass of NaOH (input to scrubber)} = 4.4 \times 40 \text{ kg/day} = 176 \text{ kg/day}$$

$$\therefore \text{Mass of Neutralized products} = \frac{397}{\text{day}} (141 + 80 + 176) \frac{\text{kg}}{\text{day}} = 397 \text{ kg/day}$$

PER DAY MATERIAL BALANCE:

INPUTS	MASS	OUTPUTS	MASS
Bayticol P Acid	653 kg	Bayticol P Acid chloride	661 kg
Thionyl Chloride	276 kg	Neutralized products	397 kg
NaOH	176 kg	Unreacted reactants	47 kg
TOTAL	1105 kg	TOTAL	1105 kg

Hence, Material balance around unit operations STR-1 and Scrubber is shown.

MASS BALANCE AROUND STR-2

~~Stoichiometric~~

$$\begin{aligned} \text{Mass of unreacted reactants} &= -\text{Mass of Flumethrin} + \text{Mass of input reactants} \\ &= -1000 + (471 + 661 + 108) \text{ kg/day} \\ \text{Mass of unreacted reactants} &= 240 \text{ kg/day} \end{aligned}$$

INPUTS	MASS	OUTPUTS	MASS
Baytisol P Acid Chloride	661 kg	Flumethrin	1000 kg
Sodium Cyanide	108 kg	Unreacted reactants	240 kg
AF 3 P	471 kg		
TOTAL	1240 kg	TOTAL	1240 kg

Hence, Material balance around unit operation STR-2 is shown.

The previous calculations were based on stoichiometric assumptions. However, in large-scale industrial production, inefficiencies such as side reactions, incomplete conversions, and material losses must be considered. Based on data from existing patents and research papers, the actual material balance accounts for these factors, ensuring a more realistic estimation of reactant consumption and product yield. These adjustments help optimize raw material usage, minimize waste, and improve overall process efficiency.

Additionally, the market analysis and other teams have relied on this industrial material balance for their assessments, as it provides a more accurate representation of real-world production conditions compared to theoretical stoichiometric data.

Step-1: Preparation of Bayticol P acid chloride

Material Balance:

Input	kg		Output	Kg
Bayticol P Acid	590	→	Bayticol P Acid Chloride	627
Thionyl Chloride	277		Toluene with product to stage 2	941
Toluene	1805		HCl gas	76
DMF	1		SO ₂ gas	130
Water	1544		Rec. Toluene	835
Sodium hydroxide	69		Aq. Effluent	1648
			Residue	29
	4286			4286

Step-2: Preparation of Flumethrin

Material Balance:

Input	kg		Output	Kg
Bayticol P Acid	627	→	Flumethrin	1000
Toluene with product to stage 2	941		Rec. Toluene	3026
4-Fluro 3-Phenoxy Benzaldehyde	430		Aq. Effluent	1605
Sodium Cyanide	222		Residue	89
Toluene	2174			

Sodium Bisulphite	111		
Water	1213		
Tetraytyl ammonium Bromide	2		
	5720		5720

Energy Balance:ENERGY BALANCE IN STR-1

Assuming all reactants are initially at room temperature, $T = 25^\circ\text{C}$.
STR-1 operates at $T = 80^\circ\text{C}$

\therefore Heat required to bring reactants to reaction temperature:

$$\Delta T = 55^\circ\text{C}$$

$$C_p(\text{SO}_2) \approx 0.86 \text{ kJ/kg}\cdot\text{K}$$

$$C_p(\text{Bayticol P Acid}) \approx 2.0 \text{ kJ/kg}\cdot\text{K}$$

$$C_p(\text{HCl aq}) \approx 4.18 \text{ kJ/kg}\cdot\text{K}$$

$$C_p(\text{SO}_2) \approx 0.62 \text{ kJ/kg}\cdot\text{K}$$

$$Q = m C_p \Delta T$$

$$\dot{Q}_{\text{BPA}} = 663 \frac{\text{kg}}{\text{day}} \times 2 \frac{\text{kJ}}{\text{kg}\cdot\text{K}} \times 55 \text{ K} = 7.830 \text{ kJ/day}$$

$$\dot{Q}_{\text{SO}_2} = 276 \frac{\text{kg}}{\text{day}} \times 0.86 \frac{\text{kJ}}{\text{kg}\cdot\text{K}} \times 55 \text{ K} = 13099 \text{ kJ/day}$$

$$\therefore \dot{Q}_{\text{total req}} = 84929 \text{ kJ/day} \approx 85000 \text{ kJ/day}$$

$\Delta H_{\text{rxn-1}} \approx -50 \text{ kJ/mol}$, 2.3 kmol/day of Bayticol P Acid ~~chloride~~

$$\therefore \Delta H = 50 \frac{\text{kJ}}{\text{mol}} \times 2.3 \frac{\text{kmol}}{\text{day}} = -115000 \text{ kJ/day}$$

This reaction is Exothermic.

$$\therefore \dot{Q}_{\text{net}} = 85000 - 115000 \text{ kJ/day} = -30000 \text{ kJ/day}$$

$$\boxed{\dot{Q}_{\text{net}} = -30000 \text{ kJ/day}}$$

ENERGY BALANCE IN STR-2

Assuming all reactants are initially at room temperature, $T = 25^\circ\text{C}$,
STR-2 operates at $T = 60^\circ\text{C}$

\therefore Heat required to bring reactants to reaction temperature:

$$\Delta T = 35^\circ\text{C}$$

$$C_p(\text{4F3P}) = 1.5 \text{ kJ/kg} \cdot \text{K}$$

$$C_p(\text{Bayticol P-Acid Chloride}) = 1.3 \text{ kJ/kg} \cdot \text{K}$$

$$C_p(\text{NaCN}) = 1.44 \text{ kJ/kg} \cdot \text{K}$$

$$\dot{Q} = \dot{m} C_p \Delta T$$

$$\dot{Q}_{\text{4F3P}} = 471 \frac{\text{kg}}{\text{day}} \times 1.5 \frac{\text{kJ}}{\text{kg} \cdot \text{K}} \times 35 \text{ K} = 24727.5 \text{ kJ/day}$$

$$\dot{Q}_{\text{BPAC}} = 661 \frac{\text{kg}}{\text{day}} \times 1.3 \frac{\text{kJ}}{\text{kg} \cdot \text{K}} \times 35 \text{ K} = 300039.5 \text{ kJ/day}$$

$$\dot{Q}_{\text{NaCN}} = 108 \frac{\text{kg}}{\text{day}} \times 1.44 \frac{\text{kJ}}{\text{kg} \cdot \text{K}} \times 35 \text{ K} = 5443.2 \text{ kJ/day}$$

$$\dot{Q}_{\text{total req}} \approx 60200 \text{ kJ/day}$$

$$\Delta H_{\text{rxn-2}} \approx -75 \text{ kJ/mol} \times 2.2 \frac{\text{kmol}}{\text{day}} \text{ of 4F3P}$$

$$\therefore \Delta H = -75 \frac{\text{kJ}}{\text{mol}} \times 2.2 \frac{\text{kmol}}{\text{day}} = -16350 \text{ kJ/day}$$

$$\therefore \dot{Q}_{\text{net}} = -16350 \frac{\text{kJ}}{\text{day}} + 60200 \text{ kJ/day}$$

$$\dot{Q}_{\text{net}} = -10390 \text{ kJ/day}$$

List of Contributions of each author:

P. Shruti Sekhar : Identified the chemical Flumethrin and the reactions involved in its production. Designed the process flow sheet and did the stoichiometric mass balance and drafted the technical patent.

Shantanu Prakash : Identified reactor types and other unit operations, estimated yield. Complete Stoichiometric Material balance , Energy balance and drafted the technical patent .

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