

# MECE 6388: HW #3

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September 29, 2018

## 2.2-7 Cubic performance index

Let

$$x_{k+1} = ax_k + bu_k,$$

where  $x_k$  and  $u_k$  are scalars, and

$$J = \frac{1}{3}s_N x_N^3 + \frac{1}{3} \sum_{k=0}^{N-1} (qx_k^3 + ru_k^3)$$

- (a) Write state and costate equations and stationarity condition.
- (b) When can we solve for  $u_k$ ? Under this condition, eliminate  $u_k$  from the equation.
- (c) Solve the open-loop control problem (i.e.,  $x_N$  fixed,  $s_N=0$ ,  $q=0$ ).

*Solution*

To solve the costate and stationarity conditions, we must first define the Hamiltonian function,  $H(x_k, u_k)$ . We start by defining the Hamiltonian function,  $H^k$ ,

$$H^k = L^k + \lambda_{k+1}^T f^k$$

where

$$\begin{aligned} L^k &= \frac{1}{3}(qx_k^3 + ru_k^3) \\ f^k &= ax_k + bu_k \end{aligned}$$

Therefore

$$H^k = \frac{1}{3}(qx_k^3 + ru_k^3) + \lambda_{k+1}(ax_k + bu_k)$$

The state, costate, and stationarity condition are given by the following equations

$$x_{k+1} = ax_k + bu_k \tag{1.1}$$

$$\begin{aligned} \lambda_k &= \frac{\partial H^k}{\partial x_k} = qx_k^2 + a\lambda_{k+1} \\ \lambda_k &= qx_k^2 + a\lambda_{k+1} \end{aligned} \tag{1.2}$$

$$\begin{aligned} 0 &= \frac{\partial H^k}{\partial u_k} = ru_k^2 + b\lambda_{k+1} \\ u_k^2 &= -\frac{b}{r}\lambda_{k+1} \\ u_k &= \sqrt{-\frac{b}{r}\lambda_{k+1}} \end{aligned} \tag{1.3}$$

b) Given the constraints in our equation for  $u_k$ , we can see that the terms inside the square root must be positive. We know that  $r > 0$  so that gives us the constraint

$$-b\lambda_{k+1} \geq 0$$

Assuming that this condition is true, we can plug (1.3) into (1.1) and (1.2) to give us the state and costate equations without  $u_k$

$$x_{k+1} = ax_k + b\left(\sqrt{-\frac{b}{r}\lambda_{k+1}}\right)$$

$$\boxed{\begin{aligned} x_{k+1} &= ax_k + \left(\sqrt{-\frac{b^3}{r}\lambda_{k+1}}\right) \\ \lambda_k &= qx_k^2 + a\lambda_{k+1} \end{aligned}}$$

c) To solve the open loop control problem, we let  $s_N = q = 0, r = 1$ .  
Now we can write our state and costate equations solved in part b) as

$$\begin{aligned} \lambda_k &= a\lambda_{k+1} \\ \lambda_k &= a^{N-k}\lambda_N \end{aligned} \tag{1.4}$$

$$\begin{aligned} x_{k+1} &= ax_k + \left(\sqrt{-b^3\lambda_{k+1}}\right) \\ x_{k+1} &= ax_k + \sqrt{-b^3a^{N-k-1}\lambda_N} \end{aligned} \tag{1.5}$$

Plugging in for  $k=0,1,2,3$  gives us

$$\begin{aligned} x_1 &= ax_0 + \sqrt{-b^3a^{N-1}\lambda_N} \\ x_2 &= a^2x_0 + \sqrt{-b^3a^{N+1}\lambda_N} + \sqrt{-b^3a^{N-2}\lambda_N} \\ x_3 &= a^3x_0 + \sqrt{-b^3a^{N+3}\lambda_N} + \sqrt{-b^3a^N\lambda_N} + \sqrt{-b^3a^{N-3}\lambda_N} \\ x_k &= a^kx_0 + \sqrt{-b^3\lambda_N} \sum_{i=0}^{k-1} (\sqrt{a^{N+2k-3-3i}}) \\ x_k &= a^kx_0 + \sqrt{-b^3\lambda_N a^{N+2k-3}} \sum_{i=0}^{k-1} (a^{-\frac{3}{2}i}) \end{aligned} \tag{1.6}$$

Using the formula for the sum of a geometric series, we can rewrite (1.6) as

$$x_k = a^kx_0 + \sqrt{-b^3\lambda_N a^{N+2k-3}} \left( \frac{1 - a^{-\frac{3}{2}k}}{1 - a^{-\frac{3}{2}}} \right) \tag{1.7}$$

Since the final state is fixed ( $x_N = r_N$ ) we can write

$$\begin{aligned} x_N &= r_N = a^N x_0 + \sqrt{-b^3\lambda_N a^{3N-3}} \left( \frac{1 - a^{-\frac{3}{2}N}}{1 - a^{-\frac{3}{2}}} \right) \\ \frac{(r_N - a^N x_0)(1 - a^{-\frac{3}{2}})}{1 - a^{-\frac{3}{2}N}} &= \sqrt{-b^3\lambda_N a^{3N-3}} \end{aligned}$$

$$\boxed{\lambda_N = -\frac{(r_N - a^N x_0)^2 (1 - a^{-\frac{3}{2}})^2}{a^{3N-3} b^3 (1 - a^{-\frac{3}{2}N})^2}} \tag{1.8}$$

We can use equation (1.4) to solve for  $\lambda_k$  now that we have  $\lambda_N$ .

$$\lambda_k = a^{N-k} \lambda_N$$

Once we have  $\lambda_k$ , we can solve for  $u_k$  using equation (1.3).

$$u_k = \sqrt{-\frac{b}{r} \lambda_{k+1}}$$

Finally, once we have  $u_k$ , we can solve for  $x_k$  forward in time using equation (1.1)

$$x_{k+1} = ax_k + bu_k$$

## 2.3-1 Digital control of harmonic oscillator

A harmonic oscillator is described by

$$\dot{x}_1 = x_2 \quad (2.1)$$

$$\dot{x}_2 = -\omega_n^2 x_1 + u \quad (2.2)$$

- (a) Discretize the plant using a sampling period of T.
- (b) With the discretized plant, associate a performance index of

$$J = \frac{1}{2}[s_1(x_N^1)^2 + s_2(x_N^2)^2] + \frac{1}{2} \sum_{k=0}^{N-1} [q_1(x_k^1)^2 + q_2(x_k^2)^2 + ru_k^2]$$

where the state is  $x_k = [x_k^1 \quad x_k^2]^T$ . Write scalar equations for a digital optimal controller.

- (c) Write a MATLAB subroutine to simulate the plant dynamics and use the time response program lsim.m to obtain zero-input state trajectories.
- (d) Write a MATLAB subroutine to compute and store the optimal control gains and to update the control  $u_k$  given the current state  $x_k$ . Write a MATLAB driver program to obtain time response plots for the optimal controller.

*Solution*

- a) To discretize the plant, we use the following equations.

$$A^s = e^{AT} \quad (2.3)$$

$$B^s = \int_0^T e^{A\tau} B d\tau \quad (2.4)$$

where A, B are found by putting the plant into the state space form  $\dot{x} = Ax + Bu$ . Equations (2.1) and (2.2) can be rewritten as

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

which tells us that  $A = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & 0 \end{bmatrix}$ ,  $B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$ . We can solve for the eigenvalues of A,  $\lambda_{1,2} = \pm j\omega_n$ .

To solve equation (2.3), we will invoke the Cayley-Hamilton Theorem. The Cayley-Hamilton Theorem states that the matrix exponential  $e^{AT}$  can be solved by

$$e^{AT} = \sum_{k=0}^{n-1} \alpha_k A^k \quad (2.5)$$

$$e^{\lambda_i T} = \sum_{k=0}^{n-1} \alpha_k \lambda_i^k \quad (2.6)$$

where the  $\alpha_i$ 's are determined from the set of equations given by the eigenvalues of A. Using (2.5), we can write

$$e^{AT} = \alpha_0 I + \alpha_1 A$$

To solve for  $\alpha_0, \alpha_1$ , we use equation (2.6)

$$\begin{aligned} e^{-\omega_n T j} &= \alpha_0 - j\omega_n \alpha_1 \\ \cos(-\omega_n T) + j\sin(-\omega_n T) &= \alpha_0 - j\omega_n \alpha_1 \end{aligned} \quad (2.7)$$

$$\begin{aligned} e^{\omega_n T j} &= \alpha_0 + j\omega_n \alpha_1 \\ \cos(\omega_n T) + j\sin(\omega_n T) &= \alpha_0 + j\omega_n \alpha_1 \end{aligned} \quad (2.8)$$

(2.7)+(2.8) gives us

$$\begin{aligned} 2\cos(\omega_n T) &= 2\alpha_0 \\ \alpha_0 &= \cos(\omega_n T) \end{aligned} \quad (2.9)$$

Plugging in (2.9) to (2.7)

$$\begin{aligned} \cos(-\omega_n T) + j\sin(-\omega_n T) &= \cos(\omega_n T) - j\omega_n \alpha_1 \\ \sin(-\omega_n T) &= -\omega_n \alpha_1 \\ \alpha_1 &= \frac{\sin(\omega_n T)}{\omega_n} \end{aligned} \quad (2.10)$$

Now that we have  $\alpha_0, \alpha_1$ , we can find  $e^{AT}$  from (2.5)

$$\begin{aligned} e^{AT} &= (\cos(\omega_n T))I + \left(\frac{\sin(\omega_n T)}{\omega_n}\right)A \\ e^{AT} &= \begin{bmatrix} \cos(\omega_n T) & \frac{\sin(\omega_n T)}{\omega_n} \\ -\omega_n \sin(\omega_n T) & \cos(\omega_n T) \end{bmatrix} \end{aligned} \quad (2.11)$$

Now that we have  $A^s$ , we can plug (2.11) into (2.4) to solve for  $B^s$

$$\begin{aligned} B^s &= \int_0^T e^{A\tau} B d\tau \\ B^s &= \int_0^T \begin{bmatrix} \cos(\omega_n \tau) & \frac{\sin(\omega_n \tau)}{\omega_n} \\ -\omega_n \sin(\omega_n \tau) & \cos(\omega_n \tau) \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} d\tau \\ B^s &= \int_0^T \begin{bmatrix} \frac{\sin(\omega_n \tau)}{\omega_n} \\ \cos(\omega_n \tau) \end{bmatrix} d\tau \\ B^s &= \begin{bmatrix} \frac{-\cos(\omega_n \tau)}{\omega_n^2} \Big|_0^T \\ \frac{\sin(\omega_n \tau)}{\omega_n} \Big|_0^T \end{bmatrix} \\ B^s &= \begin{bmatrix} \frac{1}{\omega_n^2} (1 - \cos(\omega_n T)) \\ \frac{\sin(\omega_n T)}{\omega_n} \end{bmatrix} \end{aligned} \quad (2.12)$$

$$x_{k+1} = \begin{bmatrix} \cos(\omega_n T) & \frac{\sin(\omega_n T)}{\omega_n} \\ -\omega_n \sin(\omega_n T) & \cos(\omega_n T) \end{bmatrix} x_k + \begin{bmatrix} \frac{1}{\omega_n^2} (1 - \cos(\omega_n T)) \\ \frac{\sin(\omega_n T)}{\omega_n} \end{bmatrix} u_k$$

b) Since we know that  $S_k$  is symmetric for all  $k$ , let

$$S_k = \begin{bmatrix} s_1 & s_2 \\ s_2 & s_3 \end{bmatrix}$$

Then the feedback gain is updated by

$$\begin{aligned} \delta &= B^T S_{k+1} B + r \\ \delta &= r + \frac{s_1 T^4}{4} + s_2 T^3 + s_3 T^2 \\ K_k &= B^T S_{k+1} A \frac{1}{\delta} \end{aligned}$$

We can write

$$\begin{aligned} k_1 &= \left(\frac{s_1 T^2}{2} + s_2 T\right) \frac{1}{\delta} \\ k_2 &= \left(\frac{s_1 T^3}{2} + \frac{3s_2 T^2}{2} + s_3 T\right) \frac{1}{\delta} \end{aligned}$$

We can write the closed-loop plant matrix

$$A_k^{cl} = A - BK_k$$

$$A_k^{cl} = \begin{bmatrix} a_{11}^{cl} & a_{12}^{cl} \\ a_{21}^{cl} & a_{22}^{cl} \end{bmatrix} = \begin{bmatrix} 1 - \frac{k_1 T^a}{2} & T - \frac{k_2 T^2}{2} \\ -k_1 T & 1 - k_2 T \end{bmatrix}$$

The updated cost kernel is

$$S_k = A^T S_{k+1} A_k^{cl} + Q$$

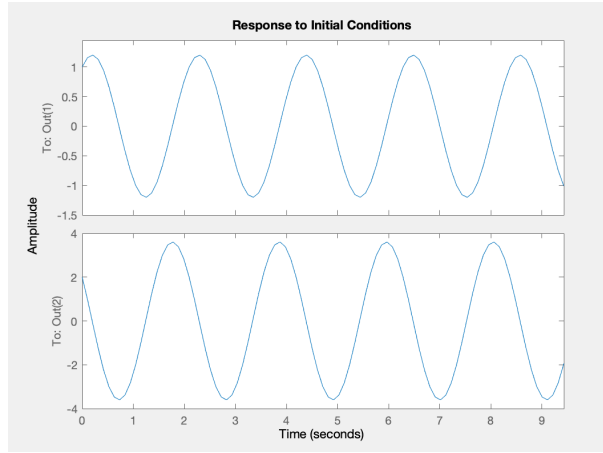
which yields the scalar updates:

$$s_1 = s_1 a_{11}^{cl} + s_2 a_{22}^{cl} + q_d$$

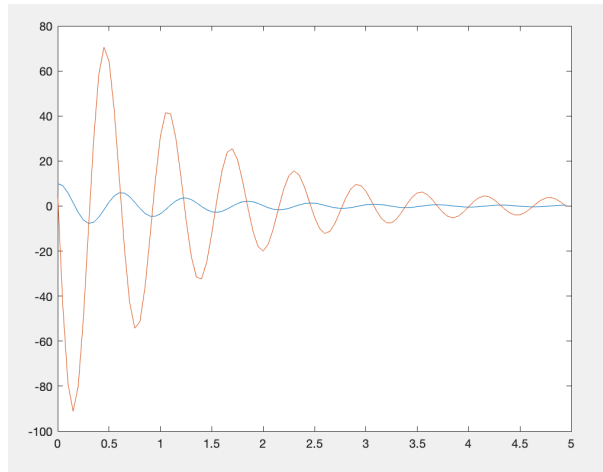
$$s_2 = s_1 a_{12}^{cl} + s_2 a_{22}^{cl}$$

$$s_3 = (s_1 T + s_2) a_{12}^{cl} + (s_2 T + s_3) a_{22}^{cl} + q_v$$

c) The unforced system (assuming  $w_n = 3$ ,  $T=0.001$ ) shown below is marginally stable.



d) The response plots for the optimal controller is shown by



The MATLAB code is given below

```

1 - clear
2 - clc
3 - close all
4
5 - wn=10;
6 - t0=0;
7 - tf=5;
8 - N=100;
9
10 - T0=(tf-t0)/N;
11 - A_d=[cos(wn*T0), sin(wn*T0)/wn; -wn*sin(wn*T0), cos(wn*T0)];
12 - B_d=[1/(wn^2)*(1-cos(wn*T0)); sin(wn*T0)/wn];
13 - s1=1;
14 - s2=0;
15 - s3=1;
16 - Q=eye(2);
17 - r=1;
18 - x0=[10;5];
19
20
21 - delta_array=zeros(1,N);
22 - Sk_array=cell(1,N);
23 - xk_array=cell(1,N);
24 - uk_array=zeros(1,N);
25 - xk_array{1}=x0;
26 - Kk_array=cell(1,N);
27 - Sk_array(N)=[s1 s2; s2 s3];
28 - xk1_array=zeros(1,N);
29 - xk2_array=zeros(1,N);
30
31 - for k=1:(N-1)
32 -     delta_array(1,N-k)=r+((s1/4)*T0^4)+(s2*T0^3)+s3*T0^2;
33 -     k1=((s1*T0^2)/2+s2*T0)/delta_array(1,N-k);
34 -     k2=((s1*T0^3)/2+(3*s2*T0^2)/2+s3*T0)/delta_array(1,N-k);
35 -     Kk_array(N-k)=[k1 k2];
36 -     a_cl11=1-(k1*T0^2)/2;
37 -     a_cl12=T0-(k2*T0^2)/2;
38 -     a_cl21=-k1*T0;
39 -     a_cl22=1-k2*T0;
40 -     s1=s1*a_cl11+s2*a_cl21+Q(1,1);
41 -     s2=s1*a_cl12+s2*a_cl22;
42 -     s3=(s1*T0+s2)*a_cl12+(s2*T0+s3)*a_cl22+Q(2,2);
43 -     Sk_array(N-k)=[s1 s2; s2 s3];
44 - end
45 - for k=1:(N-1)
46 -     uk_array(1,k)=-Kk_array{k}*xk_array{k};
47 -     xk_array{k+1}=A_d*xk_array{k}+B_d*uk_array(1,k);
48 - end
49 - for k=1:N
50 -     xk_array{k}(1)
51 -     xk1_array(1,k)=xk_array{k}(1);
52 -     xk2_array(1,k)=xk_array{k}(2);
53 - end
54 - xk_array{N}
55 - uk_array(1,N-1)
56
57 - T=0:T0:4.955;
58 - U=uk_array;
59
60 - plot(T,xk1_array)
61 - hold on
62 - plot(T,xk2_array)
63

```

## 2.3-2 Digital control of an unstable system

Repeat the previous problem for

$$\dot{x}_1 = x_2 \quad (3.1)$$

$$\dot{x}_2 = a^2 x_1 + bu \quad (3.2)$$

*Solution*

a) To discretize the plant, we use the following equations.

$$A^s = e^{AT} \quad (3.3)$$

$$B^s = \int_0^T e^{A\tau} B d\tau \quad (3.4)$$

where A, B are found by putting the plant into the state space form  $\dot{x} = Ax + Bu$ . Equations (2.1) and (2.2) can be rewritten as

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ a^2 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ b \end{bmatrix} u$$

which tells us that  $A = \begin{bmatrix} 0 & 1 \\ a^2 & 0 \end{bmatrix}$ ,  $B = \begin{bmatrix} 0 \\ b \end{bmatrix}$ . We can solve for the eigenvalues of A,  $\lambda_{1,2} = \pm a$ .

To solve equation (3.3), we will invoke the Cayley-Hamilton Theorem. The Cayley-Hamilton Theorem states that the matrix exponential  $e^{AT}$  can be solved by

$$e^{AT} = \sum_{k=0}^{n-1} \alpha_k A^k \quad (3.5)$$

$$e^{\lambda_i T} = \sum_{k=0}^{n-1} \alpha_k \lambda_i^k \quad (3.6)$$

where the  $\alpha_i$ 's are determined from the set of equations given by the eigenvalues of A. Using (3.5), we can write

$$e^{AT} = \alpha_0 I + \alpha_1 A$$

To solve for  $\alpha_0, \alpha_1$ , we use equation (3.6)

$$e^{-aT} = \alpha_0 - a\alpha_1 \quad (3.7)$$

$$e^{aT} = \alpha_0 + a\alpha_1 \quad (3.8)$$

(3.7)+(3.8) gives us

$$\begin{aligned} (e^{-aT} + e^{aT}) &= 2\alpha_0 \\ \alpha_0 &= \frac{1}{2}(e^{-aT} + e^{aT}) \\ \alpha_0 &= \cosh(aT) \end{aligned} \quad (3.9)$$

Plugging in (3.9) to (3.7)

$$\begin{aligned} e^{-aT} &= \frac{1}{2}(e^{-aT} + e^{aT}) - a\alpha_1 \\ a\alpha_1 &= \frac{1}{2}(e^{aT} - e^{-aT}) \\ \alpha_1 &= \frac{1}{a} \sinh(aT) \end{aligned} \quad (3.10)$$



Now that we have  $\alpha_0, \alpha_1$ , we can find  $e^{AT}$  from (2.5)

$$e^{AT} = (\cosh(aT))I + \frac{1}{a}\sinh(aT)A$$

$$e^{AT} = \begin{bmatrix} \cosh(aT) & \frac{1}{a}\sinh(aT) \\ a\sinh(aT) & \cosh(aT) \end{bmatrix}$$

Now that we have  $A^s$ , we can use equation (2.4) to solve for  $B^s$

$$B^s = \int_0^T e^{A\tau} B d\tau$$

$$B^s = \int_0^T \begin{bmatrix} \cosh(a\tau) & \frac{1}{a}\sinh(a\tau) \\ a\sinh(a\tau) & \cosh(a\tau) \end{bmatrix} \begin{bmatrix} 0 \\ b \end{bmatrix} d\tau$$

$$B^s = \int_0^T \begin{bmatrix} \frac{b}{a}\sinh(a\tau) \\ b\cosh(a\tau) \end{bmatrix} d\tau$$

$$B^s = \begin{bmatrix} \frac{b}{a^2}\cosh(a\tau)|_0^T \\ \frac{b}{a}\sinh(a\tau)|_0^T \end{bmatrix}$$

$$B^s = \begin{bmatrix} \frac{b}{a^2}(\cosh(aT) - 1) \\ \frac{b}{a}\sinh(aT) \end{bmatrix}$$

$$x_{k+1} = \begin{bmatrix} \cosh(aT) & \frac{1}{a}\sinh(aT) \\ a\sinh(aT) & \cosh(aT) \end{bmatrix} x_k + \begin{bmatrix} \frac{b}{a^2}(\cosh(aT) - 1) \\ \frac{b}{a}\sinh(aT) \end{bmatrix} u_k$$

b) Since we know that  $S_k$  is symmetric for all k, let

$$S_k = \begin{bmatrix} s_1 & s_2 \\ s_2 & s_3 \end{bmatrix}$$

Then the feedback gain is updated by

$$\delta = B^T S_{k+1} B + r$$

$$\delta = r + \frac{s_1 T^4}{4} + s_2 T^3 + s_3 T^2$$

$$K_k = B^T S_{k+1} A \frac{1}{\delta}$$

We can write

$$k_1 = \left(\frac{s_1 T^2}{2} + s_2 T\right) \frac{1}{\delta}$$

$$k_2 = \left(\frac{s_1 T^3}{2} + \frac{3s_2 T^2}{2} + s_3 T\right) \frac{1}{\delta}$$

We can write the closed-loop plant matrix

$$A_k^{cl} = A - B K_k$$

$$A_k^{cl} = \begin{bmatrix} a_{11}^{cl} & a_{12}^{cl} \\ a_{21}^{cl} & a_{22}^{cl} \end{bmatrix} = \begin{bmatrix} 1 - \frac{k_1 T^a}{2} & T - \frac{k_2 T^2}{2} \\ -k_1 T & 1 - k_2 T \end{bmatrix}$$

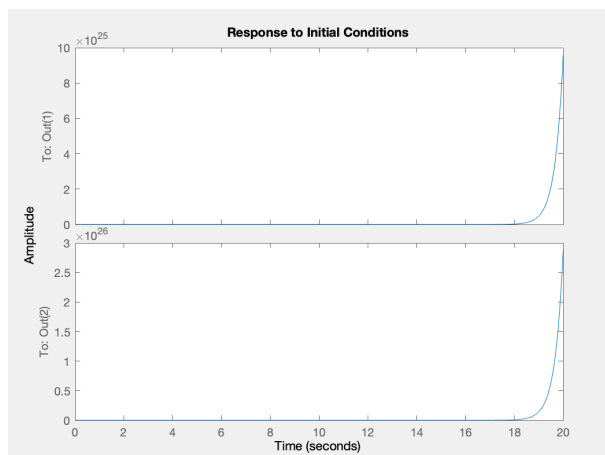
The updated cost kernel is

$$S_k = A^T S_{k+1} A_k^{cl} + Q$$

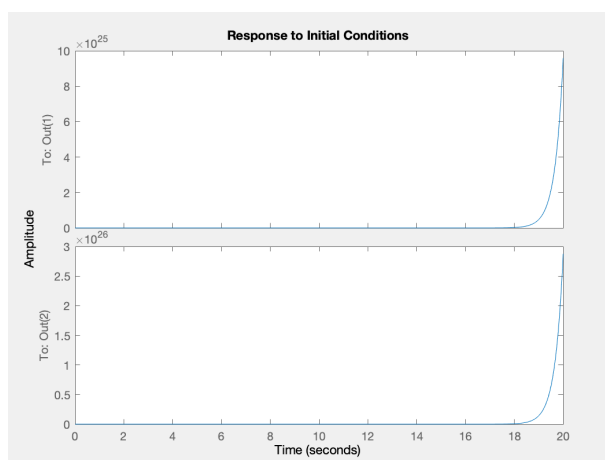
which yields the scalar updates:

$$\begin{aligned} s_1 &= s_1 a_{11}^{cl} + s_2 a_{22}^{cl} + q_d \\ s_2 &= s_1 a_{12}^{cl} + s_2 a_{22}^{cl} \\ s_3 &= (s_1 T + s_2) a_{12}^{cl} + (s_2 T + s_3) a_{22}^{cl} + q_v \end{aligned}$$

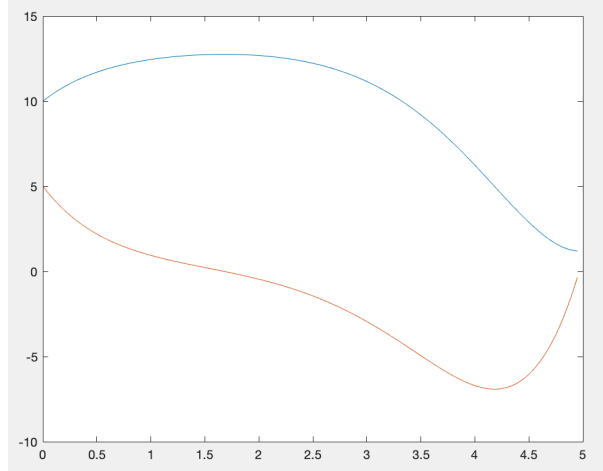
The unforced system (assuming  $a=3$ ,  $b=2$ ,  $T=0.001$ ) shown below is clearly unstable.



c) The unforced system (assuming  $w_n = 3$ ,  $T=0.001$ ) shown below is marginally stable.



d) The response plots for the optimal controller is shown by



The MATLAB code is given below

```

1 - clear
2 - clc
3 - close all
4
5 - a=1;
6 - b=1;
7 - t0=0;
8 - tf=5;
9 - N=100;
10
11 - T0=(tf-t0)/N;
12 - A_d=[cosh(a*T0), (1/a)*sinh(a*T0); a*sinh(a*T0), cosh(a*T0)];
13 - B_d=[b/(a^2)*(cosh(a*T0)-1); (b/a)*sinh(a*T0)];
14 - s1=100;
15 - s2=0;
16 - s3=100;
17 - Q=eye(2);
18 - r=1;
19 - x0=[10;5];
20
21
22 - delta_array=zeros(1,N);
23 - Sk_array=cell(1,N);
24 - xk_array=cell(1,N);
25 - uk_array=zeros(1,N);
26 - xk_array{1}=x0;
27 - Kk_array=cell(1,N);
28 - Sk_array(N)=[s1 s2 s3];
29 - xk1_array=zeros(1,N);
30 - xk2_array=zeros(1,N);
31
32 - Acl=eye(2);
33 - for k=1:(N-1)
34 -     delta_array(1,N-k)=r+((s1/4)*T0^4)+(s2*T0^3)+s3*T0^2;
35 -     k1=((s1*T0^2)/2+s2*T0)/delta_array(1,N-k);
36 -     k2=((s1*T0^3)/2+(3*s2*T0^2)/2+s3*T0)/delta_array(1,N-k);
37 -     Kk_array{N-k}=[k1 k2];
38 -     a_cl11=1-(k1*T0^2)/2;
39 -     a_cl12=T0-(k2*T0^2)/2;
40 -     a_cl21=-k1*T0;
41 -     a_cl22=1-k2*T0;
42 -     s1=s1*a_cl11+s2*a_cl21+Q(1,1);
43 -     s2=s1*a_cl12+s2*a_cl22;
44 -     s3=(s1*T0+s2)*a_cl12+(s2*T0+s3)*a_cl22+Q(2,2);
45 -     Sk_array{N-k}=[s1 s2 s3];
46 - end
47 - for k=1:(N-1)
48 -     uk_array(1,k)=-Kk_array{k}*xk_array{k};
49 -     xk_array{k+1}=A_d*xk_array{k}+B_d*uk_array(1,k);
50 - end
51 - for k=1:N
52 -     xk_array{k}(1)
53 -     xk1_array(1,k)=xk_array{k}(1);
54 -     xk2_array(1,k)=xk_array{k}(2);
55 - end
56 - xk_array{N}
57 - uk_array(1,N-1)
58
59 - T=t0:T0:tf;
60 - U=uk_array;
61
62 - plot(T,xk2_array)

```

## 2.4-1 Steady-state behavior

In this problem we consider a rather unrealistic discrete system because it is simple enough to allow an analytic treatment. Thus, let the plant

$$x_{k+1} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x_k + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u_k$$

have the performance index of

$$J_0 = \frac{1}{2} s_N^T x_N + \frac{1}{2} \sum_{k=0}^{N-1} (x_k^T \begin{bmatrix} q_1 & q_2 \\ q_2 & q_1 \end{bmatrix} x_k + r u_k^2)$$

- Find the optimal steady-state (i.e.,  $N \rightarrow \infty$ ) Riccati solution  $S_\infty^*$  and show that it is positive definite. Find the optimal steady-state gain  $K_\infty^*$  and determine when it is nonzero.
- Find the optimal steady-state closed-loop plant and demonstrate its stability.
- Now the suboptimal constant feedback

$$u_k = -K_\infty^* x_k$$

is applied to the plant. Find scalar updates for the components of the sub-optimal cost kernel  $S_k$ . Find the suboptimal steady-state cost kernel  $S_\infty$  and demonstrate that  $S_\infty = S_\infty^*$ .

*Solution*

To solve this problem we can analytically solve equation (2.4-12) from the book

$$S = A^T [S - SB(B^T SB + R)^{-1} B^T S] A + Q$$

Plugging in A,B,R=r,Q, assuming  $S = \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix}$

$$\begin{aligned} S &= A^T [S - SB \left( \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} + r \right)^{-1} B^T S] A + Q \\ S &= A^T \left[ S - \frac{1}{s_4 + r} \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix} \right] A + Q \\ S &= \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \left[ \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix} - \frac{1}{s_4 + r} \begin{bmatrix} s_2 s_3 & s_2 s_4 \\ s_3 s_4 & s_4^2 \end{bmatrix} \right] \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} q_1 & q_2 \\ q_2 & q_1 \end{bmatrix} \\ \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix} &= \begin{bmatrix} 0 & 0 \\ 0 & s_1 - \frac{s_2 s_3}{r + s_4} \end{bmatrix} + \begin{bmatrix} q_1 & q_2 \\ q_2 & q_1 \end{bmatrix} \\ \begin{bmatrix} s_1 & s_2 \\ s_3 & s_4 \end{bmatrix} &= \begin{bmatrix} q_1 & q_2 \\ q_2 & q_1 + s_1 - \frac{s_2 s_3}{r + s_4} \end{bmatrix} \end{aligned}$$

This allows us to solve for  $s_i$  in terms of  $q_1, q_2$ , and  $r$

$$\begin{aligned} s_1 &= q_1 \\ s_2 &= q_2 \\ s_3 &= q_2 \\ s_4 &= q_1 + s_1 - \frac{s_2 s_3}{r + s_4} \\ s_4^2 + r s_4 &= 2q_1 r + 2q_1 s_4 - s_2 s_3 \\ s_4^2 + r s_4 &= 2q_1 r + 2q_1 s_4 - s_2 s_3 \\ s_4^2 + (r - 2q_1) s_4 + (s_2 s_3 - 2q_1 r) &= 0 \\ s_4 &= \frac{(2q_1 - r) \pm \sqrt{(r - 2q_1)^2 - 4(s_2 s_3 - 2q_1 r)}}{2} \end{aligned}$$

Now that we have  $s_1, s_2, s_3, s_4$ , we have

$$S_{\infty} = \begin{bmatrix} q_1 & q_2 \\ q_2 & s_4 \end{bmatrix}$$

We can see that  $S_{\infty}$  is symmetric and is positive definite if  $q_1 > 0$ ,  $q_1 s_4 - q_2^2 > 0$ . These are both true so we have shown it is symmetric and positive definite.

To find  $K_{\infty}$  we use the following equation (2.4-13) from the book

$$K_{\infty} = (B^T S_{\infty} B + R)^{-1} B^T S_{\infty} A$$

$$K_{\infty} = \frac{1}{r + s_4} \begin{bmatrix} 0 & 1 \end{bmatrix} S_{\infty} \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}$$

$$K_{\infty} = \frac{1}{r + s_4} \begin{bmatrix} 0 & q_2 \end{bmatrix}$$

b) We now look at evaluating the closed loop system

$$A_{cl} = A - B K_{\infty}$$

$$A_{cl} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 0 & q_2 \end{bmatrix}$$

$$A_{cl} = \begin{bmatrix} 0 & 1 \\ 0 & -\frac{q_2}{r+s_4} \end{bmatrix}$$

This gives us eigenvalues of

$$\lambda_{1,2} = 0, -\frac{q_2}{r + s_4}$$

Because  $q_2, r, s_4$  are all positive, we see that both eigenvalues are stable and the closed-loop plant is stable.

## 2.4-2 Analytic Riccati solution

Let  $A = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$ ,  $B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$ ,  $S_N = I$ ,  $Q = I$

- Let  $r=0.1$ . Find the Hamiltonian matrix  $H$  and its eigenvalues and eigenvectors. Find the analytic expression for Riccati solution  $S_k$ . Find the steady-state solution  $S_\infty$  using (2.4-42). Find the optimal steady-state gain  $K_\infty$  using (2.4-63) and also using Ackermann's formula.
- Let  $r=1$ . Find the Hamiltonian matrix and its eigenstructure. Find the steady-state solution  $S_\infty$  and gain  $K_\infty$ . (Hint: See the discussion following (2.4-63).)

*Solution*

The Hamiltonian matrix  $H$  is given by the following equation

$$H = \begin{bmatrix} A^{-1} & A^{-1}BR^{-1}B^T \\ QA^{-1} & A^T + QA^{-1}BR^{-1}B^T \end{bmatrix}$$

$$H = \begin{bmatrix} 1 & -1 & 0 & -10 \\ 0 & 1 & 0 & 10 \\ 1 & -1 & 1 & -10 \\ 0 & 1 & 1 & 11 \end{bmatrix}$$

We can use MATLAB to determine the eigenvalues and eigenvectors of the matrix  $H$  as

$$\lambda_{1,2,3,4} = 10.7802, 2.7654, 0.3616, 0.0928$$

$$v_{1,2,3,4} = \begin{bmatrix} -0.1013 \\ -0.9907 \\ 0.0104 \\ 0.0899 \end{bmatrix}, \begin{bmatrix} -0.4740 \\ -0.8369 \\ 0.2685 \\ 0.0534 \end{bmatrix}, \begin{bmatrix} -0.5081 \\ 0.3243 \\ -0.7959 \\ 0.0573 \end{bmatrix}, \begin{bmatrix} -0.5113 \\ 0.4639 \\ -0.5636 \\ 0.4537 \end{bmatrix}$$

The analytic expression for the Riccati solution  $S_k$  is given by

$$S_k = A^T[S_{k+1} - S_{k+1}B(B^TS_{k+1}B + R)^{-1}B^TS_{k+1}]A + Q$$

To find the steady-state solution ( $S_\infty$ ), we are instructed to use equation (2.4-42)

$$S_\infty = W_{21}W_{11}^{-1}$$

Therefore to find  $S_\infty$  we must define and solve  $W$ .

First, let us define  $M$  to be a diagonal matrix containing  $n$  eigenvalues outside the unit circle. Then we can define  $D$  as

$$D = \begin{bmatrix} M & 0 \\ 0 & M^{-1} \end{bmatrix}$$

$$D = \begin{bmatrix} 10.7802 & 0 & 0 & 0 \\ 0 & 2.7654 & 0 & 0 \\ 0 & 0 & 0.0928 & 0 \\ 0 & 0 & 0 & 0.3616 \end{bmatrix}$$

$W$  is defined as a nonsingular matrix whose columns are the eigenvectors of  $H$  such that

$$W^{-1}HW = D$$

Matching our eigenvectors that we found earlier to their eigenvalues in the D matrix, we can find W to be

$$W = \begin{bmatrix} -0.5113 & -0.5081 & -0.1013 & 0.4740 \\ 0.4639 & 0.3243 & -0.9907 & 0.8369 \\ -0.5636 & -0.7959 & 0.0104 & -0.2685 \\ 0.4537 & 0.0573 & 0.0899 & -0.0534 \end{bmatrix}$$

Now all that's left to solve for  $S_\infty$  is to partition W to solve for  $W_{11}$ ,  $W_{12}$ ,  $W_{21}$ ,  $W_{22}$ .

$$\begin{aligned} W &= \begin{bmatrix} W_{11} & W_{12} \\ W_{21} & W_{22} \end{bmatrix} \\ W_{11} &= \begin{bmatrix} -0.5113 & -0.5081 \\ 0.4639 & 0.3243 \end{bmatrix} \\ W_{12} &= \begin{bmatrix} -0.1013 & 0.4740 \\ -0.9907 & 0.8369 \end{bmatrix} \\ W_{21} &= \begin{bmatrix} -0.5636 & -0.7959 \\ 0.4537 & 0.0573 \end{bmatrix} \\ W_{22} &= \begin{bmatrix} 0.0104 & -0.0534 \\ 0.0899 & -0.0534 \end{bmatrix} \end{aligned}$$

We now have everything we need to solve  $S_\infty$  so we plug  $W_{11}$  and  $W_{21}$  into equation ()

$$\begin{aligned} S_\infty &= W_{21}W_{11}^{-1} \\ S_\infty &= \begin{bmatrix} -0.5636 & -0.7959 \\ 0.4537 & 0.0573 \end{bmatrix} \begin{bmatrix} -0.5113 & -0.5081 \\ 0.4639 & 0.3243 \end{bmatrix}^{-1} \\ S_\infty &= \begin{bmatrix} 2.6687 & 1.7266 \\ 1.7266 & 2.8812 \end{bmatrix} \end{aligned}$$

To find  $K_\infty$ , we plug into our equation

$$K_\infty = (B^T S_\infty B + R)^{-1} B^T S_\infty A$$

$$K_\infty = \begin{bmatrix} 0.5792 & 1.5456 \end{bmatrix}$$

Ackermann's formula can be used to solve the Algebraic Ricatti Equation (ARE). The optimal closed-loop poles are the stable eigenvalues of  $H^{-1}$ . Using MATLAB, we can calculate these to be

$$\lambda_{1,2,3,4} = 10.7802, 2.7654, 0.3616, 0.0928$$

Therefore the desired closed loop characteristic polynomial is

$$\Delta^{cl}(z) = z^2 - 0.4544z + 0.0335$$

The reachability matrix is

$$\begin{aligned} U_2 &= \begin{bmatrix} B & AB \end{bmatrix} \\ U_2 &= \begin{bmatrix} 0 & 1 \\ 1 & 1 \end{bmatrix} \end{aligned}$$

Finally, we define  $e_n$  as the last column of the nxn identity matrix. For our n=2 case

$$e_2 = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

According to Ackermann's formula

$$K_{\infty} = e_n^T U_n^{-1} \Delta^d(A)$$

$$K_{\infty} = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 1 & 1 \end{bmatrix}^{-1} (A^2 - 0.4544A + 0.0335)$$

$$K_{\infty} = \begin{bmatrix} 0.5792 & 1.5456 \end{bmatrix}$$

As we can see, these two methods produce the same result as we would expect.

b) The Hamiltonian matrix H is given by the following equation

$$H = \begin{bmatrix} A^{-1} & A^{-1}BR^{-1}B^T \\ QA^{-1} & A^T + QA^{-1}BR^{-1}B^T \end{bmatrix}$$

$$H = \begin{bmatrix} 1 & -1 & 0 & -1 \\ 0 & 1 & 0 & 1 \\ 1 & -1 & 1 & -1 \\ 0 & 1 & 1 & 2 \end{bmatrix}$$

To find the eigenstructure, we first find the eigenvalues and eigenvectors of  $H^{-1}$

$$\lambda_{1,2,3,4} = 2.1220 + 1.0538i, 2.1220 - 1.0538i, 0.3780 + 0.1877i, 0.3780 - 0.1877i$$

$$v_{1,2,3,4} = \begin{bmatrix} -0.3330 + 0.3128i \\ -0.7032 + 0.0000i \\ 0.0186 - 0.2962i \\ 0.4374 + 0.1320i \end{bmatrix}, \begin{bmatrix} -0.3330 - 0.3128i \\ -0.7032 + 0.0000i \\ 0.0186 + 0.2962i \\ 0.4374 - 0.1320i \end{bmatrix}, \begin{bmatrix} 0.4374 - 0.1320i \\ -0.2472 + 0.1642i \\ 0.7032 + 0.0000i \\ -0.1044 + 0.4448i \end{bmatrix}, \begin{bmatrix} 0.4374 + 0.1320i \\ -0.2472 - 0.1642i \\ 0.7032 + 0.0000i \\ -0.1044 - 0.4448i \end{bmatrix}$$

Now we create the diagonal matrix M, using the stable eigenvalues of  $H^{-1}$

$$M = \begin{bmatrix} 0.3616 & 0 \\ 0 & 0.0928 \end{bmatrix}$$

and the associate eigenvectors

$$\begin{bmatrix} X \\ \Lambda \end{bmatrix} = \begin{bmatrix} 0.4374 - 0.1320i & 0.4374 + 0.1320i \\ -0.2472 + 0.1642i & -0.2472 - 0.1642i \\ 0.7032 + 0.0000i & 0.7032 + 0.0000i \\ -0.1044 + 0.4448i & -0.1044 - 0.4448i \end{bmatrix}$$

$$X = \begin{bmatrix} 0.4374 - 0.1320i & 0.4374 + 0.1320i \\ -0.2472 + 0.1642i & -0.2472 - 0.1642i \end{bmatrix}$$

$$\Lambda = \begin{bmatrix} 0.7032 + 0.0000i & 0.7032 + 0.0000i \\ -0.1044 + 0.4448i & -0.1044 - 0.4448i \end{bmatrix}$$

Now that we have  $\Lambda$  and X, we can plug in to find  $S_{\infty}$ .

$$S_{\infty} = \Lambda X^{-1}$$

$$S_{\infty} = \begin{bmatrix} 2.9471 & 2.3692 \\ 2.3692 & 4.6131 \end{bmatrix}$$

We can also solve for  $K_{\infty}$  using the following equation

$$K_{\infty} = \frac{1}{r} B^T \Lambda M X^{-1}$$

$$K_{\infty} = \begin{bmatrix} 0.4221 & 1.2439 \end{bmatrix}$$