Dequer come x2y+xy2=2ex-y Can of temperat line at (11) differentiate the curve on both sides. $\frac{d}{dx}(x^2y) + \frac{d}{dx}(xy^2) = \frac{d}{dx}(2e^{x-y}) = 0$ x2 dy + y(2x) + x2y dy + y2 = 26x-y (1-dy) x dy + 2xy + 2xy dy +y2= 2ex-9- 2et-9 dy $x^{2} \frac{dy}{dx} + 2xy \frac{dy}{dx} + 2e^{x-y} \frac{dy}{dx} = 2e^{x-y} - 2xy - y^{2}$ dy [22+2xy+2ex-y] = 2ex-y-2xy-y2 $\frac{dy}{dx} = \frac{2e^{2y} - 2xy - y'}{x^2 + 2xy + 2e^{x} - y'}$:. the slope at (1,1) & is con so $m = \frac{dy}{dx} = \frac{2e^{1-1} - 2(1)(1) - 2e^{1-1}}{1^2 + 2(1)(1) + 2e^{1-1}}$ $m = \frac{2 - 2 - 1}{1 + 2 + 2}$ $\left| m = -\frac{1}{5} \right|$ using slope form. $y-y_1 = m(x-x_1)$ $y-1 = -\frac{1}{5}(x-1)$ y=-1(x-1)+1] is the come of the targent line.

let lingth of the rectangular prism be 'L' width of the rectangular prism be 'w' Depth of the rectangular prism be D. i. given that depth is geometric mean of its length and width so, D=JLXW >0 ii. the depth volume of the prism is equal to its Suzjaci area. LWD = 2 (LW+WD+DL) >@ Substitute (1) in (2). LWJLW = 2 [LW+ LJLW + WJLW] LW JIW = 2 JIW [JIW + L+W] LW = 2 TEW + L+W differentiate with respect to 'w' on both sides and apply thain rule. (uv) = uv+ val L'W+LC(1) = 2 2 2 [L'W+L] + L'+1] L'W+L=1 [L'W]+ L +2L+2° L' [w-w-2] = 1 - 12w +2-L LI [w/Lw =w-25w]=oL=LJLw+2JLW : dL = L-LJLW +2 JLW
dw - wJzw + w-zJzw ... de is the rate of change of length short of prism with respect to width. Heyore, dl _ L-LD+2D WD+W-(2D) WD - 12 en + 3- Jule du - 67 - 3- Jace agu = 1/30 = - 22 = 672 2x-9-xx-9-xx

3) given H:[0,24] > R Hardons proving and t∈[0,24] measured in hours? t=0 corresponds to midnight H(t) measures temperatures in degrees Fahrenheit at time t. A) given dota set is D = (to, Ho), ..., (tn, Hn) to extinate the average temperature given in the Idata setal a rot bow of blesde absence all to get the average of light & right Riemann sum, we use trapezoidal rule for numerical. approximation in whe essel It It is now $\int_{1}^{\infty} f(x) dx = \sum_{i=0}^{\infty} \frac{(x_{i})^{2} + f(x_{i+1})^{2}}{(x_{i})^{2}} \int_{1}^{\infty} \frac{dx}{(x_{i})^{2}} dx = \int_{1}^{\infty} \frac{dx}{(x_{i})^{2}} \int_{1}^{\infty} \frac{dx}$

Show it was $\Delta x \left(f(x_0) + 2\left(\sum_{i=1}^{n+1} f(x_i)\right) + f(x_n)\right)$

So, from the given data $\Delta t = 15 \text{ min} = \frac{1}{4} \text{ howy}$

 $\int f(\alpha) dx = \frac{1}{24} \sum_{i=0}^{\infty} \left(\frac{1}{4i} + \frac{1}{4i+1}\right) \left(\frac{1}{4i}\right) \frac{1}{24} \frac{1}{4i}$

here, N > no. of measurements Hi, Hiti > Consecutive temperaturs.

So,
$$\Delta t = \frac{24}{N} \Rightarrow N = \frac{24}{\Delta t}$$

$$N = \frac{24}{4} \Rightarrow A = N = 96$$

Now, average temperature =
$$H$$
 $H = L$
 $V = V$
 $V = V$

B) f: R > R on an interval [a, b] = 1 Stalda

This formula should be used for a longe no of Sample values of because of following reasons:

of the arg value integration gives an underestimate of the area. If the lusses the no-of divition, the more area under curve is left out.

who the more no of division, the lesser area under the curve is left out, which is more accurat.

Hence, It is always a better practise to take Sample points approaching in timity as the Space between them neverly reaches zero Ex the function has a continuous set of Samples.

So, at = 24 = 30, at = 30, at = 96

C)
$$H(t) = 32 + 18 \sin \left(\frac{11}{24} + t \right)$$

Fintegrate on both sides

$$= \frac{1}{b-a} \int_{0}^{b} H(t) dt \quad \left(\begin{array}{c} \text{Riemann average} \\ \text{equation} \end{array} \right)$$

$$= \frac{1}{24-0} \int_{0}^{24} 32 + 18 \sin \left(\frac{11}{24} + t \right) dt$$

$$= \frac{1}{24} \int_{0}^{32} 4 - 18 \cos \left(\frac{11}{24} + t \right) \times \frac{24}{11} \int_{0}^{24} dt$$

$$= \left(\frac{32}{24} + \frac{18}{24} \times \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{11}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left(\frac{11}{24} + t \right) \int_{0}^{24} \frac{24}{11} \times \cos \left$$

... The average temperature is 43.46°F

Fiven path
$$b(x) = \lambda e^{\lambda x}$$
, $x \ge 0$

to calculate variance $Var(x) = \int (x-\lambda')^2 \rho(x) dx$

Splitting the limits from $-\infty$ to ∞ to

 $Var(x) = \int (x-\lambda')^2 \rho(x) dx + \int (x-\lambda')^2 \rho(x) dx$
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 $Var(x) = \int (x-\lambda')^2 \rho(x) dx$
 $Var(x) = \int (x^2 + \frac{1}{\lambda^2} - 2x + \frac{1}{\lambda}) \lambda e^{-\lambda x} dx$
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$$= \frac{\lambda}{\lambda^{3}} \int u^{2}e^{u} du + \frac{1}{\lambda^{2}} \int e^{u} du - \frac{2}{\lambda^{2}} \int u e^{u} du$$

$$= \frac{\lambda}{\lambda^{2}} \int u^{2}e^{u} du + \frac{1}{\lambda^{2}} \int e^{u} du - \frac{2}{\lambda^{2}} \int u e^{u} du$$

$$= \frac{1}{\lambda^{2}} \left(\int u^{2}e^{u} du \right) - \int (\frac{1}{\lambda^{2}}u) (-e^{u}) du + \frac{1}{\lambda^{2}} (-e^{u}) du$$

$$= \frac{2}{\lambda^{2}} \left(\int u e^{u} du \right)$$

$$= \frac{2}{\lambda^{2}} \left(\int u e^{u} du \right)$$

$$= \frac{2}{\lambda^{2}} \left(\int u e^{u} du \right)$$

$$= \left(\frac{u^{2}}{\lambda^{2}} e^{-u} + \frac{2}{\lambda^{2}} \int u e^{u} du - \frac{2}{\lambda^{2}} \int u e^{u} du \right)$$

$$= \left(\frac{u^{2}}{\lambda^{2}} e^{-u} - \frac{e^{-u}}{\lambda^{2}} \right)$$

$$= \left(\frac{1}{\lambda^{2}} e^{-u} - \frac{e^{-u}}{\lambda^{2}} \right)$$

$$= \left(\frac{1}{$$