

DESIGN AND PERFORMANCE OF HIGH LASER POWER INTERFEROMETERS FOR  
GRAVITATIONAL-WAVE DETECTION

By

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My dedication.

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## LIST OF SYMBOLS, NOMENCLATURE, AND ABBREVIATIONS

ADC	analog-to-digital converter
ASC	Angular Sensing and Control
DAC	digital-to-analog converter
EOM	electro-optic modulator
FI	Faraday isolator
GW	gravitational wave
IO	Input Optics
LIGO	Laser Interferometer Gravitational-wave Observatory
LSC	length sensing and control
MC	mode cleaner
MMT	mode matching telescope
PSL	pre-stabilized laser
PRC	power recycling cavity
REFL	reflected beam
RF	radio frequency
RM	recycling mirror
TGG	Terbium Gallium Garnate
TM	test mass
VIRGO	Variability of Solar Irradiance and Gravity Oscillations
WFS	wave-front sensor

Abstract of dissertation Presented to the Graduate School  
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A prediction of Einstein's general theory of relativity, gravitational waves are perturbations of the flat space-time Minkowski metric that travel at the speed of light. Indirectly measured by Hulse and Taylor in the 1970s through the energy they carried away from a binary pulsar system, gravitational waves have yet to be directly detected. The Laser Interferometer Gravitational-wave Observatory (LIGO) is part of a global network of gravitational-wave detectors that seeks to directly detect gravitational waves and to study their sources.

LIGO operates on the principle of measuring the gravitational wave's physical signature of a strain, or relative displacement of inertial masses. An extremely small effect whose biggest of expected transient signals on Earth is on the order of  $10^{-23}$  ([verify this!](#)), gravitational-wave strain can only be measured by detectors so sensitive to displacement as to (collide with) brush into the realm of quantum physics. To improve their sensitivities and to demonstrate advanced technologies, the LIGO observatories in Hanford, WA and Livingston, LA underwent an upgrade between fall 2007 and summer 2009 called Enhanced LIGO. This dissertation focuses on the experimental challenges of one of the goals of the upgrade: operating at an increased laser power.

[Write this final paragraph describing work.](#)

# CHAPTER 1

## THE SEARCH FOR GRAVITATIONAL WAVES

**Write 1-2 pages providing a synopsis of the history of GWs and programs to detect them.**

The field of ground-based gravitational-wave (GW) physics is rapidly approaching a state with a high likelihood of detecting GWs for the first time. Such a detection will not only validate part of Einstein's general theory of relativity, but initiate an era of astrophysical observation of the universe through GWs. Gravitational waves are dynamic strains in space-time that travel at the speed of light and are generated by non-axisymmetric acceleration of mass. The frequency of the gravitational wave depends on its source. A first detection is expected to witness an event such as a binary black hole/neutron star merger. This chapter provides the theoretical framework of gravitational wave generation and presents various ways to detect GWs, including the current status of an effort to do so. I explain the purpose of this dissertation in the context of these current effort, and I conclude with an outline of the content found in the chapters that follow.

### 1.1 The Theory of Gravitational Radiation

Gravitational radiation is a perturbation  $|h_{\mu\nu}| \ll 1$  to the flat space-time Minkowski metric  $\eta_{\mu\nu} = \text{diag}(-1, 1, 1, 1)$ . The metric describing space-time in the presence of gravitational radiation is therefore

$$g_{\mu\nu} = \eta_{\mu\nu} + h_{\mu\nu}. \quad (1.1.1)$$

Just as in electrodynamics where one has freedom in choosing the vector potential  $\vec{A}$  for calculating the magnetic field  $\vec{B} = \vec{\nabla} \times \vec{A}$ , one also has freedom in general relativity in choosing the form of  $h_{\mu\nu}$  for ease of calculation. A convenient and popular choice is called the transverse-traceless (TT) gauge in which

$$h_{\mu\nu} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & h_+ & h_\times & 0 \\ 0 & h_\times & -h_+ & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (1.1.2)$$

where the + and  $\times$  represent two linearly independent polarizations. Without loss of generality, we consider the  $h_+$  polarization in the example that follows.

For a gravitational wave traveling along the  $z$  axis, the metric is given by:

$$ds^2 = -c^2 dt^2 + [1 + h_+(t)] dx^2 + [1 - h_+(t)] dy^2. \quad (1.1.3)$$

This says the TT coordinate system is stretched along the  $x$  axis and compressed along the  $y$  axis by a factor of

$$\sqrt{1 \pm h_+(t)} \approx 1 \pm \frac{1}{2} h_+(t). \quad (1.1.4)$$

Therefore, the *proper distance* between two free masses located along either the  $x$  or the  $y$  axes changes by the factor in Eq. 1.1.4; their coordinate separations remain constant. The GW perturbation is a dimensionless strain

$$h = 2 \frac{\Delta L}{L}. \quad (1.1.5)$$

## 1.2 Sources

Any object with an accelerating mass quadrupole moment generates gravitational waves. The typical strain amplitudes, however, are extremely tiny: a binary system of coalescing  $1M_\odot$  neutron stars in the Virgo Cluster (a distance of 15 Mpc) would produce a maximum GW strain on Earth of only  $10^{-21}$ . [Not right–fix this!!](#) The strain is proportional to source mass and velocity, and inversely proportional to distance from the observer:

$$h \approx \frac{GMv^2}{Rc^4} \quad (1.2.1)$$

Consequently, the most promising sources of detectable gravitational waves are nearby, fast-moving, massive astrophysical objects that include

- supernovae
- binary stars (orbiting or coalescing)
- spinning neutron stars
- cosmological/astrophysical background

and can be categorized as producing periodic, burst, or stochastic GWs.

Stably orbiting binary star systems comprised of black holes or neutron stars as well as rapidly spinning non-axisymmetric pulsars are considered periodic sources since they will produce GWs of relatively constant frequency. These reliable sources of GWs require a long integration time to pick out their signal above noise. The Hulse-Taylor binary, for instance, falls into this category. Supernovae are burst sources since the gravitational collapse will produce a short-lived, unmodeled emission of GWs. Binaries in their final tens of milliseconds of inspiral also fall into this category. Finally, the anisotropies in the inflation of the universe together with the hum of all distant astrophysical sources will create a stochastic background of radiation. Coherent cross-correlation between multiple detectors is necessary for measuring the constant amplitude, broad-spectrum GW background.

Directly detecting gravitational radiation from any such source will reveal information that electromagnetic radiation cannot convey. The frequency of the GW tells about the dynamical timescale of the source. Only through GW radiation, for example, can mass and spin properties of a black hole be revealed.

### 1.3 Methods of Detection

- Hulse/Taylor
- Resonant bars
- Pulsar timing
- CMB polarization (B-modes)
- Interferometry

For an approachable overview of the history of the field, including detector design choices and estimated GW strain amplitudes of various sources, refer to Ref. [2].

### 1.4 State of Ground-based Interferometry

A network of first generation kilometer-scale laser interferometer gravitational-wave detectors completed its integrated 2-year data collection run in 2007, called S5. The instruments were: the American Laser Interferometer Gravitational-wave Observatories (LIGO)[3], one in

Livingston, LA with 4 km long arms and two in Hanford, WA with 4 km and 2 km long arms; the 3 km French-Italian detector VIRGO[4] in Cascina, Italy; and the 600 m German-British detector GEO[5] in Ruthe, Germany. Multiple separated detectors increase detection confidence through signal coincidence and improve source localization through triangulation.

The first generation of LIGO, known as Initial LIGO, achieved its design goal of sensitivity to GWs in the 40 Hz - 7000 Hz band which included a record strain sensitivity of  $2 \times 10^{-23} / \sqrt{\text{Hz}}$  at 155 Hz. However, only the loudest of sources produce enough GW strain to appear in LIGO's band, and no gravitational wave has yet been found in the S5 data. A second generation of LIGO detectors, Advanced LIGO, has been designed to be at least an order of magnitude more sensitive at several hundred Hz and above and include an impressive increase in bandwidth down to 10 Hz, dramatically increasing the chances of detection. The baseline Advanced LIGO design [6] improves upon Initial LIGO by featuring better seismic isolation, the addition of a signal recycling mirror at the output port, homodyne readout, and an increase in laser power from 10 W to 165 W.

To test some of Advanced LIGO's new technologies so unforeseen difficulties could be addressed and so that a more sensitive data taking run could take place, increasing the chances of detection, an incremental upgrade to the interferometers was carried out after S5 [7]. This project, Enhanced LIGO, culminated with the S6 science run from July 2009 to October 2010. An output mode cleaner was designed, built and installed, and DC readout of the GW signal was implemented [8]. An Advanced LIGO active seismic isolation table was also built, installed, and tested [9, Ch. 5]. In addition, the 10 W Initial LIGO laser was replaced with a 35 W laser [10]. Accompanying the increase in laser power, the test mass Thermal Compensation System [11], the Alignment Sensing and Control, and the Input Optics were modified.

As of the writing of this dissertation (September 2011), construction and installation of Advanced LIGO is underway. The vacuum systems are being retro-fitted to accompany the new layout, and at LLO the 165 W laser has been installed. At both sites, the new seismic isolation platforms and multi-level suspension cages are being mass-produced. The By 2012, the first of

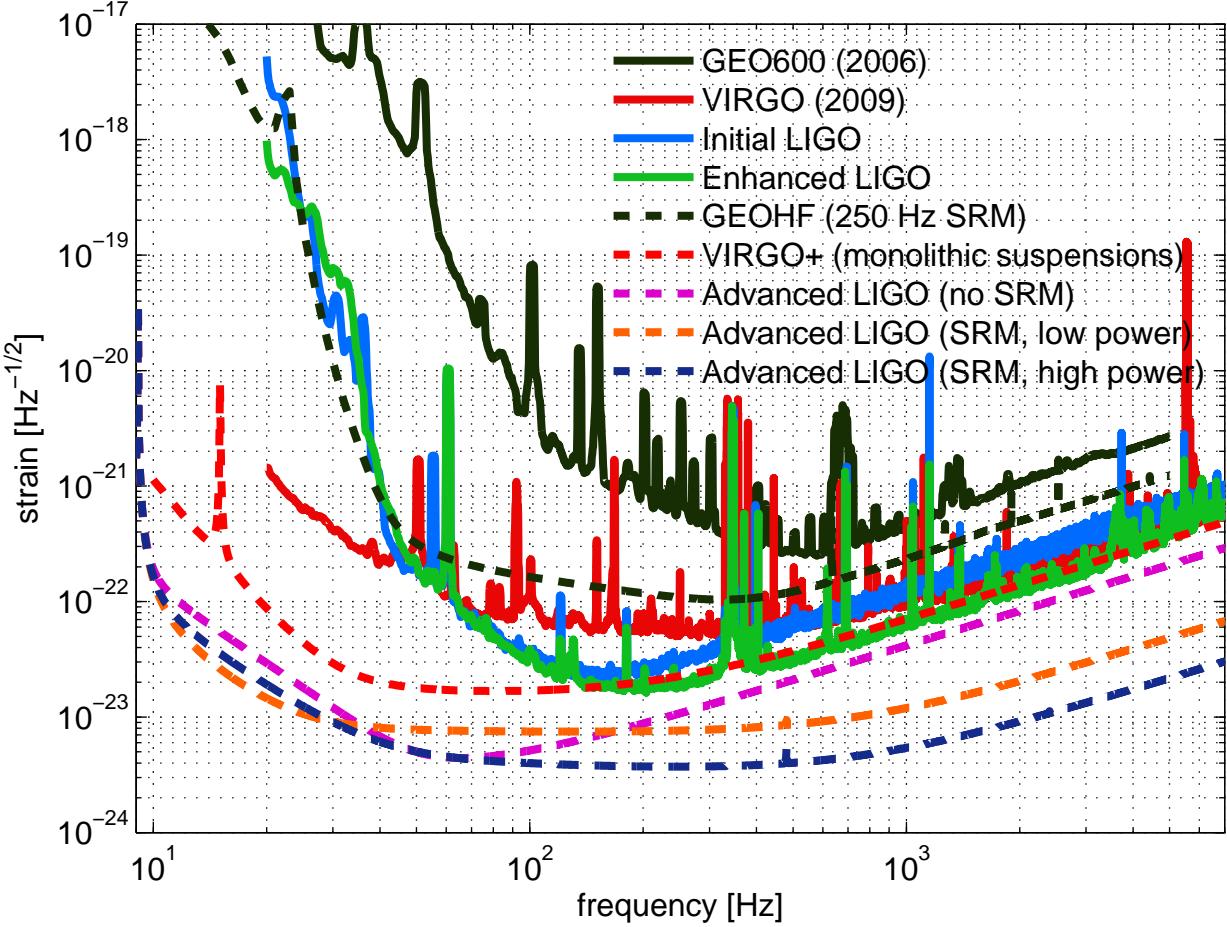


Figure 1-1. Strain sensitivities of LIGO-VIRGO collaboration interferometers.

the suspended mirrors will be installed and testing begun. Simultaneously, VIRGO and GEO are both undergoing their own upgrades as well [4] [12]. Figure 1-1 shows the achieved and theoretical future noise curves of this network of ground-based GW detectors.

### 1.5 Purpose of this Work

The purpose of this work is to demonstrate the capability of an interferometric gravitational wave detector to operate at several times the highest of laser powers previously used. From a naïve standpoint, more power is desirable since strain sensitivity improves by  $\sqrt{P}$  in the high frequency ( $> 200$  Hz) shot-noise-limited region. However, as detectors become more sensitive at low frequencies ( $< 70$  Hz) in the years to come, radiation pressure noise will become the dominant noise source there, making high laser power operation a design trade-off. Currently,

seismic noise limits low frequency sensitivity, so exploring the technical world of increasing the laser power is a fruitful adventure.

More power introduces radiation pressure and thermally induced side effects that must all be addressed for effective interferometer operation. Concerns about the practical difficulties of handling high power effects abounded during Initial LIGO when operating at the design power of 10 W proved more difficult and less straight-forward than expected. To achieve the Advanced LIGO design sensitivity, an ambitious 160 W of input power is needed. Without an understanding of the thermal and radiation pressure problems at 10 W, Advanced LIGO becomes a daunting goal.

The work presented in this dissertation was carried out during Enhanced LIGO to verify and investigate the predicted and unforeseen effects of as much as 25 W of laser power. I present the design and the measurements I made of the performance of two of the interferometer subsystems that are affected by an increase in laser power: the Input Optics and the Angular Sensing and Control. I show that the thermal and radiation pressure effects on these subsystems are well understood and should not pose [unsolvable, pick different word](#) problems for Advanced LIGO.

### **1.5.1 The Input Optics High Power Story**

The performance of the Initial LIGO Input Optics degraded as the result of absorbing too much heat while the input power ramped up to 7 W. Particular issues that needed to be addressed for any further increase in power included thermal steering of the beam rejected by the interferometer, a decrease in the optical isolation, and thermal lensing that drove the spatial mode of the beam directed at the interferometer away from optimal. I describe the design of the improved Input Optics for Enhanced LIGO which includes less absorptive optical components in order to conquer thermal issues at the source and changes to the design architecture that compensate for any residual effects. I also present the set of measurements I made to characterize the Input Optics performance with up to 30 W input power. I show that we can expect the Input Optics to perform well for Advanced LIGO.

### 1.5.2 The Angular Sensing and Control High Power Story

Radiation pressure creates torques, a long-known concept, and the optical torque's ability to de-stabilize optical cavities was first recognized in 1991 by Solimeno et al. [13]. However, the theory of radiation pressure's effect on angular mechanical transfer functions was not fully appreciated and published until 2006 by Sidles and Sigg [14]. The concern arised that radiation pressure might be the factor limiting Initial LIGO's ability to increase the input power. Eiichi Hirose showed that the optical torque was present and measurable, but that it was *not* limiting Initial LIGO's power [15].<sup>1</sup> The concern of the optical torque's role in cavity dynamics shifted to Enhanced and Advanced LIGO, which were designed to operate at four times and 20 times the laser power of Initial LIGO, respectively. Lisa Barsotti developed a numerical model of the angular sensing and controls for Enhanced LIGO, specifically including radiation pressure torque. She showed that, in principle, the radiation pressure torque can be controlled without detrimental consequences to the sensitivity of the detector [16]. We implemented Barsotti's theoretical control scheme and I measured its performance with up to 20 W of input power, demonstrating a thorough understanding of the principles at work and providing confidence in the ability to control radiation pressure torques in Advanced LIGO. I also improved upon Hirose's measurement of the optical angular (anti-)spring. In addition, through post-analysis of angular data, I demonstrate the potential of a technique that may be used in Advanced LIGO for reducing the angular control signals.

### 1.5.3 Outline of this Dissertation

The organization of this dissertation is as follows. Chapter 2 describes the measurement apparatus, the LIGO interferometer, focusing on key aspects which are relevant for the rest of the thesis, including the motivation for more laser power. Chapter 3 presents the design and performance of the Enhanced LIGO Input Optics with up to 30 W input power. Chapter 4

---

<sup>1</sup> In fact, after the Enhanced LIGO laser was installed, and before any changes were made to the ASC, we successfully operated the interferometer with 14 W input power.

introduces the Angular Sensing and Control, describing the causes of angular mirror motion, why angular motion matters, and how it was sensed and controlled in Initial LIGO. Chapter 5 derives the coupled cavity eigenfunctions that result from radiation pressure torque, setting the stage for changes to the ASC to accompany high power. Chapter 6 presents the characterization and performance of the Enhanced LIGO ASC with up to 20 W input power, and Chapter 7 shows the direct measurement of the optical (anti-)spring. A summary and conclusions are in Chapter 8.

## CHAPTER 2

### DESIGN BASICS OF LASER INTERFEROMETERS FOR GRAVITATIONAL-WAVE DETECTION

I introduce in this chapter some of the basic principles in the design of sensitive instruments (and the LIGO detectors in particular) to set the stage for delving into the details of the following chapters.

#### 2.1 Signal Versus Noise

The factors that must be considered in the design of any detector can be grouped into two categories: signal and noise. The ability to make a claim of detection is largely dependent on the magnitude of the signal to noise ratio (SNR). An SNR of 8 is desired for detection confidence in LIGO.

For laser interferometers operating with DC readout, the strength of the GW signal is proportional to the length of the arms and the amount of power in the arms. (See Eq. 7-1.) The change in the distance between the mirrors,  $\Delta L$ , is bigger for a given strain the longer the arms. And with more circulating power, the greater the amount of power that will show up at the AS port for a given displacement from the dark fringe. Therefore, the two fundamental ways to make a GW produce a bigger signal in an interferometer are:

1. make the arms longer
2. increase the circulating power

No matter how large a signal one might have, it won't be found confidently, or at all, if there is too much noise. The noise itself is best grouped into categories of displacement noise and sensing noise which affect the length of the arms and the measurement of the signal, respectively. Interferometers for GW detection are plagued primarily by displacement noise below 70 Hz and sensing noise above 200 Hz.

In the next sections I will describe briefly the specific types of displacement and sensing noises affecting the sensitivity of laser interferometers. A summary of the noise budget is shown in Fig. 2-1.

Figure 2-1. Noise budget place holder.

### 2.1.1 Displacement Noise

ground motion, thermal noise

seismic noise physically displaces the mirrors, resulting in changes in the length of the arm.

### 2.1.2 Sensing Noise

stray light, shot noise

Shot noise is a quantum mechanical effect of the detection of photons which creates uncertainty in the phase of the light, and therefore the power, at the AS port.

## 2.2 Measuring GW Strain with Light

### 2.2.1 Light as a Photon

Consider two wave packets leaving the beam splitter of a Michelson interferometer at the same time, each heading down a different arm. If an appropriately polarized gravitational wave is present, the amount of time the wave packet takes to travel down a stretched arm and back is:

$$t_{rt+} = \frac{2L}{c} \left( 1 + \frac{h_+}{2} \right) \quad (2.2.1)$$

Likewise, for a compressed arm the roundtrip travel time is:

$$t_{rt-} = \frac{2L}{c} \left( 1 - \frac{h_+}{2} \right) \quad (2.2.2)$$

There is a non-zero  $2Lh_+/c$  difference in arrival times at the beam splitter, a quantity one could measure with an accurate stationary clock. This demonstrates intuitively that a laser interferometer can detect gravitational waves.

It should be noted that we had to use the approximation that the gravitational wave wavelength  $\lambda_{gw}$  is much larger than the interferometer arm length  $L$ . This means that the temporal variation of  $h_+(t)$  is negligible during the time it takes the photon to make its roundtrip. Thus,  $h_+$  is treated as a constant in Eqs. 2.2.1 and 2.2.2.

## 2.2.2 Light as a Wave

The detector at the beam splitter is not a clock, but a photodetector which is sensitive to phase. It would be informative, therefore, to express the difference in arrival times as a difference in phase. To do so, we must move away from the photon model and think about the wave model of light. The light wave's phase is given by  $\phi = \omega t$  where  $t$  is the proper time. Then, the difference in phase between the two light beams after each has completed its roundtrip is:

$$\Delta\phi = \phi_{rt+} - \phi_{rt-} = \frac{2L\omega}{c}h_+ \quad (2.2.3)$$

Two time derivatives yields

$$\frac{d^2\Delta\phi}{dt^2} = \frac{2L\omega}{c}\partial_t\partial_t h_+. \quad (2.2.4)$$

It can be shown [17] that the Riemann tensor in the TT gauge is  $R_{tkti} = -\frac{1}{2}\partial_t\partial_t h_{ki}$ , and gauge invariant. Therefore, our physically measurable quantity can be expressed as being manifestly gauge invariant, proving that a laser interferometer can detect the effect of gravitational waves.

## 2.3 Power-recycled Fabry-Perot Michelson Interferometers

The typical detector configuration is a power-recycled Fabry-Perot Michelson laser interferometer featuring suspended test masses in vacuum as depicted in Figure 2-2. A diode-pumped, power amplified, and intensity and frequency stabilized Nd:YAG laser emits light at 1064 nm. The laser is directed to a Michelson interferometer whose two arm lengths are set to maintain destructive interference of the recombined light at the anti-symmetric (AS) port. An appropriately polarized gravitational wave will differentially change the arm lengths, producing signal at the AS port proportional to the GW strain and the input power.

The Fabry-Perot cavities of the Michelson arms increases the phase gain of the DARM signal

A power recycling mirror (RM) at the symmetric port is a modification to the Michelson interferometer that increases the circulating laser power

in the arms and therefore improve the detector's sensitivity to GWs.

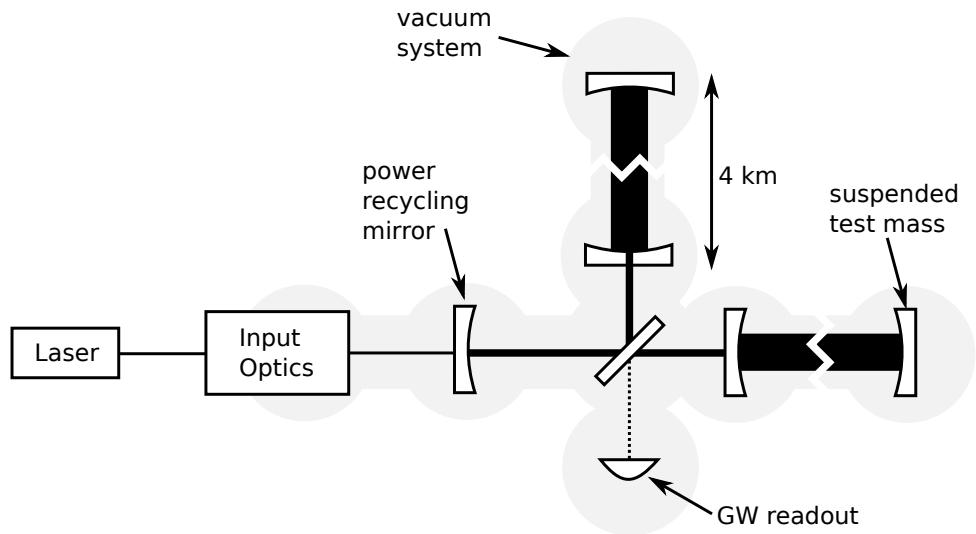


Figure 2-2. Power-recycled Fabry-Perot Michelson laser interferometer.

## 2.4 Controlling the Interferometer

The ability of the interferometer to provide a differential arm length signal depends on the many interferometer cavities being locked ([define locking!](#)) all at once. It is the light, after all, that serves as our probe of arm length. The motion of the mirrors without any control is too large for a locked state to naturally occur. The rms pendular displacement of the mirrors without control is  $1 \mu\text{m}$ , equivalent to a full laser wavelength. The arm length would swing from one free spectral range (FSR) to the next, never staying put long enough at any particular FSR.

The motion of the interferometer mirrors must be controlled enough so that resonance is achieved and error signals fall in a linear regime. Since the strain sensitivity is determined by mathematically undoing the (carefully measured) effect of the control system on DARM, control does not directly improve the strain sensitivity. The purpose length control does serve is to make the strain measurement possible. For other degrees of freedom, such as angular motion, only the controlled residual matters .. Control, however, introduces noise so there is a fine balance that must be found between too much and too little control.

Design considerations for the control loops include how much motion at what frequencies can be tolerated, and the signal to noise ratio of the motion sensor.

### 2.4.1 RF Sidebands

Phase modulation multiplies carrier light with field  $E_0 e^{i\omega t}$  by  $e^{i\Gamma \sin(\Omega t)}$ , where  $\Gamma$  is the modulation index and  $\Omega$  is the frequency of the phase modulation. Using the Jacobi-Anger expression,

$$e^{iz \sin \theta} = \sum_{n=-\infty}^{\infty} J_n(z) e^{in\theta}, \quad (2.4.1)$$

where  $J_n$  are the Bessel functions, we can write the first few terms ( $n = 0, 1, -1$ ) of the phase-modulated field:

$$E_{modulated} = E_0 J_0(\Gamma) e^{i\omega t} + E_0 J_1(\Gamma) e^{i(\omega+\Omega)t} + E_0 J_{-1}(\Gamma) e^{i(\omega-\Omega)t} + \dots \quad (2.4.2)$$

We see that both an upper and lower primary sideband are created, with frequencies  $\omega + \Omega$  and  $\omega - \Omega$ . Phase modulation does produce an infinite number of sidebands, yet the amplitude of the Bessel function decays rapidly with higher  $|n|$ , so only this first set of sidebands are significant.

### 2.4.2 Digital Control in LIGO

Although the interferometer is an analog instrument, it is interfaced through a digital control system. The analog sensor signals are sent through an analog-to-digital converter (ADC), digitally filtered, and then sent through a digital-to-analog converter (DAC) before returning to the interferometer's actuators as control signals. The use of a digital control system means complex filters can be more easily implemented than they would with analog electronics, and the potential

There are a select few control systems that remain completely analog, like the laser intensity stabilization servo (ISS). When the frequencies of interest extend beyond several tens of thousands of Hz, the use of computers becomes impractical.

### 2.4.3 Mirror Suspension and Actuation

The primary interferometer optics are suspended in vacuum so that they act like free masses at the frequencies in the GW detection band. Each mirror is hung from a single [xx m diameter](#) wire that loops around the bottom of the barrel of the mirror as shown in Fig. 4-2. Stand-offs glued just above the mirror's center of mass on both sides of the barrel mark the final point

of contact of the wire with the mirror, and both ends of the wire are clamped to the top of a suspension cage.

Each mirror is equipped with four optical sensor and electro-magnetic (OSEM) actuators for providing control to the mirror. Magnets arranged to form the four corners of a square are glued on the mirror's back surface, and the OSEM units envelop them. Length control of the cavities, for instance, sends current of the same magnitude through each coil on a given mirror to provide a piston force for changing the mirror's position.

Minimal contact with the mirrors is necessary to avoid thermal noise. Therefore, the suspensions provide minimal damping to the mirrors. Damping for the large optics is instead achieved electronically through the use of optical levers. They provide velocity damping only (no DC control) between 0.2 Hz and 2 Hz. The open loop transfer function of the optical lever servo is in the Appendix (Figure 10-1).

The suspensions are AC damped at all times for each of the large optics through optical lever witnesses. Keeping the mirrors quiet enough with respect to their local ground is necessary to allow for the initial locking of the interferometer, so each suspended optic, small and large, is quieted by its OSEM signals during the initial locking stages. After the interferometer is locked, the angular OSEM feedback is turned off, and the position OSEM feedback remains.

pitch and yaw

## 2.5 DC readout / more laser power

Increasing the laser power in the interferometer is a

Shot noise is a Poissonian process: the average number of photons striking a detector,  $\langle x \rangle$ , is equal to the variance of the mean number of photons,  $\langle x^2 \rangle - \langle x \rangle^2$ , from a given chunk of time  $\tau$  to another. For large  $\langle x \rangle$ , the distribution becomes Gaussian, but the mean and variance are still equivalent. Based on this property and Parseval's theorem, the power on a detector due to shot noise is:

$$P_{SN} = \frac{\langle x \rangle}{\tau} h\nu = \sqrt{2P_{DC}h\nu} \quad (2.5.1)$$

where  $P_{DC}$  is the DC power on the photodiode,  $h = 6.626 \times 10^{-34}$  Js is Planck's constant, and  $\nu = 2.82 \times 10^{14}$  Hz is the frequency of the incident light. The units of shot noise are W/ $\sqrt{\text{Hz}}$ .

DC readout, as used in Enhanced LIGO, operates with a small offset,  $x_0 \approx 10\text{pm}$ , from the dark fringe. Strain induced in the interferometer can therefore be directly read out at the dark port as simply a linear function of power. We are interested in the optical gain of this form of readout, the change in power at the AS port per change in differential arm length.

The power at the dark port as a function of differential arm length,  $x$ , is

$$P_{AS} = P_{BS} \sin^2(g_\phi kx) \quad (2.5.2)$$

where  $g_\phi = 137$  is phase gain of the Fabry-Perot arms and  $k = 5.9 \times 10^6 \text{m}^{-1}$  is the wavenumber.

The derivative is the optical gain:

$$\frac{dP_{AS}}{dx} = P_{BS} g_\phi k \sin(g_\phi kx) \cos(g_\phi kx) \quad (2.5.3)$$

The sensitivity of DC readout to gravitational wave strain is dependent not only on the optical gain, but on the noise at detector. The shot-noise-limited sensitivity is the shot noise divided by the optical gain:

$$aoeu \quad (2.5.4)$$

## CHAPTER 3

### INPUT OPTICS DESIGN AND CHARACTERIZATION

#### 3.1 Function of the Input Optics

The Input Optics is one of the primary subsystems of the LIGO interferometers. Its purpose is to deliver an aligned, spatially pure, mode-matched beam with phase-modulation sidebands to the power-recycled Fabry-Perot Michelson interferometer. The IO also prevents the backscattering of light into the laser and distributes the control sidebands reflected from the interferometer (designated the *reflected port*) to photodiodes for sensing and controlling the length and alignment of the interferometer. In addition, the IO provides an intermediate level of frequency stabilization and must have high overall optical efficiency. It must perform these functions without limiting the strain sensitivity of the LIGO interferometer. Finally, it must operate robustly and continuously over years of operation. The conceptual design is found in Ref. [18].

As shown in Fig. 3-1, the Input Optics subsystem consists of four components located between the pre-stabilized laser and the power recycling mirror:

- electro-optic modulator (EOM)
- mode cleaner cavity (MC)
- Faraday isolator (FI)
- mode-matching telescope (MMT)

Each element is a common building block of many optical experiments and not unique to LIGO. However, their roles specific to the successful operation of interferometry for gravitational-wave detection are of interest and demand further attention. Here, we briefly review the purpose of each of the Input Optics components; further details about the design requirements are in Ref. [19].

##### 3.1.1 Electro-optic Modulator

The Length Sensing and Control (LSC) and Angular Sensing and Control (ASC) subsystems require phase modulation of the laser light at RF frequencies. This modulation is produced by an EOM, generating sidebands of the laser light which act as references against which

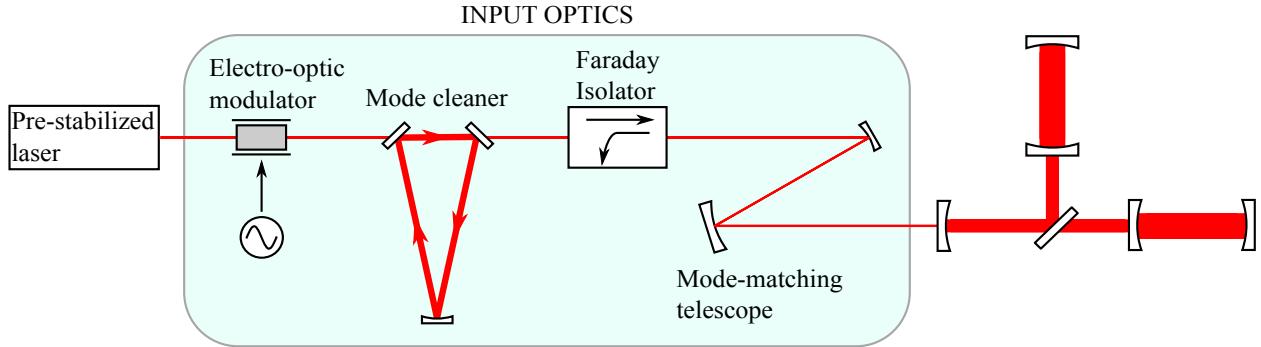


Figure 3-1. Block diagram of the Input Optics subsystem. The IO is located between the pre-stabilized laser and the recycling mirror and consists of four components: electro-optic modulator, mode cleaner, Faraday isolator, and mode-matching telescope. The electro-optic modulator is the only IO component outside of the vacuum system. Diagram is not to scale.

interferometer length and angle changes are measured [20]. The sideband light must be either resonant only in the recycling cavity or not resonant in the interferometer at all. The sidebands must be offset from the carrier by integer multiples of the mode cleaner free spectral range so that neither MC length fluctuations nor phase modulation of the sidebands (due to phase noise of the RF oscillator) are converted to amplitude modulation.

### 3.1.2 Mode Cleaner

Stably aligned cavities, limited junk light, and a frequency and amplitude stabilized laser are key features of any ultra sensitive laser interferometer. The mode cleaner, at the heart of the IO, plays a major role to this effect.

A three-mirror triangular ring cavity, the mode cleaner suppresses laser output not in the fundamental  $\text{TEM}_{00}$  mode, serving two major purposes. It enables the robustness of the ASC since higher order modes would otherwise contaminate the angular sensing signals of the interferometer. Also, all non- $\text{TEM}_{00}$  light on the length sensing photodiodes, including those used for the GW readout, contributes shot noise but not signal and therefore diminishes the signal to noise ratio. The mode cleaner is thus largely responsible for achieving an aligned, minimally shot-noise-limited interferometer.

The mode cleaner also plays an active role in laser frequency stabilization [21]. A frequency-stabilized laser is necessary for ensuring that the signal at the anti-symmetric port is due to arm length fluctuations rather than laser frequency fluctuations. In principle, the two-arm geometry of LIGO facilitates this distinction, but imbalances between the arms allow frequency noise to couple into the gravitational wave channel. At low frequencies ( $< 100$  Hz) the average interferometer arm length drives the mode cleaner length, which in turn adjusts the laser frequency. At high frequencies (up to 20 kHz), the common arm length adds an electronic offset to the MC error point, also resulting in a shift of the laser frequency. As a result, the light transmitted through the MC is matched to the very quiet arms.

The mode cleaner acts as a passive laser amplitude fluctuation filter. Laser power fluctuations that couple to the antisymmetric port cause noise in the GW readout. The mode cleaner suppresses laser amplitude noise above its pole frequency of about 4500 Hz. In addition, the MC passively suppresses beam jitter at frequencies above 10 Hz.

### 3.1.3 Faraday Isolator

Faraday isolators are four-port optical devices which utilize the Faraday effect to allow for non-reciprocal polarization switching of laser beams. Any reflected light from the interferometer due to impedance mismatch, mode mismatch, non-resonant sidebands, or signal needs to be diverted to protect the laser from back propagating light, which can introduce amplitude and phase noise. This diversion of the reflected light is also necessary for extracting length and angular information about the interferometer's cavities. The Faraday isolator accomplishes both needs.

### 3.1.4 Mode-matching Telescope

The lowest order mode cleaner and arm cavity spatial eigenmodes need to be matched for maximal power buildup in the interferometer. The mode-matching telescope is a set of three suspended concave mirrors between the mode cleaner and interferometer that expand the beam from a radius of 1.6 mm at the mode cleaner waist to a radius of 37 mm at the recycling mirror.

The MMT should play a passive role by delivering properly shaped light to the interferometer without introducing beam jitter or any significant aberration that can reduce mode coupling.

### 3.2 Thermal Problems in Initial LIGO

The Initial LIGO interferometers were equipped with a 10 W laser, yet operated with only 7 W input power to the interferometer due to power-related problems with other subsystems. The EOM was located in the 10 W beam and the other components experienced anywhere up to 7 W power. The 7 W operational limit was not due to the failure of the Input Optics; however, many aspects of the IO performance did degrade with power.

One of the primary problems of the Initial LIGO Input Optics [22] was thermal deflection of the back propagating beam due to thermally-induced refractive index gradients in the Faraday isolator. A significant beam drift between the interferometer’s locked and unlocked states led to clipping of the reflected beam on the photodiodes used for length and alignment control. Our measurements determined a deflection of approximately 100  $\mu\text{rad}/\text{W}$  in the FI. This was mitigated at the time by the design and implementation of an active beam steering servo on the beam rejected by the isolator.

There were also known limits to the power the IO could sustain. Thermal lensing in the Faraday isolator optics would start to significantly alter the beam mode at powers greater than 10 W, leading to a several percent reduction in mode matching to the interferometer [1]. Additionally, the absorptive FI elements would create thermal birefringence, degrading the optical efficiency and isolation ratio with power [23]. The Initial LIGO New Focus electro-optic modulators had an operational power limit of around 10 W. There was a high risk of damage to the crystals under the stress of the 0.4 mm radius beam. Also, anisotropic thermal lensing with focal lengths as severe as 3.3 m at 10 W made the EOMs unsuitable for much higher power. Finally, the mode cleaner mirrors exhibited high absorption (as much as 24 ppm per mirror), enough that thermal lensing of the MC optics at Enhanced LIGO powers would induce higher order modal frequency degeneracy and result in a power-dependent mode mismatch into the

interferometer [24, 25]. In fact, as input power increased from 1 W to 7 W the mode matching decreased from 90% to 83%.

In addition to the thermal limitations of the Initial LIGO IO, optical efficiency in delivering light from the laser into the interferometer was not optimal. Of the light entering the Input Optics chain, only 60% remained by the time it reached the power recycling mirror. Moreover, since only 90% at best of the light at the recycling mirror was coupled into the arm cavity mode, room was left for improvement in the implementation of the MMT.

### 3.3 Enhanced LIGO Input Optics Design

The Enhanced LIGO Input Optics design addressed the thermal effects that compromised the performance of Initial LIGO, and accommodated up to four times the power of Initial LIGO. Also, the design was a prototype for handling the 165 W laser planned for Advanced LIGO. Since the adverse thermal properties of the Initial LIGO IO (beam drift, birefringence, and lensing) are all attributable primarily to absorption of laser light by the optical elements, the primary design consideration was finding optics with excellent thermo-optical properties [1]. Both the EOM and the FI were replaced for Enhanced LIGO. Only minor changes were made to the MC and MMT. A detailed layout of the Enhanced LIGO IO is shown in Figure 3-2.

#### 3.3.1 Electro-optic Modulator Design

We replaced the commercially-made New Focus 4003 resonant phase modulator of Initial LIGO with an EOM design and construction of our own. Both a new crystal choice and architectural design change allow for superior performance.

The Enhanced LIGO EOM design uses a crystal of rubidium titanyl phosphate (RTP), which has at most 1/10 the absorption coefficient at 1064 nm of the lithium niobate ( $\text{LiNbO}_3$ ) crystal from Initial LIGO. At 200 W the RTP should produce a thermal lens of 200 m and higher order mode content of less than 1%, compared to the 3.3 m lens the  $\text{LiNbO}_3$  produces at 10 W. The RTP has a minimal risk of damage, since it has both twice the damage threshold of  $\text{LiNbO}_3$  and is subjected to a beam twice the size of that in Initial LIGO. RTP and  $\text{LiNbO}_3$  have similar

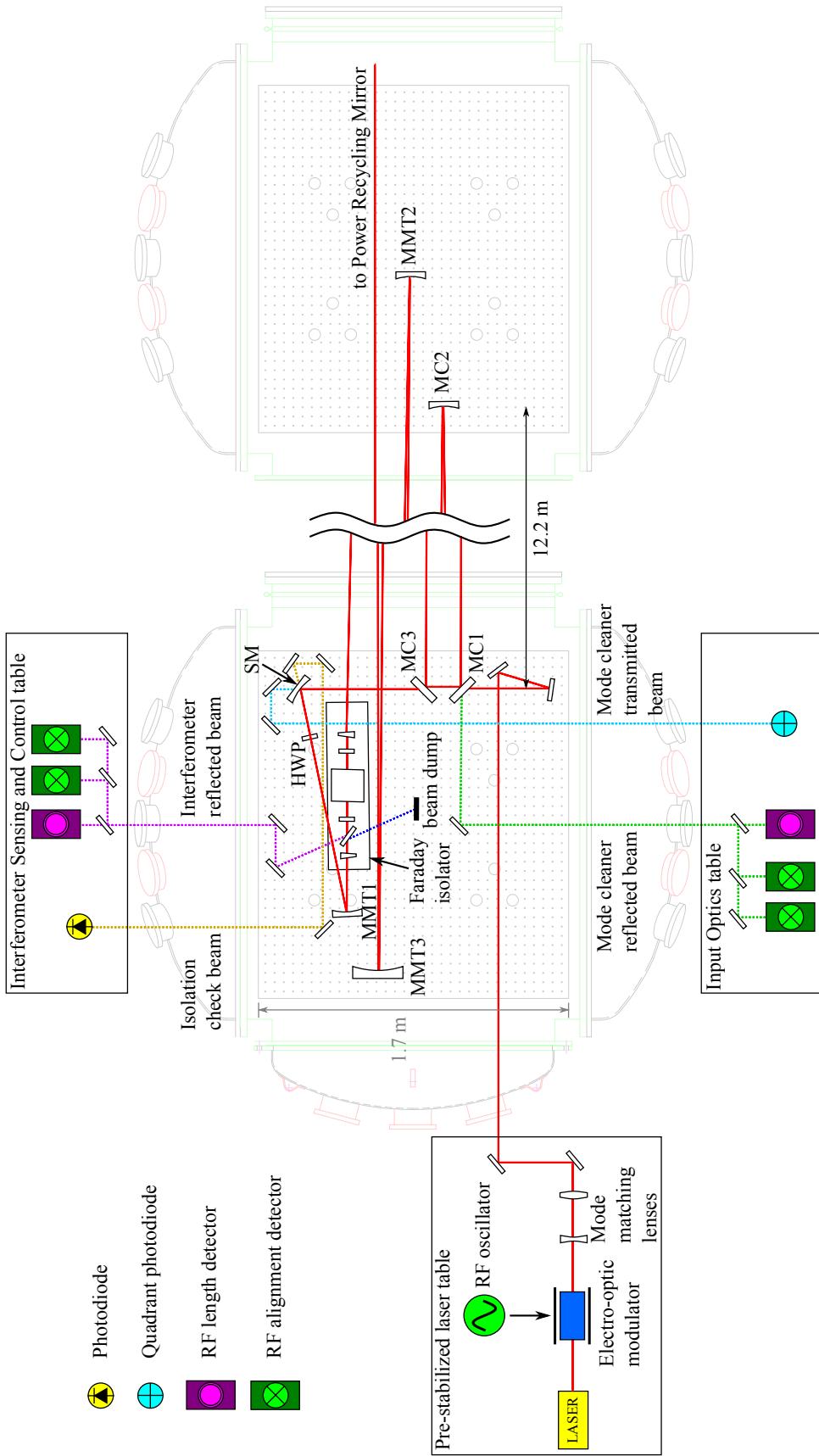


Figure 3-2. Enhanced LIGO Input Optics optical and sensing configuration. The HAM1 (horizontal access module) vacuum chamber is featured in the center, with locations of all major optics superimposed. HAM2 is shown on the right, with its components. These tables are separated by 12 m. The primary beam path, beginning at the pre-stabilized laser and going to the power recycling mirror, is shown in red as a solid line, and auxiliary beams are different colors and dotted. The MMTs, MCs, and steering mirror (SM) are suspended; all other optics are fixed to the seismically isolated table. The laser and sensing and diagnostic photodiodes are on in-air tables.

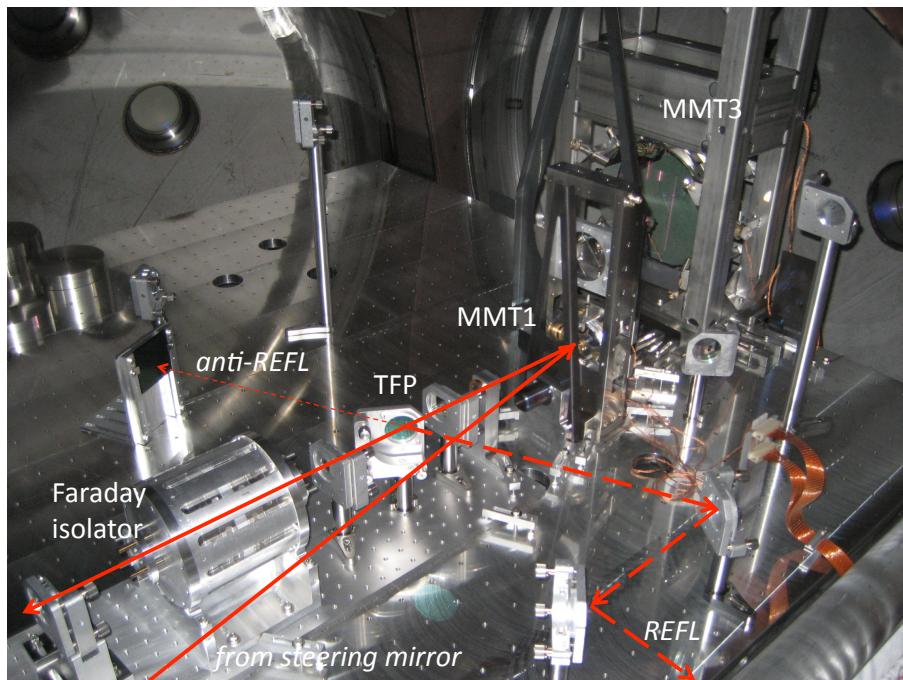
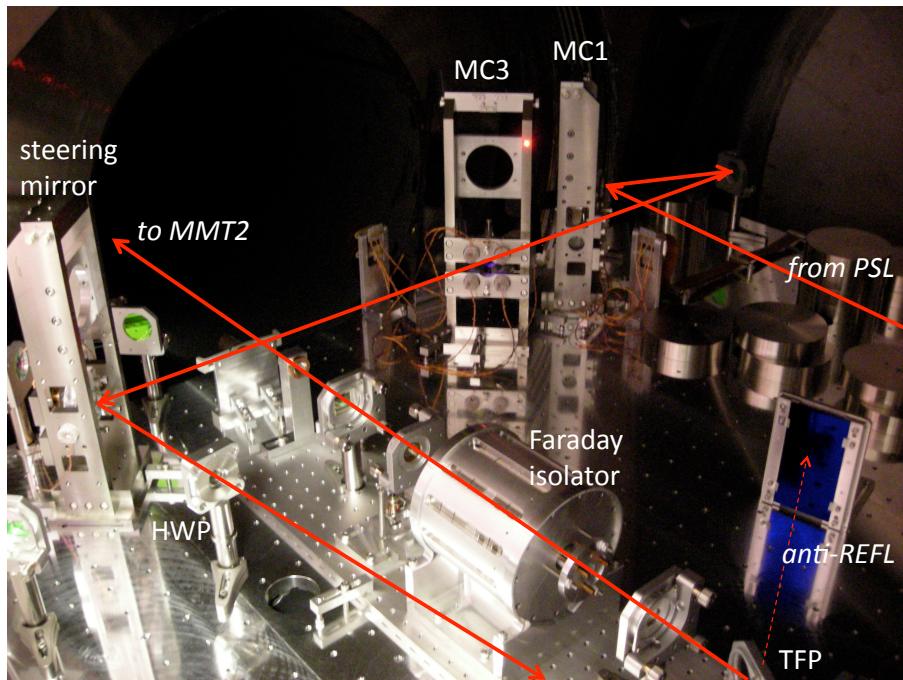


Figure 3-3. Photographs of Enhanced LIGO Input Optics *in situ*. fix font type and size

Table 3-1. Comparison of selected properties of the Initial and Enhanced LIGO EOM crystals, LiNbO<sub>3</sub> and RTP, respectively. RTP was preferred for Enhanced LIGO because of its lower absorption, superior thermal properties, and similar electro-optic properties [1].

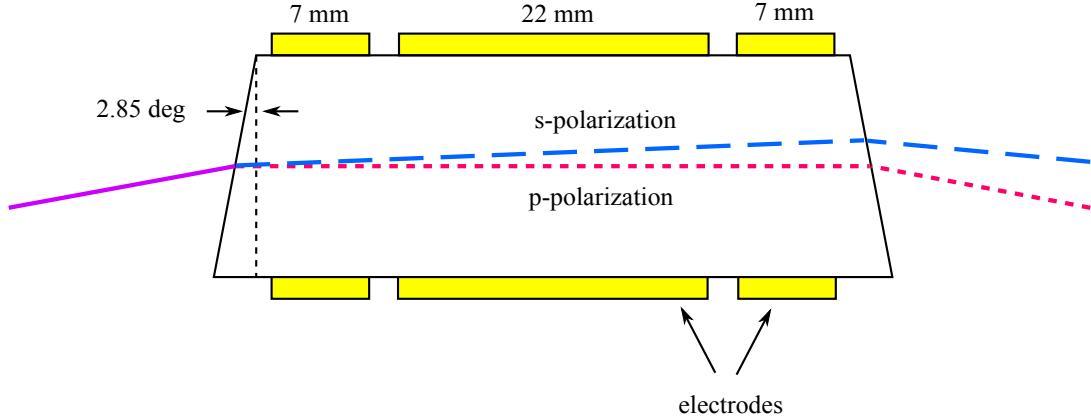
	units	LiNbO <sub>3</sub>	RTP
damage threshold	MW/cm <sup>2</sup>	280	> 600
absorption coeff. at 1064 nm	cm <sup>-1</sup>	< 0.005	< 0.0005
electro-optic coeff. ( $n_z^3 r_{33}$ )	pm/V	306	239
$dn_y/dT$	$10^{-6}/K$	5.4	2.79
$dn_z/dT$	$10^{-6}/K$	37.9	9.24

electro-optic coefficients. Also, RTP's  $dn/dT$  anisotropy is 50% smaller. Table 3-1 compares the properties of most interest of the two crystals.

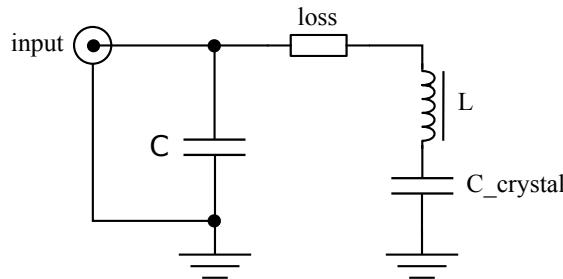
We procured the RTP crystals from Raicol and packaged them into specially designed custom built modulators. The crystal dimensions are  $4 \times 4 \times 40$  mm and their faces are wedged by  $2.85^\circ$  and anti-reflection (AR) coated. The wedge serves to separate the polarizations and prevents an etalon effect, resulting in a suppression of amplitude modulation. Only one crystal is used in the EOM in order to reduce the number of surface reflections. Three separate pairs of electrodes, each with its own resonant LC circuit, are placed across the crystal in series, producing the three required sets of RF sidebands: 24.5 MHz, 33.3 MHz and 61.2 MHz. A diagram is shown in Fig. 3-4. Reference [26] contains further details about the modulator architecture.

### 3.3.2 Mode Cleaner Design

The mode cleaner is a suspended 12.2 m long triangular ring cavity with finesse  $\mathcal{F}=1282$  (refer to Appendix 9.4 for a measurement of the finesse) and free spectral range of 12.243 MHz. The three mirror architecture was selected over the standard two mirror linear filter cavity because it acts as a polarization filter and because it eliminates direct path back propagation to the laser [27]. A pick-off of the reflected beam is naturally facilitated for use in generating control signals. A potential downside to the three mirror design is the introduction of astigmatism, but this effect is negligible due to the small opening angle of the mode cleaner.



A A single RTP crystal is sandwiched between three sets of electrodes that apply three different modulation frequencies. The wedged ends of the crystal separate the polarizations of the light. The p-polarized light is used in the interferometer.



B A schematic for each of the three impedance matching circuits of the EOM. For the three sets of electrodes, each of which creates its own  $C_{crystal}$ , a capacitor is placed parallel to the LC circuit formed by the crystal and a hand-wound inductor. The circuits provide  $50\ \Omega$  input impedance on resonance and are housed in a separate box from the crystal.

Figure 3-4. Electro-optic modulator design.

The MC has a round-trip length of 24.5 m. The beam waist has a radius of 1.63 mm and is located between two  $45^\circ$  flat mirrors, MC1 and MC3 (see Fig. 3-2). A concave third mirror, MC2, with an 18.15 m radius of curvature forms the far point of the mode cleaner's isosceles triangle shape. The power stored in the MC is 408 times the amount coupled in, equivalent to about 2.7 kW in Initial LIGO and at most 11 kW for Enhanced LIGO. The peak irradiances are  $32\text{ kW/cm}^2$  and  $132\text{ kW/cm}^2$  for Initial LIGO and Enhanced LIGO, respectively. The scattering losses of each mirror due to measured surface microroughness are 22 ppm.

The mode cleaner mirrors are 75 mm in diameter and 25 mm thick. The substrate material is fused silica and the mirror coating is made of alternating layers of silica and tantalum. In order to reduce the absorption of heat in these materials and therefore improve the transmission and

modal quality of the beam in the mode cleaner, we removed particulate by drag wiping the surface of the MC mirrors with methanol and optical tissues. The mode cleaner was otherwise identical to that in Initial LIGO.

### 3.3.3 Faraday Isolator Design

The Enhanced LIGO Faraday isolator design required not only the use of low absorption optics, but additional design choices to mitigate any residual thermal lensing and birefringence. In addition, trade-offs between optical throughput in the forward direction, optical isolation in the backwards direction, and feasibility of physical access of the return beam for signal use were considered. The result is that the Enhanced LIGO Faraday isolator needed a completely new architecture and new optics compared to both the Initial LIGO FI and commercially available isolators.

Figure 3-5 shows a schematic of the Enhanced LIGO Faraday Isolator. It begins and ends with low absorption calcite wedge polarizers (CWP). Between the CWPs is a thin film polarizer (TFP), a deuterated potassium dihydrogen phosphate (DKDP) element, a half-wave plate (HWP), and a Faraday rotator. The rotator is made of two low absorption terbium gallium garnet (TGG) crystals sandwiching a quartz rotator (QR) inside a 7-disc magnet with a maximum field strength of 1.16 T. The forward propagating beam upon passing through the TGG, QR, TGG, and HWP elements is rotated by  $+22.5^\circ - 67.5^\circ + 22.5^\circ + 22.5^\circ = 0^\circ$ . In the reverse direction, the rotation through HWP, TGG, QR, TGG is  $-22.5^\circ + 22.5^\circ + 67.5^\circ + 22.5^\circ = 90^\circ$ . The TGG crystals are non-reciprocal devices while the QR is reciprocal.

#### 3.3.3.1 Thermal birefringence

Thermal birefringence is addressed in the Faraday rotator by the use of the two TGG crystals and one quartz rotator rather than the typical single TGG [28]. In this configuration, any thermal polarization distortions that the beam experiences while passing through the first TGG rotator will be partially undone upon passing through the second. (Add sentence of further explanation.) The multiple elements in the magnet required a larger magnetic field than in Initial LIGO and

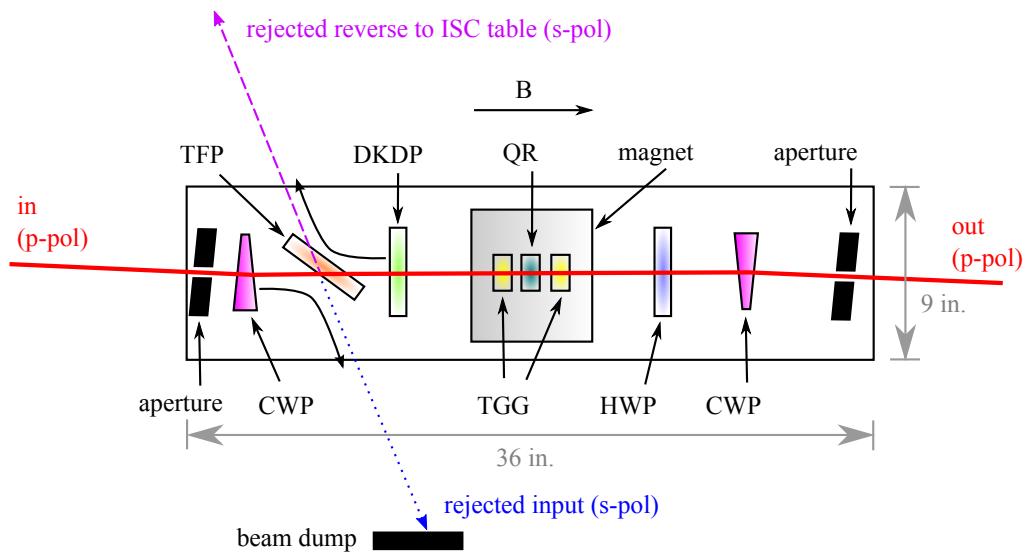
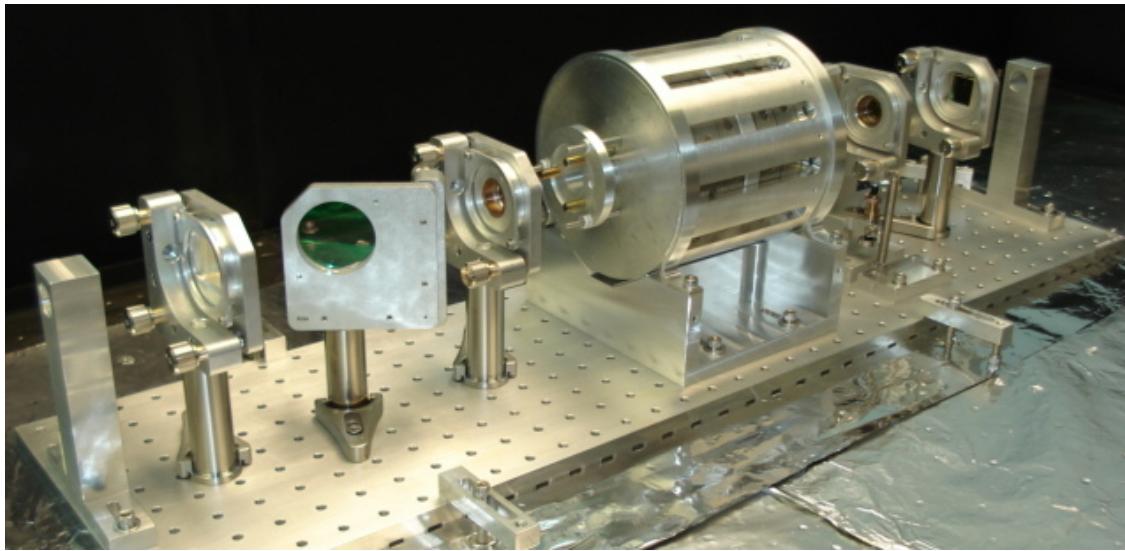


Figure 3-5. Faraday isolator photograph and schematic. The Faraday isolator preserves the polarization of the light in the forward-going direction and rotates it by 90 degrees in the reverse direction. Light from the MC enters from the left and exits at the right towards the interferometer. It is ideally p-polarized, but any s-polarization contamination is promptly diverted  $\sim 10$  mrad by the CWP and then reflected by the TFP and dumped. The p-polarized reflected beam from the interferometer enters from the right and is rotated to s-polarized light which is picked-off by the TFP and sent to the Interferometer Sensing and Control (ISC) table. Any imperfections in the Faraday rotation of the interferometer return beam results in p-polarized light traveling backwards along the original input path.

a Faraday rotator housing that is 15.5 cm in diameter by 16.1 cm long. The TGG diameter is 20 mm.

### 3.3.3.2 Thermal lensing

Thermal lensing in the Faraday isolator is addressed by including DKDP, a negative  $dn/dT$  material, in the beam path. Absorption of light in the DKDP results in a de-focusing of the beam, which partially compensates for the thermal focusing induced by absorption in the TGGs [29, 30]. The optical path length (thickness) of the DKDP is chosen to slightly over-compensate the positive thermal lens induced in the TGG crystals, anticipating other positive thermal lenses in the system.

### 3.3.3.3 Polarizers

The polarizers used (two CWP<sup>s</sup> and one TFP) each offer advantages and disadvantages related to optical efficiency in the forward-propagating direction, optical isolation in the reflected direction, and thermal beam drift. The CWP<sup>s</sup> have very high extinction ratios ( $> 10^5$ ) and high transmission ( $> 99\%$ ) contributing to good optical efficiency and isolation performance. However, the angle separating the exiting orthogonal polarizations of light is very small, on the order of 10 mrad. This requires relatively large distances to pick off the beams needed for interferometer sensing and control. In addition, thermally induced index of refraction gradients due to the  $4.95^\circ$  wedge angle of the CWP<sup>s</sup> result in thermal drift. However, the CWP<sup>s</sup> for the Enhanced LIGO Faraday have a measured low absorption of  $0.0013 \text{ cm}^{-1}$  with an expected thermal lens of 60 m at 30 W and drift of less than  $1.3 \mu\text{rad/W}$  [1].

The advantages of the thin film polarizer over the calcite wedge polarizer are that it exhibits negligible thermal drift when compared with CWP<sup>s</sup> and it operates at the Brewster angle of  $55^\circ$ , thus diverting the return beam in an easily accessible way. However, the TFP has a lower transmission than the CWP, about 96%, and an extinction ratio of only  $10^3$ .

Thus, the combination of CWP<sup>s</sup> and a TFP combines the best of each to provide a high extinction ratio (from the CWP<sup>s</sup>) and ease of reflected beam extraction (from the TFP). The downsides that remain when using both polarizers are that there is still some thermal drift from

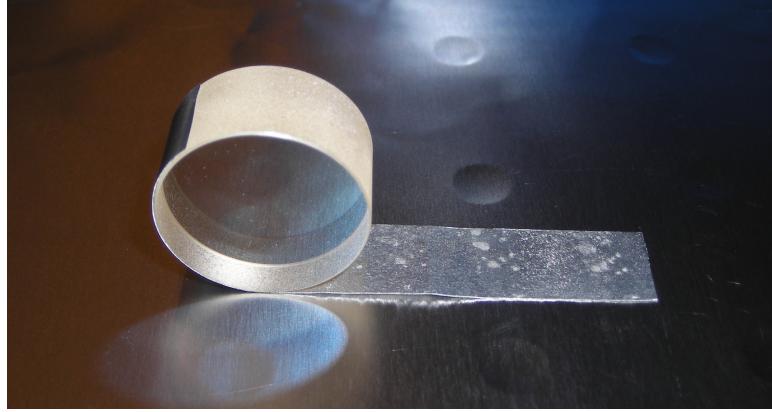


Figure 3-6. Photo of TGG crystal with indium foil wrapping.

the CWP<sub>s</sub>. Also the transmission is reduced due to the TFP and to the fact that there are 16 surfaces from which light can scatter.

### 3.3.3.4 Heat conduction

Faraday isolators operating in a vacuum environment suffer from increased heating with respect to those operating in air. Convective cooling at the faces of the optical components is no longer an effective heat removal channel, so proper heat sinking is essential to minimize thermal lensing and depolarization. It has been shown that Faraday isolators carefully aligned in air can experience a dramatic reduction in isolation ratio (> 10-15 dB) when placed in vacuum [31]. The dominant cause is the coupling of the photoelastic effect to the temperature gradient induced by laser beam absorption. Also of importance is the temperature dependence of the Verdet constant—different spatial parts of the beam experience different linear polarizations in the presence of a temperature gradient.

To improve heat conduction away from the Faraday rotator optical components, we designed housing for the TGG and quartz crystals that provided improved heat sinking to the Faraday rotator. We also wrapped the TGGs with indium foil as pictured in Fig. 3-6 to improve contact with the housing, and we cushioned the DKDP and the HWP with indium wire in their aluminum holders. This has the additional effect of avoiding the development of thermal stresses in the crystals, an especially important consideration for the very fragile DKDP.

### 3.3.4 Mode-matching Telescope Design

The mode matching into the interferometer (at Livingston) was measured to be at best 90% in Initial LIGO. Because of the stringent requirements placed on the LIGO vacuum system to reduce phase noise through scattering by residual gas, standard opto-mechanical translators are not permitted in the vacuum; it is therefore not possible to physically move the mode matching telescope mirrors while operating the interferometer. Through a combination of needing to move the MMTs in order to fit the new Faraday isolator on the in-vacuum optics table and additional measurements and models to determine how to improve the coupling, a new set of MMT positions was chosen for Enhanced LIGO. Fundamental design considerations are discussed in Ref. [32].

## 3.4 Performance of the Enhanced LIGO Input Optics

The most convincing figure of merit for the Input Optics performance is that the Enhanced LIGO interferometers achieved low-noise operation with 20 W input power without thermal issues from the IO. Additionally, the Input Optics were operated successfully up to the available 30 W of power. (Instabilities with other interferometer subsystems limited the Enhanced LIGO science run operation to 20 W.) We present in this section detailed measurements of the Input Optics performance during Enhanced LIGO. Specific measurements and results presented in figures and the text come from Livingston; performance at Hanford was similar and is included in tables summarizing the results.

### 3.4.1 Optical efficiency

The optical efficiency of the Enhanced LIGO Input Optics from EOM to recycling mirror was 75%, a marked improvement over the approximate 60% that was measured for Initial LIGO. A substantial part of the improvement came from the discovery and subsequent correction of a 6.5% loss at the second of the in-vacuum steering mirrors directing light into the MC (refer to Fig. 3-2). A 45° reflecting mirror had been used for a beam with an 8° angle of incidence. Losses attributable to the mode cleaner and Faraday isolator are described in the following sections. A summary of the IO power budget is found in Table 3-2.

Table 3-2. Enhanced LIGO Input Optics power budget. Errors are  $\pm 1\%$ , except for the TFP loss whose error is  $\pm 0.1\%$ . The composite mode cleaner transmission is the percentage of power after the MC to before the MC and is the product of the MC visibility and transmission. Initial LIGO values, where known, are included in parentheses and have errors of several percent.

	Livingston	Hanford
Mode cleaner visibility	92%	97%
Mode cleaner transmission	88%	90%
Composite MC transmission	81% (72%)	87%
Faraday transmission	93% (86%)	94% (86%)
- Thin film polarizer loss	4.0%	2.7%
IO efficiency (PSL to RM)	75% (60%)	82%

### 3.4.1.1 Mode cleaner losses

The mode cleaner was the greatest single source of power loss in both Initial and Enhanced LIGO. The mode cleaner visibility, defined here as

$$\text{visibility} = 1 - \frac{P_{\text{reflected}}}{P_{\text{in}}}, \quad (3.4.1)$$

the ratio of the amount of light coupled into the MC to the amount impinging the mode cleaner input mirror, was 92%. Losses are the result of higher order mode content and mode mismatch into the MC. The visibility was constant within 0.04% up to 30 W input power at both sites, providing a positive indication that thermal aberrations in the mode cleaner were negligible.

Of the light coupled into the mode cleaner, 88% was transmitted, corresponding to an average loss of 98 ppm per mirror. Based on the mirrors' known surface micro-roughness, the scatter loss is expected to be 22 ppm/mirror. Part of the discrepancy between expectation and measurement was determined to come from poor AR coatings. We measured a 1.3% reflection from the AR coatings on MC mirrors at both Livingston and Hanford, a transmitted power loss equivalent to 10 ppm of intracavity loss per mirror.

Another source of MC losses is through absorption of heat by particulates residing on the mirror's surface. We measured the absorption with a technique that makes use of the frequency shift of the thermally driven drumhead eigenfrequencies of the mirror substrate [33]. The frequency shift directly correlates with the MC absorption via the substrate's change in Young's

Table 3-3. Absorption values for the Livingston and Hanford mode cleaner mirrors before (in parentheses) and after drag wiping. The precision is  $\pm 10\%$ .

mirror	Livingston	Hanford
MC1	2.1 ppm (18.7 ppm)	5.8 (6.1 ppm)
MC2	2.0 ppm (5.5 ppm)	7.6 (23.9 ppm)
MC3	3.4 ppm (12.8 ppm)	15.6 (12.5 ppm)

modulus with temperature,  $dY/dT$ . A finite element model (COMSOL) was used to compute the expected frequency shift from a temperature change of the substrate resulting from the mirror coating absorption. The eigenfrequencies for each mirror at room temperature are 28164 Hz, 28209 Hz, and 28237 Hz, respectively.

We cycled the power into the mode cleaner between 0.9 W and 5.1 W at 3 hour intervals, allowing enough time for a thermal characteristic time constant to be established. At the same time, we recorded the frequencies of the high Q drumhead mode peaks as found in the mode cleaner frequency error signal, heterodyned down by 28 kHz. See Figure 3-7. Correcting for ambient temperature fluctuations, we find a frequency shift of 0.043, 0.043, and 0.072 Hz/W. As a result of drag-wiping the mirrors, the absorption decreased from 18.7, 5.5 and 12.8 ppm per mirror, respectively, to 2.1, 2.0, and 3.4 ppm per mirror. The final results for both Livingston and Hanford are shown in Table 3-3.

### 3.4.1.2 Faraday isolator losses

The Faraday isolator was the second greatest source of power loss with its transmission of 93%. This was an improvement over the 86% transmission of the Initial LIGO FI. The most lossy element in the Faraday isolator was the thin film polarizer, accounting for 4% of total losses. The integrated losses from AR coatings and absorption in the TGGs, CWP, HWP, and DKDP account for the remaining 3% of missing power.

### 3.4.2 Faraday Isolation Ratio

The isolation ratio is defined as the ratio of power incident on the Faraday in the reverse direction (the light reflected from the interferometer) to the power transmitted in the reverse direction and is often quoted in decibels: isolation ratio =  $10 \log_{10}(P_{in-reverse}/P_{out-reverse})$ . We

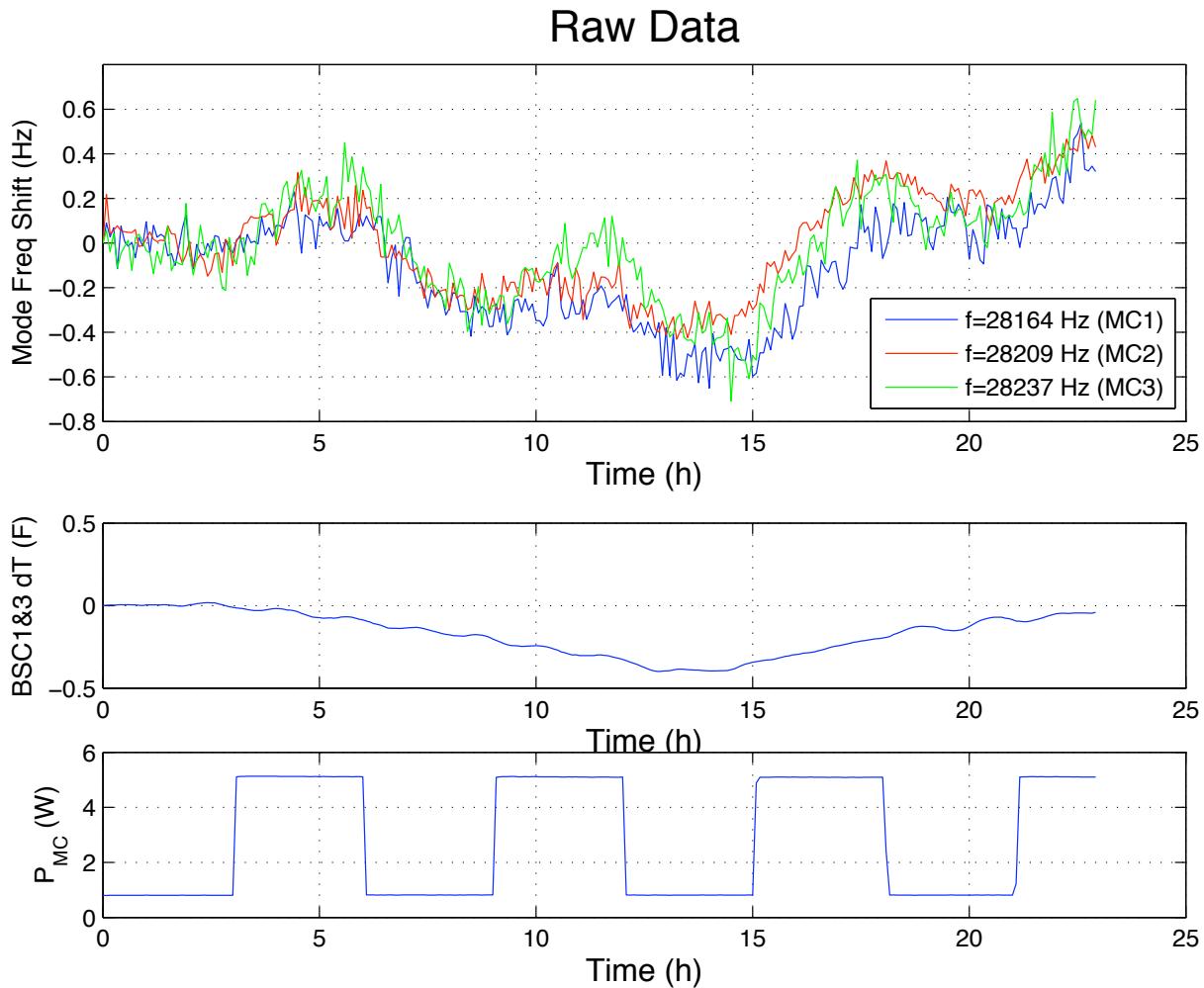


Figure 3-7. Data from the mode cleaner absorption measurement. Power into the MC was cycled between 0.9 W and 5.1 W at 3 hour intervals (bottom frame) and the change in frequency of the drumhead mode of each mirror was recorded (top frame). The ambient temperature (middle frame) was also recorded in order to correct for its effects.

measured the isolation ratio of the Faraday isolator as a function of input power both in air prior to installation and *in situ* during Enhanced LIGO operation.

To measure the in-vacuum isolation ratio, we misaligned the interferometer arms so that the input beam would be promptly reflected off of the 97% reflective recycling mirror. This also has the consequence that the Faraday isolator is subjected to twice the input power. Our isolation monitor was a pick-off of the backwards transmitted beam taken immediately after transmission through the Faraday that we sent out of a vacuum chamber viewport. Refer to the *isolation check*

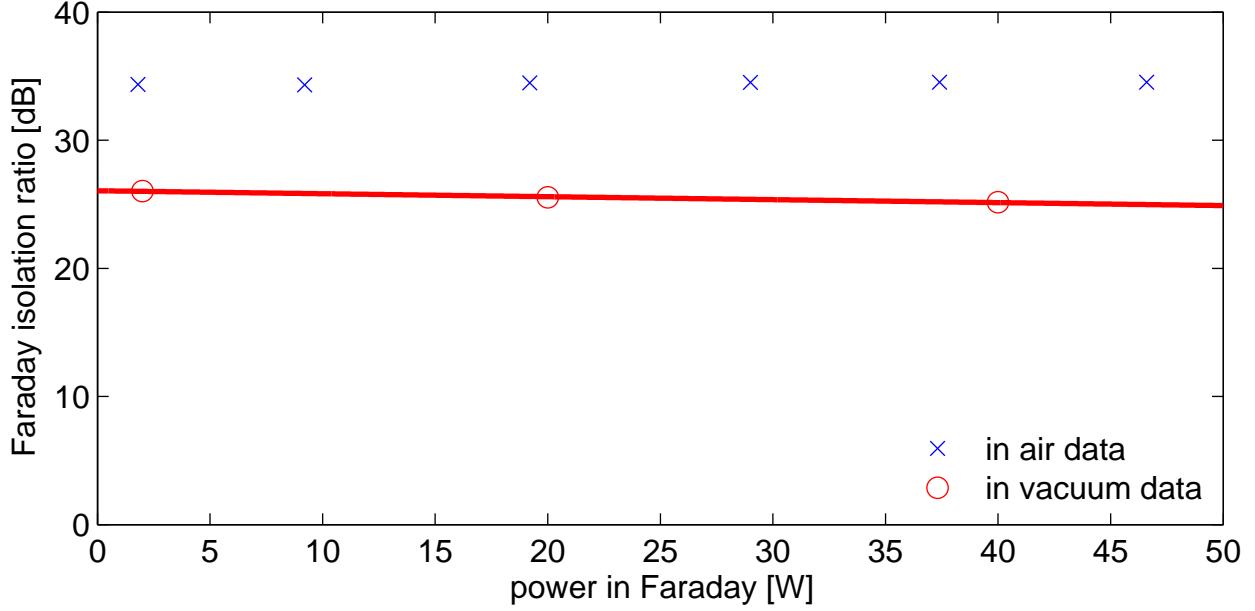


Figure 3-8. Faraday isolator isolation ratio as measured in air prior to installation and *in situ* in vacuum. The isolation worsens by a factor of 6 upon placement of the Faraday in vacuum due to lack of air convection. The solid line is a linear fit to the in-vacuum data, indicating a degradation in isolation of 0.02 dB/W.

beam in Fig. 3-2. The in air measurement was done similarly, except in an optics lab with a reflecting mirror placed directly after the Faraday.

Figure 3-8 shows our isolation ratio data. Most notably, we observe an isolation decrease of a factor of six upon placing the Faraday isolator in vacuum, a result consistent with that reported by Ref. [31]. In air the isolation ratio is a constant  $34.46 \pm 0.04$  dB from low power up to 47 W, and in vacuum the isolation ratio is 26.5 dB at low power. The underlying cause is the absence of cooling by air convection. If we attribute the loss to the TGGs, then based on the change in TGG polarization rotation angle necessary to produce the measured isolation drop of 8 dB and the temperature dependence of the TGG's Verdet constant, we can put an upper limit of 11 K on the crystal temperature rise from air to vacuum. Furthermore, a degradation of 0.02 dB/W is measured in vacuum.

### 3.4.3 Thermal steering

We measured the *in situ* thermal angular drift of both the beam transmitted through the mode cleaner and of the reflected beam from the Faraday isolator with up to 25 W input power. Just as

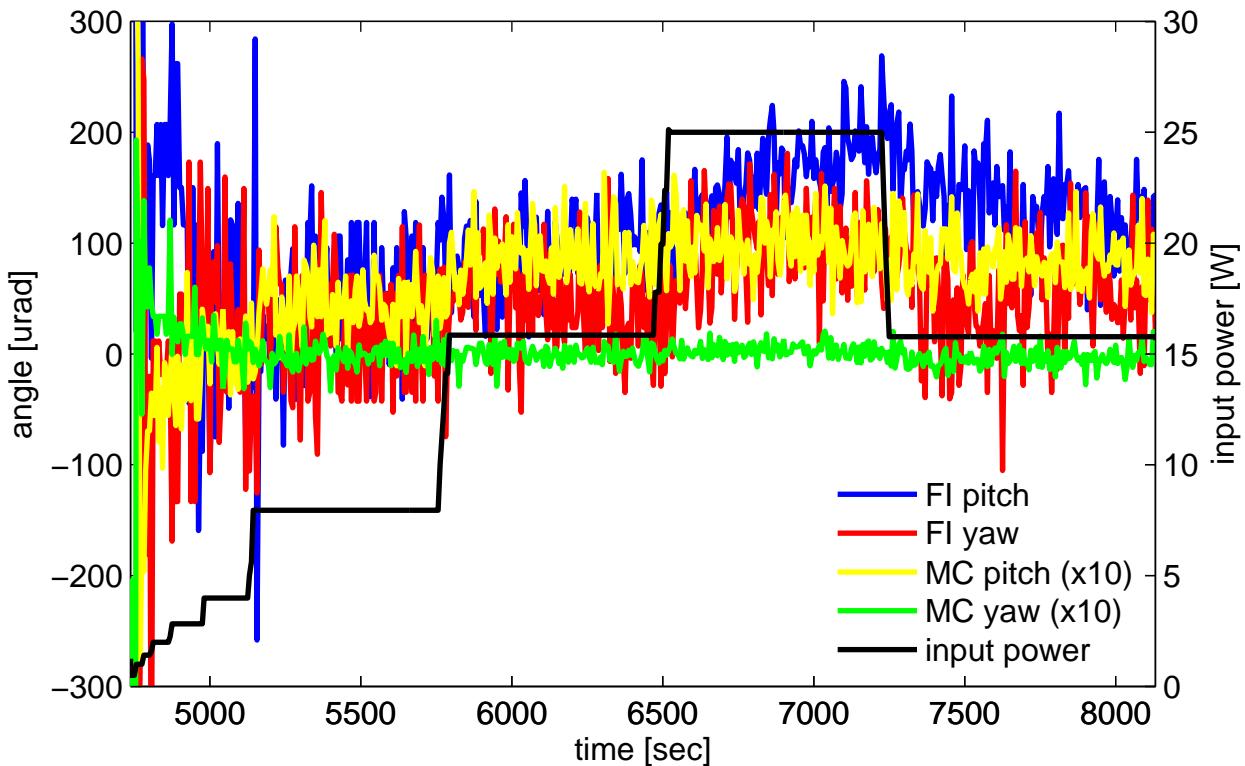
for the isolation ratio measurement, we misaligned the interferometer arms so that the input beam would be promptly reflected off of the recycling mirror. The Faraday rotator was thus subjected to up to 50 W total and the MC to 25 W.

Pitch and yaw motion of the mode cleaner transmitted and interferometer reflected beams were recorded using the quadrant photodiode (QPD) on the Input Optics table and the RF alignment detectors on the Interferometer Sensing and Control table (see Fig. 3-2). There are no lenses between the MC waist and its measurement QPD, so only the path length between the two were needed to calibrate in radians the pitch and yaw signals on the QPD. The interferometer reflected beam, however, passes through several lenses. Thus, ray transfer matrices and the two alignment detectors were necessary to extract the Faraday drift calibration.

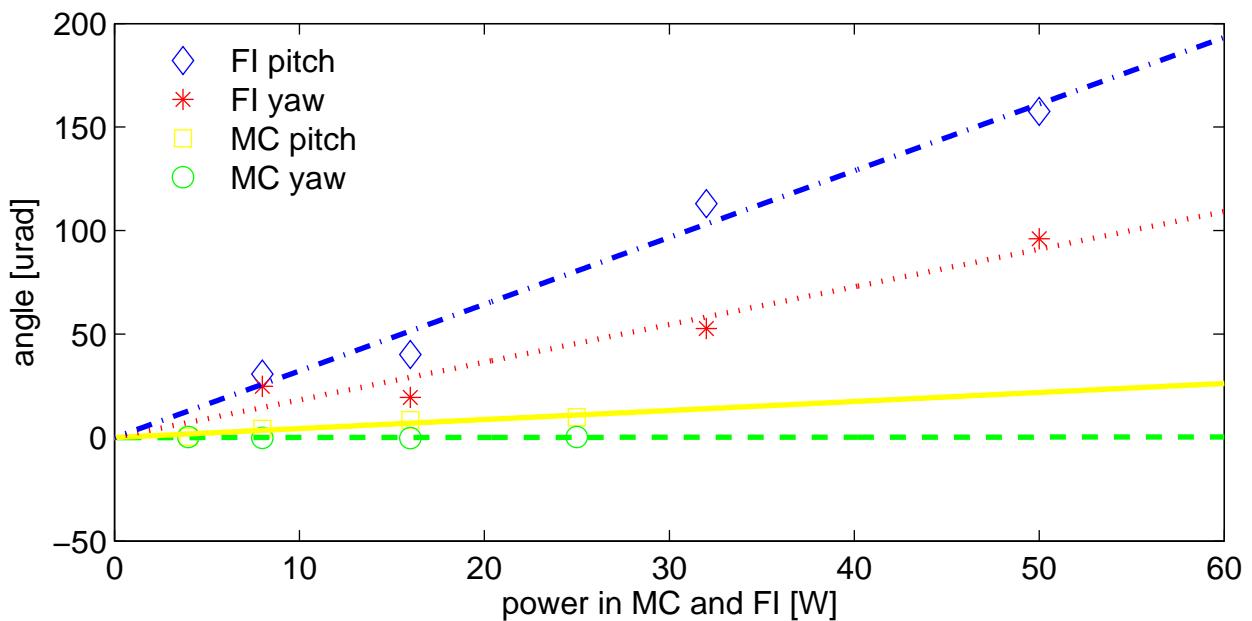
Figure 3-9 shows the calibrated beam steering data. The angle of the beam out of the mode cleaner does not change measurably as a function of input power in yaw (4.7 nrad/W) and changes by only 440 nrad/W in pitch. For the Faraday isolator, we record a beam drift originating at the center of the Faraday rotator of 1.8  $\mu$ rad/W in yaw and 3.2  $\mu$ rad/W in pitch. Therefore, when ramping the input power up to 30 W during a full interferometer lock, the upper limit on the drift experienced by the reflected beam is about 100  $\mu$ rad. This is a thirty-fold reduction with respect to the Initial LIGO Faraday isolator and represents a fifth of the beam's divergence angle,  $\theta_{div} = 490 \mu$ rad.

### 3.4.4 Thermal Lensing

We measured the profiles of both the beam transmitted through the mode cleaner and the reflected beam picked off by the Faraday isolator at low ( $\sim 1$  W) and high ( $\sim 25$  W) input powers to assess the degree of thermal lensing induced in the MC and FI. Again, we misaligned the interferometer arms so that the input beam would be promptly reflected off the recycling mirror. We picked off a fraction of the reflected beam on the Interferometer Sensing and Control table and of the mode cleaner transmitted beam on the Input Optics table (refer to Fig. 3-2), placed lenses in each of their paths, and measured the beam diameters at several locations on



A Angular motion of the beam at the MC waist and FI rotator as the input power is stepped. The beam is double-passed through the Faraday isolator, so it experiences twice the input power.



B Average beam angle per power level in the MC and FI. Linear fits to the data are also shown. The slopes for MC yaw, MC pitch, FI yaw, and FI pitch, respectively, are 0.0047, 0.44, 1.8, and 3.2  $\mu$ rad/W.

Figure 3-9. Mode cleaner and Faraday isolator thermal drift data.

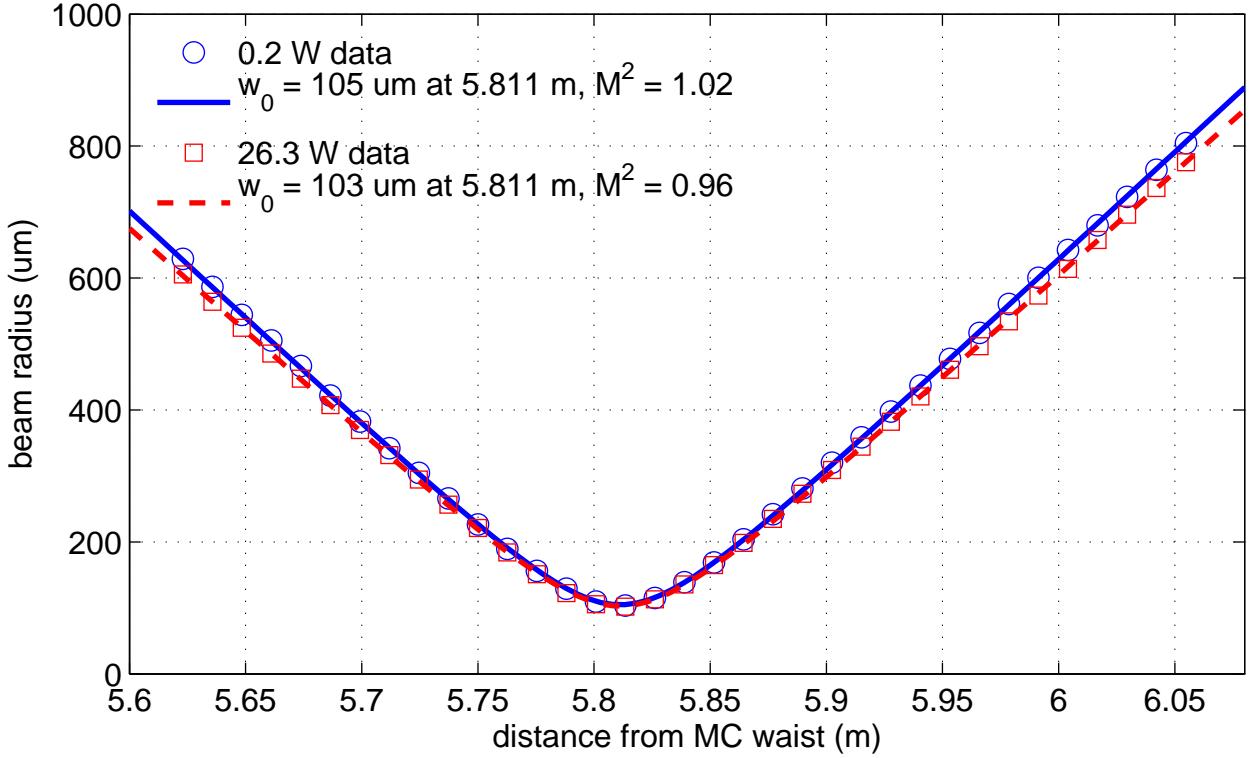


Figure 3-10. Profile at high and low powers of a pick-off of the beam transmitted through the mode cleaner. The precision of the beam profiler is  $\pm 5\%$ . Within the error of the measurement, there are no obvious degradations.

either side of the waists created by the lenses. A change in the beam waist size or position as a function of laser power indicates the presence of a thermal lens.

As seen in Fig. 3-10 and 3-11, the waists of the two sets of data are collocated—no thermal lens is measured. For the Faraday isolator, the divergence of the low and high power beams differs, indicating that the beam quality degrades with power. The  $M^2$  factor at 1 W is 1.04 indicating the beam is nearly perfectly a TEM<sub>00</sub> mode. At 25 W,  $M^2$  increases to 1.19, corresponding to increased higher order mode content. The percentage of power in higher order modes depends strongly on the mode order and relative phases of the modes, and thus cannot be determined from this measurement [34].

The results for the mode cleaner data are consistent with no thermal lensing. The high and low power beam profiles are within each other's error bars and well below our requirements.

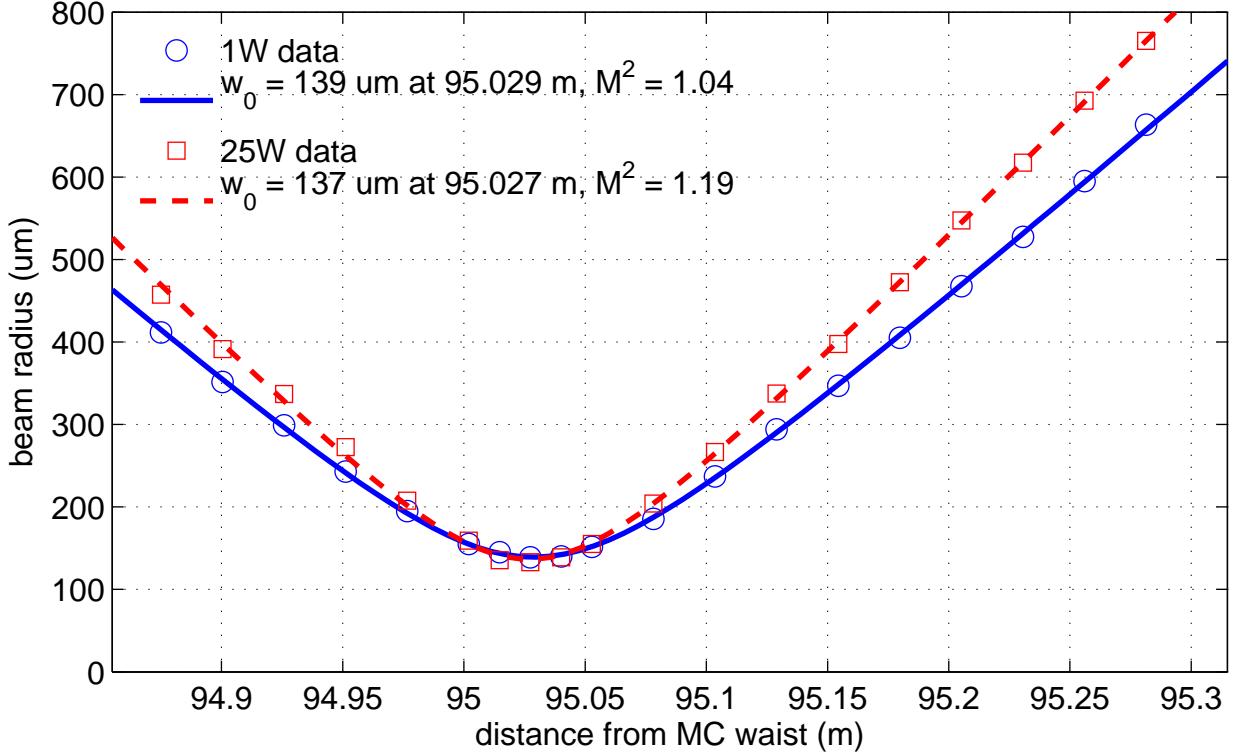


Figure 3-11. Faraday isolator thermal lensing data. With 25 W into the Faraday isolator (corresponding to 50 W in double pass), the beam has a steeper divergence than a pure TEM<sub>00</sub> beam, indicating the presence of higher order modes. Errors are  $\pm 5.0\%$  for each data point.

Figure 3-12. EOM thermal lensing data.

We also measured the thermal lensing of the electro-optic modulator prior to its installation in Enhanced LIGO by comparing beam profiles of a 160 W beam with and without the EOM in its path. The data for both cross-sections of the beam is presented in Fig. 3-12. We observe no significant thermal lensing in the y-direction and a small effect in the x-direction. An upper limit for the thermal lens in the x-direction can be calculated to be greater than 4 m, which is 10 times larger than the Rayleigh range of the spatial mode. The mode matching degradation is therefore less than 1%. Although a direct test for Advanced LIGO because of the power used, this measurement also serves to demonstrate the effectiveness of the EOM design for Enhanced LIGO powers.

### **3.4.5 Mode Matching**

We measured the effectiveness of the mode-matching telescope by taking the ratio of power at the reflected port when all of the interferometer cavities are on resonance to the power in the reflected beam when the cavities are unlocked. Since the impedance matching is near perfect, all light at the reflected port during interferometer lock is attributable to a mode mismatch. Initially, anywhere between 10% and 17% of the light was rejected by the cavity due to poor, power-dependent mode matching. After translating the mode-matching telescope mirrors during a vacuum chamber incursion and upgrading the other IO components, the ratio we measured was 8% independent of input power. The MMT succeeds at coupling 92% of the light into the interferometer at all times, marking both an improvement in MMT mirror placement and success in eliminating measurable thermal issues.

## **3.5 Implications for Advanced LIGO**

As with other Advanced LIGO interferometer components, Enhanced LIGO served as a technology demonstrator for the Advanced LIGO Input Optics, albeit at lower laser powers. The performance of the Enhanced LIGO Input Optics components, at 20 W of input power allows us to infer their performance in Advanced LIGO. The requirements for the Advanced LIGO Input Optics demand are for similar performance to Enhanced LIGO, but with almost 8 times the laser power.

The Enhanced LIGO electro-optic modulator showed no thermal lensing, degraded transmission, nor damage in over 1 million hours of sustained operation. Measurements of the thermal lensing in RTP at powers up to 160 W show a relative power loss of < 0.4%, indicating that thermal lensing should be negligible in Advanced LIGO. Peak irradiances in the EOM will be approximately four times that of Enhanced LIGO (a 45% larger beam diameter will somewhat offset the increased power). Testing of RTP at 10 times the expected Advanced LIGO irradiance over 100 hours show no signs of damage or degraded transmission.

The mode cleaner showed no measurable change in operational state as a function of input power. This bodes well for the Advanced LIGO mode cleaner. Compared with the Enhanced

LIGO mode cleaner, the Advanced LIGO mode cleaner is designed with a lower finesse (520) than Initial LIGO (1282). For 150 W input power, the Advanced LIGO mode cleaner will operate with 3 times greater stored power than Initial LIGO. The corresponding peak irradiance is  $400 \text{ kW/m}^2$ , well below the continuous wave coating damage threshold. Absorption in the Advanced LIGO mode cleaner mirror optical coatings has been measured at 0.5 ppm, roughly four times less than the best mirror coating absorption in Enhanced LIGO, so the expected thermal loading due to coating absorption should be reduced in Advanced LIGO. The larger Advanced LIGO mode cleaner mirror substrates and higher input powers result in a significantly higher contribution to bulk absorption, roughly 20 times Enhanced LIGO, however the expected thermal lensing leads to small change (< 0.5%) in the output mode [25].

The Enhanced LIGO data obtained from the Faraday isolator allows us to make several predictions about how it will perform in Advanced LIGO. The measured isolation ratio decrease of 0.02 dB/W will result in a loss of 3 dB for a 150 W power level expected for Advanced LIGO relative to its cold state. However, the Advanced LIGO Faraday isolator will employ an adjustable half wave plate *in situ*, which will allow for a partial restoration of the isolation ratio. The maximum thermally induced angular steering expected is 480  $\mu\text{rad}$ (using a drift rate of 3.2  $\mu\text{rad/W}$ ), approximately equal to the beam divergence angle. This has some implications for the Advanced LIGO length and alignment sensing and control system, since the reflected Faraday isolator beam is used as a sensing beam. Operation of Advanced LIGO at high powers will likely require the use of a beam stabilization servo to lock the position of the reflected beam on the sensing photodiodes. Although no measurable thermal lensing was observed (no change in the beam waist size or position), the measured presence of higher order modes in the FI at high powers is suggestive of imperfect thermal lens compensation by the DKDP. This potentially can be reduced by a careful selection of the thickness of the DKDP to better match the absorbed power in the TGG crystals.

### **3.6 Summary**

In summary, we have presented a comprehensive investigation of the Enhanced LIGO Input Optics, including the function, design, and performance of the IO. Several improvements to the design and implementation of the Enhanced LIGO IO over the Initial LIGO IO have lead to improved optical throughput and coupling to the main interferometer through a substantial reduction in thermo-optical effects in the major IO optical components, including the electro-optic modulators, mode cleaner, and Faraday isolator. The IO performance in Enhanced LIGO enables us to infer its performance in Advanced LIGO, and indicates that high power interferometry will be possible without severe thermal effects.

## CHAPTER 4

### ANGULAR MOTION OF THE INTERFEROMETER MIRRORS

**write this introduction!** For light to resonate in the interferometer, the mirrors need to point at one another and remain stationary with respect to this pointing. In practice, however, the mirrors are subject to external disturbances.

The mode defined by the mirrors needs good overlap with the input beam's mode. (cavity axis aligned in angle and translation with input axis)

The mirrors in LIGO are suspended, both to isolate them from ground motion and to simulate inertial test masses.

It is necessary to actively align the mirrors for several reasons:

- find the optimal DC alignment of the interferometer
- suppress any motion that does result from external disturbances
- counteract a high power static instability

Furthermore, due to radiation pressure interaction, the system is not even stable at high power.

mirrors are subject to external disturbances, plus they're not stable. we have to do something about it.

mirrors move around, this is bad, moreover they're not even stable.

While we usually talk about the need to control the lengths, for every length degree of freedom, there are two angular degrees of freedom that need to be sensed and controlled for the same reasons.

The mirrors are statically unstable and need to be held in place.

This chapter discusses the causes of mirror angular displacement and the effects of residual mirror motion on the interferometer.

Any torque produces an angular displacement of the mirror as governed by the mirror's torque to angle transfer function.

A consequence is that even when all of the mirrors are perfectly aligned at all frequencies, the simple existence of light in the interferometer makes the arm cavities statically unstable when high enough laser powers are used.

## 4.1 Tolerance for Angular Motion

Make this section correct! power fluctuations only couple quadratically (bi-linearly) to DARM, but the contrast defect thing is *indistinguishable* from gravitational waves. the A2L should still be emphasized.

Besides allowing the interferometer to be in a locked state, minimal motion of the mirrors is necessary to achieve the highest possible sensitivity to strain. The requirements for how much motion is tolerable stem from two effects of misalignment that directly couple to strain sensitivity: failure to achieve maximum power gain, and angle to length coupling. The misalignment tolerances are dictated by what is necessary to prevent the strain sensitivity of the perfectly aligned interferometer from degrading by more than 0.5% in the detection band of 40-7000 Hz [35].

Because the strain sensitivity is proportional to the power buildup (see Eq. 7-1), a decrease in circulating power directly results in a decrease of shot-noise-limited DARM. Differing power fluctuations in the two arm cavities results in a changing contrast defect, a difference in the amount of light returning from one arm compared to the other, which increases the shot noise at the AS port. Excessive fluctuations in the power recycling cavity makes for inconsistent signal to noise ratios for the signals that depend on sideband power. To maintain a power buildup within 1% of maximum, the core optics must have an angular displacement of less than  $10^{-8}$  rad rms with respect to the cavity axis [36]. The derivation of power buildup as a function of mirror angle displacement is found in Appendix 10.5.

**work this paragraph in somewhere** The idea is that when the axis of rotation of a mirror coincides with the center of the beam, any tilt of the mirror about this axis does not affect the path length of the reflected beam. However, if there is a mismatch between rotation axis and beam location, then the light will pick up a longitudinal phase shift when the mirror is tilted. During a full interferometer lock, this is recorded by DARM.

When the beam is located a distance  $x$  away from the center of the mirror, an angular displacement of the mirror  $\theta$  about its center results in a path length change of the beam

$$\Delta L = x * \theta \quad (4.1.1)$$

which has a direct impact on DARM. Therefore, the alignment specifications must include not only tolerable levels of angular motion, but requirements for the physical centering of the beam spots on the mirrors. As detailed in Ref. [36], the beams must be centered on the core optics within 1 mm. At DC, for  $x = 1$  mm and  $\theta = 10^{-7}$  rad,  $\Delta L = 10^{-10}$  m which is four orders of magnitude below the DARM rms of  $10^{-6}$  m. [Convolve my bsm spectra and residual mirror motion spectra to show example.](#)

## 4.2 Sources of Angular Mirror Motion

There is a continuous stream of changing torque inputs to the mirrors that cause them to twist and turn in pitch and in yaw. Some torque inputs exist regardless of the state of the interferometer, while others are a direct consequence of the control systems. The primary torque inputs are introduced here, and further discussion of some of them is found later in the chapter.

The list includes:

- ground motion
- seismic isolation
- coil actuators (length to angle)
- noise impression from the angular control system
- radiation pressure

[say something about seismometer feed-forward signals.](#) [say something about imperfect HEPI pos actuation](#)

### 4.2.1 Ground Motion

The most egregious of these torque inputs is ground motion that makes its way through the multiple stages of seismic isolation to the mirror suspensions and thence to the mirrors. Ground motion is the only source of angular motion that is present regardless of the state of interferometer operation. An example of the shape and amount of angular motion experienced by the core optics due to seismic noise during a relatively quiet seismic time is shown in Fig. 4-1. These spectra include the effect of local velocity damping since the optical levers are always on (see Sec. 2.4.3). The rms mirror motion is of the order  $10^{-7}$  rad. This is the motion that needs to be controlled interferometrically.

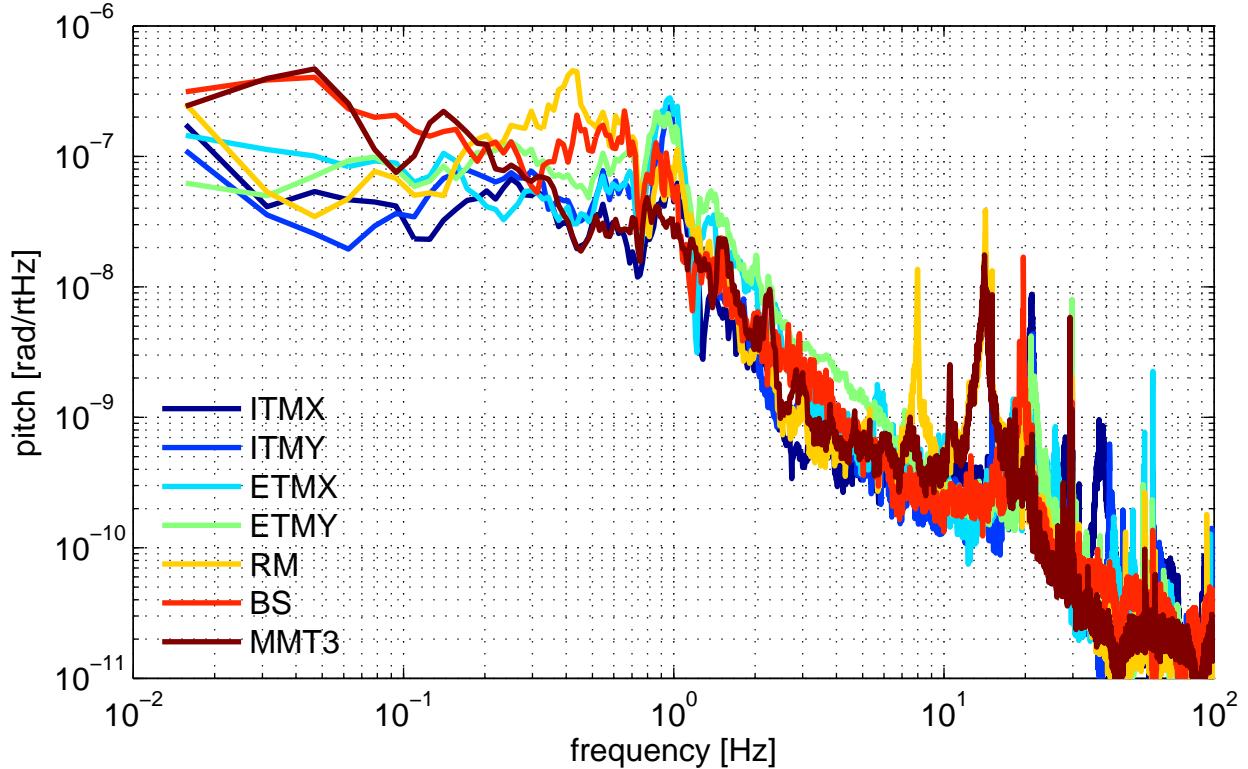


Figure 4-1. Typical angular motion of the core suspended mirrors in the absence of interferometric control. Velocity damping provided by the OSEMs and the optical levers is present. Once the interferometer is locked, the OSEM damping is ramped off.

Proof that this motion indeed originates from the ground can be provided by computing Wiener filters for the seismometer signals to see their coherence with the optical lever error signals. Figures are in appendix [10.3](#)

#### 4.2.2 Coil Actuators

Imperfections in the behavior of the actuators on the rear of the test masses can convert piston (pure translation) drives into torque. The lengths of the cavities are carefully controlled (that's what we strive to be most sensitive to!) and any imbalances between the four electromagnets on a single mirror will create a coupling from length drive to angle (L2A). This effect is measurable, but is carefully tuned out through selecting appropriate digital gains for each of the coils. Relative gain variation is 10% of average. The ability to tune the gains perfectly is limited and the residual length to angle coupling is about 1%. For the typical rms length drive of 1  $\mu$ mon

a core optic and osems separated by a distance of  $\sqrt{2}R$  where  $R$  is the radius of the optic, the 1% L2A coupling results in a  $10^{-8}$  radian displacement:

$$\theta = \frac{0.01 * 10^{-6} \text{ m}}{\sqrt{2} * 0.125 \text{ m}} \approx 10^{-8} \text{ rad.} \quad (4.2.1)$$

#### 4.2.3 Noise from Angular Control

The angular control system, which strives to counteract the above torque inputs to reduce angular motion, introduces angular mirror motion itself. The primary way it contributes noise is through imperfect sensing of the angular displacements. The alignment is also undercontrolled, which ends up allowing the control system to impress input beam motion on the mirrors. These issues are explained in more detail in [4.7](#).

#### 4.2.4 Radiation Pressure

Radiation pressure creates a torque when the beam impinges the mirror off-center. The force on the mirror due to radiation pressure is derived from the change in momentum of a photon upon reflection off the mirror and results in:

$$F_{rp} = \frac{2P}{c} \quad (4.2.2)$$

where  $P$  is the power of the light reflected by the mirror and  $c$  is the speed of light. Assuming the beam of photons strikes the mirror perpendicular to its surface, the torque exerted on a mirror due to radiation pressure is

$$\tau_{rp} = \frac{2Px}{c} \quad (4.2.3)$$

where  $x$  is the distance of the beam from the mirror's center of mass. For a 40 kW beam 1 mm off-center, the torque is on the order of  $10^{-7}$  Nm, yielding an angular displacement of the order  $10^{-7}$  rad as determined by the pendulum torque to angle transfer function (see Section [4.3](#)).

Amongst the various torque inputs, radiation pressure plays a unique role in mirror motion because the torque it exerts depends on the angles of the mirrors. It is best treated not as an external torque, but as a modification to the pendulum torque to angle transfer function. Chapter [5](#)

dedicates a discussion to this matter. In all, radiation pressure shapes the angular dynamics of the mirrors in LIGO and plays an important role in the design of an angular control system.

### 4.3 The Mirror as a Torsion Pendulum

Understanding exactly how these sources of torque on the mirrors convert to angular motion requires a model of the mirror's torque to angle transfer function. The mirrors in LIGO may be regarded as torsion pendula. Each mirror is suspended from a single [xx m diameter](#) wire that loops around the bottom of the barrel of the mirror as shown in Fig. 4-2. Stand-offs glued just above the mirror's center of mass on both sides of the barrel mark the final point of contact of the wire with the mirror, and both ends of the wire are clamped to the top of a suspension cage. The mirror is free to twist an angle  $\theta$  about a horizontal axis passing through its center of mass to create motion in *pitch* and about a vertical axis passing through its center of mass to create a motion in *yaw*.

The angular equation of motion of the mirror is governed by the sum of all torques on the mirror. First, let's consider the most simplistic scenario where there is only a pendulum restoring torque  $\tau_p = -\kappa_p \theta$ , where  $\kappa_p$  is the pendulum's torsional constant. The equation of motion is

$$I\ddot{\theta} + \kappa_p\theta = 0, \quad (4.3.1)$$

which has a solution of  $\theta(t) = \sin(\omega_0 t)$ , where  $\omega_0 = \sqrt{\kappa_p/I}$  is the resonant angular frequency and  $I$  is the mirror's moment of inertia. The pendulum torsional constant serves to make the mirror oscillate indefinitely about its equilibrium position upon the slightest of displacements.

#### 4.3.1 Torque to Angle Transfer Function of a Pendulum

We are particularly interested in the pendulum's response to an external torque, such as seismic noise. In order to calculate the torque to angle transfer function, we must include an external torque term,  $\tau_{ext}$ , in the equation of motion:

$$I\ddot{\theta} + \gamma\dot{\theta} + \kappa_p\theta = \tau_{ext}. \quad (4.3.2)$$

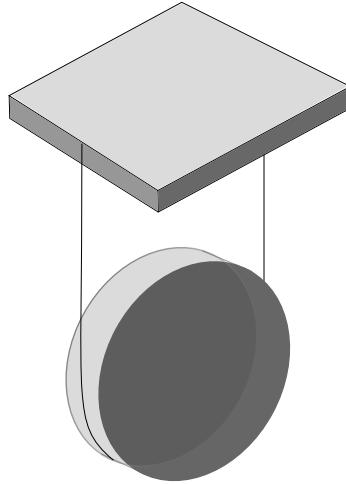


Figure 4-2. Cartoon of a LIGO suspension. [Improve this.](#)

Here, we have also introduced a velocity damping term,  $\gamma$ , to best model reality. Taking the Laplace transform to convert from the time domain to the frequency domain, we have:

$$Is^2\Theta + \gamma s\Theta + \kappa_p\Theta = \tau_{ext} \quad (4.3.3)$$

where  $s$  is a complex parameter. The transfer function is then defined as

$$H(s) := \frac{\Theta(s)}{\tau_{ext}(s)} = \frac{1}{Is^2 + \gamma s + \kappa_p}. \quad (4.3.4)$$

We are only interested in examining the transfer function for a pure sine wave excitation,  $e^{i\omega t}$ , so we substitute  $s = i\omega$  to get

$$H(\omega) = \frac{1/I}{\omega_0^2 - \omega^2 + i\gamma\omega/I}. \quad (4.3.5)$$

The resonant frequency of this damped system can be computed by finding the  $\omega$  at which the amplitude of the transfer function,  $[I^2[\omega^2 - \omega_0^2]^2 + \gamma^2\omega^2]^{-1/2}$ , is maximized:

$$\omega_{res} = \sqrt{\omega_0^2 - \frac{\gamma^2}{2I^2}}. \quad (4.3.6)$$

We note that damping serves to reduce the resonant frequency.

A quantity that is more familiar than  $\gamma$  for describing the losses of a system with a real resonance is the quality factor,  $Q := \omega_{res}/\text{FWHM}$ , where FWHM is the full-width-half-max

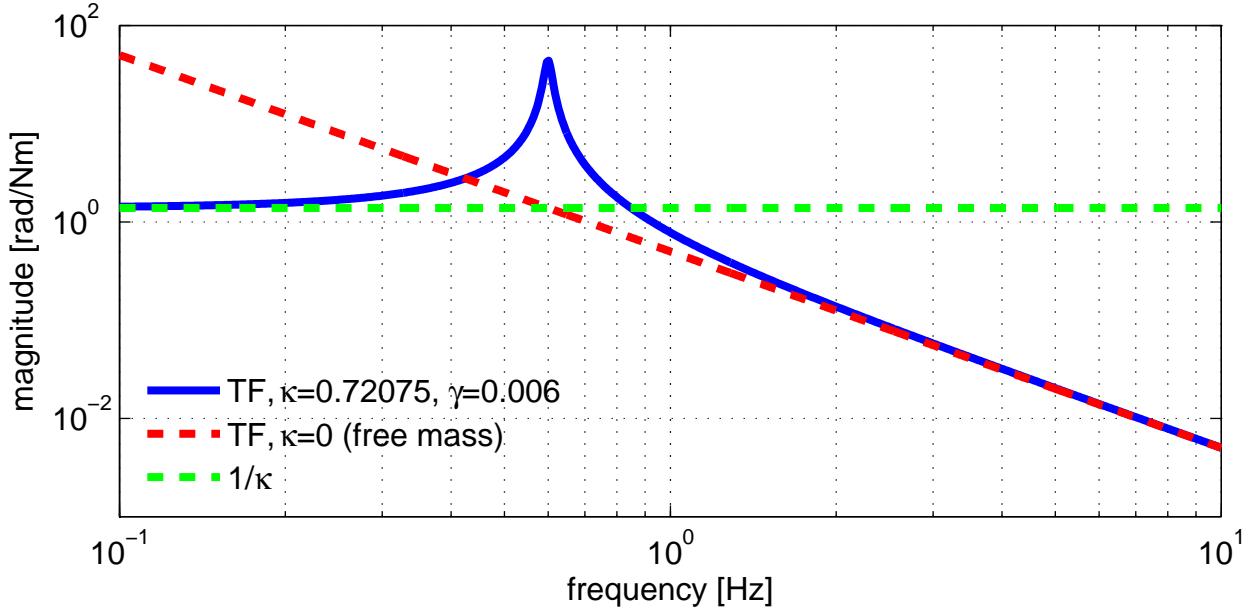


Figure 4-3. Torque to pitch transfer function of a LIGO core optic (blue). The optic acts like a free mass at high frequencies (red) and the DC magnitude of the transfer function is determined by the inverse torsional constant (green). A damping constant  $\gamma = 0.006$  ( $Q = 32$ ) was selected for pictorial representation only. The resonant frequency of LIGO core optics in yaw is 0.5 Hz.

of the transfer function's amplitude-squared resonance. When the losses are small,  $\omega_{res} \approx \omega_0$  and  $\text{FWHM} \approx \gamma/I$  (see Feynman 23-4). The quality factor is then well approximated by  $Q = \sqrt{\kappa_p I}/\gamma$ . The transfer function written in terms of  $Q$  is

$$H(\omega) = \frac{1/I}{\omega_0^2 - \omega^2 + i\omega\omega_0/Q}. \quad (4.3.7)$$

Figure 4-3 shows the pendulum torque to angle transfer function (for pitch) using the parameters of a LIGO core optic. For external torques applied to the mirror above its resonant frequency, the mirror acts like a free mass, one that is not held in place by suspension wires nor subject to damping. For torques applied to the mirror below its resonant frequency, the mirror's angle is determined by the inverse of the torsional constant.

#### 4.4 Overview of Interferometer Alignment

There are 8 mirrors whose pitch and yaw angles must be sensed and controlled. The sensing is accomplished by 8 sensors, which fall into three groups:

- camera image (BS)
- quadrant photodiodes (QPDX, QPDY)
- wavefront sensors (WFS1, WFS2, WFS3, WFS4)

[Figure 10-3 shows the locations of these sensors.](#) The alignment of these mirrors using these sensors can be simplified by considering the interferometer alignment as happening in two basic units: the input beam and the power recycled Fabry-Perot Michelson. The alignment of the latter is nearly self-contained and can in fact be compacted down to a representative single mirror. The remaining jobs are to align the input beam and this “single mirror” to one another and to keep the y-arm perpendicular to the x-arm.

The self-contained alignment of the power recycled Fabry-Perot Michelson is realized through the set of wavefront sensors (WFS<sup>1</sup> ), whose principle of operation is described in Section 4.5. The pitch and yaw motions of the five mirrors in this unit, ETMX, ETMY, ITMX, ITMY, and the PRM, are sensed by the pitch and yaw of five WFS signals, WFS1Q, WFS2I, WFS2Q, WFS3I, and WFS4I, where I and Q denote in-phase and quadrature demodulation, respectively. These WFS look at light at the AS port, at the reflected port, and in the power recycling cavity. Their control signals are used to control the relative motions of these five mirrors up to a couple Hz.

The MMT-directed input beam and the interferometer “mirror” need to be aligned so that the input beam is perfectly reflected upon itself. The input beam follows the interferometer over minute time scales; at higher frequencies the interferometer follows the input beam. The low frequency matching of the input beam pointing to the interferometer “mirror” is realized through the pitch and yaw signals of QPDX, a QPD which monitors the position of the light transmitted through the x-arm, and the pitch and yaw signals of a camera that monitors the beam location on the beam splitter. These two alignment sensors adjust the pointing of MMT1 and MMT3 on about minute time scales. An example of the BS camera image is shown in Fig. 4-4. The higher

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<sup>1</sup> Pronounced “woofs”.

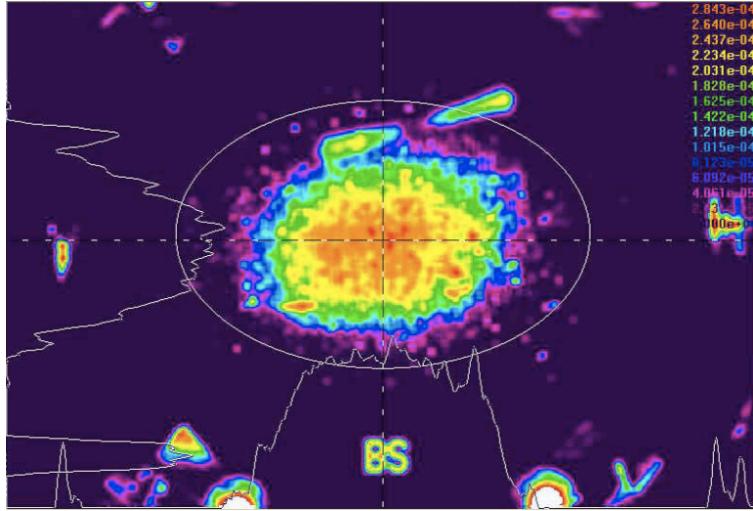


Figure 4-4. Image of beam on beam splitter as used in the beam centering servo. The beam appears stretched because the camera's viewing angle is at  $45^\circ$  with respect to the mirror surface. The color scale is arbitrary, but orange is strong, violet is weak.

frequency matching of the input beam pointing to the interferometer is achieved by the reflected port Fabry-Perot Michelson wavefront sensors, up to a couple Hz.

The one additional step needed for full interferometer alignment is to maintain the relative alignment of the y-arm to the x-arm as the x-arm and input beam together move around. This is accomplished through the pitch and yaw signals of QPDY, the QPD that monitors the light transmitted through the y-arm, which sense how the beam splitter should be pointed.<sup>2</sup>

All mirror angles are of course interdependent and they must track each other. However, a rough hierarchy of who follows who can be established since ultimately the interferometer is bolted to the ground and necessarily maintains some DC orientation. This orientation comes from QPDX and QPDY, which are physically attached to piers standing on the ground and force the beams transmitted through the ETMs to stay put at a certain location on their sensors. In all, the input beam must make it to those two exact places and the other mirrors are left to line themselves up accordingly. A diagram of this alignment scheme is in Fig. 4-5.

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<sup>2</sup> QPDX also sends a signal to the BS to compensate for whatever it has MMT3 do.

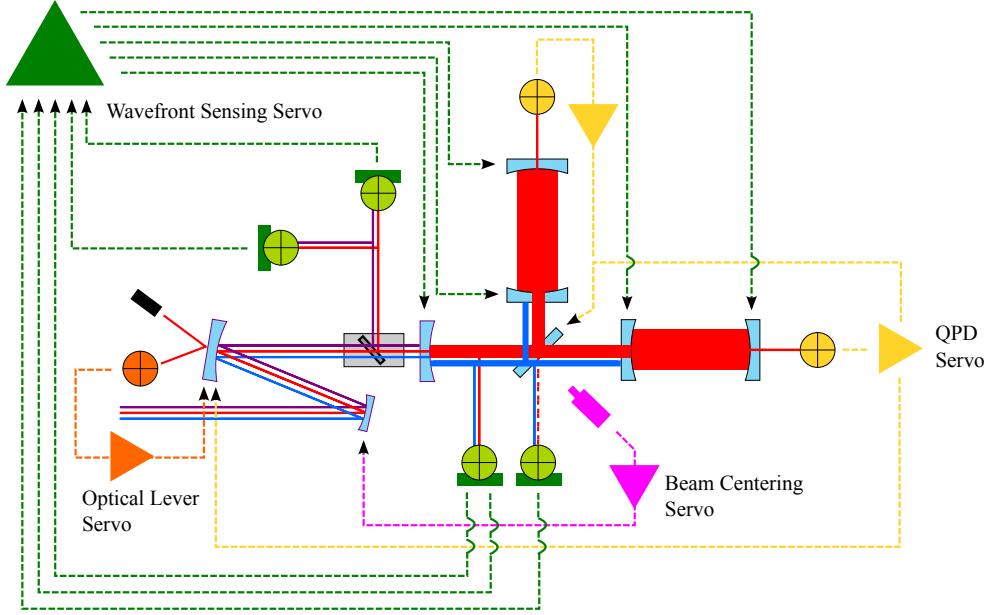


Figure 4-5. Schematic of the alignment sensing and control system, showing the placement of sensors and which mirrors they control. The QPD servo and Beam Centering Servo (BCS) together direct the input beam to follow the FPM unit on minute time scales. The QPD servo additionally keeps the BS properly directing light into the y-arm. The wavefront sensing servo maintains the alignment of the FPM mirrors with respect to each other up to several Hz. Each of the seven large optics has its own velocity damping optical lever servo. Replace this with two drawings, one showing WFS and one showing other sensors. Label and make less cluttered.

This alignment process involving the WFS, QPDs, and BS camera relies on the entire interferometer already being locked. It manages the continuous fine-tuning of mirror angles so that maximal power buildup in the interferometer is maintained, and so that the interferometer does not wander from its linear operating point—define!. How to achieve the initial alignment of all of the mirrors is an interesting process in itself and is documented in Appendix 10.6.

#### 4.5 The Wavefront Sensing Scheme

Wavefront sensors for angular sensing are the single photodiode equivalent of length sensing. Wavefront sensors are quadrant photodiodes equipped with RF electronics. They rely on the Pound-Drever-Hall locking scheme to produce error signals. [overview of basic wavefront sensing, references for details](#)

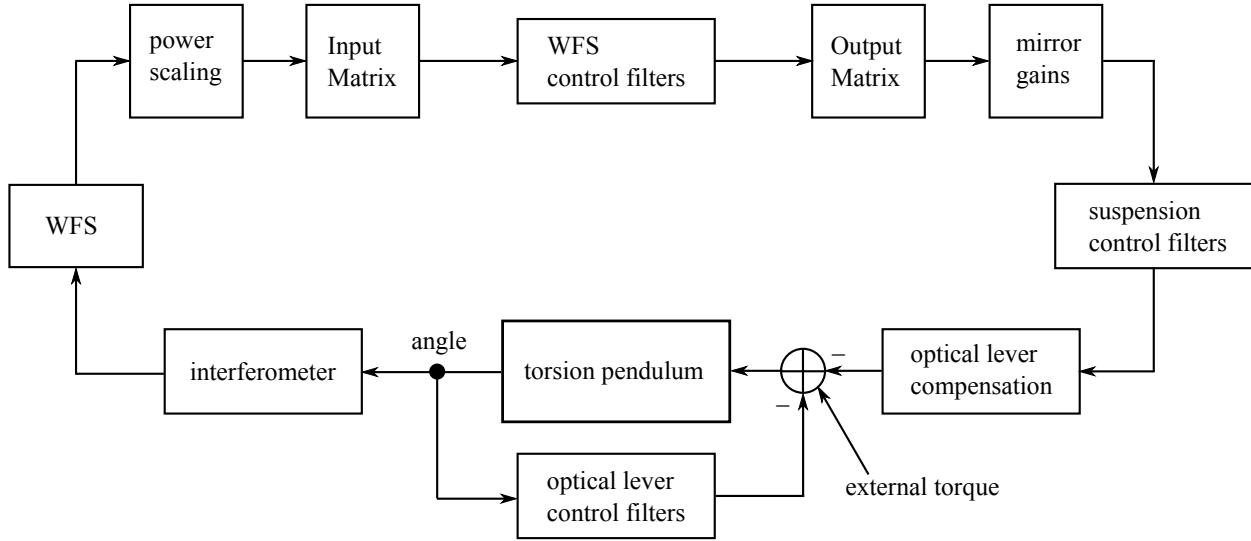


Figure 4-6. ASC control servo. [Highlight analog versus digital.](#)

#### 4.6 The Angular Control Servo

When the interferometer is locked, the optical levers and the wavefront sensors provide simultaneous feedback to the mirror angles. The optical levers provide local damping, and the WFS maintain both the alignment of the power-recycled Michelson with the input beam and the internal alignment of the power-recycled Michelson. The study and characterization of the elements of this angular control system when the laser power is increased is the topic of the remainder of this chapter and the next. Creating a clear picture of the servo without the inclusion of radiation pressure is warranted.

Fig. 4-6 is a block diagram of the major components to the angular control servo. The torsion-like pendula of the interferometer are subject to external torque which is converted to mirror angle. The interferometer, in turn, turns the mirror angles into TEM10/01 modes at its various ports, and these modes are converted into error signals by the wavefront sensors. The voltages produced by the wavefront sensors are digitized and manipulated by the front-end computers to create control signals that are then [made analog](#) for actuation on the mirrors. The result of this process is a suppression of the error signal seen by the WFS and therefore a suppression of the physical mirror motions.

In Initial LIGO, the wavefront sensor signals were combined via the Input Matrix to form error signals for the differential and common ETM and ITM motions ([explain more](#)). WFS control filters were designed for this basis and then those control signals were divvied out to appropriate mirrors via the Output Matrix.

#### 4.6.1 Optical lever compensation

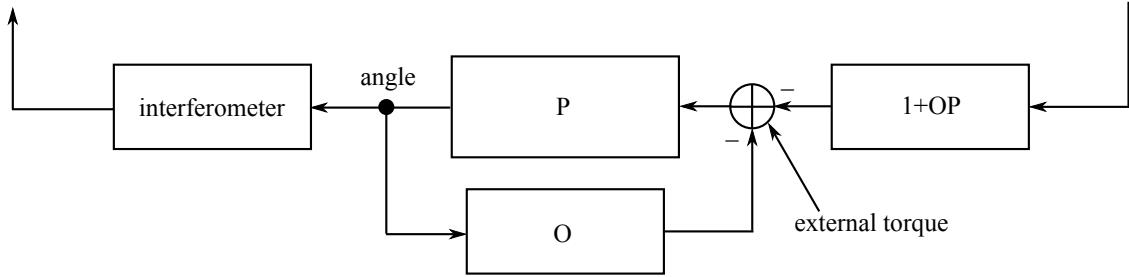
One aspect of the control servo that I will explain in detail here is the optical lever compensation. Each of the large optics has its own optical lever servo that provides velocity damping. Since both the WFS and the optical levers control the mirror motion when the interferometer is locked, we must consider the interaction of the two servos. Whether one views the interaction as the WFS controlling the optical-lever-controlled mirrors, or as the optical levers controlling the WFS-controlled-mirrors is arbitrary. For the purpose of explanation here, I use the former viewpoint.

Figure [4-7](#) zooms in on the portion of the Fig. [4-6](#) control loop picture that shows the optical lever controlling the pendulum. The torque to angle transfer function of the pendulum is our plant,  $P$ , the optical lever control is  $O$ , and the optical lever compensation is shown as  $1 + OP$ . A result of basic control theory is that the optical lever controlled pendulum loop can be represented by its closed loop transfer function:

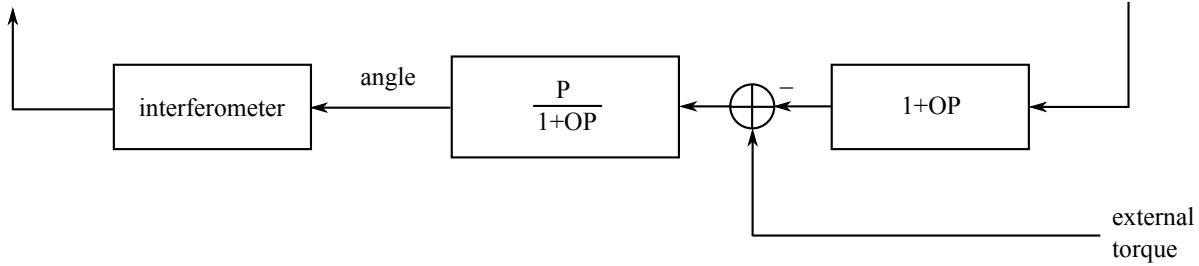
$$\text{TF}_{\text{closed}} = \frac{P}{1 + OP} \quad (4.6.1)$$

as shown in Fig. [4-7](#) B.

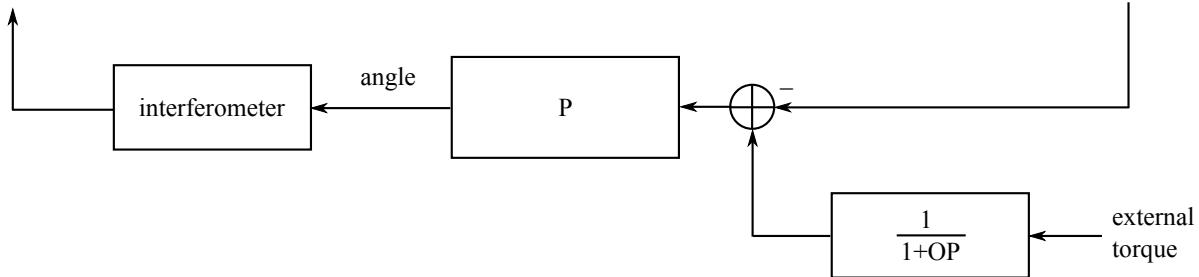
One will notice that it is not a coincidence that the optical lever compensation has the same form as the denominator of the closed loop transfer function. Together, they cancel each other out, and all that remains as the plant is the simple pendulum. Including the optical lever compensation in the ASC loop is not necessary, but it is a useful technique for simplifying the design process of the WFS control filters. One need only consider how to control the simple pendulum torque to angle transfer function, rather than the optical-lever controlled pendulum.



A Zoom of the bottom part of Fig. 4-6.  $P$  is the pendulum and  $O$  is the optical lever control filters.



B Replacement of the optical lever controlled plant with the closed loop gain representation.



C Optical lever compensation removes the optical levers from the picture of the pendulum. External torque is still suppressed by the optical lever closed loop gain.

Figure 4-7. Optical lever compensation scheme. Subfigures A, B, and C are equivalent.

#### 4.7 Angular Control Limitations

The limits for how well we can control the angular motion of the interferometer are governed by how well we are able to sense the angular motion. Several of the wavefront sensors' signals are dark-noise-limited above 20-25 Hz, as seen in Fig. 4-8. Moreover, depending on the power level, WFS1Q may instead be limited by shot noise (see Eq. ??). Any control signal derived from frequencies in the sensing noise limited regime will impress the sensor noise on the mirrors. The impression of sensor noise cannot be avoided entirely in the presence of

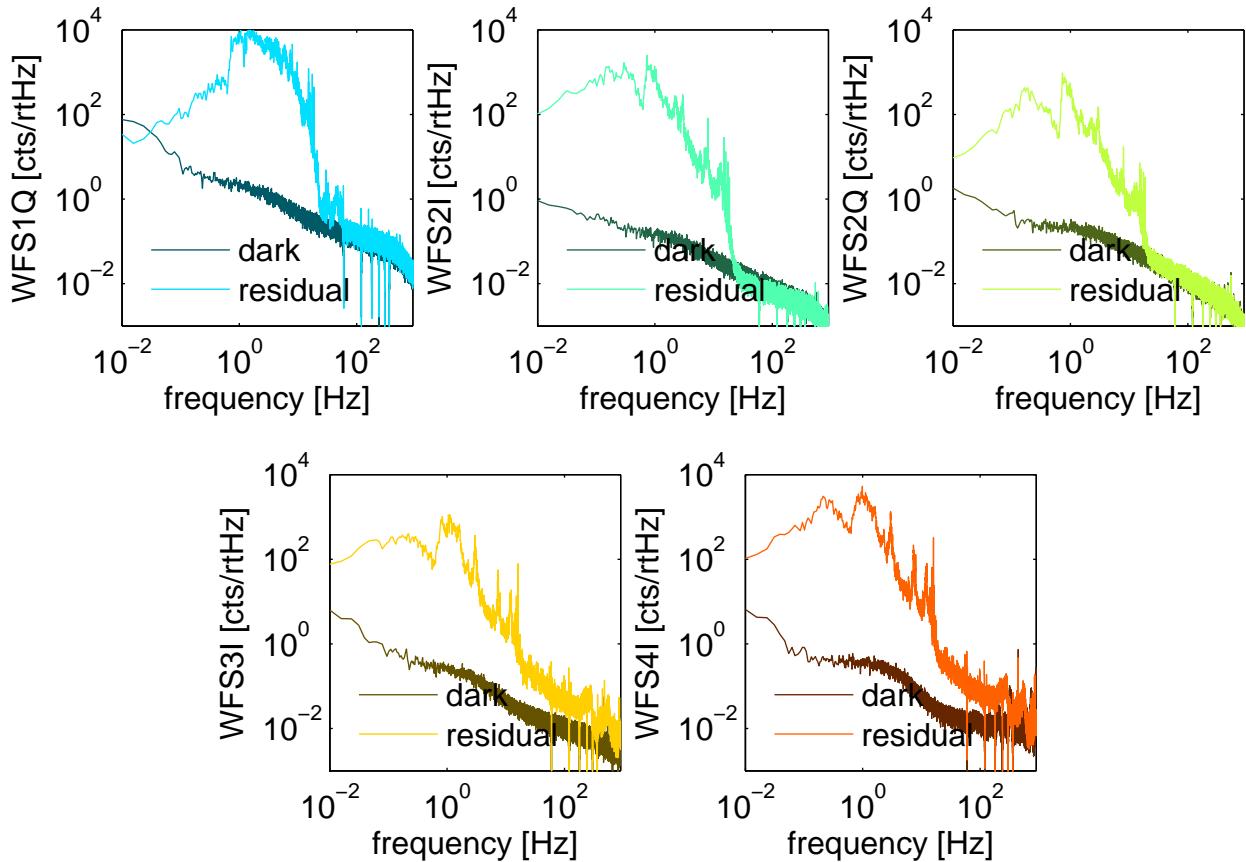


Figure 4-8. WFS dark noise compared to typical error signal. [Include shot noise, too, especially for WFS1.](#) The excess signal above the dark noise in WFS3I and WFS4I above 20 Hz is likely acoustic noise, although this hypothesis has not been verified. WFS1 and WFS2 are on a floating table in a sound proof chamber, while WFS3 and WFS4 are on a non-seismically isolated table without a sound proof enclosure.

feedback, but can be mitigated by including amongst the control filters a steep cut-off beginning at frequencies where sensor noise dominates.

Besides the sensing noise, there are also sometimes real signals that result in more harm than good when used as feedback. The HAM seismic isolation tables used by the Input Optics (the core optics are suspended from BSC tables) have stack modes at 0.8 to 3 Hz that ring up the MMTs. At low frequencies, around 1 Hz, some of the WFS signals are dominated by these angular fluctuations of the input beam. The resulting attempt of the mirrors to follow the input beam jitter leads to a magnification of the motion because of the drastically different length

scales. Large power fluctuations in both arms and the power recycling cavity ensue, leading to departure from the linear error signal regime and often lock loss.

Other limitations to the reduction of mirror motion result from the nature of control loops. The cut-off filter, for example, reduces the phase margin of the open loop gain, necessarily pushing down the unity gain frequency (UGF) and therefore the magnitude of suppression at all frequencies below the UGF. A less aggressive cut-off filter, while improving the servo's stability and allowing for higher overall gains, leads to more impression of sensing noise on the optics. Also, if the phase margin of the loop is low, mirror motion will be amplified through gain peaking.

## CHAPTER 5

### THE EFFECT OF HIGH LASER POWER ON INTERFEROMETER ALIGNMENT

The torque induced by radiation pressure, as introduced in Sec. 4.2.4, couples the angular motion of the suspended mirrors, complicating the plant for which controls must be designed. The derivation of the angular response of the mirrors to external torque in the presence of radiation pressure is presented in several publications, but I provide my own derivation here for completeness. This effect is, after all, the foundation for this work’s investigation of high power effects in the angular sensing and control.

**this needs re-writing** Namely, radiation pressure torque has the effect of breaking the symmetry of the equations of motion of each of the mirrors. Since Enhanced LIGO embarks on the path of increasing the laser power, examining the effect of radiation pressure torque in detail is warranted. Here, we derive a set of eigenfunctions that diagonalize the linear cavity’s response to radiation pressure and describe the mirrors’ equations of motion in this new eigenbasis. The torque to angle transfer functions of the new eigenmodes are modified such that one mode is statically unstable at Enhanced LIGO powers.

#### 5.1 The Radiation Pressure Angular Spring

The geometric axis of a cavity formed by two spherical mirrors is dictated by the line joining the two centers of curvature. Only if the mirrors are pointed directly at one another will the cavity geometric axis pass through the centers of the mirrors. Should a laser beam resonate in the cavity, it will do so along this geometric axis. Thus, if the mirrors are tilted away from one another, the beam spot on each mirror will not be centered. The relationship between the positions of the beams on the mirrors relative to center,  $x_i$ , and the angles of the mirrors,  $\theta_i$ , is given by:

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \frac{L}{1 - g_1 g_2} \begin{bmatrix} g_2 & 1 \\ 1 & g_1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}. \quad (5.1.1)$$

The  $g$ -factor is defined as  $g_i = 1 - R_i/L$  where  $R_i$  is the radius of curvature of each of the mirrors, respectively, and  $L$  is the length of the cavity. It is 0.73 (0.71) for the LLO (LHO) ITM and 0.54 (0.45) for the LLO (LHO) ETM.

We saw in the previous chapter that the radiation pressure torque on a mirror depends on the position of the beam on the mirror,  $\tau_{rp} = 2Px/c$  (Eq. 4.2.3). Based on Eq. 5.1.1 the radiation pressure torque on a mirror that is part of a Fabry-Pérot cavity is therefore dependent on the angle of both the mirror of interest and the second mirror forming the cavity:

$$\begin{bmatrix} \tau_{rp,1} \\ \tau_{rp,2} \end{bmatrix} = \frac{2PL}{c(1-g_1g_2)} \begin{bmatrix} g_2 & 1 \\ 1 & g_1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}. \quad (5.1.2)$$

This is more succinctly expressed as

$$\vec{\tau}_{rp} = -\mathbf{K}_{rp}\vec{\theta}, \quad (5.1.3)$$

where  $\mathbf{K}_{rp}$  is the *torsional stiffness matrix*. Equation 5.1.3 is the expression that describes the radiation pressure angular spring.

### 5.1.1 Diagonalizing the Modified Equations of Motion

The radiation pressure spring modifies the pendulum angular equation of motion and therefore the torque to angle transfer function through the addition of an angle-dependent torque term. Re-writing Eq. 4.3.2 in matrix form and with the radiation pressure spring term, the two equations that describe the motion of two mirrors forming a Fabry-Pérot cavity is:

$$\mathbf{I}\ddot{\vec{\theta}} + \gamma\dot{\vec{\theta}} + \kappa_p\vec{\theta} - \frac{2PL}{c(1-g_1g_2)} \begin{bmatrix} g_2 & 1 \\ 1 & g_1 \end{bmatrix} \vec{\theta} = \vec{\tau}_{ext}. \quad (5.1.4)$$

$\mathbf{I}$ ,  $\gamma$ , and  $\kappa_p$  are  $2 \times 2$  diagonal matrices and  $\vec{\theta}$  and  $\vec{\tau}_{ext}$  are  $2 \times 1$  vectors as in the previous section. Due to the non-diagonal matrix in Eq. 5.1.4, the motions of each of the mirrors forming the cavity are tied to one another. The natural way to work with such a system is to rotate the coupled equations into a new basis. The resulting de-coupled equations of motion will described specific combinations of mirror tilts instead of the tilt of an individual mirror. Vectors in the rotated basis are written with primes.

In order to decouple the two equations of Eq. 5.1.4, we need to diagonalize  $\mathbf{K}_{rp}$ . The subscripts  $a$  and  $b$  are used to denote the elements of the diagonalized basis, to contrast the 1 and

2 which denote the mirror basis. Ignoring the constants of matrix  $\mathbf{K}_{rp}$ , its eigenvalues are

$$\lambda_a = \frac{g_1 + g_2 + \sqrt{(g_1 - g_2)^2 + 4}}{2} \quad (5.1.5)$$

$$\lambda_b = \frac{g_1 + g_2 - \sqrt{(g_1 - g_2)^2 + 4}}{2} \quad (5.1.6)$$

and its eigenvectors are

$$\vec{v}_a = \begin{bmatrix} 1 \\ \frac{g_1 - g_2 + \sqrt{(g_1 - g_2)^2 + 4}}{2} \end{bmatrix} \quad (5.1.7)$$

$$\vec{v}_b = \begin{bmatrix} \frac{-g_1 + g_2 - \sqrt{(g_1 - g_2)^2 + 4}}{2} \\ 1 \end{bmatrix}. \quad (5.1.8)$$

Therefore, the matrix

$$\mathbf{S} = \begin{bmatrix} \vec{v}_a & \vec{v}_b \end{bmatrix} = \begin{bmatrix} 1 & \frac{-g_1 + g_2 - \sqrt{(g_1 - g_2)^2 + 4}}{2} \\ \frac{g_1 - g_2 + \sqrt{(g_1 - g_2)^2 + 4}}{2} & 1 \end{bmatrix} \quad (5.1.9)$$

diagonalizes  $\mathbf{K}_{rp}$  such that

$$\mathbf{S}^{-1} \mathbf{K}_{rp} \mathbf{S} = \mathbf{D} = \begin{bmatrix} \lambda_a & 0 \\ 0 & \lambda_b \end{bmatrix} = \begin{bmatrix} \frac{g_1 + g_2 + \sqrt{(g_1 - g_2)^2 + 4}}{2} & 0 \\ 0 & \frac{g_1 + g_2 - \sqrt{(g_1 - g_2)^2 + 4}}{2} \end{bmatrix}. \quad (5.1.10)$$

The matrix of eigenvectors,  $\mathbf{S}$ , is the basis transformation matrix. It serves to define the torque and angle vectors in the new basis. For example,

$$\vec{\theta}' = \begin{bmatrix} \theta_a \\ \theta_b \end{bmatrix} = \mathbf{S}^{-1} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} = \mathbf{S}^{-1} \vec{\theta}. \quad (5.1.11)$$

Rearranging Eq. 5.1.10 to the form  $\mathbf{K}_{rp} = \mathbf{SDS}^{-1}$  and substituting it into Eq. 5.1.4, we have:

$$\mathbf{I} \ddot{\vec{\theta}} + \gamma \dot{\vec{\theta}} + \kappa_p \vec{\theta} - \frac{2PL}{c(1 - g_1 g_2)} \mathbf{SDS}^{-1} \vec{\theta} = \vec{\tau}_{ext} \quad (5.1.12)$$

Table 5-1. Geometric parameters of the LIGO arm cavity eigenmodes.  $x_i$  are the beam locations on the mirrors relative to center,  $a$  is the cavity axis displacement at the waist, and  $\alpha$  is the cavity axis angle with respect to a line joining the centers of the mirrors.

Differences between LLO and LHO arise from the mirrors at each site having different radii of curvature. Quantities are expressed as a function of the amount of tilt in a particular mode.

cavity parameter	unit	LLO $\vec{v}_a$ mode	LLO $\vec{v}_b$ mode	LHO $\vec{v}_a$ mode	LHO $\vec{v}_b$ mode
$ x_1 $	mm/urad	9.88	2.44	8.20	2.51
$ x_2 $	mm/urad	10.84	2.22	9.35	2.20
$ a $	mm/urad	10.17	1.01	8.48	1.34
$ \alpha $	urad/urad	0.24	1.17	0.29	1.18

Multiplying on the left by  $\mathbf{S}^{-1}$ , taking advantage of the diagonal  $\mathbf{I}$ ,  $\gamma$ , and  $\kappa_p$  matrices, and using  $\mathbf{S}^{-1}$  to change the basis of each of the vectors, the de-coupled equations of motion are:

$$\mathbf{I}\ddot{\theta}' + \gamma\dot{\theta}' + \kappa_p\vec{\theta}' - \frac{2PL}{c(1-g_1g_2)} \begin{bmatrix} \lambda_a & 0 \\ 0 & \lambda_b \end{bmatrix} \vec{\theta}' = \vec{\tau}'_{ext}. \quad (5.1.13)$$

The radiation pressure torsion constant,  $\kappa_{rp}$ , is

$$\kappa_{rp} = -\frac{2PL}{c(1-g_1g_2)} \lambda \quad (5.1.14)$$

where  $\lambda = \lambda_a$  or  $\lambda_b$ , depending on the mode in question.

The angular motion of the Fabry-Pérot cavity is no longer described by the motions of its individual mirrors. Due to radiation pressure, the cavity is treated as a unit and the two orthogonal modes of angular motion are combinations of the two mirrors' angles. The eigenvectors  $\vec{v}_a$  and  $\vec{v}_b$  describe these two sets of orthogonal mirror tilts, and the eigenvalues  $\lambda_a$  and  $\lambda_b$  (along with their common constants) quantify the magnitude of the radiation pressure torsional spring constant for each of the modes. While the equations of motion had been identical for each of the individual mirrors, the decoupled equations in the presence of radiation pressure breaks that symmetry.

Table 5-1 outlines the characteristics of these two eigenmodes for the specific geometry of the LIGO arm cavities. The amount of beam displacement on each mirror is given as a function of the amount of tilt in one eigenmode or the other. Furthermore, the amount of cavity axis

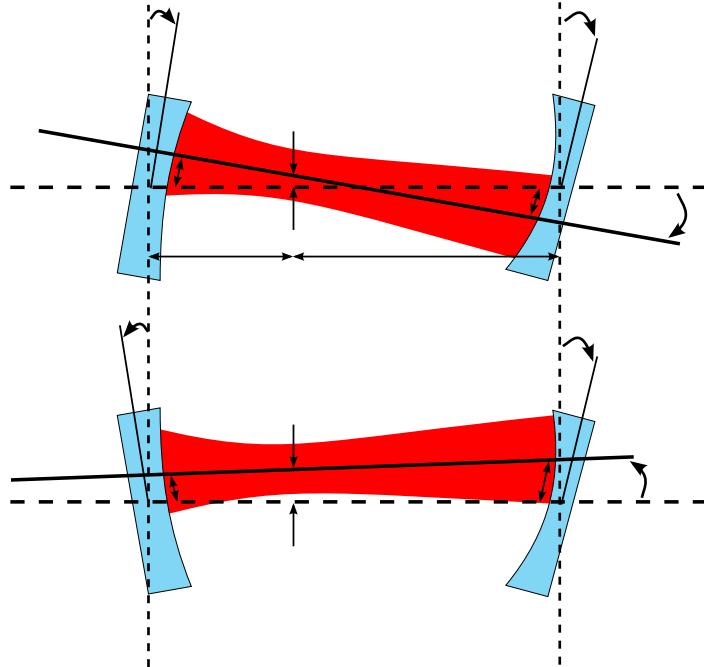


Figure 5-1. Illustration of the orthogonal modes of cavity tilt. The upper diagram shows tilts given by eigenvector  $\vec{v}_b$  and the lower diagram shows  $\vec{v}_a$ . [Labels](#).

displacement  $a$  and cavity axis tilt  $\alpha$  is also calculated for each eigenmode using the geometric relationship between a set of mirror tilts and their cavity axis as derived in Appendix 10.4. Figure 5-1 illustrates a cavity in each of the two eigenmodes when using the parameters from Table 5-1.

### 5.1.2 Soft and Hard Modes

The torque to angle transfer function of each of these eigenmodes has the same form as that of a single pendulum (Eq. 4.3.4), but the torsion constant is modified. More importantly, the spring constant is modified differently for each mode, yielding distinct behaviors of the two eigenmodes. In this section, we analyze these behaviors and accordingly introduce the names *soft* and *hard* to use in place of  $a$  and  $b$  for describing the two modes.

Just as in Sec. 4.3.1, we can take the Laplace transform of each of the equations in Eq. 5.1.13 to get the general form of the modal torque to angle transfer function:

$$H'(s) = \frac{\Theta'(s)}{\tau'_{ext}(s)} = \frac{1}{Is^2 + \gamma s + \kappa_p + \kappa_{rp}}. \quad (5.1.15)$$

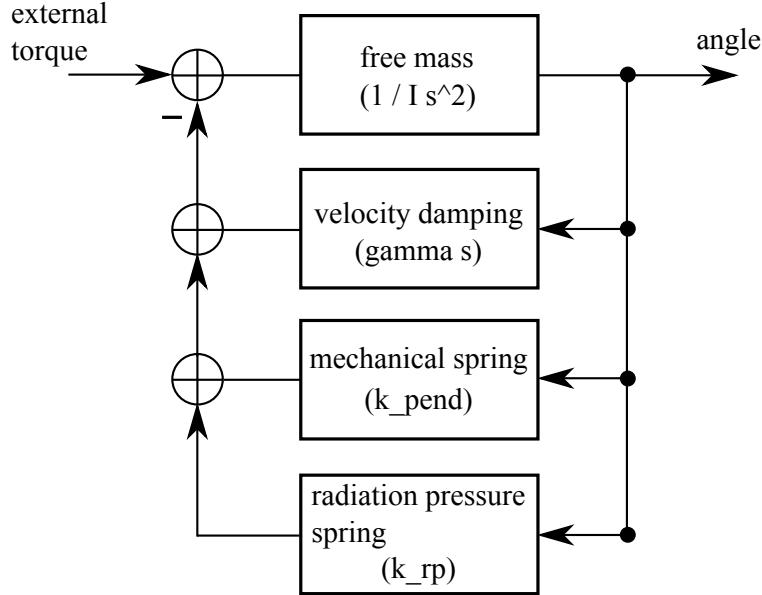


Figure 5-2. Demonstration of how radiation pressure modifies the torque to angle transfer function of a Fabry-Pérot cavity's eigenmodes.

Figure 5-2 shows the control theory view of the addition of the radiation pressure spring constant to the transfer function.

The magnitude and sign of the total torsional spring constant,  $\kappa_{tot} = \kappa_p + \kappa_{rp}$ , conveys critical information about the stability of the cavity and the nature of its response to external torque. Recalling the equation of an angular spring,  $\tau = -\kappa_{tot}\theta$ , a restoring torque is provided only if  $\kappa_{tot} > 0$ , which is equivalent to the condition for stability. If  $\kappa_{tot} < 0$ , the spring is an anti-spring, resulting in an unstable, run-away situation. Furthermore, while  $\kappa_{tot}$  is positive, its magnitude directly relates to the stiffness of the spring.

The stability criteria for the coupled cavity eigenmodes depend on the relationship between  $\kappa_p$  and  $\kappa_{rp}$ :

$$\text{stable: } k_{tot} > 0 \implies \frac{2PL}{c(1-g_1g_2)}\lambda < \kappa_p \quad (5.1.16)$$

$$\text{unstable: } k_{tot} < 0 \implies \frac{2PL}{c(1-g_1g_2)}\lambda > \kappa_p. \quad (5.1.17)$$

The pendulum spring constant,  $\kappa_p$ , is always positive, so we can conclude with certainty that the cavity eigenmode is stable as long as the quantity on the left-hand side of Eq. 5.1.17 is negative.

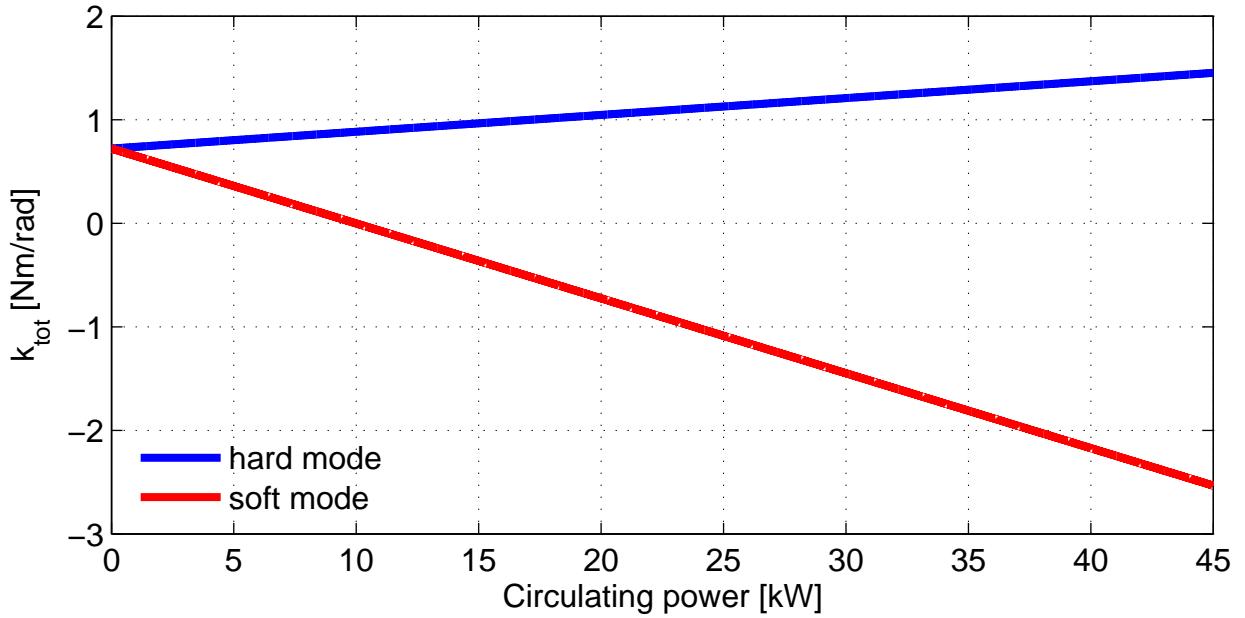


Figure 5-3. Torsional spring constants (pitch) of an optically coupled cavity for LLO parameters. The soft mode is unstable when the spring constant is negative. [Include LHO](#).

However, if this quantity is positive, then its magnitude compared to  $\kappa_p$  determines stability.

Since  $P$ ,  $L$ , and  $c$  are all positive numbers and the  $g$ -factor is restricted to  $0 < g_1 g_2 < 1$ <sup>1</sup>, the sign of the left-hand side is determined solely by that of  $\lambda$ . From the  $g$ -parameter restriction, it can be shown that  $\lambda_a$  is always positive and that  $\lambda_b$  is always negative. Therefore, the mode whose mirror angles are described by  $\vec{v}_a$  is either stable or unstable, and the mode described by  $\vec{v}_b$  will always be stable.

The precise situation for the potentially unstable mode depends on the one non-constant variable, the circulating power  $P$ . There is a critical power at which  $\kappa_{rp} = -\kappa_p$ , and at any greater power, instability ensues. In general, as power increases, the total spring constant for the potentially unstable mode decreases, creating a softer spring, and the total spring constant for the unconditionally stable mode increases, creating a stiffer spring. Thus arise the terms *soft* and *hard* to describe the two eigenmodes that have been referred to by  $\vec{v}_a$  and  $\vec{v}_b$ , respectively.

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<sup>1</sup> This is the necessary condition for a two mirror resonator to form a stable periodic focusing system. [37, p. 747]

Table 5-2. Torsional spring constants (pitch) for the soft and hard modes of a typical Initial LIGO power and the highest of Enhanced LIGO powers. The soft mode in Enhanced LIGO is unstable. The  $\kappa_p$  values assume a resonant frequency of 0.6 Hz. [maybe include aLIGO on this table as well.](#)

	$P_{circ}$	$\kappa_p$	$\kappa_{tot}$ , soft mode	$\kappa_{tot}$ , hard mode
Initial LIGO	9 kW	0.721 Nm/rad	0.0734 Nm/rad	0.867 Nm/rad
Enhanced LIGO	40 kW	0.721 Nm/rad	-2.18 Nm/rad	1.38 Nm/rad

Figure 5-3 shows the dependence of  $\kappa_{tot}$  on circulating power for the soft and hard modes of a LIGO arm cavity. Without power in the cavity, the modes are identical and their spring constants are simply that of the individual pendula. The symmetry-breaking effect of radiation pressure comes into play as soon as light resonates in the cavity: the hard mode's spring constant increases and the soft mode's spring constant decreases. The critical power at which the soft mode becomes unstable is 10 kW, which corresponds to approximately 6 W input power (for Enhanced LIGO efficiencies) to the interferometer. Above the critical power, radiation pressure creates an optical anti-spring.

Table 5-2 highlights the values of the spring constants for the typical power that was used in Initial LIGO (9 kW) and for the highest of powers achieved in Enhanced LIGO (40 kW). The corresponding transfer functions for these spring constants is found in Fig. 5-4. The resonant frequency,  $\omega_0 = \sqrt{\kappa_{tot}/I}$ , increases with power for the hard modes and decreases for the soft modes. Once  $\kappa_{tot}$  becomes negative, as is the case for the Enhanced LIGO soft mode, there is no real resonant frequency.

One final comment about the analysis of the modified transfer function (Eq. 5.1.15) is that the two poles,

$$s = s_{\pm} = \frac{-\gamma \pm \sqrt{\gamma^2 - 4I\kappa_{tot}}}{2I}, \quad (5.1.18)$$

provide an additional ([find better word](#)) way to view the stability of the system. As long as the poles are negative, the impulse response will decay or be sinusoidal. However, if a pole is positive, the system's motion will experience exponential growth. The constraints for  $s_{\pm}$  to be in a particular half of the s-plane are easily derived from Eq. 5.1.18. Note that  $s_-$  will always be in the left half of the plane and that  $s_+$  is the pole that has the potential of falling in the right half

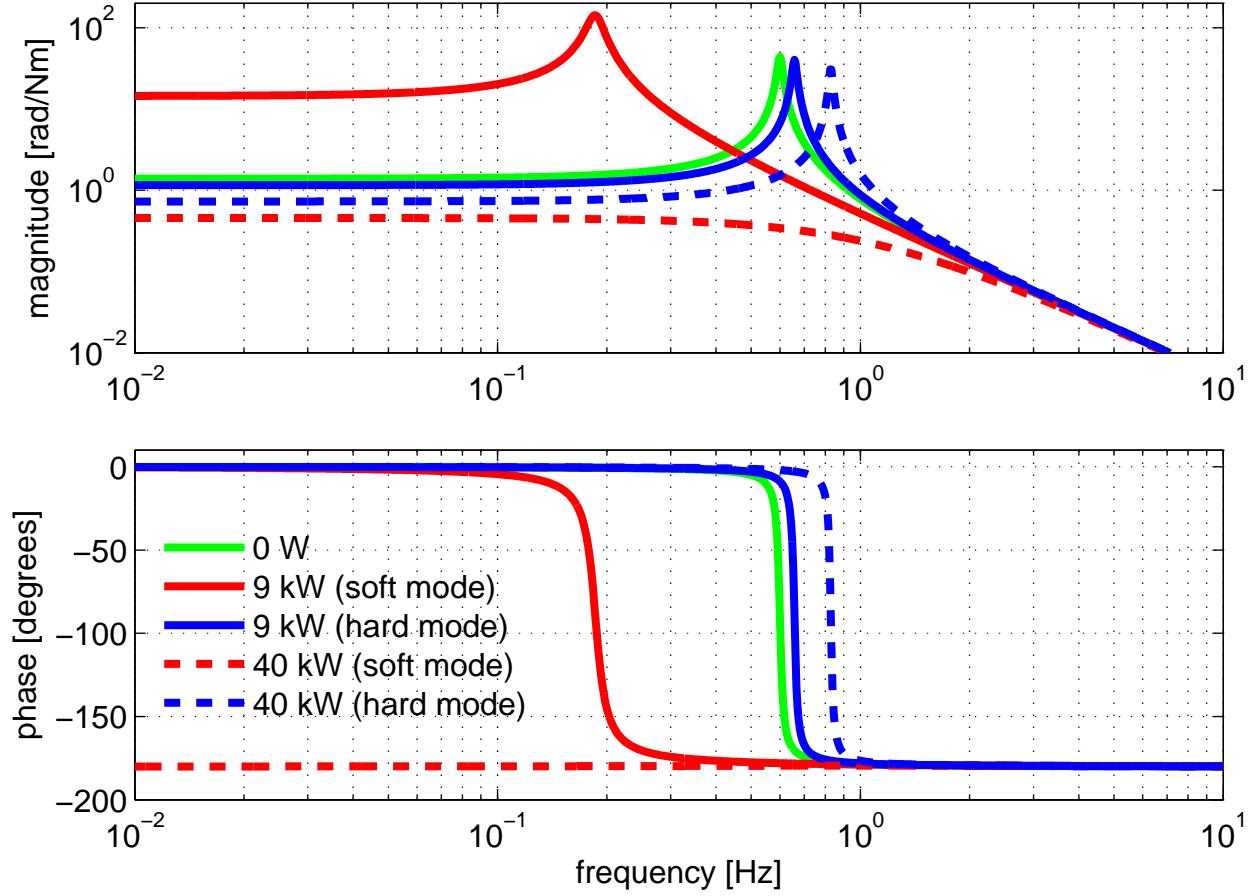


Figure 5-4. Single cavity opto-mechanical transfer function for pitch. The resonant frequency increases with power for the hard mode, but decreases for the soft mode, eventually becoming imaginary.  $P_{circ} = 9$  kW (5.25 W input) was a typical operating power for Initial LIGO and  $P_{circ} = 40$  kW (23.5 W input) is the highest of powers reached for Enhanced LIGO.

Table 5-3. Conditions on total torsional constant  $\kappa_{tot}$  for determining system stability.

$\kappa_{tot}$ condition	pole $s_+$	impulse response
$\kappa_{tot} < 0$	real positive	statically unstable
$\kappa_{tot} = 0$	zero	
$0 < \kappa_{tot} < \gamma^2/4I$	real negative	stable decay
$\kappa_{tot} > \gamma^2/4I$	real negative, and imaginary	stable, oscillatory

of the plane. Table 5-3 show how the s-plane locations for  $s_+$  depend on  $\kappa_{tot}$ . The sign of  $\kappa_{tot}$  determines stability, as expected, and we see that the nature of the stable response depends on the damping coefficient. Figure 5-5 plots the pole locations for a range of  $\kappa_{tot}$  experienced while powering up Enhanced LIGO.

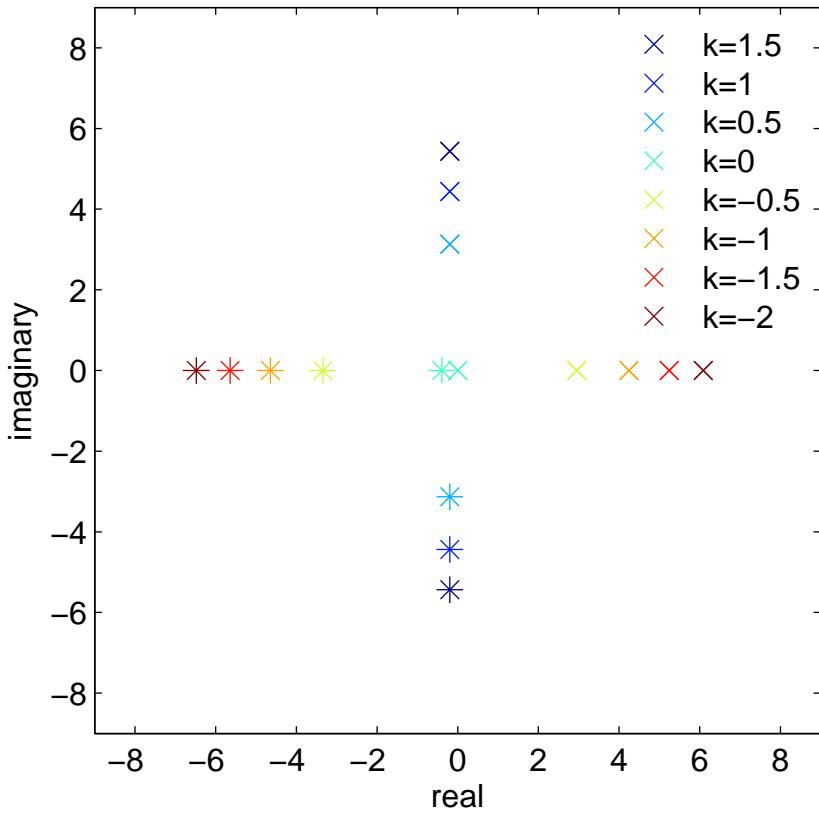


Figure 5-5. Poles of the torque to pitch transfer function as a function of torsional constant,  $\kappa_{tot}$ . Crosses show  $s_+$  and asterisks show  $s_-$ . Poles in the right half of the s-plane indicate the system is unstable.

Table 5-4. Opto-mechanical parameters for the LIGO Livingston and LIGO Hanford cavities. Differences result because the mirrors at each site have different radii of curvature.  
[Reference in text. put in appendix?](#)

parameter	label	LLO	LHO
ITM g-factor	$g_1$	0.73	0.71
ETM g-factor	$g_2$	0.54	0.45
arm length	$L$	3995 m	3995 m
test mass moment of inertia	$I$	0.0507 kg m <sup>2</sup>	0.0507 kg m <sup>2</sup>
pendulum torsion constant	$\kappa_p$	0.72 Nm/rad (pitch) 0.50 Nm/rad (yaw)	0.72 Nm/rad (pitch) 0.50 Nm/rad (yaw)
soft mode eigenvector	$\vec{v}_1$	(1, 1.10)	(1, 1.14)
hard mode eigenvector	$\vec{v}_2$	(-1.10, 1)	(-1.14, 1)
power when soft mode is unstable	$P_{crit}$	10.0 kW (pitch) 7.0 kW (yaw)	11.6 kW (pitch) 8.0 kW (yaw)

## 5.2 Implications

The Enhanced LIGO goal of increasing the input power to 30 W from the Initial LIGO 7 W makes radiation pressure torques cross into the realm of significance. In particular, the soft opto-mechanical mode which just approached instability for Initial LIGO powers actually becomes unstable for Enhanced LIGO powers. The transfer functions for which controls must be designed are no longer those of a pendulum with resonance at 0.6 Hz (pitch) or 0.5 Hz (yaw), but those of the soft and hard eigenmodes, whose resonances change with power. The plant of Fig. 4-6 is now treated as the cavity's radiation pressure-modified torque to angle transfer function, not a simple stand-alone pendulum transfer function.

An elegant implication of the purely geometric description of the cavity axis is that the radiation pressure eigenmodes are orthogonal independently of power.

[put this elsewhere?](#) One complication of having a radiation pressure modified and therefore power dependent plant,  $P_{rp}$ , is that the optical lever compensation (described in Sec. 4.6.1) is no longer valid. The compensation of  $1 + OP$  is hard-coded in the digital control system, where the model for  $P$  is that of a simple pendulum. The only way to achieve perfect compensation would be to load a new model of  $P$  into the compensation filter bank for each new power and for each optic. Doing this in Enhanced LIGO was not practical, so only at low powers does the optical lever compensation actually cancel out the effect of the optical-lever-controlled radiation pressure-modified plant,  $P_{rp}/1 + OP_{rp}$ , and leave simply  $P_{rp}$  for the WFS to control. It turns out that as power increases, the imperfect compensation actually make the loops more stable (Ref. Barsotti).

The sensors in Initial LIGO were not tuned to specifically look for the combined mirror motions that create the soft and hard modes. The only way to provide adequate control for both modes would be to increase the gain of all of the angular control loops. Since some of the sensors are [less good](#) than others, this would result in excessive impression of sensor noise on DARM. To minimize impact on strain sensitivity while reducing the angular motion of the interferometer's mirrors to the levels necessary for stable operation, we need to pick out the combination of

sensors that together sense specifically the hard mode or the soft mode, and then design controls that specifically address the characteristics of just one mode. This is the foundation of the ASC work for Enhanced LIGO: switching the WFS control to the radiation pressure eigenmode basis, and increasing the gains of only those loops that require it. [I need to make sure this is accurate.](#)

## CHAPTER 6

### ANGULAR SENSING AND CONTROL CHARACTERIZATION AND PERFORMANCE IN THE RADIATION PRESSURE EIGENBASIS

This intro is a work in progress! Set up reader to hear about measurements of the Enhanced LIGO system. The basis for angular control in Initial LIGO was the sensor basis. The wavefront sensors are located such that they sense common/differential ETM/ITM angular motion and the filters were designed to feed back to those sets of motions. This does not, however, lend itself to easily handling radiation pressure torque. Since the WFS basis is not the radiation pressure eigenbasis of Section 5.1.1, each control servo handled combinations of the soft and hard modes. Due to radiation pressure, each mirror has two resonances, a more complicated plant than that offered by the eigenbasis which has a single resonance for each mode.

The meat of the Enhanced LIGO ASC upgrade was to switch the control servo from the sensor basis to the natural radiation pressure eigenmode basis, and to keep the contamination to DARM at a minimum.

Although the interferometer is very sensitive to ground motion, the range of seismic activity for which it can maintain full lock is reasonably large. The microseism (0.1-0.35 Hz) varies by factors of several seasonally (it's worse in the winter), and the 1-3 Hz motion varies by factors of several from day to night. Seismic motion the interferometer typically cannot handle includes events like earthquakes (0.03-0.1 Hz) and heavy activity on site (3-10 Hz). Motion at these frequencies are otherwise constant and at a level so as to not affect interferometer operation.

For completeness and for satisfaction for the trained eye, I include in Appendix 10.9 seismic spectra from the time of each measurement I present. For some people, this may seem excessive, but almost all of the mirror motion is in fact due to the ground, so the relevance is high ([fix wording](#)).

## 6.1 Calibrations

Since the data is collected digitally, the units are in digital counts. This must be converted into physical units in order to facilitate comparison to models and to make meaningful statements. The typical method of calibrating a digital channel is to inject a signal of known amplitude into the system and take the ratio with the amplitude of the digital measurement of the signal. Two ways of determining the physical amplitude of the injected signal are ([see if I can classify calibration methods](#))

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- 

I describe in this section the calibrations I made of some of the angular sensing channels, all the while demonstrating particular examples of these methods.

### 6.1.1 Beam Spot Motion

A quantity of interest is how much the beam moves on the ITMs and ETMs. It is this beam spot motion which, together with the mirror angular motion, creates a length signal that contributes noise to DARM. An elegant way of following the motion of the beam on the test masses is to track pickoffs of the light transmitted or reflected from the mirrors. We have such signals naturally available for the ETMs and ITMs from the QPDs which are otherwise used for ASC sensing. For example, QPDX and QPDY see the light transmitted through each of the ETMs and WFS2 sees the pickoff of light from the wedge of ITMX.

To calibrate the counts of the QPD and WFS2 pitch and yaw error signals,  
`L1:ASC-QPDY_{PIT,YAW}_IN1` and `L1:ASC-WFS2_DC{Pitch, Yaw}Mon`, I moved the beam

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<sup>1</sup> The convention for the naming of the WFS control signals is WFS1, WFS2A, WFS2B, WFS3, and WFS4, as seen in the channel names. This can be misleading because of the similarity to the sensor names (WFS1Q, WFS2I, WFS2Q, WFS3, and WFS4), potentially leading one to assume a one-to-one correspondence. For clarity in this dissertation, I refer to the WFS control signals by the degrees of freedom they represent: dSoft, cSoft, dHard, cHard, and RM.

a known distance on the test mass,  $\Delta x$ , and recorded the corresponding  $\Delta y$  of the QPD and WFS2 readback. The ratio  $\Delta x/\Delta y$  is the calibration from counts to meters. The details of the procedure are described below.

### 6.1.1.1 Moving the beam

Moving the beam on the mirrors in a controlled fashion is straightforward because of the ASC system. All that we need to do is introduce an offset to the setpoint of the beam centering aspect of the ASC servo. For the ETMs we put a DC offset in the L1:ASC-QPD{X,Y}-{PIT, YAW}-{OFFSET} channel and for the ITMs we changed the  $X$  and  $Y$  targets of the beam splitter beam centering servo.

### 6.1.1.2 Measuring how much the beam has moved

The more difficult task is measuring just how much the beam has moved. For this, we make use of the lever arm mechanism of angle to length coupling. ([This should be explained in the previous chapter, so maybe just reference it.](#)) The idea is that when the axis of rotation of a mirror coincides with the center of the beam, any tilt of the mirror about this axis does not affect the path length of the reflected beam. However, if there is a mismatch between rotation axis and beam location, then the light will pick up a longitudinal phase shift when the mirror is tilted. During a full interferometer lock, this is recorded by DARM.

The concept of the measurement is to move the axis of rotation of the mirror so that it passes through the center of the beam. We use the OSEMs to change the location of the axis of rotation, and we use DARM to determine when the axis is aligned with the beam center. For example, if we drive the top two osems more than the bottom two osems, we've created an axis of rotation that sits below the center of mass. The result of such tuning is an effective rebalance of the center of mass of the mirror so that it is aligned with the center of the beam. The procedure is:

1. Shake the mirror at some frequency  $f$  (we use 39.5 Hz) during a full lock
2. Demodulate DARM at  $f$  for several different sets of osem gains
3. Fit a quadratic to the demodulated data to pinpoint the osem gains that minimize the coupling to DARM

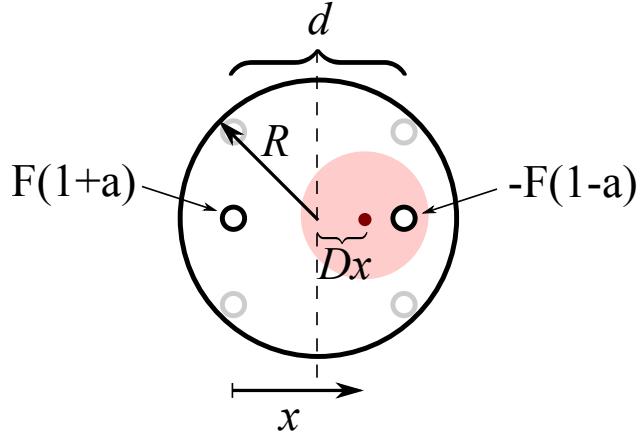


Figure 6-1. Geometry of osems and mirror as used for calculating the location of the axis of rotation when the torques are unequal. Need latex in inkscape!

Relating the osem gains to absolute beam position on the mirror requires only the geometry of the mirror and osem setup as sketched in Fig. 6-1. We estimate the osem locations as being on the edge of the mirror such that the length  $d$  of one side of the square that they form is given by  $d = \sqrt{2}R$ , where  $R = 12.5$  cm is the radius of the mirror. Then, collapsing the four osems into a representative two at the centers of two opposite sides of the square and assigning them gains of  $1 + \alpha$  and  $-(1 - \alpha)$  for a force  $F$ , we can evaluate where the pivot point  $x$  is located by setting the sum of the torques equal to zero:

$$F[1 + \alpha]x = F[1 - \alpha][d - x]. \quad (6.1.1)$$

Therefore, the beam location relative to center,  $\Delta x$ , is

$$\Delta x := \frac{d}{2} - x = \alpha \frac{d}{2}, \quad (6.1.2)$$

and for a change in a pitch or yaw coil gain, the change in beam position,  $\Delta x$ , is:

$$|\Delta x| = \frac{|\Delta \text{gain}|R}{\sqrt{2}}. \quad (6.1.3)$$

Table 6-1. Calibrations to be used with the QPDX, QPDY, and WFS2 DC pitch and yaw error signals for a measure of beam spot motion.

	ETMX	ETMY	ITMs
pitch	1.03e-5 m/ct	1.21e-5 m/ct	5.52e-2 m/ct
yaw	0.88e-5 m/ct	0.80e-5 m/ct	4.79e-2 m/ct

The final calibrations of these channels are shown in Table 6-1.<sup>2</sup>

### 6.1.2 Angular Mirror Motion

The optical levers provide a straightforward measure of individual mirror motion. The channels I calibrated were of the form L1:SUS-ETMX\_OPLEV\_{P,Y}ERROR, the optical lever error signals for each of the large optics. I made use of the dependence of power in a misaligned cavity to calibrate the ETM and ITM optical levers, and used a less precise, rudimentary method to calibrate the RM, BS, and MMT3 optical levers.

#### 6.1.2.1 ETM and ITM optical levers

I calibrated the arm cavity optical levers by tracking the power loss in the locked arm as one of its mirrors is tilted. The closed form expression for cavity power as a function of mirror tilt is derived in Appendix 10.5. All that is needed is a quadratic fit to the data collected. From the fit parameters, I can determine the factor,  $\Delta\theta/\Delta y$ , which converts the digital counts of the optical lever channel,  $y$ , to units of radians.

To make the measurement, I locked a single arm and maximized the power build up. Then I slowly stepped the pitch or yaw pointing of one of the mirrors away to one side of resonance, and then back and to the other side, repeating this several times. All the while, I recorded the optical lever error signal of the mirror whose angle I was changing, and the power in the arm as determined from L1:LSC-NPTR{X,Y}\_OUT16, the amount of light transmitted through the ETMs.

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<sup>2</sup> A minor technicality is that since there are no filters between the QPD error signals and the offset channel, their units are exactly the same. Thus, calculating meters of beam spot motion as a function of offset serves to calibrate the error point. For convenience, this is what I did.

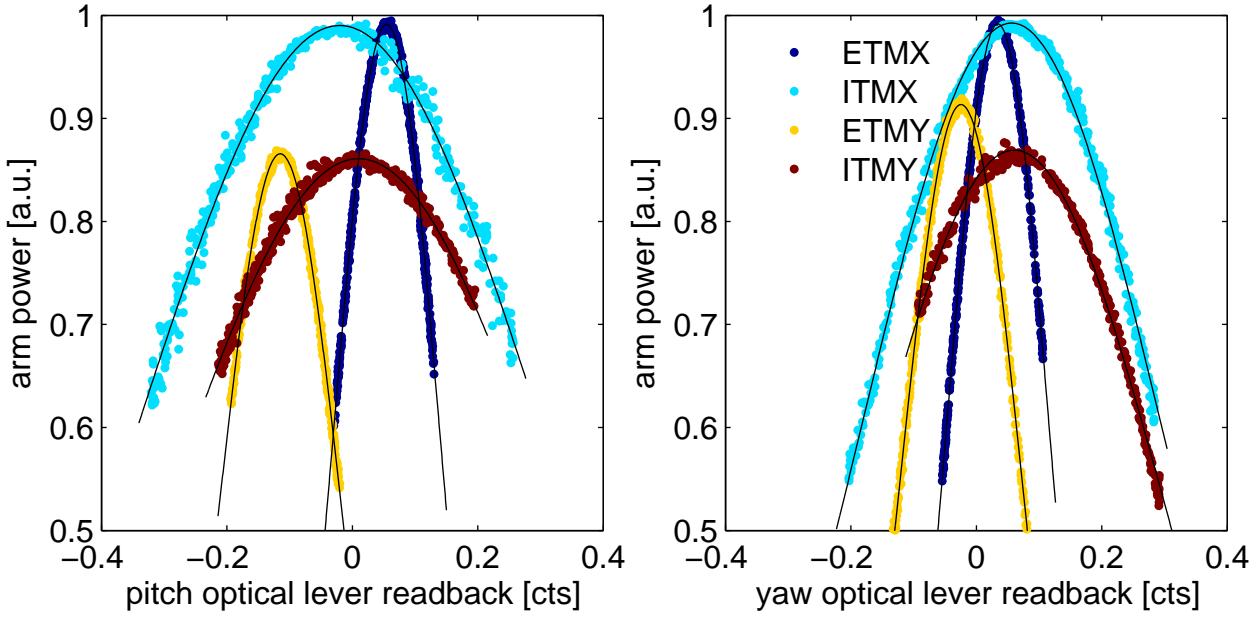


Figure 6-2. Optical lever calibration data and fits to Eq. 6.1.4.

From Eq. 10.5.28, we see that the power in the arm,  $P$ , is a function of the form

$$P = P_{max} \exp [-b(y - y_0)^2], \quad (6.1.4)$$

where  $b$  is related to physical cavity axis displacement  $a$  and tilt  $\alpha$  by  $by^2 = (a/w_0)^2 + (\alpha/\theta_0)^2$ .

In order to relate the optical lever signal,  $y$ , to physical cavity parameters, we divide by  $\Delta\theta^2$  and rearrange to get:

$$\frac{\Delta\theta}{\Delta y} = \sqrt{b} \left[ \left[ \frac{\Delta a / \Delta\theta}{w_0} \right]^2 + \left[ \frac{\Delta \alpha / \Delta\theta}{\theta_0} \right]^2 \right]^{-\frac{1}{2}}. \quad (6.1.5)$$

The terms in the numerators on the right hand side are fixed constants based on the cavity geometry and can be calculated using Eq. 10.4.4. The measurement data and fits are shown for both pitch and yaw in Fig. 6-2. The ETM optical levers make use of a broader range of optical lever signal than do the ITMs. (Also note that the maximum power in the y-arm is about 10% less than that in the x-arm. This is true at both Hanford and Livingston, and is due to the priority given to the x-arm in the alignment scheme, as explained in Appendix 10.6.)

Table 6-2. Calibrations to be used with the optical lever error signals for a measure of angular mirror motion. Units are  $\mu\text{rad}/\text{ct}$ .

	ETMX	ETMY	ITMX	ITMY	RM	BS	MMT3
pitch	49.4	43.0	14.9	15.6	61.9	47.3	57.4
yaw	50.7	43.3	20.1	20.2	42.5	63.5	55.5

### 6.1.2.2 RM, BS, and MMT3 optical levers

To calibrate the RM, BS and MMT3 optical levers, I used my own eyes and the camera images and known dimensions of the ETM beam cages. With the interferometer unlocked, I moved the optics in pitch and yaw, tracking the beam's movement on the ETM cages. In order to calibrate the RM, I used the reflection off ITMY to the RM and onto the ETMY cage. The BS and MMT3 required only straight shots to the ETMs. For yaw, I moved the mirrors until the beam was centered on each vertical suspension post, and for pitch I moved the beam from the center of the mirror to the top of the cage. The beam moves by  $x = 2\theta$  on across the cage when the mirror moves by  $\theta$ , so with small angle approximations, the mirror angle is simply  $x/2L$  where  $L$  is the distance from mirror to ETM cage.

The final  $\Delta\theta/\Delta x$  calibrations of all optical levers are in Table 6-2.

### 6.1.3 WFS Error Signals

The WFS error signals (i.e. L1:ASC-WFS1\_Q1) are physically Watts of power at the detectors. Converting the error signal in digital counts to Watts requires working backwards through the electronics, and can be divided into two parts. First, we must calibrate the WFS demodulation chain to backtrack WFS counts into voltage of signal at the input to the mixer. Second, we must convert voltage at the mixer into Watts at the sensor based on properties of the photodetector RF electronics. [For now, it suffices to calibrate the signal in Volts.](#)

The analog to digital RF chain for the WFS includes a demodulation board, a whitening board, an anti-alias board, and the ADC. This chain can be calibrated by injecting a sine wave of the same frequency as a typical WFS signal, yet of known voltage into the WFS demodulation board. Comparing the peak to peak voltage of this input sine wave to the peak to peak amplitude

Table 6-3. Demodulation chain calibration for each quadrant of each WFS. Units are  $\mu\text{V}/\text{count}$ .

	q1	q2	q3	q4	average
WFS1	0.35	0.32	0.34	0.35	0.34
WFS2	8.8	8.6	8.7	8.5	8.7
WFS3	6.4	5.8	5.8	5.7	5.9
WFS4	6.3	5.4	5.3	7.4	6.1

of the resulting digital counts signal provides the Volts per count conversion. The calibrations are presented in Table 6-3.

It should be noted that the demodulation chain calibration numbers for all quadrants of a particular WFS differ no more than 20% from the average. The demodulation chain does not significantly distort the error signals.

## 6.2 The ASC Change of Basis

make block figure!

### 6.2.1 WFS Input Matrix

(Move optical gain discussion somewhere else?) Optical gain is a term used in LIGO to described the amount of laser power produced at some interferometer port for a given physical change of some aspect of the interferometer. Ideally, photodiodes are placed where the optical gain is high. For the case of the wavefront sensors, one is placed at the anti-symmetric port where differential-mode signals are transmitted, one is placed to look at a pick-off of the beam in the recycling cavity which contains common and differential information, and two are placed at the reflected port, where common-mode signals end up. The precise locations are determined from the Gouy phases of the light. Details are found in Ref. xx.

The WFS optical gain is a measure of how much TEM01/TEM10 mode shows up at the locations of the wavefront sensors when a mirror (or specific combination of mirrors) moves in angle. Given the wavefront sensor is designed to measure the amplitude of this higher order mode, its error signal conveys the optical gain.

The optical gain for each of the optics' motions is not concentrated in one place, although it can appear more strongly in one location compared to another. In order to make use of as much

Table 6-4. Optical gain at 9.7 Hz in units of WFS counts / dof radian (pitch). Numbers in gray are the measurement results that have coherences less than 0.9. Boxes highlight the elements actually used in the control system. All other elements are set to zero.  
 change to Volts!

WFS1Q	WFS2I	WFS2Q	WFS3I	WFS4I	
5.8e+12	3.3e+09	6.7e+09	-1.3e+09	2.2e+09	dSoft
9.2e+11	-3.7e+09	-4.0e+09	3.4e+08	-1.7e+09	dHard
5.4e+10	-1.3e+09	2.1e+10	-3.9e+09	-1.7e+10	cSoft
4.9e+11	-1.6e+09	-2.4e+10	1.2e+09	-1.9e+10	cHard
2.6e+11	-1.1e+09	-2.4e+10	7.0e+09	-3.5e+10	RM

of the information as possible, we must use all sensors that witness a particular motion. However, when there are multiple signals at a particular place, the WFS error signals tell us the sum of all optical gains at its location. The amount of optical gain at each detector for each motion at one particular frequency forms the *sensing matrix*. The inverse of the sensing matrix is known as the *input matrix*, which tells how to take the appropriate weighted sum of signals in order to reconstruct a particular motion. The procedure for measuring the sensing matrix is as follows:

1. excite one of the mirrors (or specific combination of mirrors) at frequency  $f$
2. demodulate each of the WFS signals at  $f$
3. normalize to the phase of the excitation readback
4. repeat for each mirror (or sets of mirrors)

A key aspect of the measurement is that a notch filter at frequency  $f$  is engaged so the control servo does not suppress our excitation.

An example calibrated sensing matrix in the radiation pressure eigenbasis as taken during a 10 W lock is shown in Table 6-4. Rows represent excitation and columns are the wavefront sensors. Before inverting to create the input matrix, the smallest of the elements (which are more or less equivalent to the elements for which optical gain is also expected to be weak), are artificially set to zero. This avoids the contamination of strong signals by those with weak signal-to-noise ratios. The elements that remain after this process are highlighted by boxes. Note that the sensing matrix is in fact composed of two sub-matrices: one for the differential degrees of freedom, and one for the common degrees of freedom.

Paragraph discussing sensing matrix numbers.

Table 6-5. WFS output matrix (pitch). For the Livingston cavity geometry  $r = 0.91$  and for Hanford  $r = 0.87$ .

dSoft	dHard	cSoft	cHard	RM	
1	$r$	1	$r$	0	ETMX
-1	$-r$	1	$r$	0	ETMY
$r$	-1	$r$	-1	0	ITMX
$-r$	1	$r$	-1	0	ITMY
0	0	0	0	1	RM

## 6.2.2 WFS Output Matrix

The WFS output matrix determines how to convert the radiation pressure eigenbasis control signals into individual mirror control signals. It is the basis transformation matrix,  $S$ , as defined in Eq. 5.1.9. The matrix is arbitrarily normalized so the largest element is 1, and it is repeated with appropriate sign changes to form differential and common soft and hard modes of the two arms. The output matrix is shown in Table 6-5, where the  $r$  is 0.91 for Livingston and 0.87 for Hanford.

## 6.2.3 Diagonalizing the WFS Drive Matrix

**fix this** During the sensing matrix measurement, the optical levers provide a record of the motion of the test masses. Properly combining the optical lever responses tells the amplitude of each radiation pressure degree of freedom's movement. The actual numbers for the measurement data presented in Table 6-4 are found in Table 6-6. This now allows us to complete the first part of obtaining an optical gain matrix. Each row of the sensing matrix should be divided by the amplitude of that dof's excitation, the diagonal elements of Table 6-6. The result of doing so gives the angular optical gain of the interferometer in terms of WFS digital counts per radian.

**write out the rest of this section**  $D = \text{'drive'}$  = DOF excitation to DOF excited matrix  
 $(\theta_{\text{dof}})$   $U = \text{'unknown'}$  = hardware mostly; coils, etc.  $M = \text{'mirror'}$  = mirror gains; a diagonal matrix  $C = \text{'control'}$  = ASC output matrix

We have  $D = U * M * C$ . A drive is multiplied first by the output matrix ( $C$ ), then by the mirror gains ( $M$ ), then put into hardware ( $U$ ) to create what's actually excited.

Table 6-6. Actual eigenbasis motion during sensing matrix excitations as witnessed by the optical levers. Columns are excitations and rows are the pitch motions at 9.7 Hz in units of  $\mu\text{rad}$ . Ideally, this would be a diagonal matrix. It mostly is.

dSoft	dHard	cSoft	cHard	RM	
<b>5.1e-06</b>	-5.2e-08	6.1e-07	-3.8e-08	-1.8e-07	dSoft
-3.4e-07	<b>5.0e-06</b>	7.3e-07	-1.0e-06	2.4e-07	dHard
-4.1e-07	-3.3e-08	<b>5.9e-06</b>	6.8e-07	2.5e-07	cSoft
-6.4e-07	-5.9e-07	1.1e-06	<b>5.7e-06</b>	4.7e-07	cHard
-1.6e-07	-1.8e-06	-5.5e-07	2.6e-06	<b>5.6e-06</b>	RM

Table 6-7. Mirror gains for diagonalization of drive matrix.

ETMX	ETMY	ITMX	ITMY	RM
1.33	1.38	0.96	0.87	1.0

To make D diagonal, we want to find a new M, M\_new, which must have the property

$$M_{\text{new}} = \text{inv}(U)^* \text{inv}(C) = M^* C^* \text{inv}(D)^* \text{inv}(C)$$

### 6.3 Sensing Matrix Stability

Show how the sensing matrix changes in time (APS presentation).

### 6.4 Input Beam Motion

The beam centering and QPD servos operate up to only about 50 mHz, meaning the beam-centering degree of freedom is uncontrolled at higher frequencies. Since beam spot motion on the test masses couples to DARM, anything that causes the beam's position on the test mass to change on time scales faster than half a minute becomes itself a direct noise source for DARM. The HAM seismic isolation tables from which the input optics are suspended have resonant “stack” modes from about 0.8 Hz to 3 Hz. The excess table motion at these frequencies is transmitted to the MMTs. Jitter on the pointing of the input beam is thus a primary contender for beam spot motion on the test masses.

The wavefront servos are the mechanism by which input beam motion is impressed on the test masses; they are responsible, among other things, for making the interferometer follow the input beam up to several Hz. The WFS detect differences between the angle of the cavity (as determined by the angles of the mirrors) and the angle of the beam impinging the cavity. If either the input beam or the cavity angle changes, the WFS will move the mirrors to correct for the

angle mismatch. Thus, even if the mirrors are perfectly quiet, a non-stationary input beam will result in mirror motion and mirror motion in turn creates beam spot motion (see Eq. 5.1.1).

I measured the impression of the input beam motion on the mirrors by increasing the gain of the common-degree-of-freedom WFS servos (CH, CS, RM) for about 10 minutes. Comparing the amount of angular motion of the mirrors as witnessed by the optical levers from this time of high common WFS gain to a time with nominal WFS gain and similar seismic motion, we can see the effect directly. Fig. 6-3 shows comparison spectra, demonstrating how there is higher test mass motion around 1 Hz when the common WFS gains are higher. The rms mirror motion also increases by about 20%.

It is possible for the extra mirror motion to result from gain peaking of the WFS servos. However, a plot of the WFS error signals during the time of nominal gain and high gain shows that there is not, in fact, any evidence of gain peaking. The common WFS spectra in Fig. 6-4 do not show any extra noise when their gains are higher. It is worth noting that the higher gain is evident in the common WFS spectra by the extra suppression seen below 1 Hz. Also, the differential WFS spectra are unchanged, as expected. It can therefore be concluded with reasonable certainty that the increase in test mass motion between 1 and 2 Hz during this test is indeed due to the WFS impressing input beam motion on the mirrors.

## 6.5 The Marginally-stable Power Recycling Cavity

The power recycling cavity (PRC) is the linear cavity formed by the RM and ITMs. Since the radius of curvature of both the RM and the ITMs points in the same direction, the cavity is geometrically unstable. For example, in its cold state at LLO the  $g$ -factor of the cavity is 1.00005 and at LHO it's 1.00003. The beam in the PRC is not spatially contained and the cavity is degenerate with respect to higher order modes. The heating of the ITMs from the kilowatts of power in the arm cavities together with the ITM thermal compensation system (TCS) serve the role of making the PRC geometrically stable for interferometer operation. The heating and cooling of the ITMs is a very complicated process and therefore not very precise, so the value of the hot PRC's  $g$ -factor is usually not constant.

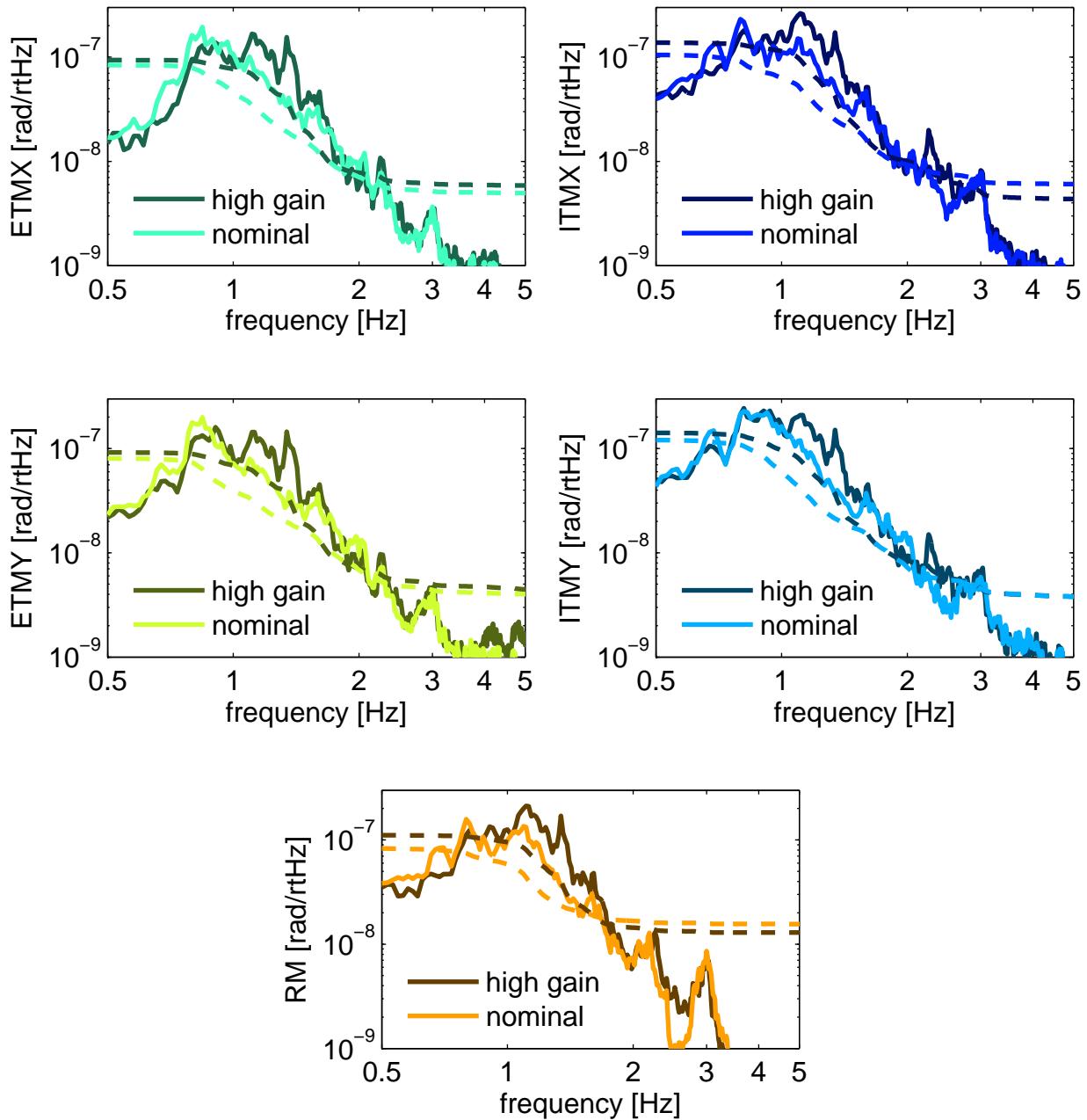


Figure 6-3. Input beam motion impression on the core mirrors (pitch). Residual mirror motion as witnessed by the optical levers when the common WFS gains ( $c_{\text{Soft}}$ ,  $c_{\text{Hard}}$ , RM) are increased to  $2.5 \times$  nominal is compared to residual mirror motion when the WFS gains are nominal. Both spectra come from a time of similar seismic activity (typical weekday afternoon noise), shown in Fig. 10-5.

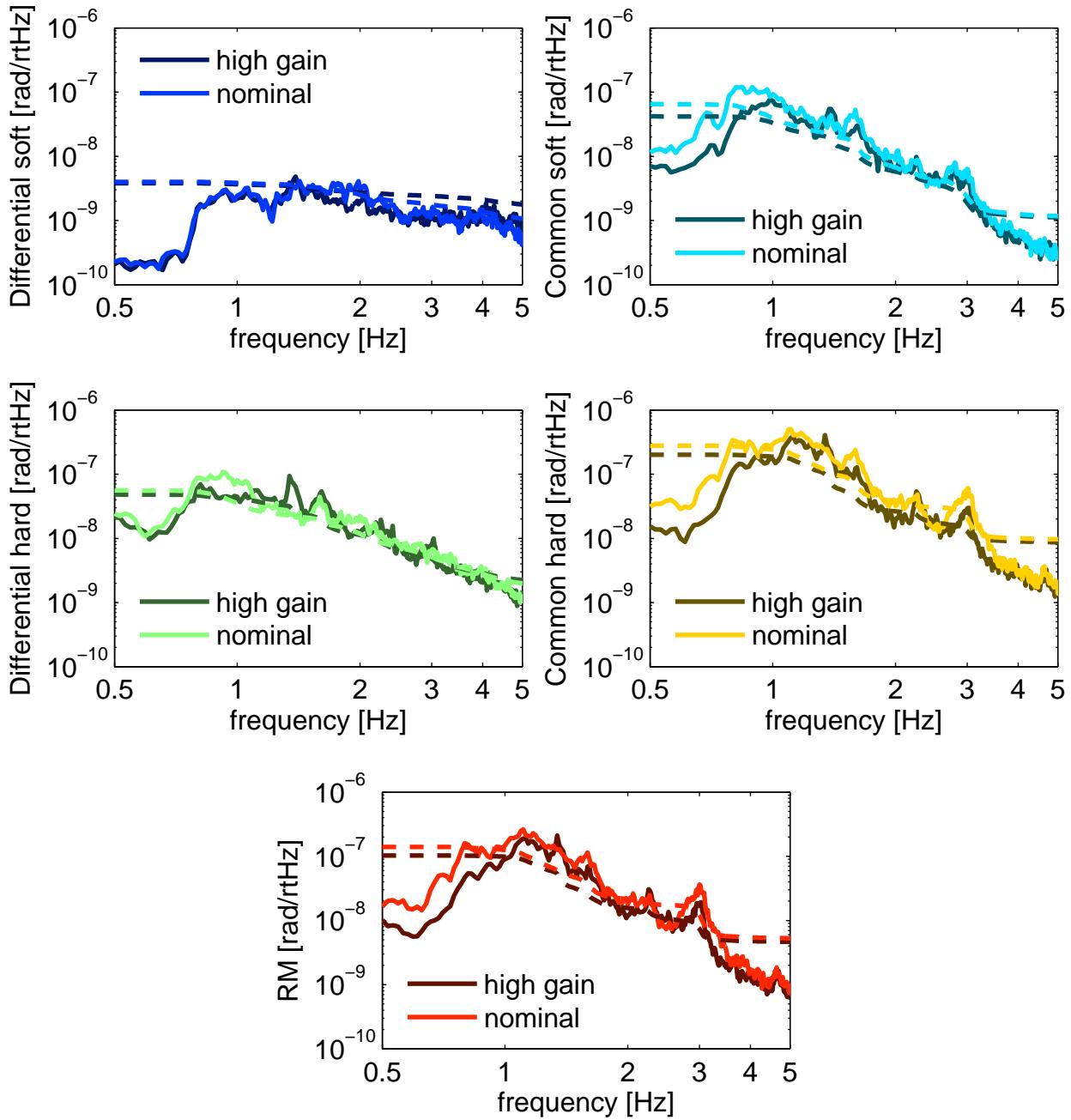


Figure 6-4. Comparison of WFS error signals (the residual motion) during a time of normal operation and a time when the common WFS gains were  $2.5 \times$  higher than nominal. This excludes gain peaking as a cause of the extra mirror motion witnessed during the time of high gain. Fig. 10-5 shows the ground motion spectra at the time of this measurement.

**differentiate magnitude of SPOB vs fluctuations in SPOB.** The changing  $g$ -factor has potentially severe consequences for the ASC. Because of its geometry, the power build-up in the PRC is very sensitive to both the mirror angles and the  $g$ -factor. Power fluctuation is detrimental because the signal to noise ratios of the sensors that probe the PRC light degrade due to the presence of increased junk light that contributes shot noise but not signal. WFS1Q, WFS2I, and WFS2Q are the most sensitive to the PRC because their signals are derived from the 25 MHz sidebands. Their sensitivity to mirror motion is therefore subject to change. Since achieving a flat power build-up in the PRC is a difficult task (too much motion in the PRC is quite often a cause of lock loss when making measurements), we must update the real-time control system to reflect their changing sensitivities. Otherwise, the mirror angles will not be accurately controlled.

An estimate of the expected power fluctuations based on the  $g$ -factor and RM motion is a straightforward exercise when using Eq. 10.4.4 and Eq. 10.5.28 as derived in the Appendix. If we estimate the  $g$ -factors of the RM and ITM as  $g_{RM} = 1 + \delta$  and  $g_{ITM} = 1 - \delta$  (where  $\delta = 6 \times 10^{-4}$  for LLO the cold state) and approximate the distance of each mirror to the cavity waist as  $z$  since the two mirrors are very close to each other compared to the waist location, then Eq. 10.4.4 reduces to:

$$\begin{bmatrix} a_{PRC} \\ \alpha_{PRC} \end{bmatrix} = \begin{bmatrix} z(2+\delta)/\delta & z(2-\delta)/\delta \\ -1/\delta & -1/\delta \end{bmatrix} \begin{bmatrix} \theta_{RM} \\ \theta_{ITM} \end{bmatrix}. \quad (6.5.1)$$

Fig. 6-5 plots the power in the PRC as a function of  $\theta_{RM}$  for several values of  $\delta$ , demonstrating the sensitivity of the PRC to the ITM heating. For example, the typical RM angular displacement of  $10^{-7}$  rad results in a 66% power loss when the PRC  $g$ -factor is very near instability with a value of  $1 - 0.0001$ . Only as the  $g$ -factor moves further from 1 does the angular motion of the RM have less and less of an effect on the power build-up.

### 6.5.1 Power Scaling

The signal at the wavefront sensors is proportional to the amplitude of the sidebands, or the square root of the sideband power. Thus, as the PRC  $g$ -factor and therefore the power in the

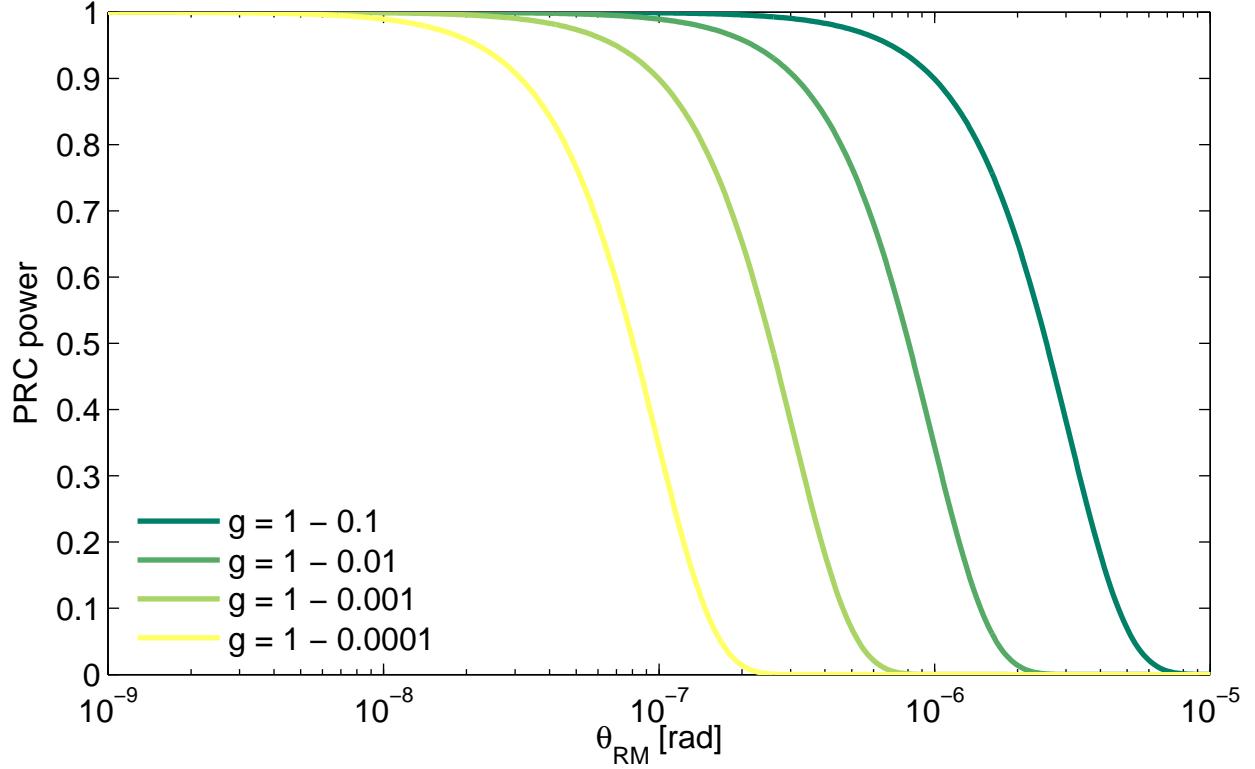


Figure 6-5. Dependence of power build-up in the power recycling cavity on the PRC's  $g$ -factor and the RM tilt. TCS is necessary for stabilizing the PRC's geometry and therefore its sensitivity to mirror motion. For simplicity, the ITM is assumed stationary in these plots.

recycling cavity changes, so do the WFS1 and WFS2 optical gains. In order to compensate for this  $g$ -factor dependence, we multiply the WFS{1Q, 2I, 2Q} error signals in real-time by

$$\frac{1}{P_{in}} \left[ \frac{\text{NSPOB}}{350} \right]^{-1/2} \quad (6.5.2)$$

and WFS3I and WFS4I by  $1/P_{in}$ . NSPOB is the normalized sideband power in the PRC as measured by the  $2f$ -demodulated POB signal, and the 350 is the reference NSPOB, treated as nominal. Thus, during interferometer operation, all WFS signals are normalized to input power and are not dependent on the PRC power. This correction to the WFS signals is called power scaling.

To verify that the WFS optical gains do indeed scale with the sideband power as expected, I tracked the WFS optical gain as  $g$  changes. I excited three of the test masses (ETMX, ITMX,

RM) at three different frequencies (9.7 Hz, 10.7 Hz, and 11.7 Hz, respectively) during a full interferometer lock and changed the TCS settings so that over the course of 15 minutes the  $g$ -factor steadily changed. Demodulating each of the WFS signals at each of the three excitation frequencies as a function of time shows how the strength of the signal at the WFS due to the motion of these three mirrors changes. To compensate for the difference in pendulum responses to the excitations, I multiplied the demodulated signals for a particular excitation  $f$  by  $(f/9.7)^2$ . I also normalized the response by the phase of the mirror's motion as witnessed by the optical levers.

The results are shown in Fig. 6-6, and include a plot of how NSPOB changed over time. As expected, WFS1Q, WFS2I, and WFS2Q show dependence on the PRC power, and therefore the  $g$ -factor. The WFS3 and WFS4 sensing elements are flat. Fitting lines to each of the tracked elements, we find a good fit with the expected power of 1/2 dependence.

## **6.6 WFS Servo Open Loop Transfer Functions**

### **6.7 Residual Angular Motion**

### **6.8 ASC to DARM Noisebudget**

Broadband effect on DARM.

#### **6.8.1 Tuning the Cut-off Filters**

The cut-off frequency of the lowpass filters for the WFS control are of particular importance in the DARM noisebudget. The lowpass filter is necessary for suppressing the impression of sensing noise on suspension control.

### **6.9 Feed-Forward**

Implementing a method of Wiener filtering, I show that the angular sensing and control error signals can be predicted by ground motion witnessed by local seismometers.

Using S6 data, I evaluated the potential benefits of seismic feed-forward for the angular degrees of freedom. I designed FIR Wiener filters from simultaneous seismometer and ASC error signal time series. The Wiener filter minimizes the mean square error between the ASC error signal and the Wiener filtered seismometer data. The filtered seismometer data can be a good

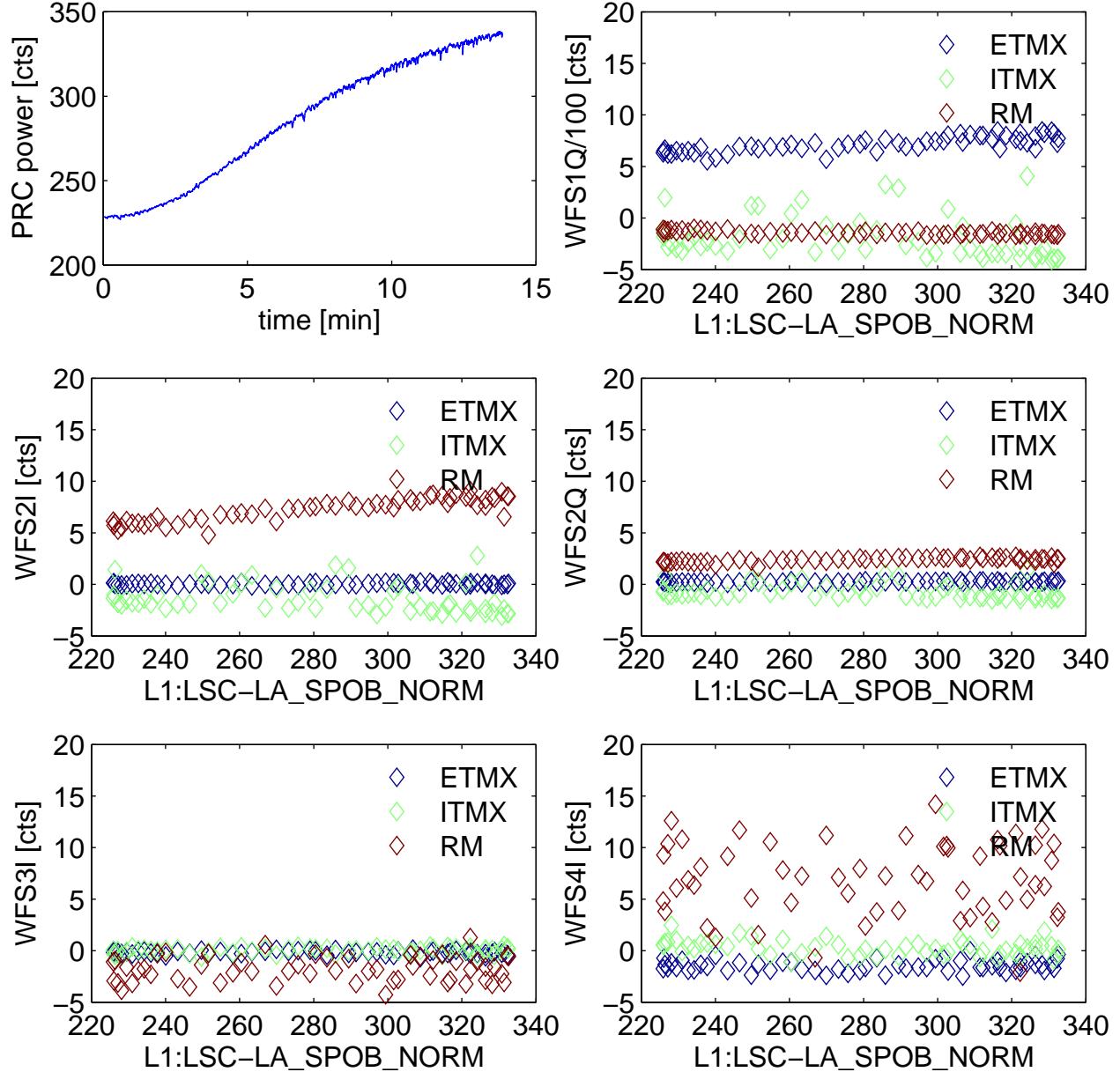


Figure 6-6. WFS optical response as a function of power recycling cavity geometry. WFS1Q, WFS2I, WFS2Q are more sensitive to test mass motion as the power in the recycling cavity increases. To achieve a dependable feedback system, the error signals are scaled in real-time, forcing their responses to be flat with power. This range of SPOB is low for normal operations. [plot as ratio of first value](#).

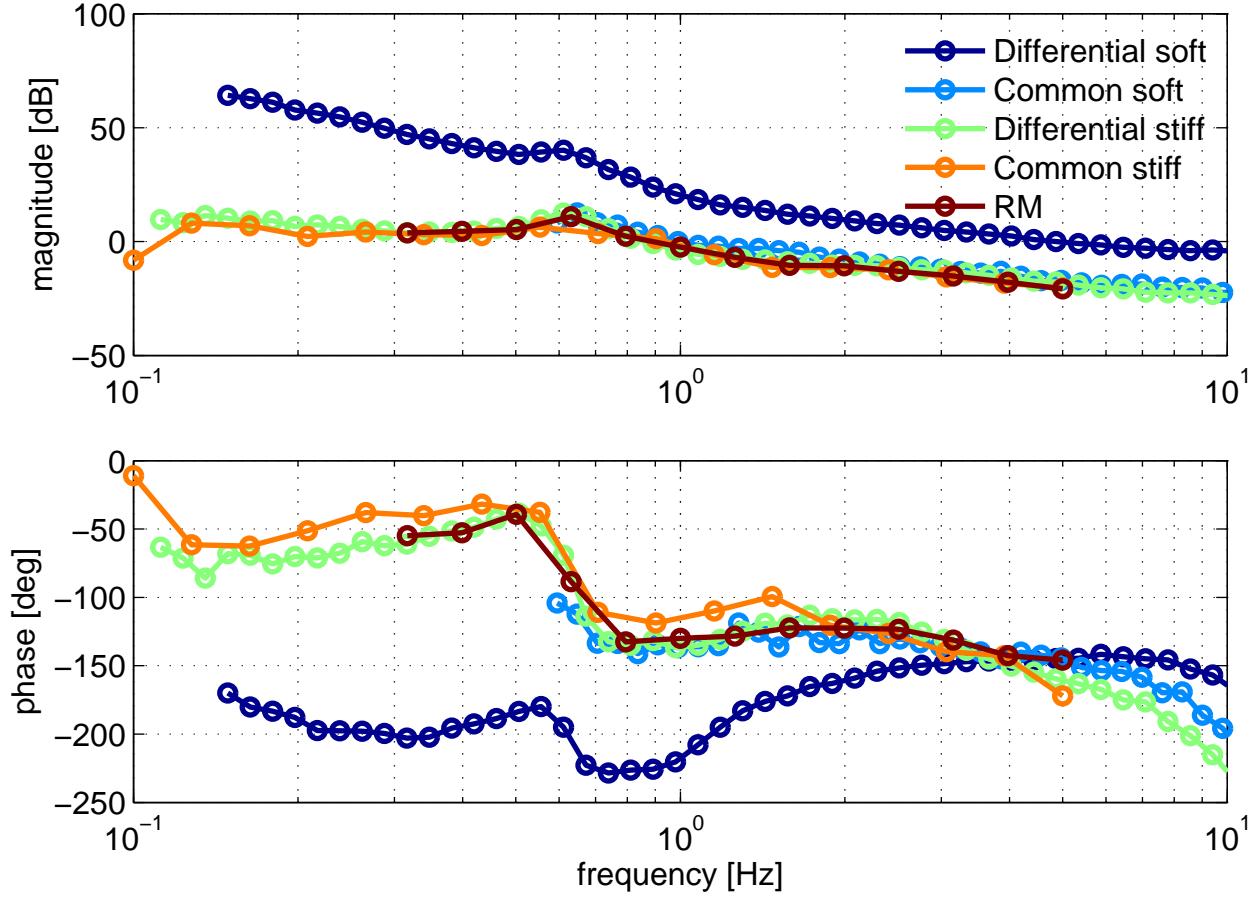


Figure 6-7. Open loop gains (pitch) of the 5 WFS loops as measured with 6 W input power.

approximation to the ASC error signal and thus fed-forward. I found that with a sufficiently long Wiener filter and 30 minutes worth of data, we can accurately predict the ASC error signal from 0.1 to 20 Hz. If implemented, the rms angular mirror motion would be reduced by a factor of ten and yield a potential reduction in DARM at low frequencies. More importantly, less angular mirror motion would make for a more stable interferometer, necessary for high power operation, a key challenge for aLIGO.

[put in Wiener filter figures; explain Wiener filtering or reference?](#)

## 6.10 Advanced LIGO

The Advanced LIGO interferometers will have heavier mirrors, a stable recycling cavity, and more circulating power.

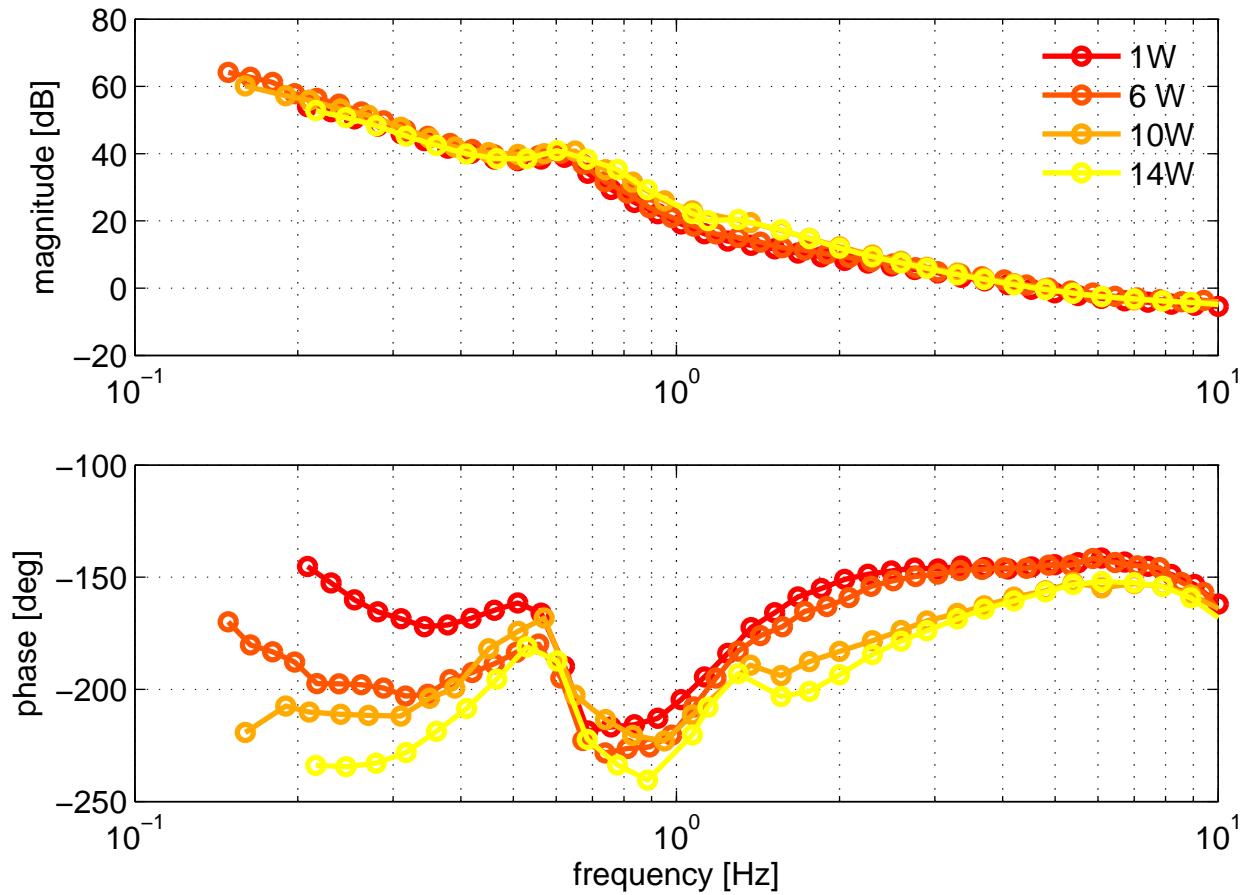


Figure 6-8. Open loop gains (pitch) of the differential soft (WFS1) loop as measured at four different powers.

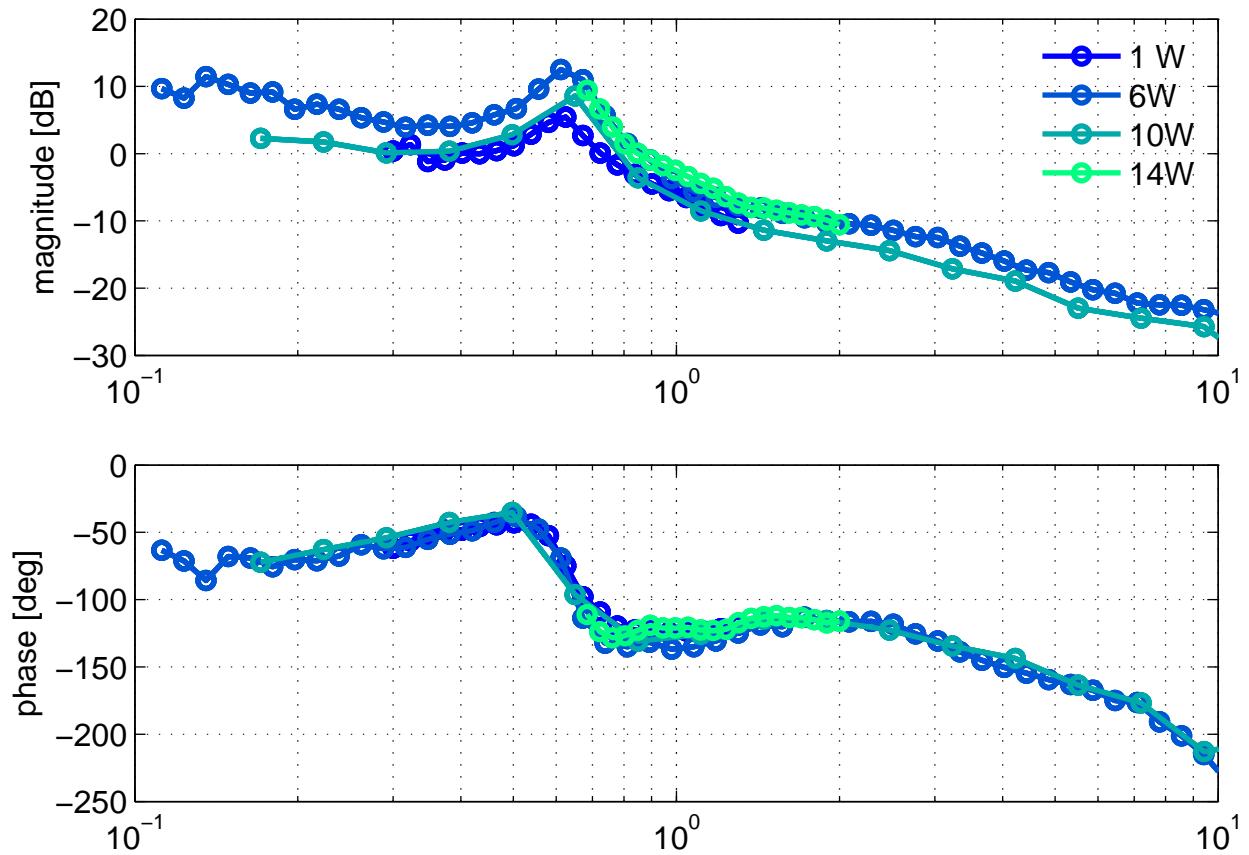


Figure 6-9. Open loop gains (pitch) of the differential hard (WFS2B) loop as measured at four different powers.

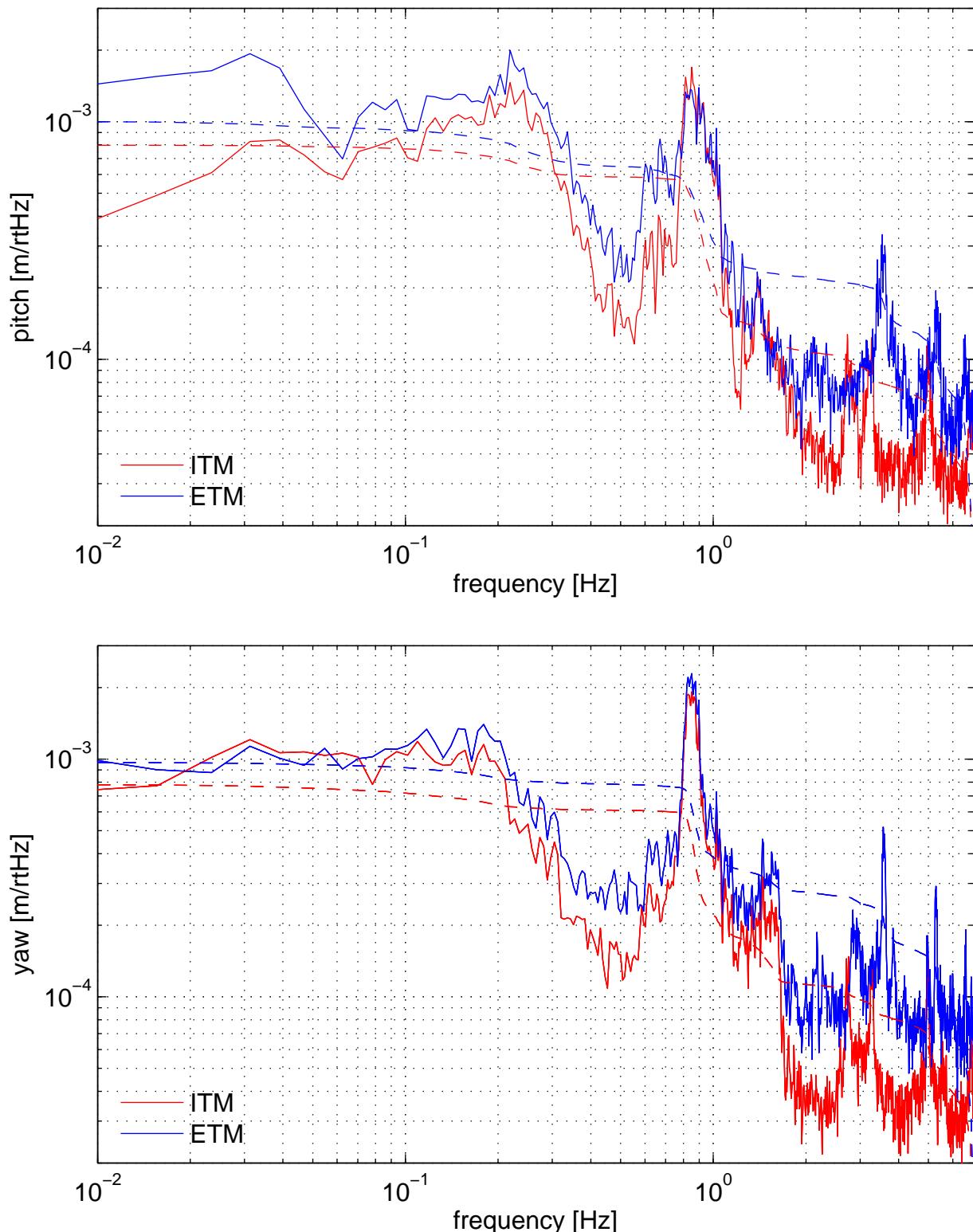


Figure 6-10. Beam spot motion on the ITMs and ETMs during a 16 W lock at night (May21, 2010, 06:02:30 UTC).

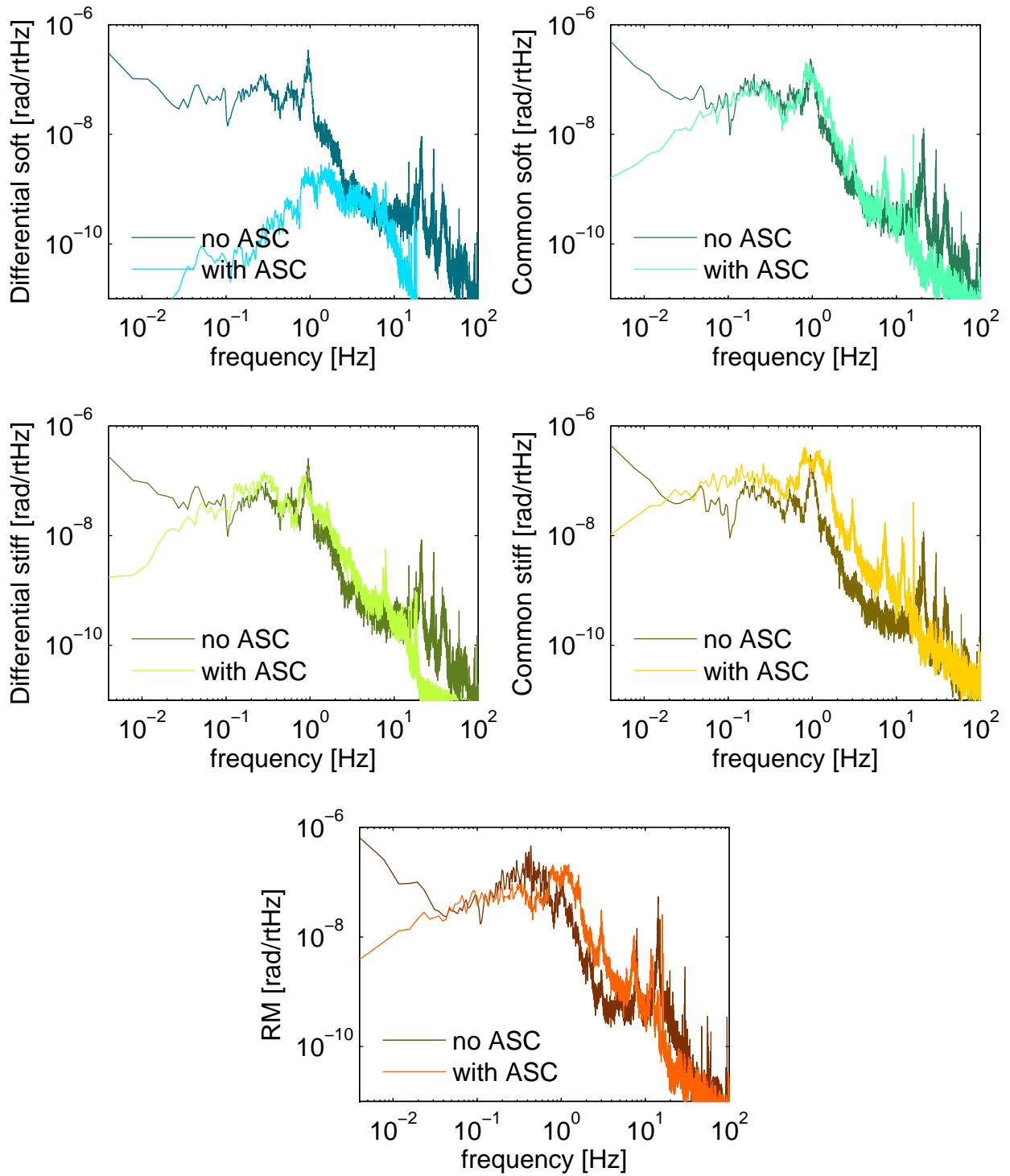


Figure 6-11. Propagation of WFS sensor error signals from 10 W lock through input matrix and power scaling to eigenbasis, compared with eigenbasis reconstruction of optical lever signals when interferometer not locked, but optics under oplev damping. Data are taken 45 minutes apart. [Perhaps include loop-undone backgrounds, too, using my measured OLTFs to show match to optical lever background.](#)

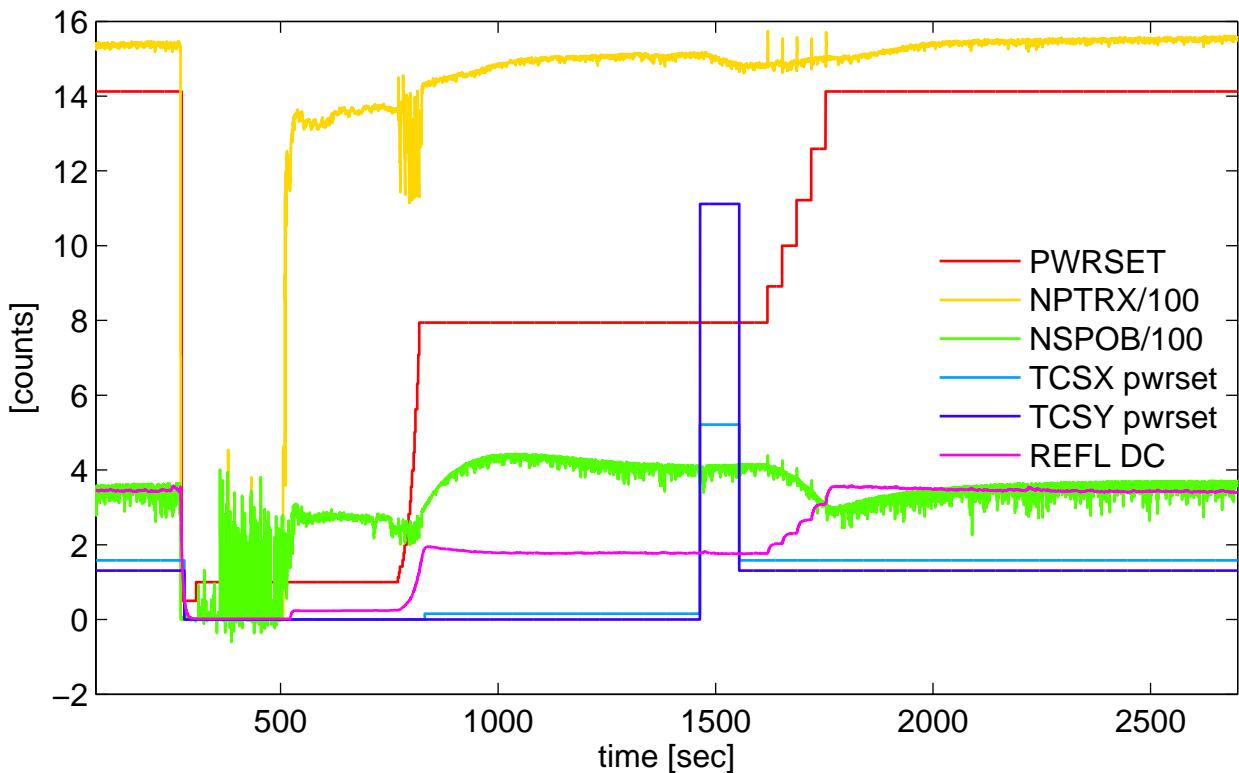


Figure 6-12. Time series of interferometer signals showing a typical lock loss and re-lock followed by an increase of power to 14 W. (From July 23, 2009 elog.) [work this in somewhere.](#)

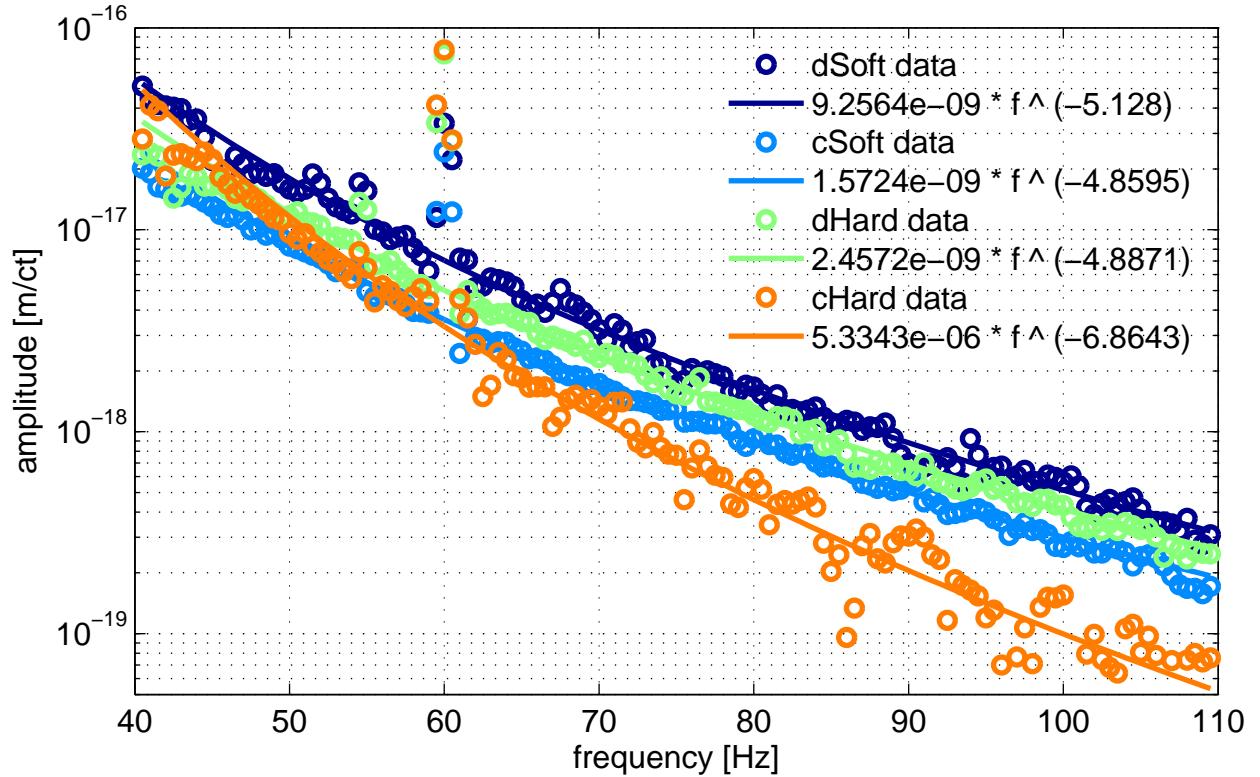


Figure 6-13. ASC to DARM transfer function for four of the five wavefront sensor loops. The RM to DARM transfer function could not be measured because the contribution is so small. The fitted curves can be multiplied by the WFS error signals at any time to calculate the ASC noise contribution to DARM. [Need to turn cts into Volts.](#)

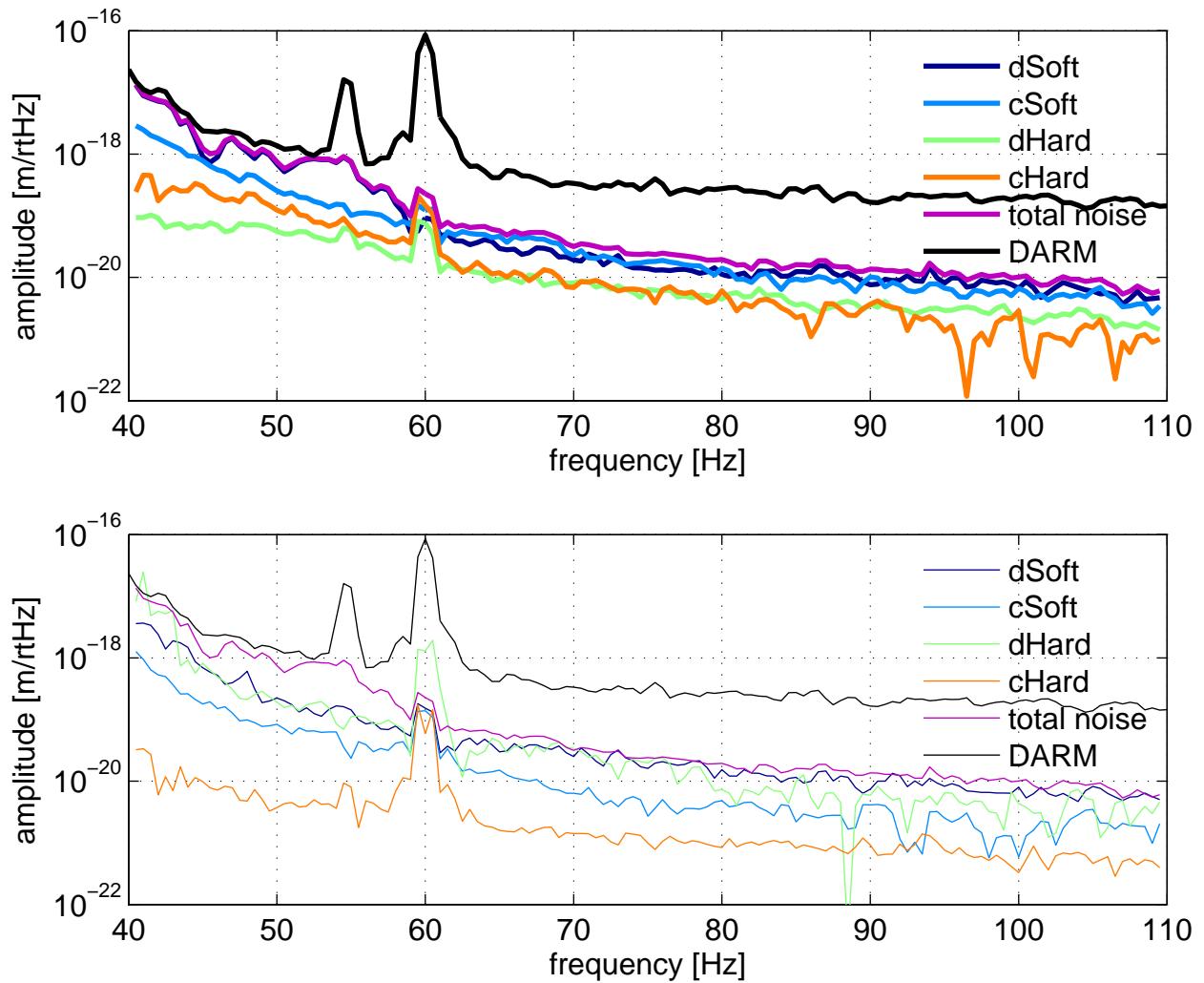


Figure 6-14. Wavefront sensor to DARM noisebudget for pitch (top) and yaw (bottom) during a 14 W lock (July 17, 2009). [which line width?](#)

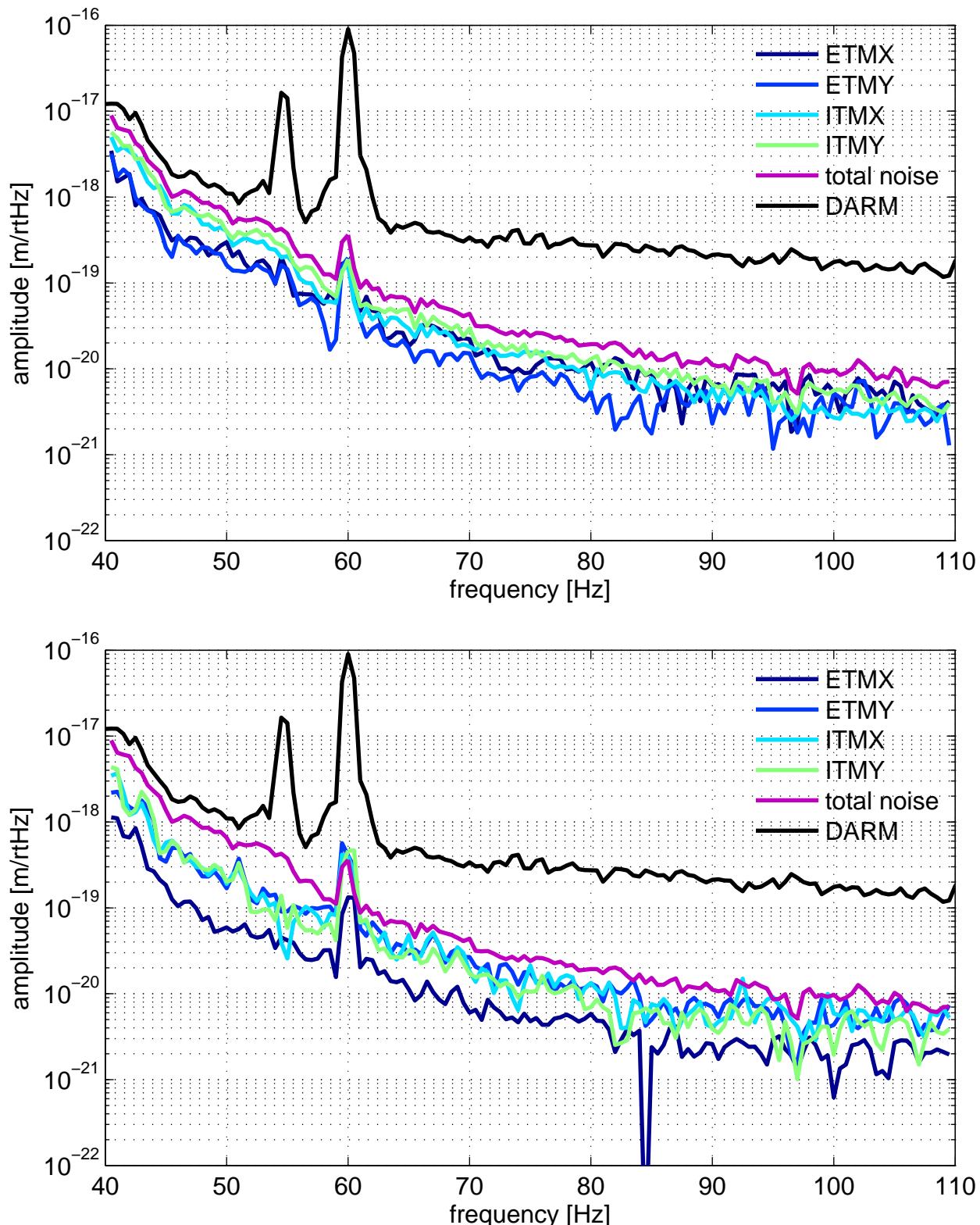


Figure 6-15. Optic to DARM noisebudget for pitch (top) and yaw (bottom) during a 14 W lock (July 17, 2009). [This height or previous figure's height?](#)

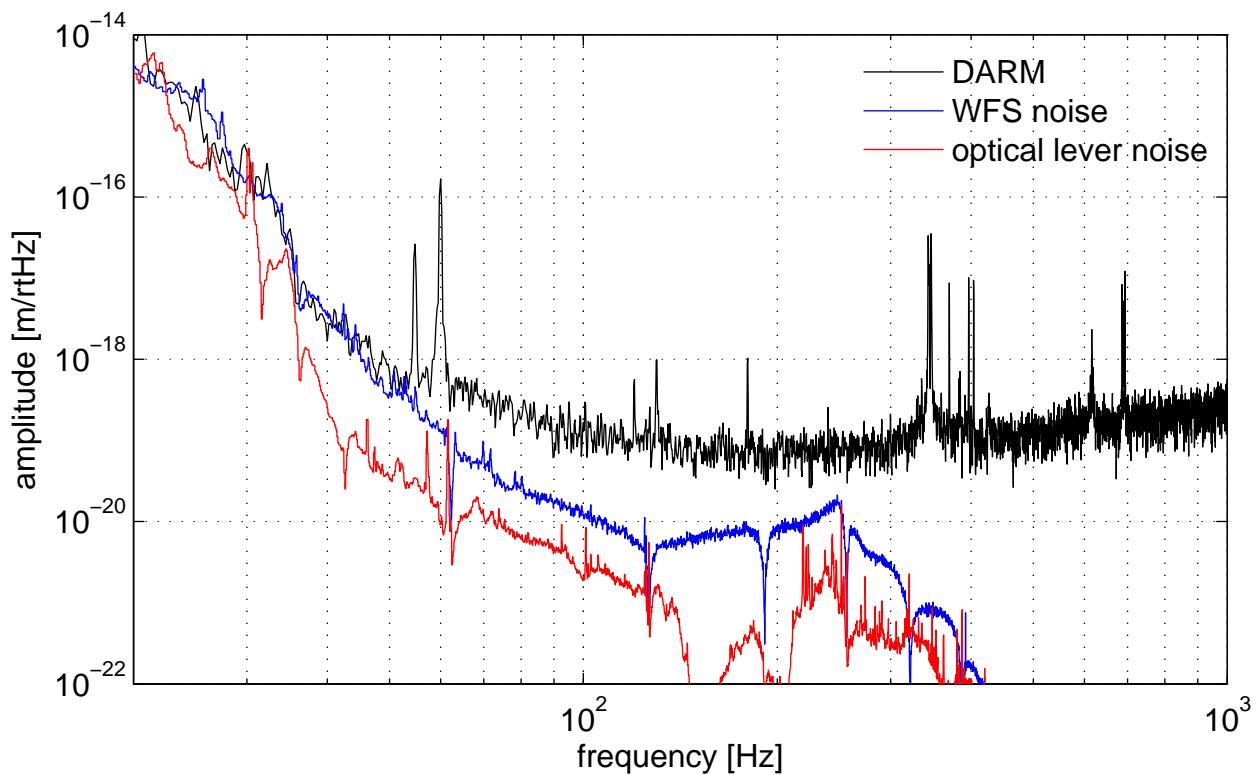


Figure 6-16. Total WFS and optical lever noise contribution to DARM during a 16 W lock at night (gps time 958456964). Pitch and yaw contributions are added in quadrature under the assumption they are de-coupled.

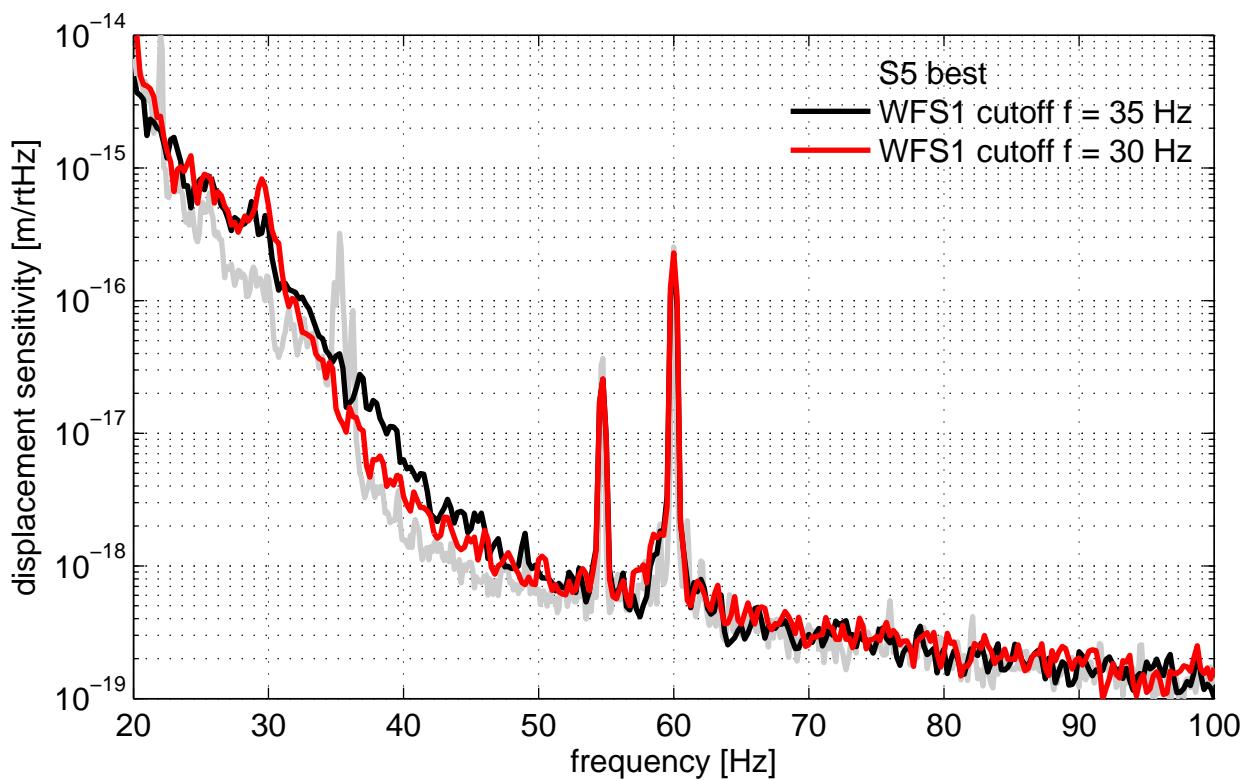


Figure 6-17. Effect of the WFS1 lowpass filter cutoff frequency on strain sensitivity. [gray legend line missing?](#)

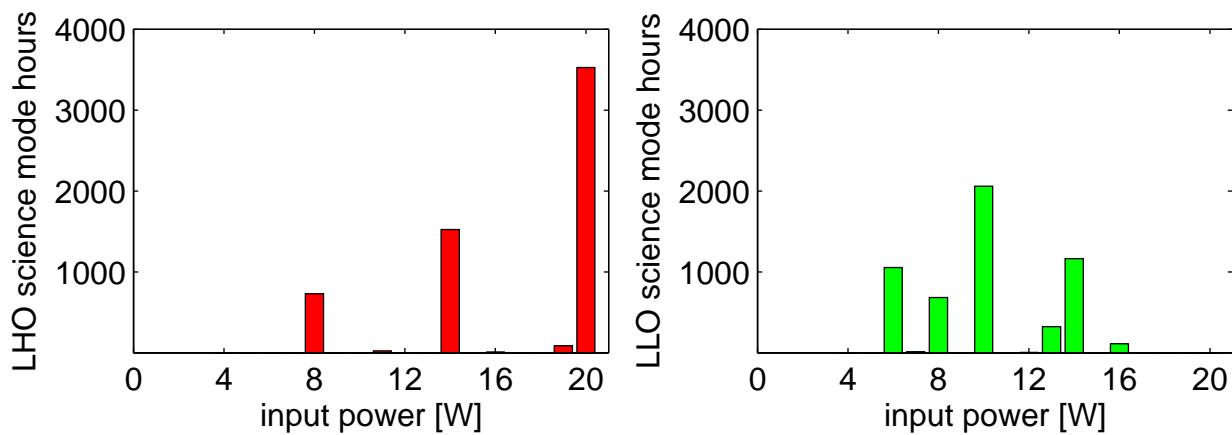


Figure 6-18. Histogram of input powers used during S6.

CHAPTER 7  
EXPERIMENTAL MEASUREMENT OF THE SIDLES-SIGG EFFECT

highlight by having as a separate chapter here or lump with previous (characterization) chapter?

**7.1 Measured modes**

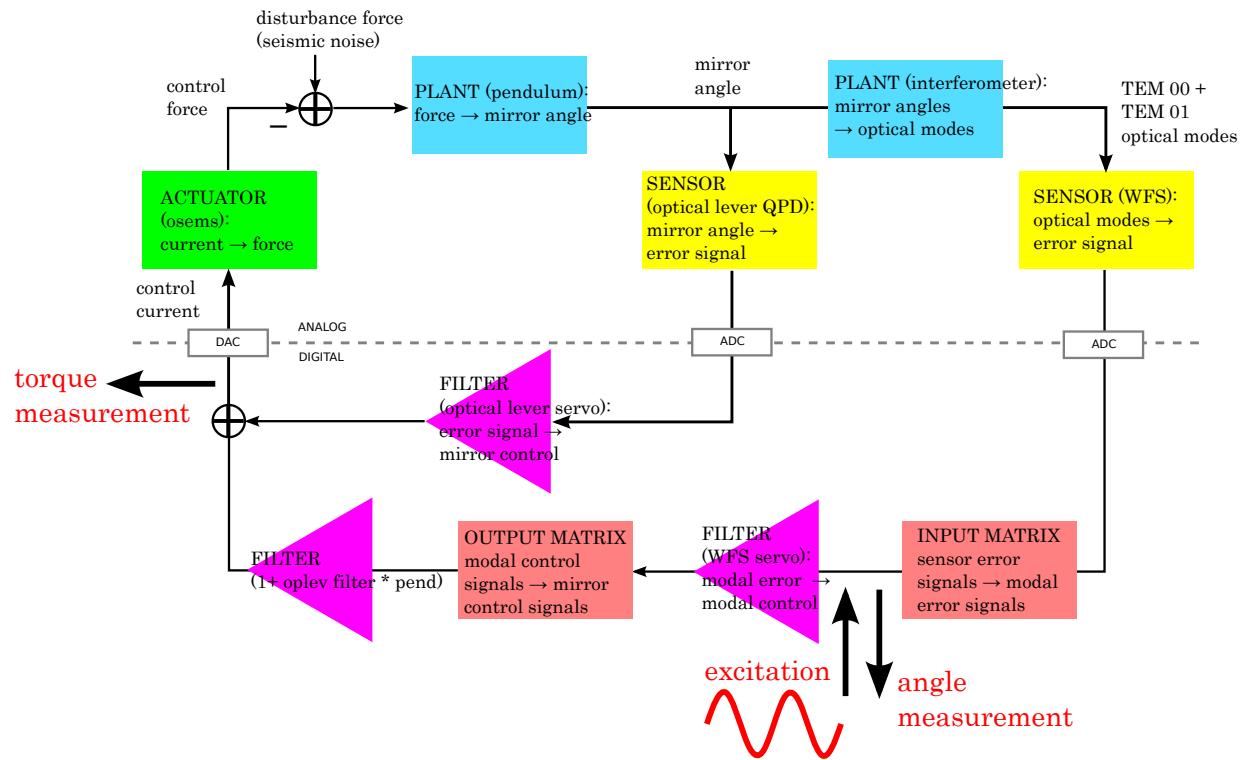


Figure 7-1

## CHAPTER 8 SUMMARY

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## CHAPTER 9

### APPENDIX A

#### 9.1 Overlap integrals

A measure of the mode matching can be given by the amount of power coupled from one mode into another. This is calculated as the square of the overlap integral of two fields,  $\psi_1$  and  $\psi_2$ , for a particular z-axis (propagation direction) cross-section:

$$P = |\langle \psi | \psi' \rangle|^2 = \left[ \int_{-\infty}^{\infty} \psi^*(x) \psi'(x) dx \right]^2 \quad (9.1.1)$$

We are interested in the lowest order Hermite-Gaussian mode:

$$\psi(x, z) = u_0(x, z) = \left[ \frac{2}{\pi w_0^2} \right]^{1/4} \left[ \frac{q_0}{q(z)} \right]^{1/2} \exp \left[ \frac{-ikx^2}{2q(z)} \right] \quad (9.1.2)$$

which can be rewritten as a function of  $x$  and  $q$  using  $q_0 = i\text{Im}(q)$ , and  $w_0^2 = -2q_0i/k$ :

$$u_0(x, q) = \left[ \frac{-k\text{Im}(q)}{\pi q^2} \right]^{1/4} \exp \left[ \frac{-ikx^2}{2q} \right] \quad (9.1.3)$$

Eq. (9.1.3) is normalized such that  $\langle u_0 | u_0 \rangle = 1$ .

We want to know the square of the overlap integral for two fields given by different  $q$  parameters at one location  $z$ . First, the overlap integral:

$$\langle q_1 | q_2 \rangle = \int_{-\infty}^{\infty} u_0(x, q_1) u_0(x, q_2) dx \quad (9.1.4)$$

$$= \left[ \frac{k^2 \text{Im}(q_1^*) \text{Im}(q_2)}{\pi^2 q_1^{*2} q_2^2} \right]^{1/4} \int_{-\infty}^{\infty} \exp \left[ - \left[ \frac{-ik}{2q_1^*} + \frac{ik}{2q_2} \right] x^2 \right] dx \quad (9.1.5)$$

$$= \left[ - \frac{k^2 \text{Im}(q_1) \text{Im}(q_2)}{\pi^2 q_1^{*2} q_2^2} \right]^{1/4} \sqrt{\frac{\pi}{\left[ \frac{-ik}{2q_1^*} + \frac{ik}{2q_2} \right]}} \quad (9.1.6)$$

$$= [\text{Im}(q_1) \text{Im}(q_2)]^{1/4} \sqrt{\frac{2}{q_1^* q_2 (1/q_2 - 1/q_1^*)}} \quad (9.1.7)$$

Then, the power is given by:

$$|\langle q_1 | q_2 \rangle|^2 = \frac{2\sqrt{\text{Im}(q_1)\text{Im}(q_2)}}{\sqrt{q_1^* q_1 q_2^* q_2 \left[ \frac{1}{q_2} - \frac{1}{q_1^*} \right] \left[ \frac{1}{q_2^*} - \frac{1}{q_1} \right]}} \quad (9.1.8)$$

$$= \frac{2\sqrt{\text{Im}(q_1)\text{Im}(q_2)}}{|q_2 - q_1^*|} \quad (9.1.9)$$

Note that Eq. (9.1.9) simplifies to 1 when  $q_1 = q_2$  as expected and that this whole formulation assumes that the beams are propagating along the same  $z$ -axis.

## 9.2 Gaussian beam on a split photodetector

The power per area of a Gaussian beam traveling along the  $z$ -axis is

$$p(x, y) = \frac{2P_0}{\pi w^2} \exp\left[\frac{-2x^2}{w^2}\right] \exp\left[\frac{-2y^2}{w^2}\right] \quad (9.2.1)$$

where  $w$  is the beam radius at  $z$ . This has been normalized such that  $\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p(x, y) dx dy = P_0$ .

Then, for a beam displaced by  $x_0$  from the center of a split photodetector, the power on the left side is

$$P_{left} = \frac{2P_0}{\pi w^2} \int_{-\infty}^{x_0} \exp\left[\frac{-2x^2}{w^2}\right] dx \int_{-\infty}^{\infty} \exp\left[\frac{-2y^2}{w^2}\right] dy \quad (9.2.2)$$

$$= \sqrt{\frac{2}{\pi}} \frac{P_0}{w} \left[ \int_{-\infty}^0 \exp\left[\frac{-2x^2}{w^2}\right] dx + \int_0^{x_0} \exp\left[\frac{-2x^2}{w^2}\right] dx \right] \quad (9.2.3)$$

$$= \sqrt{\frac{2}{\pi}} \frac{P_0}{w} \left[ \frac{w}{2} \sqrt{\frac{\pi}{2}} + \frac{w}{2} \sqrt{\frac{\pi}{2}} \int_0^{\sqrt{2}x_0/w} \exp[-t^2] dt \right] \quad (9.2.4)$$

$$= \frac{P_0}{2} \left[ 1 + \text{erf}\left(\frac{\sqrt{2}x_0}{w}\right) \right]. \quad (9.2.5)$$

where  $\text{erf}(t_0) \equiv \frac{2}{\sqrt{\pi}} \int_0^{t_0} \exp[-t^2] dt$ . The power on the right side is:

$$P_{right} = \frac{P_0}{2} \left[ 1 - \text{erf}\left(\frac{\sqrt{2}x_0}{w}\right) \right]. \quad (9.2.6)$$

We create a normalized yaw as

$$\text{YAW} = \frac{P_{left} - P_{right}}{P_0} = \text{erf}\left(\frac{\sqrt{2}x_0}{w}\right). \quad (9.2.7)$$

Using the Taylor series expansion of the error function, we have a first order estimate for the relationship between normalized yaw and beam displacement  $x_0$  for a beam of diameter(??)  $w$ :

$$\frac{x_0}{\text{YAW}} \approx \frac{w}{2} \sqrt{\frac{\pi}{2}}. \quad (9.2.8)$$

The same equation holds true for pitch.

### 9.3 ABCD matrix formalism

For the input beam model and for the Input Optics beam drift calibrations, the ABCD matrix formalism is a useful tool to propagate a Gaussian beam. I choose to ignore the fact that the MC beam passes through the substrate of MC3 on its way to the Faraday. I also treat the beam splitter as a flat mirror and ignore the presence of its substrate. I use the thickness of the large optic substrates,  $t = 0.01$  m, and account for index of refraction effects when passing through optics. Signs of radii of curvature are defined per the front face of the optic; for example, all main LIGO optics have a positive  $R$ .

For a beam that strikes a flat interface and exits at a curved interface (ie. forward-going transmission through RM):

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ (n_2 - n_1)/Rn_1 & n_2/n_1 \end{bmatrix} \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & n_1/n_2 \end{bmatrix} \quad (9.3.1)$$

For a beam that strikes a curved interface and exits at a flat interface (ie. transmission through ETM):

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & n_2/n_1 \end{bmatrix} \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ (n_1 - n_2)/-Rn_2 & n_1/n_2 \end{bmatrix} \quad (9.3.2)$$

For a beam that strikes a flat interface, travels through the substrate, reflects off the back of a curved interface, travels through substrate and exits at the original flat interface (ie. single bounce

off RM):

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & n_2/n_1 \end{bmatrix} \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 2/R & 1 \end{bmatrix} \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & n_1/n_2 \end{bmatrix} \quad (9.3.3)$$

Finally, for prompt reflection off a curved interface (ie. reflection off MMTs):

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -\frac{2}{R} & 1 \end{bmatrix} \quad (9.3.4)$$

and for propagation a distance  $d$  through vacuum:

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix}. \quad (9.3.5)$$

For each of these  $n_1 = 1$  is the index of refraction of vacuum and  $n_2 = 1.44963$  is the index of refraction of the fused silica used for the optics. Table 10-1 shows the radii of curvature of each of the optics for both sites.

### 9.3.1 Beam Drift Calibration

We use the ABCD matrix formulation to convert pitch and yaw data of WFS3 and WFS4 into a position and angle at the Faraday isolator. The basic relationship between beam displacement and angle at one location to displacement and angle at another location is given by:

$$\begin{bmatrix} x_1 \\ x'_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} x_0 \\ x'_0 \end{bmatrix} \quad (9.3.6)$$

For this application, we want to relate the beam positions on the WFS,  $x_3$  and  $x_4$ , to the beam position and angle,  $x_{FI}$  and  $x'_{FI}$ , at the Faraday isolator. Using only the top equation of Eq. 9.3.6 since the WFS are sensitive to beam position only and not angle, we can write a new relation

$$\begin{bmatrix} x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} A_3 & B_3 \\ A_4 & B_4 \end{bmatrix} \begin{bmatrix} x_{FI} \\ x'_{FI} \end{bmatrix} \quad (9.3.7)$$

where  $A_3, B_3$  and  $A_4, B_4$  are the A and B ABCD matrix elements for the beam paths from the Faraday isolator to WFS3 and WFS4, respectively. Taking the inverse and writing  $x_3$  and  $x_4$  as a function of the pitch and yaw recorded by the WFS (see Appendix 9.2), the useful equation is

$$\begin{bmatrix} x_{FI} \\ x'_{FI} \end{bmatrix} = \begin{bmatrix} A_3 & B_3 \\ A_4 & B_4 \end{bmatrix}^{-1} \begin{bmatrix} w_3 & 0 \\ 0 & w_4 \end{bmatrix} \frac{1}{2} \sqrt{\frac{\pi}{2}} \begin{bmatrix} DOF_3 \\ DOF_4 \end{bmatrix} \quad (9.3.8)$$

where  $w_3$  and  $w_4$  are the radii of the beam at each WFS and DOF can mean PIT or YAW.

#### 9.4 Mode cleaner pole

Optical cavities act as low pass filters for intensity variations of the light sent into them. The model for an intensity noise transfer function of a cavity is that of a single pole:

$$\frac{E_{after}}{E_{before}} = \frac{1}{1 + s/s_0} = \frac{s_0}{s_0 - s} \quad (9.4.1)$$

where  $s$  is a complex parameter. However, we are interested in only purely sinusoidal variations in intensity so we let  $s$  be purely imaginary,  $s = i\omega$ , where  $\omega$  is an angular frequency.

We measured the intensity noise transfer function of the Livingston mode cleaner upon completion of the Enhanced LIGO Input Optics upgrade. We modulated the intensity of the laser light going into the MC by injecting a swept-sine excitation in L1:PSL-ISS\_EXC and measured the power variation of the light in two places: before and after the mode cleaner. We used a single photodetector (PDA55) in order to eliminate the PD response, and therefore made the measurement twice. We ensured there was 1V DC on the PD in both locations.

Figure 9-1 shows the transfer function data and the fit (to both magnitude and phase simultaneously). The fit has a pole frequency of  $f_p = 4762$  Hz. The  $1/e$  ringdown time of the mode cleaner is therefore  $\tau = 1/4\pi f_{MC} = 16.7$   $\mu$ s and the finesse is  $\mathcal{F} = \text{FSR}/2f_p = 1282$ .

#### 9.5 Carrier Mode Matching into the Interferometer

The mode matching into the interferometer can be measured by comparing the power reflected from the interferometer during a full lock to the power reflected with a single bounce off the RM.

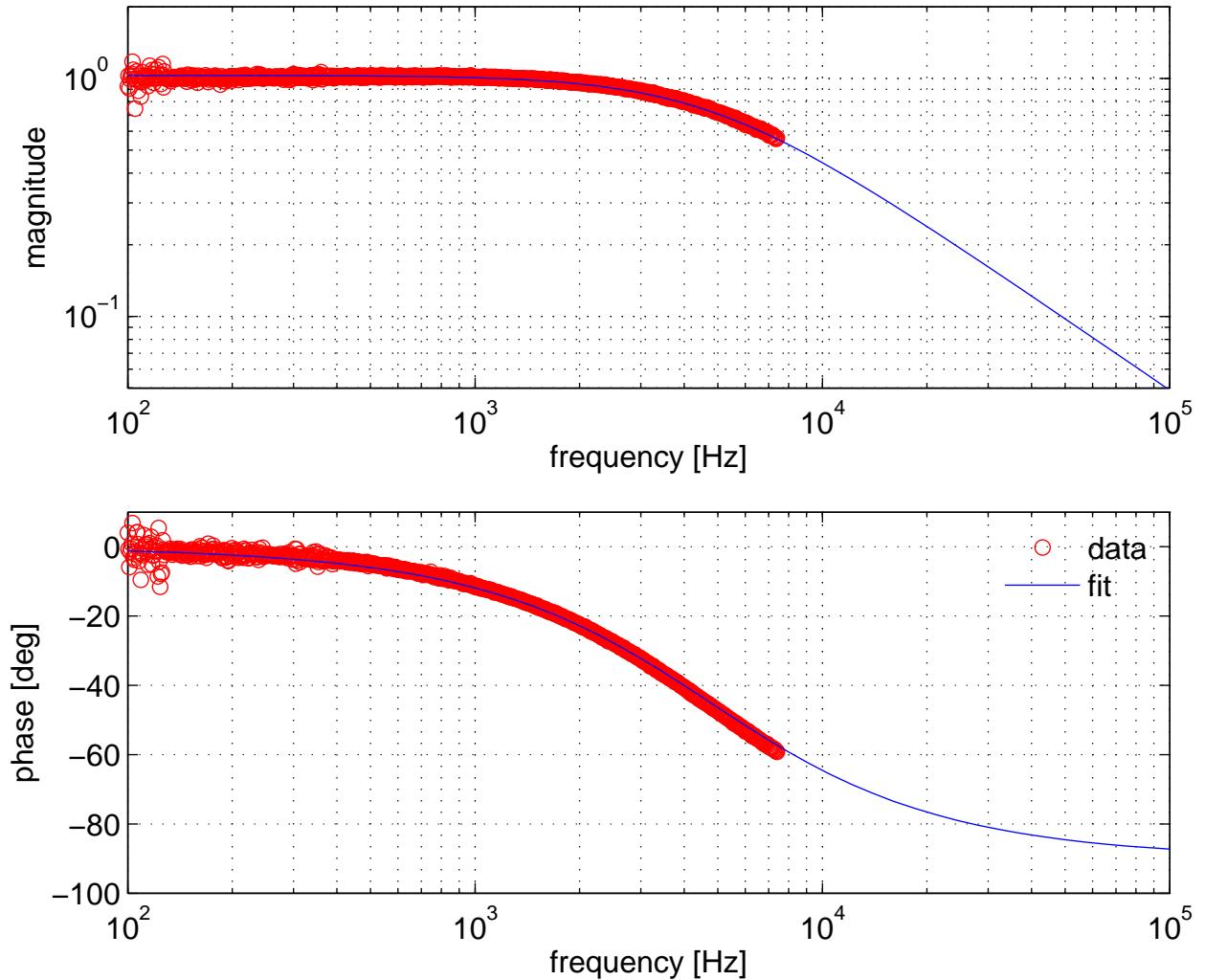


Figure 9-1. Livingston mode cleaner intensity noise transfer function. Red open circles are data; solid blue line is a single pole fit. Relating fit parameters to the model, the pole frequency is  $f_{MC} = 4762$  Hz.

First, we will look at the interferometer visibility—what percentage of power sent to the interferometer is reflected by it.

Then, we'll consider the sources of reflected light and deduce from the visibility measurements just how much of the reflected light is due to a mode mismatch.

For Livingston, we will see that the visibility is a very close approximation of the mode mismatch. However, at Hanford, much of the reflected light is due to an impedance mismatch, so further analysis of the visibility is presented to determine the mode matching.

### 9.5.1 Interferometer visibility

The visibility is a measure of how much carrier light is reflected from the locked interferometer compared to how much carrier light is sent in. Ideally, all of the light should be coupled into the interferometer. However, any mode mismatch of the input beam to the cavity or any mismatch of interferometer losses to PRM reflectivity (impedance mismatch, see Section 9.5.2) will cause carrier light to be reflected. The visibility summarizes the compound effect of all of these sources of reflected light.

To measure the visibility, we need to know only a few numbers. We must have a measure of how much light is sent to the interferometer for normalization purposes and we must have a measure of the DC reflected power when the interferometer is not locked (all light is reflected off of the RM) and when it is locked. The visibility is then given by:

$$\text{visibility} = 1 - \frac{P_{\text{REFL}_{\text{locked}}}}{P_{\text{REFL}_{\text{unlocked}}}} \frac{P_{\text{IN}_{\text{unlocked}}}}{P_{\text{IN}_{\text{locked}}}} \quad (9.5.1)$$

We have two measures of how much light is being sent into the interferometer and several of how much light is reflected. L1: I00-MC\_PWR\_IN is a pick off of the light on the PSL table just before it enters vacuum and L1: I00-MC\_TRANS\_SUM is a pick off of the light just after the MC. L1:LSC-REFL\_DC is a record of the power at the REFL port as seen by one of the LSC REFL PDs. There are others, like WFS3 sum, WFS4 sum, and the trigger PD that we could also look at. Together, these channels tell a story about the percentage of incoming light rejected by the interferometer.

An example for LLO is shown in Figure 9-2. The lock stretch ends at  $t = 5$  min. Note that the amount of reflected light is increasing up to the end of the lock as the interferometer is losing stability. When lock is lost, the common mode servo kicks the mode cleaner out of lock too, and the MC trans power drops to 0. About 15 seconds later the MC relocks and then the power into it increases. About 15 seconds after that, at 5.5 minutes, the MC WFS turn on, improving the alignment of the MC to the input beam and we see another step in the power getting through the MC. The interferometer is still not locked, so all light (except for 2.7%) is reflected off of the

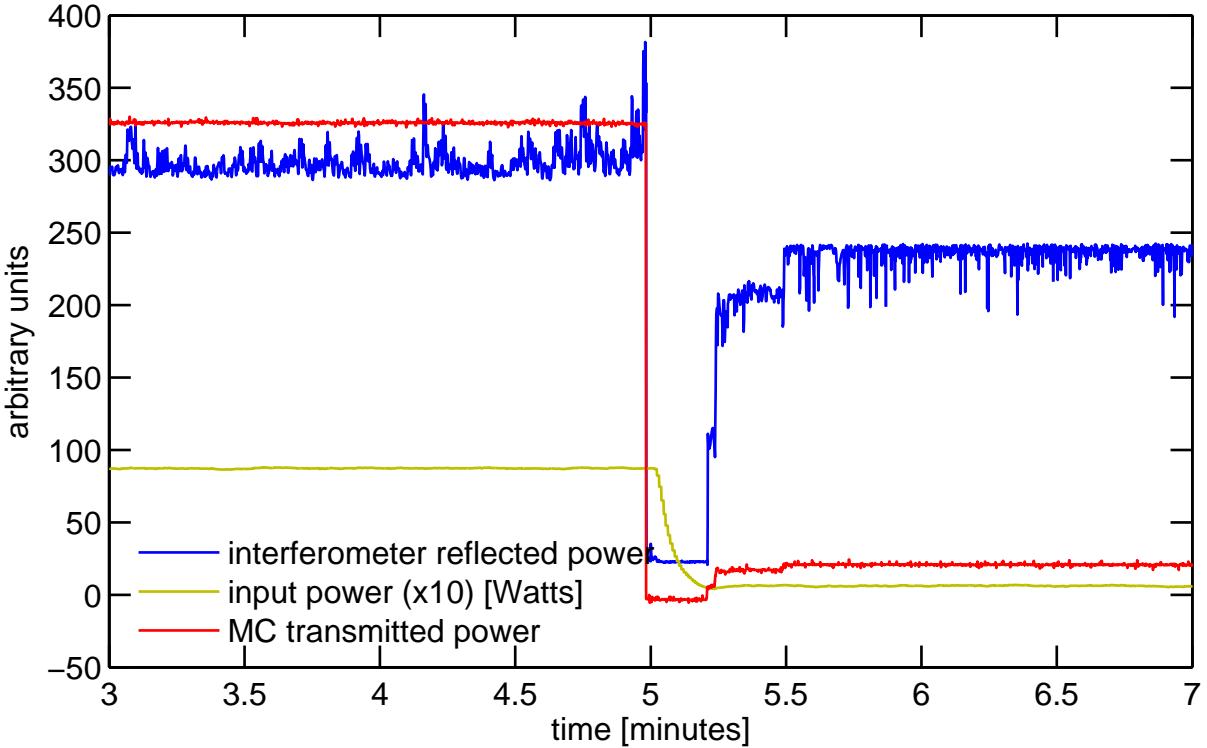


Figure 9-2. End of an 8.7 W lock at Livingston on Feb. 23, 2010. The mode cleaner re-locks at 0.5 W about 20 seconds after lock loss and then the power is increased to 2 W. Comparison of the minimum interferometer reflected power during lock and the maximum reflected power out of lock provides a measure of interferometer mode matching.

recycling mirror, as seen by REFL DC. The downward spikes are the result of interferometer flashes, instances of all mirrors lining up correctly to let some light in.

The reason we look at two records of the light sent into the interferometer is because from one power to the next, each gives a different ratio of power increase. Since we don't have a good reason to trust one more than the other, we'll take the average of the two ratios for use in the visibility calculation. In this example, PWR IN says that the locked state compared to the unlocked state had  $87/6.5 = 13.4$  times more power. However, MC TRANS says that ratio is  $326/21 = 15.5$ . We'll meet in the middle and use a locked to unlocked input power ratio of 14.5.

Then, we will look at the average minimum of REFL when the interferometer is locked (here, about 290) and the average maximum when it is not (241) for a measure of power reflected. The dark value, of course, must be subtracted from each—in this case it's -22.5. The

Segment	Date	Time of day	PWR IN	REFL DC	Visibility: trigger PD
0169	July 31, 2009	afternoon	7.2 W	92.1%	92.0%
1009	Nov. 20, 2009	evening	5.7 W	91.7%	91.8%
1380	Jan 6, 2010	evening	5.5 W	92.3%	
1630	Feb 23, 2010	morning	8.7 W	92.1%	91.8%
2180	May 20, 2010	evening	11.6 W	91.6%	91.7%
2223	May 27, 2010	evening	11.5 W	91.9%	91.2%
2424	June 29, 2010	night	9.0 W	91.9%	
2999	Sep. 14, 2010	evening	9.7 W	91.6%	
3159	Oct. 2, 2010	morning	4.1 W	91.8%	
3272	Oct. 20, 2010	night	7.1 W	91.5%	92.1%

Table 9-1. Livingston

Segment	Date	Time of day	PWR IN	REFLPD1	WFS3 DC	WFS4 DC	Visibility: trigger PD
0128	July 20, 2009	morning	7.9 W	75.5%	94.0%	93.9%	94.8%
0685	Nov. 9, 2009	evening	13.9 W	72.5%	93.9%	94.1%	94.7%
0999	Jan 1, 2010	morning	14.0 W	81.1%	93.8%	94.2%	94.4%
2026	July 9, 2010	night	20.3 W	80.1%	92.6%	92.6%	93.4%
2340	Oct 5, 2010	night	20.1 W	78.0%	91.6%	92.1%	93.3%

Table 9-2. Hanford

visibility is thus:

$$\text{visibility} = 1 - \frac{290 - 22.5}{15.5(241 - 22.5)} = 92.1\%. \quad (9.5.2)$$

The exact same calculation made for a pseudo-random sampling of Livingston lock stretches is shown in Table 9-1.

## 9.5.2 Impedance matching

The lower limit for the amount of power in the interferometer's reflected beam can be calculated simply based on the reflectivities of the mirrors. A cavity is impedance matched when the input and output couplers have the same reflectivity—all light sent at the cavity is coupled into it. If there's a difference between the reflectivities of the two mirrors, the cavity is over- or under-coupled and light will be reflected.

Treating the interferometer arms as a single mirror that forms a cavity with the RM, we want the RM transmission to match the transmission of the arms. This must include all losses in the

interferometer such as absorption, scattering, and ETM transmission. Design estimates resulted in an RM power transmission of 2.7%.

If losses don't equal 2.7% in reality, then we have an impedance mismatch and we will see light at the REFL port. We can measure the losses implicitly via the carrier recycling gain and therefore provide a good estimate of power in REFL due to impedance mismatch. The amplitude reflectivity of the interferometer is:

$$r_{ifo} = \frac{r_{arms} - r_{rm}}{1 - r_{rm}r_{arms}}. \quad (9.5.3)$$

The composite arm cavity amplitude reflectivity is  $r_{arms}$  and the RM amplitude reflectivity is  $r_{rm} = \sqrt{0.973}$ .

It is not so simple to know what  $r_{arms}$  is in practice. A precise measure of all losses in the arms would be needed. Therefore, we turn to writing  $r_{arms}$  in terms of a quantity that we can measure quite well, the power recycled Michelson carrier gain  $G_{cr}$ :

$$G_{cr} = g_{cr}^2 = \left[ \frac{t_{rm}}{1 - r_{rm}r_{arms}} \right]^2. \quad (9.5.4)$$

Solving for  $r_{arms}$  as a function of

Figure 9-3 shows  $R_{ifo} = r_{ifo}^2$  as a function of  $G_{cr}$ . Curves for a couple different RM reflectivities are shown to give an idea of how the interferometer reflectivity would change for minor mis-approximations of the RM reflectivity.

Experimentally, the recycling gain is measured as

$$G_{cr} = g_{cr}^2 = T_{rm} \frac{\text{NPTRX} + \text{NPTRY}}{2}, \quad (9.5.5)$$

which assumes the NPTRs are calibrated such that NPTRX=NPTRY=1 during a single arm lock. Figure 9-4 shows the measured carrier recycling gain for each interferometer during the S6 science segments.

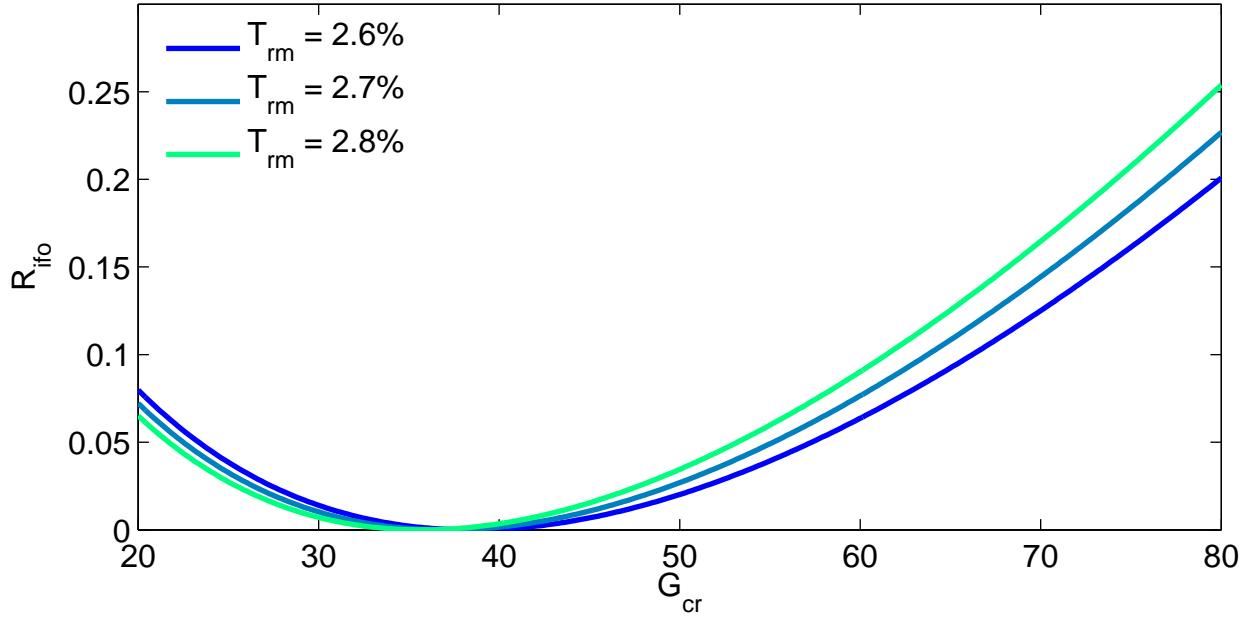


Figure 9-3. Interferometer reflectivity due to impedance mismatch. The percentage of power incident on the RM that is reflected by the interferometer is a function of carrier recycling gain and RM reflectivity. The carrier recycling gain is 39 for LLO and 75 for Hanford. The recycling mirror power transmission is nominally 2.7%.

Figure 9-4. Carrier recycling gain during S6.

### 9.5.3 Mode matching

Any difference between the amount of light seen in REFL and what's expected from impedance mismatch can be contributed to imperfect mode matching.

For Livingston, the story is pretty straightforward. The interferometer is nearly perfectly impedance matched, so all light at the REFL port is due to imperfect mode matching. Thus, the LLO mode mismatch during S6 was 8%.

We can't quite put together a clean case for Hanford yet as there's so much uncertainty in both the recycling gain and the visibility numbers. The carrier recycling gain may be as low as 53 or as high as 75. The visibility is either 77.5% or 93.5%. Table 9-3 summarizes the possibilities.

	$G_{cr}$	impedance mismatch	visibility	mode mismatch
LLO	39	0.07%	$91.84\% \pm 0.07\%$	8%
LHO	53	4.0%	93.5%	2.5%
			77.5%	18.5%
	75	18.4%	93.5%	impossible
			77.5%	4.1%

Table 9-3. Summary of interferometer parameters used to determine mode matching.

## CHAPTER 10

### APPENDIX B

#### 10.1 Parameters

#### 10.2 Optical lever open loop transfer function

#### 10.3 Seismic contributions to optical lever spectra

#### 10.4 Misaligned cavity axis

Here I provide the geometric argument that shows how to calculate the tilt  $\alpha$  and displacement  $a$  of a cavity as a function of mirror misalignment. Cavity tilt is defined by the angle formed between the line that connects the two beam spots (as given by Eq. 5.1.1) and the line joining the centers of the mirrors. Cavity displacement uses the same two lines, yet is defined by the distance between them at the location of the waist of the resonant spatial mode. Based on pure geometry, the cavity displacement and tilt are:

$$\begin{bmatrix} a \\ \alpha \end{bmatrix} = \frac{1}{L} \begin{bmatrix} z_2 & z_1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad (10.4.1)$$

where  $z_i$  is the distance to the waist from mirror  $i$  calculated as:

$$z_1 = \frac{g_2(1-g_1)L}{g_1+g_2-2g_1g_2} \quad (10.4.2)$$

$$z_2 = L - z_1. \quad (10.4.3)$$

Clearly, we can combine Eqs. (5.1.1) and (10.4.1) to arrive at an equation directly relating mirror tilt to cavity displacement and tilt:

$$\begin{bmatrix} a \\ \alpha \end{bmatrix} = \frac{1}{1-g_1g_2} \begin{bmatrix} g_2z_2+z_1 & z_2+g_1z_1 \\ -g_2+1 & -1+g_1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}. \quad (10.4.4)$$

#### 10.5 Power in a misaligned cavity

I'll show how to calculate the power in a cavity as a function of cavity axis displacement and tilt. Combined with the results of Eq. 10.4.4 we determine how the power build-up in a cavity depends on a single mirror's angular displacement.

Table 10-1. Mirror ROCs.

optic	L1 ROC [km]	H1 ROC [km]	reference
MC1	0.01725		IO As-Built
MC2	80		
MC3	0.01725		
MMT1	6.76		
MMT2	3.16		
MMT3	25.16		
RM	15.78	14.40	Garilynn's site
BS	-189	-336	
ITMX	14.760	13.910	
ITMY	14.520	13.600	
ETMX	8.730	7.260	
ETMY	8.720	7.320	

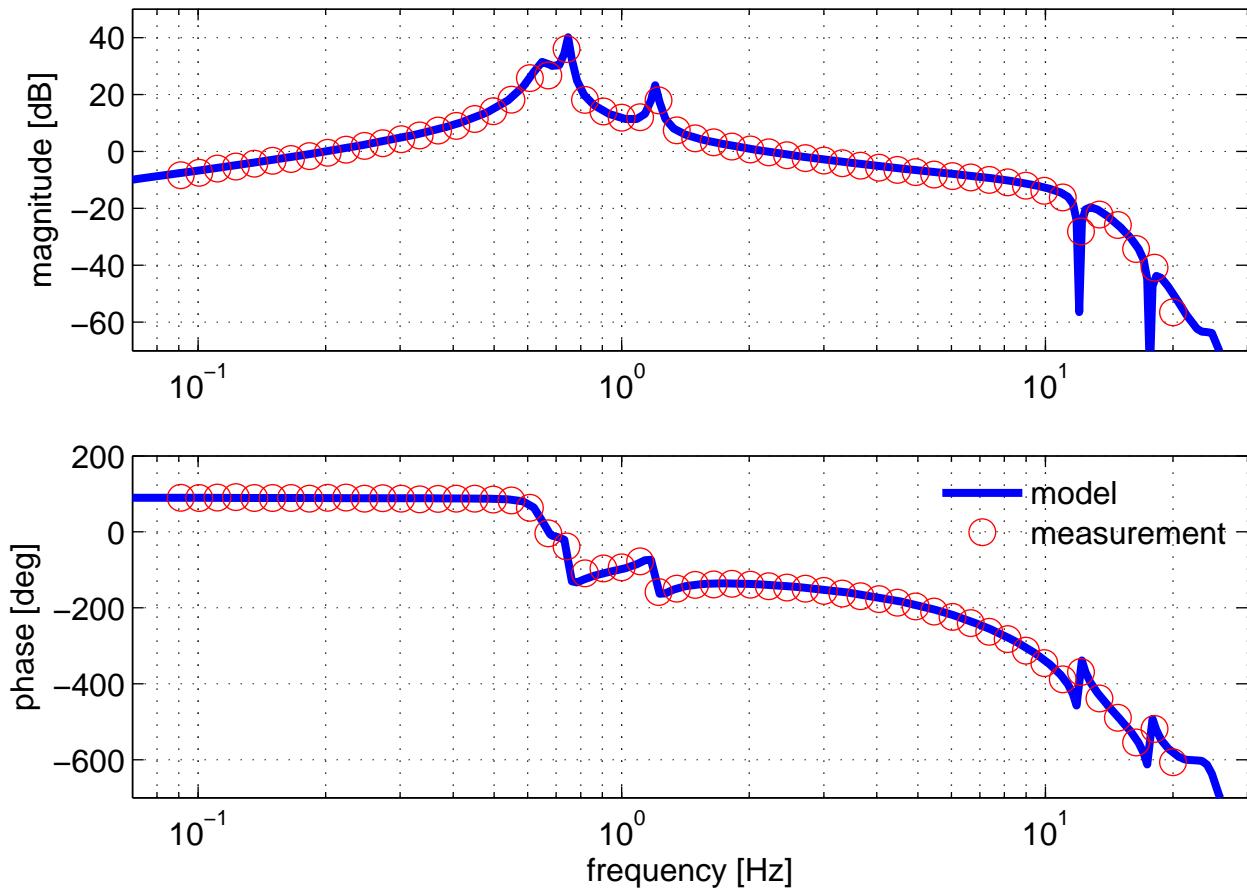


Figure 10-1. ETMX pitch optical lever open loop transfer function. Uses the filters in the oplev servo filter bank, only (no coil output filters). The model of the plant is tuned to match the data, resulting in a pitch resonance of 0.65 Hz and a damping factor of  $\gamma = 0.02$ . The UGF is at 2.2 Hz and the phase margin is  $38^\circ$ .

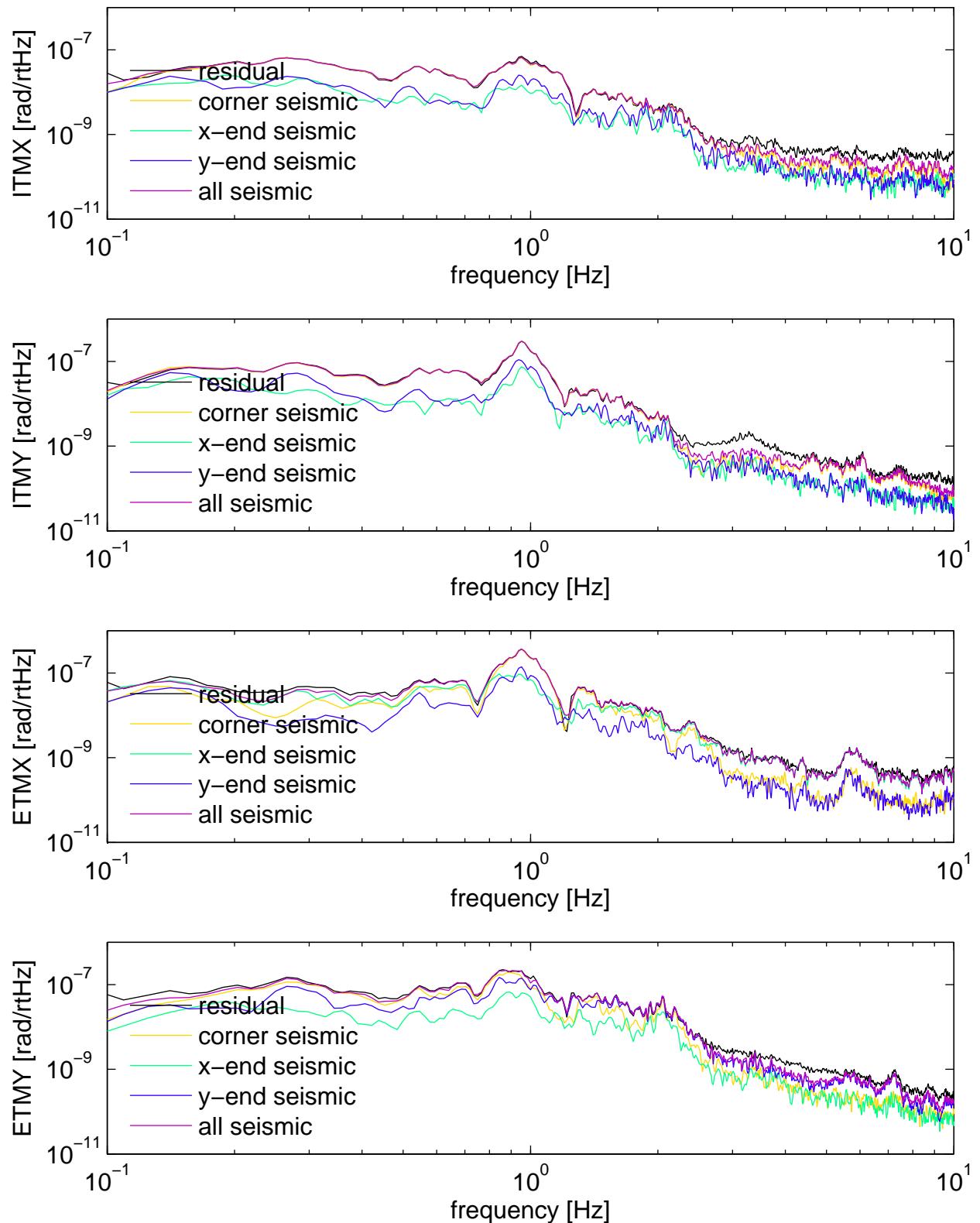


Figure 10-2. Contribution of sesimic noise to optical lever error signal. The interferometer was unlocked and optical lever and OSEM AC damping present.

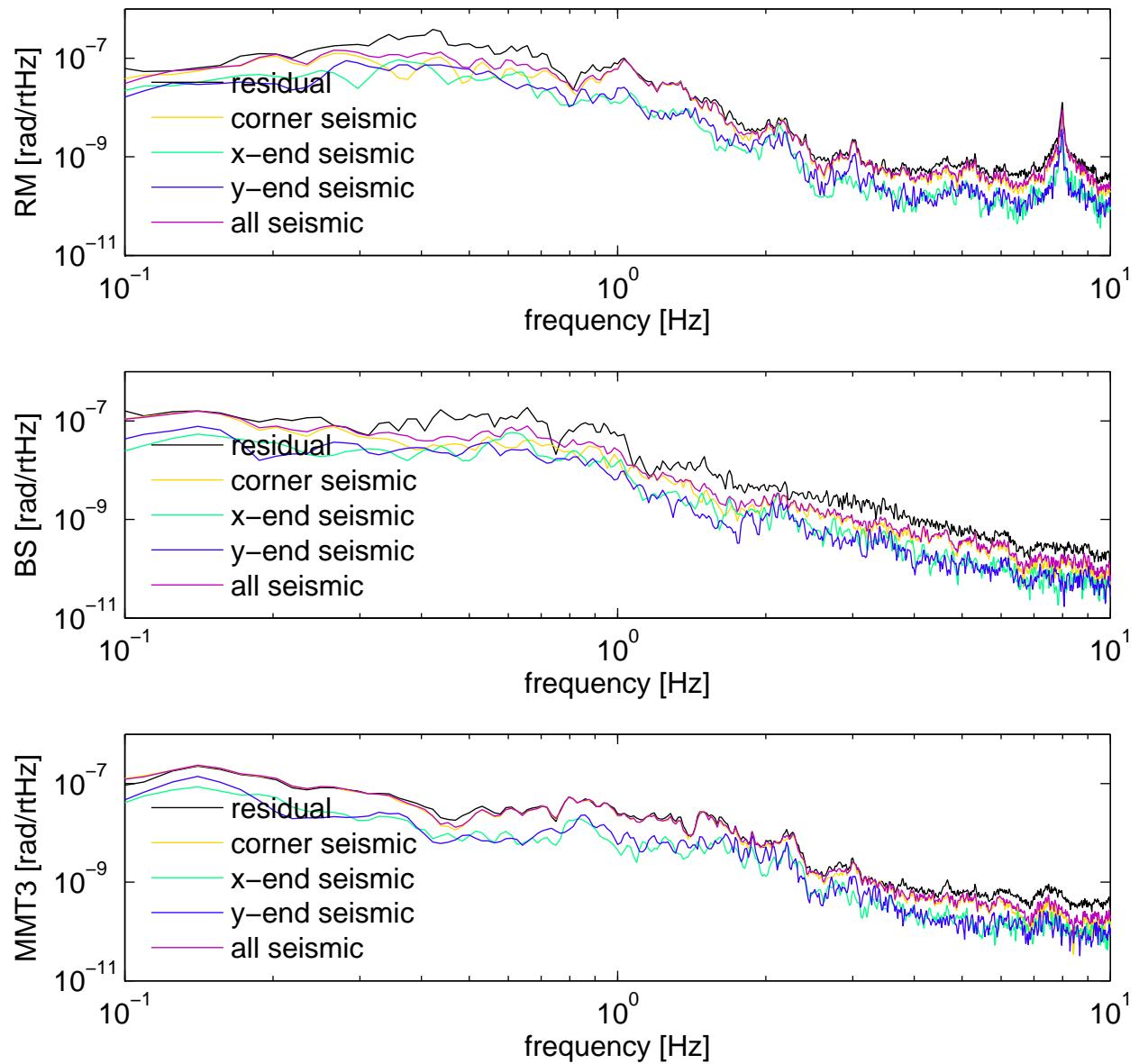


Figure 10-3. Contribution of sesismic noise to optical lever error signal. The interferometer was unlocked and optical lever and OSEM AC damping present.

The field of a lowest-order Gaussian laser beam along one axis at the beam waist is:

$$\psi(x) = U_0(x) = \left[ \frac{2}{\pi w_0^2} \right]^{1/4} \exp \left[ - \left[ \frac{x}{w_0} \right]^2 \right] \quad (10.5.1)$$

where  $w_0$  is the beam waist radius and  $U_0$  is the lowest-order Hermite polynomial. The Hermite polynomials are orthonormal, ie.  $\langle U_i | U_j \rangle = \delta_{ij}$ . For example, the next to lowest order polynomial is:

$$U_1(x) = \left( \frac{2}{\pi w_0^2} \right)^{1/4} \frac{2x}{w_0} \exp [-(x/w_0)^2] = \frac{2x}{w_0} U_0(x) \quad (10.5.2)$$

### 10.5.1 Displaced cavity

The field of a cavity with a *displaced* z-axis at the cavity waist is:

$$\psi'(x) = \psi(x - a) \quad (10.5.3)$$

$$= U_0(x - a) \quad (10.5.4)$$

$$= c_0 U_0(x) + c_1 U_1(x) + c_2 U_2(x) + \dots \quad (10.5.5)$$

$$(10.5.6)$$

where  $a$  is the displacement of the axis and  $c_i$  are constants.

We want to know  $c_0$ , the projection of the displaced cavity field onto the beam field:

$$c_0 = \langle \psi | \psi' \rangle \quad (10.5.7)$$

$$= \int_{-\infty}^{\infty} \psi(x) \psi'(x) dx \quad (10.5.8)$$

$$= \exp [-a^2 / 2w_0^2] \quad (10.5.9)$$

The power in this mode is the square of the overlap of the two fields:

$$P_0 = |\langle \psi | \psi' \rangle|^2 \quad (10.5.10)$$

$$= \exp [-[a/w_0]^2] \quad (10.5.11)$$

For the purpose of wavefront sensing, we need to know the amplitude,  $c_1$ , of the first order  $U_1$  field. This can be approximated as demonstrated in Anderson [38] using the Taylor series

expansion of the exponential in  $\psi'(x) = U_0(x - a)$ , assuming a displacement  $a$  that's small compared to waist size  $w_0$ .

$$\psi'(x) = \left[ \frac{2}{\pi w_0^2} \right]^{1/4} \exp \left[ - \left[ \frac{x-a}{w_0} \right]^2 \right] \quad (10.5.12)$$

$$= \left[ \frac{2}{\pi w_0^2} \right]^{1/4} \left[ 1 - \left[ \frac{x-a}{w_0} \right]^2 + \mathcal{O}(a^4) \right] \quad (10.5.13)$$

$$= \left[ \frac{2}{\pi w_0^2} \right]^{1/4} \left[ \frac{2xa}{w_0^2} \left[ 1 - \frac{x^2}{w_0^2} + \dots \right] + \left[ 1 - \frac{x^2}{w_0^2} + \frac{1}{2} \frac{x^4}{w_0^4} - \dots \right] + \mathcal{O}(a^2) \right] \quad (10.5.14)$$

$$= \left[ \frac{2}{\pi w_0^2} \right]^{1/4} \left[ 1 + \frac{2xa}{w_0^2} + \mathcal{O}(a^2) \right] \exp \left[ - \left[ \frac{x}{w_0} \right]^2 \right] \quad (10.5.15)$$

$$= U_0(x) + \frac{a}{w_0} U_1(x) + \dots \quad (10.5.16)$$

Notice that here we find  $c_0 = 1$ , which is consistent with the exact result of Eq. 10.5.9 when we apply our  $a^2 \approx 0$  approximation. We find that the amplitude of the first order Hermite-Gauss field for a displaced cavity is

$$c_1 = a/w_0. \quad (10.5.17)$$

### 10.5.2 Tilted cavity

The field of a cavity with a *tilted* z-axis at the cavity waist is a tad more complex to derive. We assume the tilt,  $\alpha$ , is small such that  $\sin \alpha \approx \alpha$  and  $\cos \alpha \approx 1$ . Also, we assume the beam divergence angle,  $\theta_0 = \lambda/\pi w_0$ , is small such that the wavefronts near the waist can be considered parallel to one another.

Here, the important quantity to consider is the phase of the cavity field at the cross-section of the beam waist. The phase is either advanced or retarded compared to that of the beam:

$$\psi'(x) = \psi(x') \exp[-ikz'] \quad (10.5.18)$$

$$\approx \psi(x \cos \alpha) \exp[-ikx \sin \alpha] \quad (10.5.19)$$

$$\approx \psi(x) \exp[-ikx \alpha] \quad (10.5.20)$$

$$= U_0(x) \exp[-ikx \alpha] \quad (10.5.21)$$

where  $k = 2\pi/\lambda$  and  $\lambda$  is the wavelength of the laser light.

The overlap of the fields of the beam and tilted cavity is  $\exp[-\alpha^2/2\theta_0^2]$ . Therefore the power is:

$$P_0 = \exp[-(\alpha/\theta_0)^2]. \quad (10.5.22)$$

An expansion of the exponential in Eq. 10.5.21 for a small tilt  $\alpha$  gives:

$$\psi'(x) = U_0(x)[1 + ikx\alpha + \mathcal{O}(\alpha^2)] \quad (10.5.23)$$

$$= U_0(x) + \frac{ik\alpha w_0}{2} U_1(x) + \mathcal{O}(\alpha^2). \quad (10.5.24)$$

Therefore, the amplitude of the first order Hermite-Gauss field for a tilted cavity is

$$c_1 = ik\alpha w_0/2. \quad (10.5.25)$$

### 10.5.3 Displaced and tilted cavity

The most general case, of course, is to have a cavity axis that is both displaced *and* tilted at the beam waist:

$$\psi'(x) = \psi(x-a) \exp[-ik(x-a)\alpha]. \quad (10.5.26)$$

We find:

$$\langle \psi | \psi' \rangle = \exp\left[-\frac{a^2}{2w_0^2}\right] \exp\left[-\frac{\alpha^2}{2\theta_0^2}\right] \exp\left[-\frac{ia\alpha}{x_0\theta_0}\right] \quad (10.5.27)$$

and

$$P_0 = \exp\left[-\frac{a^2}{w_0^2}\right] \exp\left[-\frac{\alpha^2}{\theta_0^2}\right]. \quad (10.5.28)$$

## 10.6 Initial DC alignment of the interferometer

After any kind of in-vacuum work, the DC alignment of the mirrors is usually too poor for the interferometer to lock. A bootstrapping process of tweaking the alignment by hand is necessary, assuming the mirrors start out pointing in generally the right direction, as is usually the case. As pointed out in 4.4, the QPDs at the end stations are the fixed reference points for the overall alignment, so this process begins with making sure the light reaches them. We then adjust

the rest of the mirrors to maximize power build-up in the arms and to maximze spatial overlap of the light reflected from each arm.

An outline of the process is presented here. “Misalign” means to intentionally point a mirror so far away from any known good positions as to eliminate it from the configuration. “Align” and “restore” mean to bring a mirror or configuration to the best known position(s). Centering the beam on a mirror is accomplished by using the suspension cage surrounding the mirror as a reference. Camera images and QPD readback provide the signals used for beam centering.

### **X-arm**

- restore the x-arm (misalign RM, ITMY, and ETMY, align ITMX and ETMX)
- use ITMX to center the beam on QPDX
- use ETMX to center the beam on ITMX
- with x-arm locked, use MMT3 to maximize the x-arm power build-up (NPTRX, can expect about 95%)
- save the MMT3, ITMX, and ETMX alignment settings

### **Y-arm**

- restore the y-arm (misalign ITMX and ETMX, align ITMY and ETMY)
- use ITMY to center the beam on QPDY
- use ETMY to center the beam on ITMY
- with y-arm locked, use BS to maximize the y-arm power build-up (NPTRY, can expect about 90%)
- save the BS, ITMY, and ETMY alignment settings

### **Relative x-arm and y-arm**

- note AS beam position on camera while toggling between x-arm and y-arm locks
- use ETMs to align the two AS beams
- restore the Michelson (misalign ETMs, align ITMs)
- use BS to make AS port as dark as possible
- re-do y-arm alignment if ambitious

### **Recycling mirror**

- restore the PRM (misalign ETMs, align ITMs and RM)
- use RM to center beam on ETMY cage

### **Restore full interferometer—off you go!**

## 10.7 Photodiodes

The basic photoconductive photodiode is depicted in Fig. 7-1. A negative voltage applied to the anode, represented by the line, does not yield any current across the photodiode until electrons are released by the energy of photons striking the diode. Electrons flow in the direction of the cathode which is connected to ground, producing a current

$$i_\gamma = \frac{q_e}{hv} P \epsilon \quad (10.7.1)$$

where  $q_e$  is the electron charge,  $h$  is Planck's constant,  $v$  is the frequency of the incident light,  $P$  is the power of the light, and  $\epsilon$  is the quantum efficiency of the diode. The quantity  $q_e/hv$  is known as the *responsivity*. For LIGO where  $\lambda = 1064$  nm, the responsivity is 0.86 A/W.

## 10.8 Channel names

**finish this or skip!** It is often perplexing why there are so many channels with almost identical names. And just what those names mean can also sometimes be elusive. The best advice I have to offer about how to figure out for one's self what the root of the channel name conveys about the data it represents is to browse the MEDM screens. The MEDM screens pictorially show the flow of which channels are derived from others, and whether they sit before or after an excitation point, for example. They also sometimes offer hints as to exactly what calculation is done under the scene in the front-end code to compute new channels.

The topic I want to cover here is the difference between the OUT, OUT16, OUTPUT, and OUTMON channel name extensions. They appear in all of the subsystems, and it is crucial to realize that some are good for analyzing data and some good for getting only a sense in real-time of what's going on. Some are typically recorded to disk, and some are not. These concepts extend to other common name extensions as well.

## 10.9 Seismic spectra

There are three seismometers at LLO for the purpose of monitoring the ground motion at the corner station and two end stations. The calibration for the digitally collected data is  $2.4 \times 10^{-9}$  m/s/count. As stated in the introduction of Ch. 6, I include here snapshots of the ground motion

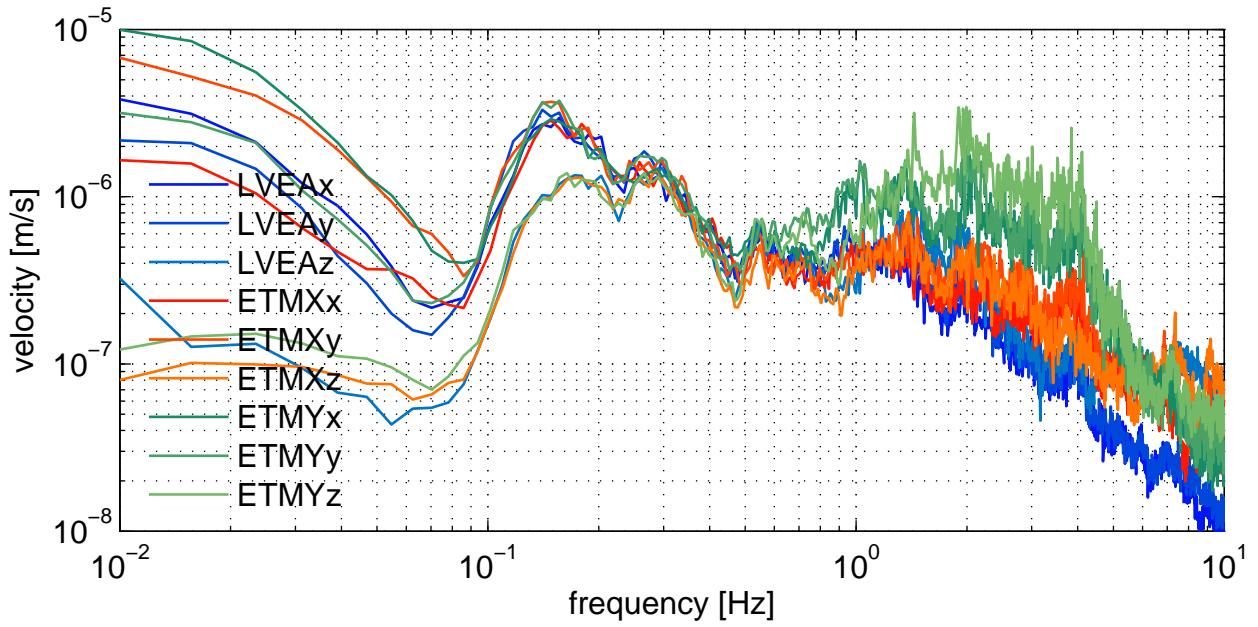


Figure 10-4. Ground motion at time of optical lever spectra when the interferometer was unlocked. GPS time 956751915.

at the time of ground motion-sensitive measurements. Each spectra represents 30 minutes of data centered around the time of the measurement. There are three degrees of freedom for each seismometer,  $x$ ,  $y$ , and  $z$ . They are aligned with the interferometer's  $x$  and  $y$  arm coordinate system.

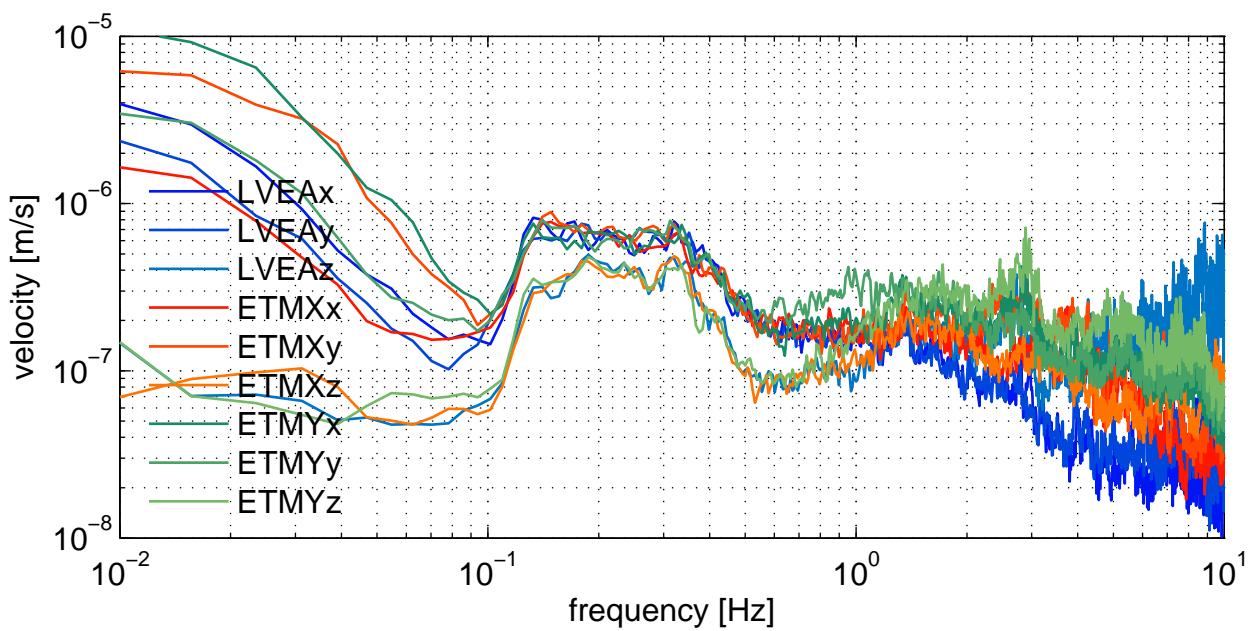


Figure 10-5. Ground motion at time of input beam motion impression measurement. GPS time 971128215.

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