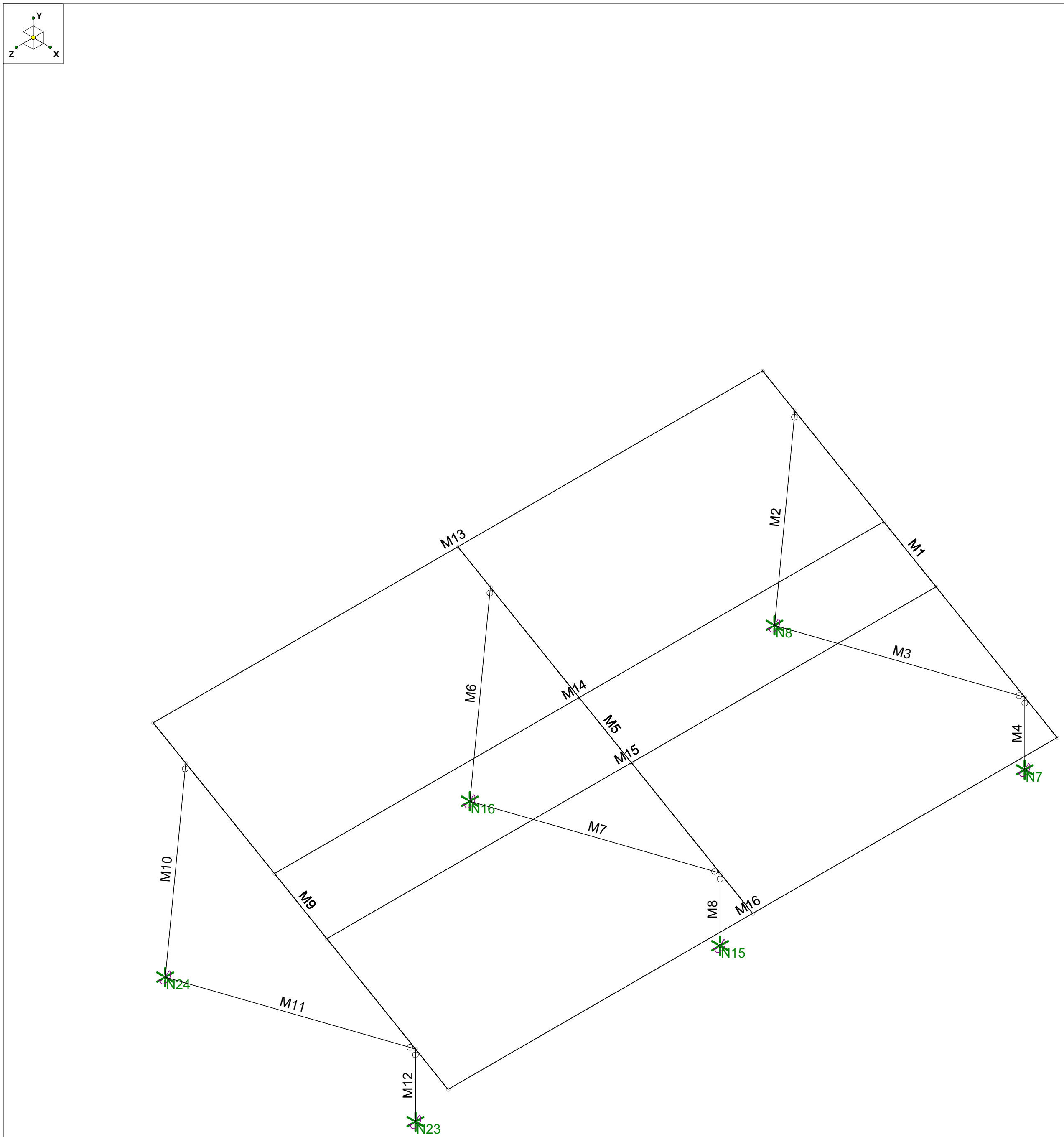


Schletter, Inc.	Standard PVMax Racking System	30° Tilt w/ Seismic Design
HCV	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

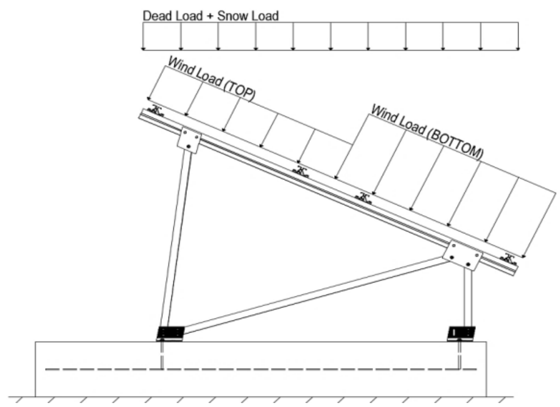
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	2000 mm	Height =	1900 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 2
Module Tilt = 30°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads

Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 16.49 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.73
C_e = 0.90
C_t = 1.20

2.3 Wind Loads

Design Wind Speed, V = 130 mph — Exposure Category = C
Height < 15 ft — Importance Category = II

Peak Velocity Pressure, q_z = 26.53 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.150	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.850	
$Cf-_{TOP, OUTER PURLIN}$	=	-2.600	
$Cf-_{TOP, INNER PURLIN}$	=	-2.000	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.100	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.07	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	**Diagonal Struts**	Location	**Front Reactions**	Location
M13	Top	M3	Outer	N7	Outer
M14	Mid-Top	M7	Inner	N15	Inner
M15	Mid-Bottom	M11	Outer	N23	Outer
M16	Bottom				

Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

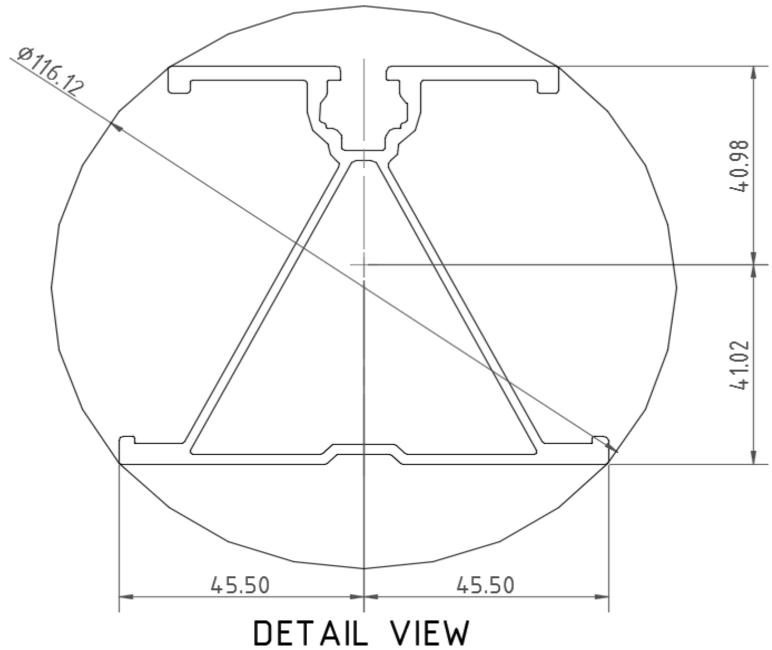
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

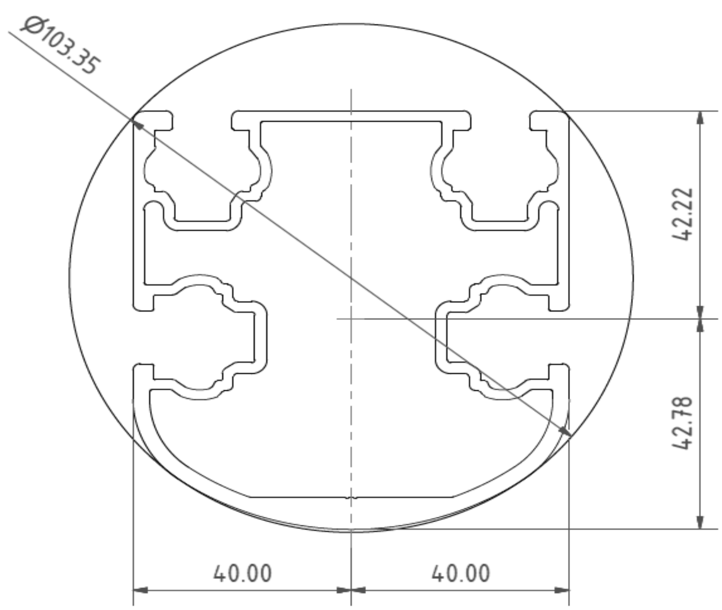
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	102	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.483	k-ft
M_z =	0.295	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	79%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

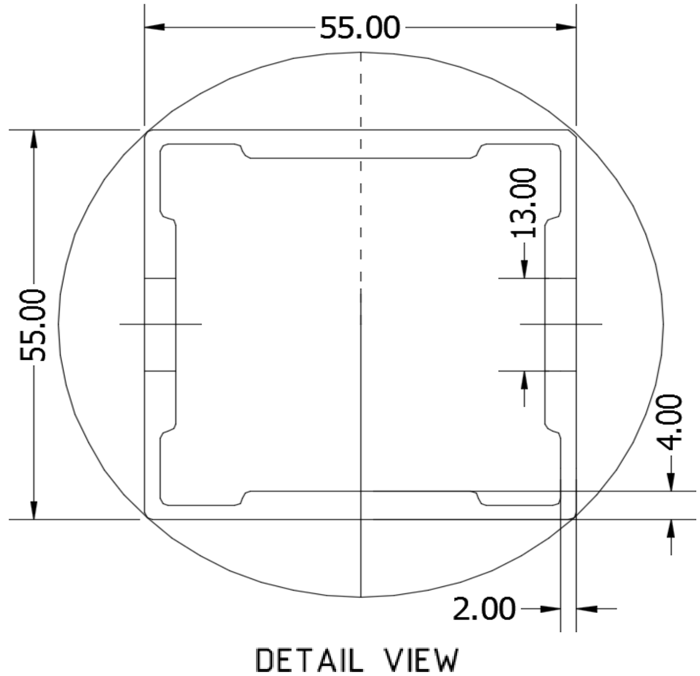
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	104.56	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.00	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-3.298	k-ft
M_z =	0.000	k-ft
P_n =	-0.956	k
$M_{y\ allowable}$ =	3.422	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	98%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

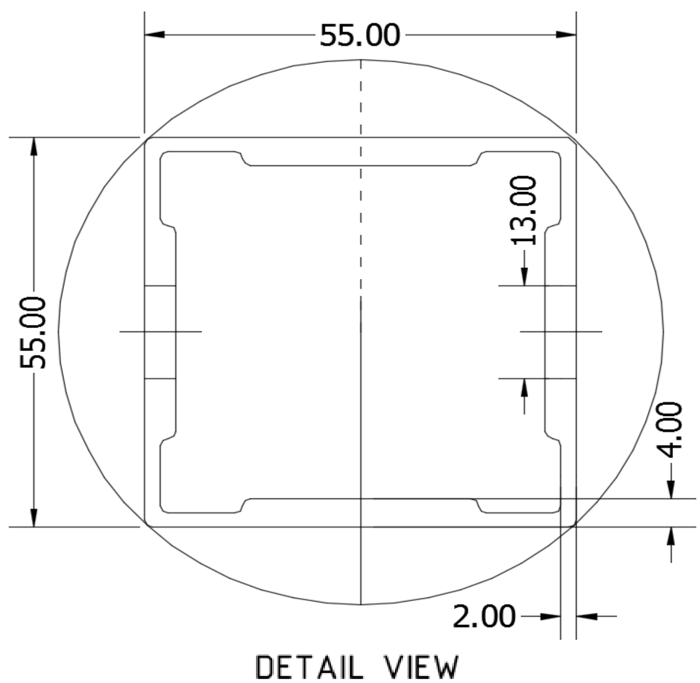
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	24.80	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.572	k-ft
P_n =	0.119	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	41%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

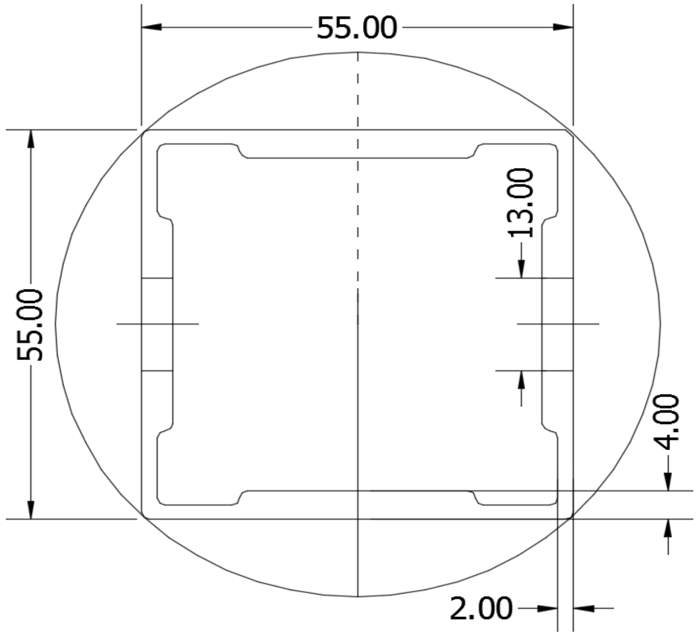
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	98.03	in
$\Phi F_{ty\ AXIAL}$ =	6.11	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.011	k-ft
M_z =	0.000	k-ft
P_n =	2.553	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	6.000	k
Utilization =	43%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	78.35	in
$\Phi F_{ty\ AXIAL}$ =	8.88	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.011	k-ft
M_z =	0.000	k-ft
P_n =	3.194	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	8.726	k
Utilization =	37%	



DETAIL VIEW

5. FOUNDATION DESIGN CALCULATIONS

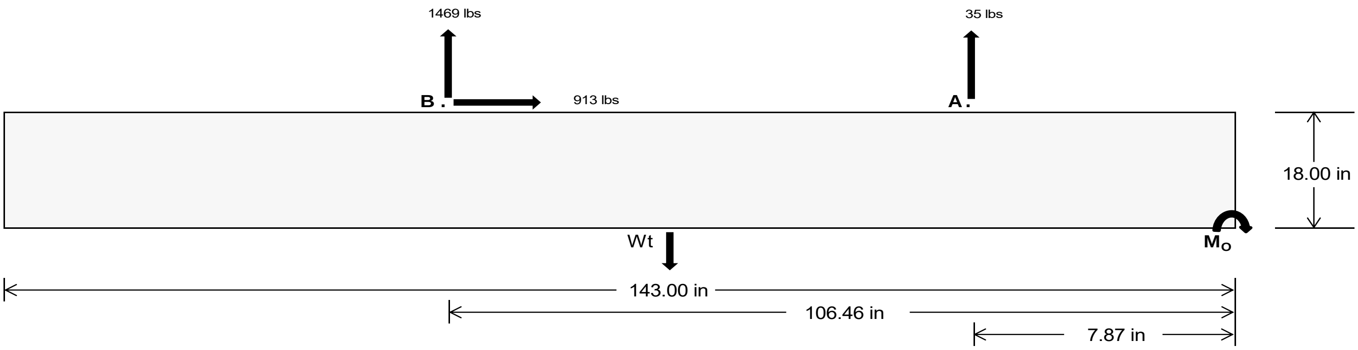
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	174.83	6381.89	k
Compressive Load =	3421.08	4948.58	k
Lateral Load =	379.25	3955.81	k
Moment (Weak Axis) =	0.74	0.27	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties	
Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

Footing Reinforcement
Use fiber reinforcing with (2) #5 rebar.

Overturning Check	
M_O =	173045.8 in-lbs
Resisting Force Required =	2420.22 lbs
S.F. =	1.67
Weight Required =	4033.70 lbs
Minimum Width =	35 in in
Weight Provided =	7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.

Sliding	
Force =	912.69 lbs
Friction =	0.4
Weight Required =	2281.72 lbs
Resisting Weight =	7559.64 lbs
Additional Weight Required =	0 lbs

Use a 143in long x 35in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion	
Sliding Force =	912.69 lbs
Cohesion =	130 psf
Area =	34.76 ft^2
Resisting =	3779.82 lbs
Additional Weight Required =	0 lbs

Use a 143in long x 35in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key	
Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	35 in	36 in	37 in	38 in
P_{ftg} = (145 pcf)(11.92 ft)(1.5 ft)(2.92 ft) =	7560 lbs	7776 lbs	7992 lbs	8208 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in
F_A	1191 lbs	1191 lbs	1191 lbs	1191 lbs	1246 lbs	1246 lbs	1246 lbs	1246 lbs	1702 lbs	1702 lbs	1702 lbs	1702 lbs	-71 lbs	-71 lbs	-71 lbs	-71 lbs
F_B	1176 lbs	1176 lbs	1176 lbs	1176 lbs	2073 lbs	2073 lbs	2073 lbs	2073 lbs	2314 lbs	2314 lbs	2314 lbs	2314 lbs	-2937 lbs	-2937 lbs	-2937 lbs	-2937 lbs
F_V	164 lbs	164 lbs	164 lbs	164 lbs	1652 lbs	1652 lbs	1652 lbs	1652 lbs	1346 lbs	1346 lbs	1346 lbs	1346 lbs	-1825 lbs	-1825 lbs	-1825 lbs	-1825 lbs
P_{total}	9927 lbs	10143 lbs	10359 lbs	10575 lbs	10878 lbs	11094 lbs	11310 lbs	11526 lbs	11575 lbs	11791 lbs	12007 lbs	12223 lbs	1528 lbs	1657 lbs	1787 lbs	1916 lbs
M	3136 lbs-ft	3136 lbs-ft	3136 lbs-ft	3136 lbs-ft	3043 lbs-ft	3043 lbs-ft	3043 lbs-ft	3043 lbs-ft	4302 lbs-ft	4302 lbs-ft	4302 lbs-ft	4302 lbs-ft	5442 lbs-ft	5442 lbs-ft	5442 lbs-ft	5442 lbs-ft
e	0.32 ft	0.31 ft	0.30 ft	0.30 ft	0.28 ft	0.27 ft	0.27 ft	0.26 ft	0.37 ft	0.36 ft	0.36 ft	0.35 ft	3.56 ft	3.28 ft	3.05 ft	2.84 ft
L/6	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft
f_{min}	240.2 psf	239.5 psf	239.0 psf	238.4 psf	268.9 psf	267.5 psf	266.1 psf	264.8 psf	270.7 psf	269.2 psf	267.8 psf	266.5 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	331.0 psf	327.9 psf	324.9 psf	322.1 psf	357.1 psf	353.2 psf	349.5 psf	346.0 psf	395.3 psf	390.4 psf	385.7 psf	381.3 psf	145.7 psf	137.7 psf	132.6 psf	129.4 psf

Maximum Bearing Pressure = 395 psf
Allowable Bearing Pressure = 1500 psf

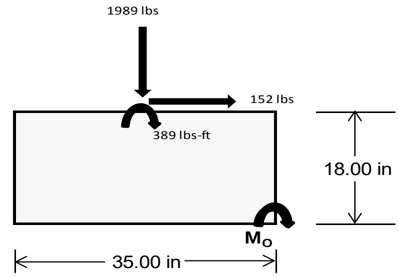
Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 2283.6 ft-lbs
Resisting Force Required = 1565.92 lbs
S.F. = 1.67
Weight Required = 2609.87 lbs
Minimum Width = 35 in in
Weight Provided = 7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	35 in			35 in			35 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	319 lbs	617 lbs	191 lbs	787 lbs	1989 lbs	688 lbs	138 lbs	181 lbs	11 lbs
F_V	213 lbs	207 lbs	218 lbs	155 lbs	152 lbs	170 lbs	214 lbs	208 lbs	216 lbs
P_{total}	9678 lbs	9976 lbs	9549 lbs	9696 lbs	10898 lbs	9597 lbs	2875 lbs	2917 lbs	2747 lbs
M	832 lbs-ft	816 lbs-ft	846 lbs-ft	617 lbs-ft	618 lbs-ft	664 lbs-ft	831 lbs-ft	814 lbs-ft	836 lbs-ft
e	0.09 ft	0.08 ft	0.09 ft	0.06 ft	0.06 ft	0.07 ft	0.29 ft	0.28 ft	0.30 ft
L/6	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft
f_{min}	229.2 psf	238.8 psf	224.7 psf	242.4 psf	277.0 psf	236.8 psf	33.5 psf	35.7 psf	29.5 psf
f_{max}	327.7 psf	335.3 psf	324.8 psf	315.5 psf	350.1 psf	315.4 psf	131.9 psf	132.1 psf	128.5 psf

Maximum Bearing Pressure = 350 psf
Allowable Bearing Pressure = 1500 psf

Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 143in long x 31in wide x 18in tall ballast foundation and fiber reinforcing with (2) #5 rebar.

5.3 Foundation Anchors

Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

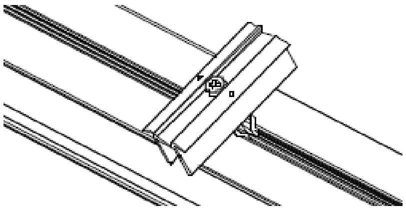
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

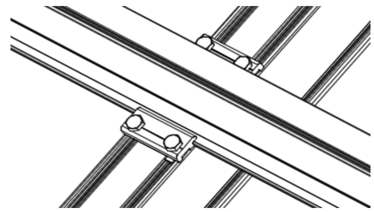
Fastening of Modules to Purlins

Maximum Uplifting Force =	0.762 k
Allowable Uplift =	1.214 k
Utilization =	63%



Fastening of Purlins to Girders

Maximum Uplifting Force =	2.310 k
Allowable Uplift =	4.357 k
Utilization =	53%



6.2 Strut Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut

Maximum Axial Load =	2.632 k
M12 Bolt Capacity =	12.808 k
Strut Bearing Capacity =	7.421 k
Utilization =	35%

Rear Strut

Maximum Axial Load =	4.292 k
M12 Bolt Capacity =	12.808 k
Strut Bearing Capacity =	7.421 k
Utilization =	58%

Diagonal Strut

Maximum Axial Load =	2.676 k
M12 Bolt Shear Capacity =	12.808 k
Strut Bearing Capacity =	7.421 k
Utilization =	36%

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

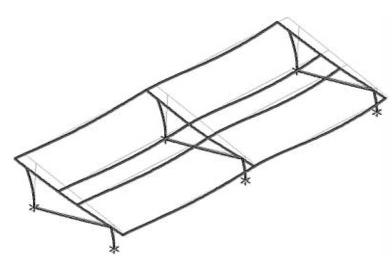
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	60.93 in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$
	1.219 in
Max Drift, Δ_{MAX} =	0.794 in

0.794 ≤ 1.219, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 102 in

J = 0.432

282.18

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 27.9 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

$\varphi F_L St$= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in³

$M_{max}St$ = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 102

J = 0.432

179.449

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.0

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in³

$M_{max}Wk$ = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:

3.4.14

L_b = 104.56 in
J = 1.08
179.85

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.0 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

Weak Axis:

3.4.14

L_b = 104.56
J = 1.08
190.335

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 28.9

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Used

Rb/t = 18.1

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$S2 = C_t$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 31.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 35.2

m = 0.68

C_0 = 41.067

Cc = 43.717

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 73.8

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

3.4.18

h/t = 16.2

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40

Cc = 40

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt=	29.0 ksi		φF_LWk=	33.3 ksi	
Ix =	984962 mm^4		Iy =	923544 mm^4	
	2.366 in^4			2.219 in^4	
y =	43.717 mm		x =	40 mm	
Sx =	1.375 in^3		Sy =	1.409 in^3	
M_{max}St =	3.323 k-ft		M_{max}Wk =	3.904 k-ft	

Compression

3.4.9

b/t = 16.2

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

b/t = 7.4

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 31.09 ksi

φF_L= 31.09 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.87952

φF_L= φcc(Bc-Dc*λ)

φF_L= 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 98.03 in

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4 ksi

Weak Axis:

3.4.14

L_b = 98.03

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

3.4.16.1

Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

$\varphi F_L = 1.17\varphi yFcy$

$\varphi F_L =$ 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L St =$ 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St$ = 1.460 k-ft

$\varphi F_L Wk =$ 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk$ = 1.460 k-ft

Compression

3.4.7

λ = 2.26776

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.89749

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

$\varphi F_L =$ 6.10803 ksi

3.4.9

b/t = 24.5
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

b/t = 24.5
S1 = 12.21
S2 = 32.70
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 6.11 ksi
A = 663.99 mm^2
1.03 in^2
P_{max} = 6.29 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = __**55x55**__

Strong Axis:

3.4.14

L_b = 78.35 in
J = 0.942
122.273

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 29.8 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

Weak Axis:

3.4.14

L_b = 78.35
J = 0.942
122.273

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 29.8

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.8125

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83375

φF_L= (φccFcy)/(λ²)

φF_L= 8.88278 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 8.88 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 9.14 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-9.843	-9.843	0	0
2	M14	Y	-9.843	-9.843	0	0
3	M15	Y	-9.843	-9.843	0	0
4	M16	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-5.454	-5.454	0	0
2	M14	Y	-5.454	-5.454	0	0
3	M15	Y	-5.454	-5.454	0	0
4	M16	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-46.866	-46.866	0	0
2	M14	Y	-46.866	-46.866	0	0
3	M15	Y	-46.866	-46.866	0	0
4	M16	Y	-46.866	-46.866	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-100.114	-100.114	0	0
2	M14	y	-100.114	-100.114	0	0
3	M15	y	-161.053	-161.053	0	0
4	M16	y	-161.053	-161.053	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	226.345	226.345	0	0
2	M14	y	174.112	174.112	0	0
3	M15	y	95.761	95.761	0	0
4	M16	y	95.761	95.761	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	7.874	7.874	0	0
2	M14	Z	7.874	7.874	0	0
3	M15	Z	7.874	7.874	0	0
4	M16	Z	7.874	7.874	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	818.238	2	1219.98	2	.658	1	.003	1	0	1	0	1
2		min	-994.367	3	-1549.622	3	-34.731	5	-.208	4	0	1	0	1
3	N7	max	.032	9	1021.267	1	-.888	12	-.002	12	0	1	0	1
4		min	-.235	2	-70.992	5	-291.734	4	-.572	4	0	1	0	1
5	N15	max	.013	9	2631.601	1	0	3	0	3	0	1	0	1
6		min	-2.375	2	-134.482	3	-274.611	4	-.548	4	0	1	0	1
7	N16	max	2806.208	2	3806.597	2	0	3	0	3	0	1	0	1
8		min	-3042.933	3	-4909.148	3	-34.785	5	-.21	4	0	1	0	1
9	N23	max	.046	14	1021.267	1	13.209	1	.026	1	0	1	0	1
10		min	-.235	2	-10.848	3	-281.74	5	-.557	4	0	1	0	1
11	N24	max	818.238	2	1219.98	2	-.057	12	0	12	0	1	0	1
12		min	-994.367	3	-1549.622	3	-35.523	5	-.21	4	0	1	0	1
13	Totals:	max	4439.839	2	10376.012	2	0	3						
14		min	-5031.822	3	-8164.571	3	-946.834	4						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	76.414	4	411.476	2	-9.827	12	0	15	.211	1	0	4
2			min	5.56	12	-705.969	3	-178.238	1	-.015	2	.016	12	0	3
3		2	max	75.469	1	286.621	2	-7.855	12	0	15	.13	4	.568	3
4			min	5.56	12	-497.321	3	-136.398	1	-.015	2	.005	10	-.33	2
5		3	max	75.469	1	161.765	2	-5.884	12	0	15	.076	5	.939	3
6			min	5.56	12	-288.672	3	-94.558	1	-.015	2	-.046	1	-.541	2
7		4	max	75.469	1	36.91	2	-3.912	12	0	15	.042	5	1.113	3
8			min	5.56	12	-80.024	3	-52.718	1	-.015	2	-.116	1	-.635	2
9		5	max	75.469	1	128.624	3	-.466	10	0	15	.01	5	1.091	3
10			min	5.56	12	-87.946	2	-35.046	4	-.015	2	-.146	1	-.611	2
11		6	max	75.469	1	337.272	3	30.962	1	0	15	-.007	12	.871	3
12			min	1.627	15	-212.801	2	-28.763	5	-.015	2	-.136	1	-.469	2
13		7	max	75.469	1	545.921	3	72.801	1	0	15	-.006	12	.453	3
14			min	-8.514	5	-337.657	2	-25.762	5	-.015	2	-.087	1	-.209	2
15		8	max	75.469	1	754.569	3	114.641	1	0	15	.004	2	.169	2
16			min	-19.659	5	-462.512	2	-22.761	5	-.015	2	-.068	4	-.161	3
17		9	max	75.469	1	963.217	3	156.481	1	0	15	.129	1	.664	2
18			min	-30.804	5	-587.367	2	-19.76	5	-.015	2	-.087	5	-.972	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	75.469	1	1171.865	3	198.321	1	.003	14	.297	1	1.278	2
20			min	5.56	12	-712.223	2	-124.318	14	-.015	2	.008	12	-1.98	3
21		11	max	75.469	1	587.367	2	-5.945	12	.015	2	.136	4	.664	2
22			min	5.56	12	-963.217	3	-156.481	1	0	15	0	3	-.972	3
23		12	max	75.469	1	462.512	2	-3.973	12	.015	2	.067	4	.169	2
24			min	5.56	12	-754.569	3	-114.641	1	0	15	-.006	3	-.161	3
25		13	max	75.469	1	337.657	2	-2.002	12	.015	2	.031	5	.453	3
26			min	5.56	12	-545.921	3	-72.801	1	0	15	-.087	1	-.209	2
27		14	max	75.469	1	212.801	2	.182	3	.015	2	0	15	.871	3
28			min	5.38	15	-337.272	3	-40.604	4	0	15	-.136	1	-.469	2
29		15	max	75.469	1	87.946	2	10.878	1	.015	2	-.007	12	1.091	3
30			min	-3.005	5	-128.624	3	-30.078	5	0	15	-.146	1	-.611	2
31		16	max	75.469	1	80.024	3	52.718	1	.015	2	-.004	12	1.113	3
32			min	-14.15	5	-36.91	2	-27.078	5	0	15	-.116	1	-.635	2
33		17	max	75.469	1	288.672	3	94.558	1	.015	2	.002	3	.939	3
34			min	-25.295	5	-161.765	2	-24.077	5	0	15	-.094	4	-.541	2
35		18	max	75.469	1	497.321	3	136.398	1	.015	2	.063	1	.568	3
36			min	-36.44	5	-286.621	2	-21.076	5	0	15	-.104	5	-.33	2
37		19	max	75.469	1	705.969	3	178.238	1	.015	2	.211	1	0	1
38			min	-47.585	5	-411.476	2	-18.076	5	0	15	-.122	5	0	3
39	M14	1	max	48.716	4	469.924	2	-10.182	12	.013	3	.294	4	0	4
40			min	2.924	12	-574.655	3	-185.475	1	-.015	2	.018	12	0	3
41		2	max	45.292	1	345.069	2	-8.211	12	.013	3	.199	4	.467	3
42			min	2.924	12	-415.338	3	-143.635	1	-.015	2	.009	10	-.385	2
43		3	max	45.292	1	220.213	2	-6.239	12	.013	3	.118	5	.785	3
44			min	2.924	12	-256.021	3	-101.796	1	-.015	2	-.019	1	-.652	2
45		4	max	45.292	1	95.358	2	-4.268	12	.013	3	.066	5	.951	3
46			min	2.924	12	-96.704	3	-68.913	4	-.015	2	-.095	1	-.801	2
47		5	max	45.292	1	62.613	3	-1.352	10	.013	3	.016	5	.967	3
48			min	-6.325	5	-31.624	1	-56.235	4	-.015	2	-.132	1	-.832	2
49		6	max	45.292	1	221.93	3	23.724	1	.013	3	-.007	12	.833	3
50			min	-17.47	5	-154.353	2	-47.89	5	-.015	2	-.13	1	-.745	2
51		7	max	45.292	1	381.247	3	65.564	1	.013	3	-.006	12	.548	3
52			min	-28.615	5	-279.209	2	-44.889	5	-.015	2	-.096	4	-.54	2
53		8	max	45.292	1	540.564	3	107.404	1	.013	3	.002	10	.113	3
54			min	-39.76	5	-404.064	2	-41.889	5	-.015	2	-.119	4	-.218	2
55		9	max	45.292	1	699.881	3	149.244	1	.013	3	.115	1	.239	1
56			min	-50.905	5	-528.919	2	-38.888	5	-.015	2	-.153	5	-.473	3
57		10	max	78.703	4	859.198	3	191.084	1	.013	3	.295	4	.781	2
58			min	2.924	12	-653.775	2	-130.107	14	-.015	2	.007	12	-1.209	3
59		11	max	67.558	4	528.919	2	-5.59	12	.015	2	.199	4	.239	1
60			min	2.924	12	-699.881	3	-149.244	1	-.013	3	0	3	-.473	3
61		12	max	56.413	4	404.064	2	-3.618	12	.015	2	.115	4	.113	3
62			min	2.924	12	-540.564	3	-107.404	1	-.013	3	-.006	3	-.218	2
63		13	max	45.292	1	279.209	2	-1.647	12	.015	2	.062	5	.548	3
64			min	2.924	12	-381.247	3	-70.066	4	-.013	3	-.088	1	-.54	2
65		14	max	45.292	1	154.353	2	.717	3	.015	2	.012	5	.833	3
66			min	2.924	12	-221.93	3	-57.388	4	-.013	3	-.13	1	-.745	2
67		15	max	45.292	1	31.624	1	18.116	1	.015	2	-.006	12	.967	3
68			min	2.924	12	-62.613	3	-48.164	5	-.013	3	-.132	1	-.832	2
69		16	max	45.292	1	96.704	3	59.956	1	.015	2	-.003	12	.951	3
70			min	.687	15	-95.358	2	-45.164	5	-.013	3	-.102	4	-.801	2
71		17	max	45.292	1	256.021	3	101.796	1	.015	2	.004	3	.785	3
72			min	-10.093	5	-220.213	2	-42.163	5	-.013	3	-.127	4	-.652	2
73		18	max	45.292	1	415.338	3	143.635	1	.015	2	.097	1	.467	3
74			min	-21.238	5	-345.069	2	-39.162	5	-.013	3	-.159	5	-.385	2
75		19	max	45.292	1	574.655	3	185.475	1	.015	2	.252	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-32.383	5	-469.924	2	-36.161	5	-.013	3	-.194	5	0	3
77	M15	1	max	89.012	5	664.225	2	-10.057	12	.015	2	.363	4	0	2
78			min	-48.054	1	-325.55	3	-185.434	1	-.011	3	.017	12	0	3
79		2	max	77.867	5	481.816	2	-8.086	12	.015	2	.253	4	.267	3
80			min	-48.054	1	-240.231	3	-143.594	1	-.011	3	.009	12	-.541	2
81		3	max	66.722	5	299.407	2	-6.115	12	.015	2	.157	5	.454	3
82			min	-48.054	1	-154.912	3	-101.755	1	-.011	3	-.019	1	-.91	2
83		4	max	55.577	5	116.998	2	-4.143	12	.015	2	.089	5	.56	3
84			min	-48.054	1	-69.594	3	-84.71	4	-.011	3	-.096	1	-1.107	2
85		5	max	44.433	5	15.725	3	-1.406	10	.015	2	.025	5	.585	3
86			min	-48.054	1	-65.411	2	-72.031	4	-.011	3	-.133	1	-1.131	2
87		6	max	33.288	5	101.044	3	23.765	1	.015	2	-.007	12	.53	3
88			min	-48.054	1	-247.82	2	-63.627	5	-.011	3	-.13	1	-.983	2
89		7	max	22.143	5	186.363	3	65.605	1	.015	2	-.006	12	.394	3
90			min	-48.054	1	-430.229	2	-60.626	5	-.011	3	-.117	4	-.663	2
91		8	max	10.998	5	271.682	3	107.445	1	.015	2	.001	10	.178	3
92			min	-48.054	1	-612.638	2	-57.626	5	-.011	3	-.155	4	-.171	2
93		9	max	.029	15	357.001	3	149.285	1	.015	2	.115	1	.494	2
94			min	-48.054	1	-795.047	2	-54.625	5	-.011	3	-.204	5	-.119	3
95		10	max	-3.616	12	442.32	3	191.125	1	.015	2	.361	4	1.331	2
96			min	-48.054	1	-977.456	2	-138.184	14	-.011	3	.007	12	-.496	3
97		11	max	-3.616	12	795.047	2	-5.714	12	.011	3	.249	4	.494	2
98			min	-48.054	1	-357.001	3	-149.285	1	-.015	2	0	3	-.119	3
99		12	max	-3.616	12	612.638	2	-3.743	12	.011	3	.15	4	.178	3
100			min	-48.054	1	-271.682	3	-107.445	1	-.015	2	-.006	1	-.171	2
101		13	max	-3.616	12	430.229	2	-1.771	12	.011	3	.082	5	.394	3
102			min	-48.054	1	-186.363	3	-85.913	4	-.015	2	-.088	1	-.663	2
103		14	max	-3.616	12	247.82	2	.51	3	.011	3	.018	5	.53	3
104			min	-53.098	4	-101.044	3	-73.235	4	-.015	2	-.13	1	-.983	2
105		15	max	-3.616	12	65.411	2	18.075	1	.011	3	-.006	12	.585	3
106			min	-64.243	4	-15.725	3	-63.907	5	-.015	2	-.133	1	-1.131	2
107		16	max	-3.616	12	69.594	3	59.915	1	.011	3	-.003	12	.56	3
108			min	-75.388	4	-116.998	2	-60.906	5	-.015	2	-.126	4	-1.107	2
109		17	max	-3.616	12	154.912	3	101.755	1	.011	3	.004	3	.454	3
110			min	-86.533	4	-299.407	2	-57.906	5	-.015	2	-.165	4	-.91	2
111		18	max	-3.616	12	240.231	3	143.594	1	.011	3	.097	1	.267	3
112			min	-97.677	4	-481.816	2	-54.905	5	-.015	2	-.212	5	-.541	2
113		19	max	-3.616	12	325.55	3	185.434	1	.011	3	.252	1	0	2
114			min	-108.822	4	-664.225	2	-51.904	5	-.015	2	-.263	5	0	5
115	M16	1	max	83.508	5	608.531	2	-9.44	12	.01	1	.264	4	0	2
116			min	-85.258	1	-278.5	3	-178.789	1	-.013	3	.014	12	0	3
117		2	max	72.363	5	426.122	2	-7.469	12	.01	1	.176	4	.223	3
118			min	-85.258	1	-193.181	3	-136.949	1	-.013	3	.006	10	-.489	2
119		3	max	61.218	5	243.713	2	-5.497	12	.01	1	.109	5	.365	3
120			min	-85.258	1	-107.862	3	-95.109	1	-.013	3	-.045	1	-.805	2
121		4	max	50.073	5	61.304	2	-3.526	12	.01	1	.062	5	.426	3
122			min	-85.258	1	-22.543	3	-60.97	4	-.013	3	-.115	1	-.949	2
123		5	max	38.928	5	62.776	3	-.732	10	.01	1	.019	5	.407	3
124			min	-85.258	1	-121.105	2	-48.292	4	-.013	3	-.145	1	-.921	2
125		6	max	27.783	5	148.095	3	30.411	1	.01	1	-.007	12	.308	3
126			min	-85.258	1	-303.514	2	-41.789	5	-.013	3	-.136	1	-.72	2
127		7	max	16.638	5	233.414	3	72.251	1	.01	1	-.006	12	.128	3
128			min	-85.258	1	-485.923	2	-38.788	5	-.013	3	-.088	1	-.347	2
129		8	max	5.493	5	318.733	3	114.091	1	.01	1	.003	2	.198	2
130			min	-85.258	1	-668.332	2	-35.788	5	-.013	3	-.097	4	-.133	3
131		9	max	-3.709	15	404.052	3	155.931	1	.01	1	.128	1	.915	2
132			min	-85.258	1	-850.741	2	-32.787	5	-.013	3	-.128	5	-.474	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-5.699	12	489.371	3	197.771	1	.01	1	.295	1	1.805	2
134			min	-85.258	1	-1033.15	2	-130.817	14	-.013	3	.009	12	-.896	3
135		11	max	-4.28	15	850.741	2	-6.332	12	.013	3	.177	4	.915	2
136			min	-85.258	1	-404.052	3	-155.931	1	-.01	1	.002	12	-.474	3
137		12	max	-5.699	12	668.332	2	-4.36	12	.013	3	.096	4	.198	2
138			min	-85.258	1	-318.733	3	-114.091	1	-.01	1	-.004	3	-.133	3
139		13	max	-5.699	12	485.923	2	-2.389	12	.013	3	.047	5	.128	3
140			min	-85.258	1	-233.414	3	-72.251	1	-.01	1	-.088	1	-.347	2
141		14	max	-5.699	12	303.514	2	-.417	12	.013	3	.002	5	.308	3
142			min	-85.258	1	-148.095	3	-53.646	4	-.01	1	-.136	1	-.72	2
143		15	max	-5.699	12	121.105	2	11.429	1	.013	3	-.007	12	.407	3
144			min	-85.258	1	-62.776	3	-43.072	5	-.01	1	-.145	1	-.921	2
145		16	max	-5.699	12	22.543	3	53.269	1	.013	3	-.004	12	.426	3
146			min	-85.258	1	-61.304	2	-40.071	5	-.01	1	-.115	1	-.949	2
147		17	max	-5.699	12	107.862	3	95.109	1	.013	3	0	3	.365	3
148			min	-94.349	4	-243.713	2	-37.07	5	-.01	1	-.127	4	-.805	2
149		18	max	-5.699	12	193.181	3	136.949	1	.013	3	.065	1	.223	3
150			min	-105.494	4	-426.122	2	-34.07	5	-.01	1	-.149	5	-.489	2
151		19	max	-5.699	12	278.5	3	178.789	1	.013	3	.214	1	0	2
152			min	-116.639	4	-608.531	2	-31.069	5	-.01	1	-.18	5	0	5
153	M2	1	max	1030.378	2	2.058	4	.42	1	0	3	0	3	0	1
154			min	-1354.342	3	.499	15	-29.142	4	0	4	0	2	0	1
155		2	max	1030.907	2	1.987	4	.42	1	0	3	0	1	0	15
156			min	-1353.945	3	.482	15	-29.603	4	0	4	-.011	4	0	4
157		3	max	1031.436	2	1.916	4	.42	1	0	3	0	1	0	15
158			min	-1353.548	3	.465	15	-30.064	4	0	4	-.021	4	-.001	4
159		4	max	1031.966	2	1.845	4	.42	1	0	3	0	1	0	15
160			min	-1353.151	3	.449	15	-30.525	4	0	4	-.032	4	-.002	4
161		5	max	1032.495	2	1.774	4	.42	1	0	3	0	1	0	15
162			min	-1352.754	3	.432	15	-30.987	4	0	4	-.043	4	-.003	4
163		6	max	1033.024	2	1.703	4	.42	1	0	3	0	1	0	15
164			min	-1352.357	3	.415	15	-31.448	4	0	4	-.054	4	-.003	4
165		7	max	1033.554	2	1.632	4	.42	1	0	3	0	1	0	15
166			min	-1351.96	3	.399	15	-31.909	4	0	4	-.066	4	-.004	4
167		8	max	1034.083	2	1.561	4	.42	1	0	3	.001	1	-.001	15
168			min	-1351.563	3	.382	15	-32.37	4	0	4	-.077	4	-.005	4
169		9	max	1034.612	2	1.49	4	.42	1	0	3	.001	1	-.001	15
170			min	-1351.166	3	.365	15	-32.831	4	0	4	-.089	4	-.005	4
171		10	max	1035.141	2	1.419	4	.42	1	0	3	.001	1	-.001	15
172			min	-1350.769	3	.349	15	-33.293	4	0	4	-.101	4	-.006	4
173		11	max	1035.671	2	1.348	4	.42	1	0	3	.001	1	-.001	15
174			min	-1350.372	3	.332	15	-33.754	4	0	4	-.113	4	-.006	4
175		12	max	1036.2	2	1.277	4	.42	1	0	3	.002	1	-.002	15
176			min	-1349.975	3	.315	15	-34.215	4	0	4	-.125	4	-.007	4
177		13	max	1036.729	2	1.206	4	.42	1	0	3	.002	1	-.002	15
178			min	-1349.578	3	.29	12	-34.676	4	0	4	-.137	4	-.007	4
179		14	max	1037.259	2	1.135	4	.42	1	0	3	.002	1	-.002	15
180			min	-1349.181	3	.262	12	-35.137	4	0	4	-.15	4	-.007	4
181		15	max	1037.788	2	1.064	4	.42	1	0	3	.002	1	-.002	15
182			min	-1348.784	3	.234	12	-35.599	4	0	4	-.163	4	-.008	4
183		16	max	1038.317	2	.993	4	.42	1	0	3	.002	1	-.002	15
184			min	-1348.387	3	.207	12	-36.06	4	0	4	-.175	4	-.008	4
185		17	max	1038.846	2	.922	4	.42	1	0	3	.002	1	-.002	15
186			min	-1347.99	3	.179	12	-36.521	4	0	4	-.188	4	-.009	4
187		18	max	1039.376	2	.851	4	.42	1	0	3	.003	1	-.002	15
188			min	-1347.593	3	.151	12	-36.982	4	0	4	-.202	4	-.009	4
189		19	max	1039.905	2	.783	2	.42	1	0	3	.003	1	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-1347.196	3	.124	12	-37.444	4	0	4	-.215	4	-.009	4
191	M3	1	max	733.33	2	8.902	4	1.662	4	0	12	0	1	.009	4
192			min	-879.484	3	2.104	15	.023	12	0	4	-.023	4	.002	15
193		2	max	733.159	2	8.033	4	2.267	4	0	12	0	1	.005	4
194			min	-879.611	3	1.9	15	.023	12	0	4	-.022	4	0	12
195		3	max	732.989	2	7.164	4	2.872	4	0	12	0	1	.002	2
196			min	-879.739	3	1.695	15	.023	12	0	4	-.021	4	0	3
197		4	max	732.819	2	6.295	4	3.477	4	0	12	0	1	0	2
198			min	-879.867	3	1.491	15	.023	12	0	4	-.019	4	-.003	3
199		5	max	732.648	2	5.426	4	4.082	4	0	12	0	1	0	15
200			min	-879.995	3	1.287	15	.023	12	0	4	-.018	5	-.004	6
201		6	max	732.478	2	4.557	4	4.687	4	0	12	.001	1	-.001	15
202			min	-880.122	3	1.083	15	.023	12	0	4	-.016	5	-.007	6
203		7	max	732.308	2	3.688	4	5.292	4	0	12	.001	1	-.002	15
204			min	-880.25	3	.878	15	.023	12	0	4	-.013	5	-.009	6
205		8	max	732.137	2	2.819	4	5.897	4	0	12	.001	1	-.002	15
206			min	-880.378	3	.674	15	.023	12	0	4	-.011	5	-.01	6
207		9	max	731.967	2	1.95	4	6.502	4	0	12	.002	1	-.003	15
208			min	-880.506	3	.47	15	.023	12	0	4	-.008	5	-.011	6
209		10	max	731.797	2	1.082	4	7.107	4	0	12	.002	1	-.003	15
210			min	-880.633	3	.266	15	.023	12	0	4	-.005	5	-.012	6
211		11	max	731.626	2	.299	2	7.712	4	0	12	.002	1	-.003	15
212			min	-880.761	3	-.103	3	.023	12	0	4	-.001	5	-.012	6
213		12	max	731.456	2	-.143	15	8.317	4	0	12	.003	4	-.003	15
214			min	-880.889	3	-.657	6	.023	12	0	4	0	12	-.012	6
215		13	max	731.286	2	-.347	15	8.922	4	0	12	.007	4	-.003	15
216			min	-881.017	3	-1.526	6	.023	12	0	4	0	12	-.012	6
217		14	max	731.115	2	-.551	15	9.528	4	0	12	.011	4	-.002	15
218			min	-881.144	3	-2.395	6	.023	12	0	4	0	12	-.011	6
219		15	max	730.945	2	-.755	15	10.133	4	0	12	.016	4	-.002	15
220			min	-881.272	3	-3.264	6	.023	12	0	4	0	12	-.009	6
221		16	max	730.775	2	-.96	15	10.738	4	0	12	.021	4	-.002	15
222			min	-881.4	3	-4.133	6	.023	12	0	4	0	12	-.008	6
223		17	max	730.604	2	-1.164	15	11.343	4	0	12	.026	4	-.001	15
224			min	-881.528	3	-5.002	6	.023	12	0	4	0	12	-.006	6
225		18	max	730.434	2	-1.368	15	11.948	4	0	12	.031	4	0	15
226			min	-881.656	3	-5.871	6	.023	12	0	4	0	12	-.003	6
227		19	max	730.264	2	-1.572	15	12.553	4	0	12	.037	4	0	1
228			min	-881.783	3	-6.739	6	.023	12	0	4	0	12	0	1
229	M4	1	max	1018.201	1	0	1	-.888	12	0	1	.03	4	0	1
230			min	-72.423	5	0	1	-290.068	4	0	1	0	12	0	1
231		2	max	1018.371	1	0	1	-.888	12	0	1	0	1	0	1
232			min	-72.343	5	0	1	-290.216	4	0	1	-.004	5	0	1
233		3	max	1018.542	1	0	1	-.888	12	0	1	0	12	0	1
234			min	-72.264	5	0	1	-290.364	4	0	1	-.037	4	0	1
235		4	max	1018.712	1	0	1	-.888	12	0	1	0	12	0	1
236			min	-72.184	5	0	1	-290.511	4	0	1	-.07	4	0	1
237		5	max	1018.882	1	0	1	-.888	12	0	1	0	12	0	1
238			min	-72.105	5	0	1	-290.659	4	0	1	-.103	4	0	1
239		6	max	1019.053	1	0	1	-.888	12	0	1	0	12	0	1
240			min	-72.025	5	0	1	-290.807	4	0	1	-.137	4	0	1
241		7	max	1019.223	1	0	1	-.888	12	0	1	0	12	0	1
242			min	-71.946	5	0	1	-290.954	4	0	1	-.17	4	0	1
243		8	max	1019.393	1	0	1	-.888	12	0	1	0	12	0	1
244			min	-71.866	5	0	1	-291.102	4	0	1	-.204	4	0	1
245		9	max	1019.564	1	0	1	-.888	12	0	1	0	12	0	1
246			min	-71.787	5	0	1	-291.25	4	0	1	-.237	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	1019.734	1	0	1	-.888	12	0	1	0	12	0	1
248			min	-71.707	5	0	1	-291.397	4	0	1	-.271	4	0	1
249		11	max	1019.904	1	0	1	-.888	12	0	1	0	12	0	1
250			min	-71.628	5	0	1	-291.545	4	0	1	-.304	4	0	1
251		12	max	1020.075	1	0	1	-.888	12	0	1	0	12	0	1
252			min	-71.548	5	0	1	-291.692	4	0	1	-.338	4	0	1
253		13	max	1020.245	1	0	1	-.888	12	0	1	-.001	12	0	1
254			min	-71.469	5	0	1	-291.84	4	0	1	-.371	4	0	1
255		14	max	1020.415	1	0	1	-.888	12	0	1	-.001	12	0	1
256			min	-71.389	5	0	1	-291.988	4	0	1	-.405	4	0	1
257		15	max	1020.586	1	0	1	-.888	12	0	1	-.001	12	0	1
258			min	-71.31	5	0	1	-292.135	4	0	1	-.438	4	0	1
259		16	max	1020.756	1	0	1	-.888	12	0	1	-.001	12	0	1
260			min	-71.23	5	0	1	-292.283	4	0	1	-.472	4	0	1
261		17	max	1020.926	1	0	1	-.888	12	0	1	-.001	12	0	1
262			min	-71.151	5	0	1	-292.431	4	0	1	-.505	4	0	1
263		18	max	1021.097	1	0	1	-.888	12	0	1	-.002	12	0	1
264			min	-71.071	5	0	1	-292.578	4	0	1	-.539	4	0	1
265		19	max	1021.267	1	0	1	-.888	12	0	1	-.002	12	0	1
266			min	-70.992	5	0	1	-292.726	4	0	1	-.572	4	0	1
267	M6	1	max	3184.172	2	2.257	2	0	1	0	1	0	4	0	1
268			min	-4292.044	3	.273	12	-29.478	4	0	4	0	1	0	1
269		2	max	3184.702	2	2.201	2	0	1	0	1	0	1	0	12
270			min	-4291.647	3	.245	12	-29.94	4	0	4	-.011	4	0	2
271		3	max	3185.231	2	2.146	2	0	1	0	1	0	1	0	12
272			min	-4291.251	3	.217	12	-30.401	4	0	4	-.021	4	-.002	2
273		4	max	3185.76	2	2.091	2	0	1	0	1	0	1	0	12
274			min	-4290.854	3	.19	12	-30.862	4	0	4	-.032	4	-.002	2
275		5	max	3186.289	2	2.035	2	0	1	0	1	0	1	0	12
276			min	-4290.457	3	.157	3	-31.323	4	0	4	-.044	4	-.003	2
277		6	max	3186.819	2	1.98	2	0	1	0	1	0	1	0	12
278			min	-4290.06	3	.115	3	-31.784	4	0	4	-.055	4	-.004	2
279		7	max	3187.348	2	1.925	2	0	1	0	1	0	1	0	12
280			min	-4289.663	3	.074	3	-32.246	4	0	4	-.066	4	-.005	2
281		8	max	3187.877	2	1.869	2	0	1	0	1	0	1	0	12
282			min	-4289.266	3	.032	3	-32.707	4	0	4	-.078	4	-.005	2
283		9	max	3188.407	2	1.814	2	0	1	0	1	0	1	0	3
284			min	-4288.869	3	-.009	3	-33.168	4	0	4	-.09	4	-.006	2
285		10	max	3188.936	2	1.759	2	0	1	0	1	0	1	0	3
286			min	-4288.472	3	-.051	3	-33.629	4	0	4	-.102	4	-.006	2
287		11	max	3189.465	2	1.703	2	0	1	0	1	0	1	0	3
288			min	-4288.075	3	-.092	3	-34.09	4	0	4	-.114	4	-.007	2
289		12	max	3189.995	2	1.648	2	0	1	0	1	0	1	0	3
290			min	-4287.678	3	-.134	3	-34.552	4	0	4	-.126	4	-.008	2
291		13	max	3190.524	2	1.593	2	0	1	0	1	0	1	0	3
292			min	-4287.281	3	-.175	3	-35.013	4	0	4	-.139	4	-.008	2
293		14	max	3191.053	2	1.537	2	0	1	0	1	0	1	0	3
294			min	-4286.884	3	-.217	3	-35.474	4	0	4	-.151	4	-.009	2
295		15	max	3191.582	2	1.482	2	0	1	0	1	0	1	0	3
296			min	-4286.487	3	-.258	3	-35.935	4	0	4	-.164	4	-.009	2
297		16	max	3192.112	2	1.427	2	0	1	0	1	0	1	0	3
298			min	-4286.09	3	-.3	3	-36.397	4	0	4	-.177	4	-.01	2
299		17	max	3192.641	2	1.371	2	0	1	0	1	0	1	0	3
300			min	-4285.693	3	-.341	3	-36.858	4	0	4	-.19	4	-.01	2
301		18	max	3193.17	2	1.316	2	0	1	0	1	0	1	0	3
302			min	-4285.296	3	-.383	3	-37.319	4	0	4	-.204	4	-.011	2
303		19	max	3193.7	2	1.26	2	0	1	0	1	0	1	0	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-4284.899	3	-.424	3	-37.78	4	0	4	-.217	4	-.011	2
305	M7	1	max	2553.255	2	8.903	6	1.21	4	0	1	0	1	.011	2
306			min	-2673.743	3	2.091	15	0	1	0	4	-.023	4	0	3
307		2	max	2553.084	2	8.034	6	1.815	4	0	1	0	1	.008	2
308			min	-2673.871	3	1.886	15	0	1	0	4	-.023	4	-.002	3
309		3	max	2552.914	2	7.165	6	2.42	4	0	1	0	1	.005	2
310			min	-2673.999	3	1.682	15	0	1	0	4	-.022	4	-.004	3
311		4	max	2552.744	2	6.296	6	3.025	4	0	1	0	1	.002	2
312			min	-2674.126	3	1.478	15	0	1	0	4	-.02	4	-.006	3
313		5	max	2552.573	2	5.427	6	3.63	4	0	1	0	1	0	2
314			min	-2674.254	3	1.274	15	0	1	0	4	-.019	4	-.007	3
315		6	max	2552.403	2	4.558	6	4.235	4	0	1	0	1	-.002	15
316			min	-2674.382	3	1.069	15	0	1	0	4	-.017	4	-.008	3
317		7	max	2552.233	2	3.689	6	4.84	4	0	1	0	1	-.002	15
318			min	-2674.51	3	.865	15	0	1	0	4	-.015	4	-.009	3
319		8	max	2552.062	2	2.821	6	5.445	4	0	1	0	1	-.002	15
320			min	-2674.637	3	.661	15	0	1	0	4	-.012	4	-.01	4
321		9	max	2551.892	2	2.018	2	6.05	4	0	1	0	1	-.003	15
322			min	-2674.765	3	.357	12	0	1	0	4	-.01	4	-.011	4
323		10	max	2551.722	2	1.341	2	6.655	4	0	1	0	1	-.003	15
324			min	-2674.893	3	-.039	3	0	1	0	4	-.007	4	-.012	4
325		11	max	2551.551	2	.663	2	7.261	4	0	1	0	1	-.003	15
326			min	-2675.021	3	-.546	3	0	1	0	4	-.003	5	-.012	4
327		12	max	2551.381	2	-.014	2	7.866	4	0	1	0	4	-.003	15
328			min	-2675.148	3	-1.054	3	0	1	0	4	0	1	-.012	4
329		13	max	2551.211	2	-.36	15	8.471	4	0	1	.004	4	-.003	15
330			min	-2675.276	3	-1.562	3	0	1	0	4	0	1	-.012	4
331		14	max	2551.04	2	-.565	15	9.076	4	0	1	.008	4	-.003	15
332			min	-2675.404	3	-2.393	4	0	1	0	4	0	1	-.011	4
333		15	max	2550.87	2	-.769	15	9.681	4	0	1	.013	4	-.002	15
334			min	-2675.532	3	-3.262	4	0	1	0	4	0	1	-.009	4
335		16	max	2550.7	2	-.973	15	10.286	4	0	1	.017	4	-.002	15
336			min	-2675.659	3	-4.131	4	0	1	0	4	0	1	-.008	4
337		17	max	2550.529	2	-1.177	15	10.891	4	0	1	.022	4	-.001	15
338			min	-2675.787	3	-5	4	0	1	0	4	0	1	-.006	4
339		18	max	2550.359	2	-1.382	15	11.496	4	0	1	.028	4	0	15
340			min	-2675.915	3	-5.868	4	0	1	0	4	0	1	-.003	4
341		19	max	2550.188	2	-1.586	15	12.101	4	0	1	.033	4	0	1
342			min	-2676.043	3	-6.737	4	0	1	0	4	0	1	0	1
343	M8	1	max	2628.534	1	0	1	0	1	0	1	.027	4	0	1
344			min	-136.782	3	0	1	-276.604	4	0	1	0	1	0	1
345		2	max	2628.705	1	0	1	0	1	0	1	0	1	0	1
346			min	-136.654	3	0	1	-276.752	4	0	1	-.005	4	0	1
347		3	max	2628.875	1	0	1	0	1	0	1	0	1	0	1
348			min	-136.527	3	0	1	-276.9	4	0	1	-.037	4	0	1
349		4	max	2629.045	1	0	1	0	1	0	1	0	1	0	1
350			min	-136.399	3	0	1	-277.047	4	0	1	-.069	4	0	1
351		5	max	2629.216	1	0	1	0	1	0	1	0	1	0	1
352			min	-136.271	3	0	1	-277.195	4	0	1	-.101	4	0	1
353		6	max	2629.386	1	0	1	0	1	0	1	0	1	0	1
354			min	-136.143	3	0	1	-277.343	4	0	1	-.132	4	0	1
355		7	max	2629.556	1	0	1	0	1	0	1	0	1	0	1
356			min	-136.016	3	0	1	-277.49	4	0	1	-.164	4	0	1
357		8	max	2629.727	1	0	1	0	1	0	1	0	1	0	1
358			min	-135.888	3	0	1	-277.638	4	0	1	-.196	4	0	1
359		9	max	2629.897	1	0	1	0	1	0	1	0	1	0	1
360			min	-135.76	3	0	1	-277.785	4	0	1	-.228	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	2630.068	1	0	1	0	1	0	1	0	1	0	1
362			min	-135.632	3	0	1	-277.933	4	0	1	-.26	4	0	1
363		11	max	2630.238	1	0	1	0	1	0	1	0	1	0	1
364			min	-135.505	3	0	1	-278.081	4	0	1	-.292	4	0	1
365		12	max	2630.408	1	0	1	0	1	0	1	0	1	0	1
366			min	-135.377	3	0	1	-278.228	4	0	1	-.324	4	0	1
367		13	max	2630.579	1	0	1	0	1	0	1	0	1	0	1
368			min	-135.249	3	0	1	-278.376	4	0	1	-.356	4	0	1
369		14	max	2630.749	1	0	1	0	1	0	1	0	1	0	1
370			min	-135.121	3	0	1	-278.524	4	0	1	-.388	4	0	1
371		15	max	2630.919	1	0	1	0	1	0	1	0	1	0	1
372			min	-134.994	3	0	1	-278.671	4	0	1	-.42	4	0	1
373		16	max	2631.09	1	0	1	0	1	0	1	0	1	0	1
374			min	-134.866	3	0	1	-278.819	4	0	1	-.452	4	0	1
375		17	max	2631.26	1	0	1	0	1	0	1	0	1	0	1
376			min	-134.738	3	0	1	-278.966	4	0	1	-.484	4	0	1
377		18	max	2631.43	1	0	1	0	1	0	1	0	1	0	1
378			min	-134.61	3	0	1	-279.114	4	0	1	-.516	4	0	1
379		19	max	2631.601	1	0	1	0	1	0	1	0	1	0	1
380			min	-134.482	3	0	1	-279.262	4	0	1	-.548	4	0	1
381	M10	1	max	1030.378	2	1.99	6	-.029	12	0	1	0	4	0	1
382			min	-1354.342	3	.453	15	-29.4	4	0	5	0	3	0	1
383		2	max	1030.907	2	1.919	6	-.029	12	0	1	0	10	0	15
384			min	-1353.945	3	.436	15	-29.862	4	0	5	-.011	4	0	6
385		3	max	1031.436	2	1.848	6	-.029	12	0	1	0	10	0	15
386			min	-1353.548	3	.419	15	-30.323	4	0	5	-.021	4	-.001	6
387		4	max	1031.966	2	1.777	6	-.029	12	0	1	0	12	0	15
388			min	-1353.151	3	.403	15	-30.784	4	0	5	-.032	4	-.002	6
389		5	max	1032.495	2	1.706	6	-.029	12	0	1	0	12	0	15
390			min	-1352.754	3	.386	15	-31.245	4	0	5	-.043	4	-.003	6
391		6	max	1033.024	2	1.635	6	-.029	12	0	1	0	12	0	15
392			min	-1352.357	3	.369	15	-31.706	4	0	5	-.055	4	-.003	6
393		7	max	1033.554	2	1.563	6	-.029	12	0	1	0	12	0	15
394			min	-1351.96	3	.353	15	-32.168	4	0	5	-.066	4	-.004	6
395		8	max	1034.083	2	1.492	6	-.029	12	0	1	0	12	0	15
396			min	-1351.563	3	.336	15	-32.629	4	0	5	-.078	4	-.004	6
397		9	max	1034.612	2	1.421	6	-.029	12	0	1	0	12	-.001	15
398			min	-1351.166	3	.319	15	-33.09	4	0	5	-.09	4	-.005	6
399		10	max	1035.141	2	1.35	6	-.029	12	0	1	0	12	-.001	15
400			min	-1350.769	3	.302	15	-33.551	4	0	5	-.102	4	-.005	6
401		11	max	1035.671	2	1.279	6	-.029	12	0	1	0	12	-.001	15
402			min	-1350.372	3	.286	15	-34.013	4	0	5	-.114	4	-.006	6
403		12	max	1036.2	2	1.208	6	-.029	12	0	1	0	12	-.001	15
404			min	-1349.975	3	.269	15	-34.474	4	0	5	-.126	4	-.006	6
405		13	max	1036.729	2	1.137	6	-.029	12	0	1	0	12	-.002	15
406			min	-1349.578	3	.252	15	-34.935	4	0	5	-.138	4	-.007	6
407		14	max	1037.259	2	1.066	6	-.029	12	0	1	0	12	-.002	15
408			min	-1349.181	3	.236	15	-35.396	4	0	5	-.151	4	-.007	6
409		15	max	1037.788	2	1.004	2	-.029	12	0	1	0	12	-.002	15
410			min	-1348.784	3	.219	15	-35.857	4	0	5	-.164	4	-.007	6
411		16	max	1038.317	2	.949	2	-.029	12	0	1	0	12	-.002	15
412			min	-1348.387	3	.202	15	-36.319	4	0	5	-.177	4	-.008	6
413		17	max	1038.846	2	.893	2	-.029	12	0	1	0	12	-.002	15
414			min	-1347.99	3	.179	12	-36.78	4	0	5	-.19	4	-.008	6
415		18	max	1039.376	2	.838	2	-.029	12	0	1	0	12	-.002	15
416			min	-1347.593	3	.151	12	-37.241	4	0	5	-.203	4	-.008	6
417		19	max	1039.905	2	.783	2	-.029	12	0	1	0	12	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-1347.196	3	.124	12	-37.702	4	0	5	-.217	4	-.009	6
419	M11	1	max	733.33	2	8.849	6	1.452	4	0	1	0	12	.009	6
420			min	-879.484	3	2.069	15	-.341	1	0	4	-.023	4	.002	15
421		2	max	733.159	2	7.98	6	2.057	4	0	1	0	12	.005	2
422			min	-879.611	3	1.865	15	-.341	1	0	4	-.022	4	0	12
423		3	max	732.989	2	7.112	6	2.663	4	0	1	0	12	.002	2
424			min	-879.739	3	1.66	15	-.341	1	0	4	-.021	4	0	3
425		4	max	732.819	2	6.243	6	3.268	4	0	1	0	12	0	2
426			min	-879.867	3	1.456	15	-.341	1	0	4	-.02	4	-.003	3
427		5	max	732.648	2	5.374	6	3.873	4	0	1	0	12	-.001	15
428			min	-879.995	3	1.252	15	-.341	1	0	4	-.018	4	-.005	4
429		6	max	732.478	2	4.505	6	4.478	4	0	1	0	12	-.002	15
430			min	-880.122	3	1.048	15	-.341	1	0	4	-.016	4	-.007	4
431		7	max	732.308	2	3.636	6	5.083	4	0	1	0	12	-.002	15
432			min	-880.25	3	.843	15	-.341	1	0	4	-.014	4	-.009	4
433		8	max	732.137	2	2.767	6	5.688	4	0	1	0	12	-.003	15
434			min	-880.378	3	.639	15	-.341	1	0	4	-.011	4	-.01	4
435		9	max	731.967	2	1.898	6	6.293	4	0	1	0	12	-.003	15
436			min	-880.506	3	.435	15	-.341	1	0	4	-.009	4	-.012	4
437		10	max	731.797	2	1.029	6	6.898	4	0	1	0	12	-.003	15
438			min	-880.633	3	.231	15	-.341	1	0	4	-.006	4	-.012	4
439		11	max	731.626	2	.299	2	7.503	4	0	1	0	12	-.003	15
440			min	-880.761	3	-.103	3	-.341	1	0	4	-.002	4	-.012	4
441		12	max	731.456	2	-.178	15	8.108	4	0	1	.002	5	-.003	15
442			min	-880.889	3	-.709	4	-.341	1	0	4	-.002	1	-.012	4
443		13	max	731.286	2	-.382	15	8.713	4	0	1	.006	5	-.003	15
444			min	-881.017	3	-1.578	4	-.341	1	0	4	-.002	1	-.012	4
445		14	max	731.115	2	-.586	15	9.318	4	0	1	.01	5	-.003	15
446			min	-881.144	3	-2.447	4	-.341	1	0	4	-.002	1	-.011	4
447		15	max	730.945	2	-.791	15	9.923	4	0	1	.015	5	-.002	15
448			min	-881.272	3	-3.316	4	-.341	1	0	4	-.003	1	-.01	4
449		16	max	730.775	2	-.995	15	10.528	4	0	1	.019	5	-.002	15
450			min	-881.4	3	-4.185	4	-.341	1	0	4	-.003	1	-.008	4
451		17	max	730.604	2	-1.199	15	11.134	4	0	1	.025	5	-.001	15
452			min	-881.528	3	-5.054	4	-.341	1	0	4	-.003	1	-.006	4
453		18	max	730.434	2	-1.403	15	11.739	4	0	1	.03	5	0	15
454			min	-881.656	3	-5.923	4	-.341	1	0	4	-.003	1	-.003	4
455		19	max	730.264	2	-1.608	15	12.344	4	0	1	.036	5	0	1
456			min	-881.783	3	-6.792	4	-.341	1	0	4	-.003	1	0	1
457	M12	1	max	1018.201	1	0	1	13.587	1	0	1	.029	5	0	1
458			min	-13.148	3	0	1	-281.683	4	0	1	-.003	1	0	1
459		2	max	1018.371	1	0	1	13.587	1	0	1	0	12	0	1
460			min	-13.02	3	0	1	-281.83	4	0	1	-.004	4	0	1
461		3	max	1018.542	1	0	1	13.587	1	0	1	0	1	0	1
462			min	-12.892	3	0	1	-281.978	4	0	1	-.036	4	0	1
463		4	max	1018.712	1	0	1	13.587	1	0	1	.002	1	0	1
464			min	-12.764	3	0	1	-282.126	4	0	1	-.069	4	0	1
465		5	max	1018.882	1	0	1	13.587	1	0	1	.004	1	0	1
466			min	-12.637	3	0	1	-282.273	4	0	1	-.101	4	0	1
467		6	max	1019.053	1	0	1	13.587	1	0	1	.005	1	0	1
468			min	-12.509	3	0	1	-282.421	4	0	1	-.134	4	0	1
469		7	max	1019.223	1	0	1	13.587	1	0	1	.007	1	0	1
470			min	-12.381	3	0	1	-282.569	4	0	1	-.166	4	0	1
471		8	max	1019.393	1	0	1	13.587	1	0	1	.008	1	0	1
472			min	-12.253	3	0	1	-282.716	4	0	1	-.199	4	0	1
473		9	max	1019.564	1	0	1	13.587	1	0	1	.01	1	0	1
474			min	-12.126	3	0	1	-282.864	4	0	1	-.231	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	1019.734	1	0	1	13.587	1	0	1	.011	1	0	1
476			min	-11.998	3	0	1	-283.011	4	0	1	-.263	4	0	1
477		11	max	1019.904	1	0	1	13.587	1	0	1	.013	1	0	1
478			min	-11.87	3	0	1	-283.159	4	0	1	-.296	4	0	1
479		12	max	1020.075	1	0	1	13.587	1	0	1	.015	1	0	1
480			min	-11.742	3	0	1	-283.307	4	0	1	-.329	4	0	1
481		13	max	1020.245	1	0	1	13.587	1	0	1	.016	1	0	1
482			min	-11.615	3	0	1	-283.454	4	0	1	-.361	4	0	1
483		14	max	1020.415	1	0	1	13.587	1	0	1	.018	1	0	1
484			min	-11.487	3	0	1	-283.602	4	0	1	-.394	4	0	1
485		15	max	1020.586	1	0	1	13.587	1	0	1	.019	1	0	1
486			min	-11.359	3	0	1	-283.75	4	0	1	-.426	4	0	1
487		16	max	1020.756	1	0	1	13.587	1	0	1	.021	1	0	1
488			min	-11.231	3	0	1	-283.897	4	0	1	-.459	4	0	1
489		17	max	1020.926	1	0	1	13.587	1	0	1	.022	1	0	1
490			min	-11.104	3	0	1	-284.045	4	0	1	-.491	4	0	1
491		18	max	1021.097	1	0	1	13.587	1	0	1	.024	1	0	1
492			min	-10.976	3	0	1	-284.192	4	0	1	-.524	4	0	1
493		19	max	1021.267	1	0	1	13.587	1	0	1	.026	1	0	1
494			min	-10.848	3	0	1	-284.34	4	0	1	-.557	4	0	1
495	M1	1	max	178.245	1	705.897	3	47.525	5	0	1	.211	1	0	15
496			min	-18.076	5	-410.483	2	-75.342	1	0	3	-.122	5	-.015	2
497		2	max	179.087	1	704.802	3	48.985	5	0	1	.165	1	.24	2
498			min	-17.683	5	-411.942	2	-75.342	1	0	3	-.092	5	-.44	3
499		3	max	568.304	3	522.371	2	22.131	5	0	3	.118	1	.486	2
500			min	-343.239	2	-538.327	3	-75.119	1	0	2	-.062	5	-.863	3
501		4	max	568.936	3	520.912	2	23.591	5	0	3	.071	1	.171	1
502			min	-342.397	2	-539.422	3	-75.119	1	0	2	-.048	5	-.529	3
503		5	max	569.568	3	519.453	2	25.052	5	0	3	.025	1	-.005	15
504			min	-341.554	2	-540.516	3	-75.119	1	0	2	-.033	5	-.194	3
505		6	max	570.199	3	517.993	2	26.512	5	0	3	-.002	12	.142	3
506			min	-340.712	2	-541.61	3	-75.119	1	0	2	-.022	1	-.483	2
507		7	max	570.831	3	516.534	2	27.972	5	0	3	0	5	.479	3
508			min	-339.87	2	-542.705	3	-75.119	1	0	2	-.069	1	-.804	2
509		8	max	571.463	3	515.075	2	29.432	5	0	3	.018	5	.816	3
510			min	-339.027	2	-543.799	3	-75.119	1	0	2	-.115	1	-1.124	2
511		9	max	587.597	3	48.779	2	63.074	5	0	9	.073	1	.951	3
512			min	-262.056	2	.438	15	-120.464	1	0	3	-.145	5	-1.285	2
513		10	max	588.229	3	47.32	2	64.534	5	0	9	0	10	.929	3
514			min	-261.214	2	-.006	5	-120.464	1	0	3	-.107	4	-1.314	2
515		11	max	588.861	3	45.861	2	65.995	5	0	9	-.005	12	.909	3
516			min	-260.372	2	-1.82	4	-120.464	1	0	3	-.083	4	-1.343	2
517		12	max	604.79	3	363.467	3	163.797	5	0	2	.113	1	.795	3
518			min	-183.336	2	-617.338	2	-72.45	1	0	3	-.263	5	-1.191	2
519		13	max	605.421	3	362.373	3	165.257	5	0	2	.068	1	.57	3
520			min	-182.493	2	-618.797	2	-72.45	1	0	3	-.161	5	-.808	2
521		14	max	606.053	3	361.278	3	166.717	5	0	2	.023	1	.346	3
522			min	-181.651	2	-620.256	2	-72.45	1	0	3	-.058	5	-.423	2
523		15	max	606.685	3	360.184	3	168.178	5	0	2	.046	5	.122	3
524			min	-180.809	2	-621.715	2	-72.45	1	0	3	-.022	1	-.063	1
525		16	max	607.317	3	359.09	3	169.638	5	0	2	.151	5	.348	2
526			min	-179.966	2	-623.174	2	-72.45	1	0	3	-.067	1	-.102	3
527		17	max	607.949	3	357.995	3	171.098	5	0	2	.257	5	.736	2
528			min	-179.124	2	-624.633	2	-72.45	1	0	3	-.112	1	-.324	3
529		18	max	30.675	5	610.855	2	-5.699	12	0	5	.24	5	.37	2
530			min	-179.625	1	-277.539	3	-118.156	4	0	2	-.161	1	-.159	3
531		19	max	31.068	5	609.396	2	-5.699	12	0	5	.18	5	.013	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-178.783	1	-278.633	3	-116.695	4	0	2	-.214	1	-.01	1
533	M5	1	max	396.629	1	2343.611	3	94.755	5	0	1	0	1	.03	2
534			min	15.834	12	-1419.798	2	0	1	0	4	-.255	4	0	15
535		2	max	397.471	1	2342.517	3	96.215	5	0	1	0	1	.912	2
536			min	16.255	12	-1421.257	2	0	1	0	4	-.196	4	-1.45	3
537		3	max	1770.099	3	1443.831	2	72.608	4	0	4	0	1	1.763	2
538			min	-1125.671	2	-1621.018	3	0	1	0	1	-.136	4	-2.86	3
539		4	max	1770.731	3	1442.372	2	74.068	4	0	4	0	1	.867	2
540			min	-1124.828	2	-1622.113	3	0	1	0	1	-.09	4	-1.854	3
541		5	max	1771.362	3	1440.913	2	75.528	4	0	4	0	1	.033	9
542			min	-1123.986	2	-1623.207	3	0	1	0	1	-.044	4	-.847	3
543		6	max	1771.994	3	1439.454	2	76.989	4	0	4	.003	4	.161	3
544			min	-1123.144	2	-1624.301	3	0	1	0	1	0	1	-.921	2
545		7	max	1772.626	3	1437.995	2	78.449	4	0	4	.052	4	1.169	3
546			min	-1122.301	2	-1625.396	3	0	1	0	1	0	1	-1.814	2
547		8	max	1773.258	3	1436.536	2	79.909	4	0	4	.101	4	2.179	3
548			min	-1121.459	2	-1626.49	3	0	1	0	1	0	1	-2.706	2
549		9	max	1796.115	3	164.742	2	212.193	4	0	1	0	1	2.509	3
550			min	-957.952	2	.442	15	0	1	0	1	-.225	4	-3.096	2
551		10	max	1796.747	3	163.283	2	213.654	4	0	1	0	1	2.428	3
552			min	-957.109	2	.001	15	0	1	0	1	-.093	4	-3.197	2
553		11	max	1797.378	3	161.824	2	215.114	4	0	1	.04	4	2.348	3
554			min	-956.267	2	-1.591	6	0	1	0	1	0	1	-3.298	2
555		12	max	1820.645	3	1058.893	3	230.906	4	0	1	0	1	2.058	3
556			min	-792.89	2	-1767.646	2	0	1	0	4	-.379	4	-2.949	2
557		13	max	1821.277	3	1057.799	3	232.366	4	0	1	0	1	1.402	3
558			min	-792.048	2	-1769.105	2	0	1	0	4	-.235	4	-1.852	2
559		14	max	1821.909	3	1056.704	3	233.827	4	0	1	0	1	.745	3
560			min	-791.206	2	-1770.564	2	0	1	0	4	-.09	4	-.753	2
561		15	max	1822.541	3	1055.61	3	235.287	4	0	1	.055	4	.346	2
562			min	-790.363	2	-1772.023	2	0	1	0	4	0	1	0	15
563		16	max	1823.173	3	1054.516	3	236.747	4	0	1	.202	4	1.446	2
564			min	-789.521	2	-1773.483	2	0	1	0	4	0	1	-.565	3
565		17	max	1823.804	3	1053.422	3	238.207	4	0	1	.349	4	2.547	2
566			min	-788.678	2	-1774.942	2	0	1	0	4	0	1	-1.219	3
567		18	max	-17.026	12	2071.384	2	0	1	0	4	.375	4	1.303	2
568			min	-396.395	1	-978.203	3	-22.857	5	0	1	0	1	-.634	3
569		19	max	-16.605	12	2069.925	2	0	1	0	4	.362	4	.019	1
570			min	-395.553	1	-979.298	3	-21.397	5	0	1	0	1	-.027	3
571	M9	1	max	178.245	1	705.897	3	76.689	4	0	3	-.016	12	0	15
572			min	9.826	12	-410.483	2	5.559	12	0	4	-.211	1	-.015	2
573		2	max	179.087	1	704.802	3	78.149	4	0	3	-.012	12	.24	2
574			min	10.247	12	-411.942	2	5.559	12	0	4	-.165	1	-.44	3
575		3	max	568.304	3	522.371	2	75.119	1	0	2	-.009	12	.486	2
576			min	-343.239	2	-538.327	3	5.529	12	0	3	-.118	1	-.863	3
577		4	max	568.936	3	520.912	2	75.119	1	0	2	-.005	12	.171	1
578			min	-342.397	2	-539.422	3	5.529	12	0	3	-.076	4	-.529	3
579		5	max	569.568	3	519.453	2	75.119	1	0	2	-.002	12	-.005	15
580			min	-341.554	2	-540.516	3	5.529	12	0	3	-.042	4	-.194	3
581		6	max	570.199	3	517.993	2	75.119	1	0	2	.022	1	.142	3
582			min	-340.712	2	-541.61	3	5.529	12	0	3	-.013	5	-.483	2
583		7	max	570.831	3	516.534	2	75.119	1	0	2	.069	1	.479	3
584			min	-339.87	2	-542.705	3	5.529	12	0	3	.005	12	-.804	2
585		8	max	571.463	3	515.075	2	75.119	1	0	2	.115	1	.816	3
586			min	-339.027	2	-543.799	3	5.529	12	0	3	.008	12	-1.124	2
587		9	max	587.597	3	48.779	2	120.464	1	0	3	-.005	12	.951	3
588			min	-262.056	2	.454	15	8.446	12	0	9	-.175	4	-1.285	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	588.229	3	47.32	2	120.464	1	0	3	.001	1	.929	3
590			min	-261.214	2	.013	15	8.446	12	0	9	-.106	4	-1.314	2
591		11	max	588.861	3	45.861	2	120.464	1	0	3	.076	1	.909	3
592			min	-260.372	2	-1.702	6	8.446	12	0	9	-.054	5	-1.343	2
593		12	max	604.79	3	363.467	3	193.857	4	0	3	-.008	12	.795	3
594			min	-183.336	2	-617.338	2	4.836	12	0	2	-.309	4	-1.191	2
595		13	max	605.421	3	362.373	3	195.317	4	0	3	-.005	12	.57	3
596			min	-182.493	2	-618.797	2	4.836	12	0	2	-.188	4	-.808	2
597		14	max	606.053	3	361.278	3	196.777	4	0	3	-.002	12	.346	3
598			min	-181.651	2	-620.256	2	4.836	12	0	2	-.067	4	-.423	2
599		15	max	606.685	3	360.184	3	198.237	4	0	3	.056	4	.122	3
600			min	-180.809	2	-621.715	2	4.836	12	0	2	.001	12	-.063	1
601		16	max	607.317	3	359.09	3	199.698	4	0	3	.179	4	.348	2
602			min	-179.966	2	-623.174	2	4.836	12	0	2	.004	12	-.102	3
603		17	max	607.949	3	357.995	3	201.158	4	0	3	.304	4	.736	2
604			min	-179.124	2	-624.633	2	4.836	12	0	2	.007	12	-.324	3
605		18	max	-9.862	12	610.855	2	85.378	1	0	2	.304	4	.37	2
606			min	-179.625	1	-277.539	3	-85.246	5	0	3	.011	12	-.159	3
607		19	max	-9.441	12	609.396	2	85.378	1	0	2	.264	4	.013	3
608			min	-178.783	1	-278.633	3	-83.786	5	0	3	.014	12	-.01	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.197	2	.011	3	1.357e-2	2	NC	1	NC	1
2			min	-.825	4	-.051	3	-.006	2	-3.528e-3	3	NC	1	NC	1
3		2	max	0	1	.158	3	.027	1	1.482e-2	2	NC	4	NC	2
4			min	-.825	4	.003	15	-.019	5	-3.356e-3	3	976.952	3	7418.863	1
5		3	max	0	1	.328	3	.064	1	1.608e-2	2	NC	5	NC	3
6			min	-.825	4	-.007	9	-.024	5	-3.184e-3	3	538.872	3	3168.077	1
7		4	max	0	1	.432	3	.095	1	1.733e-2	2	NC	5	NC	3
8			min	-.825	4	-.031	1	-.018	5	-3.013e-3	3	422.364	3	2143.459	1
9		5	max	0	1	.459	3	.11	1	1.859e-2	2	NC	5	NC	3
10			min	-.825	4	-.024	1	-.006	5	-2.841e-3	3	400.181	3	1855.408	1
11		6	max	0	1	.41	3	.104	1	1.984e-2	2	NC	5	NC	5
12			min	-.825	4	-.003	9	.004	10	-2.67e-3	3	442.982	3	1953.128	1
13		7	max	0	1	.3	3	.08	1	2.109e-2	2	NC	4	NC	5
14			min	-.825	4	.003	15	0	10	-2.498e-3	3	581.519	3	2549.393	1
15		8	max	0	1	.237	2	.044	1	2.235e-2	2	NC	4	NC	2
16			min	-.825	4	.006	15	-.007	10	-2.327e-3	3	970.684	3	4675.531	1
17		9	max	0	1	.323	2	.034	3	2.36e-2	2	NC	4	NC	1
18			min	-.825	4	.008	15	-.016	2	-2.155e-3	3	1615.955	2	8736.999	4
19		10	max	0	1	.361	2	.033	3	2.485e-2	2	NC	5	NC	1
20			min	-.825	4	-.027	3	-.023	2	-1.984e-3	3	1242.014	2	9226.372	3
21		11	max	0	12	.323	2	.034	3	2.36e-2	2	NC	4	NC	1
22			min	-.825	4	.008	15	-.016	2	-2.155e-3	3	1615.955	2	9028.187	3
23		12	max	0	12	.237	2	.044	1	2.235e-2	2	NC	4	NC	2
24			min	-.825	4	.005	15	-.014	5	-2.327e-3	3	970.684	3	4675.531	1
25		13	max	0	12	.3	3	.08	1	2.109e-2	2	NC	4	NC	4
26			min	-.825	4	.003	15	-.005	5	-2.498e-3	3	581.519	3	2549.393	1
27		14	max	0	12	.41	3	.104	1	1.984e-2	2	NC	5	NC	5
28			min	-.825	4	-.003	9	.004	10	-2.67e-3	3	442.982	3	1953.128	1
29		15	max	0	12	.459	3	.11	1	1.859e-2	2	NC	5	NC	3
30			min	-.825	4	-.024	1	.006	10	-2.841e-3	3	400.181	3	1855.408	1
31		16	max	0	12	.432	3	.095	1	1.733e-2	2	NC	5	NC	3
32			min	-.825	4	-.031	1	.005	10	-3.013e-3	3	422.364	3	2143.459	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	12	.328	3	.064	1	1.608e-2	2	NC	5	NC	3
34			min	-.825	4	-.007	9	.003	10	-3.184e-3	3	538.872	3	3168.077	1
35		18	max	0	12	.158	3	.031	4	1.482e-2	2	NC	4	NC	2
36			min	-.825	4	.002	15	-.001	10	-3.356e-3	3	976.952	3	6337.29	4
37		19	max	0	12	.197	2	.011	3	1.357e-2	2	NC	1	NC	1
38			min	-.825	4	-.051	3	-.006	2	-3.528e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.398	3	.01	3	7.637e-3	2	NC	1	NC	1
40			min	-.606	4	-.595	2	-.006	2	-5.944e-3	3	NC	1	NC	1
41		2	max	0	1	.653	3	.018	1	8.849e-3	2	NC	5	NC	1
42			min	-.606	4	-.848	2	-.029	5	-7.011e-3	3	798.381	3	7554.653	5
43		3	max	0	1	.877	3	.049	1	1.006e-2	2	NC	5	NC	2
44			min	-.606	4	-1.075	2	-.035	5	-8.079e-3	3	425.367	2	4169.533	1
45		4	max	0	1	1.045	3	.078	1	1.127e-2	2	NC	15	NC	3
46			min	-.606	4	-1.256	2	-.025	5	-9.146e-3	3	308.779	2	2606.769	1
47		5	max	0	1	1.148	3	.095	1	1.249e-2	2	NC	15	NC	3
48			min	-.606	4	-1.381	2	-.006	5	-1.021e-2	3	259.622	2	2159.262	1
49		6	max	0	1	1.182	3	.093	1	1.37e-2	2	9961.391	15	NC	3
50			min	-.606	4	-1.448	2	.003	10	-1.128e-2	3	239.251	2	2209.233	1
51		7	max	0	1	1.159	3	.072	1	1.491e-2	2	9934.197	15	NC	3
52			min	-.606	4	-1.463	2	0	10	-1.235e-2	3	235.153	2	2824.563	1
53		8	max	0	1	1.098	3	.053	4	1.612e-2	2	NC	15	NC	2
54			min	-.606	4	-1.44	2	-.006	10	-1.341e-2	3	241.47	2	3764.033	4
55		9	max	0	1	1.029	3	.036	4	1.733e-2	2	NC	15	NC	1
56			min	-.606	4	-1.403	2	-.014	2	-1.448e-2	3	252.658	2	5461.967	4
57		10	max	0	1	.995	3	.029	3	1.855e-2	2	NC	15	NC	1
58			min	-.606	4	-1.382	2	-.021	2	-1.555e-2	3	259.384	2	NC	1
59		11	max	0	12	1.029	3	.03	3	1.733e-2	2	NC	15	NC	1
60			min	-.606	4	-1.403	2	-.029	5	-1.448e-2	3	252.658	2	7598.069	5
61		12	max	0	12	1.098	3	.04	1	1.612e-2	2	NC	15	NC	2
62			min	-.606	4	-1.44	2	-.033	5	-1.341e-2	3	241.47	2	5084.125	1
63		13	max	0	12	1.159	3	.072	1	1.491e-2	2	9934.017	15	NC	3
64			min	-.606	4	-1.463	2	-.022	5	-1.235e-2	3	235.153	2	2824.563	1
65		14	max	0	12	1.182	3	.093	1	1.37e-2	2	9961.121	15	NC	3
66			min	-.606	4	-1.448	2	-.002	5	-1.128e-2	3	239.251	2	2209.233	1
67		15	max	0	12	1.148	3	.095	1	1.249e-2	2	NC	15	NC	3
68			min	-.606	4	-1.381	2	.005	10	-1.021e-2	3	259.622	2	2159.262	1
69		16	max	0	12	1.045	3	.078	1	1.127e-2	2	NC	15	NC	3
70			min	-.606	4	-1.256	2	.004	10	-9.146e-3	3	308.779	2	2606.769	1
71		17	max	0	12	.877	3	.056	4	1.006e-2	2	NC	5	NC	2
72			min	-.606	4	-1.075	2	.001	10	-8.079e-3	3	425.367	2	3558.039	4
73		18	max	0	12	.653	3	.038	4	8.849e-3	2	NC	5	NC	1
74			min	-.606	4	-.848	2	-.002	10	-7.011e-3	3	798.381	3	5303.272	4
75		19	max	0	12	.398	3	.01	3	7.637e-3	2	NC	1	NC	1
76			min	-.607	4	-.595	2	-.006	2	-5.944e-3	3	NC	1	NC	1
77	M15	1	max	0	12	.406	3	.009	3	5.087e-3	3	NC	1	NC	1
78			min	-.487	4	-.594	2	-.005	2	-7.955e-3	2	NC	1	NC	1
79		2	max	0	12	.591	3	.018	1	5.996e-3	3	NC	5	NC	1
80			min	-.487	4	-.903	2	-.04	5	-9.225e-3	2	659.143	2	4891.168	5
81		3	max	0	12	.758	3	.049	1	6.904e-3	3	NC	5	NC	2
82			min	-.487	4	-1.176	2	-.049	5	-1.05e-2	2	350.699	2	3987.011	5
83		4	max	0	12	.892	3	.079	1	7.813e-3	3	NC	15	NC	3
84			min	-.487	4	-1.384	2	-.037	5	-1.177e-2	2	258.066	2	2594.083	1
85		5	max	0	12	.988	3	.095	1	8.722e-3	3	NC	15	NC	3
86			min	-.487	4	-1.516	2	-.011	5	-1.304e-2	2	221.264	2	2149.147	1
87		6	max	0	12	1.043	3	.093	1	9.63e-3	3	9989.106	15	NC	3
88			min	-.487	4	-1.568	2	.004	10	-1.431e-2	2	209.357	2	2197.737	1
89		7	max	0	12	1.061	3	.073	1	1.054e-2	3	9965.635	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.487	4	-1.552	2	0	10	-1.558e-2	2	212.883	2	2805.021	1
91		8	max	0	12	1.051	3	.064	4	1.145e-2	3	NC	15	NC	2
92			min	-.487	4	-1.49	2	-.005	10	-1.685e-2	2	227.623	2	3139.246	4
93		9	max	0	12	1.029	3	.045	4	1.236e-2	3	NC	15	NC	1
94			min	-.487	4	-1.417	2	-.013	2	-1.812e-2	2	247.839	2	4404.897	4
95		10	max	0	1	1.016	3	.027	3	1.326e-2	3	NC	15	NC	1
96			min	-.487	4	-1.38	2	-.02	2	-1.939e-2	2	259.539	2	NC	1
97		11	max	0	1	1.029	3	.027	3	1.236e-2	3	NC	15	NC	1
98			min	-.487	4	-1.417	2	-.038	5	-1.812e-2	2	247.839	2	5402.621	5
99		12	max	0	1	1.051	3	.041	1	1.145e-2	3	NC	15	NC	2
100			min	-.487	4	-1.49	2	-.044	5	-1.685e-2	2	227.623	2	4619.965	5
101		13	max	0	1	1.061	3	.073	1	1.054e-2	3	9965.494	15	NC	3
102			min	-.487	4	-1.552	2	-.03	5	-1.558e-2	2	212.883	2	2805.021	1
103		14	max	0	1	1.043	3	.093	1	9.63e-3	3	9988.9	15	NC	3
104			min	-.487	4	-1.568	2	-.003	5	-1.431e-2	2	209.357	2	2197.737	1
105		15	max	0	1	.988	3	.095	1	8.722e-3	3	NC	15	NC	3
106			min	-.487	4	-1.516	2	.005	10	-1.304e-2	2	221.264	2	2149.147	1
107		16	max	0	1	.892	3	.079	1	7.813e-3	3	NC	15	NC	3
108			min	-.486	4	-1.384	2	.004	10	-1.177e-2	2	258.066	2	2594.083	1
109		17	max	0	1	.758	3	.07	4	6.904e-3	3	NC	5	NC	2
110			min	-.486	4	-1.176	2	.002	10	-1.05e-2	2	350.699	2	2860.999	4
111		18	max	0	1	.591	3	.048	4	5.996e-3	3	NC	5	NC	1
112			min	-.486	4	-.903	2	-.002	10	-9.225e-3	2	659.143	2	4138.906	4
113		19	max	0	1	.406	3	.009	3	5.087e-3	3	NC	1	NC	1
114			min	-.486	4	-.594	2	-.005	2	-7.955e-3	2	NC	1	NC	1
115	M16	1	max	0	12	.174	2	.008	3	9.502e-3	3	NC	1	NC	1
116			min	-.134	4	-.141	3	-.005	2	-1.136e-2	2	NC	1	NC	1
117		2	max	0	12	.038	1	.027	1	1.062e-2	3	NC	4	NC	2
118			min	-.134	4	-.083	3	-.029	5	-1.212e-2	2	1281.471	2	7506.375	1
119		3	max	0	12	.004	13	.064	1	1.174e-2	3	NC	5	NC	3
120			min	-.134	4	-.11	2	-.037	5	-1.288e-2	2	716.248	2	3184.212	1
121		4	max	0	12	0	5	.095	1	1.286e-2	3	NC	5	NC	3
122			min	-.134	4	-.18	2	-.029	5	-1.364e-2	2	575.48	2	2145.513	1
123		5	max	0	12	0	13	.11	1	1.398e-2	3	NC	5	NC	3
124			min	-.134	4	-.184	2	-.013	5	-1.44e-2	2	569.824	2	1850.175	1
125		6	max	0	12	.006	4	.105	1	1.51e-2	3	NC	5	NC	3
126			min	-.134	4	-.123	2	.004	15	-1.516e-2	2	686.011	2	1938.171	1
127		7	max	0	12	.034	9	.081	1	1.622e-2	3	NC	3	NC	3
128			min	-.134	4	-.138	3	.002	10	-1.592e-2	2	1092.207	2	2508.016	1
129		8	max	0	12	.145	1	.045	1	1.734e-2	3	NC	1	NC	2
130			min	-.134	4	-.209	3	-.004	10	-1.668e-2	2	2988.691	3	4492.335	1
131		9	max	0	12	.243	1	.029	4	1.846e-2	3	NC	4	NC	1
132			min	-.134	4	-.27	3	-.011	2	-1.744e-2	2	1580.653	3	6792.727	4
133		10	max	0	1	.294	2	.023	3	1.958e-2	3	NC	5	NC	1
134			min	-.134	4	-.297	3	-.018	2	-1.82e-2	2	1309.239	3	NC	1
135		11	max	0	1	.243	1	.024	3	1.846e-2	3	NC	4	NC	1
136			min	-.134	4	-.27	3	-.022	5	-1.744e-2	2	1580.653	3	NC	1
137		12	max	0	1	.145	1	.045	1	1.734e-2	3	NC	1	NC	2
138			min	-.134	4	-.209	3	-.022	5	-1.668e-2	2	2988.691	3	4492.335	1
139		13	max	0	1	.034	9	.081	1	1.622e-2	3	NC	3	NC	3
140			min	-.134	4	-.138	3	-.01	5	-1.592e-2	2	1092.207	2	2508.016	1
141		14	max	0	1	.005	6	.105	1	1.51e-2	3	NC	5	NC	3
142			min	-.134	4	-.123	2	.006	10	-1.516e-2	2	686.011	2	1938.171	1
143		15	max	0	1	0	13	.11	1	1.398e-2	3	NC	5	NC	3
144			min	-.134	4	-.184	2	.008	10	-1.44e-2	2	569.824	2	1850.175	1
145		16	max	0	1	0	15	.095	1	1.286e-2	3	NC	5	NC	3
146			min	-.134	4	-.18	2	.007	10	-1.364e-2	2	575.48	2	2145.513	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.003	13	.064	1	1.174e-2	3	NC	5	NC	3
148			min	-.134	4	-.11	2	.004	10	-1.288e-2	2	716.248	2	3184.212	1
149		18	max	0	1	.038	1	.041	4	1.062e-2	3	NC	4	NC	2
150			min	-.134	4	-.083	3	0	10	-1.212e-2	2	1281.471	2	4928.967	4
151		19	max	0	1	.174	2	.008	3	9.502e-3	3	NC	1	NC	1
152			min	-.134	4	-.141	3	-.005	2	-1.136e-2	2	NC	1	NC	1
153	M2	1	max	.008	2	.01	2	.01	1	2.363e-3	5	NC	1	NC	2
154			min	-.01	3	-.016	3	-.772	4	-2.256e-4	1	7437.462	2	100.366	4
155		2	max	.007	2	.009	2	.009	1	2.401e-3	5	NC	1	NC	2
156			min	-.01	3	-.016	3	-.709	4	-2.143e-4	1	8736.538	2	109.238	4
157		3	max	.007	2	.007	2	.008	1	2.439e-3	5	NC	1	NC	2
158			min	-.009	3	-.016	3	-.647	4	-2.03e-4	1	NC	1	119.766	4
159		4	max	.006	2	.006	2	.007	1	2.477e-3	5	NC	1	NC	1
160			min	-.008	3	-.015	3	-.585	4	-1.918e-4	1	NC	1	132.383	4
161		5	max	.006	2	.004	2	.007	1	2.515e-3	5	NC	1	NC	1
162			min	-.008	3	-.014	3	-.525	4	-1.805e-4	1	NC	1	147.673	4
163		6	max	.006	2	.003	2	.006	1	2.553e-3	5	NC	1	NC	1
164			min	-.007	3	-.014	3	-.466	4	-1.692e-4	1	NC	1	166.448	4
165		7	max	.005	2	.002	2	.005	1	2.591e-3	5	NC	1	NC	1
166			min	-.007	3	-.013	3	-.408	4	-1.579e-4	1	NC	1	189.857	4
167		8	max	.005	2	0	2	.004	1	2.629e-3	5	NC	1	NC	1
168			min	-.006	3	-.013	3	-.353	4	-1.467e-4	1	NC	1	219.577	4
169		9	max	.004	2	0	2	.004	1	2.667e-3	5	NC	1	NC	1
170			min	-.006	3	-.012	3	-.3	4	-1.354e-4	1	NC	1	258.128	4
171		10	max	.004	2	-.001	15	.003	1	2.708e-3	4	NC	1	NC	1
172			min	-.005	3	-.011	3	-.25	4	-1.241e-4	1	NC	1	309.443	4
173		11	max	.003	2	-.001	15	.003	1	2.749e-3	4	NC	1	NC	1
174			min	-.004	3	-.01	3	-.204	4	-1.128e-4	1	NC	1	379.951	4
175		12	max	.003	2	-.001	15	.002	1	2.791e-3	4	NC	1	NC	1
176			min	-.004	3	-.009	3	-.161	4	-1.016e-4	1	NC	1	480.753	4
177		13	max	.003	2	-.001	15	.002	1	2.832e-3	4	NC	1	NC	1
178			min	-.003	3	-.008	3	-.123	4	-9.029e-5	1	NC	1	632.415	4
179		14	max	.002	2	-.001	15	.001	1	2.874e-3	4	NC	1	NC	1
180			min	-.003	3	-.007	3	-.088	4	-7.901e-5	1	NC	1	876.68	4
181		15	max	.002	2	-.001	15	0	1	2.915e-3	4	NC	1	NC	1
182			min	-.002	3	-.006	3	-.059	4	-6.774e-5	1	NC	1	1309.478	4
183		16	max	.001	2	0	15	0	1	2.957e-3	4	NC	1	NC	1
184			min	-.002	3	-.005	3	-.035	4	-5.646e-5	1	NC	1	2194.869	4
185		17	max	0	2	0	15	0	1	2.998e-3	4	NC	1	NC	1
186			min	-.001	3	-.003	6	-.017	4	-4.519e-5	1	NC	1	4505.45	4
187		18	max	0	2	0	15	0	1	3.04e-3	4	NC	1	NC	1
188			min	0	3	-.002	6	-.005	4	-3.391e-5	1	NC	1	NC	1
189		19	max	0	1	0	1	0	1	3.081e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	-2.263e-5	1	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	4.445e-6	1	NC	1	NC	1
192			min	0	1	0	1	0	1	-6.678e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.016	4	2.976e-5	1	NC	1	NC	1
194			min	0	2	-.003	6	0	1	1.994e-6	12	NC	1	NC	1
195		3	max	0	3	-.001	15	.032	4	7.188e-4	4	NC	1	NC	1
196			min	0	2	-.006	6	0	1	3.613e-6	12	NC	1	NC	1
197		4	max	.001	3	-.002	15	.046	4	1.412e-3	4	NC	1	NC	1
198			min	-.001	2	-.009	6	0	1	5.233e-6	12	NC	1	9226.715	5
199		5	max	.002	3	-.003	15	.059	4	2.105e-3	4	NC	1	NC	1
200			min	-.002	2	-.012	6	0	1	6.852e-6	12	8530.741	6	8197.651	5
201		6	max	.002	3	-.003	15	.071	4	2.799e-3	4	NC	5	NC	1
202			min	-.002	2	-.015	6	0	1	8.471e-6	12	6912.12	6	7950.786	5
203		7	max	.003	3	-.004	15	.082	4	3.492e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.002	2	-.017	6	0	1	1.009e-5	12	5937.299	6	8274.911	5
205		8	max	.003	3	-.004	15	.092	4	4.185e-3	4	NC	5	NC	1
206			min	-.003	2	-.019	6	0	3	1.171e-5	12	5336.07	6	9219.252	5
207		9	max	.004	3	-.005	15	.102	4	4.879e-3	4	NC	5	NC	1
208			min	-.003	2	-.02	6	0	12	1.333e-5	12	4981.245	6	NC	1
209		10	max	.004	3	-.005	15	.111	4	5.572e-3	4	NC	5	NC	1
210			min	-.004	2	-.021	6	0	12	1.495e-5	12	4811.161	6	NC	1
211		11	max	.005	3	-.005	15	.12	4	6.265e-3	4	NC	5	NC	1
212			min	-.004	2	-.021	6	0	12	1.657e-5	12	4800.81	6	NC	1
213		12	max	.005	3	-.004	15	.129	4	6.959e-3	4	NC	5	NC	1
214			min	-.004	2	-.021	6	0	12	1.819e-5	12	4952.253	6	NC	1
215		13	max	.006	3	-.004	15	.138	4	7.652e-3	4	NC	5	NC	1
216			min	-.005	2	-.019	6	0	12	1.981e-5	12	5296.647	6	NC	1
217		14	max	.006	3	-.004	15	.148	4	8.345e-3	4	NC	5	NC	1
218			min	-.005	2	-.017	6	0	12	2.143e-5	12	5910.333	6	NC	1
219		15	max	.007	3	-.003	15	.158	4	9.039e-3	4	NC	3	NC	1
220			min	-.006	2	-.015	6	0	12	2.305e-5	12	6962.276	6	NC	1
221		16	max	.007	3	-.002	15	.169	4	9.732e-3	4	NC	1	NC	1
222			min	-.006	2	-.012	6	0	12	2.466e-5	12	8861.515	6	NC	1
223		17	max	.008	3	-.001	15	.181	4	1.043e-2	4	NC	1	NC	1
224			min	-.006	2	-.008	6	0	12	2.628e-5	12	NC	1	NC	1
225		18	max	.008	3	0	15	.195	4	1.112e-2	4	NC	1	NC	1
226			min	-.007	2	-.005	1	0	12	2.79e-5	12	NC	1	NC	1
227		19	max	.009	3	0	5	.211	4	1.181e-2	4	NC	1	NC	1
228			min	-.007	2	-.002	3	0	12	2.952e-5	12	NC	1	NC	1
229	M4	1	max	.002	1	.007	2	0	12	1.693e-4	1	NC	1	NC	3
230			min	0	5	-.009	3	-.211	4	-8.821e-5	5	NC	1	117.724	4
231		2	max	.002	1	.006	2	0	12	1.693e-4	1	NC	1	NC	3
232			min	0	5	-.008	3	-.194	4	-8.821e-5	5	NC	1	127.991	4
233		3	max	.002	1	.006	2	0	12	1.693e-4	1	NC	1	NC	3
234			min	0	5	-.008	3	-.177	4	-8.821e-5	5	NC	1	140.212	4
235		4	max	.002	1	.006	2	0	12	1.693e-4	1	NC	1	NC	3
236			min	0	5	-.007	3	-.16	4	-8.821e-5	5	NC	1	154.892	4
237		5	max	.002	1	.005	2	0	12	1.693e-4	1	NC	1	NC	3
238			min	0	5	-.007	3	-.144	4	-8.821e-5	5	NC	1	172.721	4
239		6	max	.002	1	.005	2	0	12	1.693e-4	1	NC	1	NC	2
240			min	0	5	-.006	3	-.127	4	-8.821e-5	5	NC	1	194.655	4
241		7	max	.002	1	.005	2	0	12	1.693e-4	1	NC	1	NC	2
242			min	0	5	-.006	3	-.112	4	-8.821e-5	5	NC	1	222.05	4
243		8	max	.001	1	.004	2	0	12	1.693e-4	1	NC	1	NC	2
244			min	0	5	-.005	3	-.097	4	-8.821e-5	5	NC	1	256.884	4
245		9	max	.001	1	.004	2	0	12	1.693e-4	1	NC	1	NC	2
246			min	0	5	-.005	3	-.082	4	-8.821e-5	5	NC	1	302.136	4
247		10	max	.001	1	.003	2	0	12	1.693e-4	1	NC	1	NC	2
248			min	0	5	-.004	3	-.068	4	-8.821e-5	5	NC	1	362.461	4
249		11	max	.001	1	.003	2	0	12	1.693e-4	1	NC	1	NC	1
250			min	0	5	-.004	3	-.056	4	-8.821e-5	5	NC	1	445.473	4
251		12	max	0	1	.003	2	0	12	1.693e-4	1	NC	1	NC	1
252			min	0	5	-.003	3	-.044	4	-8.821e-5	5	NC	1	564.344	4
253		13	max	0	1	.002	2	0	12	1.693e-4	1	NC	1	NC	1
254			min	0	5	-.003	3	-.033	4	-8.821e-5	5	NC	1	743.518	4
255		14	max	0	1	.002	2	0	12	1.693e-4	1	NC	1	NC	1
256			min	0	5	-.002	3	-.024	4	-8.821e-5	5	NC	1	1032.723	4
257		15	max	0	1	.002	2	0	12	1.693e-4	1	NC	1	NC	1
258			min	0	5	-.002	3	-.016	4	-8.821e-5	5	NC	1	1546.572	4
259		16	max	0	1	.001	2	0	12	1.693e-4	1	NC	1	NC	1
260			min	0	5	-.001	3	-.01	4	-8.821e-5	5	NC	1	2601.845	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	1.693e-4	1	NC	1	NC	1
262			min	0	5	0	3	-.005	4	-8.821e-5	5	NC	1	5372.802	4
263		18	max	0	1	0	2	0	12	1.693e-4	1	NC	1	NC	1
264			min	0	5	0	3	-.001	4	-8.821e-5	5	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.693e-4	1	NC	1	NC	1
266			min	0	1	0	1	0	1	-8.821e-5	5	NC	1	NC	1
267	M6	1	max	.024	2	.036	2	0	1	2.485e-3	4	NC	3	NC	1
268			min	-.032	3	-.05	3	-.78	4	0	1	2139.79	2	99.311	4
269		2	max	.022	2	.033	2	0	1	2.521e-3	4	NC	3	NC	1
270			min	-.03	3	-.048	3	-.717	4	0	1	2353.3	2	108.09	4
271		3	max	.021	2	.03	2	0	1	2.557e-3	4	NC	3	NC	1
272			min	-.028	3	-.045	3	-.654	4	0	1	2611.83	2	118.508	4
273		4	max	.02	2	.026	2	0	1	2.593e-3	4	NC	3	NC	1
274			min	-.027	3	-.042	3	-.592	4	0	1	2928.425	2	130.993	4
275		5	max	.018	2	.023	2	0	1	2.629e-3	4	NC	3	NC	1
276			min	-.025	3	-.04	3	-.53	4	0	1	3321.387	2	146.123	4
277		6	max	.017	2	.02	2	0	1	2.665e-3	4	NC	3	NC	1
278			min	-.023	3	-.037	3	-.47	4	0	1	3817.042	2	164.701	4
279		7	max	.016	2	.017	2	0	1	2.701e-3	4	NC	1	NC	1
280			min	-.021	3	-.034	3	-.412	4	0	1	4454.391	2	187.866	4
281		8	max	.015	2	.015	2	0	1	2.737e-3	4	NC	1	NC	1
282			min	-.02	3	-.031	3	-.357	4	0	1	5293.246	2	217.274	4
283		9	max	.013	2	.012	2	0	1	2.773e-3	4	NC	1	NC	1
284			min	-.018	3	-.028	3	-.303	4	0	1	6429.265	2	255.42	4
285		10	max	.012	2	.01	2	0	1	2.809e-3	4	NC	1	NC	1
286			min	-.016	3	-.026	3	-.253	4	0	1	8023.484	2	306.195	4
287		11	max	.011	2	.007	2	0	1	2.845e-3	4	NC	1	NC	1
288			min	-.014	3	-.023	3	-.206	4	0	1	NC	1	375.959	4
289		12	max	.009	2	.006	2	0	1	2.881e-3	4	NC	1	NC	1
290			min	-.012	3	-.02	3	-.163	4	0	1	NC	1	475.693	4
291		13	max	.008	2	.004	2	0	1	2.917e-3	4	NC	1	NC	1
292			min	-.011	3	-.017	3	-.124	4	0	1	NC	1	625.74	4
293		14	max	.007	2	.002	2	0	1	2.953e-3	4	NC	1	NC	1
294			min	-.009	3	-.014	3	-.089	4	0	1	NC	1	867.385	4
295		15	max	.005	2	.001	2	0	1	2.989e-3	4	NC	1	NC	1
296			min	-.007	3	-.011	3	-.06	4	0	1	NC	1	1295.493	4
297		16	max	.004	2	0	2	0	1	3.025e-3	4	NC	1	NC	1
298			min	-.005	3	-.009	3	-.036	4	0	1	NC	1	2171.136	4
299		17	max	.003	2	0	2	0	1	3.06e-3	4	NC	1	NC	1
300			min	-.004	3	-.006	3	-.017	4	0	1	NC	1	4455.578	4
301		18	max	.001	2	0	2	0	1	3.096e-3	4	NC	1	NC	1
302			min	-.002	3	-.003	3	-.005	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	3.132e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-6.795e-4	4	NC	1	NC	1
307		2	max	.001	3	0	15	.017	4	0	1	NC	1	NC	1
308			min	-.001	2	-.004	3	0	1	-9.403e-6	5	NC	1	NC	1
309		3	max	.003	3	-.001	15	.032	4	6.629e-4	4	NC	1	NC	1
310			min	-.003	2	-.007	3	0	1	0	1	NC	1	NC	1
311		4	max	.004	3	-.002	15	.047	4	1.334e-3	4	NC	1	NC	1
312			min	-.004	2	-.011	3	0	1	0	1	NC	1	7894.714	4
313		5	max	.006	3	-.003	15	.06	4	2.005e-3	4	NC	1	NC	1
314			min	-.006	2	-.014	3	0	1	0	1	8270.23	3	6876.094	4
315		6	max	.007	3	-.004	15	.072	4	2.677e-3	4	NC	1	NC	1
316			min	-.007	2	-.016	3	0	1	0	1	6921.177	4	6502.503	4
317		7	max	.009	3	-.004	15	.083	4	3.348e-3	4	NC	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.008	2	-.019	3	0	1	0	1	5944.462	4	6546.072	4
319		8	max	.01	3	-.005	15	.093	4	4.019e-3	4	NC	2	NC	1
320			min	-.01	2	-.02	3	0	1	0	1	5342.05	4	6966.268	4
321		9	max	.012	3	-.005	15	.103	4	4.69e-3	4	NC	5	NC	1
322			min	-.011	2	-.021	3	0	1	0	1	4986.473	4	7843.746	4
323		10	max	.013	3	-.005	15	.112	4	5.361e-3	4	NC	5	NC	1
324			min	-.012	2	-.022	3	0	1	0	1	4815.922	4	9425.776	4
325		11	max	.015	3	-.005	15	.12	4	6.033e-3	4	NC	5	NC	1
326			min	-.014	2	-.022	3	0	1	0	1	4805.318	4	NC	1
327		12	max	.016	3	-.005	15	.129	4	6.704e-3	4	NC	5	NC	1
328			min	-.015	2	-.022	3	0	1	0	1	4956.693	4	NC	1
329		13	max	.017	3	-.005	15	.137	4	7.375e-3	4	NC	5	NC	1
330			min	-.017	2	-.021	3	0	1	0	1	5301.206	4	NC	1
331		14	max	.019	3	-.004	15	.146	4	8.046e-3	4	NC	2	NC	1
332			min	-.018	2	-.019	3	0	1	0	1	5915.244	4	NC	1
333		15	max	.02	3	-.004	15	.155	4	8.717e-3	4	NC	1	NC	1
334			min	-.019	2	-.017	3	0	1	0	1	6967.892	4	NC	1
335		16	max	.022	3	-.003	15	.165	4	9.389e-3	4	NC	1	NC	1
336			min	-.021	2	-.015	3	0	1	0	1	8868.493	4	NC	1
337		17	max	.023	3	-.002	15	.176	4	1.006e-2	4	NC	1	NC	1
338			min	-.022	2	-.012	3	0	1	0	1	NC	1	NC	1
339		18	max	.025	3	-.001	15	.188	4	1.073e-2	4	NC	1	NC	1
340			min	-.024	2	-.009	3	0	1	0	1	NC	1	NC	1
341		19	max	.026	3	0	10	.202	4	1.14e-2	4	NC	1	NC	1
342			min	-.025	2	-.006	3	0	1	0	1	NC	1	NC	1
343	M8	1	max	.006	1	.024	2	0	1	0	1	NC	1	NC	1
344			min	0	3	-.027	3	-.202	4	-2.756e-4	4	NC	1	122.794	4
345		2	max	.006	1	.023	2	0	1	0	1	NC	1	NC	1
346			min	0	3	-.025	3	-.186	4	-2.756e-4	4	NC	1	133.523	4
347		3	max	.006	1	.022	2	0	1	0	1	NC	1	NC	1
348			min	0	3	-.024	3	-.17	4	-2.756e-4	4	NC	1	146.292	4
349		4	max	.005	1	.02	2	0	1	0	1	NC	1	NC	1
350			min	0	3	-.022	3	-.153	4	-2.756e-4	4	NC	1	161.631	4
351		5	max	.005	1	.019	2	0	1	0	1	NC	1	NC	1
352			min	0	3	-.021	3	-.138	4	-2.756e-4	4	NC	1	180.258	4
353		6	max	.005	1	.018	2	0	1	0	1	NC	1	NC	1
354			min	0	3	-.019	3	-.122	4	-2.756e-4	4	NC	1	203.173	4
355		7	max	.004	1	.016	2	0	1	0	1	NC	1	NC	1
356			min	0	3	-.018	3	-.107	4	-2.756e-4	4	NC	1	231.794	4
357		8	max	.004	1	.015	2	0	1	0	1	NC	1	NC	1
358			min	0	3	-.016	3	-.092	4	-2.756e-4	4	NC	1	268.186	4
359		9	max	.003	1	.013	2	0	1	0	1	NC	1	NC	1
360			min	0	3	-.015	3	-.079	4	-2.756e-4	4	NC	1	315.461	4
361		10	max	.003	1	.012	2	0	1	0	1	NC	1	NC	1
362			min	0	3	-.013	3	-.066	4	-2.756e-4	4	NC	1	378.483	4
363		11	max	.003	1	.011	2	0	1	0	1	NC	1	NC	1
364			min	0	3	-.012	3	-.053	4	-2.756e-4	4	NC	1	465.209	4
365		12	max	.002	1	.009	2	0	1	0	1	NC	1	NC	1
366			min	0	3	-.01	3	-.042	4	-2.756e-4	4	NC	1	589.4	4
367		13	max	.002	1	.008	2	0	1	0	1	NC	1	NC	1
368			min	0	3	-.009	3	-.032	4	-2.756e-4	4	NC	1	776.6	4
369		14	max	.002	1	.007	2	0	1	0	1	NC	1	NC	1
370			min	0	3	-.007	3	-.023	4	-2.756e-4	4	NC	1	1078.768	4
371		15	max	.001	1	.005	2	0	1	0	1	NC	1	NC	1
372			min	0	3	-.006	3	-.015	4	-2.756e-4	4	NC	1	1615.671	4
373		16	max	.001	1	.004	2	0	1	0	1	NC	1	NC	1
374			min	0	3	-.004	3	-.009	4	-2.756e-4	4	NC	1	2718.348	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	1	.003	2	0	1	0	1	NC	1	NC	1
376			min	0	3	-.003	3	-.004	4	-2.756e-4	4	NC	1	5613.994	4
377		18	max	0	1	.001	2	0	1	0	1	NC	1	NC	1
378			min	0	3	-.001	3	-.001	4	-2.756e-4	4	NC	1	NC	1
379		19	max	0	1	0	1	0	1	0	1	NC	1	NC	1
380			min	0	1	0	1	0	1	-2.756e-4	4	NC	1	NC	1
381	M10	1	max	.008	2	.01	2	0	12	2.473e-3	4	NC	1	NC	2
382			min	-.01	3	-.016	3	-.778	4	1.779e-5	12	7437.462	2	99.581	4
383		2	max	.007	2	.009	2	0	12	2.508e-3	4	NC	1	NC	2
384			min	-.01	3	-.016	3	-.715	4	1.691e-5	12	8736.538	2	108.385	4
385		3	max	.007	2	.007	2	0	12	2.542e-3	4	NC	1	NC	2
386			min	-.009	3	-.016	3	-.652	4	1.602e-5	12	NC	1	118.833	4
387		4	max	.006	2	.006	2	0	12	2.577e-3	4	NC	1	NC	1
388			min	-.008	3	-.015	3	-.59	4	1.514e-5	12	NC	1	131.353	4
389		5	max	.006	2	.004	2	0	12	2.611e-3	4	NC	1	NC	1
390			min	-.008	3	-.014	3	-.529	4	1.425e-5	12	NC	1	146.526	4
391		6	max	.006	2	.003	2	0	12	2.646e-3	4	NC	1	NC	1
392			min	-.007	3	-.014	3	-.469	4	1.337e-5	12	NC	1	165.157	4
393		7	max	.005	2	.002	2	0	12	2.68e-3	4	NC	1	NC	1
394			min	-.007	3	-.013	3	-.411	4	1.248e-5	12	NC	1	188.389	4
395		8	max	.005	2	0	2	0	12	2.715e-3	4	NC	1	NC	1
396			min	-.006	3	-.013	3	-.356	4	1.16e-5	12	NC	1	217.884	4
397		9	max	.004	2	0	2	0	12	2.75e-3	4	NC	1	NC	1
398			min	-.006	3	-.012	3	-.303	4	1.071e-5	12	NC	1	256.143	4
399		10	max	.004	2	-.001	2	0	12	2.784e-3	4	NC	1	NC	1
400			min	-.005	3	-.011	3	-.252	4	9.826e-6	12	NC	1	307.071	4
401		11	max	.003	2	-.002	2	0	12	2.819e-3	4	NC	1	NC	1
402			min	-.004	3	-.01	3	-.206	4	8.94e-6	12	NC	1	377.05	4
403		12	max	.003	2	-.002	15	0	12	2.853e-3	4	NC	1	NC	1
404			min	-.004	3	-.009	3	-.162	4	8.055e-6	12	NC	1	477.098	4
405		13	max	.003	2	-.002	15	0	12	2.888e-3	4	NC	1	NC	1
406			min	-.003	3	-.008	3	-.123	4	7.17e-6	12	NC	1	627.633	4
407		14	max	.002	2	-.002	15	0	12	2.922e-3	4	NC	1	NC	1
408			min	-.003	3	-.007	3	-.089	4	6.285e-6	12	NC	1	870.095	4
409		15	max	.002	2	-.002	15	0	12	2.957e-3	4	NC	1	NC	1
410			min	-.002	3	-.006	4	-.06	4	5.399e-6	12	NC	1	1299.729	4
411		16	max	.001	2	-.001	15	0	12	2.991e-3	4	NC	1	NC	1
412			min	-.002	3	-.005	4	-.036	4	4.514e-6	12	NC	1	2178.737	4
413		17	max	0	2	0	15	0	12	3.026e-3	4	NC	1	NC	1
414			min	-.001	3	-.004	4	-.017	4	3.629e-6	12	NC	1	4473.057	4
415		18	max	0	2	0	15	0	12	3.06e-3	4	NC	1	NC	1
416			min	0	3	-.002	4	-.005	4	2.744e-6	12	NC	1	NC	1
417		19	max	0	1	0	1	0	1	3.095e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	1.859e-6	12	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	-3.745e-7	12	NC	1	NC	1
420			min	0	1	0	1	0	1	-6.705e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.017	4	1.27e-5	5	NC	1	NC	1
422			min	0	2	-.003	4	0	12	-2.976e-5	1	NC	1	NC	1
423		3	max	0	3	-.002	15	.032	4	6.862e-4	5	NC	1	NC	1
424			min	0	2	-.006	4	0	12	-5.508e-5	1	NC	1	NC	1
425		4	max	.001	3	-.002	15	.046	4	1.363e-3	4	NC	1	NC	1
426			min	-.001	2	-.009	4	0	12	-8.039e-5	1	NC	1	8621.769	4
427		5	max	.002	3	-.003	15	.059	4	2.04e-3	4	NC	1	NC	1
428			min	-.002	2	-.013	4	0	12	-1.057e-4	1	8243.266	4	7601.906	4
429		6	max	.002	3	-.004	15	.071	4	2.718e-3	4	NC	5	NC	1
430			min	-.002	2	-.016	4	0	12	-1.31e-4	1	6699.263	4	7300.24	4
431		7	max	.003	3	-.004	15	.082	4	3.396e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.002	2	-.018	4	0	10	-1.563e-4	1	5768.534	4	7497.024	4
433		8	max	.003	3	-.005	15	.092	4	4.073e-3	4	NC	5	NC	1
434			min	-.003	2	-.02	4	0	1	-1.817e-4	1	5194.862	4	8195.982	4
435		9	max	.004	3	-.005	15	.102	4	4.751e-3	4	NC	5	NC	1
436			min	-.003	2	-.022	4	0	1	-2.07e-4	1	4857.598	4	9590.837	4
437		10	max	.004	3	-.006	15	.111	4	5.429e-3	4	NC	5	NC	1
438			min	-.004	2	-.022	4	0	1	-2.323e-4	1	4698.384	4	NC	1
439		11	max	.005	3	-.006	15	.12	4	6.106e-3	4	NC	5	NC	1
440			min	-.004	2	-.023	4	-.001	1	-2.576e-4	1	4693.883	4	NC	1
441		12	max	.005	3	-.005	15	.128	4	6.784e-3	4	NC	5	NC	1
442			min	-.004	2	-.022	4	-.002	1	-2.829e-4	1	4846.846	4	NC	1
443		13	max	.006	3	-.005	15	.137	4	7.462e-3	4	NC	5	NC	1
444			min	-.005	2	-.021	4	-.002	1	-3.082e-4	1	5188.318	4	NC	1
445		14	max	.006	3	-.005	15	.146	4	8.139e-3	4	NC	5	NC	1
446			min	-.005	2	-.019	4	-.003	1	-3.336e-4	1	5793.552	4	NC	1
447		15	max	.007	3	-.004	15	.156	4	8.817e-3	4	NC	3	NC	1
448			min	-.006	2	-.016	4	-.004	1	-3.589e-4	1	6828.656	4	NC	1
449		16	max	.007	3	-.003	15	.166	4	9.495e-3	4	NC	1	NC	1
450			min	-.006	2	-.013	4	-.005	1	-3.842e-4	1	8695.402	4	NC	1
451		17	max	.008	3	-.002	15	.178	4	1.017e-2	4	NC	1	NC	1
452			min	-.006	2	-.009	4	-.006	1	-4.095e-4	1	NC	1	NC	1
453		18	max	.008	3	-.002	15	.19	4	1.085e-2	4	NC	1	NC	1
454			min	-.007	2	-.006	4	-.008	1	-4.348e-4	1	NC	1	NC	1
455		19	max	.009	3	0	10	.205	4	1.153e-2	4	NC	1	NC	1
456			min	-.007	2	-.002	3	-.009	1	-4.601e-4	1	NC	1	NC	1
457	M12	1	max	.002	1	.007	2	.009	1	-1.156e-5	12	NC	1	NC	3
458			min	0	3	-.009	3	-.205	4	-1.693e-4	1	NC	1	120.984	4
459		2	max	.002	1	.006	2	.008	1	-1.156e-5	12	NC	1	NC	3
460			min	0	3	-.008	3	-.189	4	-1.693e-4	1	NC	1	131.543	4
461		3	max	.002	1	.006	2	.008	1	-1.156e-5	12	NC	1	NC	3
462			min	0	3	-.008	3	-.172	4	-1.693e-4	1	NC	1	144.11	4
463		4	max	.002	1	.006	2	.007	1	-1.156e-5	12	NC	1	NC	3
464			min	0	3	-.007	3	-.156	4	-1.693e-4	1	NC	1	159.206	4
465		5	max	.002	1	.005	2	.006	1	-1.156e-5	12	NC	1	NC	3
466			min	0	3	-.007	3	-.14	4	-1.693e-4	1	NC	1	177.54	4
467		6	max	.002	1	.005	2	.006	1	-1.156e-5	12	NC	1	NC	2
468			min	0	3	-.006	3	-.124	4	-1.693e-4	1	NC	1	200.094	4
469		7	max	.002	1	.005	2	.005	1	-1.156e-5	12	NC	1	NC	2
470			min	0	3	-.006	3	-.109	4	-1.693e-4	1	NC	1	228.265	4
471		8	max	.001	1	.004	2	.004	1	-1.156e-5	12	NC	1	NC	2
472			min	0	3	-.005	3	-.094	4	-1.693e-4	1	NC	1	264.084	4
473		9	max	.001	1	.004	2	.004	1	-1.156e-5	12	NC	1	NC	2
474			min	0	3	-.005	3	-.08	4	-1.693e-4	1	NC	1	310.616	4
475		10	max	.001	1	.003	2	.003	1	-1.156e-5	12	NC	1	NC	2
476			min	0	3	-.004	3	-.067	4	-1.693e-4	1	NC	1	372.647	4
477		11	max	.001	1	.003	2	.002	1	-1.156e-5	12	NC	1	NC	1
478			min	0	3	-.004	3	-.054	4	-1.693e-4	1	NC	1	458.007	4
479		12	max	0	1	.003	2	.002	1	-1.156e-5	12	NC	1	NC	1
480			min	0	3	-.003	3	-.043	4	-1.693e-4	1	NC	1	580.242	4
481		13	max	0	1	.002	2	.001	1	-1.156e-5	12	NC	1	NC	1
482			min	0	3	-.003	3	-.032	4	-1.693e-4	1	NC	1	764.489	4
483		14	max	0	1	.002	2	.001	1	-1.156e-5	12	NC	1	NC	1
484			min	0	3	-.002	3	-.023	4	-1.693e-4	1	NC	1	1061.884	4
485		15	max	0	1	.002	2	0	1	-1.156e-5	12	NC	1	NC	1
486			min	0	3	-.002	3	-.016	4	-1.693e-4	1	NC	1	1590.293	4
487		16	max	0	1	.001	2	0	1	-1.156e-5	12	NC	1	NC	1
488			min	0	3	-.001	3	-.009	4	-1.693e-4	1	NC	1	2675.489	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	-1.156e-5	12	NC	1	NC	1
490			min	0	3	0	3	-.004	4	-1.693e-4	1	NC	1	5525.094	4
491		18	max	0	1	0	2	0	1	-1.156e-5	12	NC	1	NC	1
492			min	0	3	0	3	-.001	4	-1.693e-4	1	NC	1	NC	1
493		19	max	0	1	0	1	0	1	-1.156e-5	12	NC	1	NC	1
494			min	0	1	0	1	0	1	-1.693e-4	1	NC	1	NC	1
495	M1	1	max	.011	3	.197	2	.825	4	8.817e-3	2	NC	1	NC	1
496			min	-.006	2	-.051	3	0	12	-1.912e-2	3	NC	1	NC	1
497		2	max	.011	3	.095	2	.799	4	8.007e-3	4	NC	5	NC	1
498			min	-.006	2	-.023	3	-.007	1	-9.49e-3	3	1335.586	2	9603.23	5
499		3	max	.011	3	.017	3	.772	4	1.422e-2	4	NC	5	NC	1
500			min	-.006	2	-.013	2	-.01	1	-1.95e-4	1	646.355	2	5324.42	5
501		4	max	.011	3	.078	3	.743	4	1.227e-2	4	NC	15	NC	1
502			min	-.006	2	-.133	2	-.009	1	-4.365e-3	3	410.869	2	3885.29	5
503		5	max	.01	3	.154	3	.713	4	1.032e-2	4	NC	15	NC	1
504			min	-.006	2	-.258	2	-.006	1	-8.622e-3	3	298.145	2	3160.513	5
505		6	max	.01	3	.236	3	.682	4	1.264e-2	2	8450.206	15	NC	1
506			min	-.006	2	-.378	2	-.003	1	-1.288e-2	3	235.782	2	2715.645	5
507		7	max	.01	3	.313	3	.651	4	1.686e-2	2	7134.929	15	NC	1
508			min	-.006	2	-.485	2	0	3	-1.714e-2	3	198.852	2	2387.726	4
509		8	max	.01	3	.378	3	.619	4	2.109e-2	2	6356.027	15	NC	1
510			min	-.006	2	-.57	2	0	12	-2.139e-2	3	176.962	2	2132.537	4
511		9	max	.01	3	.42	3	.587	4	2.375e-2	2	5948.256	15	NC	1
512			min	-.006	2	-.623	2	0	1	-2.189e-2	3	165.538	2	1953.509	4
513		10	max	.009	3	.435	3	.55	4	2.536e-2	2	5823.547	15	NC	1
514			min	-.005	2	-.641	2	0	12	-1.986e-2	3	162.193	2	1891.933	4
515		11	max	.009	3	.425	3	.511	4	2.698e-2	2	5947.919	15	NC	1
516			min	-.005	2	-.623	2	0	12	-1.784e-2	3	166.137	2	1917.418	4
517		12	max	.009	3	.389	3	.469	4	2.59e-2	2	6355.232	15	NC	1
518			min	-.005	2	-.567	2	0	1	-1.539e-2	3	178.735	2	2031.841	4
519		13	max	.009	3	.332	3	.42	4	2.078e-2	2	7133.388	15	NC	1
520			min	-.005	2	-.478	2	0	1	-1.231e-2	3	203.063	2	2392.15	4
521		14	max	.008	3	.258	3	.368	4	1.566e-2	2	8447.392	15	NC	1
522			min	-.005	2	-.367	2	0	12	-9.235e-3	3	244.632	2	3210.803	4
523		15	max	.008	3	.175	3	.313	4	1.054e-2	2	NC	15	NC	1
524			min	-.005	2	-.245	2	0	12	-6.157e-3	3	316.086	2	5175.575	4
525		16	max	.008	3	.089	3	.26	4	9.23e-3	4	NC	15	NC	1
526			min	-.005	2	-.121	2	0	12	-3.079e-3	3	448.066	2	NC	1
527		17	max	.008	3	.006	3	.211	4	1.049e-2	4	NC	5	NC	1
528			min	-.005	2	-.007	2	0	12	-7.173e-7	3	728.982	2	NC	1
529		18	max	.008	3	.089	2	.17	4	7.364e-3	2	NC	5	NC	1
530			min	-.005	2	-.07	3	0	12	-2.642e-3	3	1543.949	2	NC	1
531		19	max	.008	3	.174	2	.134	4	1.464e-2	2	NC	1	NC	1
532			min	-.005	2	-.141	3	0	1	-5.385e-3	3	NC	1	NC	1
533	M5	1	max	.033	3	.361	2	.825	4	0	1	NC	1	NC	1
534			min	-.023	2	-.027	3	0	1	-1.175e-5	4	NC	1	NC	1
535		2	max	.033	3	.173	2	.805	4	7.289e-3	4	NC	5	NC	1
536			min	-.023	2	-.008	3	0	1	0	1	726.996	2	7220.903	4
537		3	max	.033	3	.051	3	.78	4	1.441e-2	4	NC	15	NC	1
538			min	-.023	2	-.041	2	0	1	0	1	340.194	2	4279.497	4
539		4	max	.032	3	.183	3	.75	4	1.174e-2	4	8349.012	15	NC	1
540			min	-.023	2	-.298	2	0	1	0	1	207.014	2	3351.126	4
541		5	max	.032	3	.366	3	.718	4	9.075e-3	4	5807.603	15	NC	1
542			min	-.023	2	-.579	2	0	1	0	1	144.916	2	2914.279	4
543		6	max	.031	3	.572	3	.684	4	6.405e-3	4	4451.307	15	NC	1
544			min	-.022	2	-.859	2	0	1	0	1	111.547	2	2644.355	4
545		7	max	.03	3	.773	3	.65	4	3.735e-3	4	3671.561	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.022	2	-1.114	2	0	1	0	1	92.257	2	2415.673	4
547		8	max	.03	3	.943	3	.618	4	1.065e-3	4	3219.856	15	NC	1
548			min	-.021	2	-1.319	2	0	1	0	1	81.039	2	2168.148	4
549		9	max	.029	3	1.052	3	.587	4	0	1	2988.567	15	NC	1
550			min	-.021	2	-1.45	2	0	1	-7.25e-6	5	75.28	2	1945.784	4
551		10	max	.028	3	1.091	3	.55	4	0	1	2918.886	15	NC	1
552			min	-.02	2	-1.494	2	0	1	-6.996e-6	5	73.601	2	1907.977	4
553		11	max	.027	3	1.064	3	.51	4	0	1	2988.745	15	NC	1
554			min	-.02	2	-1.45	2	0	1	-6.742e-6	5	75.582	2	1946.646	4
555		12	max	.027	3	.971	3	.47	4	7.347e-4	4	3220.277	15	NC	1
556			min	-.02	2	-1.314	2	0	1	0	1	82.03	2	1991.239	4
557		13	max	.026	3	.821	3	.422	4	2.578e-3	4	3672.41	15	NC	1
558			min	-.019	2	-1.097	2	0	1	0	1	94.84	2	2331.049	4
559		14	max	.025	3	.633	3	.367	4	4.422e-3	4	4452.95	15	NC	1
560			min	-.019	2	-.829	2	0	1	0	1	117.428	2	3291.739	4
561		15	max	.025	3	.424	3	.309	4	6.265e-3	4	5810.834	15	NC	1
562			min	-.019	2	-.54	2	0	1	0	1	157.92	2	6303.46	4
563		16	max	.024	3	.213	3	.253	4	8.109e-3	4	8355.772	15	NC	1
564			min	-.018	2	-.26	2	0	1	0	1	236.963	2	NC	1
565		17	max	.023	3	.017	3	.203	4	9.952e-3	4	NC	15	NC	1
566			min	-.018	2	-.021	2	0	1	0	1	415.623	2	NC	1
567		18	max	.023	3	.155	2	.163	4	5.033e-3	4	NC	5	NC	1
568			min	-.018	2	-.149	3	0	1	0	1	936.034	2	NC	1
569		19	max	.023	3	.294	2	.134	4	0	1	NC	1	NC	1
570			min	-.018	2	-.297	3	0	1	-6.906e-6	4	NC	1	NC	1
571	M9	1	max	.011	3	.197	2	.825	4	1.912e-2	3	NC	1	NC	1
572			min	-.006	2	-.051	3	0	1	-8.817e-3	2	NC	1	NC	1
573		2	max	.011	3	.095	2	.804	4	9.49e-3	3	NC	5	NC	1
574			min	-.006	2	-.023	3	0	12	-4.317e-3	2	1335.586	2	7866.652	4
575		3	max	.011	3	.017	3	.778	4	1.436e-2	4	NC	5	NC	1
576			min	-.006	2	-.013	2	0	12	-1.139e-5	10	646.355	2	4558.284	4
577		4	max	.011	3	.078	3	.748	4	1.131e-2	5	NC	15	NC	1
578			min	-.006	2	-.133	2	0	12	-4.195e-3	2	410.869	2	3482.515	4
579		5	max	.01	3	.154	3	.717	4	8.622e-3	3	NC	15	NC	1
580			min	-.006	2	-.258	2	0	12	-8.418e-3	2	298.145	2	2957.929	4
581		6	max	.01	3	.236	3	.684	4	1.288e-2	3	8408.944	15	NC	1
582			min	-.006	2	-.378	2	0	12	-1.264e-2	2	235.782	2	2634.262	4
583		7	max	.01	3	.313	3	.651	4	1.714e-2	3	7101.114	15	NC	1
584			min	-.006	2	-.485	2	0	1	-1.686e-2	2	198.852	2	2384.357	4
585		8	max	.01	3	.378	3	.619	4	2.139e-2	3	6326.523	15	NC	1
586			min	-.006	2	-.57	2	0	1	-2.109e-2	2	176.962	2	2149.231	4
587		9	max	.01	3	.42	3	.587	4	2.189e-2	3	5920.953	15	NC	1
588			min	-.006	2	-.623	2	0	12	-2.375e-2	2	165.538	2	1947.135	4
589		10	max	.009	3	.435	3	.55	4	1.986e-2	3	5796.879	15	NC	1
590			min	-.005	2	-.641	2	0	1	-2.536e-2	2	162.193	2	1892.965	4
591		11	max	.009	3	.425	3	.511	4	1.784e-2	3	5920.589	15	NC	1
592			min	-.005	2	-.623	2	0	1	-2.698e-2	2	166.137	2	1925.14	4
593		12	max	.009	3	.389	3	.469	4	1.539e-2	3	6325.824	15	NC	1
594			min	-.005	2	-.567	2	0	12	-2.59e-2	2	178.735	2	2016.623	4
595		13	max	.009	3	.332	3	.421	4	1.231e-2	3	7100.025	15	NC	1
596			min	-.005	2	-.478	2	0	10	-2.078e-2	2	203.063	2	2390.691	4
597		14	max	.008	3	.258	3	.366	4	9.235e-3	3	8407.291	15	NC	1
598			min	-.005	2	-.367	2	-.002	1	-1.566e-2	2	244.632	2	3308.859	5
599		15	max	.008	3	.175	3	.31	4	6.157e-3	3	NC	15	NC	1
600			min	-.005	2	-.245	2	-.006	1	-1.054e-2	2	316.086	2	5701.551	5
601		16	max	.008	3	.089	3	.255	4	8.084e-3	5	NC	15	NC	1
602			min	-.005	2	-.121	2	-.008	1	-5.421e-3	2	448.066	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.008	3	.006	3	.206	4	1.014e-2	4	NC	5	NC	1
604			min	-.005	2	-.007	2	-.009	1	-6.076e-4	1	728.982	2	NC	1
605		18	max	.008	3	.089	2	.166	4	4.93e-3	5	NC	5	NC	1
606			min	-.005	2	-.07	3	-.007	1	-7.364e-3	2	1543.949	2	NC	1
607		19	max	.008	3	.174	2	.134	4	5.385e-3	3	NC	1	NC	1
608			min	-.005	2	-.141	3	0	12	-1.464e-2	2	NC	1	NC	1

Anchor Designer™
Software
Version 2.4.6025.0

Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	1/5
Project:	Standard PVMax - Worst Case, 14-40 Inch Width		
Address:			
Phone:			
E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

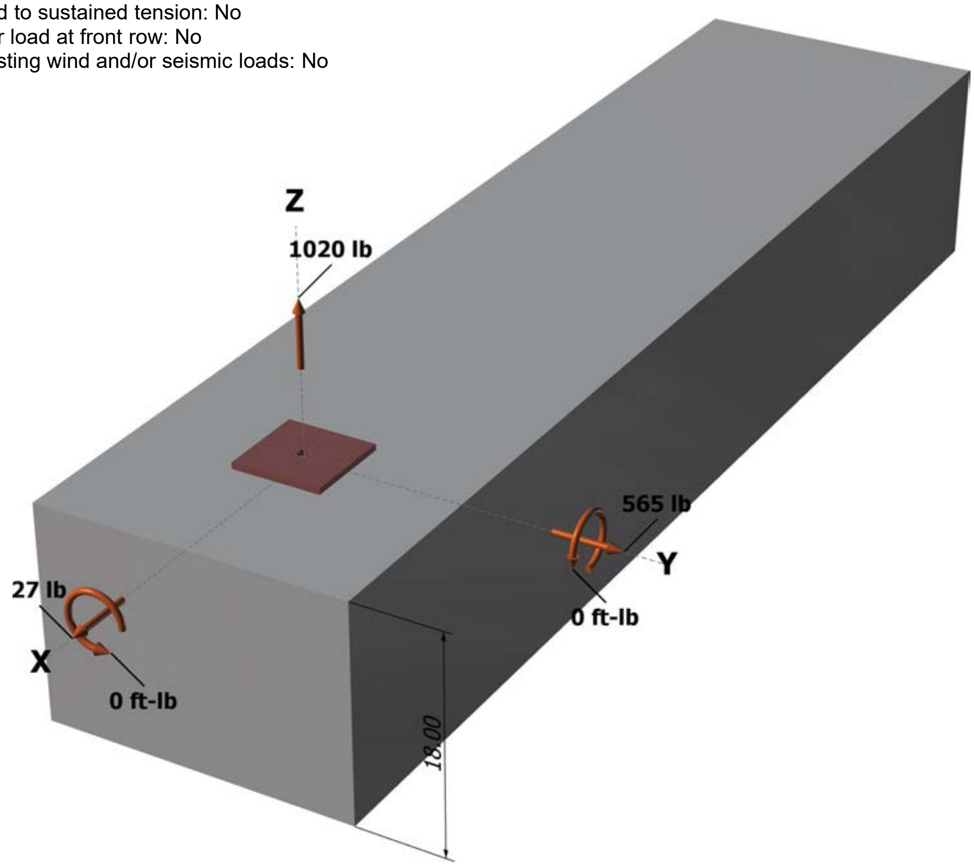
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'$_c$ (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>

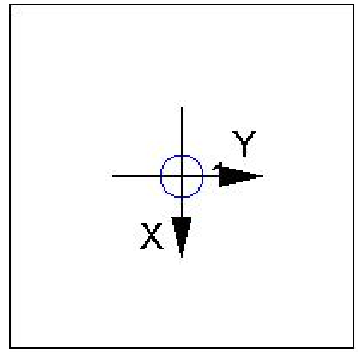
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1020.0	27.0	565.0	565.6
Sum	1020.0	27.0	565.0	565.6

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1020
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\Psi_{p,Na}N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi \min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	1020	6071	0.17	Pass
Concrete breakout	1020	5710	0.18	Pass
Adhesive	**1020**	**5365**	**0.19**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**566**	**3156**	**0.18**	**Pass (Governs)**
T Concrete breakout y+	565	3934	0.14	Pass
T Concrete breakout x+	27	3018	0.01	Pass
|| Concrete breakout y+	27	8508	0.00	Pass
|| Concrete breakout x+	565	6875	0.08	Pass
Concrete breakout, combined	-	-	0.14	Pass
Pryout	566	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.19	0.00	19.0 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.

SIMPSON Strong-Tie	Anchor Designer™ Software Version 2.4.6025.0

Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	1/5
Project:	Standard PVMax - Worst Case, 21-31 Inch Width		
Address:			
Phone:			
E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

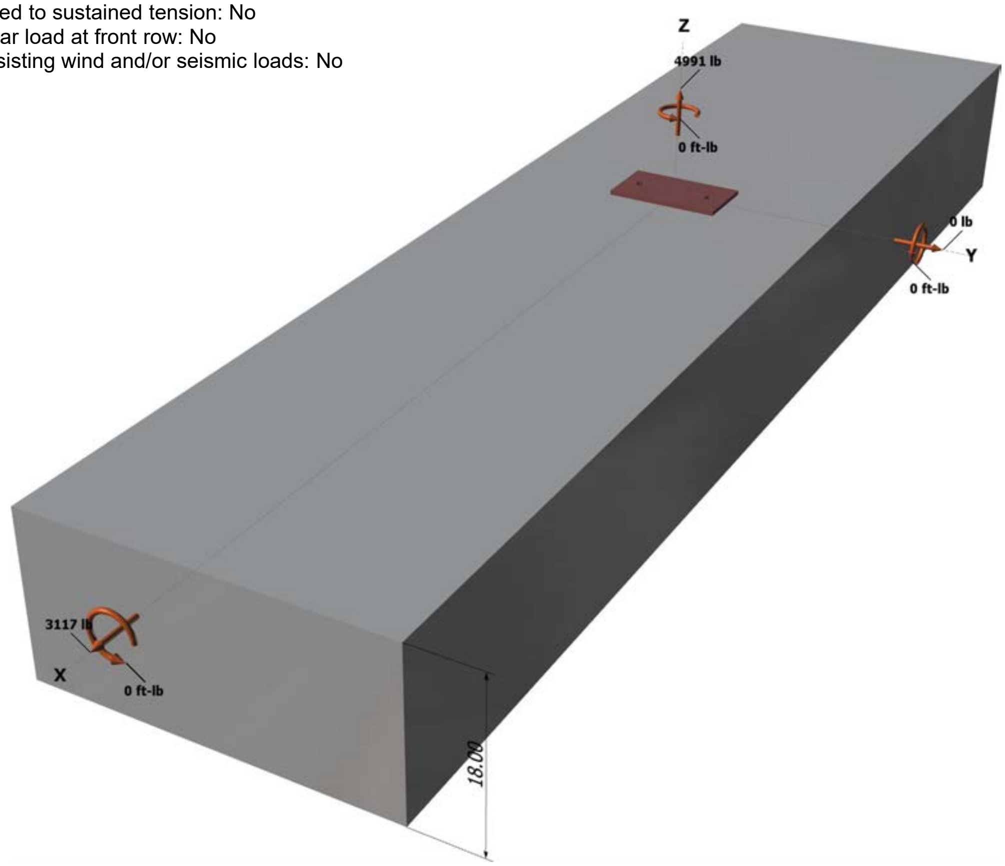
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

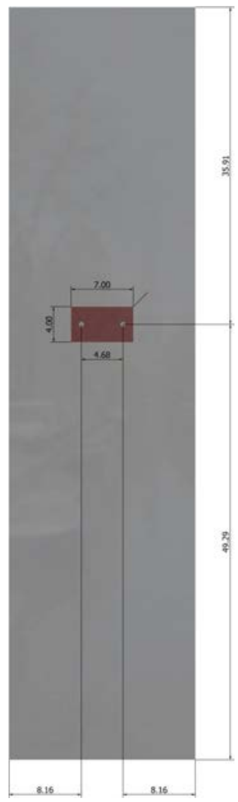
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



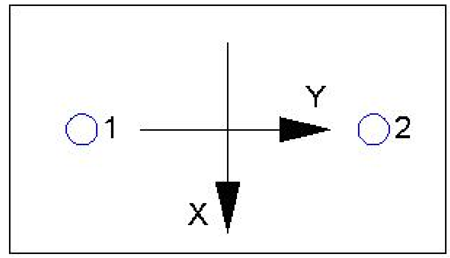
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2495.5	1558.5	0.0	1558.5
2	2495.5	1558.5	0.0	1558.5
Sum	4991.0	3117.0	0.0	3117.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 4991
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
378.00	324.00	1.000	0.972	1.00	1.000	12492	0.65	9208

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi (A_{Na} / A_{Na0}) \Psi_{ed,Na} \Psi_{g,Na} \Psi_{ec,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\ (A_{Vc} / A_{Vco})\ \Psi_{ec,V}\ \Psi_{ed,V}\ \Psi_{c,V}\ \Psi_{h,V} V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
378.00	648.00	1.000	0.836	1.000	1.000	15593	0.70	5323

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.16	8744

$\phi V_{cbx} = \phi\ (2)(A_{Vc} / A_{Vco})\ \Psi_{ed,V}\ \Psi_{c,V}\ \Psi_{h,V} V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
299.64	299.64	1.000	1.000	1.000	8744	0.70	12241

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\ \min|k_{cp}N_{ag}\ ;\ k_{cp}N_{cbg}| = \phi\ \min|k_{cp}(A_{Na} / A_{Na0})\ \Psi_{ed,Na}\ \Psi_{g,Na}\ \Psi_{ec,Na}\ \Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\ \Psi_{ec,N}\ \Psi_{ed,N}\ \Psi_{c,N}\ \Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
378.00	324.00	1.000	0.972	1.000	1.000	12492	14166	0.70

ϕV_{cpg} (lb)
19833

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	2496	6071	0.41	Pass
Concrete breakout	4991	9208	0.54	Pass
Adhesive	**4991**	**8093**	**0.62**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	1559	3156	0.49	Pass
T Concrete breakout x+	**3117**	**5323**	**0.59**	**Pass (Governs)**

|| Concrete breakout y-	**1559**	**12241**	**0.13**	**Pass (Governs)**
Pryout	3117	19833	0.16	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.3	0.62	0.59	120.2 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.