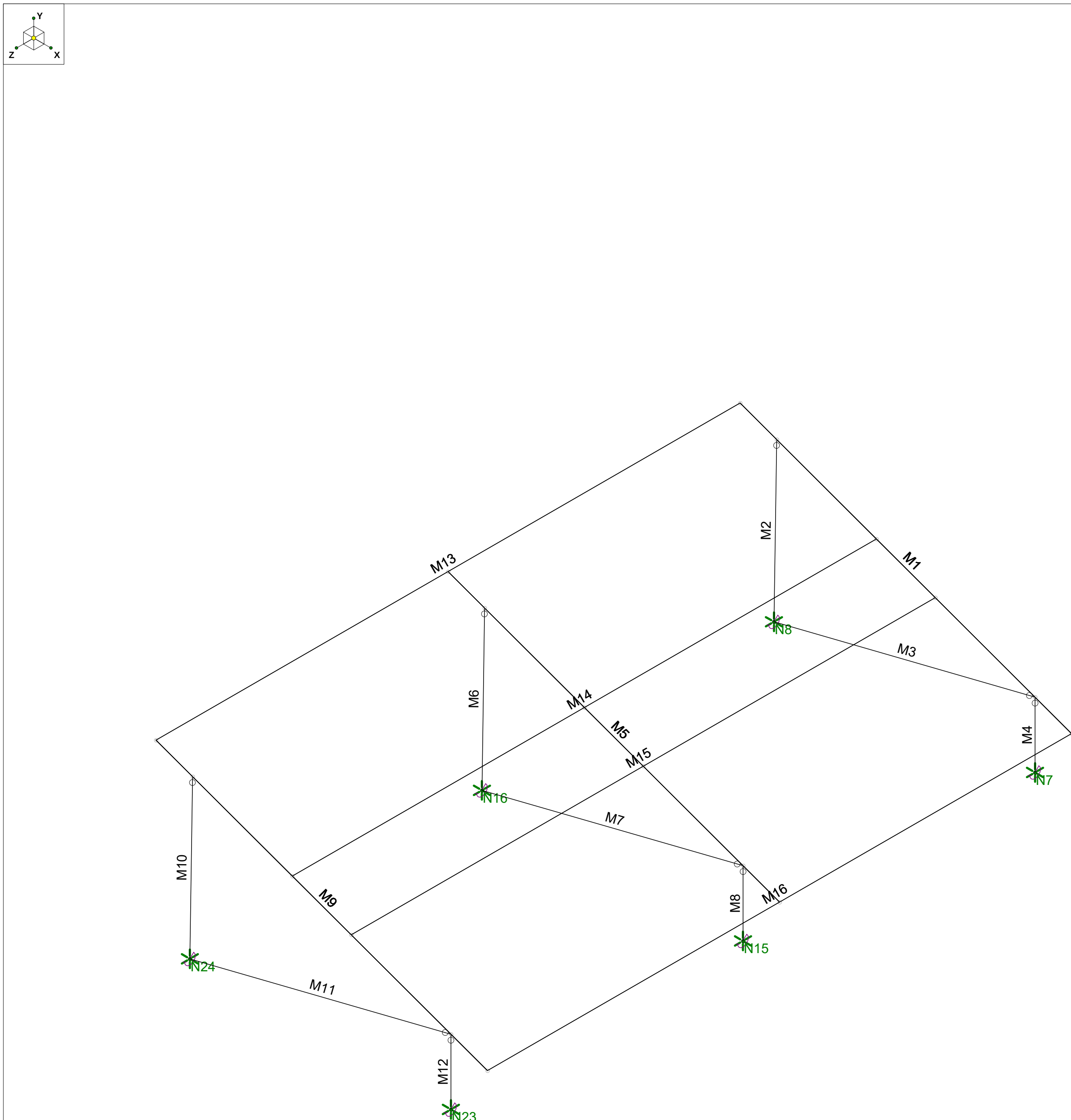


Schletter, Inc.	Standard PVMax Racking System Representative Calculations - ASCE 7-05	20° Tilt w/ Seismic Design
HCV		

1. INTRODUCTION

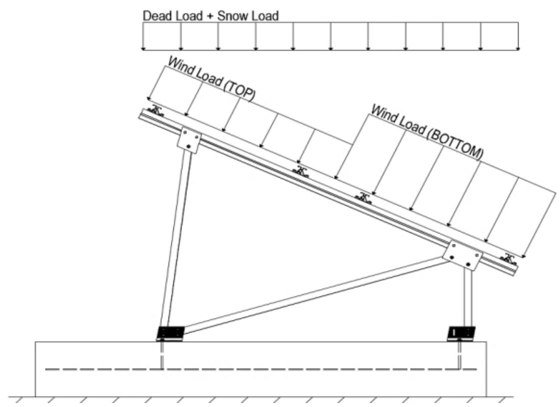
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	2000 mm	Height =	1900 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 2
Module Tilt = 20°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 20.62 psf *(ASCE 7-05, Eq. 7-2)*
I_s = 1.00
C_s = 0.91
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 85 mph
Height < 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 11.34 psf *Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.050	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.650	
$Cf-_{TOP, OUTER PURLIN}$	=	-2.400	
$Cf-_{TOP, INNER PURLIN}$	=	-1.840	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.000	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.06	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W
1.2D + 1.6W + 0.5S
0.9D + 1.6W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 1.0W
1.0D + 0.75L + 0.75W + 0.75S
0.6D + 1.0W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	**Diagonal Struts**	Location	**Front Reactions**	Location
M13	Top	M3	Outer	N7	Outer
M14	Mid-Top	M7	Inner	N15	Inner
M15	Mid-Bottom	M11	Outer	N23	Outer
M16	Bottom				

Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

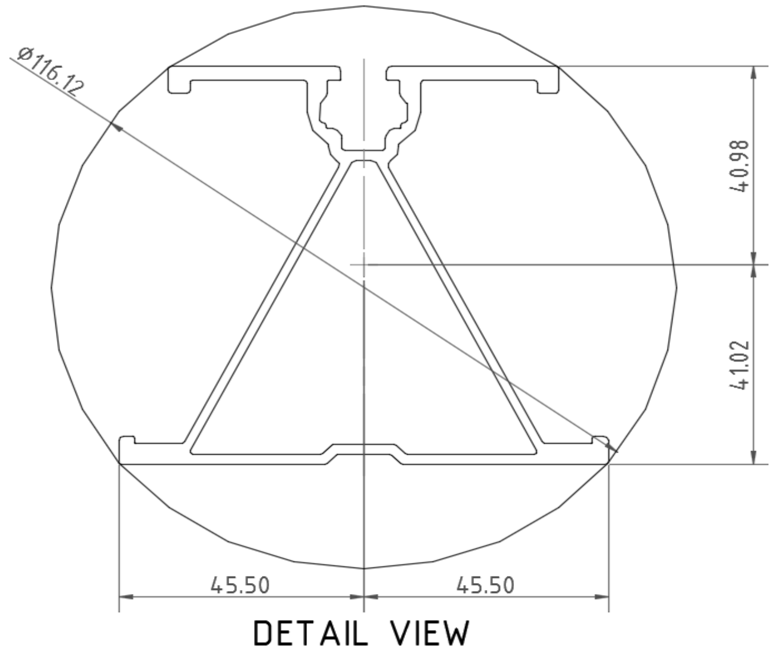
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

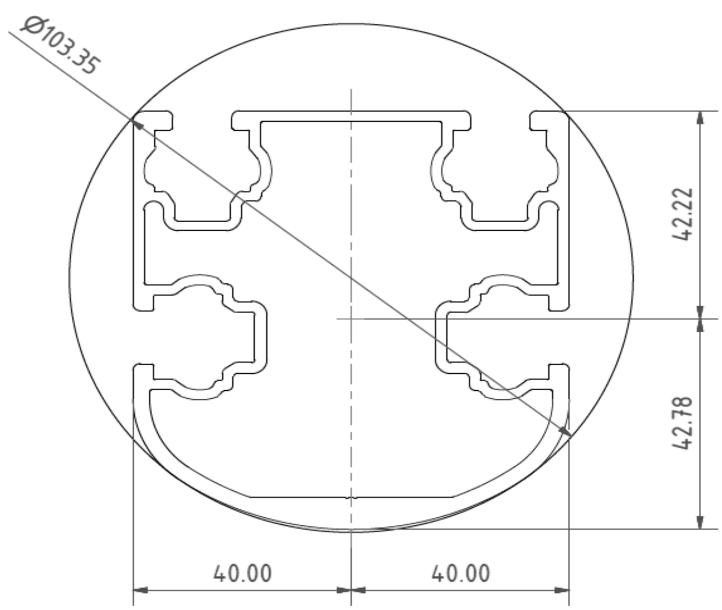
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	111	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.759	k-ft
M_z =	0.308	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	90%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

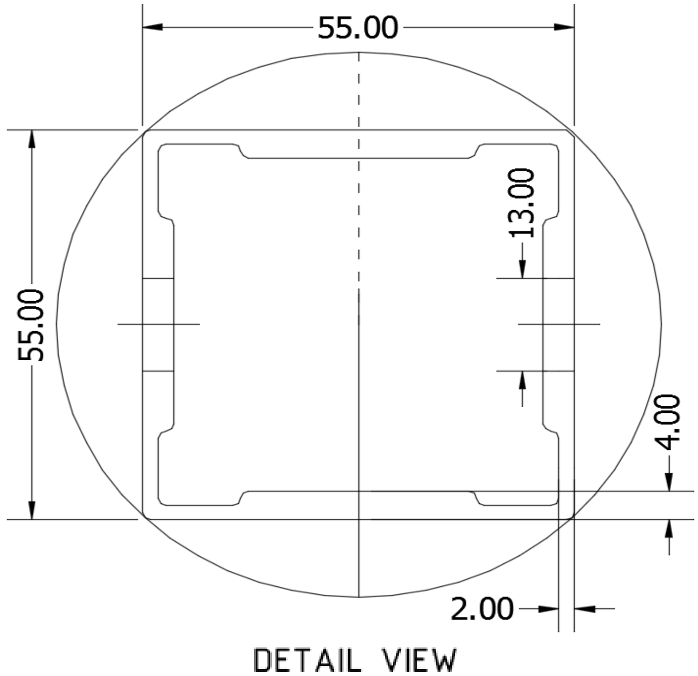
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	104.56	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.00	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-3.332	k-ft
M_z =	0.000	k-ft
P_n =	-0.360	k
$M_{y\ allowable}$ =	3.422	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	98%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

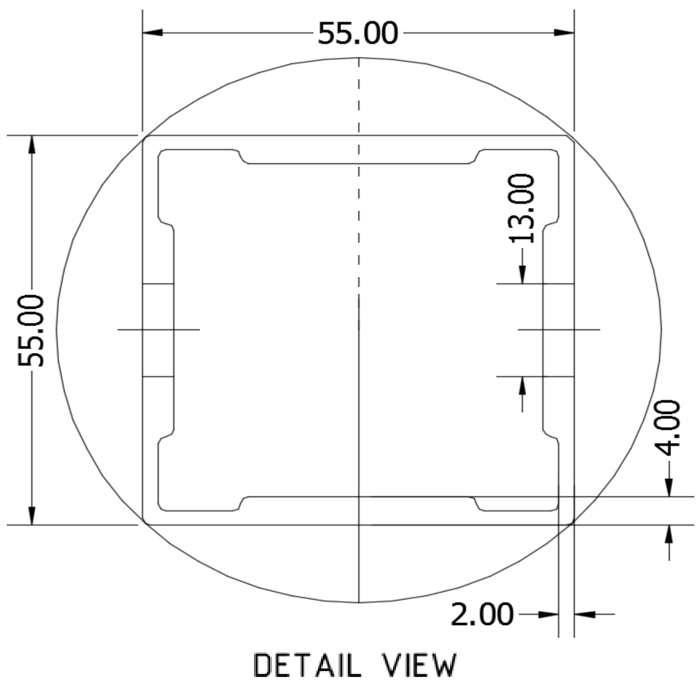
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	24.80	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.549	k-ft
P_n =	0.679	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	41%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

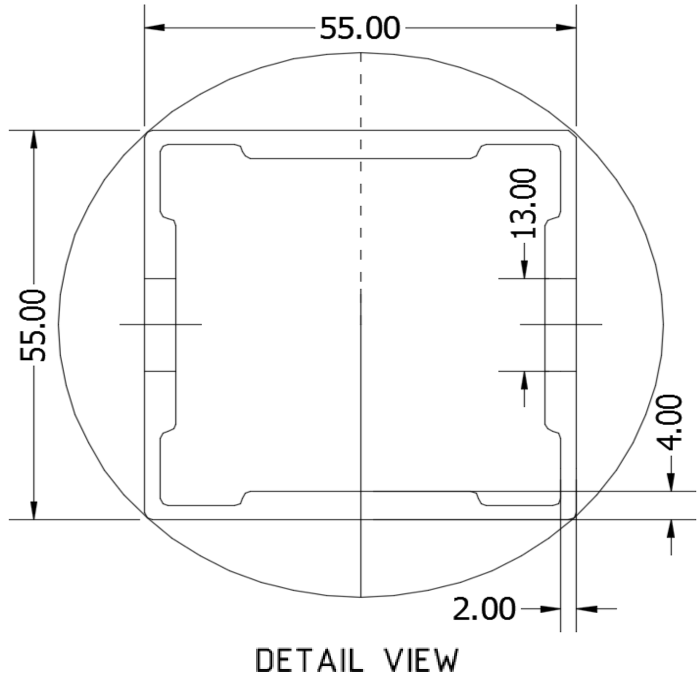
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	98.03	in
$\Phi F_{ty\ AXIAL}$ =	6.11	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.012	k-ft
M_z =	0.000	k-ft
P_n =	1.349	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	6.000	k
Utilization =	23%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.10	in
$\Phi F_{ty\ AXIAL}$ =	13.63	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.011	k-ft
M_z =	-0.328	k-ft
P_n =	0.709	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.386	k
Utilization =	29%	



5. FOUNDATION DESIGN CALCULATIONS

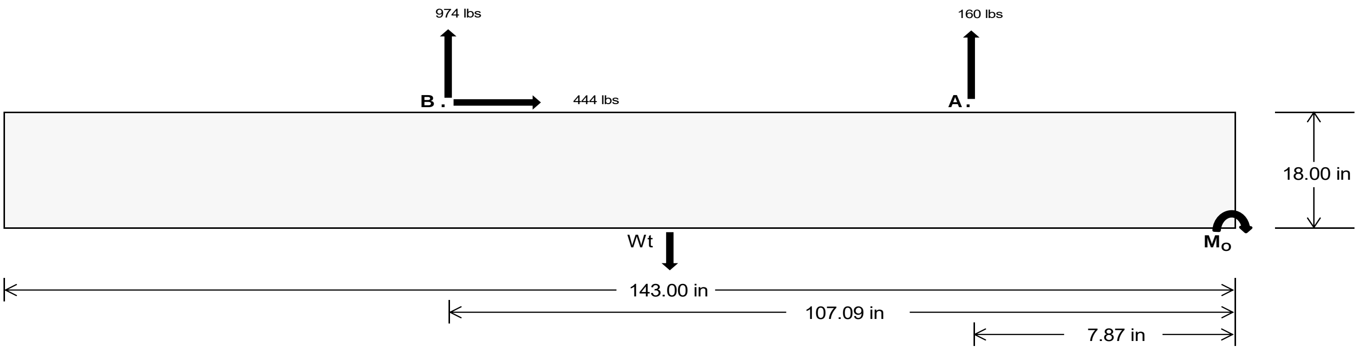
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	680.77	4067.38	k
Compressive Load =	4231.00	4743.69	k
Lateral Load =	361.71	1849.38	k
Moment (Weak Axis) =	0.74	0.42	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC tables 1804.2 (2003, 2006) & 1806.2 (2009).



<u>Concrete Properties</u>

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

<u>Footing Reinforcement</u>

Use fiber reinforcing with (2) #5 rebar.

<u>Overturning Check</u>

M_O =	113613.8 in-lbs
Resisting Force Required =	1589.00 lbs
S.F. =	1.67
Weight Required =	2648.34 lbs
Minimum Width =	35 in in
Weight Provided =	7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.

<u>Sliding</u>

Force =	444.36 lbs
Friction =	0.4
Weight Required =	1110.90 lbs
Resisting Weight =	7559.64 lbs
Additional Weight Required =	0 lbs

Use a 143in long x 35in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

<u>Cohesion</u>

Sliding Force =	444.36 lbs
Cohesion =	130 psf
Area =	34.76 ft^2
Resisting =	3779.82 lbs
Additional Weight Required =	0 lbs

Use a 143in long x 35in wide x 18in tall ballast foundation. Cohesion is OK.

<u>Shear Key</u>

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

<u>Bearing Pressure</u>

	Ballast Width			
	35 in	36 in	37 in	38 in
P_{ftg} = (145 pcf)(11.92 ft)(1.5 ft)(2.92 ft) =	7560 lbs	7776 lbs	7992 lbs	8208 lbs

ASD LC	1.0D + 1.0S				1.0D + 1.0W				1.0D + 0.75L + 0.75W + 0.75S				0.6D + 1.0W			
Width	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in
F_A	1627 lbs	1627 lbs	1627 lbs	1627 lbs	1216 lbs	1216 lbs	1216 lbs	1216 lbs	1999 lbs	1999 lbs	1999 lbs	1999 lbs	-321 lbs	-321 lbs	-321 lbs	-321 lbs
F_B	1753 lbs	1753 lbs	1753 lbs	1753 lbs	1478 lbs	1478 lbs	1478 lbs	1478 lbs	2281 lbs	2281 lbs	2281 lbs	2281 lbs	-1949 lbs	-1949 lbs	-1949 lbs	-1949 lbs
F_V	177 lbs	177 lbs	177 lbs	177 lbs	804 lbs	804 lbs	804 lbs	804 lbs	723 lbs	723 lbs	723 lbs	723 lbs	-889 lbs	-889 lbs	-889 lbs	-889 lbs
P_{total}	10939 lbs	11155 lbs	11371 lbs	11587 lbs	10253 lbs	10469 lbs	10685 lbs	10901 lbs	11840 lbs	12056 lbs	12272 lbs	12488 lbs	2266 lbs	2396 lbs	2525 lbs	2655 lbs
M	3692 lbs-ft	3692 lbs-ft	3692 lbs-ft	3692 lbs-ft	3269 lbs-ft	3269 lbs-ft	3269 lbs-ft	3269 lbs-ft	4919 lbs-ft	4919 lbs-ft	4919 lbs-ft	4919 lbs-ft	2745 lbs-ft	2745 lbs-ft	2745 lbs-ft	2745 lbs-ft
e	0.34 ft	0.33 ft	0.32 ft	0.32 ft	0.32 ft	0.31 ft	0.31 ft	0.30 ft	0.42 ft	0.41 ft	0.40 ft	0.39 ft	1.21 ft	1.15 ft	1.09 ft	1.03 ft
L/6	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft
f_{min}	261.3 psf	260.0 psf	258.9 psf	257.8 psf	247.6 psf	246.8 psf	246.0 psf	245.3 psf	269.4 psf	267.9 psf	266.6 psf	265.3 psf	25.4 psf	28.3 psf	31.1 psf	33.7 psf
f_{max}	368.2 psf	364.0 psf	360.1 psf	356.3 psf	342.4 psf	338.9 psf	335.6 psf	332.5 psf	411.9 psf	406.5 psf	401.4 psf	396.6 psf	105.0 psf	105.7 psf	106.3 psf	107.0 psf

Maximum Bearing Pressure =	412 psf
Allowable Bearing Pressure =	1500 psf

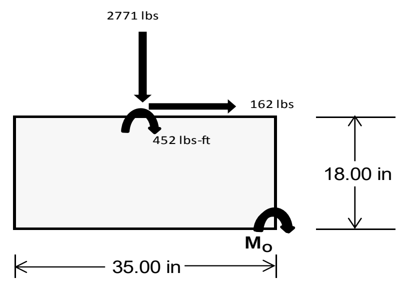
Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 3345.6 ft-lbs
Resisting Force Required = 2294.12 lbs
S.F. = 1.67
Weight Required = 3823.54 lbs
Minimum Width = 35 in in
Weight Provided = 7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	35 in			35 in			35 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	295 lbs	681 lbs	229 lbs	978 lbs	2771 lbs	927 lbs	109 lbs	199 lbs	44 lbs
F_V	228 lbs	223 lbs	231 lbs	168 lbs	162 lbs	181 lbs	228 lbs	224 lbs	229 lbs
P_{total}	9654 lbs	10039 lbs	9588 lbs	9887 lbs	11680 lbs	9836 lbs	2846 lbs	2936 lbs	2781 lbs
M	928 lbs-ft	915 lbs-ft	939 lbs-ft	699 lbs-ft	695 lbs-ft	741 lbs-ft	924 lbs-ft	912 lbs-ft	928 lbs-ft
e	0.10 ft	0.09 ft	0.10 ft	0.07 ft	0.06 ft	0.08 ft	0.32 ft	0.31 ft	0.33 ft
L/6	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft
f_{min}	222.9 psf	234.7 psf	220.3 psf	243.1 psf	294.9 psf	239.1 psf	27.2 psf	30.5 psf	25.1 psf
f_{max}	332.7 psf	343.0 psf	331.4 psf	325.8 psf	377.2 psf	326.8 psf	136.6 psf	138.4 psf	134.9 psf

Maximum Bearing Pressure = 377 psf
Allowable Bearing Pressure = 1500 psf

Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 143in long x 22in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

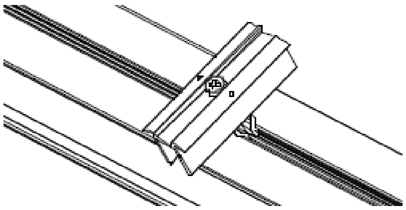
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

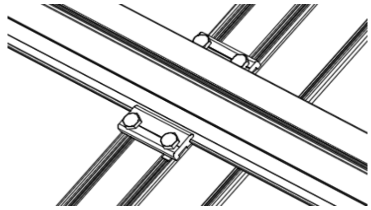
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.475	k
Allowable Uplift =	1.214	k
Utilization =	39%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	1.540	k
Allowable Uplift =	4.357	k
Utilization =	35%	



6.2 Strut Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	3.255	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	44%	

Rear Strut		
Maximum Axial Load =	3.432	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	46%	

Diagonal Strut		
Maximum Axial Load =	1.420	k
M12 Bolt Shear Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	19%	

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

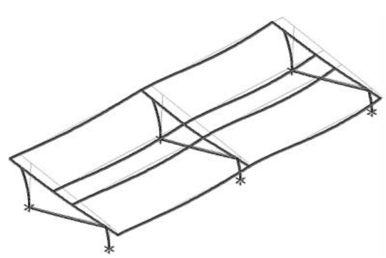
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	51.89	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	1.038	in
Max Drift, Δ_{MAX} =	0.724	in

$0.724 \le 1.038$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 111 in

J = 0.432

307.078

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 27.6 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in³

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 111

J = 0.432

195.283

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.8

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in³

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:

3.4.14

L_b = 104.56 in
J = 1.08
179.85

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.0 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

Weak Axis:

3.4.14

L_b = 104.56
J = 1.08
190.335

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 28.9

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Used

Rb/t = 18.1

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 31.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 35.2

m = 0.68

C_0 = 41.067

Cc = 43.717

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 73.8

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.0 ksi

Ix = 984962 mm^4

2.366 in^4

y = 43.717 mm

Sx = 1.375 in³

M_{max}St = 3.323 k-ft

3.4.18

h/t = 16.2

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40

Cc = 40

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 923544 mm^4

2.219 in^4

x = 40 mm

Sy = 1.409 in³

M_{max}Wk = 3.904 k-ft

Compression

3.4.9

b/t = 16.2

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

b/t = 7.4

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 31.09 ksi

φF_L= 31.09 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.87952

φF_L= φcc(Bc-Dc*λ)

φF_L= 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 98.03 in

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4 ksi

Weak Axis:

3.4.14

L_b = 98.03

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 2.26776

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.89749

φF_L= (φccFcy)/(λ²)

φF_L= 6.10803 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 6.11 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 6.29 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

$L_b =$ 61.10 in

J = 0.942

95.3524

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)/2}))}]$

$\varphi F_L =$ 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

Weak Axis:

3.4.14

$L_b =$ 61.1

J = 0.942

95.3524

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)/2}))}]$

$\varphi F_L =$ 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$S2 = C_t$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

<u>Compression</u>

3.4.7

λ = 1.41345

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.77788

φF_L= (φccFcy)/(λ²)

φF_L= 13.6277 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 13.63 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 14.03 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-9.843	-9.843	0	0
2	M14	Y	-9.843	-9.843	0	0
3	M15	Y	-9.843	-9.843	0	0
4	M16	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-5.454	-5.454	0	0
2	M14	Y	-5.454	-5.454	0	0
3	M15	Y	-5.454	-5.454	0	0
4	M16	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-63.565	-63.565	0	0
2	M14	Y	-63.565	-63.565	0	0
3	M15	Y	-63.565	-63.565	0	0
4	M16	Y	-63.565	-63.565	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-39.079	-39.079	0	0
2	M14	y	-39.079	-39.079	0	0
3	M15	y	-61.409	-61.409	0	0
4	M16	y	-61.409	-61.409	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	89.322	89.322	0	0
2	M14	y	68.481	68.481	0	0
3	M15	y	37.218	37.218	0	0
4	M16	y	37.218	37.218	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	7.874	7.874	0	0
2	M14	Z	7.874	7.874	0	0
3	M15	Z	7.874	7.874	0	0
4	M16	Z	7.874	7.874	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8														
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6														
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65..	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	342.224	2	1115.537	1	.997	1	.005	1	0	1	0	1
2		min	-464.093	3	-969.362	3	-68.963	5	-.323	4	0	1	0	1
3	N7	max	.035	9	1177.332	1	-.603	12	-.001	12	0	1	0	1
4		min	-.101	2	-142.359	3	-278.237	4	-.569	4	0	1	0	1
5	N15	max	0	15	3254.617	1	0	1	0	1	0	1	0	1
6		min	-1.235	2	-523.673	3	-263.893	4	-.549	4	0	1	0	1
7	N16	max	1351.627	2	3648.996	1	0	11	0	1	0	1	0	1
8		min	-1422.603	3	-3128.754	3	-68.716	5	-.326	4	0	1	0	1
9	N23	max	.043	14	1177.332	1	13.031	1	.027	1	0	1	0	1
10		min	-.101	2	-142.359	3	-269.718	4	-.554	4	0	1	0	1
11	N24	max	342.224	2	1115.537	1	-.058	12	0	12	0	1	0	1
12		min	-464.093	3	-969.362	3	-69.65	5	-.325	4	0	1	0	1
13	Totals:	max	2034.64	2	11489.35	1	0	1						
14		min	-2351.14	3	-5875.869	3	-1012.393	4						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	83.575	4	475.837	1	-6.925	12	0	15	.228	1	0	4
2			min	3.938	12	-476.026	3	-173.624	1	-.014	1	.011	12	0	3
3		2	max	81.541	1	332.329	1	-5.458	12	0	15	.109	4	.417	3
4			min	3.938	12	-335.189	3	-133.087	1	-.014	1	.005	12	-.415	1
5		3	max	81.541	1	188.821	1	-3.99	12	0	15	.062	5	.689	3
6			min	3.938	12	-194.352	3	-92.549	1	-.014	1	-.046	1	-.683	1
7		4	max	81.541	1	45.314	1	-2.523	12	0	15	.034	5	.816	3
8			min	3.938	12	-53.515	3	-52.012	1	-.014	1	-.12	1	-.803	1
9		5	max	81.541	1	87.322	3	-.722	10	0	15	.008	5	.799	3
10			min	3.938	12	-98.194	1	-26.809	4	-.014	1	-.153	1	-.776	1
11		6	max	81.541	1	228.159	3	29.063	1	0	15	-.006	12	.637	3
12			min	3.453	15	-241.702	1	-21.518	5	-.014	1	-.143	1	-.602	1
13		7	max	81.541	1	368.996	3	69.601	1	0	15	-.005	12	.33	3
14			min	-6.787	5	-385.209	1	-19.285	5	-.014	1	-.093	1	-.279	1
15		8	max	81.541	1	509.833	3	110.139	1	0	15	.001	2	.19	1
16			min	-18.916	5	-528.717	1	-17.051	5	-.014	1	-.056	4	-.122	3
17		9	max	81.541	1	650.669	3	150.676	1	0	15	.134	1	.807	1
18			min	-31.044	5	-672.225	1	-14.817	5	-.014	1	-.071	5	-.718	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	81.541	1	791.506	3	191.214	1	.014	1	.309	1	1.572	1
20			min	3.938	12	-815.732	1	-113.398	14	-.001	3	.008	12	-1.459	3
21		11	max	81.541	1	672.225	1	-4.815	12	.014	1	.134	1	.807	1
22			min	3.938	12	-650.669	3	-150.676	1	0	15	.002	12	-.718	3
23		12	max	81.541	1	528.717	1	-3.348	12	.014	1	.055	4	.19	1
24			min	3.938	12	-509.833	3	-110.139	1	0	15	-.003	3	-.122	3
25		13	max	81.541	1	385.209	1	-1.88	12	.014	1	.026	5	.33	3
26			min	3.938	12	-368.996	3	-69.601	1	0	15	-.093	1	-.279	1
27		14	max	81.541	1	241.702	1	-.413	12	.014	1	0	15	.637	3
28			min	2.335	15	-228.159	3	-31.224	4	0	15	-.143	1	-.602	1
29		15	max	81.541	1	98.194	1	11.474	1	.014	1	-.005	12	.799	3
30			min	-8.559	5	-87.322	3	-22.448	5	0	15	-.153	1	-.776	1
31		16	max	81.541	1	53.515	3	52.012	1	.014	1	-.004	12	.816	3
32			min	-20.687	5	-45.314	1	-20.214	5	0	15	-.12	1	-.803	1
33		17	max	81.541	1	194.352	3	92.549	1	.014	1	0	3	.689	3
34			min	-32.816	5	-188.821	1	-17.98	5	0	15	-.078	4	-.683	1
35		18	max	81.541	1	335.189	3	133.087	1	.014	1	.07	1	.417	3
36			min	-44.944	5	-332.329	1	-15.747	5	0	15	-.084	5	-.415	1
37		19	max	81.541	1	476.026	3	173.624	1	.014	1	.228	1	0	1
38			min	-57.072	5	-475.837	1	-13.513	5	0	15	-.099	5	0	5
39	M14	1	max	58.834	4	524.648	1	-7.166	12	.008	3	.269	1	0	1
40			min	2.055	12	-378.596	3	-180.223	1	-.014	1	.013	12	0	3
41		2	max	46.705	4	381.14	1	-5.699	12	.008	3	.163	4	.334	3
42			min	2.055	12	-272.031	3	-139.686	1	-.014	1	.006	12	-.465	1
43		3	max	46.49	1	237.633	1	-4.231	12	.008	3	.093	5	.559	3
44			min	2.055	12	-165.466	3	-99.148	1	-.014	1	-.019	1	-.783	1
45		4	max	46.49	1	94.125	1	-2.764	12	.008	3	.052	5	.674	3
46			min	2.055	12	-58.9	3	-58.611	1	-.014	1	-.1	1	-.954	1
47		5	max	46.49	1	47.665	3	-1.296	12	.008	3	.012	5	.68	3
48			min	.432	15	-49.383	1	-42	4	-.014	1	-.139	1	-.977	1
49		6	max	46.49	1	154.23	3	22.464	1	.008	3	-.005	12	.576	3
50			min	-11.475	5	-192.89	1	-34.963	5	-.014	1	-.137	1	-.852	1
51		7	max	46.49	1	260.795	3	63.002	1	.008	3	-.004	12	.363	3
52			min	-23.604	5	-336.398	1	-32.729	5	-.014	1	-.093	1	-.58	1
53		8	max	46.49	1	367.36	3	103.54	1	.008	3	0	10	.04	3
54			min	-35.732	5	-479.906	1	-30.496	5	-.014	1	-.096	4	-.161	1
55		9	max	46.49	1	473.925	3	144.077	1	.008	3	.12	1	.406	1
56			min	-47.86	5	-623.414	1	-28.262	5	-.014	1	-.122	5	-.392	3
57		10	max	74.327	4	580.49	3	184.615	1	.014	1	.289	1	1.121	1
58			min	2.055	12	-766.921	1	-116.941	14	-.008	3	.007	12	-.934	3
59		11	max	62.199	4	623.414	1	-4.574	12	.014	1	.163	4	.406	1
60			min	2.055	12	-473.925	3	-144.077	1	-.008	3	.002	12	-.392	3
61		12	max	50.071	4	479.906	1	-3.106	12	.014	1	.092	4	.04	3
62			min	2.055	12	-367.36	3	-103.54	1	-.008	3	-.007	1	-.161	1
63		13	max	46.49	1	336.398	1	-1.639	12	.014	1	.049	5	.363	3
64			min	2.055	12	-260.795	3	-63.002	1	-.008	3	-.093	1	-.58	1
65		14	max	46.49	1	192.89	1	-.171	12	.014	1	.01	5	.576	3
66			min	2.055	12	-154.23	3	-42.959	4	-.008	3	-.137	1	-.852	1
67		15	max	46.49	1	49.383	1	18.073	1	.014	1	-.005	12	.68	3
68			min	2.055	12	-47.665	3	-35.166	5	-.008	3	-.139	1	-.977	1
69		16	max	46.49	1	58.9	3	58.611	1	.014	1	-.003	12	.674	3
70			min	-8.134	5	-94.125	1	-32.932	5	-.008	3	-.1	1	-.954	1
71		17	max	46.49	1	165.466	3	99.148	1	.014	1	.002	3	.559	3
72			min	-20.262	5	-237.633	1	-30.699	5	-.008	3	-.102	4	-.783	1
73		18	max	46.49	1	272.031	3	139.686	1	.014	1	.104	1	.334	3
74			min	-32.391	5	-381.14	1	-28.465	5	-.008	3	-.126	5	-.465	1
75		19	max	46.49	1	378.596	3	180.223	1	.014	1	.269	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-44.519	5	-524.648	1	-26.231	5	-.008	3	-.154	5	0	3
77	M15	1	max	90.848	5	586.574	1	-7.112	12	.015	1	.311	4	0	1
78			min	-49.589	1	-205.499	3	-180.172	1	-.007	3	.012	12	0	3
79		2	max	78.72	5	424.707	1	-5.644	12	.015	1	.215	4	.183	3
80			min	-49.589	1	-150.344	3	-139.634	1	-.007	3	.006	12	-.52	1
81		3	max	66.591	5	262.839	1	-4.176	12	.015	1	.131	5	.309	3
82			min	-49.589	1	-95.189	3	-99.096	1	-.007	3	-.019	1	-.873	1
83		4	max	54.463	5	100.971	1	-2.709	12	.015	1	.075	5	.379	3
84			min	-49.589	1	-40.034	3	-66.703	4	-.007	3	-.1	1	-1.06	1
85		5	max	42.335	5	15.121	3	-1.241	12	.015	1	.021	5	.391	3
86			min	-49.589	1	-60.897	1	-56.092	4	-.007	3	-.139	1	-1.081	1
87		6	max	30.206	5	70.276	3	22.516	1	.015	1	-.005	12	.347	3
88			min	-49.589	1	-222.765	1	-49.039	5	-.007	3	-.137	1	-.935	1
89		7	max	18.078	5	125.43	3	63.054	1	.015	1	-.004	12	.247	3
90			min	-49.589	1	-384.633	1	-46.805	5	-.007	3	-.101	4	-.623	1
91		8	max	5.95	5	180.585	3	103.591	1	.015	1	0	10	.09	3
92			min	-49.589	1	-546.501	1	-44.571	5	-.007	3	-.131	4	-.144	1
93		9	max	-2.436	12	235.74	3	144.129	1	.015	1	.12	1	.501	1
94			min	-49.589	1	-708.369	1	-42.338	5	-.007	3	-.171	5	-.124	3
95		10	max	-2.436	12	315.916	14	184.667	1	.007	3	.309	4	1.312	1
96			min	-49.589	1	-870.237	1	-124.118	14	-.015	1	.008	12	-.395	3
97		11	max	.322	15	708.369	1	-4.629	12	.007	3	.213	4	.501	1
98			min	-49.589	1	-235.74	3	-144.129	1	-.015	1	.002	12	-.124	3
99		12	max	-2.436	12	546.501	1	-3.161	12	.007	3	.127	4	.09	3
100			min	-49.589	1	-180.585	3	-103.591	1	-.015	1	-.007	1	-.144	1
101		13	max	-2.436	12	384.633	1	-1.694	12	.007	3	.069	5	.247	3
102			min	-49.589	1	-125.43	3	-67.695	4	-.015	1	-.093	1	-.623	1
103		14	max	-2.436	12	222.765	1	-.226	12	.007	3	.015	5	.347	3
104			min	-49.589	1	-70.276	3	-57.083	4	-.015	1	-.137	1	-.935	1
105		15	max	-2.436	12	60.897	1	18.021	1	.007	3	-.005	12	.391	3
106			min	-59.401	4	-15.121	3	-49.243	5	-.015	1	-.139	1	-1.081	1
107		16	max	-2.436	12	40.034	3	58.559	1	.007	3	-.003	12	.379	3
108			min	-71.529	4	-100.971	1	-47.009	5	-.015	1	-.108	4	-1.06	1
109		17	max	-2.436	12	95.189	3	99.096	1	.007	3	.001	3	.309	3
110			min	-83.658	4	-262.839	1	-44.776	5	-.015	1	-.139	4	-.873	1
111		18	max	-2.436	12	150.344	3	139.634	1	.007	3	.104	1	.183	3
112			min	-95.786	4	-424.707	1	-42.542	5	-.015	1	-.178	5	-.52	1
113		19	max	-2.436	12	205.499	3	180.172	1	.007	3	.268	1	0	1
114			min	-107.914	4	-586.574	1	-40.308	5	-.015	1	-.22	5	0	5
115	M16	1	max	86.658	5	538.267	1	-6.76	12	.013	1	.23	1	0	1
116			min	-90.476	1	-181.019	3	-174.062	1	-.009	3	.01	12	0	3
117		2	max	74.529	5	376.399	1	-5.293	12	.013	1	.147	4	.158	3
118			min	-90.476	1	-125.864	3	-133.525	1	-.009	3	.004	12	-.47	1
119		3	max	62.401	5	214.531	1	-3.825	12	.013	1	.089	5	.259	3
120			min	-90.476	1	-70.709	3	-92.987	1	-.009	3	-.044	1	-.774	1
121		4	max	50.273	5	52.663	1	-2.357	12	.013	1	.051	5	.303	3
122			min	-90.476	1	-15.554	3	-52.449	1	-.009	3	-.119	1	-.911	1
123		5	max	38.145	5	39.6	3	-.853	10	.013	1	.015	5	.291	3
124			min	-90.476	1	-109.204	1	-36.915	4	-.009	3	-.152	1	-.882	1
125		6	max	26.016	5	94.755	3	28.626	1	.013	1	-.006	12	.222	3
126			min	-90.476	1	-271.072	1	-31.484	5	-.009	3	-.143	1	-.687	1
127		7	max	13.888	5	149.91	3	69.163	1	.013	1	-.004	12	.096	3
128			min	-90.476	1	-432.94	1	-29.25	5	-.009	3	-.093	1	-.325	1
129		8	max	1.76	5	205.065	3	109.701	1	.013	1	0	2	.203	1
130			min	-90.476	1	-594.808	1	-27.017	5	-.009	3	-.081	4	-.087	3
131		9	max	-4.101	12	260.22	3	150.238	1	.013	1	.132	1	.898	1
132			min	-90.476	1	-756.676	1	-24.783	5	-.009	3	-.105	5	-.326	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-4.101	12	335.082	14	190.776	1	.009	3	.308	1	1.759	1
134			min	-90.476	1	-918.544	1	-118.307	14	-.013	1	.009	12	-.621	3
135		11	max	.536	5	756.676	1	-4.98	12	.009	3	.149	4	.898	1
136			min	-90.476	1	-260.22	3	-150.238	1	-.013	1	.003	12	-.326	3
137		12	max	-4.101	12	594.808	1	-3.513	12	.009	3	.08	4	.203	1
138			min	-90.476	1	-205.065	3	-109.701	1	-.013	1	-.002	3	-.087	3
139		13	max	-4.101	12	432.94	1	-2.045	12	.009	3	.039	5	.096	3
140			min	-90.476	1	-149.91	3	-69.163	1	-.013	1	-.093	1	-.325	1
141		14	max	-4.101	12	271.072	1	-.578	12	.009	3	.003	5	.222	3
142			min	-90.476	1	-94.755	3	-41.158	4	-.013	1	-.143	1	-.687	1
143		15	max	-4.101	12	109.204	1	11.912	1	.009	3	-.005	12	.291	3
144			min	-90.476	1	-39.6	3	-32.39	5	-.013	1	-.152	1	-.882	1
145		16	max	-4.101	12	15.554	3	52.449	1	.009	3	-.004	12	.303	3
146			min	-90.476	1	-52.663	1	-30.157	5	-.013	1	-.119	1	-.911	1
147		17	max	-4.101	12	70.709	3	92.987	1	.009	3	0	12	.259	3
148			min	-92.084	4	-214.531	1	-27.923	5	-.013	1	-.104	4	-.774	1
149		18	max	-4.101	12	125.864	3	133.525	1	.009	3	.072	1	.158	3
150			min	-104.212	4	-376.399	1	-25.689	5	-.013	1	-.121	5	-.47	1
151		19	max	-4.101	12	181.019	3	174.062	1	.009	3	.23	1	0	1
152			min	-116.34	4	-538.267	1	-23.456	5	-.013	1	-.147	5	0	5
153	M2	1	max	1090.371	1	2.21	4	.963	1	0	3	0	5	0	1
154			min	-867.704	3	.543	15	-61.012	4	0	1	0	1	0	1
155		2	max	1090.787	1	2.202	4	.963	1	0	3	0	1	0	15
156			min	-867.392	3	.541	15	-61.372	4	0	1	-.017	4	0	4
157		3	max	1091.203	1	2.193	4	.963	1	0	3	0	1	0	15
158			min	-867.08	3	.539	15	-61.732	4	0	1	-.034	4	-.001	4
159		4	max	1091.619	1	2.184	4	.963	1	0	3	0	1	0	15
160			min	-866.768	3	.537	15	-62.093	4	0	1	-.052	4	-.002	4
161		5	max	1092.035	1	2.176	4	.963	1	0	3	.001	1	0	15
162			min	-866.456	3	.534	15	-62.453	4	0	1	-.069	4	-.002	4
163		6	max	1092.451	1	2.167	4	.963	1	0	3	.001	1	0	15
164			min	-866.145	3	.532	15	-62.814	4	0	1	-.087	4	-.003	4
165		7	max	1092.867	1	2.158	4	.963	1	0	3	.002	1	0	15
166			min	-865.833	3	.53	15	-63.174	4	0	1	-.104	4	-.004	4
167		8	max	1093.283	1	2.149	4	.963	1	0	3	.002	1	-.001	15
168			min	-865.521	3	.528	15	-63.535	4	0	1	-.122	4	-.004	4
169		9	max	1093.698	1	2.141	4	.963	1	0	3	.002	1	-.001	15
170			min	-865.209	3	.526	15	-63.895	4	0	1	-.14	4	-.005	4
171		10	max	1094.114	1	2.132	4	.963	1	0	3	.002	1	-.001	15
172			min	-864.897	3	.524	15	-64.256	4	0	1	-.158	4	-.005	4
173		11	max	1094.53	1	2.123	4	.963	1	0	3	.003	1	-.001	15
174			min	-864.585	3	.522	15	-64.616	4	0	1	-.176	4	-.006	4
175		12	max	1094.946	1	2.115	4	.963	1	0	3	.003	1	-.002	15
176			min	-864.273	3	.52	15	-64.977	4	0	1	-.194	4	-.007	4
177		13	max	1095.362	1	2.106	4	.963	1	0	3	.003	1	-.002	15
178			min	-863.961	3	.518	15	-65.337	4	0	1	-.213	4	-.007	4
179		14	max	1095.778	1	2.097	4	.963	1	0	3	.003	1	-.002	15
180			min	-863.649	3	.516	15	-65.698	4	0	1	-.231	4	-.008	4
181		15	max	1096.194	1	2.088	4	.963	1	0	3	.004	1	-.002	15
182			min	-863.337	3	.514	15	-66.058	4	0	1	-.249	4	-.008	4
183		16	max	1096.61	1	2.08	4	.963	1	0	3	.004	1	-.002	15
184			min	-863.025	3	.512	15	-66.419	4	0	1	-.268	4	-.009	4
185		17	max	1097.026	1	2.071	4	.963	1	0	3	.004	1	-.002	15
186			min	-862.714	3	.51	15	-66.779	4	0	1	-.287	4	-.01	4
187		18	max	1097.441	1	2.062	4	.963	1	0	3	.005	1	-.003	15
188			min	-862.402	3	.508	15	-67.14	4	0	1	-.305	4	-.01	4
189		19	max	1097.857	1	2.054	4	.963	1	0	3	.005	1	-.003	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-862.09	3	.506	15	-67.5	4	0	1	-.324	4	-.011	4
191	M3	1	max	338.468	2	9.133	4	.221	1	0	12	0	1	.011	4
192			min	-463.397	3	2.16	15	-3.5	5	0	4	-.005	4	.003	15
193		2	max	338.297	2	8.258	4	.221	1	0	12	0	1	.007	4
194			min	-463.525	3	1.955	15	-2.892	5	0	4	-.007	4	.002	15
195		3	max	338.127	2	7.384	4	.221	1	0	12	0	1	.003	4
196			min	-463.652	3	1.749	15	-2.283	5	0	4	-.008	4	0	12
197		4	max	337.957	2	6.509	4	.221	1	0	12	0	1	0	2
198			min	-463.78	3	1.544	15	-1.674	5	0	4	-.009	4	-.001	3
199		5	max	337.786	2	5.635	4	.221	1	0	12	0	1	0	15
200			min	-463.908	3	1.338	15	-1.065	5	0	4	-.01	5	-.003	6
201		6	max	337.616	2	4.76	4	.221	1	0	12	0	1	-.001	15
202			min	-464.036	3	1.133	15	-.457	5	0	4	-.01	5	-.006	6
203		7	max	337.446	2	3.886	4	.221	1	0	12	0	1	-.002	15
204			min	-464.163	3	.927	15	.01	12	0	4	-.01	5	-.008	6
205		8	max	337.275	2	3.011	4	.822	4	0	12	0	1	-.002	15
206			min	-464.291	3	.722	15	.01	12	0	4	-.01	5	-.009	6
207		9	max	337.105	2	2.137	4	1.431	4	0	12	0	1	-.002	15
208			min	-464.419	3	.516	15	.01	12	0	4	-.009	5	-.011	6
209		10	max	336.935	2	1.263	4	2.039	4	0	12	.001	1	-.003	15
210			min	-464.547	3	.31	15	.01	12	0	4	-.009	5	-.011	6
211		11	max	336.764	2	.388	4	2.648	4	0	12	.001	1	-.003	15
212			min	-464.674	3	.044	12	.01	12	0	4	-.008	5	-.012	6
213		12	max	336.594	2	-.101	15	3.257	4	0	12	.001	1	-.003	15
214			min	-464.802	3	-.488	6	.01	12	0	4	-.006	5	-.012	6
215		13	max	336.424	2	-.306	15	3.865	4	0	12	.001	1	-.003	15
216			min	-464.93	3	-1.362	6	.01	12	0	4	-.004	5	-.011	6
217		14	max	336.253	2	-.512	15	4.474	4	0	12	.001	1	-.002	15
218			min	-465.058	3	-2.236	6	.01	12	0	4	-.003	5	-.01	6
219		15	max	336.083	2	-.717	15	5.083	4	0	12	.002	1	-.002	15
220			min	-465.185	3	-3.111	6	.01	12	0	4	0	5	-.009	6
221		16	max	335.912	2	-.923	15	5.692	4	0	12	.003	4	-.002	15
222			min	-465.313	3	-3.985	6	.01	12	0	4	0	12	-.008	6
223		17	max	335.742	2	-1.128	15	6.3	4	0	12	.005	4	-.001	15
224			min	-465.441	3	-4.86	6	.01	12	0	4	0	12	-.005	6
225		18	max	335.572	2	-1.334	15	6.909	4	0	12	.009	4	0	15
226			min	-465.569	3	-5.734	6	.01	12	0	4	0	12	-.003	6
227		19	max	335.401	2	-1.54	15	7.518	4	0	12	.012	4	0	1
228			min	-465.696	3	-6.609	6	.01	12	0	4	0	12	0	1
229	M4	1	max	1174.265	1	0	1	-.601	12	0	1	.007	4	0	1
230			min	-144.659	3	0	1	-277.175	4	0	1	0	12	0	1
231		2	max	1174.436	1	0	1	-.601	12	0	1	0	12	0	1
232			min	-144.531	3	0	1	-277.323	4	0	1	-.025	4	0	1
233		3	max	1174.606	1	0	1	-.601	12	0	1	0	12	0	1
234			min	-144.403	3	0	1	-277.471	4	0	1	-.057	4	0	1
235		4	max	1174.776	1	0	1	-.601	12	0	1	0	12	0	1
236			min	-144.276	3	0	1	-277.618	4	0	1	-.088	4	0	1
237		5	max	1174.947	1	0	1	-.601	12	0	1	0	12	0	1
238			min	-144.148	3	0	1	-277.766	4	0	1	-.12	4	0	1
239		6	max	1175.117	1	0	1	-.601	12	0	1	0	12	0	1
240			min	-144.02	3	0	1	-277.914	4	0	1	-.152	4	0	1
241		7	max	1175.287	1	0	1	-.601	12	0	1	0	12	0	1
242			min	-143.892	3	0	1	-278.061	4	0	1	-.184	4	0	1
243		8	max	1175.458	1	0	1	-.601	12	0	1	0	12	0	1
244			min	-143.765	3	0	1	-278.209	4	0	1	-.216	4	0	1
245		9	max	1175.628	1	0	1	-.601	12	0	1	0	12	0	1
246			min	-143.637	3	0	1	-278.357	4	0	1	-.248	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	1175.798	1	0	1	-.601	12	0	1	0	12	0	1
248			min	-143.509	3	0	1	-278.504	4	0	1	-.28	4	0	1
249		11	max	1175.969	1	0	1	-.601	12	0	1	0	12	0	1
250			min	-143.381	3	0	1	-278.652	4	0	1	-.312	4	0	1
251		12	max	1176.139	1	0	1	-.601	12	0	1	0	12	0	1
252			min	-143.254	3	0	1	-278.799	4	0	1	-.344	4	0	1
253		13	max	1176.309	1	0	1	-.601	12	0	1	0	12	0	1
254			min	-143.126	3	0	1	-278.947	4	0	1	-.376	4	0	1
255		14	max	1176.48	1	0	1	-.601	12	0	1	0	12	0	1
256			min	-142.998	3	0	1	-279.095	4	0	1	-.408	4	0	1
257		15	max	1176.65	1	0	1	-.601	12	0	1	0	12	0	1
258			min	-142.87	3	0	1	-279.242	4	0	1	-.44	4	0	1
259		16	max	1176.82	1	0	1	-.601	12	0	1	0	12	0	1
260			min	-142.743	3	0	1	-279.39	4	0	1	-.472	4	0	1
261		17	max	1176.991	1	0	1	-.601	12	0	1	-.001	12	0	1
262			min	-142.615	3	0	1	-279.538	4	0	1	-.504	4	0	1
263		18	max	1177.161	1	0	1	-.601	12	0	1	-.001	12	0	1
264			min	-142.487	3	0	1	-279.685	4	0	1	-.536	4	0	1
265		19	max	1177.332	1	0	1	-.601	12	0	1	-.001	12	0	1
266			min	-142.359	3	0	1	-279.833	4	0	1	-.569	4	0	1
267	M6	1	max	3424.958	1	2.367	2	0	1	0	1	0	4	0	1
268			min	-2795.711	3	.344	12	-61.676	4	0	4	0	1	0	1
269		2	max	3425.374	1	2.36	2	0	1	0	1	0	1	0	12
270			min	-2795.399	3	.341	12	-62.036	4	0	4	-.017	4	0	2
271		3	max	3425.79	1	2.354	2	0	1	0	1	0	1	0	12
272			min	-2795.087	3	.337	12	-62.397	4	0	4	-.035	4	-.001	2
273		4	max	3426.206	1	2.347	2	0	1	0	1	0	1	0	12
274			min	-2794.775	3	.334	12	-62.757	4	0	4	-.052	4	-.002	2
275		5	max	3426.622	1	2.34	2	0	1	0	1	0	1	0	12
276			min	-2794.463	3	.33	12	-63.117	4	0	4	-.07	4	-.003	2
277		6	max	3427.038	1	2.333	2	0	1	0	1	0	1	0	12
278			min	-2794.151	3	.327	12	-63.478	4	0	4	-.088	4	-.003	2
279		7	max	3427.454	1	2.326	2	0	1	0	1	0	1	0	12
280			min	-2793.839	3	.324	12	-63.838	4	0	4	-.106	4	-.004	2
281		8	max	3427.87	1	2.32	2	0	1	0	1	0	1	0	12
282			min	-2793.527	3	.32	12	-64.199	4	0	4	-.124	4	-.005	2
283		9	max	3428.285	1	2.313	2	0	1	0	1	0	1	0	12
284			min	-2793.215	3	.317	12	-64.559	4	0	4	-.142	4	-.005	2
285		10	max	3428.701	1	2.306	2	0	1	0	1	0	1	0	12
286			min	-2792.903	3	.313	12	-64.92	4	0	4	-.16	4	-.006	2
287		11	max	3429.117	1	2.299	2	0	1	0	1	0	1	0	12
288			min	-2792.591	3	.31	12	-65.28	4	0	4	-.178	4	-.007	2
289		12	max	3429.533	1	2.292	2	0	1	0	1	0	1	-.001	12
290			min	-2792.28	3	.307	12	-65.641	4	0	4	-.196	4	-.007	2
291		13	max	3429.949	1	2.286	2	0	1	0	1	0	1	-.001	12
292			min	-2791.968	3	.303	12	-66.001	4	0	4	-.215	4	-.008	2
293		14	max	3430.365	1	2.279	2	0	1	0	1	0	1	-.001	12
294			min	-2791.656	3	.3	12	-66.362	4	0	4	-.233	4	-.008	2
295		15	max	3430.781	1	2.272	2	0	1	0	1	0	1	-.001	12
296			min	-2791.344	3	.296	12	-66.722	4	0	4	-.252	4	-.009	2
297		16	max	3431.197	1	2.265	2	0	1	0	1	0	1	-.001	12
298			min	-2791.032	3	.293	12	-67.083	4	0	4	-.271	4	-.01	2
299		17	max	3431.613	1	2.259	2	0	1	0	1	0	1	-.001	12
300			min	-2790.72	3	.29	12	-67.443	4	0	4	-.29	4	-.01	2
301		18	max	3432.028	1	2.252	2	0	1	0	1	0	1	-.002	12
302			min	-2790.408	3	.286	12	-67.804	4	0	4	-.309	4	-.011	2
303		19	max	3432.444	1	2.245	2	0	1	0	1	0	1	-.002	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-2790.096	3	.283	12	-68.164	4	0	4	-.328	4	-.012	2
305	M7	1	max	1348.98	2	9.143	6	0	1	0	1	0	1	.012	2
306			min	-1417.42	3	2.145	15	-3.72	5	0	4	-.006	4	.002	12
307		2	max	1348.81	2	8.268	6	0	1	0	1	0	1	.008	2
308			min	-1417.548	3	1.939	15	-3.112	5	0	4	-.007	4	0	3
309		3	max	1348.64	2	7.394	6	0	1	0	1	0	1	.005	2
310			min	-1417.676	3	1.734	15	-2.503	5	0	4	-.008	4	-.002	3
311		4	max	1348.469	2	6.519	6	0	1	0	1	0	1	.002	2
312			min	-1417.803	3	1.528	15	-1.894	5	0	4	-.009	4	-.004	3
313		5	max	1348.299	2	5.645	6	0	1	0	1	0	1	0	2
314			min	-1417.931	3	1.323	15	-1.286	5	0	4	-.01	4	-.005	3
315		6	max	1348.129	2	4.77	6	0	1	0	1	0	1	-.001	15
316			min	-1418.059	3	1.117	15	-.677	5	0	4	-.011	4	-.006	3
317		7	max	1347.958	2	3.896	6	0	1	0	1	0	1	-.002	15
318			min	-1418.187	3	.912	15	-.068	5	0	4	-.011	4	-.008	4
319		8	max	1347.788	2	3.022	6	.548	4	0	1	0	1	-.002	15
320			min	-1418.314	3	.706	15	0	1	0	4	-.011	4	-.009	4
321		9	max	1347.617	2	2.147	6	1.157	4	0	1	0	1	-.002	15
322			min	-1418.442	3	.501	15	0	1	0	4	-.01	4	-.011	4
323		10	max	1347.447	2	1.366	2	1.765	4	0	1	0	1	-.003	15
324			min	-1418.57	3	.186	12	0	1	0	4	-.01	4	-.011	4
325		11	max	1347.277	2	.684	2	2.374	4	0	1	0	1	-.003	15
326			min	-1418.698	3	-.262	3	0	1	0	4	-.009	4	-.012	4
327		12	max	1347.106	2	.003	2	2.983	4	0	1	0	1	-.003	15
328			min	-1418.826	3	-.773	3	0	1	0	4	-.007	4	-.012	4
329		13	max	1346.936	2	-.322	15	3.591	4	0	1	0	1	-.003	15
330			min	-1418.953	3	-1.351	4	0	1	0	4	-.006	4	-.011	4
331		14	max	1346.766	2	-.527	15	4.2	4	0	1	0	1	-.002	15
332			min	-1419.081	3	-2.225	4	0	1	0	4	-.004	4	-.01	4
333		15	max	1346.595	2	-.733	15	4.809	4	0	1	0	1	-.002	15
334			min	-1419.209	3	-3.1	4	0	1	0	4	-.002	4	-.009	4
335		16	max	1346.425	2	-.938	15	5.418	4	0	1	0	5	-.002	15
336			min	-1419.337	3	-3.974	4	0	1	0	4	0	1	-.008	4
337		17	max	1346.255	2	-1.144	15	6.026	4	0	1	.003	5	-.001	15
338			min	-1419.464	3	-4.848	4	0	1	0	4	0	1	-.005	4
339		18	max	1346.084	2	-1.349	15	6.635	4	0	1	.006	5	0	15
340			min	-1419.592	3	-5.723	4	0	1	0	4	0	1	-.003	4
341		19	max	1345.914	2	-1.555	15	7.244	4	0	1	.01	5	0	1
342			min	-1419.72	3	-6.597	4	0	1	0	4	0	1	0	1
343	M8	1	max	3251.551	1	0	1	0	1	0	1	.006	5	0	1
344			min	-525.973	3	0	1	-266.86	4	0	1	0	1	0	1
345		2	max	3251.722	1	0	1	0	1	0	1	0	1	0	1
346			min	-525.845	3	0	1	-267.008	4	0	1	-.025	4	0	1
347		3	max	3251.892	1	0	1	0	1	0	1	0	1	0	1
348			min	-525.717	3	0	1	-267.155	4	0	1	-.056	4	0	1
349		4	max	3252.062	1	0	1	0	1	0	1	0	1	0	1
350			min	-525.589	3	0	1	-267.303	4	0	1	-.086	4	0	1
351		5	max	3252.233	1	0	1	0	1	0	1	0	1	0	1
352			min	-525.462	3	0	1	-267.451	4	0	1	-.117	4	0	1
353		6	max	3252.403	1	0	1	0	1	0	1	0	1	0	1
354			min	-525.334	3	0	1	-267.598	4	0	1	-.148	4	0	1
355		7	max	3252.573	1	0	1	0	1	0	1	0	1	0	1
356			min	-525.206	3	0	1	-267.746	4	0	1	-.178	4	0	1
357		8	max	3252.744	1	0	1	0	1	0	1	0	1	0	1
358			min	-525.078	3	0	1	-267.894	4	0	1	-.209	4	0	1
359		9	max	3252.914	1	0	1	0	1	0	1	0	1	0	1
360			min	-524.951	3	0	1	-268.041	4	0	1	-.24	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	3253.084	1	0	1	0	1	0	1	0	1	0	1
362			min	-524.823	3	0	1	-268.189	4	0	1	-.271	4	0	1
363		11	max	3253.255	1	0	1	0	1	0	1	0	1	0	1
364			min	-524.695	3	0	1	-268.337	4	0	1	-.302	4	0	1
365		12	max	3253.425	1	0	1	0	1	0	1	0	1	0	1
366			min	-524.567	3	0	1	-268.484	4	0	1	-.332	4	0	1
367		13	max	3253.595	1	0	1	0	1	0	1	0	1	0	1
368			min	-524.44	3	0	1	-268.632	4	0	1	-.363	4	0	1
369		14	max	3253.766	1	0	1	0	1	0	1	0	1	0	1
370			min	-524.312	3	0	1	-268.779	4	0	1	-.394	4	0	1
371		15	max	3253.936	1	0	1	0	1	0	1	0	1	0	1
372			min	-524.184	3	0	1	-268.927	4	0	1	-.425	4	0	1
373		16	max	3254.106	1	0	1	0	1	0	1	0	1	0	1
374			min	-524.056	3	0	1	-269.075	4	0	1	-.456	4	0	1
375		17	max	3254.277	1	0	1	0	1	0	1	0	1	0	1
376			min	-523.929	3	0	1	-269.222	4	0	1	-.487	4	0	1
377		18	max	3254.447	1	0	1	0	1	0	1	0	1	0	1
378			min	-523.801	3	0	1	-269.37	4	0	1	-.518	4	0	1
379		19	max	3254.617	1	0	1	0	1	0	1	0	1	0	1
380			min	-523.673	3	0	1	-269.518	4	0	1	-.549	4	0	1
381	M10	1	max	1090.371	1	2.104	6	-.045	12	0	1	0	4	0	1
382			min	-867.704	3	.471	15	-61.519	4	0	5	0	3	0	1
383		2	max	1090.787	1	2.095	6	-.045	12	0	1	0	12	0	15
384			min	-867.392	3	.469	15	-61.879	4	0	5	-.017	4	0	6
385		3	max	1091.203	1	2.086	6	-.045	12	0	1	0	12	0	15
386			min	-867.08	3	.467	15	-62.24	4	0	5	-.035	4	-.001	6
387		4	max	1091.619	1	2.077	6	-.045	12	0	1	0	12	0	15
388			min	-866.768	3	.465	15	-62.6	4	0	5	-.052	4	-.002	6
389		5	max	1092.035	1	2.069	6	-.045	12	0	1	0	12	0	15
390			min	-866.456	3	.463	15	-62.96	4	0	5	-.07	4	-.002	6
391		6	max	1092.451	1	2.06	6	-.045	12	0	1	0	12	0	15
392			min	-866.145	3	.461	15	-63.321	4	0	5	-.087	4	-.003	6
393		7	max	1092.867	1	2.051	6	-.045	12	0	1	0	12	0	15
394			min	-865.833	3	.459	15	-63.681	4	0	5	-.105	4	-.003	6
395		8	max	1093.283	1	2.043	6	-.045	12	0	1	0	12	0	15
396			min	-865.521	3	.457	15	-64.042	4	0	5	-.123	4	-.004	6
397		9	max	1093.698	1	2.034	6	-.045	12	0	1	0	12	-.001	15
398			min	-865.209	3	.455	15	-64.402	4	0	5	-.141	4	-.005	6
399		10	max	1094.114	1	2.025	6	-.045	12	0	1	0	12	-.001	15
400			min	-864.897	3	.453	15	-64.763	4	0	5	-.159	4	-.005	6
401		11	max	1094.53	1	2.016	6	-.045	12	0	1	0	12	-.001	15
402			min	-864.585	3	.451	15	-65.123	4	0	5	-.178	4	-.006	6
403		12	max	1094.946	1	2.008	6	-.045	12	0	1	0	12	-.001	15
404			min	-864.273	3	.449	15	-65.484	4	0	5	-.196	4	-.006	6
405		13	max	1095.362	1	1.999	6	-.045	12	0	1	0	12	-.002	15
406			min	-863.961	3	.447	15	-65.844	4	0	5	-.214	4	-.007	6
407		14	max	1095.778	1	1.99	6	-.045	12	0	1	0	12	-.002	15
408			min	-863.649	3	.445	15	-66.205	4	0	5	-.233	4	-.007	6
409		15	max	1096.194	1	1.982	6	-.045	12	0	1	0	12	-.002	15
410			min	-863.337	3	.443	15	-66.565	4	0	5	-.251	4	-.008	6
411		16	max	1096.61	1	1.973	6	-.045	12	0	1	0	12	-.002	15
412			min	-863.025	3	.44	15	-66.926	4	0	5	-.27	4	-.009	6
413		17	max	1097.026	1	1.964	6	-.045	12	0	1	0	12	-.002	15
414			min	-862.714	3	.438	15	-67.286	4	0	5	-.289	4	-.009	6
415		18	max	1097.441	1	1.955	6	-.045	12	0	1	0	12	-.002	15
416			min	-862.402	3	.436	15	-67.647	4	0	5	-.308	4	-.01	6
417		19	max	1097.857	1	1.947	6	-.045	12	0	1	0	12	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-862.09	3	.434	15	-68.007	4	0	5	-.327	4	-.01	6
419	M11	1	max	338.468	2	9.069	6	-.01	12	0	1	0	12	.01	6
420			min	-463.397	3	2.118	15	-3.555	4	0	4	-.006	4	.002	15
421		2	max	338.297	2	8.195	6	-.01	12	0	1	0	12	.006	6
422			min	-463.525	3	1.913	15	-2.946	4	0	4	-.007	4	.001	15
423		3	max	338.127	2	7.32	6	-.01	12	0	1	0	12	.003	2
424			min	-463.652	3	1.707	15	-2.337	4	0	4	-.008	4	0	12
425		4	max	337.957	2	6.446	6	-.01	12	0	1	0	12	0	2
426			min	-463.78	3	1.501	15	-1.729	4	0	4	-.009	4	-.001	3
427		5	max	337.786	2	5.571	6	-.01	12	0	1	0	12	0	15
428			min	-463.908	3	1.296	15	-1.12	4	0	4	-.01	4	-.004	4
429		6	max	337.616	2	4.697	6	-.01	12	0	1	0	12	-.002	15
430			min	-464.036	3	1.09	15	-.511	4	0	4	-.01	4	-.006	4
431		7	max	337.446	2	3.823	6	.128	5	0	1	0	12	-.002	15
432			min	-464.163	3	.885	15	-.221	1	0	4	-.01	4	-.008	4
433		8	max	337.275	2	2.948	6	.737	5	0	1	0	12	-.002	15
434			min	-464.291	3	.679	15	-.221	1	0	4	-.01	4	-.01	4
435		9	max	337.105	2	2.074	6	1.346	5	0	1	0	12	-.003	15
436			min	-464.419	3	.474	15	-.221	1	0	4	-.01	4	-.011	4
437		10	max	336.935	2	1.199	6	1.954	5	0	1	0	12	-.003	15
438			min	-464.547	3	.268	15	-.221	1	0	4	-.009	4	-.012	4
439		11	max	336.764	2	.386	2	2.563	5	0	1	0	12	-.003	15
440			min	-464.674	3	.044	12	-.221	1	0	4	-.008	4	-.012	4
441		12	max	336.594	2	-.143	15	3.172	5	0	1	0	12	-.003	15
442			min	-464.802	3	-.551	4	-.221	1	0	4	-.007	4	-.012	4
443		13	max	336.424	2	-.349	15	3.781	5	0	1	0	12	-.003	15
444			min	-464.93	3	-1.425	4	-.221	1	0	4	-.005	4	-.012	4
445		14	max	336.253	2	-.554	15	4.389	5	0	1	0	12	-.003	15
446			min	-465.058	3	-2.3	4	-.221	1	0	4	-.003	4	-.011	4
447		15	max	336.083	2	-.76	15	4.998	5	0	1	0	12	-.002	15
448			min	-465.185	3	-3.174	4	-.221	1	0	4	-.002	1	-.009	4
449		16	max	335.912	2	-.965	15	5.607	5	0	1	.002	5	-.002	15
450			min	-465.313	3	-4.049	4	-.221	1	0	4	-.002	1	-.008	4
451		17	max	335.742	2	-1.171	15	6.215	5	0	1	.005	5	-.001	15
452			min	-465.441	3	-4.923	4	-.221	1	0	4	-.002	1	-.005	4
453		18	max	335.572	2	-1.376	15	6.824	5	0	1	.008	5	0	15
454			min	-465.569	3	-5.798	4	-.221	1	0	4	-.002	1	-.003	4
455		19	max	335.401	2	-1.582	15	7.433	5	0	1	.011	5	0	1
456			min	-465.696	3	-6.672	4	-.221	1	0	4	-.002	1	0	1
457	M12	1	max	1174.265	1	0	1	13.5	1	0	1	.007	5	0	1
458			min	-144.659	3	0	1	-270.025	4	0	1	-.001	1	0	1
459		2	max	1174.436	1	0	1	13.5	1	0	1	0	1	0	1
460			min	-144.531	3	0	1	-270.173	4	0	1	-.025	4	0	1
461		3	max	1174.606	1	0	1	13.5	1	0	1	.002	1	0	1
462			min	-144.403	3	0	1	-270.321	4	0	1	-.056	4	0	1
463		4	max	1174.776	1	0	1	13.5	1	0	1	.003	1	0	1
464			min	-144.276	3	0	1	-270.468	4	0	1	-.087	4	0	1
465		5	max	1174.947	1	0	1	13.5	1	0	1	.005	1	0	1
466			min	-144.148	3	0	1	-270.616	4	0	1	-.118	4	0	1
467		6	max	1175.117	1	0	1	13.5	1	0	1	.007	1	0	1
468			min	-144.02	3	0	1	-270.763	4	0	1	-.149	4	0	1
469		7	max	1175.287	1	0	1	13.5	1	0	1	.008	1	0	1
470			min	-143.892	3	0	1	-270.911	4	0	1	-.18	4	0	1
471		8	max	1175.458	1	0	1	13.5	1	0	1	.01	1	0	1
472			min	-143.765	3	0	1	-271.059	4	0	1	-.211	4	0	1
473		9	max	1175.628	1	0	1	13.5	1	0	1	.011	1	0	1
474			min	-143.637	3	0	1	-271.206	4	0	1	-.242	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	1175.798	1	0	1	13.5	1	0	1	.013	1	0	1
476			min	-143.509	3	0	1	-271.354	4	0	1	-.273	4	0	1
477		11	max	1175.969	1	0	1	13.5	1	0	1	.014	1	0	1
478			min	-143.381	3	0	1	-271.502	4	0	1	-.304	4	0	1
479		12	max	1176.139	1	0	1	13.5	1	0	1	.016	1	0	1
480			min	-143.254	3	0	1	-271.649	4	0	1	-.336	4	0	1
481		13	max	1176.309	1	0	1	13.5	1	0	1	.017	1	0	1
482			min	-143.126	3	0	1	-271.797	4	0	1	-.367	4	0	1
483		14	max	1176.48	1	0	1	13.5	1	0	1	.019	1	0	1
484			min	-142.998	3	0	1	-271.945	4	0	1	-.398	4	0	1
485		15	max	1176.65	1	0	1	13.5	1	0	1	.021	1	0	1
486			min	-142.87	3	0	1	-272.092	4	0	1	-.429	4	0	1
487		16	max	1176.82	1	0	1	13.5	1	0	1	.022	1	0	1
488			min	-142.743	3	0	1	-272.24	4	0	1	-.461	4	0	1
489		17	max	1176.991	1	0	1	13.5	1	0	1	.024	1	0	1
490			min	-142.615	3	0	1	-272.387	4	0	1	-.492	4	0	1
491		18	max	1177.161	1	0	1	13.5	1	0	1	.025	1	0	1
492			min	-142.487	3	0	1	-272.535	4	0	1	-.523	4	0	1
493		19	max	1177.332	1	0	1	13.5	1	0	1	.027	1	0	1
494			min	-142.359	3	0	1	-272.683	4	0	1	-.554	4	0	1
495	M1	1	max	173.629	1	476	3	57.034	5	0	1	.228	1	0	15
496			min	-13.513	5	-473.674	1	-81.407	1	0	5	-.099	5	-.014	1
497		2	max	174.206	1	474.813	3	58.494	5	0	1	.177	1	.28	1
498			min	-13.244	5	-475.257	1	-81.407	1	0	5	-.063	5	-.296	3
499		3	max	295.574	3	549.459	1	.661	5	0	3	.127	1	.564	1
500			min	-205.614	2	-347.893	3	-80.721	1	0	1	-.027	5	-.582	3
501		4	max	296.006	3	547.876	1	2.122	5	0	3	.077	1	.224	1
502			min	-205.038	2	-349.08	3	-80.721	1	0	1	-.026	5	-.366	3
503		5	max	296.438	3	546.293	1	3.582	5	0	3	.027	1	-.005	15
504			min	-204.462	2	-350.268	3	-80.721	1	0	1	-.024	5	-.148	3
505		6	max	296.871	3	544.71	1	5.042	5	0	3	-.001	12	.069	3
506			min	-203.886	2	-351.455	3	-80.721	1	0	1	-.026	4	-.454	1
507		7	max	297.303	3	543.126	1	6.502	5	0	3	-.003	12	.288	3
508			min	-203.309	2	-352.642	3	-80.721	1	0	1	-.073	1	-.792	1
509		8	max	297.735	3	541.543	1	7.962	5	0	3	-.006	12	.507	3
510			min	-202.733	2	-353.83	3	-80.721	1	0	1	-.124	1	-1.128	1
511		9	max	308.978	3	31.928	2	53.802	5	0	9	.078	1	.594	3
512			min	-131.793	2	.476	15	-127.259	1	0	3	-.146	5	-1.284	1
513		10	max	309.411	3	30.345	2	55.262	5	0	9	0	12	.578	3
514			min	-131.217	2	-.005	5	-127.259	1	0	3	-.113	4	-1.295	1
515		11	max	309.843	3	28.762	2	56.722	5	0	9	-.004	12	.564	3
516			min	-130.641	2	-1.973	4	-127.259	1	0	3	-.094	4	-1.305	1
517		12	max	320.999	3	229.202	3	154.653	5	0	1	.121	1	.492	3
518			min	-93.274	5	-576.178	1	-77.718	1	0	3	-.238	5	-1.153	1
519		13	max	321.431	3	228.015	3	156.113	5	0	1	.073	1	.35	3
520			min	-93.006	5	-577.761	1	-77.718	1	0	3	-.142	5	-.794	1
521		14	max	321.864	3	226.828	3	157.573	5	0	1	.025	1	.209	3
522			min	-92.737	5	-579.344	1	-77.718	1	0	3	-.044	5	-.435	1
523		15	max	322.296	3	225.64	3	159.034	5	0	1	.054	5	.068	3
524			min	-92.468	5	-580.927	1	-77.718	1	0	3	-.024	1	-.075	1
525		16	max	322.728	3	224.453	3	160.494	5	0	1	.153	5	.286	1
526			min	-92.199	5	-582.51	1	-77.718	1	0	3	-.072	1	-.071	3
527		17	max	323.16	3	223.265	3	161.954	5	0	1	.253	5	.648	1
528			min	-91.93	5	-584.094	1	-77.718	1	0	3	-.12	1	-.21	3
529		18	max	23.186	5	541.907	1	-4.102	12	0	5	.207	5	.323	1
530			min	-174.634	1	-179.888	3	-117.858	4	0	1	-.174	1	-.103	3
531		19	max	23.455	5	540.324	1	-4.102	12	0	5	.147	5	.009	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-174.058	1	-181.075	3	-116.398	4	0	1	-.23	1	-.013	1
533	M5	1	max	382.417	1	1582.963	3	95.31	5	0	1	0	1	.029	1
534			min	12.566	12	-1620.992	1	0	1	0	4	-.209	4	0	15
535		2	max	382.994	1	1581.776	3	96.77	5	0	1	0	1	1.035	1
536			min	12.854	12	-1622.575	1	0	1	0	4	-.15	4	-.979	3
537		3	max	932.121	3	1577.832	1	43.113	4	0	4	0	1	2.008	1
538			min	-733.707	1	-1076.111	3	0	1	0	1	-.091	4	-1.931	3
539		4	max	932.553	3	1576.248	1	44.573	4	0	4	0	1	1.029	1
540			min	-733.131	1	-1077.298	3	0	1	0	1	-.064	4	-1.263	3
541		5	max	932.986	3	1574.665	1	46.033	4	0	4	0	1	.051	1
542			min	-732.555	1	-1078.485	3	0	1	0	1	-.036	4	-.594	3
543		6	max	933.418	3	1573.082	1	47.493	4	0	4	0	1	.075	3
544			min	-731.979	1	-1079.673	3	0	1	0	1	-.007	5	-.925	1
545		7	max	933.85	3	1571.499	1	48.953	4	0	4	.023	4	.746	3
546			min	-731.403	1	-1080.86	3	0	1	0	1	0	1	-1.901	1
547		8	max	934.282	3	1569.916	1	50.413	4	0	4	.054	4	1.417	3
548			min	-730.826	1	-1082.047	3	0	1	0	1	0	1	-2.876	1
549		9	max	952.716	3	105.988	2	176.858	4	0	1	0	1	1.636	3
550			min	-559.434	2	.48	15	0	1	0	1	-.208	4	-3.26	1
551		10	max	953.148	3	104.405	2	178.318	4	0	1	0	1	1.58	3
552			min	-558.858	2	.002	15	0	1	0	1	-.098	5	-3.296	1
553		11	max	953.58	3	102.822	2	179.779	4	0	1	.013	4	1.524	3
554			min	-558.282	2	-1.707	6	0	1	0	1	0	1	-3.332	1
555		12	max	972.187	3	685.706	3	210.974	4	0	1	0	1	1.334	3
556			min	-411.203	2	-1685.682	1	0	1	0	4	-.336	4	-2.962	1
557		13	max	972.62	3	684.518	3	212.434	4	0	1	0	1	.909	3
558			min	-410.627	2	-1687.265	1	0	1	0	4	-.205	4	-1.916	1
559		14	max	973.052	3	683.331	3	213.894	4	0	1	0	1	.484	3
560			min	-410.05	2	-1688.848	1	0	1	0	4	-.072	4	-.868	1
561		15	max	973.484	3	682.143	3	215.354	4	0	1	.061	4	.22	2
562			min	-409.474	2	-1690.432	1	0	1	0	4	0	1	0	7
563		16	max	973.916	3	680.956	3	216.814	4	0	1	.195	4	1.23	1
564			min	-408.898	2	-1692.015	1	0	1	0	4	0	1	-.362	3
565		17	max	974.348	3	679.769	3	218.275	4	0	1	.33	4	2.281	1
566			min	-408.322	2	-1693.598	1	0	1	0	4	0	1	-.785	3
567		18	max	-13.184	12	1848.414	1	0	1	0	4	.32	4	1.172	1
568			min	-382.136	1	-629.841	3	-36.706	5	0	1	0	1	-.408	3
569		19	max	-12.896	12	1846.83	1	0	1	0	4	.299	4	.025	1
570			min	-381.56	1	-631.029	3	-35.245	5	0	1	0	1	-.017	3
571	M9	1	max	173.629	1	476	3	83.767	4	0	3	-.011	12	0	15
572			min	6.925	12	-473.674	1	3.938	12	0	4	-.228	1	-.014	1
573		2	max	174.206	1	474.813	3	85.227	4	0	3	-.009	12	.28	1
574			min	7.213	12	-475.257	1	3.938	12	0	4	-.177	1	-.296	3
575		3	max	295.574	3	549.459	1	80.721	1	0	1	-.006	12	.564	1
576			min	-205.614	2	-347.893	3	3.891	12	0	3	-.127	1	-.582	3
577		4	max	296.006	3	547.876	1	80.721	1	0	1	-.004	12	.224	1
578			min	-205.038	2	-349.08	3	3.891	12	0	3	-.077	1	-.366	3
579		5	max	296.438	3	546.293	1	80.721	1	0	1	-.001	12	-.005	15
580			min	-204.462	2	-350.268	3	3.891	12	0	3	-.033	4	-.148	3
581		6	max	296.871	3	544.71	1	80.721	1	0	1	.023	1	.069	3
582			min	-203.886	2	-351.455	3	3.891	12	0	3	-.019	5	-.454	1
583		7	max	297.303	3	543.126	1	80.721	1	0	1	.073	1	.288	3
584			min	-203.309	2	-352.642	3	3.891	12	0	3	-.01	5	-.792	1
585		8	max	297.735	3	541.543	1	80.721	1	0	1	.124	1	.507	3
586			min	-202.733	2	-353.83	3	3.891	12	0	3	0	15	-1.128	1
587		9	max	308.978	3	31.928	2	127.259	1	0	3	-.004	12	.594	3
588			min	-131.793	2	.488	15	5.944	12	0	9	-.172	4	-1.284	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	309.411	3	30.345	2	127.259	1	0	3	.001	1	.578	3
590			min	-131.217	2	.011	15	5.944	12	0	9	-.112	4	-1.295	1
591		11	max	309.843	3	28.762	2	127.259	1	0	3	.08	1	.564	3
592			min	-130.641	2	-1.865	6	5.944	12	0	9	-.068	5	-1.305	1
593		12	max	320.999	3	229.202	3	182.185	4	0	3	-.006	12	.492	3
594			min	-76.017	10	-576.178	1	3.51	12	0	1	-.28	4	-1.153	1
595		13	max	321.431	3	228.015	3	183.645	4	0	3	-.003	12	.35	3
596			min	-75.537	10	-577.761	1	3.51	12	0	1	-.167	4	-.794	1
597		14	max	321.864	3	226.828	3	185.105	4	0	3	-.001	12	.209	3
598			min	-75.057	10	-579.344	1	3.51	12	0	1	-.052	4	-.435	1
599		15	max	322.296	3	225.64	3	186.565	4	0	3	.063	4	.068	3
600			min	-74.577	10	-580.927	1	3.51	12	0	1	.001	12	-.075	1
601		16	max	322.728	3	224.453	3	188.025	4	0	3	.179	4	.286	1
602			min	-74.097	10	-582.51	1	3.51	12	0	1	.003	12	-.071	3
603		17	max	323.16	3	223.265	3	189.486	4	0	3	.297	4	.648	1
604			min	-73.617	10	-584.094	1	3.51	12	0	1	.005	12	-.21	3
605		18	max	-7.048	12	541.907	1	90.602	1	0	1	.266	4	.323	1
606			min	-174.634	1	-179.888	3	-88.301	5	0	3	.008	12	-.103	3
607		19	max	-6.76	12	540.324	1	90.602	1	0	1	.23	1	.009	3
608			min	-174.058	1	-181.075	3	-86.841	5	0	3	.01	12	-.013	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.188	1	.006	3	1.259e-2	1	NC	1	NC	1
2			min	-.753	4	-.027	3	-.003	2	-1.646e-3	3	NC	1	NC	1
3		2	max	0	1	.153	3	.035	1	1.389e-2	1	NC	5	NC	2
4			min	-.753	4	.002	15	-.018	5	-1.518e-3	3	1233.469	3	6617.917	1
5		3	max	0	1	.299	3	.081	1	1.519e-2	1	NC	5	NC	3
6			min	-.753	4	-.081	1	-.023	5	-1.39e-3	3	680.923	3	2791.611	1
7		4	max	0	1	.389	3	.12	1	1.65e-2	1	NC	5	NC	3
8			min	-.753	4	-.142	1	-.017	5	-1.262e-3	3	534.512	3	1874.903	1
9		5	max	0	1	.411	3	.139	1	1.78e-2	1	NC	5	NC	3
10			min	-.753	4	-.137	1	-.006	5	-1.134e-3	3	507.759	3	1612.441	1
11		6	max	0	1	.367	3	.133	1	1.911e-2	1	NC	5	NC	3
12			min	-.753	4	-.068	1	.004	15	-1.005e-3	3	564.692	3	1683.746	1
13		7	max	0	1	.27	3	.104	1	2.041e-2	1	NC	5	NC	3
14			min	-.753	4	.002	15	.004	10	-8.773e-4	3	748.283	3	2167.189	1
15		8	max	0	1	.191	1	.059	1	2.171e-2	1	NC	1	NC	2
16			min	-.753	4	.006	15	0	10	-7.493e-4	3	1279.007	3	3828.69	1
17		9	max	0	1	.315	1	.022	4	2.302e-2	1	NC	5	NC	1
18			min	-.753	4	.009	15	-.006	10	-6.212e-4	3	1750.073	1	9852.558	4
19		10	max	0	1	.37	1	.018	3	2.432e-2	1	NC	3	NC	1
20			min	-.753	4	-.016	3	-.012	2	-4.931e-4	3	1219.893	1	NC	1
21		11	max	0	12	.315	1	.019	3	2.302e-2	1	NC	5	NC	1
22			min	-.753	4	.009	15	-.014	5	-6.212e-4	3	1750.073	1	NC	1
23		12	max	0	12	.191	1	.059	1	2.171e-2	1	NC	1	NC	2
24			min	-.753	4	.006	15	-.014	5	-7.493e-4	3	1279.007	3	3828.69	1
25		13	max	0	12	.27	3	.104	1	2.041e-2	1	NC	5	NC	3
26			min	-.753	4	.002	15	-.005	5	-8.773e-4	3	748.283	3	2167.189	1
27		14	max	0	12	.367	3	.133	1	1.911e-2	1	NC	5	NC	3
28			min	-.753	4	-.068	1	.005	15	-1.005e-3	3	564.692	3	1683.746	1
29		15	max	0	12	.411	3	.139	1	1.78e-2	1	NC	5	NC	3
30			min	-.753	4	-.137	1	.009	10	-1.134e-3	3	507.759	3	1612.441	1
31		16	max	0	12	.389	3	.12	1	1.65e-2	1	NC	5	NC	3
32			min	-.753	4	-.142	1	.008	10	-1.262e-3	3	534.512	3	1874.903	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	12	.299	3	.081	1	1.519e-2	1	NC	5	NC	3
34			min	-.753	4	-.081	1	.005	10	-1.39e-3	3	680.923	3	2791.611	1
35		18	max	0	12	.153	3	.035	1	1.389e-2	1	NC	5	NC	2
36			min	-.753	4	.002	15	0	10	-1.518e-3	3	1233.469	3	6617.917	1
37		19	max	0	12	.188	1	.006	3	1.259e-2	1	NC	1	NC	1
38			min	-.753	4	-.027	3	-.003	2	-1.646e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.242	3	.005	3	7.616e-3	1	NC	1	NC	1
40			min	-.569	4	-.582	1	-.002	2	-3.747e-3	3	NC	1	NC	1
41		2	max	0	1	.442	3	.023	1	8.92e-3	1	NC	5	NC	1
42			min	-.569	4	-.903	1	-.027	5	-4.47e-3	3	691.407	1	8618.03	5
43		3	max	0	1	.615	3	.063	1	1.022e-2	1	NC	15	NC	3
44			min	-.569	4	-1.186	1	-.033	5	-5.192e-3	3	367.44	1	3625.138	1
45		4	max	0	1	.742	3	.1	1	1.153e-2	1	9973.555	15	NC	3
46			min	-.569	4	-1.405	1	-.024	5	-5.915e-3	3	269.864	1	2256.732	1
47		5	max	0	1	.813	3	.121	1	1.283e-2	1	8546.849	15	NC	3
48			min	-.569	4	-1.544	1	-.005	5	-6.637e-3	3	230.732	1	1860.815	1
49		6	max	0	1	.827	3	.119	1	1.413e-2	1	8081.162	15	NC	3
50			min	-.569	4	-1.603	1	.007	10	-7.36e-3	3	217.473	1	1891.092	1
51		7	max	0	1	.795	3	.095	1	1.544e-2	1	8209.487	15	NC	3
52			min	-.569	4	-1.591	1	.004	10	-8.082e-3	3	220.008	1	2386.53	1
53		8	max	0	1	.732	3	.055	1	1.674e-2	1	8767.557	15	NC	2
54			min	-.569	4	-1.532	1	0	10	-8.805e-3	3	233.766	1	4142.646	1
55		9	max	0	1	.667	3	.035	4	1.804e-2	1	9534.582	15	NC	1
56			min	-.569	4	-1.46	1	-.005	10	-9.527e-3	3	252.9	1	6246.264	4
57		10	max	0	1	.636	3	.016	3	1.935e-2	1	9978	15	NC	1
58			min	-.569	4	-1.423	1	-.011	2	-1.025e-2	3	263.96	1	NC	1
59		11	max	0	12	.667	3	.017	3	1.804e-2	1	9534.551	15	NC	1
60			min	-.569	4	-1.46	1	-.027	5	-9.527e-3	3	252.9	1	8630.79	5
61		12	max	0	12	.732	3	.055	1	1.674e-2	1	8767.462	15	NC	2
62			min	-.569	4	-1.532	1	-.032	5	-8.805e-3	3	233.766	1	4142.646	1
63		13	max	0	12	.795	3	.095	1	1.544e-2	1	8209.326	15	NC	3
64			min	-.569	4	-1.591	1	-.021	5	-8.082e-3	3	220.008	1	2386.53	1
65		14	max	0	12	.827	3	.119	1	1.413e-2	1	8080.93	15	NC	3
66			min	-.569	4	-1.603	1	-.002	5	-7.36e-3	3	217.473	1	1891.092	1
67		15	max	0	12	.813	3	.121	1	1.283e-2	1	8546.524	15	NC	3
68			min	-.569	4	-1.544	1	.008	10	-6.637e-3	3	230.732	1	1860.815	1
69		16	max	0	12	.742	3	.1	1	1.153e-2	1	9973.076	15	NC	3
70			min	-.569	4	-1.405	1	.007	10	-5.915e-3	3	269.864	1	2256.732	1
71		17	max	0	12	.615	3	.063	1	1.022e-2	1	NC	15	NC	3
72			min	-.569	4	-1.186	1	.003	10	-5.192e-3	3	367.44	1	3625.138	1
73		18	max	0	12	.442	3	.036	4	8.92e-3	1	NC	5	NC	1
74			min	-.569	4	-.903	1	0	10	-4.47e-3	3	691.407	1	6013.089	4
75		19	max	0	12	.242	3	.005	3	7.616e-3	1	NC	1	NC	1
76			min	-.569	4	-.582	1	-.002	2	-3.747e-3	3	NC	1	NC	1
77	M15	1	max	0	12	.248	3	.005	3	3.118e-3	3	NC	1	NC	1
78			min	-.462	4	-.581	1	-.002	2	-7.748e-3	1	NC	1	NC	1
79		2	max	0	12	.385	3	.023	1	3.716e-3	3	NC	5	NC	1
80			min	-.462	4	-.926	1	-.04	5	-9.083e-3	1	645.175	1	5810.029	5
81		3	max	0	12	.507	3	.063	1	4.314e-3	3	NC	15	NC	3
82			min	-.462	4	-1.227	1	-.049	5	-1.042e-2	1	343.767	1	3605.856	1
83		4	max	0	12	.603	3	.1	1	4.912e-3	3	9986.755	15	NC	3
84			min	-.462	4	-1.457	1	-.037	5	-1.175e-2	1	253.58	1	2247.232	1
85		5	max	0	12	.668	3	.121	1	5.511e-3	3	8559.411	15	NC	3
86			min	-.462	4	-1.599	1	-.012	5	-1.309e-2	1	218.193	1	1853.575	1
87		6	max	0	12	.701	3	.119	1	6.109e-3	3	8094.667	15	NC	3
88			min	-.462	4	-1.651	1	.007	10	-1.442e-2	1	207.472	1	1883.282	1
89		7	max	0	12	.705	3	.095	1	6.707e-3	3	8225.392	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.462	4	-1.627	1	.004	10	-1.576e-2	1	212.359	1	2374.09	1
91		8	max	0	12	.688	3	.065	4	7.305e-3	3	8787.418	15	NC	2
92			min	-.462	4	-1.551	1	0	10	-1.709e-2	1	228.926	1	3396.998	4
93		9	max	0	12	.665	3	.045	4	7.903e-3	3	9559.374	15	NC	1
94			min	-.462	4	-1.465	1	-.005	10	-1.843e-2	1	251.368	1	4835.542	4
95		10	max	0	1	.652	3	.015	3	8.501e-3	3	NC	15	NC	1
96			min	-.462	4	-1.421	1	-.01	2	-1.976e-2	1	264.372	1	NC	1
97		11	max	0	1	.665	3	.016	1	7.903e-3	3	9559.349	15	NC	1
98			min	-.462	4	-1.465	1	-.038	5	-1.843e-2	1	251.368	1	6131.892	5
99		12	max	0	1	.688	3	.056	1	7.305e-3	3	8787.35	15	NC	2
100			min	-.462	4	-1.551	1	-.044	5	-1.709e-2	1	228.926	1	4106.123	1
101		13	max	0	1	.705	3	.095	1	6.707e-3	3	8225.28	15	NC	3
102			min	-.462	4	-1.627	1	-.03	5	-1.576e-2	1	212.359	1	2374.09	1
103		14	max	0	1	.701	3	.119	1	6.109e-3	3	8094.509	15	NC	3
104			min	-.462	4	-1.651	1	-.004	5	-1.442e-2	1	207.472	1	1883.282	1
105		15	max	0	1	.668	3	.121	1	5.511e-3	3	8559.192	15	NC	3
106			min	-.462	4	-1.599	1	.008	10	-1.309e-2	1	218.193	1	1853.575	1
107		16	max	0	1	.603	3	.1	1	4.912e-3	3	9986.434	15	NC	3
108			min	-.462	4	-1.457	1	.007	10	-1.175e-2	1	253.58	1	2247.232	1
109		17	max	0	1	.507	3	.071	4	4.314e-3	3	NC	15	NC	3
110			min	-.462	4	-1.227	1	.004	10	-1.042e-2	1	343.767	1	3086.467	4
111		18	max	0	1	.385	3	.049	4	3.716e-3	3	NC	5	NC	1
112			min	-.462	4	-.926	1	0	10	-9.083e-3	1	645.175	1	4497.788	4
113		19	max	0	1	.248	3	.005	3	3.118e-3	3	NC	1	NC	1
114			min	-.462	4	-.581	1	-.002	2	-7.748e-3	1	NC	1	NC	1
115	M16	1	max	0	12	.183	1	.004	3	5.706e-3	3	NC	1	NC	1
116			min	-.146	4	-.086	3	-.002	2	-1.189e-2	1	NC	1	NC	1
117		2	max	0	12	.015	9	.034	1	6.477e-3	3	NC	5	NC	2
118			min	-.146	4	-.034	3	-.028	5	-1.303e-2	1	1260.606	1	6695.502	1
119		3	max	0	12	.005	3	.08	1	7.249e-3	3	NC	5	NC	3
120			min	-.146	4	-.144	2	-.035	5	-1.417e-2	1	707.066	1	2807.417	1
121		4	max	0	12	.023	3	.119	1	8.021e-3	3	NC	5	NC	3
122			min	-.146	4	-.215	2	-.028	5	-1.531e-2	1	571.947	1	1878.914	1
123		5	max	0	12	.015	3	.139	1	8.793e-3	3	NC	5	NC	3
124			min	-.146	4	-.217	2	-.012	5	-1.645e-2	1	573.466	1	1611.034	1
125		6	max	0	12	0	15	.134	1	9.565e-3	3	NC	5	NC	3
126			min	-.146	4	-.155	2	.005	15	-1.759e-2	1	708.533	1	1676.174	1
127		7	max	0	12	.021	9	.105	1	1.034e-2	3	NC	3	NC	3
128			min	-.146	4	-.066	3	.006	10	-1.873e-2	1	1195.707	2	2144.214	1
129		8	max	0	12	.156	1	.061	1	1.111e-2	3	NC	4	NC	2
130			min	-.146	4	-.123	3	0	10	-1.986e-2	1	4634.162	2	3728.991	1
131		9	max	0	12	.294	1	.029	4	1.188e-2	3	NC	5	NC	1
132			min	-.146	4	-.173	3	-.004	10	-2.1e-2	1	1997.627	1	7500.059	4
133		10	max	0	1	.356	1	.013	3	1.265e-2	3	NC	5	NC	1
134			min	-.146	4	-.194	3	-.009	2	-2.214e-2	1	1285.22	1	NC	1
135		11	max	0	1	.294	1	.017	1	1.188e-2	3	NC	5	NC	1
136			min	-.146	4	-.173	3	-.021	5	-2.1e-2	1	1997.627	1	NC	1
137		12	max	0	1	.156	1	.061	1	1.111e-2	3	NC	4	NC	2
138			min	-.146	4	-.123	3	-.023	5	-1.986e-2	1	4634.162	2	3728.991	1
139		13	max	0	1	.021	9	.105	1	1.034e-2	3	NC	3	NC	3
140			min	-.146	4	-.066	3	-.011	5	-1.873e-2	1	1195.707	2	2144.214	1
141		14	max	0	1	0	15	.134	1	9.565e-3	3	NC	5	NC	3
142			min	-.146	4	-.155	2	.005	15	-1.759e-2	1	708.533	1	1676.174	1
143		15	max	0	1	.015	3	.139	1	8.793e-3	3	NC	5	NC	3
144			min	-.146	4	-.217	2	.01	12	-1.645e-2	1	573.466	1	1611.034	1
145		16	max	0	1	.023	3	.119	1	8.021e-3	3	NC	5	NC	3
146			min	-.146	4	-.215	2	.009	12	-1.531e-2	1	571.947	1	1878.914	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.005	3	.08	1	7.249e-3	3	NC	5	NC	3
148			min	-.146	4	-.144	2	.006	10	-1.417e-2	1	707.066	1	2807.417	1
149		18	max	0	1	.015	9	.04	4	6.477e-3	3	NC	5	NC	2
150			min	-.146	4	-.034	3	.001	10	-1.303e-2	1	1260.606	1	5483.304	4
151		19	max	0	1	.183	1	.004	3	5.706e-3	3	NC	1	NC	1
152			min	-.146	4	-.086	3	-.002	2	-1.189e-2	1	NC	1	NC	1
153	M2	1	max	.006	1	.005	2	.011	1	2.598e-3	5	NC	1	NC	2
154			min	-.005	3	-.008	3	-.707	4	-2.399e-4	1	NC	1	85.699	4
155		2	max	.006	1	.004	2	.01	1	2.607e-3	5	NC	1	NC	2
156			min	-.005	3	-.008	3	-.648	4	-2.247e-4	1	NC	1	93.396	4
157		3	max	.006	1	.003	2	.009	1	2.616e-3	5	NC	1	NC	2
158			min	-.004	3	-.008	3	-.591	4	-2.095e-4	1	NC	1	102.551	4
159		4	max	.005	1	.002	2	.008	1	2.624e-3	5	NC	1	NC	2
160			min	-.004	3	-.008	3	-.533	4	-1.943e-4	1	NC	1	113.55	4
161		5	max	.005	1	.001	2	.007	1	2.633e-3	5	NC	1	NC	2
162			min	-.004	3	-.007	3	-.477	4	-1.791e-4	1	NC	1	126.915	4
163		6	max	.005	1	0	2	.006	1	2.642e-3	5	NC	1	NC	2
164			min	-.004	3	-.007	3	-.422	4	-1.639e-4	1	NC	1	143.371	4
165		7	max	.004	1	0	2	.006	1	2.652e-3	4	NC	1	NC	1
166			min	-.003	3	-.007	3	-.369	4	-1.486e-4	1	NC	1	163.954	4
167		8	max	.004	1	0	15	.005	1	2.665e-3	4	NC	1	NC	1
168			min	-.003	3	-.007	3	-.318	4	-1.334e-4	1	NC	1	190.178	4
169		9	max	.004	1	0	15	.004	1	2.678e-3	4	NC	1	NC	1
170			min	-.003	3	-.006	3	-.27	4	-1.182e-4	1	NC	1	224.33	4
171		10	max	.003	1	0	15	.003	1	2.691e-3	4	NC	1	NC	1
172			min	-.003	3	-.006	3	-.224	4	-1.03e-4	1	NC	1	270.005	4
173		11	max	.003	1	0	15	.003	1	2.704e-3	4	NC	1	NC	1
174			min	-.002	3	-.006	3	-.182	4	-8.776e-5	1	NC	1	333.117	4
175		12	max	.002	1	0	15	.002	1	2.717e-3	4	NC	1	NC	1
176			min	-.002	3	-.005	3	-.143	4	-7.255e-5	1	NC	1	423.975	4
177		13	max	.002	1	0	15	.002	1	2.73e-3	4	NC	1	NC	1
178			min	-.002	3	-.005	3	-.108	4	-5.733e-5	1	NC	1	561.888	4
179		14	max	.002	1	0	15	.001	1	2.743e-3	4	NC	1	NC	1
180			min	-.001	3	-.004	3	-.077	4	-4.211e-5	1	NC	1	786.629	4
181		15	max	.001	1	0	15	0	1	2.756e-3	4	NC	1	NC	1
182			min	-.001	3	-.003	3	-.051	4	-2.689e-5	1	NC	1	1191.435	4
183		16	max	.001	1	0	15	0	1	2.769e-3	4	NC	1	NC	1
184			min	0	3	-.003	6	-.03	4	-1.167e-5	1	NC	1	2040.546	4
185		17	max	0	1	0	15	0	1	2.782e-3	4	NC	1	NC	1
186			min	0	3	-.002	6	-.014	4	-2.329e-7	3	NC	1	4354.909	4
187		18	max	0	1	0	15	0	1	2.794e-3	4	NC	1	NC	1
188			min	0	3	-.001	6	-.004	4	6.099e-7	12	NC	1	NC	1
189		19	max	0	1	0	1	0	1	2.807e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	1.358e-6	12	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	-4.301e-7	12	NC	1	NC	1
192			min	0	1	0	1	0	1	-5.413e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.016	4	1.824e-4	4	NC	1	NC	1
194			min	0	2	-.002	6	0	12	9.079e-7	12	NC	1	NC	1
195		3	max	0	3	-.001	15	.031	4	9.06e-4	4	NC	1	NC	1
196			min	0	2	-.005	6	0	12	2.246e-6	12	NC	1	NC	1
197		4	max	0	3	-.002	15	.045	4	1.63e-3	4	NC	1	NC	1
198			min	0	2	-.008	6	0	12	3.584e-6	12	NC	1	NC	1
199		5	max	.001	3	-.002	15	.059	4	2.353e-3	4	NC	1	NC	1
200			min	0	2	-.011	6	0	12	4.922e-6	12	9466.312	6	8377.311	5
201		6	max	.001	3	-.003	15	.073	4	3.077e-3	4	NC	2	NC	1
202			min	0	2	-.014	6	0	12	6.26e-6	12	7582.385	6	7309.545	5
203		7	max	.002	3	-.004	15	.086	4	3.801e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.001	2	-.016	6	0	12	7.598e-6	12	6453.077	6	6727.781	5
205		8	max	.002	3	-.004	15	.098	4	4.524e-3	4	NC	5	NC	1
206			min	-.001	2	-.018	6	0	12	8.936e-6	12	5755.957	6	6459.126	5
207		9	max	.002	3	-.004	15	.11	4	5.248e-3	4	NC	5	NC	1
208			min	-.001	2	-.019	6	0	12	1.027e-5	12	5339.719	6	6431.894	5
209		10	max	.002	3	-.004	15	.122	4	5.972e-3	4	NC	5	NC	1
210			min	-.002	2	-.02	6	0	12	1.161e-5	12	5130.544	6	6627.512	5
211		11	max	.003	3	-.004	15	.133	4	6.695e-3	4	NC	5	NC	1
212			min	-.002	2	-.02	6	0	12	1.295e-5	12	5097.126	6	7067.329	5
213		12	max	.003	3	-.004	15	.143	4	7.419e-3	4	NC	5	NC	1
214			min	-.002	2	-.02	6	0	12	1.429e-5	12	5238.592	6	7817.993	5
215		13	max	.003	3	-.004	15	.153	4	8.143e-3	4	NC	5	NC	1
216			min	-.002	2	-.018	6	0	12	1.563e-5	12	5585.64	6	9017.618	5
217		14	max	.003	3	-.004	15	.163	4	8.866e-3	4	NC	5	NC	1
218			min	-.002	2	-.017	6	0	12	1.696e-5	12	6216.873	6	NC	1
219		15	max	.004	3	-.003	15	.173	4	9.59e-3	4	NC	3	NC	1
220			min	-.003	2	-.014	6	0	12	1.83e-5	12	7308.125	6	NC	1
221		16	max	.004	3	-.002	15	.183	4	1.031e-2	4	NC	1	NC	1
222			min	-.003	2	-.011	6	0	12	1.964e-5	12	9286.487	6	NC	1
223		17	max	.004	3	-.002	15	.192	4	1.104e-2	4	NC	1	NC	1
224			min	-.003	2	-.008	1	0	12	2.098e-5	12	NC	1	NC	1
225		18	max	.004	3	0	15	.203	4	1.176e-2	4	NC	1	NC	1
226			min	-.003	2	-.006	1	0	12	2.232e-5	12	NC	1	NC	1
227		19	max	.005	3	0	5	.213	4	1.248e-2	4	NC	1	NC	1
228			min	-.003	2	-.003	1	0	12	2.365e-5	12	NC	1	NC	1
229	M4	1	max	.003	1	.003	2	0	12	8.135e-5	1	NC	1	NC	3
230			min	0	3	-.005	3	-.213	4	-1.149e-3	4	NC	1	116.288	4
231		2	max	.003	1	.003	2	0	12	8.135e-5	1	NC	1	NC	3
232			min	0	3	-.004	3	-.196	4	-1.149e-3	4	NC	1	126.636	4
233		3	max	.002	1	.003	2	0	12	8.135e-5	1	NC	1	NC	3
234			min	0	3	-.004	3	-.179	4	-1.149e-3	4	NC	1	138.94	4
235		4	max	.002	1	.002	2	0	12	8.135e-5	1	NC	1	NC	3
236			min	0	3	-.004	3	-.161	4	-1.149e-3	4	NC	1	153.712	4
237		5	max	.002	1	.002	2	0	12	8.135e-5	1	NC	1	NC	3
238			min	0	3	-.004	3	-.145	4	-1.149e-3	4	NC	1	171.644	4
239		6	max	.002	1	.002	2	0	12	8.135e-5	1	NC	1	NC	2
240			min	0	3	-.003	3	-.128	4	-1.149e-3	4	NC	1	193.697	4
241		7	max	.002	1	.002	2	0	12	8.135e-5	1	NC	1	NC	2
242			min	0	3	-.003	3	-.112	4	-1.149e-3	4	NC	1	221.236	4
243		8	max	.002	1	.002	2	0	12	8.135e-5	1	NC	1	NC	2
244			min	0	3	-.003	3	-.097	4	-1.149e-3	4	NC	1	256.252	4
245		9	max	.002	1	.002	2	0	12	8.135e-5	1	NC	1	NC	2
246			min	0	3	-.003	3	-.082	4	-1.149e-3	4	NC	1	301.741	4
247		10	max	.001	1	.001	2	0	12	8.135e-5	1	NC	1	NC	2
248			min	0	3	-.002	3	-.068	4	-1.149e-3	4	NC	1	362.389	4
249		11	max	.001	1	.001	2	0	12	8.135e-5	1	NC	1	NC	2
250			min	0	3	-.002	3	-.056	4	-1.149e-3	4	NC	1	445.862	4
251		12	max	.001	1	.001	2	0	12	8.135e-5	1	NC	1	NC	1
252			min	0	3	-.002	3	-.044	4	-1.149e-3	4	NC	1	565.424	4
253		13	max	0	1	0	2	0	12	8.135e-5	1	NC	1	NC	1
254			min	0	3	-.002	3	-.033	4	-1.149e-3	4	NC	1	745.7	4
255		14	max	0	1	0	2	0	12	8.135e-5	1	NC	1	NC	1
256			min	0	3	-.001	3	-.024	4	-1.149e-3	4	NC	1	1036.795	4
257		15	max	0	1	0	2	0	12	8.135e-5	1	NC	1	NC	1
258			min	0	3	-.001	3	-.016	4	-1.149e-3	4	NC	1	1554.25	4
259		16	max	0	1	0	2	0	12	8.135e-5	1	NC	1	NC	1
260			min	0	3	0	3	-.009	4	-1.149e-3	4	NC	1	2617.567	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	8.135e-5	1	NC	1	NC	1
262			min	0	3	0	3	-.005	4	-1.149e-3	4	NC	1	5411.966	4
263		18	max	0	1	0	2	0	12	8.135e-5	1	NC	1	NC	1
264			min	0	3	0	3	-.001	4	-1.149e-3	4	NC	1	NC	1
265		19	max	0	1	0	1	0	1	8.135e-5	1	NC	1	NC	1
266			min	0	1	0	1	0	1	-1.149e-3	4	NC	1	NC	1
267	M6	1	max	.02	1	.019	2	0	1	2.72e-3	4	NC	3	NC	1
268			min	-.016	3	-.025	3	-.714	4	0	1	3273.275	2	84.815	4
269		2	max	.019	1	.017	2	0	1	2.725e-3	4	NC	3	NC	1
270			min	-.015	3	-.023	3	-.655	4	0	1	3612.166	2	92.433	4
271		3	max	.018	1	.015	2	0	1	2.73e-3	4	NC	3	NC	1
272			min	-.014	3	-.022	3	-.597	4	0	1	4025.771	2	101.495	4
273		4	max	.017	1	.013	2	0	1	2.735e-3	4	NC	3	NC	1
274			min	-.014	3	-.021	3	-.539	4	0	1	4537.294	2	112.381	4
275		5	max	.016	1	.012	2	0	1	2.74e-3	4	NC	3	NC	1
276			min	-.013	3	-.02	3	-.482	4	0	1	5180.036	2	125.609	4
277		6	max	.014	1	.01	2	0	1	2.745e-3	4	NC	3	NC	1
278			min	-.012	3	-.018	3	-.427	4	0	1	6003.233	2	141.897	4
279		7	max	.013	1	.009	2	0	1	2.75e-3	4	NC	1	NC	1
280			min	-.011	3	-.017	3	-.373	4	0	1	7082.304	2	162.27	4
281		8	max	.012	1	.007	2	0	1	2.755e-3	4	NC	1	NC	1
282			min	-.01	3	-.016	3	-.322	4	0	1	8537.84	2	188.226	4
283		9	max	.011	1	.006	2	0	1	2.761e-3	4	NC	1	NC	1
284			min	-.009	3	-.015	3	-.273	4	0	1	NC	1	222.03	4
285		10	max	.01	1	.004	2	0	1	2.766e-3	4	NC	1	NC	1
286			min	-.008	3	-.013	3	-.227	4	0	1	NC	1	267.24	4
287		11	max	.009	1	.003	2	0	1	2.771e-3	4	NC	1	NC	1
288			min	-.007	3	-.012	3	-.184	4	0	1	NC	1	329.71	4
289		12	max	.008	1	.002	2	0	1	2.776e-3	4	NC	1	NC	1
290			min	-.006	3	-.011	3	-.144	4	0	1	NC	1	419.644	4
291		13	max	.007	1	.001	2	0	1	2.781e-3	4	NC	1	NC	1
292			min	-.005	3	-.009	3	-.109	4	0	1	NC	1	556.159	4
293		14	max	.006	1	0	2	0	1	2.786e-3	4	NC	1	NC	1
294			min	-.005	3	-.008	3	-.078	4	0	1	NC	1	778.624	4
295		15	max	.004	1	0	2	0	1	2.791e-3	4	NC	1	NC	1
296			min	-.004	3	-.006	3	-.051	4	0	1	NC	1	1179.342	4
297		16	max	.003	1	0	2	0	1	2.796e-3	4	NC	1	NC	1
298			min	-.003	3	-.005	3	-.03	4	0	1	NC	1	2019.913	4
299		17	max	.002	1	0	2	0	1	2.801e-3	4	NC	1	NC	1
300			min	-.002	3	-.003	3	-.014	4	0	1	NC	1	4311.159	4
301		18	max	.001	1	0	2	0	1	2.807e-3	4	NC	1	NC	1
302			min	0	3	-.002	3	-.004	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	2.812e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-5.409e-4	4	NC	1	NC	1
307		2	max	0	3	0	15	.016	4	1.62e-4	4	NC	1	NC	1
308			min	0	2	-.003	3	0	1	0	1	NC	1	NC	1
309		3	max	.002	3	-.001	15	.031	4	8.649e-4	4	NC	1	NC	1
310			min	-.001	2	-.006	3	0	1	0	1	NC	1	NC	1
311		4	max	.002	3	-.002	15	.045	4	1.568e-3	4	NC	1	NC	1
312			min	-.002	2	-.008	3	0	1	0	1	NC	1	9314.164	4
313		5	max	.003	3	-.003	15	.059	4	2.271e-3	4	NC	1	NC	1
314			min	-.003	2	-.011	4	0	1	0	1	9547.311	4	7497.274	4
315		6	max	.004	3	-.003	15	.073	4	2.973e-3	4	NC	1	NC	1
316			min	-.004	2	-.014	4	0	1	0	1	7640.769	4	6506.936	4
317		7	max	.005	3	-.004	15	.086	4	3.676e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.004	2	-.016	4	0	1	0	1	6498.378	4	5952.155	4
319		8	max	.005	3	-.004	15	.098	4	4.379e-3	4	NC	2	NC	1
320			min	-.005	2	-.018	4	0	1	0	1	5793.196	4	5673.513	4
321		9	max	.006	3	-.005	15	.11	4	5.082e-3	4	NC	5	NC	1
322			min	-.006	2	-.02	4	0	1	0	1	5371.853	4	5602.225	4
323		10	max	.007	3	-.005	15	.121	4	5.785e-3	4	NC	5	NC	1
324			min	-.007	2	-.021	4	0	1	0	1	5159.497	4	5715.566	4
325		11	max	.008	3	-.005	15	.131	4	6.488e-3	4	NC	5	NC	1
326			min	-.007	2	-.021	4	0	1	0	1	5124.297	4	6023.164	4
327		12	max	.009	3	-.005	15	.141	4	7.191e-3	4	NC	5	NC	1
328			min	-.008	2	-.02	4	0	1	0	1	5265.146	4	6568.419	4
329		13	max	.009	3	-.004	15	.151	4	7.894e-3	4	NC	5	NC	1
330			min	-.009	2	-.019	4	0	1	0	1	5612.734	4	7444.663	4
331		14	max	.01	3	-.004	15	.16	4	8.596e-3	4	NC	5	NC	1
332			min	-.01	2	-.017	4	0	1	0	1	6245.906	4	8838.679	4
333		15	max	.011	3	-.003	15	.169	4	9.299e-3	4	NC	1	NC	1
334			min	-.01	2	-.015	4	0	1	0	1	7341.182	4	NC	1
335		16	max	.012	3	-.003	15	.178	4	1.e-2	4	NC	1	NC	1
336			min	-.011	2	-.012	4	0	1	0	1	9327.425	4	NC	1
337		17	max	.012	3	-.002	15	.187	4	1.071e-2	4	NC	1	NC	1
338			min	-.012	2	-.01	1	0	1	0	1	NC	1	NC	1
339		18	max	.013	3	-.001	15	.197	4	1.141e-2	4	NC	1	NC	1
340			min	-.013	2	-.008	1	0	1	0	1	NC	1	NC	1
341		19	max	.014	3	0	15	.206	4	1.211e-2	4	NC	1	NC	1
342			min	-.013	2	-.006	1	0	1	0	1	NC	1	NC	1
343	M8	1	max	.008	1	.012	2	0	1	0	1	NC	1	NC	1
344			min	-.001	3	-.014	3	-.206	4	-1.27e-3	4	NC	1	120.388	4
345		2	max	.007	1	.011	2	0	1	0	1	NC	1	NC	1
346			min	-.001	3	-.013	3	-.189	4	-1.27e-3	4	NC	1	131.112	4
347		3	max	.007	1	.011	2	0	1	0	1	NC	1	NC	1
348			min	-.001	3	-.013	3	-.172	4	-1.27e-3	4	NC	1	143.863	4
349		4	max	.006	1	.01	2	0	1	0	1	NC	1	NC	1
350			min	-.001	3	-.012	3	-.156	4	-1.27e-3	4	NC	1	159.17	4
351		5	max	.006	1	.009	2	0	1	0	1	NC	1	NC	1
352			min	0	3	-.011	3	-.14	4	-1.27e-3	4	NC	1	177.751	4
353		6	max	.006	1	.009	2	0	1	0	1	NC	1	NC	1
354			min	0	3	-.01	3	-.124	4	-1.27e-3	4	NC	1	200.603	4
355		7	max	.005	1	.008	2	0	1	0	1	NC	1	NC	1
356			min	0	3	-.009	3	-.108	4	-1.27e-3	4	NC	1	229.138	4
357		8	max	.005	1	.007	2	0	1	0	1	NC	1	NC	1
358			min	0	3	-.009	3	-.093	4	-1.27e-3	4	NC	1	265.421	4
359		9	max	.004	1	.007	2	0	1	0	1	NC	1	NC	1
360			min	0	3	-.008	3	-.079	4	-1.27e-3	4	NC	1	312.557	4
361		10	max	.004	1	.006	2	0	1	0	1	NC	1	NC	1
362			min	0	3	-.007	3	-.066	4	-1.27e-3	4	NC	1	375.4	4
363		11	max	.003	1	.005	2	0	1	0	1	NC	1	NC	1
364			min	0	3	-.006	3	-.054	4	-1.27e-3	4	NC	1	461.896	4
365		12	max	.003	1	.005	2	0	1	0	1	NC	1	NC	1
366			min	0	3	-.005	3	-.042	4	-1.27e-3	4	NC	1	585.789	4
367		13	max	.003	1	.004	2	0	1	0	1	NC	1	NC	1
368			min	0	3	-.005	3	-.032	4	-1.27e-3	4	NC	1	772.597	4
369		14	max	.002	1	.003	2	0	1	0	1	NC	1	NC	1
370			min	0	3	-.004	3	-.023	4	-1.27e-3	4	NC	1	1074.247	4
371		15	max	.002	1	.003	2	0	1	0	1	NC	1	NC	1
372			min	0	3	-.003	3	-.015	4	-1.27e-3	4	NC	1	1610.477	4
373		16	max	.001	1	.002	2	0	1	0	1	NC	1	NC	1
374			min	0	3	-.002	3	-.009	4	-1.27e-3	4	NC	1	2712.41	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	1	.001	2	0	1	0	1	NC	1	NC	1
376			min	0	3	-.002	3	-.004	4	-1.27e-3	4	NC	1	5608.418	4
377		18	max	0	1	0	2	0	1	0	1	NC	1	NC	1
378			min	0	3	0	3	-.001	4	-1.27e-3	4	NC	1	NC	1
379		19	max	0	1	0	1	0	1	0	1	NC	1	NC	1
380			min	0	1	0	1	0	1	-1.27e-3	4	NC	1	NC	1
381	M10	1	max	.006	1	.005	2	0	12	2.701e-3	4	NC	1	NC	2
382			min	-.005	3	-.008	3	-.712	4	1.211e-5	12	NC	1	85.026	4
383		2	max	.006	1	.004	2	0	12	2.706e-3	4	NC	1	NC	2
384			min	-.005	3	-.008	3	-.654	4	1.136e-5	12	NC	1	92.663	4
385		3	max	.006	1	.003	2	0	12	2.711e-3	4	NC	1	NC	2
386			min	-.004	3	-.008	3	-.595	4	1.061e-5	12	NC	1	101.748	4
387		4	max	.005	1	.002	2	0	12	2.716e-3	4	NC	1	NC	2
388			min	-.004	3	-.008	3	-.538	4	9.865e-6	12	NC	1	112.661	4
389		5	max	.005	1	.001	2	0	12	2.721e-3	4	NC	1	NC	2
390			min	-.004	3	-.007	3	-.481	4	9.117e-6	12	NC	1	125.921	4
391		6	max	.005	1	0	2	0	12	2.726e-3	4	NC	1	NC	2
392			min	-.004	3	-.007	3	-.426	4	8.368e-6	12	NC	1	142.25	4
393		7	max	.004	1	0	2	0	12	2.731e-3	4	NC	1	NC	1
394			min	-.003	3	-.007	3	-.372	4	7.62e-6	12	NC	1	162.674	4
395		8	max	.004	1	0	2	0	12	2.735e-3	4	NC	1	NC	1
396			min	-.003	3	-.007	3	-.321	4	6.872e-6	12	NC	1	188.694	4
397		9	max	.004	1	-.001	2	0	12	2.74e-3	4	NC	1	NC	1
398			min	-.003	3	-.006	3	-.272	4	6.124e-6	12	NC	1	222.582	4
399		10	max	.003	1	-.001	2	0	12	2.745e-3	4	NC	1	NC	1
400			min	-.003	3	-.006	3	-.226	4	5.376e-6	12	NC	1	267.904	4
401		11	max	.003	1	-.002	15	0	12	2.75e-3	4	NC	1	NC	1
402			min	-.002	3	-.006	3	-.183	4	4.627e-6	12	NC	1	330.53	4
403		12	max	.002	1	-.001	15	0	12	2.755e-3	4	NC	1	NC	1
404			min	-.002	3	-.005	4	-.144	4	3.879e-6	12	NC	1	420.689	4
405		13	max	.002	1	-.001	15	0	12	2.76e-3	4	NC	1	NC	1
406			min	-.002	3	-.005	4	-.109	4	3.131e-6	12	NC	1	557.545	4
407		14	max	.002	1	-.001	15	0	12	2.765e-3	4	NC	1	NC	1
408			min	-.001	3	-.005	4	-.078	4	2.383e-6	12	NC	1	780.569	4
409		15	max	.001	1	-.001	15	0	12	2.769e-3	4	NC	1	NC	1
410			min	-.001	3	-.004	4	-.051	4	1.635e-6	12	NC	1	1182.301	4
411		16	max	.001	1	0	15	0	12	2.774e-3	4	NC	1	NC	1
412			min	0	3	-.003	4	-.03	4	8.865e-7	12	NC	1	2025.015	4
413		17	max	0	1	0	15	0	12	2.779e-3	4	NC	1	NC	1
414			min	0	3	-.002	4	-.014	4	-3.547e-6	1	NC	1	4322.2	4
415		18	max	0	1	0	15	0	12	2.784e-3	4	NC	1	NC	1
416			min	0	3	-.001	4	-.004	4	-1.877e-5	1	NC	1	NC	1
417		19	max	0	1	0	1	0	1	2.789e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	-3.398e-5	1	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	1.033e-5	1	NC	1	NC	1
420			min	0	1	0	1	0	1	-5.357e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.015	4	1.718e-4	4	NC	1	NC	1
422			min	0	2	-.003	4	0	1	-2.012e-5	1	NC	1	NC	1
423		3	max	0	3	-.001	15	.03	4	8.793e-4	4	NC	1	NC	1
424			min	0	2	-.006	4	0	1	-5.057e-5	1	NC	1	NC	1
425		4	max	0	3	-.002	15	.045	4	1.587e-3	4	NC	1	NC	1
426			min	0	2	-.009	4	0	1	-8.102e-5	1	NC	1	9941.178	4
427		5	max	.001	3	-.003	15	.059	4	2.294e-3	4	NC	1	NC	1
428			min	0	2	-.012	4	0	1	-1.115e-4	1	9037.728	4	8028.031	4
429		6	max	.001	3	-.004	15	.072	4	3.002e-3	4	NC	2	NC	1
430			min	0	2	-.014	4	-.001	1	-1.419e-4	1	7271.8	4	6993.374	4
431		7	max	.002	3	-.004	15	.085	4	3.709e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.001	2	-.017	4	-.001	1	-1.724e-4	1	6211.061	4	6424.159	4
433		8	max	.002	3	-.005	15	.098	4	4.417e-3	4	NC	5	NC	1
434			min	-.001	2	-.019	4	-.002	1	-2.028e-4	1	5556.315	4	6153.15	4
435		9	max	.002	3	-.005	15	.109	4	5.124e-3	4	NC	5	NC	1
436			min	-.001	2	-.02	4	-.002	1	-2.333e-4	1	5166.953	4	6109.969	4
437		10	max	.002	3	-.005	15	.12	4	5.832e-3	4	NC	5	NC	1
438			min	-.002	2	-.021	4	-.003	1	-2.637e-4	1	4974.509	4	6274.476	4
439		11	max	.003	3	-.005	15	.131	4	6.539e-3	4	NC	5	NC	1
440			min	-.002	2	-.021	4	-.003	1	-2.942e-4	1	4950.407	4	6663.373	4
441		12	max	.003	3	-.005	15	.141	4	7.247e-3	4	NC	5	NC	1
442			min	-.002	2	-.021	4	-.004	1	-3.246e-4	1	5094.962	4	7333.946	4
443		13	max	.003	3	-.005	15	.151	4	7.954e-3	4	NC	5	NC	1
444			min	-.002	2	-.02	4	-.004	1	-3.551e-4	1	5438.888	4	8406.058	4
445		14	max	.003	3	-.004	15	.16	4	8.662e-3	4	NC	5	NC	1
446			min	-.002	2	-.018	4	-.005	1	-3.855e-4	1	6059.437	4	NC	1
447		15	max	.004	3	-.004	15	.17	4	9.369e-3	4	NC	3	NC	1
448			min	-.003	2	-.015	4	-.006	1	-4.16e-4	1	7128.699	4	NC	1
449		16	max	.004	3	-.003	15	.179	4	1.008e-2	4	NC	1	NC	1
450			min	-.003	2	-.012	4	-.007	1	-4.464e-4	1	9064.122	4	NC	1
451		17	max	.004	3	-.002	15	.188	4	1.078e-2	4	NC	1	NC	1
452			min	-.003	2	-.009	4	-.008	1	-4.769e-4	1	NC	1	NC	1
453		18	max	.004	3	-.001	15	.198	4	1.149e-2	4	NC	1	NC	1
454			min	-.003	2	-.006	1	-.009	1	-5.073e-4	1	NC	1	NC	1
455		19	max	.005	3	0	10	.208	4	1.22e-2	4	NC	1	NC	1
456			min	-.003	2	-.003	1	-.01	1	-5.378e-4	1	NC	1	NC	1
457	M12	1	max	.003	1	.003	2	.01	1	-3.88e-6	12	NC	1	NC	3
458			min	0	3	-.005	3	-.208	4	-1.192e-3	4	NC	1	119.219	4
459		2	max	.003	1	.003	2	.009	1	-3.88e-6	12	NC	1	NC	3
460			min	0	3	-.004	3	-.191	4	-1.192e-3	4	NC	1	129.832	4
461		3	max	.002	1	.003	2	.008	1	-3.88e-6	12	NC	1	NC	3
462			min	0	3	-.004	3	-.174	4	-1.192e-3	4	NC	1	142.452	4
463		4	max	.002	1	.002	2	.008	1	-3.88e-6	12	NC	1	NC	3
464			min	0	3	-.004	3	-.157	4	-1.192e-3	4	NC	1	157.601	4
465		5	max	.002	1	.002	2	.007	1	-3.88e-6	12	NC	1	NC	3
466			min	0	3	-.004	3	-.141	4	-1.192e-3	4	NC	1	175.991	4
467		6	max	.002	1	.002	2	.006	1	-3.88e-6	12	NC	1	NC	2
468			min	0	3	-.003	3	-.125	4	-1.192e-3	4	NC	1	198.607	4
469		7	max	.002	1	.002	2	.005	1	-3.88e-6	12	NC	1	NC	2
470			min	0	3	-.003	3	-.109	4	-1.192e-3	4	NC	1	226.85	4
471		8	max	.002	1	.002	2	.005	1	-3.88e-6	12	NC	1	NC	2
472			min	0	3	-.003	3	-.094	4	-1.192e-3	4	NC	1	262.76	4
473		9	max	.002	1	.002	2	.004	1	-3.88e-6	12	NC	1	NC	2
474			min	0	3	-.003	3	-.08	4	-1.192e-3	4	NC	1	309.41	4
475		10	max	.001	1	.001	2	.003	1	-3.88e-6	12	NC	1	NC	2
476			min	0	3	-.002	3	-.067	4	-1.192e-3	4	NC	1	371.607	4
477		11	max	.001	1	.001	2	.003	1	-3.88e-6	12	NC	1	NC	2
478			min	0	3	-.002	3	-.054	4	-1.192e-3	4	NC	1	457.212	4
479		12	max	.001	1	.001	2	.002	1	-3.88e-6	12	NC	1	NC	1
480			min	0	3	-.002	3	-.043	4	-1.192e-3	4	NC	1	579.829	4
481		13	max	0	1	0	2	.002	1	-3.88e-6	12	NC	1	NC	1
482			min	0	3	-.002	3	-.032	4	-1.192e-3	4	NC	1	764.711	4
483		14	max	0	1	0	2	.001	1	-3.88e-6	12	NC	1	NC	1
484			min	0	3	-.001	3	-.023	4	-1.192e-3	4	NC	1	1063.247	4
485		15	max	0	1	0	2	0	1	-3.88e-6	12	NC	1	NC	1
486			min	0	3	-.001	3	-.016	4	-1.192e-3	4	NC	1	1593.932	4
487		16	max	0	1	0	2	0	1	-3.88e-6	12	NC	1	NC	1
488			min	0	3	0	3	-.009	4	-1.192e-3	4	NC	1	2684.448	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	-3.88e-6	12	NC	1	NC	1
490			min	0	3	0	3	-.004	4	-1.192e-3	4	NC	1	5550.37	4
491		18	max	0	1	0	2	0	1	-3.88e-6	12	NC	1	NC	1
492			min	0	3	0	3	-.001	4	-1.192e-3	4	NC	1	NC	1
493		19	max	0	1	0	1	0	1	-3.88e-6	12	NC	1	NC	1
494			min	0	1	0	1	0	1	-1.192e-3	4	NC	1	NC	1
495	M1	1	max	.006	3	.188	1	.753	4	1.282e-2	1	NC	1	NC	1
496			min	-.003	2	-.027	3	0	12	-1.514e-2	3	NC	1	NC	1
497		2	max	.006	3	.094	1	.73	4	9.984e-3	4	NC	5	NC	1
498			min	-.003	2	-.013	3	-.008	1	-7.515e-3	3	1424.301	1	NC	1
499		3	max	.006	3	.008	3	.706	4	1.716e-2	4	NC	5	NC	1
500			min	-.003	2	-.008	1	-.011	1	-2.377e-4	1	683.942	1	5900.697	5
501		4	max	.006	3	.044	3	.682	4	1.497e-2	4	NC	15	NC	1
502			min	-.003	2	-.124	1	-.01	1	-3.15e-3	3	430.027	1	4160.341	5
503		5	max	.006	3	.09	3	.658	4	1.277e-2	4	9462.784	15	NC	1
504			min	-.003	2	-.246	1	-.007	1	-6.22e-3	3	309.127	1	3273.695	5
505		6	max	.006	3	.14	3	.633	4	1.469e-2	1	7477.811	15	NC	1
506			min	-.003	2	-.365	1	-.003	1	-9.291e-3	3	242.685	1	2738.448	5
507		7	max	.005	3	.189	3	.607	4	1.966e-2	1	6305.982	15	NC	1
508			min	-.002	2	-.472	1	0	3	-1.236e-2	3	203.561	1	2374.858	4
509		8	max	.005	3	.229	3	.58	4	2.463e-2	1	5612.654	15	NC	1
510			min	-.002	2	-.557	1	0	12	-1.543e-2	3	180.462	1	2111.466	4
511		9	max	.005	3	.255	3	.552	4	2.699e-2	1	5250.042	15	NC	1
512			min	-.002	2	-.61	1	0	1	-1.566e-2	3	168.434	1	1946.377	4
513		10	max	.005	3	.265	3	.52	4	2.76e-2	1	5139.268	15	NC	1
514			min	-.002	2	-.628	1	0	12	-1.399e-2	3	164.819	1	1898.837	4
515		11	max	.005	3	.259	3	.485	4	2.82e-2	1	5249.866	15	NC	1
516			min	-.002	2	-.61	1	0	12	-1.233e-2	3	168.621	1	1943.624	4
517		12	max	.005	3	.237	3	.446	4	2.649e-2	1	5612.234	15	NC	1
518			min	-.002	2	-.555	1	-.001	1	-1.049e-2	3	181.034	1	2090.265	4
519		13	max	.005	3	.202	3	.402	4	2.133e-2	1	6305.155	15	NC	1
520			min	-.002	2	-.469	1	0	1	-8.388e-3	3	204.954	1	2492.493	4
521		14	max	.005	3	.157	3	.354	4	1.616e-2	1	7476.285	15	NC	1
522			min	-.002	2	-.361	1	0	12	-6.291e-3	3	245.656	1	3382.722	4
523		15	max	.004	3	.106	3	.305	4	1.099e-2	1	9459.971	15	NC	1
524			min	-.002	2	-.241	1	0	12	-4.193e-3	3	315.202	1	5514.179	4
525		16	max	.004	3	.053	3	.257	4	1.028e-2	4	NC	15	NC	1
526			min	-.002	2	-.119	1	0	12	-2.096e-3	3	442.691	1	NC	1
527		17	max	.004	3	.003	3	.214	4	1.141e-2	4	NC	5	NC	1
528			min	-.002	2	-.004	2	0	12	1.212e-6	3	712.161	1	NC	1
529		18	max	.004	3	.094	1	.177	4	7.669e-3	1	NC	5	NC	1
530			min	-.002	2	-.043	3	0	12	-2.161e-3	3	1495.505	1	NC	1
531		19	max	.004	3	.183	1	.146	4	1.49e-2	1	NC	1	NC	1
532			min	-.002	2	-.086	3	0	1	-4.4e-3	3	NC	1	NC	1
533	M5	1	max	.018	3	.37	1	.753	4	0	1	NC	1	NC	1
534			min	-.012	2	-.016	3	0	1	-7.346e-6	4	NC	1	NC	1
535		2	max	.018	3	.186	1	.736	4	8.784e-3	4	NC	5	NC	1
536			min	-.012	2	-.009	3	0	1	0	1	729.796	1	8247.463	4
537		3	max	.018	3	.025	3	.714	4	1.736e-2	4	NC	15	NC	1
538			min	-.012	2	-.027	1	0	1	0	1	338.469	1	4778.647	4
539		4	max	.018	3	.107	3	.689	4	1.415e-2	4	6941.957	15	NC	1
540			min	-.012	2	-.291	1	0	1	0	1	203.581	1	3618.179	4
541		5	max	.017	3	.224	3	.662	4	1.093e-2	4	4836.26	15	NC	1
542			min	-.012	2	-.582	1	0	1	0	1	141.206	1	3035.671	4
543		6	max	.017	3	.358	3	.635	4	7.717e-3	4	3710.785	15	NC	1
544			min	-.012	2	-.875	1	0	1	0	1	107.966	1	2669.464	4
545		7	max	.017	3	.49	3	.607	4	4.502e-3	4	3062.968	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.011	2	-1.143	1	0	1	0	1	88.875	1	2390.187	4
547		8	max	.016	3	.601	3	.58	4	1.287e-3	4	2687.358	15	NC	1
548			min	-.011	2	-1.358	1	0	1	0	1	77.824	1	2139.678	4
549		9	max	.016	3	.673	3	.552	4	2.001e-7	14	2494.905	15	NC	1
550			min	-.011	2	-1.493	1	0	1	-3.785e-6	5	72.173	1	1942.413	4
551		10	max	.015	3	.7	3	.52	4	3.094e-7	14	2436.889	15	NC	1
552			min	-.011	2	-1.539	1	0	1	-3.588e-6	5	70.489	1	1915.726	4
553		11	max	.015	3	.683	3	.484	4	4.186e-7	14	2494.988	15	NC	1
554			min	-.01	2	-1.493	1	0	1	-3.391e-6	5	72.265	1	1970.701	4
555		12	max	.015	3	.623	3	.447	4	8.125e-4	4	2687.556	15	NC	1
556			min	-.01	2	-1.354	1	0	1	0	1	78.131	1	2052.029	4
557		13	max	.014	3	.527	3	.404	4	2.842e-3	4	3063.374	15	NC	1
558			min	-.01	2	-1.134	1	0	1	0	1	89.68	1	2430.491	4
559		14	max	.014	3	.406	3	.354	4	4.872e-3	4	3711.582	15	NC	1
560			min	-.01	2	-.861	1	0	1	0	1	109.797	1	3445.376	4
561		15	max	.014	3	.271	3	.302	4	6.902e-3	4	4837.84	15	NC	1
562			min	-.01	2	-.564	1	0	1	0	1	145.23	1	6508.72	5
563		16	max	.013	3	.134	3	.251	4	8.932e-3	4	6945.281	15	NC	1
564			min	-.01	2	-.272	1	0	1	0	1	212.73	1	NC	1
565		17	max	.013	3	.008	3	.207	4	1.096e-2	4	NC	15	NC	1
566			min	-.009	2	-.014	1	0	1	0	1	361.061	1	NC	1
567		18	max	.013	3	.187	1	.172	4	5.546e-3	4	NC	5	NC	1
568			min	-.009	2	-.099	3	0	1	0	1	791.319	1	NC	1
569		19	max	.013	3	.356	1	.146	4	0	1	NC	1	NC	1
570			min	-.009	2	-.194	3	0	1	-3.541e-6	4	NC	1	NC	1
571	M9	1	max	.006	3	.188	1	.753	4	1.514e-2	3	NC	1	NC	1
572			min	-.003	2	-.027	3	0	1	-1.282e-2	1	NC	1	NC	1
573		2	max	.006	3	.094	1	.734	4	8.269e-3	5	NC	5	NC	1
574			min	-.003	2	-.013	3	0	12	-6.189e-3	1	1424.301	1	8891.191	4
575		3	max	.006	3	.008	3	.712	4	1.73e-2	4	NC	5	NC	1
576			min	-.003	2	-.008	1	0	12	-3.807e-6	10	683.942	1	5054.61	4
577		4	max	.006	3	.044	3	.687	4	1.355e-2	5	NC	15	NC	1
578			min	-.003	2	-.124	1	0	12	-4.737e-3	1	430.027	1	3746.525	4
579		5	max	.006	3	.09	3	.661	4	1.022e-2	5	9428.127	15	NC	1
580			min	-.003	2	-.246	1	0	12	-9.711e-3	1	309.127	1	3081.934	4
581		6	max	.006	3	.14	3	.634	4	9.291e-3	3	7451.526	15	NC	1
582			min	-.003	2	-.365	1	0	12	-1.469e-2	1	242.685	1	2669.219	4
583		7	max	.005	3	.189	3	.607	4	1.236e-2	3	6284.495	15	NC	1
584			min	-.002	2	-.472	1	0	1	-1.966e-2	1	203.561	1	2371.142	4
585		8	max	.005	3	.229	3	.58	4	1.543e-2	3	5593.94	15	NC	1
586			min	-.002	2	-.557	1	0	1	-2.463e-2	1	180.462	1	2126.372	4
587		9	max	.005	3	.255	3	.552	4	1.566e-2	3	5232.742	15	NC	1
588			min	-.002	2	-.61	1	0	12	-2.699e-2	1	168.434	1	1940.714	4
589		10	max	.005	3	.265	3	.52	4	1.399e-2	3	5122.378	15	NC	1
590			min	-.002	2	-.628	1	0	1	-2.76e-2	1	164.819	1	1899.746	4
591		11	max	.005	3	.259	3	.484	4	1.233e-2	3	5232.557	15	NC	1
592			min	-.002	2	-.61	1	0	1	-2.82e-2	1	168.621	1	1950.667	4
593		12	max	.005	3	.237	3	.447	4	1.049e-2	3	5593.599	15	NC	1
594			min	-.002	2	-.555	1	0	12	-2.649e-2	1	181.034	1	2075.501	4
595		13	max	.005	3	.202	3	.402	4	8.388e-3	3	6283.994	15	NC	1
596			min	-.002	2	-.469	1	0	12	-2.133e-2	1	204.954	1	2491.766	4
597		14	max	.005	3	.157	3	.353	4	6.291e-3	3	7450.811	15	NC	1
598			min	-.002	2	-.361	1	-.003	1	-1.616e-2	1	245.656	1	3463.184	5
599		15	max	.004	3	.106	3	.302	4	6.513e-3	5	9427.08	15	NC	1
600			min	-.002	2	-.241	1	-.006	1	-1.099e-2	1	315.202	1	5998.588	5
601		16	max	.004	3	.053	3	.253	4	8.757e-3	5	NC	15	NC	1
602			min	-.002	2	-.119	1	-.009	1	-5.826e-3	1	442.691	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.004	3	.003	3	.209	4	1.108e-2	4	NC	5	NC	1
604			min	-.002	2	-.004	2	-.01	1	-6.589e-4	1	712.161	1	NC	1
605		18	max	.004	3	.094	1	.173	4	5.296e-3	5	NC	5	NC	1
606			min	-.002	2	-.043	3	-.007	1	-7.669e-3	1	1495.505	1	NC	1
607		19	max	.004	3	.183	1	.146	4	4.4e-3	3	NC	1	NC	1
608			min	-.002	2	-.086	3	0	12	-1.49e-2	1	NC	1	NC	1

Anchor Designer™
Software
Version 2.4.6025.0

Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	1/5
Project:	Standard PVMax - Worst Case, 14-40 Inch Width		
Address:			
Phone:			
E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

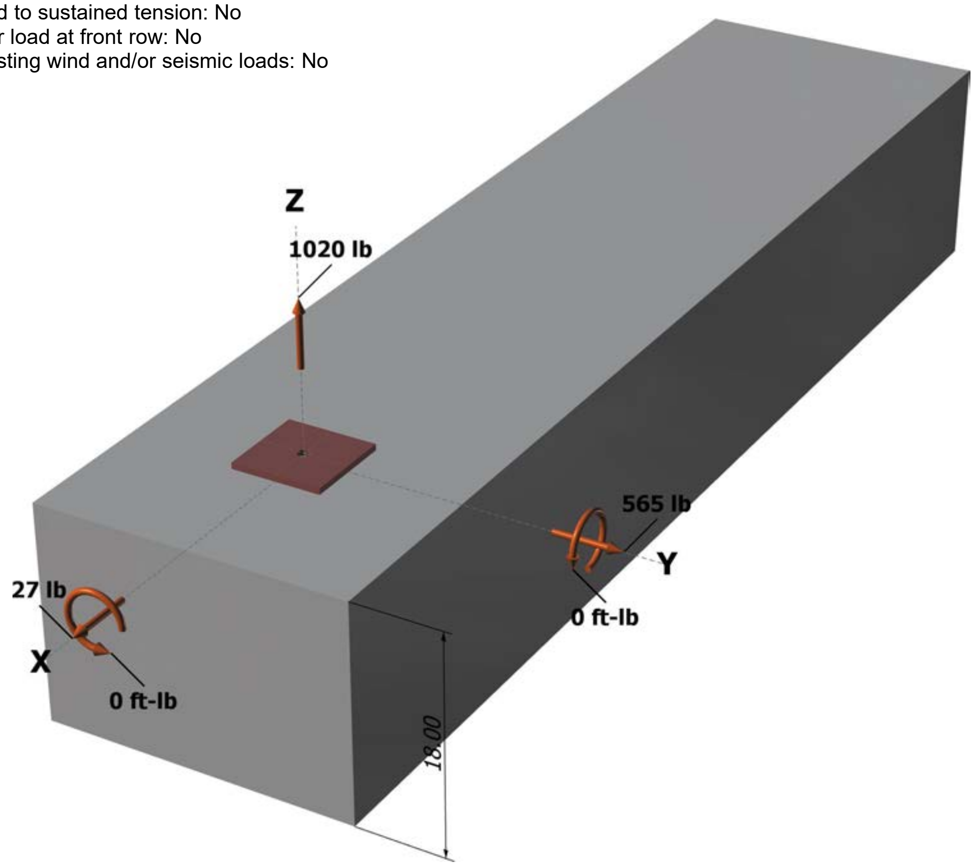
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



SIMPSON Strong-Tie

Anchor Designer™
Software
Version 2.4.6025.0

Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	2/5
Project:	Standard PVMax - Worst Case, 14-40 Inch Width		
Address:			
Phone:			
E-mail:			

<Figure 2>

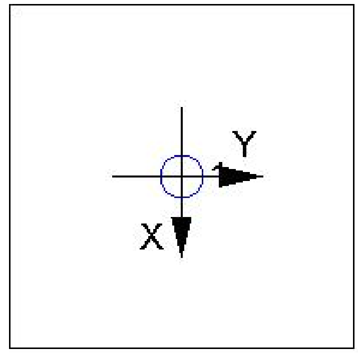
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1020.0	27.0	565.0	565.6
Sum	1020.0	27.0	565.0	565.6

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1020
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\Psi_{p,Na}N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\ (A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\ (A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\ (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\ (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\ \min|k_{cp}N_a\ ;\ k_{cp}N_{cb}| = \phi\ \min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, øN_n (lb)	Ratio	Status
Steel	1020	6071	0.17	Pass
Concrete breakout	1020	5710	0.18	Pass
Adhesive	**1020**	**5365**	**0.19**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, øV_n (lb)	Ratio	Status
Steel	**566**	**3156**	**0.18**	**Pass (Governs)**
T Concrete breakout y+	565	3934	0.14	Pass
T Concrete breakout x+	27	3018	0.01	Pass
|| Concrete breakout y+	27	8508	0.00	Pass
|| Concrete breakout x+	565	6875	0.08	Pass
Concrete breakout, combined	-	-	0.14	Pass
Pryout	566	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.19	0.00	19.0 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	1/5
Project:	Standard PVMax - Worst Case, 21-31 Inch Width		
Address:			
Phone:			
E-mail:			

SIMPSON Strong-Tie®

Anchor Designer™
Software
Version 2.4.6025.0

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

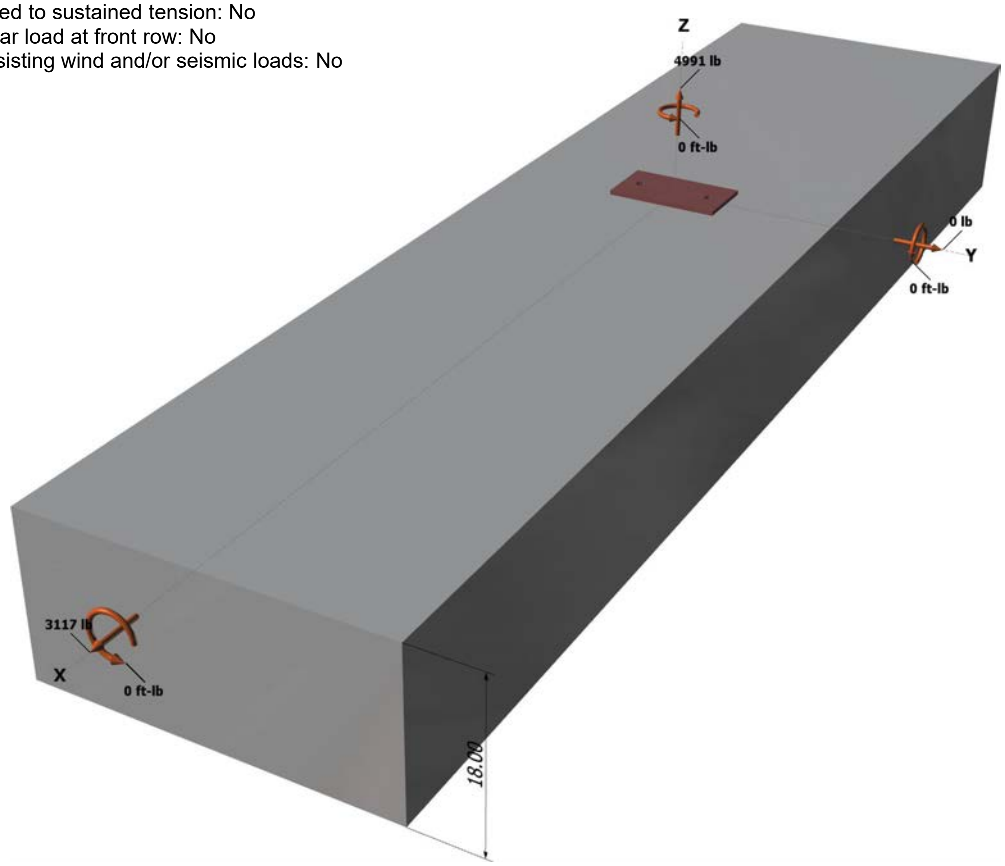
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

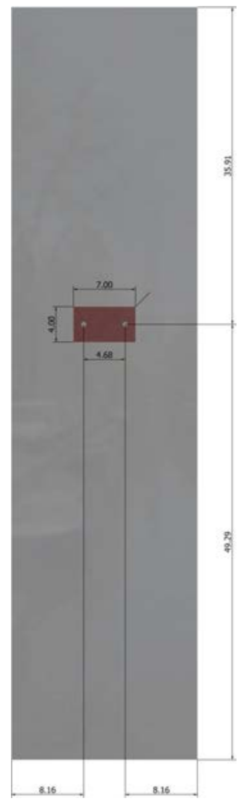
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



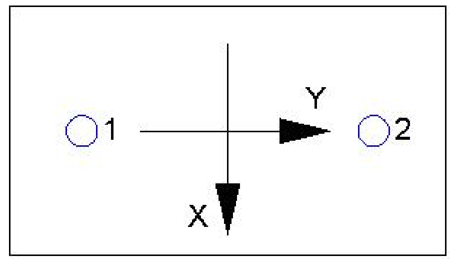
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2495.5	1558.5	0.0	1558.5
2	2495.5	1558.5	0.0	1558.5
Sum	4991.0	3117.0	0.0	3117.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 4991
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi\, (A_{Nc} / A_{Nco})\, \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
378.00	324.00	1.000	0.972	1.00	1.000	12492	0.65	9208

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\, (A_{Na} / A_{Na0})\, \Psi_{ed,Na} \Psi_{g,Na} \Psi_{ec,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\ (A_{Vc} / A_{Vco})\ \Psi_{ec,V}\ \Psi_{ed,V}\ \Psi_{c,V}\ \Psi_{h,V} V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
378.00	648.00	1.000	0.836	1.000	1.000	15593	0.70	5323

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.16	8744

$\phi V_{cbx} = \phi\ (2)(A_{Vc} / A_{Vco})\ \Psi_{ed,V}\ \Psi_{c,V}\ \Psi_{h,V} V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
299.64	299.64	1.000	1.000	1.000	8744	0.70	12241

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\ \min|k_{cp}N_{ag}\ ;\ k_{cp}N_{cbg}| = \phi\ \min|k_{cp}(A_{Na} / A_{Na0})\ \Psi_{ed,Na}\ \Psi_{g,Na}\ \Psi_{ec,Na}\ \Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\ \Psi_{ec,N}\ \Psi_{ed,N}\ \Psi_{c,N}\ \Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
378.00	324.00	1.000	0.972	1.000	1.000	12492	14166	0.70

ϕV_{cpg} (lb)
19833

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	2496	6071	0.41	Pass
Concrete breakout	4991	9208	0.54	Pass
Adhesive	**4991**	**8093**	**0.62**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	1559	3156	0.49	Pass
T Concrete breakout x+	**3117**	**5323**	**0.59**	**Pass (Governs)**

|| Concrete breakout y-	**1559**	**12241**	**0.13**	**Pass (Governs)**
Pryout	3117	19833	0.16	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.3	0.62	0.59	120.2 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.