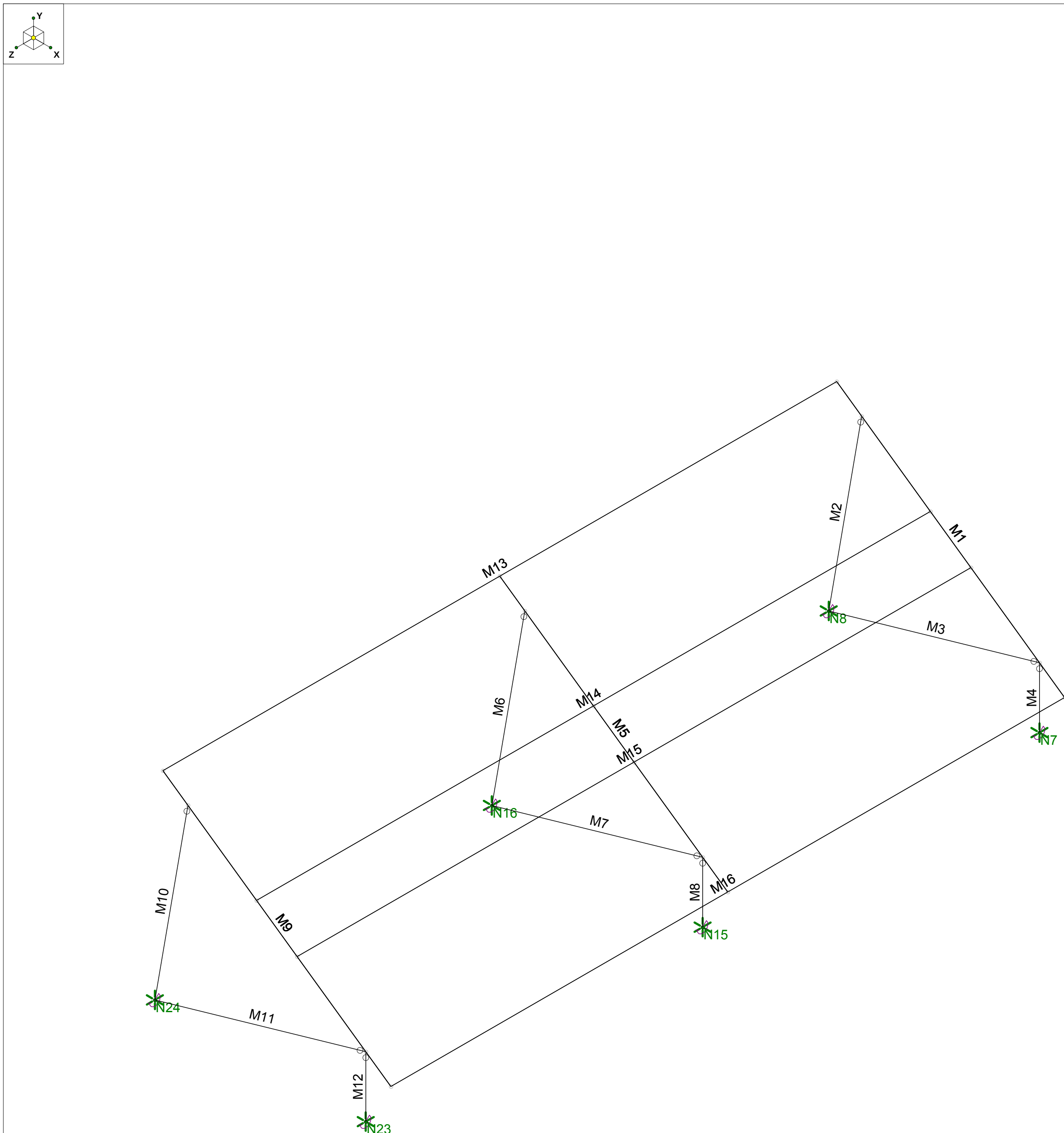


Schletter, Inc.	Standard PVMax Racking System Representative Calculations - ASCE 7-10	35° Tilt w/ Seismic Design
HCV		

1. INTRODUCTION

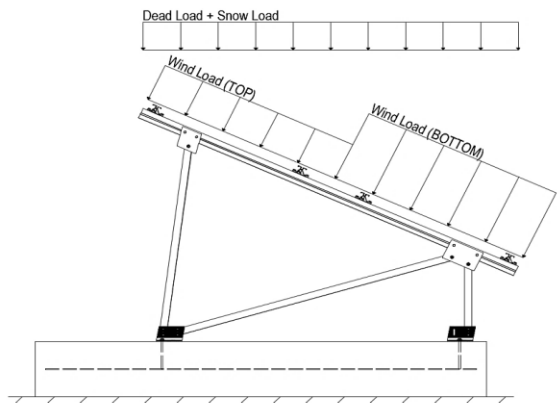
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 2
Module Tilt = 35°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 14.43 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.64
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 150 mph
Height < 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 35.33 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.200	*(Pressure)*
$Cf+_{BOTTOM}$	=	2.000	
$Cf-_{TOP, OUTER\ PURLIN}$	=	-2.700	
$Cf-_{TOP, INNER\ PURLIN}$	=	-2.100	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.200	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.06	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W ^{M}
1.54D + 1.3E + 0.2S ^{R}
0.56D + 1.3E ^{R}
1.54D + 1.25E + 0.2S ^{O}
0.56D + 1.25E ^{O}

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W ^{M}
1.238D + 0.875E ^{O}
1.1785D + 0.65625E + 0.75S ^{O}
0.362D + 0.875E ^{O}

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

^{M} *Uses the minimum allowable module dead load.*
^{R} *Include redundancy factor of 1.3.*
^{O} *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	**Diagonal Struts**	Location	**Front Reactions**	Location
M13	Top	M3	Outer	N7	Outer
M14	Mid-Top	M7	Inner	N15	Inner
M15	Mid-Bottom	M11	Outer	N23	Outer
M16	Bottom				

Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

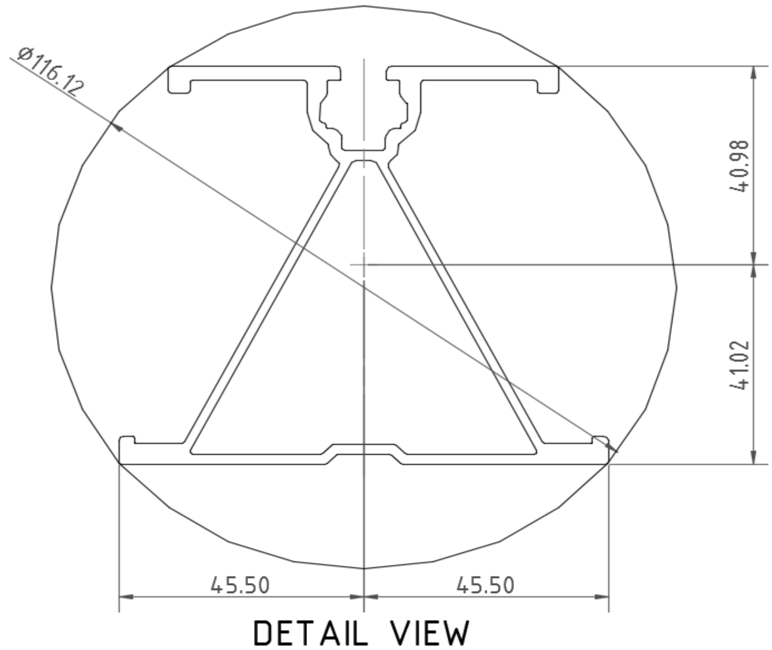
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

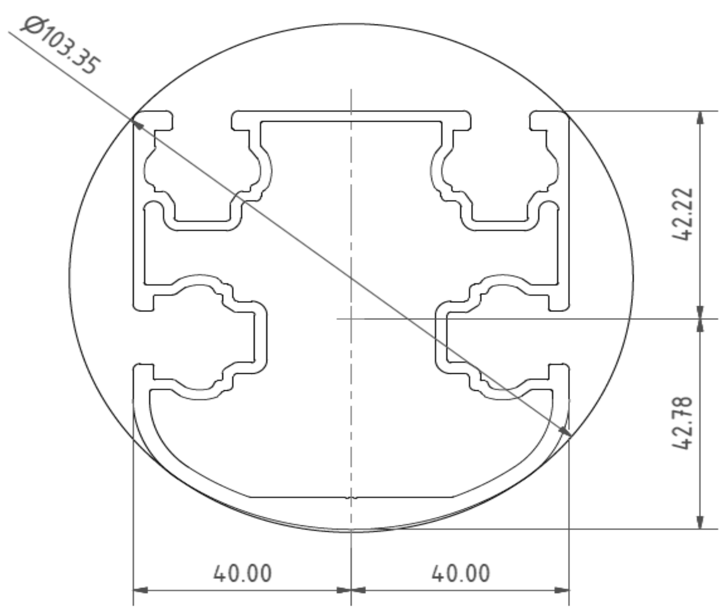
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	87	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	-1.698	k-ft
M_z =	0.002	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	61%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

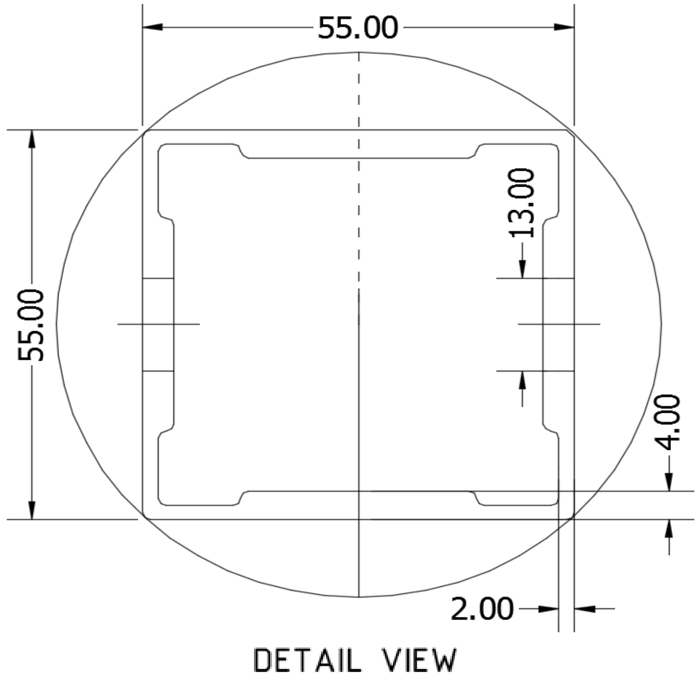
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	88.90	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.35	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-2.692	k-ft
M_z =	0.000	k-ft
P_n =	-0.981	k
$M_{y\ allowable}$ =	3.464	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	79%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

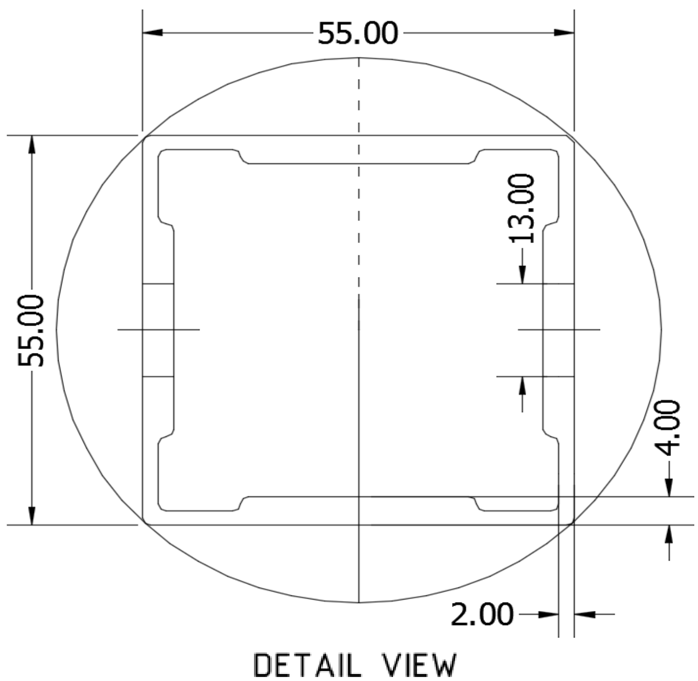
Strut Type =	55x55	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	24.80	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.415	k-ft
P_n =	0.331	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	31%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

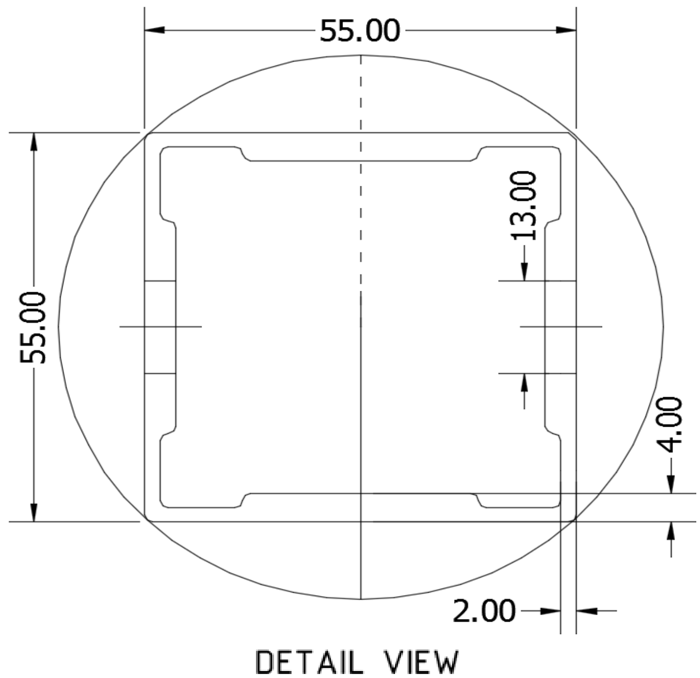
Strut Type =	55x55	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	86.60	in
$\Phi F_{ty\ AXIAL}$ =	7.50	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.009	k-ft
M_z =	0.000	k-ft
P_n =	2.852	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	7.371	k
Utilization =	39%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	78.03	in
$\Phi F_{ty\ AXIAL}$ =	8.94	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.009	k-ft
M_z =	0.000	k-ft
P_n =	2.960	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	8.786	k
Utilization =	34%	



5. FOUNDATION DESIGN CALCULATIONS

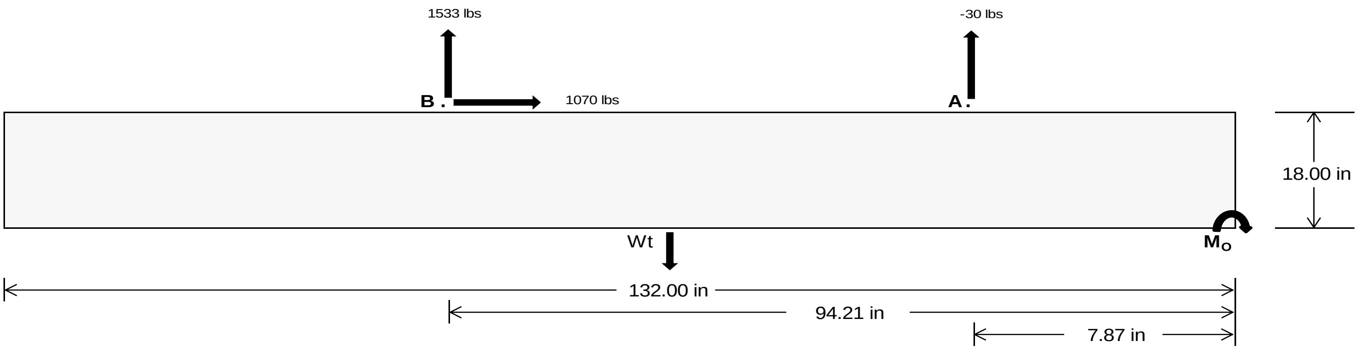
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	96.44	6653.07	k
Compressive Load =	2432.07	4820.18	k
Lateral Load =	298.11	4637.67	k
Moment (Weak Axis) =	0.55	0.15	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



<u>Concrete Properties</u>

Weight of Concrete = 145 pcf
Compressive Strength = 2500 psi
Yield Strength = 60000 psi

<u>Footing Reinforcement</u>

Use fiber reinforcing with (2) #5 rebar.

<u>Overturning Check</u>

M_O = 163405.0 in-lbs
Resisting Force Required = 2475.83 lbs
S.F. = 1.67
Weight Required = 4126.39 lbs
Minimum Width = <u>32 in</u> in
Weight Provided = 6380.00 lbs

A minimum 132in long x 32in wide x 18in tall ballast foundation is required to resist overturning.

<u>Sliding</u>

Force = 1070.08 lbs
Friction = 0.4
Weight Required = 2675.21 lbs
Resisting Weight = 6380.00 lbs
Additional Weight Required = 0 lbs

Use a 132in long x 32in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

<u>Cohesion</u>

Sliding Force = 1070.08 lbs
Cohesion = 130 psf
Area = 29.33 ft^2
Resisting = 3190.00 lbs
Additional Weight Required = 0 lbs

Use a 132in long x 32in wide x 18in tall ballast foundation. Cohesion is OK.

<u>Shear Key</u>

Additional Force = 0 lbs
Lateral Bearing Pressure = 200 psf/ft
Required Depth = 0.00 ft
f'_c = 2500 psi
Length = 8 in

Shear key is not required.

<u>Bearing Pressure</u>

	Ballast Width			
	<u>32 in</u>	<u>33 in</u>	<u>34 in</u>	<u>35 in</u>
P_{ftg} = (145 pcf)(11 ft)(1.5 ft)(2.67 ft) =	<u>6380 lbs</u>	<u>6579 lbs</u>	<u>6779 lbs</u>	<u>6978 lbs</u>

ASD LC	1.0D + 1.0S				1.0D + 0.6W			
Width	32 in	33 in	34 in	35 in	32 in	33 in	34 in	35 in
F_A	786 lbs	786 lbs	786 lbs	786 lbs	1002 lbs	1002 lbs	1002 lbs	1002 lbs
F_B	692 lbs	692 lbs	692 lbs	692 lbs	2117 lbs	2117 lbs	2117 lbs	2117 lbs
F_V	112 lbs	112 lbs	112 lbs	112 lbs	1935 lbs	1935 lbs	1935 lbs	1935 lbs
P_{total}	7859 lbs	8058 lbs	8257 lbs	8457 lbs	9499 lbs	9698 lbs	9898 lbs	10097 lbs
M	2347 lbs-ft	2347 lbs-ft	2347 lbs-ft	2347 lbs-ft	2776 lbs-ft	2776 lbs-ft	2776 lbs-ft	2776 lbs-ft
e	0.30 ft	0.29 ft	0.28 ft	0.28 ft	0.29 ft	0.29 ft	0.28 ft	0.27 ft
L/6	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft
f_{min}	224.3 psf	224.1 psf	223.9 psf	223.7 psf	272.2 psf	270.6 psf	269.0 psf	267.5 psf
f_{max}	311.5 psf	308.7 psf	306.0 psf	303.5 psf	375.4 psf	370.7 psf	366.2 psf	361.9 psf

ASD LC	1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	32 in	33 in	34 in	35 in	32 in	33 in	34 in	35 in
F_A	1242 lbs	1242 lbs	1242 lbs	1242 lbs	61 lbs	61 lbs	61 lbs	61 lbs
F_B	2020 lbs	2020 lbs	2020 lbs	2020 lbs	-3065 lbs	-3065 lbs	-3065 lbs	-3065 lbs
F_V	1522 lbs	1522 lbs	1522 lbs	1522 lbs	-2140 lbs	-2140 lbs	-2140 lbs	-2140 lbs
P_{total}	9642 lbs	9841 lbs	10041 lbs	10240 lbs	824 lbs	943 lbs	1063 lbs	1182 lbs
M	3549 lbs-ft	3549 lbs-ft	3549 lbs-ft	3549 lbs-ft	4289 lbs-ft	4289 lbs-ft	4289 lbs-ft	4289 lbs-ft
e	0.37 ft	0.36 ft	0.35 ft	0.35 ft	5.21 ft	4.55 ft	4.04 ft	3.63 ft
L/6	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft
f_{min}	262.7 psf	261.3 psf	260.0 psf	258.8 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	394.7 psf	389.3 psf	384.3 psf	379.5 psf	705.5 psf	240.1 psf	170.8 psf	144.3 psf

Maximum Bearing Pressure = 706 psf
Allowable Bearing Pressure = 1500 psf

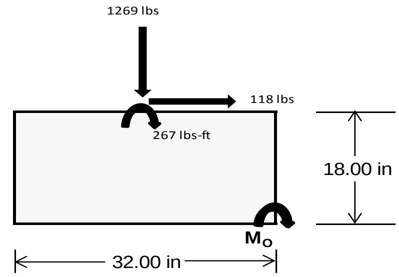
Use a 132in long x 32in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 1246.8 ft-lbs
Resisting Force Required = 935.11 lbs
S.F. = 1.67
Weight Required = 1558.52 lbs
Minimum Width = 32 in in
Weight Provided = 6380.00 lbs

A minimum 132in long x 32in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	32 in			32 in			32 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	262 lbs	461 lbs	139 lbs	540 lbs	1269 lbs	446 lbs	120 lbs	135 lbs	-3 lbs
F_V	163 lbs	159 lbs	165 lbs	120 lbs	118 lbs	127 lbs	163 lbs	160 lbs	164 lbs
P_{total}	8161 lbs	8359 lbs	8037 lbs	8059 lbs	8787 lbs	7965 lbs	2430 lbs	2444 lbs	2307 lbs
M	599 lbs-ft	591 lbs-ft	608 lbs-ft	445 lbs-ft	445 lbs-ft	467 lbs-ft	600 lbs-ft	589 lbs-ft	603 lbs-ft
e	0.07 ft	0.07 ft	0.08 ft	0.06 ft	0.05 ft	0.06 ft	0.25 ft	0.24 ft	0.26 ft
L/6	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft
f_{min}	232.3 psf	239.6 psf	227.4 psf	240.6 psf	265.5 psf	235.7 psf	36.8 psf	38.2 psf	32.4 psf
f_{max}	324.1 psf	330.3 psf	320.6 psf	308.9 psf	333.7 psf	307.4 psf	128.8 psf	128.5 psf	124.9 psf

Maximum Bearing Pressure = 334 psf
Allowable Bearing Pressure = 1500 psf

Use a 132in long x 32in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 132in long x 32in wide x 18in tall ballast foundation and fiber reinforcing with (2) #5 rebar.

5.3 Foundation Anchors

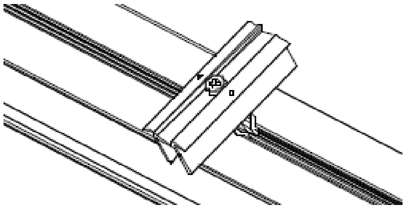
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

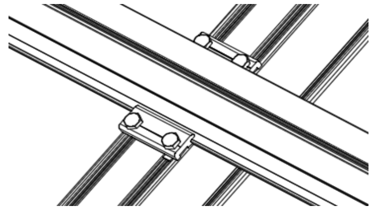
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.901	k
Allowable Uplift =	1.214	k
Utilization =	74%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	2.345	k
Allowable Uplift =	4.357	k
Utilization =	54%	



6.2 Strut Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	1.871	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	25%	

Rear Strut		
Maximum Axial Load =	4.394	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	59%	

Diagonal Strut		
Maximum Axial Load =	2.910	k
M12 Bolt Shear Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	39%	

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

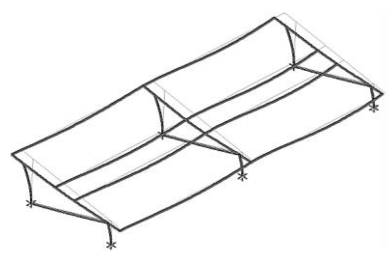
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	53.78	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	1.076	in
Max Drift, Δ_{MAX} =	0.448	in

$0.448 \leq 1.076$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 87 in

J = 0.432

240.683

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.3 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 87

J = 0.432

153.06

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:
3.4.14

L_b = 88.9 in
J = 1.08
152.913

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.4 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

Weak Axis:
3.4.14

L_b = 88.9
J = 1.08
161.829

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.2

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1	Used	3.4.16.1
Rb/t =	18.1	N/A for Weak Direction

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 31.1 ksi

3.4.18		3.4.18	
h/t =	7.4	h/t =	16.2
$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$		$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$	
S1 =	35.2	S1 =	36.9
m =	0.68	m =	0.65
C_0 =	41.067	C_0 =	40
Cc =	43.717	Cc =	40
$S2 = \frac{k_1 Bbr}{mDbr}$		$S2 = \frac{k_1 Bbr}{mDbr}$	
S2 =	73.8	S2 =	77.3
φF_L=	1.3φyFcy	φF_L=	1.3φyFcy
φF_L=	43.2 ksi	φF_L=	43.2 ksi
φF_LSt=	29.4 ksi	φF_LWk=	33.3 ksi
Ix =	984962 mm^4	Iy =	923544 mm^4
	2.366 in^4		2.219 in^4
y =	43.717 mm	x =	40 mm
Sx =	1.375 in^3	Sy =	1.409 in^3
M_{max}St =	3.363 k-ft	M_{max}Wk =	3.904 k-ft

Compression

3.4.9

b/t = 16.2
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

b/t = 7.4
S1 = 12.21
S2 = 32.70
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φc[Bt-Dt*√(Rb/t)]
φF_L= 31.09 ksi

φF_L= 31.09 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.87952

$φF_L$= φcc(Bc-Dc*λ)

$φF_L$= 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$φF_L$= φc[Bp-1.6Dp*b/t]

$φF_L$= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

$φF_L$= φc[Bp-1.6Dp*b/t]

$φF_L$= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$φF_L$= φyFcy

$φF_L$= 33.25 ksi

$φF_L$= 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 86.60 in

J = 0.942

135.148

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

$φF_L$= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

$φF_L$= 29.6 ksi

Weak Axis:

3.4.14

L_b = 86.6

J = 0.942

135.148

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

$φF_L$= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

$φF_L$= 29.6

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 2.00335

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.86047

φF_L= (φccFcy)/(λ²)

φF_L= 7.50396 ksi

3.4.9

b/t = 24.5
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

b/t = 24.5
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 7.50 ksi
A = 663.99 mm^2
1.03 in^2
P_{max} = 7.72 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:
3.4.14

L_b = 78.03 in
J = 0.942
121.773

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.8 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

Weak Axis:
3.4.14

L_b = 78.03
J = 0.942
121.773

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.8

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.80509

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83271

φF_L= (φccFcy)/(λ²)

φF_L= 8.94465 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 8.94 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 9.21 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M14	Y	-8.366	-8.366	0	0
3	M15	Y	-8.366	-8.366	0	0
4	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M14	Y	-4.45	-4.45	0	0
3	M15	Y	-4.45	-4.45	0	0
4	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-32.97	-32.97	0	0
2	M14	Y	-32.97	-32.97	0	0
3	M15	Y	-32.97	-32.97	0	0
4	M16	Y	-32.97	-32.97	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-118.221	-118.221	0	0
2	M14	y	-118.221	-118.221	0	0
3	M15	y	-197.035	-197.035	0	0
4	M16	y	-197.035	-197.035	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	265.997	265.997	0	0
2	M14	y	206.886	206.886	0	0
3	M15	y	118.221	118.221	0	0
4	M16	y	118.221	118.221	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M14	Z	6.693	6.693	0	0
3	M15	Z	6.693	6.693	0	0
4	M16	Z	6.693	6.693	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	994.497	2	1196.031	2	.334	1	.001	1	0	1	0	1
2		min	-1166.084	3	-1624.947	3	-17.758	5	-.115	4	0	1	0	1
3	N7	max	.033	3	733.721	1	-.584	12	-.001	12	0	1	0	1
4		min	-.192	2	-74.181	5	-229.316	4	-.423	4	0	1	0	1
5	N15	max	.186	3	1870.826	2	0	2	0	2	0	1	0	1
6		min	-1.836	2	71.229	15	-219.478	4	-.409	4	0	1	0	1
7	N16	max	3257.103	2	3707.832	2	0	10	0	2	0	1	0	1
8		min	-3567.438	3	-5117.748	3	-17.988	5	-.116	4	0	1	0	1
9	N23	max	.033	3	733.721	1	6.049	1	.011	1	0	1	0	1
10		min	-.192	2	60.579	12	-224.011	5	-.415	4	0	1	0	1
11	N24	max	994.497	2	1196.031	2	-.039	12	0	12	0	1	0	1
12		min	-1166.084	3	-1624.947	3	-18.267	5	-.116	4	0	1	0	1
13	Totals:	max	5243.879	2	9280.551	2	0	2						
14		min	-5899.356	3	-8003.028	3	-724.016	4						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	56.659	4	375.655	2	-9.129	12	0	15	.141	4	0	4
2			min	5.946	12	-714.085	3	-126.575	1	-.013	2	.014	12	0	3
3		2	max	53.285	1	261.727	2	-7.479	12	0	15	.09	4	.49	3
4			min	5.946	12	-503.346	3	-96.729	1	-.013	2	.002	10	-.257	2
5		3	max	53.285	1	147.8	2	-5.828	12	0	15	.053	5	.811	3
6			min	5.946	12	-292.607	3	-66.882	1	-.013	2	-.029	1	-.422	2
7		4	max	53.285	1	33.873	2	-4.177	12	0	15	.029	5	.962	3
8			min	5.946	12	-81.868	3	-38.475	4	-.013	2	-.071	1	-.495	2
9		5	max	53.285	1	128.872	3	.278	10	0	15	.007	5	.943	3
10			min	5.946	12	-80.054	2	-28.405	4	-.013	2	-.089	1	-.476	2
11		6	max	53.285	1	339.611	3	22.657	1	0	15	-.006	12	.754	3
12			min	.767	15	-193.982	2	-23.472	5	-.013	2	-.083	1	-.366	2
13		7	max	53.285	1	550.35	3	52.504	1	0	15	-.006	12	.396	3
14			min	-6.95	5	-307.909	2	-20.918	5	-.013	2	-.052	1	-.164	2
15		8	max	53.285	1	761.09	3	82.35	1	0	15	.005	2	.13	2
16			min	-15.219	5	-421.836	2	-18.364	5	-.013	2	-.047	4	-.133	3
17		9	max	53.285	1	971.829	3	112.197	1	0	15	.08	1	.516	2
18			min	-23.488	5	-535.763	2	-15.811	5	-.013	2	-.06	5	-.831	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	54.858	4	1182.568	3	142.043	1	.002	14	.183	1	.993	2
20			min	5.946	12	-649.69	2	-92.203	14	-.013	2	.002	3	-1.698	3
21		11	max	53.285	1	535.763	2	-4.076	12	.013	2	.093	4	.516	2
22			min	5.946	12	-971.829	3	-112.197	1	0	15	-.004	3	-.831	3
23		12	max	53.285	1	421.836	2	-2.425	12	.013	2	.047	4	.13	2
24			min	5.946	12	-761.09	3	-82.35	1	0	15	-.008	3	-.133	3
25		13	max	53.285	1	307.909	2	-.775	12	.013	2	.022	5	.396	3
26			min	5.946	12	-550.35	3	-52.504	1	0	15	-.052	1	-.164	2
27		14	max	53.285	1	193.982	2	1.653	3	.013	2	0	15	.754	3
28			min	5.281	15	-339.611	3	-32.735	4	0	15	-.083	1	-.366	2
29		15	max	53.285	1	80.054	2	7.189	1	.013	2	-.005	12	.943	3
30			min	-.284	15	-128.872	3	-24.571	5	0	15	-.089	1	-.476	2
31		16	max	53.285	1	81.868	3	37.036	1	.013	2	-.002	12	.962	3
32			min	-8.536	5	-33.873	2	-22.017	5	0	15	-.071	1	-.495	2
33		17	max	53.285	1	292.607	3	66.882	1	.013	2	.004	3	.811	3
34			min	-16.805	5	-147.8	2	-19.463	5	0	15	-.065	4	-.422	2
35		18	max	53.285	1	503.346	3	96.729	1	.013	2	.037	1	.49	3
36			min	-25.074	5	-261.727	2	-16.909	5	0	15	-.072	5	-.257	2
37		19	max	53.285	1	714.085	3	126.575	1	.013	2	.127	1	0	2
38			min	-33.343	5	-375.655	2	-14.355	5	0	15	-.085	5	0	3
39	M14	1	max	34.78	4	431.637	2	-9.438	12	.011	3	.204	4	0	4
40			min	2.79	12	-589.765	3	-131.638	1	-.012	2	.016	12	0	3
41		2	max	30.35	1	317.71	2	-7.787	12	.011	3	.139	4	.409	3
42			min	2.79	12	-426.643	3	-101.791	1	-.012	2	.005	10	-.302	2
43		3	max	30.35	1	203.783	2	-6.136	12	.011	3	.083	5	.687	3
44			min	2.79	12	-263.521	3	-71.945	1	-.012	2	-.013	1	-.512	2
45		4	max	30.35	1	89.856	2	-4.486	12	.011	3	.046	5	.834	3
46			min	1.462	15	-100.399	3	-56.06	4	-.012	2	-.059	1	-.63	2
47		5	max	30.35	1	62.723	3	-.431	10	.011	3	.011	5	.849	3
48			min	-6.057	5	-24.072	2	-45.99	4	-.012	2	-.081	1	-.657	2
49		6	max	30.35	1	225.845	3	17.595	1	.011	3	-.005	12	.733	3
50			min	-14.326	5	-137.999	2	-39.604	5	-.012	2	-.079	1	-.591	2
51		7	max	30.35	1	388.967	3	47.441	1	.011	3	-.006	12	.485	3
52			min	-22.596	5	-251.926	2	-37.05	5	-.012	2	-.067	4	-.434	2
53		8	max	30.35	1	552.09	3	77.288	1	.011	3	.003	2	.106	3
54			min	-30.865	5	-365.853	2	-34.496	5	-.012	2	-.083	4	-.185	2
55		9	max	30.35	1	715.212	3	107.134	1	.011	3	.072	1	.155	2
56			min	-39.134	5	-479.781	2	-31.942	5	-.012	2	-.108	5	-.404	3
57		10	max	60.359	4	878.334	3	136.981	1	.011	3	.204	4	.588	2
58			min	2.79	12	-593.708	2	-97.388	14	-.012	2	.001	3	-1.046	3
59		11	max	52.09	4	479.781	2	-3.768	12	.012	2	.138	4	.155	2
60			min	2.79	12	-715.212	3	-107.134	1	-.011	3	-.004	3	-.404	3
61		12	max	43.821	4	365.853	2	-2.117	12	.012	2	.08	5	.106	3
62			min	2.79	12	-552.09	3	-77.288	1	-.011	3	-.008	3	-.185	2
63		13	max	35.552	4	251.926	2	-.357	3	.012	2	.043	5	.485	3
64			min	2.79	12	-388.967	3	-56.934	4	-.011	3	-.053	1	-.434	2
65		14	max	30.35	1	137.999	2	2.119	3	.012	2	.008	5	.733	3
66			min	2.79	12	-225.845	3	-46.864	4	-.011	3	-.079	1	-.591	2
67		15	max	30.35	1	24.072	2	12.252	1	.012	2	-.004	12	.849	3
68			min	2.79	12	-62.723	3	-39.826	5	-.011	3	-.081	1	-.657	2
69		16	max	30.35	1	100.399	3	42.098	1	.012	2	0	3	.834	3
70			min	1.843	15	-89.856	2	-37.272	5	-.011	3	-.071	4	-.63	2
71		17	max	30.35	1	263.521	3	71.945	1	.012	2	.006	3	.687	3
72			min	-5.467	5	-203.783	2	-34.718	5	-.011	3	-.088	4	-.512	2
73		18	max	30.35	1	426.643	3	101.791	1	.012	2	.057	1	.409	3
74			min	-13.736	5	-317.71	2	-32.164	5	-.011	3	-.112	5	-.302	2
75		19	max	30.35	1	589.765	3	131.638	1	.012	2	.151	1	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-22.005	5	-431.637	2	-29.61	5	-.011	3	-.137	5	0	3
77	M15	1	max	65.906	5	645.972	2	-9.265	12	.013	2	.252	4	0	2
78			min	-31.255	1	-349.024	3	-131.671	1	-.01	3	.015	12	0	3
79		2	max	57.637	5	468.556	2	-7.614	12	.013	2	.176	4	.244	3
80			min	-31.255	1	-257.326	3	-101.825	1	-.01	3	.005	10	-.449	2
81		3	max	49.368	5	291.14	2	-5.963	12	.013	2	.11	5	.415	3
82			min	-31.255	1	-165.629	3	-79.012	4	-.01	3	-.013	1	-.755	2
83		4	max	41.099	5	113.724	2	-4.313	12	.013	2	.063	5	.511	3
84			min	-31.255	1	-73.931	3	-68.942	4	-.01	3	-.059	1	-.918	2
85		5	max	32.83	5	17.766	3	-.518	10	.013	2	.017	5	.534	3
86			min	-31.255	1	-63.693	2	-58.872	4	-.01	3	-.081	1	-.938	2
87		6	max	24.56	5	109.464	3	17.561	1	.013	2	-.005	12	.482	3
88			min	-31.255	1	-241.109	2	-52.444	5	-.01	3	-.079	1	-.815	2
89		7	max	16.291	5	201.161	3	47.408	1	.013	2	-.005	12	.357	3
90			min	-31.255	1	-418.525	2	-49.891	5	-.01	3	-.081	4	-.55	2
91		8	max	8.022	5	292.859	3	77.254	1	.013	2	.003	2	.158	3
92			min	-31.255	1	-595.941	2	-47.337	5	-.01	3	-.109	4	-.141	2
93		9	max	-.061	15	384.557	3	107.101	1	.013	2	.072	1	.41	2
94			min	-31.255	1	-773.358	2	-44.783	5	-.01	3	-.143	5	-.114	3
95		10	max	-3.574	10	476.254	3	136.947	1	.013	2	.25	4	1.105	2
96			min	-31.255	1	-950.774	2	-103.941	14	-.01	3	.002	3	-.461	3
97		11	max	-3.574	10	773.358	2	-3.94	12	.01	3	.174	4	.41	2
98			min	-31.255	1	-384.557	3	-107.101	1	-.013	2	-.003	3	-.114	3
99		12	max	-3.574	10	595.941	2	-2.29	12	.01	3	.105	5	.158	3
100			min	-31.255	1	-292.859	3	-79.915	4	-.013	2	-.007	3	-.141	2
101		13	max	-3.574	10	418.525	2	-.639	12	.01	3	.058	5	.357	3
102			min	-31.255	1	-201.161	3	-69.845	4	-.013	2	-.053	1	-.55	2
103		14	max	-3.574	10	241.109	2	1.832	3	.01	3	.012	5	.482	3
104			min	-39.093	4	-109.464	3	-59.775	4	-.013	2	-.079	1	-.815	2
105		15	max	-3.574	10	63.693	2	12.285	1	.01	3	-.004	12	.534	3
106			min	-47.362	4	-17.766	3	-52.673	5	-.013	2	-.081	1	-.938	2
107		16	max	-3.574	10	73.931	3	42.132	1	.01	3	0	12	.511	3
108			min	-55.631	4	-113.724	2	-50.119	5	-.013	2	-.088	4	-.918	2
109		17	max	-3.574	10	165.629	3	71.978	1	.01	3	.005	3	.415	3
110			min	-63.901	4	-291.14	2	-47.565	5	-.013	2	-.115	4	-.755	2
111		18	max	-3.574	10	257.326	3	101.825	1	.01	3	.057	1	.244	3
112			min	-72.17	4	-468.556	2	-45.011	5	-.013	2	-.149	5	-.449	2
113		19	max	-3.574	10	349.024	3	131.671	1	.01	3	.151	1	0	2
114			min	-80.439	4	-645.972	2	-42.457	5	-.013	2	-.184	5	0	5
115	M16	1	max	63.809	5	592.722	2	-8.558	12	.007	2	.194	4	0	2
116			min	-58.095	1	-300.357	3	-126.984	1	-.012	3	.012	12	0	3
117		2	max	55.54	5	415.306	2	-6.907	12	.007	2	.131	4	.205	3
118			min	-58.095	1	-208.66	3	-97.137	1	-.012	3	.003	10	-.406	2
119		3	max	47.27	5	237.89	2	-5.257	12	.007	2	.083	5	.336	3
120			min	-58.095	1	-116.962	3	-67.291	1	-.012	3	-.028	1	-.669	2
121		4	max	39.001	5	60.474	2	-3.606	12	.007	2	.048	5	.393	3
122			min	-58.095	1	-25.265	3	-52.358	4	-.012	3	-.07	1	-.789	2
123		5	max	30.732	5	66.433	3	-.059	10	.007	2	.015	5	.377	3
124			min	-58.095	1	-116.943	2	-42.289	4	-.012	3	-.089	1	-.767	2
125		6	max	22.463	5	158.13	3	22.249	1	.007	2	-.005	12	.286	3
126			min	-58.095	1	-294.359	2	-37.218	5	-.012	3	-.083	1	-.601	2
127		7	max	14.194	5	249.828	3	52.095	1	.007	2	-.005	12	.122	3
128			min	-58.095	1	-471.775	2	-34.664	5	-.012	3	-.059	4	-.292	2
129		8	max	5.924	5	341.525	3	81.942	1	.007	2	.004	2	.159	2
130			min	-58.095	1	-649.192	2	-32.11	5	-.012	3	-.073	4	-.116	3
131		9	max	-1.456	15	433.223	3	111.788	1	.007	2	.079	1	.754	2
132			min	-58.095	1	-826.608	2	-29.556	5	-.012	3	-.097	5	-.428	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-5.662	12	524.92	3	141.635	1	.007	2	.196	4	1.491	2
134			min	-58.095	1	-1004.024	2	-99.144	14	-.012	3	.004	12	-.814	3
135		11	max	-5.232	15	826.608	2	-4.647	12	.012	3	.13	4	.754	2
136			min	-58.095	1	-433.223	3	-111.788	1	-.007	2	-.001	3	-.428	3
137		12	max	-5.662	12	649.192	2	-2.997	12	.012	3	.072	4	.159	2
138			min	-58.095	1	-341.525	3	-81.942	1	-.007	2	-.006	3	-.116	3
139		13	max	-5.662	12	471.775	2	-1.346	12	.012	3	.036	5	.122	3
140			min	-58.095	1	-249.828	3	-56.593	4	-.007	2	-.053	1	-.292	2
141		14	max	-5.662	12	294.359	2	.7	3	.012	3	.002	5	.286	3
142			min	-58.095	1	-158.13	3	-46.523	4	-.007	2	-.083	1	-.601	2
143		15	max	-5.662	12	116.943	2	7.598	1	.012	3	-.005	12	.377	3
144			min	-58.095	1	-66.433	3	-38.294	5	-.007	2	-.089	1	-.767	2
145		16	max	-5.662	12	25.265	3	37.444	1	.012	3	-.002	12	.393	3
146			min	-64.822	4	-60.474	2	-35.74	5	-.007	2	-.078	4	-.789	2
147		17	max	-5.662	12	116.962	3	67.291	1	.012	3	.002	3	.336	3
148			min	-73.092	4	-237.89	2	-33.187	5	-.007	2	-.095	4	-.669	2
149		18	max	-5.662	12	208.66	3	97.137	1	.012	3	.038	1	.205	3
150			min	-81.361	4	-415.306	2	-30.633	5	-.007	2	-.113	5	-.406	2
151		19	max	-5.662	12	300.357	3	126.984	1	.012	3	.128	1	0	2
152			min	-89.63	4	-592.722	2	-28.079	5	-.007	2	-.137	5	0	5
153	M2	1	max	958.183	2	2.044	4	.179	1	0	3	0	3	0	1
154			min	-1392.854	3	.491	15	-15.032	4	0	4	0	2	0	1
155		2	max	958.704	2	1.925	4	.179	1	0	3	0	1	0	15
156			min	-1392.464	3	.463	15	-15.49	4	0	4	-.005	4	0	4
157		3	max	959.224	2	1.806	4	.179	1	0	3	0	1	0	15
158			min	-1392.073	3	.435	15	-15.948	4	0	4	-.011	4	-.001	4
159		4	max	959.745	2	1.687	4	.179	1	0	3	0	1	0	15
160			min	-1391.683	3	.407	15	-16.407	4	0	4	-.017	4	-.002	4
161		5	max	960.266	2	1.568	4	.179	1	0	3	0	1	0	15
162			min	-1391.292	3	.379	15	-16.865	4	0	4	-.023	4	-.003	4
163		6	max	960.787	2	1.449	4	.179	1	0	3	0	1	0	15
164			min	-1390.902	3	.351	15	-17.324	4	0	4	-.029	4	-.003	4
165		7	max	961.307	2	1.331	4	.179	1	0	3	0	1	0	15
166			min	-1390.511	3	.323	15	-17.782	4	0	4	-.035	4	-.004	4
167		8	max	961.828	2	1.212	4	.179	1	0	3	0	1	0	15
168			min	-1390.121	3	.294	12	-18.24	4	0	4	-.042	4	-.004	4
169		9	max	962.349	2	1.093	4	.179	1	0	3	0	1	-.001	15
170			min	-1389.73	3	.248	12	-18.699	4	0	4	-.048	4	-.004	4
171		10	max	962.869	2	.974	4	.179	1	0	3	0	1	-.001	15
172			min	-1389.34	3	.202	12	-19.157	4	0	4	-.055	4	-.005	4
173		11	max	963.39	2	.855	4	.179	1	0	3	0	1	-.001	15
174			min	-1388.949	3	.156	12	-19.615	4	0	4	-.062	4	-.005	4
175		12	max	963.911	2	.76	2	.179	1	0	3	0	1	-.001	15
176			min	-1388.558	3	.109	12	-20.074	4	0	4	-.069	4	-.005	4
177		13	max	964.431	2	.668	2	.179	1	0	3	0	1	-.001	15
178			min	-1388.168	3	.063	12	-20.532	4	0	4	-.076	4	-.006	4
179		14	max	964.952	2	.575	2	.179	1	0	3	0	1	-.001	15
180			min	-1387.777	3	-.003	3	-20.99	4	0	4	-.083	4	-.006	4
181		15	max	965.473	2	.482	2	.179	1	0	3	0	1	-.001	12
182			min	-1387.387	3	-.073	3	-21.449	4	0	4	-.091	4	-.006	4
183		16	max	965.994	2	.39	2	.179	1	0	3	0	1	-.001	12
184			min	-1386.996	3	-.142	3	-21.907	4	0	4	-.099	4	-.006	4
185		17	max	966.514	2	.297	2	.179	1	0	3	.001	1	-.001	12
186			min	-1386.606	3	-.212	3	-22.365	4	0	4	-.107	4	-.006	4
187		18	max	967.035	2	.204	2	.179	1	0	3	.001	1	-.001	12
188			min	-1386.215	3	-.281	3	-22.824	4	0	4	-.115	4	-.006	4
189		19	max	967.556	2	.112	2	.179	1	0	3	.001	1	-.001	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-1385.825	3	-.351	3	-23.282	4	0	4	-.123	4	-.006	4
191	M3	1	max	860.209	2	7.684	4	5.135	4	0	3	0	1	.006	4
192			min	-958.858	3	1.815	15	.018	12	0	4	-.022	4	.001	12
193		2	max	860.039	2	6.923	4	5.67	4	0	3	0	1	.004	2
194			min	-958.985	3	1.636	15	.018	12	0	4	-.02	4	0	3
195		3	max	859.868	2	6.162	4	6.204	4	0	3	0	1	.001	2
196			min	-959.113	3	1.458	15	.018	12	0	4	-.018	4	-.001	3
197		4	max	859.698	2	5.401	4	6.739	4	0	3	0	1	0	15
198			min	-959.241	3	1.279	15	.018	12	0	4	-.015	5	-.003	3
199		5	max	859.528	2	4.64	4	7.274	4	0	3	0	1	0	15
200			min	-959.369	3	1.1	15	.018	12	0	4	-.012	5	-.004	6
201		6	max	859.357	2	3.879	4	7.808	4	0	3	0	1	-.001	15
202			min	-959.496	3	.921	15	.018	12	0	4	-.009	5	-.006	6
203		7	max	859.187	2	3.118	4	8.343	4	0	3	0	1	-.002	15
204			min	-959.624	3	.742	15	.018	12	0	4	-.006	5	-.007	6
205		8	max	859.017	2	2.357	4	8.878	4	0	3	0	1	-.002	15
206			min	-959.752	3	.563	15	.018	12	0	4	-.002	5	-.008	6
207		9	max	858.846	2	1.596	4	9.412	4	0	3	.002	4	-.002	15
208			min	-959.88	3	.384	15	.018	12	0	4	0	12	-.009	6
209		10	max	858.676	2	.835	4	9.947	4	0	3	.006	4	-.002	15
210			min	-960.007	3	.173	12	.018	12	0	4	0	12	-.01	6
211		11	max	858.506	2	.217	2	10.482	4	0	3	.01	4	-.002	15
212			min	-960.135	3	-.209	3	.018	12	0	4	0	12	-.01	6
213		12	max	858.335	2	-.152	15	11.017	4	0	3	.015	4	-.002	15
214			min	-960.263	3	-.688	6	.018	12	0	4	0	12	-.01	6
215		13	max	858.165	2	-.331	15	11.551	4	0	3	.019	4	-.002	15
216			min	-960.391	3	-1.449	6	.018	12	0	4	0	12	-.009	6
217		14	max	857.995	2	-.51	15	12.086	4	0	3	.024	4	-.002	15
218			min	-960.518	3	-2.21	6	.018	12	0	4	0	12	-.009	6
219		15	max	857.824	2	-.689	15	12.621	4	0	3	.029	4	-.002	15
220			min	-960.646	3	-2.971	6	.018	12	0	4	0	12	-.007	6
221		16	max	857.654	2	-.868	15	13.155	4	0	3	.035	4	-.001	15
222			min	-960.774	3	-3.732	6	.018	12	0	4	0	12	-.006	6
223		17	max	857.484	2	-1.047	15	13.69	4	0	3	.04	4	-.001	15
224			min	-960.902	3	-4.493	6	.018	12	0	4	0	12	-.004	6
225		18	max	857.313	2	-1.226	15	14.225	4	0	3	.046	4	0	15
226			min	-961.03	3	-5.254	6	.018	12	0	4	0	12	-.002	6
227		19	max	857.143	2	-1.404	15	14.759	4	0	3	.052	4	0	1
228			min	-961.157	3	-6.015	6	.018	12	0	4	0	12	0	1
229	M4	1	max	730.655	1	0	1	-.585	12	0	1	.049	4	0	1
230			min	-75.612	5	0	1	-227.082	4	0	1	0	12	0	1
231		2	max	730.825	1	0	1	-.585	12	0	1	.023	4	0	1
232			min	-75.532	5	0	1	-227.23	4	0	1	0	12	0	1
233		3	max	730.995	1	0	1	-.585	12	0	1	0	1	0	1
234			min	-75.453	5	0	1	-227.378	4	0	1	-.003	4	0	1
235		4	max	731.166	1	0	1	-.585	12	0	1	0	12	0	1
236			min	-75.373	5	0	1	-227.525	4	0	1	-.029	4	0	1
237		5	max	731.336	1	0	1	-.585	12	0	1	0	12	0	1
238			min	-75.294	5	0	1	-227.673	4	0	1	-.055	4	0	1
239		6	max	731.506	1	0	1	-.585	12	0	1	0	12	0	1
240			min	-75.214	5	0	1	-227.82	4	0	1	-.081	4	0	1
241		7	max	731.677	1	0	1	-.585	12	0	1	0	12	0	1
242			min	-75.135	5	0	1	-227.968	4	0	1	-.107	4	0	1
243		8	max	731.847	1	0	1	-.585	12	0	1	0	12	0	1
244			min	-75.055	5	0	1	-228.116	4	0	1	-.134	4	0	1
245		9	max	732.017	1	0	1	-.585	12	0	1	0	12	0	1
246			min	-74.976	5	0	1	-228.263	4	0	1	-.16	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	732.188	1	0	1	-.585	12	0	1	0	12	0	1
248			min	-74.896	5	0	1	-228.411	4	0	1	-.186	4	0	1
249		11	max	732.358	1	0	1	-.585	12	0	1	0	12	0	1
250			min	-74.817	5	0	1	-228.559	4	0	1	-.212	4	0	1
251		12	max	732.528	1	0	1	-.585	12	0	1	0	12	0	1
252			min	-74.737	5	0	1	-228.706	4	0	1	-.238	4	0	1
253		13	max	732.699	1	0	1	-.585	12	0	1	0	12	0	1
254			min	-74.658	5	0	1	-228.854	4	0	1	-.265	4	0	1
255		14	max	732.869	1	0	1	-.585	12	0	1	0	12	0	1
256			min	-74.578	5	0	1	-229.001	4	0	1	-.291	4	0	1
257		15	max	733.039	1	0	1	-.585	12	0	1	0	12	0	1
258			min	-74.499	5	0	1	-229.149	4	0	1	-.317	4	0	1
259		16	max	733.21	1	0	1	-.585	12	0	1	0	12	0	1
260			min	-74.419	5	0	1	-229.297	4	0	1	-.344	4	0	1
261		17	max	733.38	1	0	1	-.585	12	0	1	0	12	0	1
262			min	-74.34	5	0	1	-229.444	4	0	1	-.37	4	0	1
263		18	max	733.55	1	0	1	-.585	12	0	1	0	12	0	1
264			min	-74.26	5	0	1	-229.592	4	0	1	-.396	4	0	1
265		19	max	733.721	1	0	1	-.585	12	0	1	-.001	12	0	1
266			min	-74.181	5	0	1	-229.74	4	0	1	-.423	4	0	1
267	M6	1	max	2950.168	2	2.238	2	0	1	0	1	0	4	0	1
268			min	-4394.305	3	.268	12	-15.19	4	0	4	0	1	0	1
269		2	max	2950.689	2	2.145	2	0	1	0	1	0	1	0	12
270			min	-4393.915	3	.221	12	-15.649	4	0	4	-.005	4	0	2
271		3	max	2951.21	2	2.053	2	0	1	0	1	0	1	0	12
272			min	-4393.524	3	.175	12	-16.107	4	0	4	-.011	4	-.002	2
273		4	max	2951.73	2	1.96	2	0	1	0	1	0	1	0	12
274			min	-4393.133	3	.106	3	-16.565	4	0	4	-.017	4	-.002	2
275		5	max	2952.251	2	1.867	2	0	1	0	1	0	1	0	12
276			min	-4392.743	3	.037	3	-17.024	4	0	4	-.023	4	-.003	2
277		6	max	2952.772	2	1.775	2	0	1	0	1	0	1	0	3
278			min	-4392.352	3	-.033	3	-17.482	4	0	4	-.029	4	-.004	2
279		7	max	2953.292	2	1.682	2	0	1	0	1	0	1	0	3
280			min	-4391.962	3	-.102	3	-17.94	4	0	4	-.035	4	-.004	2
281		8	max	2953.813	2	1.59	2	0	1	0	1	0	1	0	3
282			min	-4391.571	3	-.172	3	-18.399	4	0	4	-.042	4	-.005	2
283		9	max	2954.334	2	1.497	2	0	1	0	1	0	1	0	3
284			min	-4391.181	3	-.241	3	-18.857	4	0	4	-.049	4	-.005	2
285		10	max	2954.854	2	1.404	2	0	1	0	1	0	1	0	3
286			min	-4390.79	3	-.311	3	-19.315	4	0	4	-.055	4	-.006	2
287		11	max	2955.375	2	1.312	2	0	1	0	1	0	1	0	3
288			min	-4390.4	3	-.38	3	-19.774	4	0	4	-.062	4	-.006	2
289		12	max	2955.896	2	1.219	2	0	1	0	1	0	1	0	3
290			min	-4390.009	3	-.449	3	-20.232	4	0	4	-.069	4	-.007	2
291		13	max	2956.417	2	1.127	2	0	1	0	1	0	1	0	3
292			min	-4389.619	3	-.519	3	-20.69	4	0	4	-.077	4	-.007	2
293		14	max	2956.937	2	1.034	2	0	1	0	1	0	1	0	3
294			min	-4389.228	3	-.588	3	-21.149	4	0	4	-.084	4	-.008	2
295		15	max	2957.458	2	.941	2	0	1	0	1	0	1	0	3
296			min	-4388.838	3	-.658	3	-21.607	4	0	4	-.092	4	-.008	2
297		16	max	2957.979	2	.849	2	0	1	0	1	0	1	.001	3
298			min	-4388.447	3	-.727	3	-22.066	4	0	4	-.1	4	-.008	2
299		17	max	2958.499	2	.756	2	0	1	0	1	0	1	.001	3
300			min	-4388.057	3	-.797	3	-22.524	4	0	4	-.108	4	-.009	2
301		18	max	2959.02	2	.663	2	0	1	0	1	0	1	.002	3
302			min	-4387.666	3	-.866	3	-22.982	4	0	4	-.116	4	-.009	2
303		19	max	2959.541	2	.571	2	0	1	0	1	0	1	.002	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-4387.276	3	-.936	3	-23.441	4	0	4	-.124	4	-.009	2
305	M7	1	max	2852.254	2	7.682	6	4.827	4	0	1	0	1	.009	2
306			min	-2907.37	3	1.805	15	0	1	0	4	-.023	4	-.002	3
307		2	max	2852.083	2	6.921	6	5.362	4	0	1	0	1	.006	2
308			min	-2907.498	3	1.626	15	0	1	0	4	-.02	4	-.003	3
309		3	max	2851.913	2	6.16	6	5.896	4	0	1	0	1	.004	2
310			min	-2907.625	3	1.447	15	0	1	0	4	-.018	4	-.005	3
311		4	max	2851.743	2	5.399	6	6.431	4	0	1	0	1	.002	2
312			min	-2907.753	3	1.268	15	0	1	0	4	-.016	4	-.006	3
313		5	max	2851.572	2	4.638	6	6.966	4	0	1	0	1	0	2
314			min	-2907.881	3	1.089	15	0	1	0	4	-.013	4	-.007	3
315		6	max	2851.402	2	3.877	6	7.501	4	0	1	0	1	-.001	15
316			min	-2908.009	3	.91	15	0	1	0	4	-.01	4	-.007	3
317		7	max	2851.231	2	3.116	6	8.035	4	0	1	0	1	-.002	15
318			min	-2908.136	3	.731	15	0	1	0	4	-.007	5	-.008	3
319		8	max	2851.061	2	2.39	2	8.57	4	0	1	0	1	-.002	15
320			min	-2908.264	3	.465	12	0	1	0	4	-.003	5	-.008	4
321		9	max	2850.891	2	1.797	2	9.105	4	0	1	0	4	-.002	15
322			min	-2908.392	3	.169	12	0	1	0	4	0	1	-.009	4
323		10	max	2850.72	2	1.204	2	9.639	4	0	1	.004	4	-.002	15
324			min	-2908.52	3	-.266	3	0	1	0	4	0	1	-.01	4
325		11	max	2850.55	2	.611	2	10.174	4	0	1	.009	4	-.002	15
326			min	-2908.647	3	-.711	3	0	1	0	4	0	1	-.01	4
327		12	max	2850.38	2	.018	2	10.709	4	0	1	.013	4	-.002	15
328			min	-2908.775	3	-1.156	3	0	1	0	4	0	1	-.01	4
329		13	max	2850.209	2	-.342	15	11.243	4	0	1	.018	4	-.002	15
330			min	-2908.903	3	-1.6	3	0	1	0	4	0	1	-.009	4
331		14	max	2850.039	2	-.521	15	11.778	4	0	1	.022	4	-.002	15
332			min	-2909.031	3	-2.211	4	0	1	0	4	0	1	-.009	4
333		15	max	2849.869	2	-.7	15	12.313	4	0	1	.027	4	-.002	15
334			min	-2909.159	3	-2.972	4	0	1	0	4	0	1	-.007	4
335		16	max	2849.698	2	-.879	15	12.847	4	0	1	.033	4	-.001	15
336			min	-2909.286	3	-3.733	4	0	1	0	4	0	1	-.006	4
337		17	max	2849.528	2	-1.057	15	13.382	4	0	1	.038	4	-.001	15
338			min	-2909.414	3	-4.494	4	0	1	0	4	0	1	-.004	4
339		18	max	2849.358	2	-1.236	15	13.917	4	0	1	.044	4	0	15
340			min	-2909.542	3	-5.255	4	0	1	0	4	0	1	-.002	4
341		19	max	2849.187	2	-1.415	15	14.452	4	0	1	.05	4	0	1
342			min	-2909.67	3	-6.016	4	0	1	0	4	0	1	0	1
343	M8	1	max	1867.759	2	0	1	0	1	0	1	.047	4	0	1
344			min	70.304	15	0	1	-219.283	4	0	1	0	1	0	1
345		2	max	1867.93	2	0	1	0	1	0	1	.022	4	0	1
346			min	70.356	15	0	1	-219.431	4	0	1	0	1	0	1
347		3	max	1868.1	2	0	1	0	1	0	1	0	1	0	1
348			min	70.407	15	0	1	-219.579	4	0	1	-.003	4	0	1
349		4	max	1868.27	2	0	1	0	1	0	1	0	1	0	1
350			min	70.458	15	0	1	-219.726	4	0	1	-.029	4	0	1
351		5	max	1868.441	2	0	1	0	1	0	1	0	1	0	1
352			min	70.51	15	0	1	-219.874	4	0	1	-.054	4	0	1
353		6	max	1868.611	2	0	1	0	1	0	1	0	1	0	1
354			min	70.561	15	0	1	-220.021	4	0	1	-.079	4	0	1
355		7	max	1868.781	2	0	1	0	1	0	1	0	1	0	1
356			min	70.612	15	0	1	-220.169	4	0	1	-.104	4	0	1
357		8	max	1868.952	2	0	1	0	1	0	1	0	1	0	1
358			min	70.664	15	0	1	-220.317	4	0	1	-.13	4	0	1
359		9	max	1869.122	2	0	1	0	1	0	1	0	1	0	1
360			min	70.715	15	0	1	-220.464	4	0	1	-.155	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	1869.292	2	0	1	0	1	0	1	0	1	0	1
362			min	70.767	15	0	1	-220.612	4	0	1	-.18	4	0	1
363		11	max	1869.463	2	0	1	0	1	0	1	0	1	0	1
364			min	70.818	15	0	1	-220.76	4	0	1	-.206	4	0	1
365		12	max	1869.633	2	0	1	0	1	0	1	0	1	0	1
366			min	70.869	15	0	1	-220.907	4	0	1	-.231	4	0	1
367		13	max	1869.803	2	0	1	0	1	0	1	0	1	0	1
368			min	70.921	15	0	1	-221.055	4	0	1	-.256	4	0	1
369		14	max	1869.974	2	0	1	0	1	0	1	0	1	0	1
370			min	70.972	15	0	1	-221.203	4	0	1	-.282	4	0	1
371		15	max	1870.144	2	0	1	0	1	0	1	0	1	0	1
372			min	71.024	15	0	1	-221.35	4	0	1	-.307	4	0	1
373		16	max	1870.315	2	0	1	0	1	0	1	0	1	0	1
374			min	71.075	15	0	1	-221.498	4	0	1	-.333	4	0	1
375		17	max	1870.485	2	0	1	0	1	0	1	0	1	0	1
376			min	71.126	15	0	1	-221.645	4	0	1	-.358	4	0	1
377		18	max	1870.655	2	0	1	0	1	0	1	0	1	0	1
378			min	71.178	15	0	1	-221.793	4	0	1	-.383	4	0	1
379		19	max	1870.826	2	0	1	0	1	0	1	0	1	0	1
380			min	71.229	15	0	1	-221.941	4	0	1	-.409	4	0	1
381	M10	1	max	958.183	2	1.996	6	-.019	12	0	1	0	4	0	1
382			min	-1392.854	3	.459	15	-15.157	4	0	5	0	3	0	1
383		2	max	958.704	2	1.877	6	-.019	12	0	1	0	10	0	15
384			min	-1392.464	3	.431	15	-15.615	4	0	5	-.005	4	0	6
385		3	max	959.224	2	1.758	6	-.019	12	0	1	0	10	0	15
386			min	-1392.073	3	.403	15	-16.074	4	0	5	-.011	4	-.001	6
387		4	max	959.745	2	1.639	6	-.019	12	0	1	0	10	0	15
388			min	-1391.683	3	.375	15	-16.532	4	0	5	-.017	4	-.002	6
389		5	max	960.266	2	1.52	6	-.019	12	0	1	0	10	0	15
390			min	-1391.292	3	.347	15	-16.99	4	0	5	-.023	4	-.003	6
391		6	max	960.787	2	1.402	6	-.019	12	0	1	0	10	0	15
392			min	-1390.902	3	.319	15	-17.449	4	0	5	-.029	4	-.003	6
393		7	max	961.307	2	1.283	6	-.019	12	0	1	0	10	0	15
394			min	-1390.511	3	.291	15	-17.907	4	0	5	-.035	4	-.004	6
395		8	max	961.828	2	1.164	6	-.019	12	0	1	0	10	0	15
396			min	-1390.121	3	.263	15	-18.365	4	0	5	-.042	4	-.004	6
397		9	max	962.349	2	1.045	6	-.019	12	0	1	0	10	0	15
398			min	-1389.73	3	.235	15	-18.824	4	0	5	-.048	4	-.004	6
399		10	max	962.869	2	.945	2	-.019	12	0	1	0	10	-.001	15
400			min	-1389.34	3	.202	12	-19.282	4	0	5	-.055	4	-.005	6
401		11	max	963.39	2	.853	2	-.019	12	0	1	0	10	-.001	15
402			min	-1388.949	3	.156	12	-19.74	4	0	5	-.062	4	-.005	6
403		12	max	963.911	2	.76	2	-.019	12	0	1	0	10	-.001	15
404			min	-1388.558	3	.109	12	-20.199	4	0	5	-.069	4	-.005	6
405		13	max	964.431	2	.668	2	-.019	12	0	1	0	10	-.001	15
406			min	-1388.168	3	.063	12	-20.657	4	0	5	-.077	4	-.005	6
407		14	max	964.952	2	.575	2	-.019	12	0	1	0	12	-.001	15
408			min	-1387.777	3	-.003	3	-21.115	4	0	5	-.084	4	-.006	6
409		15	max	965.473	2	.482	2	-.019	12	0	1	0	12	-.001	15
410			min	-1387.387	3	-.073	3	-21.574	4	0	5	-.092	4	-.006	6
411		16	max	965.994	2	.39	2	-.019	12	0	1	0	12	-.001	15
412			min	-1386.996	3	-.142	3	-22.032	4	0	5	-.099	4	-.006	6
413		17	max	966.514	2	.297	2	-.019	12	0	1	0	12	-.001	15
414			min	-1386.606	3	-.212	3	-22.49	4	0	5	-.107	4	-.006	6
415		18	max	967.035	2	.204	2	-.019	12	0	1	0	12	-.001	15
416			min	-1386.215	3	-.281	3	-22.949	4	0	5	-.115	4	-.006	2
417		19	max	967.556	2	.112	2	-.019	12	0	1	0	12	-.001	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-1385.825	3	-.351	3	-23.407	4	0	5	-.124	4	-.006	2
419	M11	1	max	860.209	2	7.643	6	5.009	4	0	1	0	12	.006	2
420			min	-958.858	3	1.787	15	-.181	1	0	4	-.023	4	.001	12
421		2	max	860.039	2	6.882	6	5.544	4	0	1	0	12	.004	2
422			min	-958.985	3	1.609	15	-.181	1	0	4	-.02	4	0	3
423		3	max	859.868	2	6.121	6	6.079	4	0	1	0	12	.001	2
424			min	-959.113	3	1.43	15	-.181	1	0	4	-.018	4	-.001	3
425		4	max	859.698	2	5.36	6	6.613	4	0	1	0	12	0	2
426			min	-959.241	3	1.251	15	-.181	1	0	4	-.015	4	-.003	3
427		5	max	859.528	2	4.599	6	7.148	4	0	1	0	12	-.001	15
428			min	-959.369	3	1.072	15	-.181	1	0	4	-.012	4	-.004	4
429		6	max	859.357	2	3.838	6	7.683	4	0	1	0	12	-.001	15
430			min	-959.496	3	.893	15	-.181	1	0	4	-.009	4	-.006	4
431		7	max	859.187	2	3.077	6	8.218	4	0	1	0	12	-.002	15
432			min	-959.624	3	.714	15	-.181	1	0	4	-.006	4	-.007	4
433		8	max	859.017	2	2.316	6	8.752	4	0	1	0	12	-.002	15
434			min	-959.752	3	.535	15	-.181	1	0	4	-.003	4	-.009	4
435		9	max	858.846	2	1.555	6	9.287	4	0	1	.001	5	-.002	15
436			min	-959.88	3	.356	15	-.181	1	0	4	0	1	-.009	4
437		10	max	858.676	2	.81	2	9.822	4	0	1	.005	5	-.002	15
438			min	-960.007	3	.173	12	-.181	1	0	4	0	1	-.01	4
439		11	max	858.506	2	.217	2	10.356	4	0	1	.01	5	-.002	15
440			min	-960.135	3	-.209	3	-.181	1	0	4	0	1	-.01	4
441		12	max	858.335	2	-.18	15	10.891	4	0	1	.014	5	-.002	15
442			min	-960.263	3	-.729	4	-.181	1	0	4	-.001	1	-.01	4
443		13	max	858.165	2	-.359	15	11.426	4	0	1	.019	5	-.002	15
444			min	-960.391	3	-1.49	4	-.181	1	0	4	-.001	1	-.009	4
445		14	max	857.995	2	-.538	15	11.96	4	0	1	.023	5	-.002	15
446			min	-960.518	3	-2.251	4	-.181	1	0	4	-.001	1	-.009	4
447		15	max	857.824	2	-.717	15	12.495	4	0	1	.028	5	-.002	15
448			min	-960.646	3	-3.012	4	-.181	1	0	4	-.001	1	-.008	4
449		16	max	857.654	2	-.896	15	13.03	4	0	1	.034	5	-.001	15
450			min	-960.774	3	-3.773	4	-.181	1	0	4	-.001	1	-.006	4
451		17	max	857.484	2	-1.075	15	13.564	4	0	1	.039	5	-.001	15
452			min	-960.902	3	-4.534	4	-.181	1	0	4	-.001	1	-.004	4
453		18	max	857.313	2	-1.253	15	14.099	4	0	1	.045	4	0	15
454			min	-961.03	3	-5.295	4	-.181	1	0	4	-.001	1	-.002	4
455		19	max	857.143	2	-1.432	15	14.634	4	0	1	.051	4	0	1
456			min	-961.157	3	-6.056	4	-.181	1	0	4	-.002	1	0	1
457	M12	1	max	730.655	1	0	1	6.167	1	0	1	.048	4	0	1
458			min	59.046	12	0	1	-222.803	4	0	1	-.001	1	0	1
459		2	max	730.825	1	0	1	6.167	1	0	1	.023	5	0	1
460			min	59.131	12	0	1	-222.951	4	0	1	0	1	0	1
461		3	max	730.995	1	0	1	6.167	1	0	1	0	10	0	1
462			min	59.216	12	0	1	-223.099	4	0	1	-.003	4	0	1
463		4	max	731.166	1	0	1	6.167	1	0	1	0	1	0	1
464			min	59.301	12	0	1	-223.246	4	0	1	-.028	4	0	1
465		5	max	731.336	1	0	1	6.167	1	0	1	.001	1	0	1
466			min	59.386	12	0	1	-223.394	4	0	1	-.054	4	0	1
467		6	max	731.506	1	0	1	6.167	1	0	1	.002	1	0	1
468			min	59.472	12	0	1	-223.541	4	0	1	-.08	4	0	1
469		7	max	731.677	1	0	1	6.167	1	0	1	.003	1	0	1
470			min	59.557	12	0	1	-223.689	4	0	1	-.105	4	0	1
471		8	max	731.847	1	0	1	6.167	1	0	1	.003	1	0	1
472			min	59.642	12	0	1	-223.837	4	0	1	-.131	4	0	1
473		9	max	732.017	1	0	1	6.167	1	0	1	.004	1	0	1
474			min	59.727	12	0	1	-223.984	4	0	1	-.157	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	732.188	1	0	1	6.167	1	0	1	.005	1	0	1
476			min	59.812	12	0	1	-224.132	4	0	1	-.183	4	0	1
477		11	max	732.358	1	0	1	6.167	1	0	1	.006	1	0	1
478			min	59.897	12	0	1	-224.28	4	0	1	-.208	4	0	1
479		12	max	732.528	1	0	1	6.167	1	0	1	.006	1	0	1
480			min	59.983	12	0	1	-224.427	4	0	1	-.234	4	0	1
481		13	max	732.699	1	0	1	6.167	1	0	1	.007	1	0	1
482			min	60.068	12	0	1	-224.575	4	0	1	-.26	4	0	1
483		14	max	732.869	1	0	1	6.167	1	0	1	.008	1	0	1
484			min	60.153	12	0	1	-224.723	4	0	1	-.286	4	0	1
485		15	max	733.039	1	0	1	6.167	1	0	1	.008	1	0	1
486			min	60.238	12	0	1	-224.87	4	0	1	-.311	4	0	1
487		16	max	733.21	1	0	1	6.167	1	0	1	.009	1	0	1
488			min	60.323	12	0	1	-225.018	4	0	1	-.337	4	0	1
489		17	max	733.38	1	0	1	6.167	1	0	1	.01	1	0	1
490			min	60.408	12	0	1	-225.165	4	0	1	-.363	4	0	1
491		18	max	733.55	1	0	1	6.167	1	0	1	.011	1	0	1
492			min	60.494	12	0	1	-225.313	4	0	1	-.389	4	0	1
493		19	max	733.721	1	0	1	6.167	1	0	1	.011	1	0	1
494			min	60.579	12	0	1	-225.461	4	0	1	-.415	4	0	1
495	M1	1	max	126.58	1	714.029	3	33.315	5	0	2	.127	1	0	15
496			min	-14.355	5	-375.144	2	-53.239	1	0	3	-.085	5	-.013	2
497		2	max	127.402	1	713.149	3	34.557	5	0	2	.099	1	.185	2
498			min	-13.972	5	-376.317	2	-53.239	1	0	3	-.067	5	-.378	3
499		3	max	602.567	3	488.246	2	21.049	5	0	3	.07	1	.374	2
500			min	-347.044	2	-555.028	3	-53.123	1	0	2	-.049	5	-.739	3
501		4	max	603.184	3	487.073	2	22.29	5	0	3	.042	1	.117	2
502			min	-346.223	2	-555.908	3	-53.123	1	0	2	-.037	5	-.445	3
503		5	max	603.8	3	485.9	2	23.532	5	0	3	.014	1	-.003	15
504			min	-345.401	2	-556.788	3	-53.123	1	0	2	-.025	5	-.152	3
505		6	max	604.416	3	484.726	2	24.773	5	0	3	-.001	12	.142	3
506			min	-344.579	2	-557.668	3	-53.123	1	0	2	-.016	4	-.396	2
507		7	max	605.032	3	483.553	2	26.015	5	0	3	.001	5	.437	3
508			min	-343.758	2	-558.548	3	-53.123	1	0	2	-.042	1	-.652	2
509		8	max	605.649	3	482.38	2	27.256	5	0	3	.015	5	.732	3
510			min	-342.936	2	-559.428	3	-53.123	1	0	2	-.07	1	-.907	2
511		9	max	620.763	3	53.092	2	50.406	5	0	9	.044	1	.85	3
512			min	-286.534	2	.354	15	-83.497	1	0	3	-.1	5	-1.037	2
513		10	max	621.379	3	51.919	2	51.647	5	0	9	0	10	.832	3
514			min	-285.712	2	0	5	-83.497	1	0	3	-.074	4	-1.064	2
515		11	max	621.995	3	50.745	2	52.889	5	0	9	-.005	12	.815	3
516			min	-284.89	2	-1.474	4	-83.497	1	0	3	-.057	4	-1.092	2
517		12	max	636.824	3	385.118	3	125.865	5	0	2	.069	1	.714	3
518			min	-228.355	2	-594.194	2	-52.252	1	0	3	-.187	5	-.97	2
519		13	max	637.44	3	384.238	3	127.106	5	0	2	.041	1	.511	3
520			min	-227.533	2	-595.367	2	-52.252	1	0	3	-.12	5	-.656	2
521		14	max	638.057	3	383.358	3	128.348	5	0	2	.014	1	.309	3
522			min	-226.712	2	-596.54	2	-52.252	1	0	3	-.052	5	-.342	2
523		15	max	638.673	3	382.478	3	129.589	5	0	2	.016	5	.106	3
524			min	-225.89	2	-597.714	2	-52.252	1	0	3	-.014	1	-.037	1
525		16	max	639.289	3	381.598	3	130.831	5	0	2	.084	5	.289	2
526			min	-225.069	2	-598.887	2	-52.252	1	0	3	-.041	1	-.095	3
527		17	max	639.905	3	380.718	3	132.072	5	0	2	.154	5	.605	2
528			min	-224.247	2	-600.061	2	-52.252	1	0	3	-.069	1	-.296	3
529		18	max	27.695	5	594.335	2	-5.663	12	0	5	.176	5	.306	2
530			min	-127.802	1	-299.571	3	-90.888	4	0	2	-.098	1	-.147	3
531		19	max	28.078	5	593.161	2	-5.663	12	0	5	.137	5	.012	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-126.98	1	-300.451	3	-89.646	4	0	2	-.128	1	-.007	2
533	M5	1	max	284.077	1	2365.066	3	72.88	5	0	1	0	1	.026	2
534			min	11.455	12	-1296.878	2	0	1	0	4	-.176	4	0	15
535		2	max	284.899	1	2364.186	3	74.122	5	0	1	0	1	.71	2
536			min	11.865	12	-1298.051	2	0	1	0	4	-.138	4	-1.245	3
537		3	max	1866.633	3	1348.725	2	61.901	4	0	4	0	1	1.364	2
538			min	-1111.612	2	-1656.072	3	0	1	0	1	-.098	4	-2.444	3
539		4	max	1867.249	3	1347.551	2	63.143	4	0	4	0	1	.652	2
540			min	-1110.791	2	-1656.952	3	0	1	0	1	-.065	4	-1.57	3
541		5	max	1867.866	3	1346.378	2	64.384	4	0	4	0	1	.014	9
542			min	-1109.969	2	-1657.832	3	0	1	0	1	-.032	4	-.696	3
543		6	max	1868.482	3	1345.205	2	65.626	4	0	4	.003	4	.179	3
544			min	-1109.148	2	-1658.712	3	0	1	0	1	0	1	-.768	2
545		7	max	1869.098	3	1344.031	2	66.867	4	0	4	.038	4	1.055	3
546			min	-1108.326	2	-1659.592	3	0	1	0	1	0	1	-1.478	2
547		8	max	1869.714	3	1342.858	2	68.108	4	0	4	.073	4	1.931	3
548			min	-1107.504	2	-1660.472	3	0	1	0	1	0	1	-2.187	2
549		9	max	1885.902	3	179.834	2	169.619	4	0	1	0	1	2.218	3
550			min	-982.235	2	.35	15	0	1	0	1	-.156	4	-2.503	2
551		10	max	1886.518	3	178.66	2	170.861	4	0	1	0	1	2.151	3
552			min	-981.413	2	-.004	15	0	1	0	1	-.066	4	-2.598	2
553		11	max	1887.134	3	177.487	2	172.102	4	0	1	.025	4	2.084	3
554			min	-980.591	2	-1.423	6	0	1	0	1	0	1	-2.692	2
555		12	max	1903.893	3	1114.339	3	184.194	4	0	1	0	1	1.829	3
556			min	-855.588	2	-1705.122	2	0	1	0	4	-.27	4	-2.414	2
557		13	max	1904.509	3	1113.459	3	185.435	4	0	1	0	1	1.242	3
558			min	-854.766	2	-1706.295	2	0	1	0	4	-.173	4	-1.514	2
559		14	max	1905.125	3	1112.579	3	186.677	4	0	1	0	1	.654	3
560			min	-853.944	2	-1707.469	2	0	1	0	4	-.075	4	-.613	2
561		15	max	1905.742	3	1111.699	3	187.918	4	0	1	.024	4	.288	2
562			min	-853.123	2	-1708.642	2	0	1	0	4	0	1	0	13
563		16	max	1906.358	3	1110.819	3	189.159	4	0	1	.124	4	1.19	2
564			min	-852.301	2	-1709.815	2	0	1	0	4	0	1	-.519	3
565		17	max	1906.974	3	1109.939	3	190.401	4	0	1	.224	4	2.092	2
566			min	-851.48	2	-1710.989	2	0	1	0	4	0	1	-1.105	3
567		18	max	-13.005	12	2011.11	2	0	1	0	4	.278	4	1.076	2
568			min	-284.099	1	-1049.28	3	-12.152	5	0	1	0	1	-.577	3
569		19	max	-12.595	12	2009.937	2	0	1	0	4	.272	4	.015	2
570			min	-283.277	1	-1050.16	3	-10.91	5	0	1	0	1	-.023	3
571	M9	1	max	126.58	1	714.029	3	56.791	4	0	3	-.014	12	0	15
572			min	9.129	12	-375.144	2	5.946	12	0	4	-.141	4	-.013	2
573		2	max	127.402	1	713.149	3	58.032	4	0	3	-.011	12	.185	2
574			min	9.539	12	-376.317	2	5.946	12	0	4	-.111	4	-.378	3
575		3	max	602.567	3	488.246	2	53.123	1	0	2	-.008	12	.374	2
576			min	-347.044	2	-555.028	3	5.928	12	0	3	-.08	4	-.739	3
577		4	max	603.184	3	487.073	2	53.123	1	0	2	-.005	10	.117	2
578			min	-346.223	2	-555.908	3	5.928	12	0	3	-.056	4	-.445	3
579		5	max	603.8	3	485.9	2	53.123	1	0	2	-.002	10	-.003	15
580			min	-345.401	2	-556.788	3	5.928	12	0	3	-.032	4	-.152	3
581		6	max	604.416	3	484.726	2	53.123	1	0	2	.014	1	.142	3
582			min	-344.579	2	-557.668	3	5.928	12	0	3	-.01	5	-.396	2
583		7	max	605.032	3	483.553	2	53.123	1	0	2	.042	1	.437	3
584			min	-343.758	2	-558.548	3	5.928	12	0	3	.005	12	-.652	2
585		8	max	605.649	3	482.38	2	53.123	1	0	2	.07	1	.732	3
586			min	-342.936	2	-559.428	3	5.928	12	0	3	.008	12	-.907	2
587		9	max	620.763	3	53.092	2	87.31	4	0	3	-.004	12	.85	3
588			min	-286.534	2	.363	15	8.711	12	0	9	-.12	4	-1.037	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	621.379	3	51.919	2	88.551	4	0	3	0	1	.832	3
590			min	-285.712	2	.009	15	8.711	12	0	9	-.073	4	-1.064	2
591		11	max	621.995	3	50.745	2	89.793	4	0	3	.044	1	.815	3
592			min	-284.89	2	-1.423	6	8.711	12	0	9	-.038	5	-1.092	2
593		12	max	636.824	3	385.118	3	149.645	4	0	3	-.007	12	.714	3
594			min	-228.355	2	-594.194	2	5.098	12	0	2	-.218	4	-.97	2
595		13	max	637.44	3	384.238	3	150.886	4	0	3	-.004	12	.511	3
596			min	-227.533	2	-595.367	2	5.098	12	0	2	-.139	4	-.656	2
597		14	max	638.057	3	383.358	3	152.128	4	0	3	-.001	12	.309	3
598			min	-226.712	2	-596.54	2	5.098	12	0	2	-.059	4	-.342	2
599		15	max	638.673	3	382.478	3	153.369	4	0	3	.022	4	.106	3
600			min	-225.89	2	-597.714	2	5.098	12	0	2	.001	12	-.037	1
601		16	max	639.289	3	381.598	3	154.611	4	0	3	.103	4	.289	2
602			min	-225.069	2	-598.887	2	5.098	12	0	2	.004	12	-.095	3
603		17	max	639.905	3	380.718	3	155.852	4	0	3	.185	4	.605	2
604			min	-224.247	2	-600.061	2	5.098	12	0	2	.007	12	-.296	3
605		18	max	-8.969	12	594.335	2	58.14	1	0	2	.22	4	.306	2
606			min	-127.802	1	-299.571	3	-65.209	5	0	3	.009	12	-.147	3
607		19	max	-8.559	12	593.161	2	58.14	1	0	2	.194	4	.012	3
608			min	-126.98	1	-300.451	3	-63.967	5	0	3	.012	12	-.007	2

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.112	2	.01	3	9.493e-3	2	NC	1	NC	1
2			min	-.466	4	-.03	3	-.006	2	-2.991e-3	3	NC	1	NC	1
3		2	max	0	1	.103	3	.012	3	1.041e-2	2	NC	4	NC	1
4			min	-.466	4	.002	15	-.009	5	-2.905e-3	3	1313.353	3	NC	1
5		3	max	0	1	.211	3	.027	1	1.132e-2	2	NC	4	NC	2
6			min	-.466	4	-.003	9	-.011	5	-2.819e-3	3	723.647	3	6234.536	1
7		4	max	0	1	.278	3	.04	1	1.223e-2	2	NC	4	NC	2
8			min	-.466	4	-.012	1	-.008	5	-2.733e-3	3	566.072	3	4238.165	1
9		5	max	0	1	.296	3	.046	1	1.314e-2	2	NC	4	NC	2
10			min	-.466	4	-.009	1	-.003	5	-2.647e-3	3	534.535	3	3697.443	1
11		6	max	0	1	.266	3	.043	1	1.406e-2	2	NC	4	NC	2
12			min	-.466	4	-.002	9	-.002	10	-2.561e-3	3	588.178	3	3947.539	1
13		7	max	0	1	.198	3	.032	1	1.497e-2	2	NC	4	NC	2
14			min	-.466	4	.001	15	-.005	10	-2.475e-3	3	763.04	3	5312.044	1
15		8	max	0	1	.134	2	.03	3	1.588e-2	2	NC	1	NC	1
16			min	-.466	4	.002	15	-.01	2	-2.389e-3	3	1237.605	3	8710.727	3
17		9	max	0	1	.182	2	.031	3	1.679e-2	2	NC	4	NC	1
18			min	-.466	4	.003	15	-.018	2	-2.303e-3	3	2479.793	2	8527.698	3
19		10	max	0	1	.204	2	.031	3	1.771e-2	2	NC	4	NC	1
20			min	-.466	4	-.006	3	-.022	2	-2.218e-3	3	1896.897	2	8515.845	3
21		11	max	0	12	.182	2	.031	3	1.679e-2	2	NC	4	NC	1
22			min	-.466	4	.003	15	-.018	2	-2.303e-3	3	2479.793	2	8527.698	3
23		12	max	0	12	.134	2	.03	3	1.588e-2	2	NC	1	NC	1
24			min	-.466	4	.002	15	-.01	2	-2.389e-3	3	1237.605	3	8710.727	3
25		13	max	0	12	.198	3	.032	1	1.497e-2	2	NC	4	NC	2
26			min	-.466	4	.001	15	-.005	10	-2.475e-3	3	763.04	3	5312.044	1
27		14	max	0	12	.266	3	.043	1	1.406e-2	2	NC	4	NC	2
28			min	-.466	4	-.002	9	-.002	10	-2.561e-3	3	588.178	3	3947.539	1
29		15	max	0	12	.296	3	.046	1	1.314e-2	2	NC	4	NC	2
30			min	-.466	4	-.009	1	0	10	-2.647e-3	3	534.535	3	3697.443	1
31		16	max	0	12	.278	3	.04	1	1.223e-2	2	NC	4	NC	2
32			min	-.466	4	-.012	1	0	10	-2.733e-3	3	566.072	3	4238.165	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	12	.211	3	.027	1	1.132e-2	2	NC	4	NC	2
34			min	-.466	4	-.003	9	-.001	10	-2.819e-3	3	723.647	3	6234.536	1
35		18	max	0	12	.103	3	.016	4	1.041e-2	2	NC	4	NC	1
36			min	-.466	4	0	15	-.003	10	-2.905e-3	3	1313.353	3	NC	1
37		19	max	0	12	.112	2	.01	3	9.493e-3	2	NC	1	NC	1
38			min	-.466	4	-.03	3	-.006	2	-2.991e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.264	3	.009	3	5.237e-3	2	NC	1	NC	1
40			min	-.355	4	-.354	2	-.006	2	-4.449e-3	3	NC	1	NC	1
41		2	max	0	1	.429	3	.01	3	6.071e-3	2	NC	4	NC	1
42			min	-.355	4	-.502	2	-.014	5	-5.23e-3	3	1057.235	3	NC	1
43		3	max	0	1	.573	3	.021	1	6.906e-3	2	NC	5	NC	2
44			min	-.355	4	-.634	2	-.018	5	-6.012e-3	3	563.757	3	8164.517	1
45		4	max	0	1	.682	3	.033	1	7.74e-3	2	NC	5	NC	2
46			min	-.355	4	-.741	2	-.013	5	-6.794e-3	3	416.393	3	5136.292	1
47		5	max	0	1	.749	3	.04	1	8.574e-3	2	NC	5	NC	2
48			min	-.355	4	-.816	2	-.003	5	-7.576e-3	3	358.966	3	4291.234	1
49		6	max	0	1	.773	3	.038	1	9.409e-3	2	NC	5	NC	2
50			min	-.355	4	-.858	2	-.002	10	-8.358e-3	3	342.239	3	4454.655	1
51		7	max	0	1	.759	3	.029	1	1.024e-2	2	NC	5	NC	2
52			min	-.355	4	-.869	2	-.005	10	-9.14e-3	3	337.619	2	5871.099	1
53		8	max	0	1	.721	3	.027	4	1.108e-2	2	NC	5	NC	1
54			min	-.355	4	-.858	2	-.009	2	-9.922e-3	3	344.715	2	6662.203	4
55		9	max	0	1	.679	3	.027	3	1.191e-2	2	NC	5	NC	1
56			min	-.355	4	-.839	2	-.017	2	-1.07e-2	3	358.764	2	9615.299	3
57		10	max	0	1	.657	3	.027	3	1.275e-2	2	NC	5	NC	1
58			min	-.355	4	-.827	2	-.02	2	-1.149e-2	3	367.388	2	9587.275	3
59		11	max	0	12	.679	3	.027	3	1.191e-2	2	NC	5	NC	1
60			min	-.355	4	-.839	2	-.017	2	-1.07e-2	3	358.764	2	9615.299	3
61		12	max	0	12	.721	3	.027	3	1.108e-2	2	NC	5	NC	1
62			min	-.355	4	-.858	2	-.017	5	-9.922e-3	3	344.715	2	9874.153	3
63		13	max	0	12	.759	3	.029	1	1.024e-2	2	NC	5	NC	2
64			min	-.355	4	-.869	2	-.011	5	-9.14e-3	3	337.619	2	5871.099	1
65		14	max	0	12	.773	3	.038	1	9.409e-3	2	NC	5	NC	2
66			min	-.355	4	-.858	2	-.002	10	-8.358e-3	3	342.239	3	4454.655	1
67		15	max	0	12	.749	3	.04	1	8.574e-3	2	NC	5	NC	2
68			min	-.355	4	-.816	2	0	10	-7.576e-3	3	358.966	3	4291.234	1
69		16	max	0	12	.682	3	.033	1	7.74e-3	2	NC	5	NC	2
70			min	-.355	4	-.741	2	0	10	-6.794e-3	3	416.393	3	5136.292	1
71		17	max	0	12	.573	3	.029	4	6.906e-3	2	NC	5	NC	2
72			min	-.355	4	-.634	2	-.001	10	-6.012e-3	3	563.757	3	6033.895	4
73		18	max	0	12	.429	3	.019	4	6.071e-3	2	NC	4	NC	1
74			min	-.355	4	-.502	2	-.003	2	-5.23e-3	3	1057.235	3	8948	4
75		19	max	0	12	.264	3	.009	3	5.237e-3	2	NC	1	NC	1
76			min	-.355	4	-.354	2	-.006	2	-4.449e-3	3	NC	1	NC	1
77	M15	1	max	0	10	.268	3	.008	3	3.958e-3	3	NC	1	NC	1
78			min	-.294	4	-.352	2	-.005	2	-5.512e-3	2	NC	1	NC	1
79		2	max	0	10	.39	3	.01	3	4.656e-3	3	NC	4	NC	1
80			min	-.294	4	-.539	2	-.02	5	-6.399e-3	2	932.548	2	8170.981	5
81		3	max	0	10	.5	3	.021	1	5.354e-3	3	NC	5	NC	2
82			min	-.294	4	-.703	2	-.025	5	-7.285e-3	2	496.195	2	6673.876	5
83		4	max	0	10	.588	3	.033	1	6.052e-3	3	NC	5	NC	2
84			min	-.294	4	-.829	2	-.018	5	-8.171e-3	2	365.169	2	5112.468	1
85		5	max	0	10	.651	3	.04	1	6.75e-3	3	NC	5	NC	2
86			min	-.294	4	-.908	2	-.005	5	-9.058e-3	2	313.143	2	4268.878	1
87		6	max	0	10	.686	3	.039	1	7.448e-3	3	NC	5	NC	2
88			min	-.294	4	-.94	2	-.002	10	-9.944e-3	2	296.358	2	4424.846	1
89		7	max	0	10	.697	3	.031	4	8.146e-3	3	NC	5	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.294	4	-.93	2	-.004	10	-1.083e-2	2	301.441	2	5810.811	1
91		8	max	0	10	.69	3	.033	4	8.844e-3	3	NC	5	NC	1
92			min	-.294	4	-.892	2	-.008	2	-1.172e-2	2	322.441	2	5478.62	4
93		9	max	0	10	.675	3	.025	3	9.542e-3	3	NC	5	NC	1
94			min	-.294	4	-.848	2	-.015	2	-1.26e-2	2	351.237	2	7723.586	4
95		10	max	0	1	.666	3	.025	3	1.024e-2	3	NC	5	NC	1
96			min	-.294	4	-.825	2	-.019	2	-1.349e-2	2	367.944	2	NC	1
97		11	max	0	1	.675	3	.025	3	9.542e-3	3	NC	5	NC	1
98			min	-.294	4	-.848	2	-.019	5	-1.26e-2	2	351.237	2	9022.811	5
99		12	max	0	1	.69	3	.025	3	8.844e-3	3	NC	5	NC	1
100			min	-.294	4	-.892	2	-.023	5	-1.172e-2	2	322.441	2	7718.291	5
101		13	max	0	1	.697	3	.029	1	8.146e-3	3	NC	5	NC	2
102			min	-.294	4	-.93	2	-.015	5	-1.083e-2	2	301.441	2	5810.811	1
103		14	max	0	1	.686	3	.039	1	7.448e-3	3	NC	5	NC	2
104			min	-.294	4	-.94	2	-.002	10	-9.944e-3	2	296.358	2	4424.846	1
105		15	max	0	1	.651	3	.04	1	6.75e-3	3	NC	5	NC	2
106			min	-.294	4	-.908	2	0	10	-9.058e-3	2	313.143	2	4268.878	1
107		16	max	0	1	.588	3	.035	4	6.052e-3	3	NC	5	NC	2
108			min	-.294	4	-.829	2	0	10	-8.171e-3	2	365.169	2	4997.371	4
109		17	max	0	1	.5	3	.036	4	5.354e-3	3	NC	5	NC	2
110			min	-.294	4	-.703	2	-.001	10	-7.285e-3	2	496.195	2	4865.465	4
111		18	max	0	1	.39	3	.024	4	4.656e-3	3	NC	4	NC	1
112			min	-.293	4	-.539	2	-.003	10	-6.399e-3	2	932.548	2	7005.482	4
113		19	max	0	1	.268	3	.008	3	3.958e-3	3	NC	1	NC	1
114			min	-.293	4	-.352	2	-.005	2	-5.512e-3	2	NC	1	NC	1
115	M16	1	max	0	12	.099	2	.007	3	7.263e-3	3	NC	1	NC	1
116			min	-.109	4	-.089	3	-.005	2	-7.778e-3	2	NC	1	NC	1
117		2	max	0	12	.012	1	.011	1	8.095e-3	3	NC	4	NC	1
118			min	-.109	4	-.049	3	-.016	5	-8.305e-3	2	1786.746	2	NC	1
119		3	max	0	12	.002	4	.027	1	8.926e-3	3	NC	4	NC	2
120			min	-.109	4	-.076	2	-.02	5	-8.832e-3	2	997.286	2	6214.387	1
121		4	max	0	12	0	5	.041	1	9.758e-3	3	NC	4	NC	2
122			min	-.109	4	-.119	2	-.016	5	-9.359e-3	2	799.186	2	4207.765	1
123		5	max	0	12	0	13	.047	1	1.059e-2	3	NC	4	NC	2
124			min	-.109	4	-.122	2	-.007	5	-9.887e-3	2	787.547	2	3653.608	1
125		6	max	0	12	.003	4	.044	1	1.142e-2	3	NC	4	NC	2
126			min	-.109	4	-.087	2	0	10	-1.041e-2	2	939.028	2	3871.961	1
127		7	max	0	12	.013	9	.033	1	1.225e-2	3	NC	3	NC	2
128			min	-.109	4	-.079	3	-.003	10	-1.094e-2	2	1458.16	2	5131.888	1
129		8	max	0	12	.061	1	.023	4	1.308e-2	3	NC	1	NC	2
130			min	-.109	4	-.125	3	-.006	10	-1.147e-2	2	4470.565	2	7860.893	4
131		9	max	0	12	.131	2	.022	3	1.392e-2	3	NC	4	NC	1
132			min	-.109	4	-.166	3	-.014	2	-1.2e-2	2	2280.581	3	NC	1
133		10	max	0	1	.164	2	.022	3	1.475e-2	3	NC	4	NC	1
134			min	-.109	4	-.183	3	-.017	2	-1.252e-2	2	1850.785	3	NC	1
135		11	max	0	1	.131	2	.022	3	1.392e-2	3	NC	4	NC	1
136			min	-.109	4	-.166	3	-.014	2	-1.2e-2	2	2280.581	3	NC	1
137		12	max	0	1	.061	1	.022	3	1.308e-2	3	NC	1	NC	2
138			min	-.109	4	-.125	3	-.012	5	-1.147e-2	2	4470.565	2	9872.911	1
139		13	max	0	1	.013	9	.033	1	1.225e-2	3	NC	3	NC	2
140			min	-.109	4	-.079	3	-.005	5	-1.094e-2	2	1458.16	2	5131.888	1
141		14	max	0	1	.003	6	.044	1	1.142e-2	3	NC	4	NC	2
142			min	-.109	4	-.087	2	0	10	-1.041e-2	2	939.028	2	3871.961	1
143		15	max	0	1	0	13	.047	1	1.059e-2	3	NC	4	NC	2
144			min	-.109	4	-.122	2	.001	10	-9.887e-3	2	787.547	2	3653.608	1
145		16	max	0	1	0	13	.041	1	9.758e-3	3	NC	4	NC	2
146			min	-.109	4	-.119	2	.001	10	-9.359e-3	2	799.186	2	4207.765	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.001	13	.034	4	8.926e-3	3	NC	4	NC	2
148			min	-.109	4	-.076	2	0	10	-8.832e-3	2	997.286	2	5156.631	4
149		18	max	0	1	.012	1	.022	4	8.095e-3	3	NC	4	NC	1
150			min	-.109	4	-.049	3	-.002	10	-8.305e-3	2	1786.746	2	7833.646	4
151		19	max	0	1	.099	2	.007	3	7.263e-3	3	NC	1	NC	1
152			min	-.109	4	-.089	3	-.005	2	-7.778e-3	2	NC	1	NC	1
153	M2	1	max	.007	2	.01	2	.004	1	1.334e-3	5	NC	1	NC	1
154			min	-.01	3	-.016	3	-.439	4	-1.124e-4	1	7425.377	2	175.289	4
155		2	max	.007	2	.009	2	.004	1	1.37e-3	5	NC	1	NC	1
156			min	-.01	3	-.015	3	-.404	4	-1.066e-4	1	8607.117	2	190.489	4
157		3	max	.006	2	.008	2	.003	1	1.406e-3	5	NC	1	NC	1
158			min	-.009	3	-.015	3	-.369	4	-1.008e-4	1	NC	1	208.477	4
159		4	max	.006	2	.006	2	.003	1	1.441e-3	5	NC	1	NC	1
160			min	-.009	3	-.014	3	-.335	4	-9.498e-5	1	NC	1	229.969	4
161		5	max	.006	2	.005	2	.003	1	1.477e-3	5	NC	1	NC	1
162			min	-.008	3	-.014	3	-.301	4	-8.919e-5	1	NC	1	255.936	4
163		6	max	.005	2	.004	2	.002	1	1.513e-3	5	NC	1	NC	1
164			min	-.007	3	-.013	3	-.268	4	-8.339e-5	1	NC	1	287.718	4
165		7	max	.005	2	.002	2	.002	1	1.549e-3	5	NC	1	NC	1
166			min	-.007	3	-.013	3	-.235	4	-7.76e-5	1	NC	1	327.206	4
167		8	max	.004	2	.001	2	.002	1	1.584e-3	5	NC	1	NC	1
168			min	-.006	3	-.012	3	-.204	4	-7.181e-5	1	NC	1	377.141	4
169		9	max	.004	2	0	2	.002	1	1.62e-3	5	NC	1	NC	1
170			min	-.006	3	-.011	3	-.174	4	-6.602e-5	1	NC	1	441.623	4
171		10	max	.004	2	0	2	.001	1	1.656e-3	5	NC	1	NC	1
172			min	-.005	3	-.01	3	-.146	4	-6.023e-5	1	NC	1	527.009	4
173		11	max	.003	2	0	2	.001	1	1.692e-3	5	NC	1	NC	1
174			min	-.005	3	-.009	3	-.12	4	-5.444e-5	1	NC	1	643.607	4
175		12	max	.003	2	-.001	15	0	1	1.727e-3	5	NC	1	NC	1
176			min	-.004	3	-.008	3	-.095	4	-4.865e-5	1	NC	1	809.049	4
177		13	max	.002	2	-.001	15	0	1	1.764e-3	4	NC	1	NC	1
178			min	-.003	3	-.007	3	-.073	4	-4.286e-5	1	NC	1	1055.622	4
179		14	max	.002	2	0	15	0	1	1.801e-3	4	NC	1	NC	1
180			min	-.003	3	-.006	3	-.053	4	-3.707e-5	1	NC	1	1447.882	4
181		15	max	.002	2	0	15	0	1	1.839e-3	4	NC	1	NC	1
182			min	-.002	3	-.005	3	-.036	4	-3.127e-5	1	NC	1	2131.274	4
183		16	max	.001	2	0	15	0	1	1.876e-3	4	NC	1	NC	1
184			min	-.002	3	-.004	3	-.022	4	-2.548e-5	1	NC	1	3495.106	4
185		17	max	0	2	0	15	0	1	1.914e-3	4	NC	1	NC	1
186			min	-.001	3	-.003	3	-.011	4	-1.969e-5	1	NC	1	6912.974	4
187		18	max	0	2	0	15	0	1	1.951e-3	4	NC	1	NC	1
188			min	0	3	-.001	3	-.004	4	-1.39e-5	1	NC	1	NC	1
189		19	max	0	1	0	1	0	1	1.989e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	-8.11e-6	1	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	1.837e-6	1	NC	1	NC	1
192			min	0	1	0	1	0	1	-5.108e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.009	4	1.235e-5	1	NC	1	NC	1
194			min	0	2	-.002	6	0	1	-5.57e-5	5	NC	1	9646.074	4
195		3	max	0	3	0	15	.018	4	4.068e-4	4	NC	1	NC	1
196			min	0	2	-.004	6	0	1	2.2e-6	12	NC	1	5064.834	4
197		4	max	.001	3	-.001	15	.025	4	8.657e-4	4	NC	1	NC	1
198			min	-.001	2	-.006	6	0	1	3.157e-6	12	NC	1	3539.496	4
199		5	max	.002	3	-.002	15	.032	4	1.325e-3	4	NC	1	NC	1
200			min	-.002	2	-.008	6	0	1	4.114e-6	12	NC	1	2775.842	4
201		6	max	.002	3	-.002	15	.039	4	1.783e-3	4	NC	1	NC	1
202			min	-.002	2	-.01	6	0	1	5.071e-6	12	9376.446	6	2314.56	4
203		7	max	.003	3	-.002	15	.045	4	2.242e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.002	2	-.011	6	0	3	6.029e-6	12	8100.454	6	2002.173	4
205		8	max	.003	3	-.003	15	.051	4	2.701e-3	4	NC	2	NC	1
206			min	-.003	2	-.012	6	0	12	6.986e-6	12	7314.88	6	1772.635	4
207		9	max	.004	3	-.003	15	.056	4	3.16e-3	4	NC	5	NC	1
208			min	-.003	2	-.013	6	0	12	7.943e-6	12	6855.702	6	1592.784	4
209		10	max	.004	3	-.003	15	.062	4	3.619e-3	4	NC	5	NC	1
210			min	-.004	2	-.014	6	0	12	8.9e-6	12	6643.859	6	1444.197	4
211		11	max	.005	3	-.003	15	.068	4	4.078e-3	4	NC	5	NC	1
212			min	-.004	2	-.014	6	0	12	9.857e-6	12	6648.399	6	1315.971	4
213		12	max	.005	3	-.003	15	.075	4	4.536e-3	4	NC	5	NC	1
214			min	-.005	2	-.013	6	0	12	1.081e-5	12	6874.606	6	1201.45	4
215		13	max	.006	3	-.003	15	.082	4	4.995e-3	4	NC	2	NC	1
216			min	-.005	2	-.012	6	0	12	1.177e-5	12	7367.57	6	1096.587	4
217		14	max	.006	3	-.002	15	.09	4	5.454e-3	4	NC	1	NC	1
218			min	-.005	2	-.011	6	0	12	1.273e-5	12	8235.075	6	999.02	4
219		15	max	.006	3	-.002	15	.099	4	5.913e-3	4	NC	1	NC	1
220			min	-.006	2	-.009	6	0	12	1.369e-5	12	9714.163	6	907.501	4
221		16	max	.007	3	-.001	15	.109	4	6.372e-3	4	NC	1	NC	1
222			min	-.006	2	-.007	6	0	12	1.464e-5	12	NC	1	821.502	4
223		17	max	.007	3	0	15	.121	4	6.831e-3	4	NC	1	NC	1
224			min	-.007	2	-.006	3	0	12	1.56e-5	12	NC	1	740.914	4
225		18	max	.008	3	0	15	.135	4	7.29e-3	4	NC	1	NC	1
226			min	-.007	2	-.004	3	0	12	1.656e-5	12	NC	1	665.833	4
227		19	max	.008	3	0	2	.151	4	7.748e-3	4	NC	1	NC	1
228			min	-.007	2	-.003	3	0	12	1.751e-5	12	NC	1	596.405	4
229	M4	1	max	.002	1	.007	2	0	12	1.101e-3	4	NC	1	NC	2
230			min	0	5	-.009	3	-.151	4	7.647e-6	12	NC	1	164.673	4
231		2	max	.002	1	.007	2	0	12	1.101e-3	4	NC	1	NC	2
232			min	0	5	-.008	3	-.139	4	7.647e-6	12	NC	1	178.534	4
233		3	max	.002	1	.006	2	0	12	1.101e-3	4	NC	1	NC	2
234			min	0	5	-.008	3	-.127	4	7.647e-6	12	NC	1	195.063	4
235		4	max	.001	1	.006	2	0	12	1.101e-3	4	NC	1	NC	2
236			min	0	5	-.007	3	-.115	4	7.647e-6	12	NC	1	214.948	4
237		5	max	.001	1	.006	2	0	12	1.101e-3	4	NC	1	NC	2
238			min	0	5	-.007	3	-.104	4	7.647e-6	12	NC	1	239.123	4
239		6	max	.001	1	.005	2	0	12	1.101e-3	4	NC	1	NC	1
240			min	0	5	-.006	3	-.092	4	7.647e-6	12	NC	1	268.883	4
241		7	max	.001	1	.005	2	0	12	1.101e-3	4	NC	1	NC	1
242			min	0	5	-.006	3	-.081	4	7.647e-6	12	NC	1	306.068	4
243		8	max	.001	1	.004	2	0	12	1.101e-3	4	NC	1	NC	1
244			min	0	5	-.005	3	-.07	4	7.647e-6	12	NC	1	353.36	4
245		9	max	0	1	.004	2	0	12	1.101e-3	4	NC	1	NC	1
246			min	0	5	-.005	3	-.06	4	7.647e-6	12	NC	1	414.795	4
247		10	max	0	1	.004	2	0	12	1.101e-3	4	NC	1	NC	1
248			min	0	5	-.004	3	-.05	4	7.647e-6	12	NC	1	496.681	4
249		11	max	0	1	.003	2	0	12	1.101e-3	4	NC	1	NC	1
250			min	0	5	-.004	3	-.041	4	7.647e-6	12	NC	1	609.331	4
251		12	max	0	1	.003	2	0	12	1.101e-3	4	NC	1	NC	1
252			min	0	5	-.003	3	-.032	4	7.647e-6	12	NC	1	770.577	4
253		13	max	0	1	.002	2	0	12	1.101e-3	4	NC	1	NC	1
254			min	0	5	-.003	3	-.024	4	7.647e-6	12	NC	1	1013.499	4
255		14	max	0	1	.002	2	0	12	1.101e-3	4	NC	1	NC	1
256			min	0	5	-.002	3	-.018	4	7.647e-6	12	NC	1	1405.349	4
257		15	max	0	1	.002	2	0	12	1.101e-3	4	NC	1	NC	1
258			min	0	5	-.002	3	-.012	4	7.647e-6	12	NC	1	2101.031	4
259		16	max	0	1	.001	2	0	12	1.101e-3	4	NC	1	NC	1
260			min	0	5	-.001	3	-.007	4	7.647e-6	12	NC	1	3528.325	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	1.101e-3	4	NC	1	NC	1
262			min	0	5	0	3	-.003	4	7.647e-6	12	NC	1	7271.052	4
263		18	max	0	1	0	2	0	12	1.101e-3	4	NC	1	NC	1
264			min	0	5	0	3	-.001	4	7.647e-6	12	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.101e-3	4	NC	1	NC	1
266			min	0	1	0	1	0	1	7.647e-6	12	NC	1	NC	1
267	M6	1	max	.022	2	.034	2	0	1	1.392e-3	4	NC	4	NC	1
268			min	-.033	3	-.049	3	-.443	4	0	1	1576.774	3	173.742	4
269		2	max	.021	2	.031	2	0	1	1.426e-3	4	NC	4	NC	1
270			min	-.031	3	-.046	3	-.408	4	0	1	1669.499	3	188.81	4
271		3	max	.019	2	.028	2	0	1	1.461e-3	4	NC	4	NC	1
272			min	-.029	3	-.043	3	-.373	4	0	1	1773.942	3	206.641	4
273		4	max	.018	2	.025	2	0	1	1.495e-3	4	NC	4	NC	1
274			min	-.027	3	-.041	3	-.338	4	0	1	1892.584	3	227.946	4
275		5	max	.017	2	.022	2	0	1	1.53e-3	4	NC	4	NC	1
276			min	-.025	3	-.038	3	-.304	4	0	1	2028.621	3	253.688	4
277		6	max	.016	2	.02	2	0	1	1.564e-3	4	NC	4	NC	1
278			min	-.023	3	-.035	3	-.27	4	0	1	2186.229	3	285.194	4
279		7	max	.015	2	.017	2	0	1	1.599e-3	4	NC	1	NC	1
280			min	-.022	3	-.032	3	-.237	4	0	1	2370.98	3	324.339	4
281		8	max	.013	2	.014	2	0	1	1.633e-3	4	NC	1	NC	1
282			min	-.02	3	-.03	3	-.206	4	0	1	2590.476	3	373.84	4
283		9	max	.012	2	.012	2	0	1	1.667e-3	4	NC	1	NC	1
284			min	-.018	3	-.027	3	-.176	4	0	1	2855.365	3	437.761	4
285		10	max	.011	2	.01	2	0	1	1.702e-3	4	NC	1	NC	1
286			min	-.016	3	-.024	3	-.147	4	0	1	3181.034	3	522.403	4
287		11	max	.01	2	.008	2	0	1	1.736e-3	4	NC	1	NC	1
288			min	-.014	3	-.021	3	-.121	4	0	1	3590.581	3	637.982	4
289		12	max	.009	2	.006	2	0	1	1.771e-3	4	NC	1	NC	1
290			min	-.013	3	-.019	3	-.096	4	0	1	4120.319	3	801.973	4
291		13	max	.007	2	.004	2	0	1	1.805e-3	4	NC	1	NC	1
292			min	-.011	3	-.016	3	-.074	4	0	1	4830.799	3	1046.373	4
293		14	max	.006	2	.003	2	0	1	1.84e-3	4	NC	1	NC	1
294			min	-.009	3	-.013	3	-.054	4	0	1	5831.054	3	1435.154	4
295		15	max	.005	2	.002	2	0	1	1.874e-3	4	NC	1	NC	1
296			min	-.007	3	-.01	3	-.036	4	0	1	7339.219	3	2112.424	4
297		16	max	.004	2	0	2	0	1	1.909e-3	4	NC	1	NC	1
298			min	-.005	3	-.008	3	-.022	4	0	1	9864.387	3	3463.855	4
299		17	max	.002	2	0	2	0	1	1.943e-3	4	NC	1	NC	1
300			min	-.004	3	-.005	3	-.011	4	0	1	NC	1	6849.88	4
301		18	max	.001	2	0	2	0	1	1.977e-3	4	NC	1	NC	1
302			min	-.002	3	-.003	3	-.004	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	2.012e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-5.169e-4	4	NC	1	NC	1
307		2	max	.001	3	0	2	.009	4	0	1	NC	1	NC	1
308			min	-.001	2	-.003	3	0	1	-6.991e-5	5	NC	1	9534.913	4
309		3	max	.003	3	0	2	.018	4	3.778e-4	4	NC	1	NC	1
310			min	-.003	2	-.006	3	0	1	0	1	NC	1	5007.434	4
311		4	max	.004	3	-.001	15	.026	4	8.252e-4	4	NC	1	NC	1
312			min	-.004	2	-.008	3	0	1	0	1	NC	1	3501.069	4
313		5	max	.006	3	-.002	15	.033	4	1.273e-3	4	NC	1	NC	1
314			min	-.005	2	-.01	3	0	1	0	1	NC	1	2747.932	4
315		6	max	.007	3	-.002	15	.039	4	1.72e-3	4	NC	1	NC	1
316			min	-.007	2	-.012	3	0	1	0	1	8765.692	3	2293.991	4
317		7	max	.008	3	-.003	15	.045	4	2.167e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.008	2	-.014	3	0	1	0	1	7835.562	3	1987.516	4
319		8	max	.01	3	-.003	15	.051	4	2.615e-3	4	NC	1	NC	1
320			min	-.01	2	-.015	3	0	1	0	1	7286.175	3	1763.184	4
321		9	max	.011	3	-.003	15	.057	4	3.062e-3	4	NC	1	NC	1
322			min	-.011	2	-.016	3	0	1	0	1	6852.437	4	1588.148	4
323		10	max	.013	3	-.003	15	.062	4	3.509e-3	4	NC	1	NC	1
324			min	-.012	2	-.017	3	0	1	0	1	6640.865	4	1444.099	4
325		11	max	.014	3	-.003	15	.068	4	3.957e-3	4	NC	1	NC	1
326			min	-.014	2	-.017	3	0	1	0	1	6645.547	4	1320.133	4
327		12	max	.015	3	-.003	15	.074	4	4.404e-3	4	NC	1	NC	1
328			min	-.015	2	-.017	3	0	1	0	1	6871.784	4	1209.529	4
329		13	max	.017	3	-.003	15	.081	4	4.852e-3	4	NC	1	NC	1
330			min	-.016	2	-.016	3	0	1	0	1	7364.661	4	1108.139	4
331		14	max	.018	3	-.003	15	.089	4	5.299e-3	4	NC	1	NC	1
332			min	-.018	2	-.015	3	0	1	0	1	8231.93	4	1013.498	4
333		15	max	.02	3	-.002	15	.097	4	5.746e-3	4	NC	1	NC	1
334			min	-.019	2	-.014	3	0	1	0	1	9710.557	4	924.279	4
335		16	max	.021	3	-.002	15	.107	4	6.194e-3	4	NC	1	NC	1
336			min	-.021	2	-.013	3	0	1	0	1	NC	1	839.909	4
337		17	max	.022	3	0	2	.118	4	6.641e-3	4	NC	1	NC	1
338			min	-.022	2	-.011	3	0	1	0	1	NC	1	760.284	4
339		18	max	.024	3	0	2	.131	4	7.089e-3	4	NC	1	NC	1
340			min	-.023	2	-.009	3	0	1	0	1	NC	1	685.55	4
341		19	max	.025	3	.002	2	.146	4	7.536e-3	4	NC	1	NC	1
342			min	-.025	2	-.008	3	0	1	0	1	NC	1	615.935	4
343	M8	1	max	.004	2	.024	2	0	1	9.763e-4	4	NC	1	NC	1
344			min	0	15	-.026	3	-.146	4	0	1	NC	1	170.066	4
345		2	max	.004	2	.023	2	0	1	9.763e-4	4	NC	1	NC	1
346			min	0	15	-.025	3	-.135	4	0	1	NC	1	184.395	4
347		3	max	.004	2	.022	2	0	1	9.763e-4	4	NC	1	NC	1
348			min	0	15	-.023	3	-.123	4	0	1	NC	1	201.482	4
349		4	max	.004	2	.02	2	0	1	9.763e-4	4	NC	1	NC	1
350			min	0	15	-.022	3	-.112	4	0	1	NC	1	222.037	4
351		5	max	.003	2	.019	2	0	1	9.763e-4	4	NC	1	NC	1
352			min	0	15	-.02	3	-.1	4	0	1	NC	1	247.025	4
353		6	max	.003	2	.018	2	0	1	9.763e-4	4	NC	1	NC	1
354			min	0	15	-.019	3	-.089	4	0	1	NC	1	277.786	4
355		7	max	.003	2	.016	2	0	1	9.763e-4	4	NC	1	NC	1
356			min	0	15	-.018	3	-.078	4	0	1	NC	1	316.22	4
357		8	max	.003	2	.015	2	0	1	9.763e-4	4	NC	1	NC	1
358			min	0	15	-.016	3	-.068	4	0	1	NC	1	365.101	4
359		9	max	.002	2	.014	2	0	1	9.763e-4	4	NC	1	NC	1
360			min	0	15	-.015	3	-.058	4	0	1	NC	1	428.601	4
361		10	max	.002	2	.012	2	0	1	9.763e-4	4	NC	1	NC	1
362			min	0	15	-.013	3	-.048	4	0	1	NC	1	513.237	4
363		11	max	.002	2	.011	2	0	1	9.763e-4	4	NC	1	NC	1
364			min	0	15	-.012	3	-.039	4	0	1	NC	1	629.672	4
365		12	max	.002	2	.009	2	0	1	9.763e-4	4	NC	1	NC	1
366			min	0	15	-.01	3	-.031	4	0	1	NC	1	796.339	4
367		13	max	.001	2	.008	2	0	1	9.763e-4	4	NC	1	NC	1
368			min	0	15	-.009	3	-.024	4	0	1	NC	1	1047.429	4
369		14	max	.001	2	.007	2	0	1	9.763e-4	4	NC	1	NC	1
370			min	0	15	-.007	3	-.017	4	0	1	NC	1	1452.46	4
371		15	max	0	2	.005	2	0	1	9.763e-4	4	NC	1	NC	1
372			min	0	15	-.006	3	-.011	4	0	1	NC	1	2171.559	4
373		16	max	0	2	.004	2	0	1	9.763e-4	4	NC	1	NC	1
374			min	0	15	-.004	3	-.007	4	0	1	NC	1	3646.934	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	2	.003	2	0	1	9.763e-4	4	NC	1	NC	1
376			min	0	15	-.003	3	-.003	4	0	1	NC	1	7515.881	4
377		18	max	0	2	.001	2	0	1	9.763e-4	4	NC	1	NC	1
378			min	0	15	-.001	3	-.001	4	0	1	NC	1	NC	1
379		19	max	0	1	0	1	0	1	9.763e-4	4	NC	1	NC	1
380			min	0	1	0	1	0	1	0	1	NC	1	NC	1
381	M10	1	max	.007	2	.01	2	0	10	1.393e-3	4	NC	1	NC	1
382			min	-.01	3	-.016	3	-.442	4	1.243e-5	10	7425.377	2	174.136	4
383		2	max	.007	2	.009	2	0	10	1.426e-3	4	NC	1	NC	1
384			min	-.01	3	-.015	3	-.407	4	1.179e-5	10	8607.117	2	189.239	4
385		3	max	.006	2	.008	2	0	10	1.46e-3	4	NC	1	NC	1
386			min	-.009	3	-.015	3	-.372	4	1.114e-5	10	NC	1	207.113	4
387		4	max	.006	2	.006	2	0	10	1.493e-3	4	NC	1	NC	1
388			min	-.009	3	-.014	3	-.337	4	1.05e-5	10	NC	1	228.469	4
389		5	max	.006	2	.005	2	0	10	1.527e-3	4	NC	1	NC	1
390			min	-.008	3	-.014	3	-.303	4	9.851e-6	10	NC	1	254.273	4
391		6	max	.005	2	.004	2	0	12	1.56e-3	4	NC	1	NC	1
392			min	-.007	3	-.013	3	-.269	4	9.207e-6	10	NC	1	285.857	4
393		7	max	.005	2	.002	2	0	12	1.594e-3	4	NC	1	NC	1
394			min	-.007	3	-.013	3	-.237	4	8.562e-6	10	NC	1	325.1	4
395		8	max	.004	2	.001	2	0	12	1.627e-3	4	NC	1	NC	1
396			min	-.006	3	-.012	3	-.205	4	7.918e-6	10	NC	1	374.726	4
397		9	max	.004	2	0	2	0	12	1.66e-3	4	NC	1	NC	1
398			min	-.006	3	-.011	3	-.175	4	7.273e-6	10	NC	1	438.812	4
399		10	max	.004	2	0	2	0	12	1.694e-3	4	NC	1	NC	1
400			min	-.005	3	-.01	3	-.147	4	6.629e-6	10	NC	1	523.677	4
401		11	max	.003	2	0	2	0	12	1.727e-3	4	NC	1	NC	1
402			min	-.005	3	-.009	3	-.12	4	5.984e-6	10	NC	1	639.57	4
403		12	max	.003	2	-.001	2	0	12	1.761e-3	4	NC	1	NC	1
404			min	-.004	3	-.008	3	-.096	4	5.34e-6	10	NC	1	804.021	4
405		13	max	.002	2	-.002	15	0	12	1.794e-3	4	NC	1	NC	1
406			min	-.003	3	-.007	3	-.073	4	4.695e-6	10	NC	1	1049.134	4
407		14	max	.002	2	-.002	15	0	12	1.827e-3	4	NC	1	NC	1
408			min	-.003	3	-.006	3	-.054	4	4.051e-6	10	NC	1	1439.109	4
409		15	max	.002	2	-.001	15	0	12	1.861e-3	4	NC	1	NC	1
410			min	-.002	3	-.005	3	-.036	4	3.406e-6	10	NC	1	2118.602	4
411		16	max	.001	2	-.001	15	0	10	1.894e-3	4	NC	1	NC	1
412			min	-.002	3	-.004	3	-.022	4	2.762e-6	10	NC	1	3474.888	4
413		17	max	0	2	0	15	0	10	1.928e-3	4	NC	1	NC	1
414			min	-.001	3	-.003	4	-.011	4	2.117e-6	10	NC	1	6874.776	4
415		18	max	0	2	0	15	0	10	1.961e-3	4	NC	1	NC	1
416			min	0	3	-.002	4	-.004	4	1.472e-6	10	NC	1	NC	1
417		19	max	0	1	0	1	0	1	1.994e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	8.279e-7	10	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	-1.815e-7	10	NC	1	NC	1
420			min	0	1	0	1	0	1	-5.121e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.009	4	-1.243e-6	12	NC	1	NC	1
422			min	0	2	-.002	4	0	10	-6.057e-5	4	NC	1	9620.147	4
423		3	max	0	3	-.001	15	.018	4	3.925e-4	5	NC	1	NC	1
424			min	0	2	-.004	4	0	10	-2.286e-5	1	NC	1	5053.026	4
425		4	max	.001	3	-.002	15	.025	4	8.429e-4	5	NC	1	NC	1
426			min	-.001	2	-.006	4	0	10	-3.338e-5	1	NC	1	3532.989	4
427		5	max	.002	3	-.002	15	.032	4	1.294e-3	4	NC	1	NC	1
428			min	-.002	2	-.008	4	0	10	-4.389e-5	1	NC	1	2772.528	4
429		6	max	.002	3	-.003	15	.039	4	1.746e-3	4	NC	1	NC	1
430			min	-.002	2	-.01	4	0	10	-5.44e-5	1	9134.954	4	2313.669	4
431		7	max	.003	3	-.003	15	.045	4	2.197e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.002	2	-.012	4	0	1	-6.492e-5	1	7906.879	4	2003.368	4
433		8	max	.003	3	-.003	15	.051	4	2.649e-3	4	NC	2	NC	1
434			min	-.003	2	-.013	4	0	1	-7.543e-5	1	7151.435	4	1775.746	4
435		9	max	.004	3	-.003	15	.056	4	3.1e-3	4	NC	5	NC	1
436			min	-.003	2	-.014	4	0	1	-8.594e-5	1	6711.49	4	1597.695	4
437		10	max	.004	3	-.004	15	.062	4	3.552e-3	4	NC	5	NC	1
438			min	-.004	2	-.014	4	0	1	-9.646e-5	1	6511.476	4	1450.794	4
439		11	max	.005	3	-.004	15	.068	4	4.003e-3	4	NC	5	NC	1
440			min	-.004	2	-.014	4	0	1	-1.07e-4	1	6522.199	4	1324.108	4
441		12	max	.005	3	-.004	15	.074	4	4.455e-3	4	NC	5	NC	1
442			min	-.005	2	-.014	4	0	1	-1.175e-4	1	6749.626	4	1210.936	4
443		13	max	.006	3	-.003	15	.081	4	4.907e-3	4	NC	2	NC	1
444			min	-.005	2	-.013	4	-.001	1	-1.28e-4	1	7238.625	4	1107.18	4
445		14	max	.006	3	-.003	15	.089	4	5.358e-3	4	NC	1	NC	1
446			min	-.005	2	-.012	4	-.001	1	-1.385e-4	1	8095.617	4	1010.435	4
447		15	max	.006	3	-.003	15	.098	4	5.81e-3	4	NC	1	NC	1
448			min	-.006	2	-.01	4	-.002	1	-1.49e-4	1	9554.173	4	919.431	4
449		16	max	.007	3	-.002	15	.108	4	6.261e-3	4	NC	1	NC	1
450			min	-.006	2	-.008	4	-.002	1	-1.595e-4	1	NC	1	833.636	4
451		17	max	.007	3	-.002	15	.119	4	6.713e-3	4	NC	1	NC	1
452			min	-.007	2	-.006	4	-.003	1	-1.701e-4	1	NC	1	752.962	4
453		18	max	.008	3	-.001	10	.133	4	7.164e-3	4	NC	1	NC	1
454			min	-.007	2	-.004	3	-.003	1	-1.806e-4	1	NC	1	677.543	4
455		19	max	.008	3	0	2	.148	4	7.616e-3	4	NC	1	NC	1
456			min	-.007	2	-.003	3	-.004	1	-1.911e-4	1	NC	1	607.574	4
457	M12	1	max	.002	1	.007	2	.004	1	1.055e-3	5	NC	1	NC	2
458			min	0	12	-.009	3	-.148	4	-7.523e-5	1	NC	1	167.757	4
459		2	max	.002	1	.007	2	.004	1	1.055e-3	5	NC	1	NC	2
460			min	0	12	-.008	3	-.136	4	-7.523e-5	1	NC	1	181.88	4
461		3	max	.002	1	.006	2	.003	1	1.055e-3	5	NC	1	NC	2
462			min	0	12	-.008	3	-.125	4	-7.523e-5	1	NC	1	198.721	4
463		4	max	.001	1	.006	2	.003	1	1.055e-3	5	NC	1	NC	2
464			min	0	12	-.007	3	-.113	4	-7.523e-5	1	NC	1	218.98	4
465		5	max	.001	1	.006	2	.003	1	1.055e-3	5	NC	1	NC	2
466			min	0	12	-.007	3	-.102	4	-7.523e-5	1	NC	1	243.611	4
467		6	max	.001	1	.005	2	.002	1	1.055e-3	5	NC	1	NC	1
468			min	0	12	-.006	3	-.091	4	-7.523e-5	1	NC	1	273.932	4
469		7	max	.001	1	.005	2	.002	1	1.055e-3	5	NC	1	NC	1
470			min	0	12	-.006	3	-.08	4	-7.523e-5	1	NC	1	311.818	4
471		8	max	.001	1	.004	2	.002	1	1.055e-3	5	NC	1	NC	1
472			min	0	12	-.005	3	-.069	4	-7.523e-5	1	NC	1	360.001	4
473		9	max	0	1	.004	2	.002	1	1.055e-3	5	NC	1	NC	1
474			min	0	12	-.005	3	-.059	4	-7.523e-5	1	NC	1	422.593	4
475		10	max	0	1	.004	2	.001	1	1.055e-3	5	NC	1	NC	1
476			min	0	12	-.004	3	-.049	4	-7.523e-5	1	NC	1	506.021	4
477		11	max	0	1	.003	2	.001	1	1.055e-3	5	NC	1	NC	1
478			min	0	12	-.004	3	-.04	4	-7.523e-5	1	NC	1	620.793	4
479		12	max	0	1	.003	2	0	1	1.055e-3	5	NC	1	NC	1
480			min	0	12	-.003	3	-.032	4	-7.523e-5	1	NC	1	785.077	4
481		13	max	0	1	.002	2	0	1	1.055e-3	5	NC	1	NC	1
482			min	0	12	-.003	3	-.024	4	-7.523e-5	1	NC	1	1032.576	4
483		14	max	0	1	.002	2	0	1	1.055e-3	5	NC	1	NC	1
484			min	0	12	-.002	3	-.017	4	-7.523e-5	1	NC	1	1431.809	4
485		15	max	0	1	.002	2	0	1	1.055e-3	5	NC	1	NC	1
486			min	0	12	-.002	3	-.012	4	-7.523e-5	1	NC	1	2140.6	4
487		16	max	0	1	.001	2	0	1	1.055e-3	5	NC	1	NC	1
488			min	0	12	-.001	3	-.007	4	-7.523e-5	1	NC	1	3594.794	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	1.055e-3	5	NC	1	NC	1
490			min	0	12	0	3	-.003	4	-7.523e-5	1	NC	1	7408.078	4
491		18	max	0	1	0	2	0	1	1.055e-3	5	NC	1	NC	1
492			min	0	12	0	3	-.001	4	-7.523e-5	1	NC	1	NC	1
493		19	max	0	1	0	1	0	1	1.055e-3	5	NC	1	NC	1
494			min	0	1	0	1	0	1	-7.523e-5	1	NC	1	NC	1
495	M1	1	max	.01	3	.112	2	.466	4	5.887e-3	2	NC	1	NC	1
496			min	-.006	2	-.03	3	0	12	-1.423e-2	3	NC	1	NC	1
497		2	max	.01	3	.052	2	.453	4	4.432e-3	4	NC	4	NC	1
498			min	-.006	2	-.01	3	-.003	1	-7.043e-3	3	1913.373	2	NC	1
499		3	max	.01	3	.017	3	.439	4	7.961e-3	4	NC	5	NC	1
500			min	-.006	2	-.012	2	-.004	1	-9.621e-5	3	927.688	2	8327.915	5
501		4	max	.01	3	.058	3	.424	4	6.812e-3	4	NC	5	NC	1
502			min	-.006	2	-.083	2	-.004	1	-3.31e-3	3	590.724	2	6077.478	5
503		5	max	.01	3	.108	3	.409	4	5.798e-3	2	NC	5	NC	1
504			min	-.006	2	-.156	2	-.003	1	-6.524e-3	3	429.522	2	4949.972	5
505		6	max	.01	3	.16	3	.393	4	8.687e-3	2	NC	5	NC	1
506			min	-.006	2	-.227	2	-.001	1	-9.738e-3	3	340.257	2	4258.905	5
507		7	max	.009	3	.21	3	.377	4	1.158e-2	2	NC	15	NC	1
508			min	-.006	2	-.289	2	0	3	-1.295e-2	3	287.332	2	3751.12	4
509		8	max	.009	3	.252	3	.361	4	1.446e-2	2	NC	15	NC	1
510			min	-.006	2	-.339	2	0	12	-1.617e-2	3	255.923	2	3352.325	4
511		9	max	.009	3	.278	3	.345	4	1.639e-2	2	NC	15	NC	1
512			min	-.006	2	-.37	2	0	1	-1.659e-2	3	239.532	2	3066.011	4
513		10	max	.009	3	.288	3	.326	4	1.769e-2	2	NC	15	NC	1
514			min	-.006	2	-.38	2	0	10	-1.515e-2	3	234.758	2	2953.081	4
515		11	max	.009	3	.281	3	.306	4	1.899e-2	2	NC	15	NC	1
516			min	-.006	2	-.369	2	0	12	-1.371e-2	3	240.498	2	2965.242	4
517		12	max	.008	3	.257	3	.285	4	1.832e-2	2	NC	15	NC	1
518			min	-.005	2	-.337	2	0	1	-1.19e-2	3	258.81	2	3098.987	4
519		13	max	.008	3	.219	3	.26	4	1.469e-2	2	NC	15	NC	1
520			min	-.005	2	-.284	2	0	1	-9.525e-3	3	294.25	2	3558.543	4
521		14	max	.008	3	.171	3	.233	4	1.106e-2	2	NC	5	NC	1
522			min	-.005	2	-.219	2	0	12	-7.149e-3	3	354.847	2	4573.626	4
523		15	max	.008	3	.117	3	.205	4	7.429e-3	2	NC	5	NC	1
524			min	-.005	2	-.147	2	0	12	-4.773e-3	3	459.164	2	6801.281	4
525		16	max	.007	3	.06	3	.177	4	6.411e-3	4	NC	5	NC	1
526			min	-.005	2	-.074	2	0	12	-2.397e-3	3	652.332	2	NC	1
527		17	max	.007	3	.006	3	.151	4	7.47e-3	4	NC	5	NC	1
528			min	-.005	2	-.007	2	0	12	-2.111e-5	3	1065.234	2	NC	1
529		18	max	.007	3	.049	2	.128	4	5.239e-3	2	NC	4	NC	1
530			min	-.005	2	-.043	3	0	12	-2.153e-3	3	2260.14	2	NC	1
531		19	max	.007	3	.099	2	.109	4	1.051e-2	2	NC	1	NC	1
532			min	-.005	2	-.089	3	0	1	-4.391e-3	3	NC	1	NC	1
533	M5	1	max	.031	3	.204	2	.466	4	0	1	NC	1	NC	1
534			min	-.022	2	-.006	3	0	1	-9.334e-6	4	NC	1	NC	1
535		2	max	.031	3	.09	2	.456	4	4.085e-3	4	NC	5	NC	1
536			min	-.022	2	.002	15	0	1	0	1	1024.298	2	NC	1
537		3	max	.031	3	.052	3	.443	4	8.053e-3	4	NC	5	NC	1
538			min	-.022	2	-.038	2	0	1	0	1	481.323	2	6864.398	4
539		4	max	.03	3	.138	3	.428	4	6.56e-3	4	NC	5	NC	1
540			min	-.022	2	-.191	2	0	1	0	1	294.136	2	5349.417	4
541		5	max	.029	3	.256	3	.411	4	5.067e-3	4	NC	15	NC	1
542			min	-.021	2	-.356	2	0	1	0	1	206.765	2	4631.958	4
543		6	max	.029	3	.388	3	.394	4	3.574e-3	4	8563.133	15	NC	1
544			min	-.021	2	-.521	2	0	1	0	1	159.674	2	4185.913	4
545		7	max	.028	3	.517	3	.377	4	2.082e-3	4	7071.393	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.02	2	-.671	2	0	1	0	1	132.372	2	3810.882	4
547		8	max	.027	3	.624	3	.361	4	5.89e-4	4	6206.205	15	NC	1
548			min	-.02	2	-.791	2	0	1	0	1	116.453	2	3412.878	4
549		9	max	.027	3	.693	3	.345	4	0	1	5763.357	15	NC	1
550			min	-.02	2	-.867	2	0	1	-7.029e-6	5	108.273	2	3056.573	4
551		10	max	.026	3	.717	3	.326	4	0	1	5630.135	15	NC	1
552			min	-.019	2	-.893	2	0	1	-6.836e-6	5	105.896	2	2973.797	4
553		11	max	.026	3	.697	3	.306	4	0	1	5763.872	15	NC	1
554			min	-.019	2	-.867	2	0	1	-6.642e-6	5	108.753	2	3002.91	4
555		12	max	.025	3	.636	3	.285	4	5.253e-4	4	6207.385	15	NC	1
556			min	-.019	2	-.786	2	0	1	0	1	118.051	2	3043.746	4
557		13	max	.024	3	.539	3	.261	4	1.857e-3	4	7073.688	15	NC	1
558			min	-.019	2	-.658	2	0	1	0	1	136.571	2	3491.84	4
559		14	max	.024	3	.416	3	.232	4	3.188e-3	4	8567.45	15	NC	1
560			min	-.018	2	-.499	2	0	1	0	1	169.258	2	4724.193	4
561		15	max	.023	3	.281	3	.203	4	4.519e-3	4	NC	15	NC	1
562			min	-.018	2	-.328	2	0	1	0	1	227.965	2	8135.233	4
563		16	max	.022	3	.144	3	.173	4	5.851e-3	4	NC	5	NC	1
564			min	-.018	2	-.162	2	0	1	0	1	342.991	2	NC	1
565		17	max	.022	3	.017	3	.146	4	7.182e-3	4	NC	5	NC	1
566			min	-.017	2	-.02	2	0	1	0	1	604.912	2	NC	1
567		18	max	.022	3	.082	2	.125	4	3.645e-3	4	NC	5	NC	1
568			min	-.017	2	-.089	3	0	1	0	1	1346.341	3	NC	1
569		19	max	.022	3	.164	2	.109	4	0	1	NC	1	NC	1
570			min	-.017	2	-.183	3	0	1	-5.775e-6	4	NC	1	NC	1
571	M9	1	max	.01	3	.112	2	.466	4	1.423e-2	3	NC	1	NC	1
572			min	-.006	2	-.03	3	0	1	-5.887e-3	2	NC	1	NC	1
573		2	max	.01	3	.052	2	.455	4	7.043e-3	3	NC	4	NC	1
574			min	-.006	2	-.01	3	0	10	-2.887e-3	2	1913.373	2	NC	1
575		3	max	.01	3	.017	3	.442	4	8.029e-3	4	NC	5	NC	1
576			min	-.006	2	-.012	2	0	10	-2.39e-5	10	927.688	2	7244.957	4
577		4	max	.01	3	.058	3	.427	4	6.379e-3	5	NC	5	NC	1
578			min	-.006	2	-.083	2	0	10	-2.909e-3	2	590.724	2	5513.612	4
579		5	max	.01	3	.108	3	.411	4	6.524e-3	3	NC	5	NC	1
580			min	-.006	2	-.156	2	0	10	-5.798e-3	2	429.522	2	4670.101	4
581		6	max	.01	3	.16	3	.394	4	9.738e-3	3	NC	5	NC	1
582			min	-.006	2	-.227	2	0	10	-8.687e-3	2	340.257	2	4150.173	4
583		7	max	.009	3	.21	3	.377	4	1.295e-2	3	NC	15	NC	1
584			min	-.006	2	-.289	2	0	1	-1.158e-2	2	287.332	2	3750.912	4
585		8	max	.009	3	.252	3	.361	4	1.617e-2	3	NC	15	NC	1
586			min	-.006	2	-.339	2	0	1	-1.446e-2	2	255.923	2	3378.854	4
587		9	max	.009	3	.278	3	.345	4	1.659e-2	3	NC	15	NC	1
588			min	-.006	2	-.37	2	0	12	-1.639e-2	2	239.532	2	3058.021	4
589		10	max	.009	3	.288	3	.326	4	1.515e-2	3	NC	15	NC	1
590			min	-.006	2	-.38	2	0	1	-1.769e-2	2	234.758	2	2954.206	4
591		11	max	.009	3	.281	3	.306	4	1.371e-2	3	NC	15	NC	1
592			min	-.006	2	-.369	2	0	1	-1.899e-2	2	240.498	2	2974.507	4
593		12	max	.008	3	.257	3	.285	4	1.19e-2	3	NC	15	NC	1
594			min	-.005	2	-.337	2	0	12	-1.832e-2	2	258.81	2	3076.799	4
595		13	max	.008	3	.219	3	.26	4	9.525e-3	3	NC	15	NC	1
596			min	-.005	2	-.284	2	0	10	-1.469e-2	2	294.25	2	3555.202	4
597		14	max	.008	3	.171	3	.232	4	7.149e-3	3	NC	5	NC	1
598			min	-.005	2	-.219	2	-.001	1	-1.106e-2	2	354.847	2	4693.369	5
599		15	max	.008	3	.117	3	.203	4	4.773e-3	3	NC	5	NC	1
600			min	-.005	2	-.147	2	-.002	1	-7.429e-3	2	459.164	2	7348.808	5
601		16	max	.007	3	.06	3	.175	4	5.862e-3	5	NC	5	NC	1
602			min	-.005	2	-.074	2	-.004	1	-3.8e-3	2	652.332	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.007	3	.006	3	.148	4	7.301e-3	4	NC	5	NC	1
604			min	-.005	2	-.007	2	-.004	1	-2.816e-4	1	1065.234	2	NC	1
605		18	max	.007	3	.049	2	.126	4	3.607e-3	5	NC	4	NC	1
606			min	-.005	2	-.043	3	-.003	1	-5.239e-3	2	2260.14	2	NC	1
607		19	max	.007	3	.099	2	.109	4	4.391e-3	3	NC	1	NC	1
608			min	-.005	2	-.089	3	0	12	-1.051e-2	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

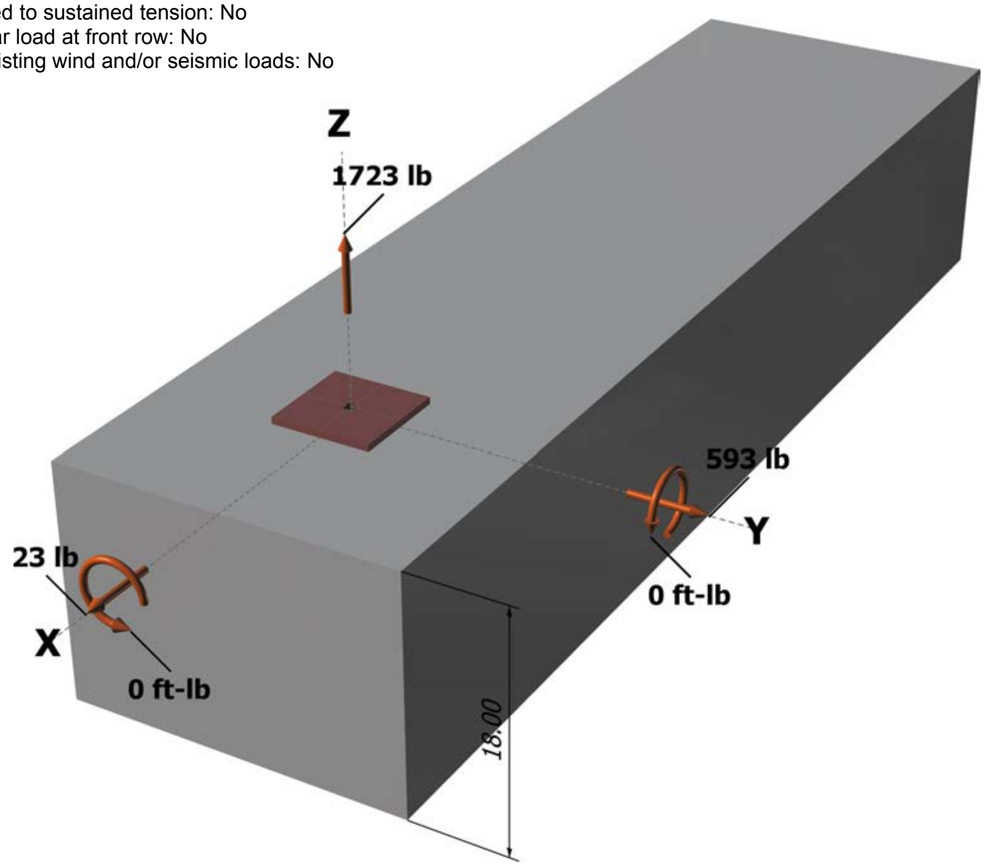
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>

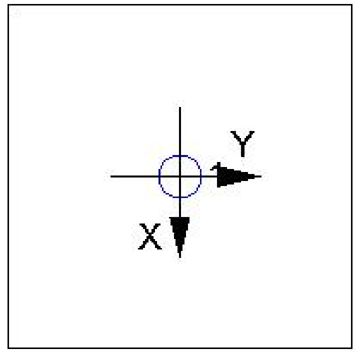
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1723.0	23.0	593.0	593.4
Sum	1723.0	23.0	593.0	593.4

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1723
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi \, (A_{Nc} / A_{Nco}) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi \, (A_{Na} / A_{Na0}) \Psi_{ed,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\,\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\,\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	1723	6071	0.28	Pass
Concrete breakout	1723	5710	0.30	Pass
Adhesive	**1723**	**5365**	**0.32**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**593**	**3156**	**0.19**	**Pass (Governs)**
T Concrete breakout y+	593	3934	0.15	Pass
T Concrete breakout x+	23	3018	0.01	Pass
|| Concrete breakout y+	23	8508	0.00	Pass
|| Concrete breakout x+	593	6875	0.09	Pass
Concrete breakout, combined	-	-	0.15	Pass
Pryout	593	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.32	0.00	32.1 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

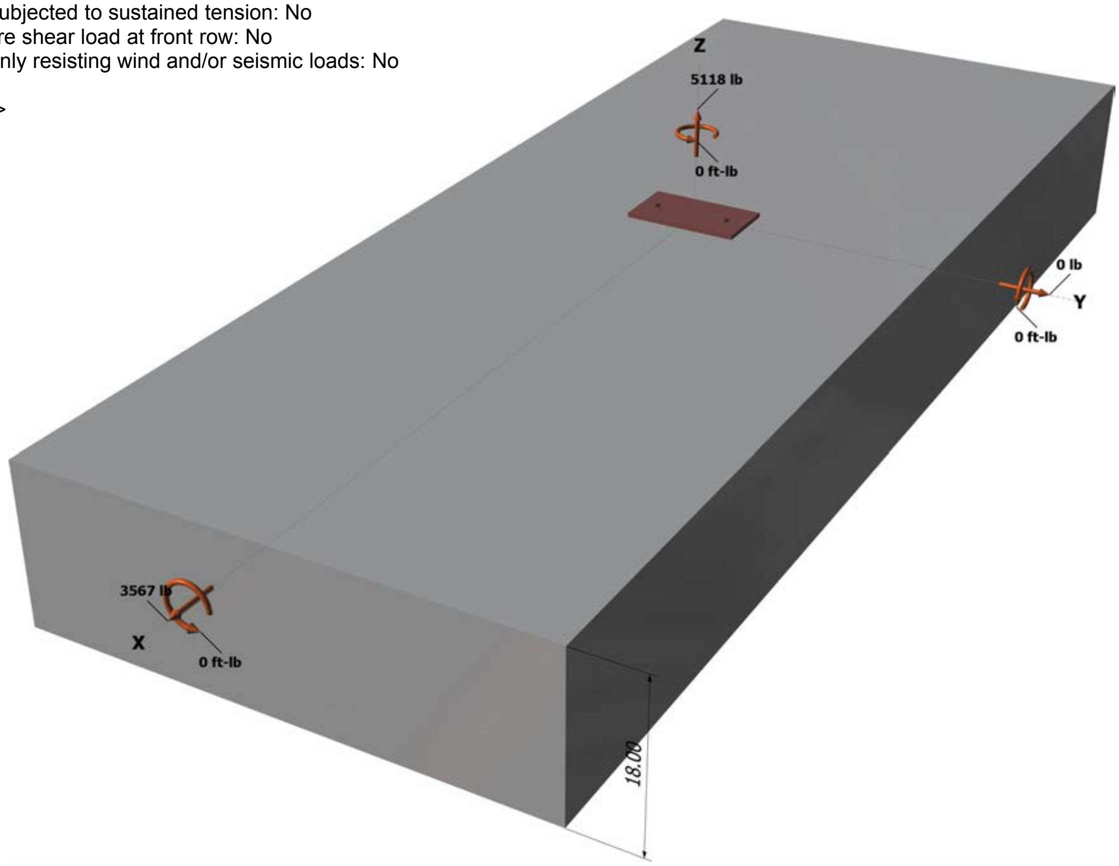
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

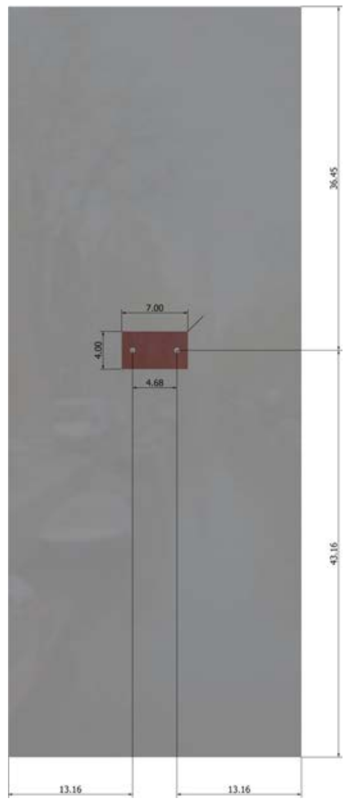
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



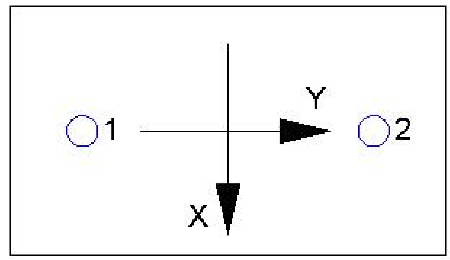
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2559.0	1783.5	0.0	1783.5
2	2559.0	1783.5	0.0	1783.5
Sum	5118.0	3567.0	0.0	3567.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 5118
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
408.24	324.00	1.000	1.000	1.00	1.000	12492	0.65	10231

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\ (A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
558.00	648.00	1.000	0.919	1.000	1.000	15593	0.70	8641

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	13.16	17908

$\phi V_{cbx} = \phi\ (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
710.64	779.34	1.000	1.000	1.000	17908	0.70	22862

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi \min|k_{cp}N_{ag}\ ;\ k_{cp}N_{cbg}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
408.24	324.00	1.000	1.000	1.000	1.000	12492	15740	0.70

ϕV_{cpg} (lb)
20601

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	2559	6071	0.42	Pass
Concrete breakout	5118	10231	0.50	Pass
Adhesive	**5118**	**8093**	**0.63**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**1784**	**3156**	**0.57**	**Pass (Governs)**
T Concrete breakout x+	3567	8641	0.41	Pass
|| Concrete breakout y-	1784	22862	0.08	Pass
Pryout	3567	20601	0.17	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.63	0.57	119.8 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.