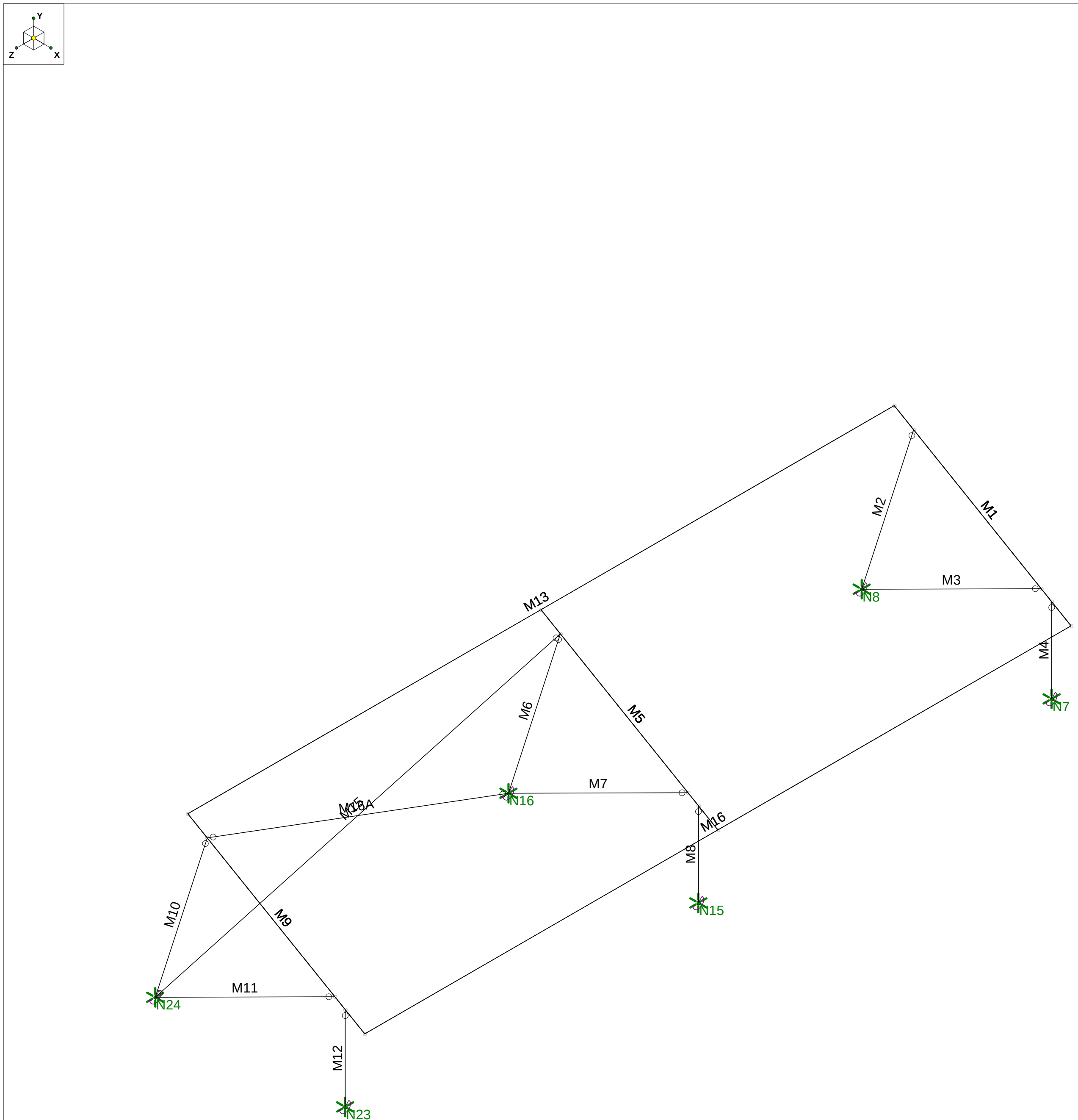


Schletter, Inc.		30ÁTilt w/o Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

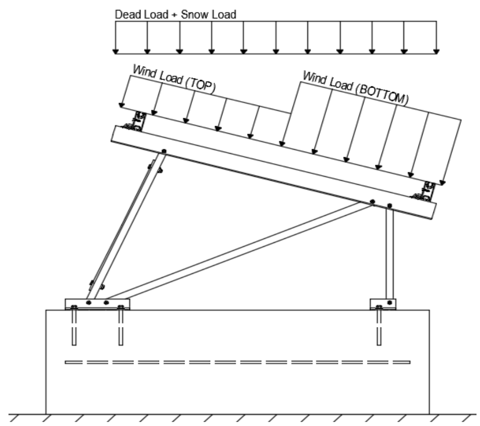
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 1
Module Tilt = 30°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	16.49	psf	*(ASCE 7-10, Eq. 7.4-1)*
I_s =	1.00		
C_s =	0.73		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads
Design Wind Speed, V = 140 mph — Exposure Category = C
Height ≤ 15 ft — Importance Category = II

Peak Velocity Pressure, q_z = 30.77 psf — *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.15	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.85	
$Cf-_{TOP}$	=	-2.3	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.1	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads - N/A

S_S =	0.00	R =	1.25
S_{DS} =	0.00	C_S =	0
S_1 =	0.00	ρ =	1.3
S_{D1} =	0.00	Ω =	1.25
T_a =	0.00	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M13	Top
M16	Bottom

Girders	Location
M1	Outer
M5	Inner
M9	Outer

Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

Diagonal Struts	Location
M3	Outer
M7	Inner
M11	Outer

Rear Struts	Location
M2	Outer
M6	Inner
M10	Outer

Bracing
M15
M16A

Front Reactions	Location
N7	Outer
N15	Inner
N23	Outer

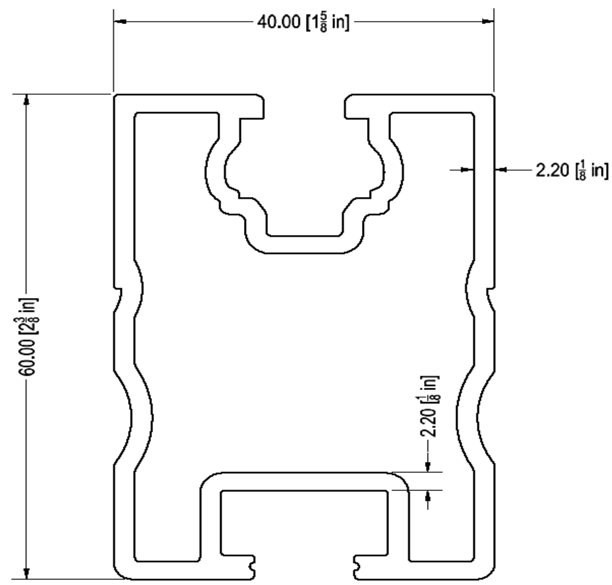
Rear Reactions	Location
N8	Outer
N16	Inner
N24	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

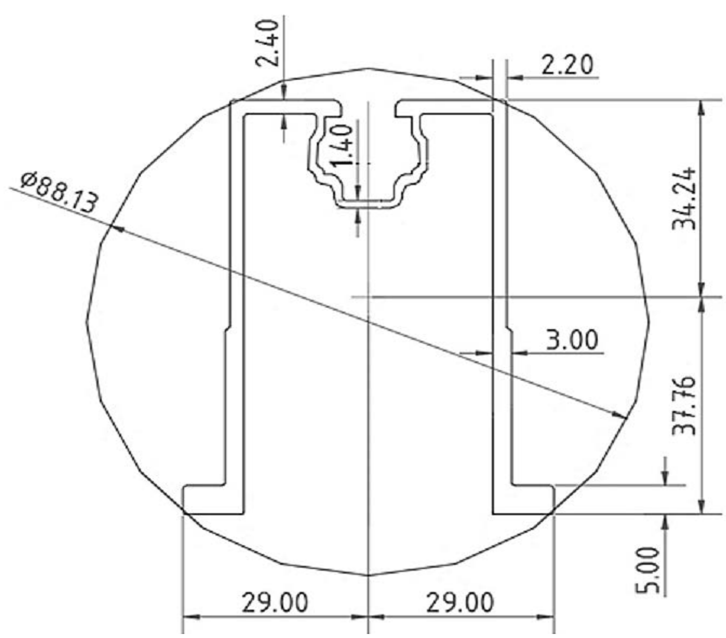
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	54	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.52	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	0.444	k-ft
M_z =	0.041	k-ft
$M_{y\ allowable}$ =	1.256	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	40%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

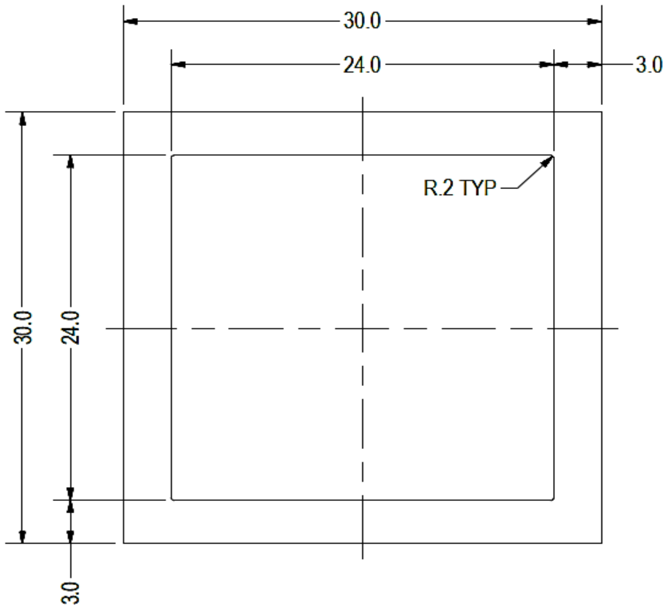
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.66	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	0.540	k-ft
M_z =	0.000	k-ft
P_n =	0.280	k
$M_{y\ allowable}$ =	1.455	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	39%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

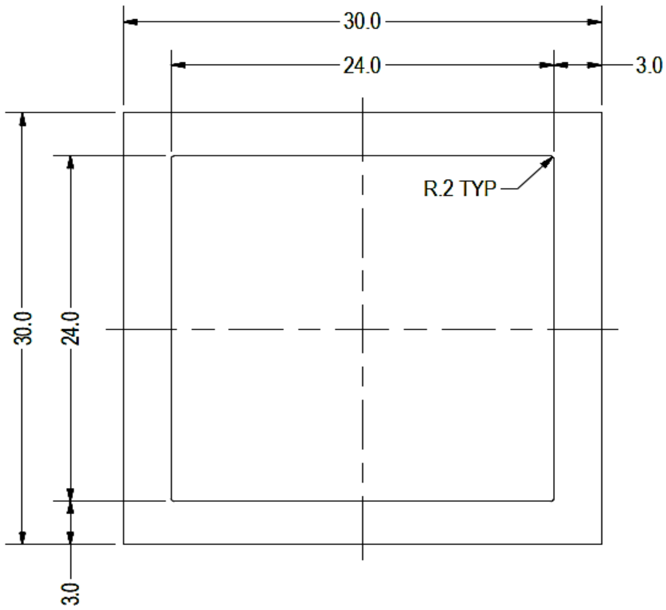
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.806	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	7%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

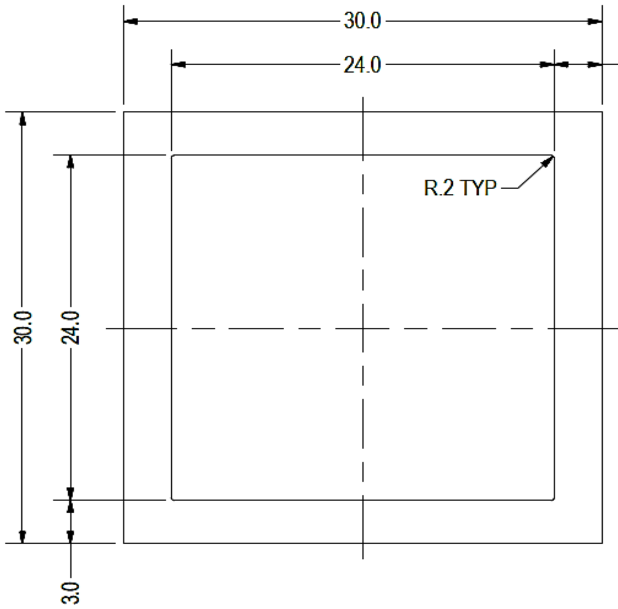
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.595	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	16%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

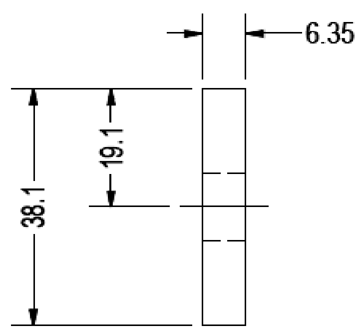
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	39.29	in
$\Phi F_{ty\ AXIAL}$ =	10.06	ksi
$\Phi F_{ty\ BENDING}$ =	30.09	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.666	k
$M_{y\ allowable}$ =	0.408	k-ft
$M_{z\ allowable}$ =	0.408	k-ft
$P_{n\ allowable}$ =	5.050	k
Utilization =	13%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.002	k-ft
P_n =	0.095	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	5%	



A cross brace kit is required every 38 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

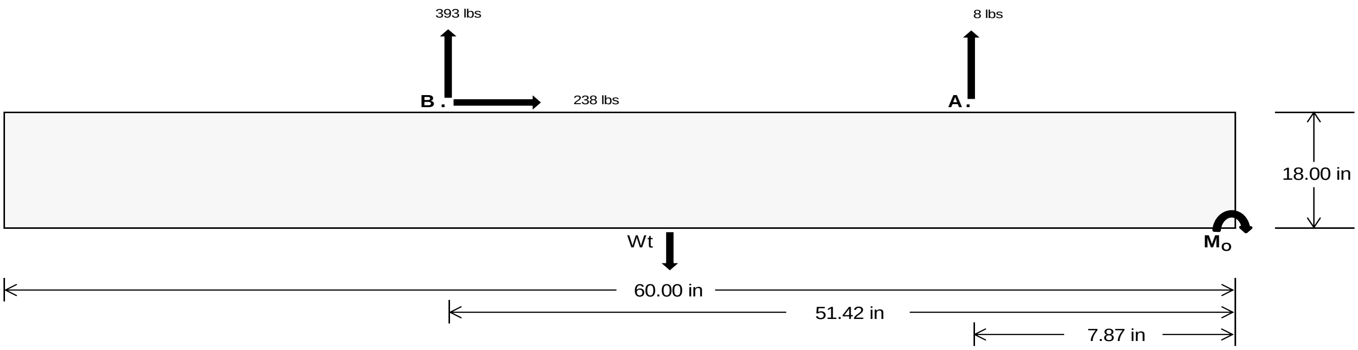
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	38.39	1708.01	k
Compressive Load =	1047.57	1154.93	k
Lateral Load =	1.70	1031.85	k
Moment (Weak Axis) =	0.00	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties
Weight of Concrete = 145 pcf
Compressive Strength = 2500 psi
Yield Strength = 60000 psi

Footing Reinforcement
Use fiber reinforcing with (1) #5 rebar.

Overturning Check
M_O = 24568.8 in-lbs
Resisting Force Required = 818.96 lbs
S.F. = 1.67
Weight Required = 1364.93 lbs
Minimum Width = 20 in in
Weight Provided = 1812.50 lbs

A minimum 60in long x 20in wide x 18in tall ballast foundation is required to resist overturning.

Sliding
Force = 238.02 lbs
Friction = 0.4
Weight Required = 595.05 lbs
Resisting Weight = 1812.50 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 20in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion
Sliding Force = 238.02 lbs
Cohesion = 130 psf
Area = 8.33 ft^2
Resisting = 906.25 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 20in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key
Additional Force = 0 lbs
Lateral Bearing Pressure = 200 psf/ft
Required Depth = 0.00 ft
f'_c = 2500 psi
Length = 8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	20 in	21 in	22 in	23 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.67 ft) =	1813 lbs	1903 lbs	1994 lbs	2084 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	20 in	21 in	22 in	23 in	20 in	21 in	22 in	23 in	20 in	21 in	22 in	23 in	20 in	21 in	22 in	23 in
F_A	361 lbs	361 lbs	361 lbs	361 lbs	372 lbs	372 lbs	372 lbs	372 lbs	517 lbs	517 lbs	517 lbs	517 lbs	-15 lbs	-15 lbs	-15 lbs	-15 lbs
F_B	246 lbs	246 lbs	246 lbs	246 lbs	486 lbs	486 lbs	486 lbs	486 lbs	526 lbs	526 lbs	526 lbs	526 lbs	-787 lbs	-787 lbs	-787 lbs	-787 lbs
F_V	36 lbs	36 lbs	36 lbs	36 lbs	428 lbs	428 lbs	428 lbs	428 lbs	345 lbs	345 lbs	345 lbs	345 lbs	-476 lbs	-476 lbs	-476 lbs	-476 lbs
P_{total}	2419 lbs	2510 lbs	2601 lbs	2691 lbs	2671 lbs	2762 lbs	2852 lbs	2943 lbs	2855 lbs	2946 lbs	3036 lbs	3127 lbs	286 lbs	340 lbs	394 lbs	449 lbs
M	280 lbs-ft	280 lbs-ft	280 lbs-ft	280 lbs-ft	461 lbs-ft	461 lbs-ft	461 lbs-ft	461 lbs-ft	532 lbs-ft	532 lbs-ft	532 lbs-ft	532 lbs-ft	662 lbs-ft	662 lbs-ft	662 lbs-ft	662 lbs-ft
e	0.12 ft	0.11 ft	0.11 ft	0.10 ft	0.17 ft	0.17 ft	0.16 ft	0.16 ft	0.19 ft	0.18 ft	0.18 ft	0.17 ft	2.32 ft	1.95 ft	1.68 ft	1.48 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	250.0 psf	248.5 psf	247.1 psf	245.8 psf	254.2 psf	252.4 psf	250.8 psf	249.4 psf	266.0 psf	263.7 psf	261.6 psf	259.7 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	330.6 psf	325.2 psf	320.3 psf	315.9 psf	386.9 psf	378.8 psf	371.5 psf	364.8 psf	419.2 psf	409.6 psf	400.9 psf	392.9 psf	627.1 psf	234.4 psf	174.7 psf	152.4 psf

Maximum Bearing Pressure = 627 psf
Allowable Bearing Pressure = 1500 psf

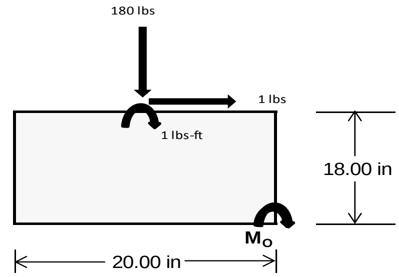
Use a 60in long x 20in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Weak Side Design

Overturning Check

M_O = 147.9 ft-lbs
Resisting Force Required = 177.52 lbs
S.F. = 1.67
Weight Required = 295.87 lbs
Minimum Width = 20 in in
Weight Provided = 1812.50 lbs

A minimum 60in long x 20in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	20 in			20 in			20 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	57 lbs	140 lbs	54 lbs	180 lbs	504 lbs	177 lbs	17 lbs	41 lbs	16 lbs
F_V	0 lbs	0 lbs	0 lbs	1 lbs	0 lbs	0 lbs	0 lbs	0 lbs	0 lbs
P_{total}	2301 lbs	2384 lbs	2298 lbs	2316 lbs	2640 lbs	2313 lbs	673 lbs	697 lbs	672 lbs
M	0 lbs-ft	0 lbs-ft	0 lbs-ft	2 lbs-ft	1 lbs-ft	1 lbs-ft	0 lbs-ft	0 lbs-ft	0 lbs-ft
e	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft
L/6	0.28 ft	1.67 ft	1.67 ft	1.66 ft	1.67 ft	1.67 ft	1.67 ft	1.67 ft	1.67 ft
f_{min}	276.0 sqft	286.0 sqft	275.7 sqft	277.0 sqft	316.5 sqft	277.3 sqft	80.7 sqft	83.6 sqft	80.6 sqft
f_{max}	276.3 psf	286.2 psf	275.8 psf	278.9 psf	317.1 psf	277.8 psf	80.8 psf	83.7 psf	80.7 psf

Maximum Bearing Pressure = 317 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 20in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 20in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

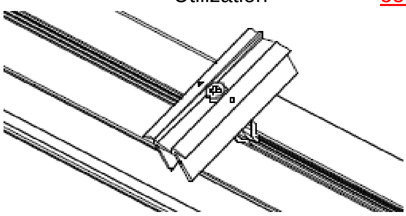
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

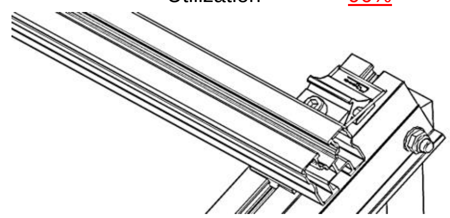
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.665	k
Allowable Uplift =	1.214	k
Utilization =	55%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	1.067	k
Allowable Uplift =	1.116	k
Utilization =	96%	



6.2 Bolted Connections

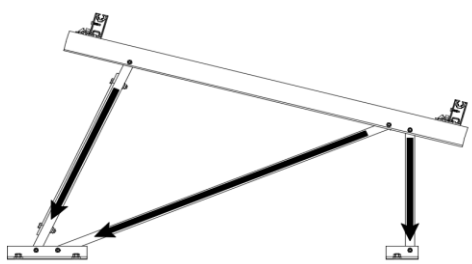
The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	0.806	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	14%	

Rear Strut		
Maximum Axial Load =	1.092	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	19%	

Diagonal Strut		
Maximum Axial Load =	0.595	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	10%	

Bracing		
Maximum Axial Load =	0.095	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	1%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

7.1 Seismic Drift - N/A

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

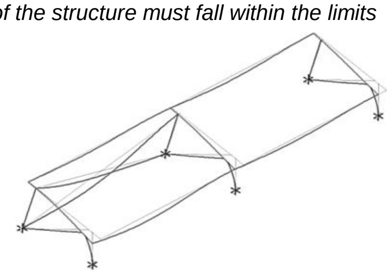
Mean Height, h_{sx} = 32.32 in

Allowable Story Drift for All Other Structures, Δ = { $0.020h_{sx}$; 0.646 in

Max Drift, Δ_{MAX} = 0.009 in

N/A

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus**

Strong Axis:

3.4.14

L_b = 54.00 in

J = 0.255

140.613

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.5 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 54.00 in

J = 0.255

146.018

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 30

Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 29.5 ksi

Ix = 250988 mm^4

0.603 in^4

y = 30 mm

Sx = 0.511 in^3

$M_{max}St$ = 1.256 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 20

Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi

Iy = 120291 mm^4

0.289 in^4

x = 20 mm

Sy = 0.367 in^3

$M_{max}Wk$ = 0.871 k-ft

Compression

3.4.9

b/t = 7.4

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 23.9

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.47 ksi

A = 578.06 mm^2

0.90 in^2

P_{max} = 25.51 kips

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in
ry = 1.374
Cb = 1.25
21.9891

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2
φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))
φF_L= 29.7 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in
ry = 1.374
Cb = 1.25
24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2
φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))
φF_L= 29.7 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7
F_{UT}= (φbk2*√(BpE))/(5.1b/t)
F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
F_{ST}= φb[Bp-1.6Dp*b/t]
F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.7 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.455 k-ft

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.8

b/t = 24.46
S1 = 3.83
S2 = 10.30
φF_L= (φck2*√(BpE))/(5.1b/t)
φF_L= 10.4 ksi

3.4.9

b/t = 4.29
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 24.46
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.9.1

b/t = 24.46
t = 2.6
ds = 6.05
rs = 3.49
S = 21.70
ρst = 0.22
F_{UT}= 10.43
F_{ST}= 28.24
φF_L= Fut + (Fst - Fut)ρst < Fst
φF_L= 14.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 14.29 ksi
A = 576.21 mm^2
0.89 in^2
P_{max} = 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 31.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.2 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.423 k-ft

Compression

3.4.7

$\lambda =$ 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.83792

$\varphi F_L = \varphi cc(Bc\text{-}Dc^*\lambda)$

$\varphi F_L =$ 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 24.52 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 12.31 kips

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in³

M_{max}St = 0.404 k-ft

Weak Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in³

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

$\lambda =$ 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.85841

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

$\varphi F_L =$ 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 7.60 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 39.29 in

J = 0.16

103.073

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.1 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.1 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in³

M_{max}St = 0.408 k-ft

Weak Axis:

3.4.14

L_b = 39.29 in

J = 0.16

103.073

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.1

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in³

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

$\lambda =$ 1.68476

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.81587

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

$\varphi F_L =$ 10.0603 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 10.06 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 5.05 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL								

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-45.999	-45.999	0	0
2	M16	Y	-45.999	-45.999	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-98.692	-98.692	0	0
2	M16	y	-158.766	-158.766	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	197.385	197.385	0	0
2	M16	y	94.402	94.402	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	217.196	2	275.976	2	0	10	0	15	0	1	0	1
2		min	-259.414	3	-410.47	3	-.134	3	0	3	0	1	0	1
3	N7	max	.002	3	295.208	1	-.026	10	0	15	0	1	0	1
4		min	-.13	2	3.536	12	-.633	1	-.001	1	0	1	0	1
5	N15	max	0	15	805.821	1	.22	9	0	1	0	1	0	1
6		min	-1.307	2	-29.53	3	-.616	3	0	3	0	1	0	1
7	N16	max	725.737	2	888.406	2	0	2	0	9	0	1	0	1
8		min	-793.732	3	-1313.854	3	-75.448	3	0	3	0	1	0	1
9	N23	max	.002	3	295.252	1	1.125	1	.002	1	0	1	0	1
10		min	-.13	2	3.922	12	.026	10	0	10	0	1	0	1
11	N24	max	217.196	2	278.574	2	76.07	3	0	1	0	1	0	1
12		min	-259.856	3	-409.334	3	0	10	0	3	0	1	0	1
13	Totals:	max	1158.561	2	2664.71	2	0	2						
14		min	-1313.042	3	-2154.67	3	0	9						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	210.341	1	.655	4	.171	1	0	10	0	15	0	1
2			min	-352.696	3	.154	15	-.065	3	0	1	0	1	0	1
3		2	max	210.466	1	.604	4	.171	1	0	10	0	15	0	15
4			min	-352.602	3	.142	15	-.065	3	0	1	0	1	0	4
5		3	max	210.592	1	.553	4	.171	1	0	10	0	15	0	15
6			min	-352.507	3	.13	15	-.065	3	0	1	0	3	0	4
7		4	max	210.718	1	.502	4	.171	1	0	10	0	9	0	15
8			min	-352.413	3	.118	15	-.065	3	0	1	0	3	0	4
9		5	max	210.844	1	.451	4	.171	1	0	10	0	9	0	15
10			min	-352.319	3	.106	15	-.065	3	0	1	0	3	0	4
11		6	max	210.97	1	.4	4	.171	1	0	10	0	1	0	15
12			min	-352.224	3	.094	15	-.065	3	0	1	0	3	0	4
13		7	max	211.096	1	.349	4	.171	1	0	10	0	1	0	15
14			min	-352.13	3	.082	15	-.065	3	0	1	0	3	0	4
15		8	max	211.222	1	.297	4	.171	1	0	10	0	1	0	15
16			min	-352.035	3	.07	15	-.065	3	0	1	0	3	0	4
17		9	max	211.348	1	.246	4	.171	1	0	10	0	1	0	15
18			min	-351.941	3	.058	15	-.065	3	0	1	0	3	0	4
19		10	max	211.473	1	.195	4	.171	1	0	10	0	1	0	15
20			min	-351.847	3	.046	15	-.065	3	0	1	0	3	0	4
21		11	max	211.599	1	.144	4	.171	1	0	10	0	1	0	15
22			min	-351.752	3	.034	15	-.065	3	0	1	0	3	0	4
23		12	max	211.725	1	.102	2	.171	1	0	10	0	1	0	15
24			min	-351.658	3	.014	12	-.065	3	0	1	0	3	0	4
25		13	max	211.851	1	.062	2	.171	1	0	10	0	1	0	15
26			min	-351.563	3	-.012	3	-.065	3	0	1	0	3	0	4
27		14	max	211.977	1	.022	2	.171	1	0	10	0	1	0	15
28			min	-351.469	3	-.042	3	-.065	3	0	1	0	3	0	4
29		15	max	212.103	1	-.014	15	.171	1	0	10	0	1	0	15
30			min	-351.375	3	-.072	3	-.065	3	0	1	0	3	0	4
31		16	max	212.229	1	-.026	15	.171	1	0	10	0	1	0	15
32			min	-351.28	3	-.112	4	-.065	3	0	1	0	3	0	4
33		17	max	212.354	1	-.038	15	.171	1	0	10	0	1	0	15
34			min	-351.186	3	-.163	4	-.065	3	0	1	0	3	0	4
35		18	max	212.48	1	-.05	15	.171	1	0	10	0	1	0	15
36			min	-351.091	3	-.214	4	-.065	3	0	1	0	3	0	4
37		19	max	212.606	1	-.062	15	.171	1	0	10	0	1	0	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
38			min	-350.997	3	-.265	4	-.065	3	0	1	0	3	0	4
39	M3	1	max	174.56	2	1.759	4	-.008	10	0	15	0	1	0	4
40			min	-170.988	3	.414	15	-.197	1	0	1	0	10	0	15
41		2	max	174.491	2	1.582	4	-.008	10	0	15	0	1	0	2
42			min	-171.04	3	.372	15	-.197	1	0	1	0	10	0	12
43		3	max	174.422	2	1.405	4	-.008	10	0	15	0	1	0	2
44			min	-171.092	3	.33	15	-.197	1	0	1	0	10	0	3
45		4	max	174.352	2	1.228	4	-.008	10	0	15	0	1	0	15
46			min	-171.144	3	.289	15	-.197	1	0	1	0	10	0	4
47		5	max	174.283	2	1.051	4	-.008	10	0	15	0	1	0	15
48			min	-171.196	3	.247	15	-.197	1	0	1	0	10	0	4
49		6	max	174.214	2	.874	4	-.008	10	0	15	0	1	0	15
50			min	-171.248	3	.206	15	-.197	1	0	1	0	10	0	4
51		7	max	174.144	2	.698	4	-.008	10	0	15	0	1	0	15
52			min	-171.3	3	.164	15	-.197	1	0	1	0	10	0	4
53		8	max	174.075	2	.521	4	-.008	10	0	15	0	1	0	15
54			min	-171.352	3	.123	15	-.197	1	0	1	0	10	-.001	4
55		9	max	174.006	2	.344	4	-.008	10	0	15	0	1	0	15
56			min	-171.404	3	.081	15	-.197	1	0	1	0	10	-.001	4
57		10	max	173.936	2	.167	4	-.008	10	0	15	0	1	0	15
58			min	-171.456	3	.039	15	-.197	1	0	1	0	10	-.001	4
59		11	max	173.867	2	.017	2	-.008	10	0	15	0	1	0	15
60			min	-171.508	3	-.037	3	-.197	1	0	1	0	10	-.001	4
61		12	max	173.798	2	-.044	15	-.008	10	0	15	0	1	0	15
62			min	-171.56	3	-.187	4	-.197	1	0	1	0	10	-.001	4
63		13	max	173.728	2	-.085	15	-.008	10	0	15	0	1	0	15
64			min	-171.612	3	-.363	4	-.197	1	0	1	0	10	-.001	4
65		14	max	173.659	2	-.127	15	-.008	10	0	15	0	1	0	15
66			min	-171.664	3	-.54	4	-.197	1	0	1	0	10	-.001	4
67		15	max	173.59	2	-.168	15	-.008	10	0	15	0	1	0	15
68			min	-171.716	3	-.717	4	-.197	1	0	1	0	10	0	4
69		16	max	173.52	2	-.21	15	-.008	10	0	15	0	9	0	15
70			min	-171.768	3	-.894	4	-.197	1	0	1	0	2	0	4
71		17	max	173.451	2	-.252	15	-.008	10	0	15	0	15	0	15
72			min	-171.819	3	-1.071	4	-.197	1	0	1	0	1	0	4
73		18	max	173.382	2	-.293	15	-.008	10	0	15	0	15	0	15
74			min	-171.871	3	-1.248	4	-.197	1	0	1	0	1	0	4
75		19	max	173.312	2	-.335	15	-.008	10	0	15	0	15	0	1
76			min	-171.923	3	-1.424	4	-.197	1	0	1	0	1	0	1
77	M4	1	max	294.043	1	0	1	-.027	15	0	1	0	3	0	1
78			min	2.953	12	0	1	-.666	1	0	1	0	2	0	1
79		2	max	294.108	1	0	1	-.027	15	0	1	0	15	0	1
80			min	2.986	12	0	1	-.666	1	0	1	0	1	0	1
81		3	max	294.173	1	0	1	-.027	15	0	1	0	15	0	1
82			min	3.018	12	0	1	-.666	1	0	1	0	1	0	1
83		4	max	294.237	1	0	1	-.027	15	0	1	0	15	0	1
84			min	3.051	12	0	1	-.666	1	0	1	0	1	0	1
85		5	max	294.302	1	0	1	-.027	15	0	1	0	15	0	1
86			min	3.083	12	0	1	-.666	1	0	1	0	1	0	1
87		6	max	294.367	1	0	1	-.027	15	0	1	0	15	0	1
88			min	3.115	12	0	1	-.666	1	0	1	0	1	0	1
89		7	max	294.431	1	0	1	-.027	15	0	1	0	15	0	1
90			min	3.148	12	0	1	-.666	1	0	1	0	1	0	1
91		8	max	294.496	1	0	1	-.027	15	0	1	0	15	0	1
92			min	3.18	12	0	1	-.666	1	0	1	0	1	0	1
93		9	max	294.561	1	0	1	-.027	15	0	1	0	15	0	1
94			min	3.212	12	0	1	-.666	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
95		10	max	294.626	1	0	1	-.027	15	0	1	0	15	0	1
96			min	3.245	12	0	1	-.666	1	0	1	0	1	0	1
97		11	max	294.69	1	0	1	-.027	15	0	1	0	15	0	1
98			min	3.277	12	0	1	-.666	1	0	1	0	1	0	1
99		12	max	294.755	1	0	1	-.027	15	0	1	0	15	0	1
100			min	3.309	12	0	1	-.666	1	0	1	0	1	0	1
101		13	max	294.82	1	0	1	-.027	15	0	1	0	15	0	1
102			min	3.342	12	0	1	-.666	1	0	1	0	1	0	1
103		14	max	294.884	1	0	1	-.027	15	0	1	0	15	0	1
104			min	3.374	12	0	1	-.666	1	0	1	0	1	0	1
105		15	max	294.949	1	0	1	-.027	15	0	1	0	15	0	1
106			min	3.406	12	0	1	-.666	1	0	1	0	1	0	1
107		16	max	295.014	1	0	1	-.027	15	0	1	0	15	0	1
108			min	3.439	12	0	1	-.666	1	0	1	0	1	0	1
109		17	max	295.078	1	0	1	-.027	15	0	1	0	15	0	1
110			min	3.471	12	0	1	-.666	1	0	1	0	1	0	1
111		18	max	295.143	1	0	1	-.027	15	0	1	0	15	0	1
112			min	3.503	12	0	1	-.666	1	0	1	-.001	1	0	1
113		19	max	295.208	1	0	1	-.027	15	0	1	0	15	0	1
114			min	3.536	12	0	1	-.666	1	0	1	-.001	1	0	1
115	M6	1	max	663.302	1	.656	4	.037	9	0	3	0	3	0	1
116			min	-1092.007	3	.154	15	-.237	3	0	2	0	2	0	1
117		2	max	663.428	1	.605	4	.037	9	0	3	0	3	0	15
118			min	-1091.913	3	.142	15	-.237	3	0	2	0	2	0	4
119		3	max	663.554	1	.554	4	.037	9	0	3	0	3	0	15
120			min	-1091.818	3	.13	15	-.237	3	0	2	0	2	0	4
121		4	max	663.68	1	.503	4	.037	9	0	3	0	3	0	15
122			min	-1091.724	3	.118	15	-.237	3	0	2	0	2	0	4
123		5	max	663.806	1	.451	4	.037	9	0	3	0	3	0	15
124			min	-1091.63	3	.106	15	-.237	3	0	2	0	2	0	4
125		6	max	663.932	1	.407	2	.037	9	0	3	0	9	0	15
126			min	-1091.535	3	.088	12	-.237	3	0	2	0	2	0	4
127		7	max	664.057	1	.367	2	.037	9	0	3	0	9	0	15
128			min	-1091.441	3	.068	12	-.237	3	0	2	0	3	0	4
129		8	max	664.183	1	.327	2	.037	9	0	3	0	9	0	15
130			min	-1091.346	3	.048	12	-.237	3	0	2	0	3	0	4
131		9	max	664.309	1	.287	2	.037	9	0	3	0	9	0	15
132			min	-1091.252	3	.028	12	-.237	3	0	2	0	3	0	4
133		10	max	664.435	1	.247	2	.037	9	0	3	0	9	0	12
134			min	-1091.158	3	.001	3	-.237	3	0	2	0	3	0	2
135		11	max	664.561	1	.207	2	.037	9	0	3	0	9	0	12
136			min	-1091.063	3	-.029	3	-.237	3	0	2	0	3	0	2
137		12	max	664.687	1	.168	2	.037	9	0	3	0	9	0	12
138			min	-1090.969	3	-.059	3	-.237	3	0	2	0	3	0	2
139		13	max	664.813	1	.128	2	.037	9	0	3	0	9	0	12
140			min	-1090.874	3	-.088	3	-.237	3	0	2	0	3	0	2
141		14	max	664.939	1	.088	2	.037	9	0	3	0	9	0	12
142			min	-1090.78	3	-.118	3	-.237	3	0	2	0	3	0	2
143		15	max	665.064	1	.048	2	.037	9	0	3	0	9	0	12
144			min	-1090.686	3	-.148	3	-.237	3	0	2	0	3	0	2
145		16	max	665.19	1	.008	2	.037	9	0	3	0	9	0	12
146			min	-1090.591	3	-.178	3	-.237	3	0	2	0	3	0	2
147		17	max	665.316	1	-.032	2	.037	9	0	3	0	9	0	12
148			min	-1090.497	3	-.208	3	-.237	3	0	2	0	3	0	2
149		18	max	665.442	1	-.05	15	.037	9	0	3	0	9	0	3
150			min	-1090.402	3	-.238	3	-.237	3	0	2	0	3	0	2
151		19	max	665.568	1	-.062	15	.037	9	0	3	0	9	0	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
152			min	-1090.308	3	-.268	3	-.237	3	0	2	0	3	0	2
153	M7	1	max	595.055	2	1.761	4	.031	3	0	1	0	1	0	2
154			min	-499.921	3	.414	15	-.01	1	0	3	0	3	0	3
155		2	max	594.986	2	1.584	4	.031	3	0	1	0	1	0	2
156			min	-499.973	3	.372	15	-.01	1	0	3	0	3	0	3
157		3	max	594.917	2	1.407	4	.031	3	0	1	0	1	0	2
158			min	-500.025	3	.331	15	-.01	1	0	3	0	3	0	3
159		4	max	594.847	2	1.23	4	.031	3	0	1	0	1	0	2
160			min	-500.077	3	.289	15	-.01	1	0	3	0	3	0	3
161		5	max	594.778	2	1.054	4	.031	3	0	1	0	1	0	15
162			min	-500.129	3	.248	15	-.01	1	0	3	0	3	0	3
163		6	max	594.709	2	.877	4	.031	3	0	1	0	1	0	15
164			min	-500.181	3	.206	15	-.01	1	0	3	0	3	0	4
165		7	max	594.639	2	.7	4	.031	3	0	1	0	1	0	15
166			min	-500.233	3	.165	15	-.01	1	0	3	0	3	0	4
167		8	max	594.57	2	.523	4	.031	3	0	1	0	1	0	15
168			min	-500.285	3	.123	15	-.01	1	0	3	0	3	-.001	4
169		9	max	594.501	2	.349	2	.031	3	0	1	0	1	0	15
170			min	-500.337	3	.077	12	-.01	1	0	3	0	3	-.001	4
171		10	max	594.431	2	.212	2	.031	3	0	1	0	1	0	15
172			min	-500.389	3	.003	3	-.01	1	0	3	0	3	-.001	4
173		11	max	594.362	2	.074	2	.031	3	0	1	0	1	0	15
174			min	-500.441	3	-.101	3	-.01	1	0	3	0	3	-.001	4
175		12	max	594.293	2	-.043	15	.031	3	0	1	0	1	0	15
176			min	-500.493	3	-.204	3	-.01	1	0	3	0	3	-.001	4
177		13	max	594.223	2	-.085	15	.031	3	0	1	0	1	0	15
178			min	-500.545	3	-.361	4	-.01	1	0	3	0	3	-.001	4
179		14	max	594.154	2	-.126	15	.031	3	0	1	0	1	0	15
180			min	-500.597	3	-.538	4	-.01	1	0	3	0	3	-.001	4
181		15	max	594.085	2	-.168	15	.031	3	0	1	0	1	0	15
182			min	-500.649	3	-.715	4	-.01	1	0	3	0	3	0	4
183		16	max	594.015	2	-.21	15	.031	3	0	1	0	1	0	15
184			min	-500.701	3	-.892	4	-.01	1	0	3	0	3	0	4
185		17	max	593.946	2	-.251	15	.031	3	0	1	0	1	0	15
186			min	-500.753	3	-1.068	4	-.01	1	0	3	0	3	0	4
187		18	max	593.877	2	-.293	15	.031	3	0	1	0	1	0	15
188			min	-500.805	3	-1.245	4	-.01	1	0	3	0	3	0	4
189		19	max	593.807	2	-.334	15	.031	3	0	1	0	1	0	1
190			min	-500.857	3	-1.422	4	-.01	1	0	3	0	3	0	1
191	M8	1	max	804.656	1	0	1	.253	1	0	1	0	2	0	1
192			min	-30.404	3	0	1	-.613	3	0	1	0	3	0	1
193		2	max	804.721	1	0	1	.253	1	0	1	0	1	0	1
194			min	-30.355	3	0	1	-.613	3	0	1	0	3	0	1
195		3	max	804.786	1	0	1	.253	1	0	1	0	1	0	1
196			min	-30.307	3	0	1	-.613	3	0	1	0	3	0	1
197		4	max	804.851	1	0	1	.253	1	0	1	0	1	0	1
198			min	-30.258	3	0	1	-.613	3	0	1	0	3	0	1
199		5	max	804.915	1	0	1	.253	1	0	1	0	1	0	1
200			min	-30.21	3	0	1	-.613	3	0	1	0	3	0	1
201		6	max	804.98	1	0	1	.253	1	0	1	0	1	0	1
202			min	-30.161	3	0	1	-.613	3	0	1	0	3	0	1
203		7	max	805.045	1	0	1	.253	1	0	1	0	1	0	1
204			min	-30.113	3	0	1	-.613	3	0	1	0	3	0	1
205		8	max	805.109	1	0	1	.253	1	0	1	0	1	0	1
206			min	-30.064	3	0	1	-.613	3	0	1	0	3	0	1
207		9	max	805.174	1	0	1	.253	1	0	1	0	1	0	1
208			min	-30.016	3	0	1	-.613	3	0	1	0	3	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
209		10	max	805.239	1	0	1	.253	1	0	1	0	1	0	1
210			min	-29.967	3	0	1	-.613	3	0	1	0	3	0	1
211		11	max	805.304	1	0	1	.253	1	0	1	0	1	0	1
212			min	-29.918	3	0	1	-.613	3	0	1	0	3	0	1
213		12	max	805.368	1	0	1	.253	1	0	1	0	1	0	1
214			min	-29.87	3	0	1	-.613	3	0	1	0	3	0	1
215		13	max	805.433	1	0	1	.253	1	0	1	0	1	0	1
216			min	-29.821	3	0	1	-.613	3	0	1	0	3	0	1
217		14	max	805.498	1	0	1	.253	1	0	1	0	1	0	1
218			min	-29.773	3	0	1	-.613	3	0	1	0	3	0	1
219		15	max	805.562	1	0	1	.253	1	0	1	0	1	0	1
220			min	-29.724	3	0	1	-.613	3	0	1	0	3	0	1
221		16	max	805.627	1	0	1	.253	1	0	1	0	1	0	1
222			min	-29.676	3	0	1	-.613	3	0	1	0	3	0	1
223		17	max	805.692	1	0	1	.253	1	0	1	0	1	0	1
224			min	-29.627	3	0	1	-.613	3	0	1	0	3	0	1
225		18	max	805.756	1	0	1	.253	1	0	1	0	1	0	1
226			min	-29.579	3	0	1	-.613	3	0	1	0	3	0	1
227		19	max	805.821	1	0	1	.253	1	0	1	0	1	0	1
228			min	-29.53	3	0	1	-.613	3	0	1	0	3	0	1
229	M10	1	max	212.214	1	.655	4	-.004	15	0	1	0	1	0	1
230			min	-296.745	3	.154	15	-.114	1	0	3	0	3	0	1
231		2	max	212.34	1	.604	4	-.004	15	0	1	0	1	0	15
232			min	-296.651	3	.142	15	-.114	1	0	3	0	3	0	4
233		3	max	212.466	1	.553	4	-.004	15	0	1	0	1	0	15
234			min	-296.557	3	.13	15	-.114	1	0	3	0	3	0	4
235		4	max	212.592	1	.502	4	-.004	15	0	1	0	1	0	15
236			min	-296.462	3	.118	15	-.114	1	0	3	0	3	0	4
237		5	max	212.718	1	.451	4	-.004	15	0	1	0	1	0	15
238			min	-296.368	3	.106	15	-.114	1	0	3	0	3	0	4
239		6	max	212.844	1	.4	4	-.004	15	0	1	0	1	0	15
240			min	-296.273	3	.094	15	-.114	1	0	3	0	3	0	4
241		7	max	212.97	1	.349	4	-.004	15	0	1	0	1	0	15
242			min	-296.179	3	.082	15	-.114	1	0	3	0	3	0	4
243		8	max	213.096	1	.297	4	-.004	15	0	1	0	9	0	15
244			min	-296.085	3	.07	15	-.114	1	0	3	0	3	0	4
245		9	max	213.221	1	.246	4	-.004	15	0	1	0	9	0	15
246			min	-295.99	3	.058	15	-.114	1	0	3	0	3	0	4
247		10	max	213.347	1	.195	4	-.004	15	0	1	0	15	0	15
248			min	-295.896	3	.046	15	-.114	1	0	3	0	3	0	4
249		11	max	213.473	1	.144	4	-.004	15	0	1	0	15	0	15
250			min	-295.801	3	.034	15	-.114	1	0	3	0	3	0	4
251		12	max	213.599	1	.102	2	-.004	15	0	1	0	15	0	15
252			min	-295.707	3	.022	15	-.114	1	0	3	0	3	0	4
253		13	max	213.725	1	.062	2	-.004	15	0	1	0	15	0	15
254			min	-295.613	3	.005	12	-.114	1	0	3	0	3	0	4
255		14	max	213.851	1	.022	2	-.004	15	0	1	0	15	0	15
256			min	-295.518	3	-.023	3	-.114	1	0	3	0	3	0	4
257		15	max	213.977	1	-.014	15	-.004	15	0	1	0	15	0	15
258			min	-295.424	3	-.061	4	-.114	1	0	3	0	3	0	4
259		16	max	214.102	1	-.026	15	-.004	15	0	1	0	15	0	15
260			min	-295.329	3	-.112	4	-.114	1	0	3	0	3	0	4
261		17	max	214.228	1	-.038	15	-.004	15	0	1	0	15	0	15
262			min	-295.235	3	-.163	4	-.114	1	0	3	0	3	0	4
263		18	max	214.354	1	-.05	15	-.004	15	0	1	0	15	0	15
264			min	-295.141	3	-.214	4	-.114	1	0	3	0	3	0	4
265		19	max	214.48	1	-.062	15	-.004	15	0	1	0	15	0	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
266			min	-295.046	3	-.265	4	-.114	1	0	3	0	1	0	4
267	M11	1	max	174.1	2	1.759	4	.21	1	0	3	0	3	0	4
268			min	-171.72	3	.414	15	-.046	3	0	10	0	1	0	15
269		2	max	174.031	2	1.582	4	.21	1	0	3	0	3	0	2
270			min	-171.772	3	.372	15	-.046	3	0	10	0	1	0	3
271		3	max	173.961	2	1.405	4	.21	1	0	3	0	3	0	2
272			min	-171.824	3	.33	15	-.046	3	0	10	0	1	0	3
273		4	max	173.892	2	1.228	4	.21	1	0	3	0	3	0	15
274			min	-171.876	3	.289	15	-.046	3	0	10	0	1	0	3
275		5	max	173.823	2	1.051	4	.21	1	0	3	0	3	0	15
276			min	-171.928	3	.247	15	-.046	3	0	10	0	1	0	4
277		6	max	173.753	2	.874	4	.21	1	0	3	0	3	0	15
278			min	-171.98	3	.206	15	-.046	3	0	10	0	1	0	4
279		7	max	173.684	2	.698	4	.21	1	0	3	0	3	0	15
280			min	-172.032	3	.164	15	-.046	3	0	10	0	1	0	4
281		8	max	173.615	2	.521	4	.21	1	0	3	0	3	0	15
282			min	-172.084	3	.123	15	-.046	3	0	10	0	1	-.001	4
283		9	max	173.545	2	.344	4	.21	1	0	3	0	3	0	15
284			min	-172.136	3	.081	15	-.046	3	0	10	0	1	-.001	4
285		10	max	173.476	2	.167	4	.21	1	0	3	0	3	0	15
286			min	-172.188	3	.039	15	-.046	3	0	10	0	1	-.001	4
287		11	max	173.407	2	.017	2	.21	1	0	3	0	3	0	15
288			min	-172.24	3	-.048	3	-.046	3	0	10	0	1	-.001	4
289		12	max	173.337	2	-.044	15	.21	1	0	3	0	3	0	15
290			min	-172.292	3	-.187	4	-.046	3	0	10	0	1	-.001	4
291		13	max	173.268	2	-.085	15	.21	1	0	3	0	3	0	15
292			min	-172.344	3	-.363	4	-.046	3	0	10	0	1	-.001	4
293		14	max	173.199	2	-.127	15	.21	1	0	3	0	3	0	15
294			min	-172.396	3	-.54	4	-.046	3	0	10	0	1	-.001	4
295		15	max	173.129	2	-.168	15	.21	1	0	3	0	3	0	15
296			min	-172.448	3	-.717	4	-.046	3	0	10	0	1	0	4
297		16	max	173.06	2	-.21	15	.21	1	0	3	0	3	0	15
298			min	-172.5	3	-.894	4	-.046	3	0	10	0	10	0	4
299		17	max	172.991	2	-.252	15	.21	1	0	3	0	3	0	15
300			min	-172.552	3	-1.071	4	-.046	3	0	10	0	10	0	4
301		18	max	172.921	2	-.293	15	.21	1	0	3	0	3	0	15
302			min	-172.604	3	-1.248	4	-.046	3	0	10	0	10	0	4
303		19	max	172.852	2	-.335	15	.21	1	0	3	0	3	0	1
304			min	-172.656	3	-1.424	4	-.046	3	0	10	0	10	0	1
305	M12	1	max	294.087	1	0	1	1.183	1	0	1	0	2	0	1
306			min	3.34	12	0	1	.027	10	0	1	0	3	0	1
307		2	max	294.152	1	0	1	1.183	1	0	1	0	1	0	1
308			min	3.372	12	0	1	.027	10	0	1	0	15	0	1
309		3	max	294.216	1	0	1	1.183	1	0	1	0	1	0	1
310			min	3.405	12	0	1	.027	10	0	1	0	15	0	1
311		4	max	294.281	1	0	1	1.183	1	0	1	0	1	0	1
312			min	3.437	12	0	1	.027	10	0	1	0	15	0	1
313		5	max	294.346	1	0	1	1.183	1	0	1	0	1	0	1
314			min	3.469	12	0	1	.027	10	0	1	0	10	0	1
315		6	max	294.411	1	0	1	1.183	1	0	1	0	1	0	1
316			min	3.502	12	0	1	.027	10	0	1	0	10	0	1
317		7	max	294.475	1	0	1	1.183	1	0	1	0	1	0	1
318			min	3.534	12	0	1	.027	10	0	1	0	10	0	1
319		8	max	294.54	1	0	1	1.183	1	0	1	0	1	0	1
320			min	3.566	12	0	1	.027	10	0	1	0	10	0	1
321		9	max	294.605	1	0	1	1.183	1	0	1	0	1	0	1
322			min	3.599	12	0	1	.027	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
323		10	max	294.669	1	0	1	1.183	1	0	1	0	1	0	1
324			min	3.631	12	0	1	.027	10	0	1	0	10	0	1
325		11	max	294.734	1	0	1	1.183	1	0	1	.001	1	0	1
326			min	3.664	12	0	1	.027	10	0	1	0	10	0	1
327		12	max	294.799	1	0	1	1.183	1	0	1	.001	1	0	1
328			min	3.696	12	0	1	.027	10	0	1	0	10	0	1
329		13	max	294.863	1	0	1	1.183	1	0	1	.001	1	0	1
330			min	3.728	12	0	1	.027	10	0	1	0	10	0	1
331		14	max	294.928	1	0	1	1.183	1	0	1	.001	1	0	1
332			min	3.761	12	0	1	.027	10	0	1	0	10	0	1
333		15	max	294.993	1	0	1	1.183	1	0	1	.001	1	0	1
334			min	3.793	12	0	1	.027	10	0	1	0	10	0	1
335		16	max	295.058	1	0	1	1.183	1	0	1	.002	1	0	1
336			min	3.825	12	0	1	.027	10	0	1	0	10	0	1
337		17	max	295.122	1	0	1	1.183	1	0	1	.002	1	0	1
338			min	3.858	12	0	1	.027	10	0	1	0	10	0	1
339		18	max	295.187	1	0	1	1.183	1	0	1	.002	1	0	1
340			min	3.89	12	0	1	.027	10	0	1	0	10	0	1
341		19	max	295.252	1	0	1	1.183	1	0	1	.002	1	0	1
342			min	3.922	12	0	1	.027	10	0	1	0	10	0	1
343	M1	1	max	87.423	1	332.148	3	-.932	10	0	2	.049	1	0	2
344			min	3.586	15	-222.248	2	-25.129	1	0	3	.002	10	0	3
345		2	max	87.563	1	331.966	3	-.932	10	0	2	.044	1	.048	2
346			min	3.628	15	-222.49	2	-25.129	1	0	3	.002	10	-.072	3
347		3	max	86.573	3	4.696	9	-.926	10	0	12	.038	1	.096	2
348			min	-13.986	10	-23.775	2	-25.045	1	0	1	.001	10	-.143	3
349		4	max	86.677	3	4.494	9	-.926	10	0	12	.033	1	.101	2
350			min	-13.87	10	-24.016	2	-25.045	1	0	1	.001	10	-.14	3
351		5	max	86.782	3	4.293	9	-.926	10	0	12	.027	1	.106	2
352			min	-13.754	10	-24.258	2	-25.045	1	0	1	0	10	-.137	3
353		6	max	86.887	3	4.091	9	-.926	10	0	12	.022	1	.112	2
354			min	-13.637	10	-24.5	2	-25.045	1	0	1	0	10	-.135	3
355		7	max	86.992	3	3.89	9	-.926	10	0	12	.016	1	.117	2
356			min	-13.521	10	-24.742	2	-25.045	1	0	1	0	10	-.132	3
357		8	max	87.096	3	3.688	9	-.926	10	0	12	.011	1	.122	2
358			min	-13.405	10	-24.984	2	-25.045	1	0	1	0	10	-.129	3
359		9	max	87.201	3	3.486	9	-.926	10	0	12	.006	1	.128	2
360			min	-13.288	10	-25.226	2	-25.045	1	0	1	0	10	-.126	3
361		10	max	87.306	3	3.285	9	-.926	10	0	12	.002	3	.133	2
362			min	-13.172	10	-25.467	2	-25.045	1	0	1	0	10	-.123	3
363		11	max	87.41	3	3.083	9	-.926	10	0	12	0	3	.139	2
364			min	-13.056	10	-25.709	2	-25.045	1	0	1	-.005	1	-.12	3
365		12	max	87.515	3	2.882	9	-.926	10	0	12	0	12	.145	2
366			min	-12.939	10	-25.951	2	-25.045	1	0	1	-.011	1	-.117	3
367		13	max	87.62	3	2.68	9	-.926	10	0	12	0	10	.15	2
368			min	-12.823	10	-26.193	2	-25.045	1	0	1	-.016	1	-.114	3
369		14	max	87.725	3	2.479	9	-.926	10	0	12	0	10	.156	2
370			min	-12.707	10	-26.435	2	-25.045	1	0	1	-.022	1	-.11	3
371		15	max	87.829	3	2.277	9	-.926	10	0	12	-.001	10	.162	2
372			min	-12.59	10	-26.676	2	-25.045	1	0	1	-.027	1	-.107	3
373		16	max	87.501	2	117.665	2	-.933	10	0	1	-.001	10	.166	2
374			min	-5.744	3	-159.127	3	-25.217	1	0	12	-.033	1	-.103	3
375		17	max	87.64	2	117.424	2	-.933	10	0	1	-.001	10	.141	2
376			min	-5.64	3	-159.308	3	-25.217	1	0	12	-.038	1	-.068	3
377		18	max	-3.627	15	325.48	2	-.959	10	0	3	-.002	10	.071	2
378			min	-87.555	1	-156.813	3	-25.916	1	0	2	-.044	1	-.034	3
379		19	max	-3.585	15	325.238	2	-.959	10	0	3	-.002	10	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
380			min	-87.415	1	-156.994	3	-25.916	1	0	2	-.049	1	0	3
381	M5	1	max	207.549	1	1073.569	3	0	2	0	1	.009	3	0	3
382			min	2.436	12	-712.459	2	-68.246	3	0	3	0	10	0	2
383		2	max	207.689	1	1073.388	3	0	2	0	1	0	9	.154	2
384			min	2.505	12	-712.701	2	-68.246	3	0	3	-.005	3	-.232	3
385		3	max	250.132	3	5.066	9	7.502	3	0	3	0	1	.306	2
386			min	-48.795	2	-82.786	2	-.273	9	0	1	-.02	3	-.46	3
387		4	max	250.237	3	4.864	9	7.502	3	0	3	0	1	.324	2
388			min	-48.655	2	-83.027	2	-.273	9	0	1	-.018	3	-.45	3
389		5	max	250.342	3	4.663	9	7.502	3	0	3	0	1	.342	2
390			min	-48.516	2	-83.269	2	-.273	9	0	1	-.016	3	-.439	3
391		6	max	250.446	3	4.461	9	7.502	3	0	3	0	1	.36	2
392			min	-48.376	2	-83.511	2	-.273	9	0	1	-.015	3	-.428	3
393		7	max	250.551	3	4.26	9	7.502	3	0	3	0	1	.378	2
394			min	-48.236	2	-83.753	2	-.273	9	0	1	-.013	3	-.418	3
395		8	max	250.656	3	4.058	9	7.502	3	0	3	0	1	.397	2
396			min	-48.097	2	-83.995	2	-.273	9	0	1	-.011	3	-.407	3
397		9	max	250.76	3	3.857	9	7.502	3	0	3	0	1	.415	2
398			min	-47.957	2	-84.237	2	-.273	9	0	1	-.01	3	-.396	3
399		10	max	250.865	3	3.655	9	7.502	3	0	3	0	2	.433	2
400			min	-47.818	2	-84.478	2	-.273	9	0	1	-.008	3	-.386	3
401		11	max	250.97	3	3.454	9	7.502	3	0	3	0	2	.451	2
402			min	-47.678	2	-84.72	2	-.273	9	0	1	-.007	3	-.375	3
403		12	max	251.075	3	3.252	9	7.502	3	0	3	0	2	.47	2
404			min	-47.538	2	-84.962	2	-.273	9	0	1	-.005	3	-.364	3
405		13	max	251.179	3	3.051	9	7.502	3	0	3	0	2	.488	2
406			min	-47.399	2	-85.204	2	-.273	9	0	1	-.003	3	-.353	3
407		14	max	251.284	3	2.849	9	7.502	3	0	3	0	2	.507	2
408			min	-47.259	2	-85.446	2	-.273	9	0	1	-.002	3	-.342	3
409		15	max	251.389	3	2.647	9	7.502	3	0	3	0	2	.525	2
410			min	-47.12	2	-85.687	2	-.273	9	0	1	0	9	-.331	3
411		16	max	279.531	2	413.107	2	7.475	3	0	3	.001	3	.54	2
412			min	-22.897	3	-469.732	3	-.288	1	0	2	0	9	-.317	3
413		17	max	279.671	2	412.866	2	7.475	3	0	3	.003	3	.45	2
414			min	-22.793	3	-469.913	3	-.288	1	0	2	0	9	-.215	3
415		18	max	-5.317	12	1044.81	2	6.864	3	0	3	.004	3	.226	2
416			min	-207.706	1	-496.567	3	-.064	1	0	1	0	9	-.107	3
417		19	max	-5.247	12	1044.568	2	6.864	3	0	3	.006	3	0	3
418			min	-207.566	1	-496.748	3	-.064	1	0	1	0	1	0	2
419	M9	1	max	87.215	1	332.078	3	72.872	3	0	3	-.002	10	0	2
420			min	3.574	15	-222.248	2	.932	10	0	2	-.049	1	0	3
421		2	max	87.355	1	331.897	3	72.872	3	0	3	-.001	12	.048	2
422			min	3.616	15	-222.49	2	.932	10	0	2	-.043	1	-.072	3
423		3	max	86.241	3	4.679	9	24.605	1	0	1	.014	3	.096	2
424			min	-13.605	10	-23.746	2	-2.195	3	0	10	-.037	1	-.143	3
425		4	max	86.346	3	4.478	9	24.605	1	0	1	.013	3	.101	2
426			min	-13.488	10	-23.987	2	-2.195	3	0	10	-.032	1	-.14	3
427		5	max	86.451	3	4.276	9	24.605	1	0	1	.013	3	.106	2
428			min	-13.372	10	-24.229	2	-2.195	3	0	10	-.027	1	-.137	3
429		6	max	86.555	3	4.075	9	24.605	1	0	1	.012	3	.112	2
430			min	-13.256	10	-24.471	2	-2.195	3	0	10	-.021	1	-.134	3
431		7	max	86.66	3	3.873	9	24.605	1	0	1	.012	3	.117	2
432			min	-13.139	10	-24.713	2	-2.195	3	0	10	-.016	1	-.132	3
433		8	max	86.765	3	3.672	9	24.605	1	0	1	.011	3	.122	2
434			min	-13.023	10	-24.955	2	-2.195	3	0	10	-.011	1	-.129	3
435		9	max	86.87	3	3.47	9	24.605	1	0	1	.011	3	.128	2
436			min	-12.906	10	-25.197	2	-2.195	3	0	10	-.005	1	-.126	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
437		10	max	86.974	3	3.269	9	24.605	1	0	1	.01	3	.133	2
438			min	-12.79	10	-25.438	2	-2.195	3	0	10	0	1	-.123	3
439		11	max	87.079	3	3.067	9	24.605	1	0	1	.01	3	.139	2
440			min	-12.674	10	-25.68	2	-2.195	3	0	10	0	10	-.12	3
441		12	max	87.184	3	2.866	9	24.605	1	0	1	.011	1	.144	2
442			min	-12.557	10	-25.922	2	-2.195	3	0	10	0	10	-.117	3
443		13	max	87.288	3	2.664	9	24.605	1	0	1	.016	1	.15	2
444			min	-12.441	10	-26.164	2	-2.195	3	0	10	0	10	-.114	3
445		14	max	87.393	3	2.463	9	24.605	1	0	1	.021	1	.156	2
446			min	-12.325	10	-26.406	2	-2.195	3	0	10	0	10	-.111	3
447		15	max	87.498	3	2.261	9	24.605	1	0	1	.027	1	.162	2
448			min	-12.208	10	-26.648	2	-2.195	3	0	10	.001	10	-.107	3
449		16	max	87.706	2	117.31	2	24.789	1	0	15	.032	1	.166	2
450			min	-6.469	3	-159.644	3	-2.236	3	0	3	.001	10	-.103	3
451		17	max	87.846	2	117.068	2	24.789	1	0	15	.038	1	.141	2
452			min	-6.365	3	-159.825	3	-2.236	3	0	3	.001	10	-.068	3
453		18	max	-3.615	15	325.48	2	25.984	1	0	2	.043	1	.071	2
454			min	-87.346	1	-156.804	3	-1.774	3	0	3	.002	10	-.034	3
455		19	max	-3.573	15	325.238	2	25.984	1	0	2	.049	1	0	2
456			min	-87.207	1	-156.985	3	-1.774	3	0	3	.002	10	0	3
457	M13	1	max	72.867	3	222.149	2	-3.574	15	0	2	.049	1	0	2
458			min	.932	10	-332.115	3	-87.209	1	0	3	.002	10	0	3
459		2	max	72.867	3	157.936	2	-2.719	15	0	2	.013	3	.142	3
460			min	.932	10	-235.576	3	-65.977	1	0	3	-.002	10	-.095	2
461		3	max	72.867	3	93.724	2	-1.864	15	0	2	.009	3	.236	3
462			min	.932	10	-139.038	3	-44.744	1	0	3	-.017	1	-.158	2
463		4	max	72.867	3	29.512	2	-.873	10	0	2	.006	3	.281	3
464			min	.932	10	-42.5	3	-23.511	1	0	3	-.034	1	-.189	2
465		5	max	72.867	3	54.039	3	1.614	2	0	2	.003	3	.278	3
466			min	.932	10	-34.7	2	-4.518	3	0	3	-.041	1	-.187	2
467		6	max	72.867	3	150.577	3	18.954	1	0	2	.001	3	.227	3
468			min	.932	10	-98.912	2	-3.274	3	0	3	-.036	1	-.154	2
469		7	max	72.867	3	247.115	3	40.187	1	0	2	0	3	.127	3
470			min	.932	10	-163.124	2	-2.031	3	0	3	-.022	1	-.089	2
471		8	max	72.867	3	343.654	3	61.42	1	0	2	.005	2	.01	1
472			min	.932	10	-227.336	2	-.787	3	0	3	0	3	-.02	3
473		9	max	72.867	3	440.192	3	82.652	1	0	2	.04	1	.139	2
474			min	.932	10	-291.549	2	.457	3	0	3	0	3	-.216	3
475		10	max	72.867	3	536.73	3	103.885	1	0	2	.086	1	.301	2
476			min	.932	10	-355.761	2	1.421	12	0	3	-.01	3	-.46	3
477		11	max	25.182	1	291.549	2	.228	3	0	3	.039	1	.139	2
478			min	.932	10	-440.192	3	-82.444	1	0	2	-.01	3	-.216	3
479		12	max	25.182	1	227.336	2	1.472	3	0	3	.005	2	.01	1
480			min	.932	10	-343.654	3	-61.212	1	0	2	-.009	3	-.02	3
481		13	max	25.182	1	163.124	2	2.716	3	0	3	0	10	.127	3
482			min	.932	10	-247.115	3	-39.979	1	0	2	-.022	1	-.089	2
483		14	max	25.182	1	98.912	2	3.959	3	0	3	-.001	15	.227	3
484			min	.932	10	-150.577	3	-18.746	1	0	2	-.036	1	-.154	2
485		15	max	25.182	1	34.7	2	5.203	3	0	3	-.002	15	.278	3
486			min	.932	10	-54.039	3	-1.614	2	0	2	-.041	1	-.187	2
487		16	max	25.182	1	42.5	3	23.719	1	0	3	0	12	.281	3
488			min	.932	10	-29.512	2	.873	10	0	2	-.034	1	-.189	2
489		17	max	25.182	1	139.038	3	44.952	1	0	3	.002	3	.236	3
490			min	.932	10	-93.724	2	1.877	15	0	2	-.017	1	-.158	2
491		18	max	25.182	1	235.576	3	66.185	1	0	3	.011	1	.142	3
492			min	.932	10	-157.936	2	2.732	15	0	2	-.002	10	-.095	2
493		19	max	25.182	1	332.115	3	87.417	1	0	3	.049	1	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
494			min	.932	10	-222.149	2	3.586	15	0	2	.002	10	0	3
495	M16	1	max	1.777	3	325.363	2	-3.573	15	0	3	.049	1	0	2
496			min	-25.93	1	-157.011	3	-87.213	1	0	2	.002	10	0	3
497		2	max	1.777	3	231.114	2	-2.719	15	0	3	.011	1	.067	3
498			min	-25.93	1	-111.964	3	-65.98	1	0	2	-.002	10	-.139	2
499		3	max	1.777	3	136.864	2	-1.864	15	0	3	0	3	.112	3
500			min	-25.93	1	-66.917	3	-44.748	1	0	2	-.017	1	-.231	2
501		4	max	1.777	3	42.615	2	-.886	10	0	3	-.001	15	.134	3
502			min	-25.93	1	-21.87	3	-23.515	1	0	2	-.034	1	-.276	2
503		5	max	1.777	3	23.176	3	1.589	2	0	3	-.002	15	.134	3
504			min	-25.93	1	-51.634	2	-3.024	3	0	2	-.041	1	-.274	2
505		6	max	1.777	3	68.223	3	18.95	1	0	3	-.001	15	.111	3
506			min	-25.93	1	-145.883	2	-1.78	3	0	2	-.036	1	-.224	2
507		7	max	1.777	3	113.27	3	40.183	1	0	3	0	10	.066	3
508			min	-25.93	1	-240.132	2	-.536	3	0	2	-.022	1	-.128	2
509		8	max	1.777	3	158.317	3	61.416	1	0	3	.005	2	.016	2
510			min	-25.93	1	-334.381	2	.658	12	0	2	-.006	3	-.002	3
511		9	max	1.777	3	203.364	3	82.648	1	0	3	.04	1	.207	2
512			min	-25.93	1	-428.63	2	1.487	12	0	2	-.005	3	-.093	3
513		10	max	-.959	10	-8.222	15	103.881	1	0	15	.086	1	.444	2
514			min	-25.93	1	-522.88	2	-4.224	3	0	2	-.004	3	-.206	3
515		11	max	-.959	10	428.63	2	-2.102	12	0	2	.039	1	.207	2
516			min	-25.864	1	-203.364	3	-82.44	1	0	3	0	3	-.093	3
517		12	max	-.959	10	334.381	2	-1.272	12	0	2	.005	2	.016	2
518			min	-25.864	1	-158.317	3	-61.207	1	0	3	-.001	3	-.002	3
519		13	max	-.959	10	240.132	2	-.443	12	0	2	0	10	.066	3
520			min	-25.864	1	-113.27	3	-39.975	1	0	3	-.022	1	-.128	2
521		14	max	-.959	10	145.883	2	.75	3	0	2	-.001	12	.111	3
522			min	-25.864	1	-68.223	3	-18.742	1	0	3	-.036	1	-.224	2
523		15	max	-.959	10	51.634	2	2.706	9	0	2	0	12	.134	3
524			min	-25.864	1	-23.176	3	-1.588	2	0	3	-.04	1	-.274	2
525		16	max	-.959	10	21.871	3	23.723	1	0	2	0	3	.134	3
526			min	-25.864	1	-42.615	2	.886	10	0	3	-.034	1	-.276	2
527		17	max	-.959	10	66.917	3	44.956	1	0	2	.002	3	.112	3
528			min	-25.864	1	-136.864	2	1.876	15	0	3	-.017	1	-.231	2
529		18	max	-.959	10	111.964	3	66.189	1	0	2	.011	1	.067	3
530			min	-25.864	1	-231.114	2	2.731	15	0	3	-.002	10	-.139	2
531		19	max	-.959	10	157.011	3	87.422	1	0	2	.049	1	0	2
532			min	-25.864	1	-325.363	2	3.585	15	0	3	.002	10	0	3
533	M15	1	max	0	1	.933	3	.108	3	0	1	0	1	0	1
534			min	-93.603	3	0	1	0	1	0	3	0	3	0	1
535		2	max	0	1	.829	3	.108	3	0	1	0	1	0	1
536			min	-93.674	3	0	1	0	1	0	3	0	3	0	3
537		3	max	0	1	.726	3	.108	3	0	1	0	1	0	1
538			min	-93.744	3	0	1	0	1	0	3	0	3	0	3
539		4	max	0	1	.622	3	.108	3	0	1	0	1	0	1
540			min	-93.815	3	0	1	0	1	0	3	0	3	0	3
541		5	max	0	1	.518	3	.108	3	0	1	0	1	0	1
542			min	-93.885	3	0	1	0	1	0	3	0	3	0	3
543		6	max	0	1	.415	3	.108	3	0	1	0	1	0	1
544			min	-93.956	3	0	1	0	1	0	3	0	3	-.001	3
545		7	max	0	1	.311	3	.108	3	0	1	0	3	0	1
546			min	-94.026	3	0	1	0	1	0	3	0	1	-.001	3
547		8	max	0	1	.207	3	.108	3	0	1	0	3	0	1
548			min	-94.097	3	0	1	0	1	0	3	0	1	-.001	3
549		9	max	0	1	.104	3	.108	3	0	1	0	3	0	1
550			min	-94.167	3	0	1	0	1	0	3	0	1	-.001	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
551		10	max	0	1	0	1	.108	3	0	1	0	3	0	1
552			min	-94.238	3	0	1	0	1	0	3	0	1	-.001	3
553		11	max	0	1	0	1	.108	3	0	1	0	3	0	1
554			min	-94.308	3	-.104	3	0	1	0	3	0	1	-.001	3
555		12	max	0	1	0	1	.108	3	0	1	0	3	0	1
556			min	-94.379	3	-.207	3	0	1	0	3	0	1	-.001	3
557		13	max	0	1	0	1	.108	3	0	1	0	3	0	1
558			min	-94.449	3	-.311	3	0	1	0	3	0	1	-.001	3
559		14	max	0	1	0	1	.108	3	0	1	0	3	0	1
560			min	-94.52	3	-.415	3	0	1	0	3	0	1	-.001	3
561		15	max	0	1	0	1	.108	3	0	1	0	3	0	1
562			min	-94.59	3	-.518	3	0	1	0	3	0	1	0	3
563		16	max	0	1	0	1	.108	3	0	1	0	3	0	1
564			min	-94.661	3	-.622	3	0	1	0	3	0	1	0	3
565		17	max	0	1	0	1	.108	3	0	1	0	3	0	1
566			min	-94.731	3	-.726	3	0	1	0	3	0	1	0	3
567		18	max	0	1	0	1	.108	3	0	1	0	3	0	1
568			min	-94.802	3	-.829	3	0	1	0	3	0	1	0	3
569		19	max	0	1	0	1	.108	3	0	1	0	3	0	1
570			min	-94.872	3	-.933	3	0	1	0	3	0	1	0	1
571	M16A	1	max	0	2	1.597	4	.034	1	0	3	0	3	0	1
572			min	-93.563	3	0	2	-.044	3	0	1	0	1	0	1
573		2	max	0	2	1.419	4	.034	1	0	3	0	3	0	2
574			min	-93.493	3	0	2	-.044	3	0	1	0	1	0	4
575		3	max	0	2	1.242	4	.034	1	0	3	0	3	0	2
576			min	-93.422	3	0	2	-.044	3	0	1	0	1	0	4
577		4	max	0	2	1.064	4	.034	1	0	3	0	3	0	2
578			min	-93.352	3	0	2	-.044	3	0	1	0	1	-.001	4
579		5	max	0	2	.887	4	.034	1	0	3	0	3	0	2
580			min	-93.281	3	0	2	-.044	3	0	1	0	1	-.002	4
581		6	max	0	2	.71	4	.034	1	0	3	0	3	0	2
582			min	-93.211	3	0	2	-.044	3	0	1	0	1	-.002	4
583		7	max	0	2	.532	4	.034	1	0	3	0	3	0	2
584			min	-93.14	3	0	2	-.044	3	0	1	0	1	-.002	4
585		8	max	0	2	.355	4	.034	1	0	3	0	3	0	2
586			min	-93.07	3	0	2	-.044	3	0	1	0	1	-.002	4
587		9	max	0	2	.177	4	.034	1	0	3	0	3	0	2
588			min	-92.999	3	0	2	-.044	3	0	1	0	1	-.002	4
589		10	max	0	2	0	1	.034	1	0	3	0	3	0	2
590			min	-92.929	3	0	1	-.044	3	0	1	0	1	-.002	4
591		11	max	0	2	0	2	.034	1	0	3	0	3	0	2
592			min	-92.858	3	-.177	4	-.044	3	0	1	0	1	-.002	4
593		12	max	0	2	0	2	.034	1	0	3	0	3	0	2
594			min	-92.788	3	-.355	4	-.044	3	0	1	0	1	-.002	4
595		13	max	.095	13	0	2	.034	1	0	3	0	1	0	2
596			min	-92.717	3	-.532	4	-.044	3	0	1	0	4	-.002	4
597		14	max	.192	13	0	2	.034	1	0	3	0	1	0	2
598			min	-92.647	3	-.71	4	-.044	3	0	1	0	3	-.002	4
599		15	max	.289	13	0	2	.034	1	0	3	0	1	0	2
600			min	-92.576	3	-.887	4	-.044	3	0	1	0	3	-.002	4
601		16	max	.386	13	0	2	.034	1	0	3	0	1	0	2
602			min	-92.506	3	-1.064	4	-.044	3	0	1	0	3	-.001	4
603		17	max	.483	13	0	2	.034	1	0	3	0	1	0	2
604			min	-92.435	3	-1.242	4	-.044	3	0	1	0	3	0	4
605		18	max	.58	13	0	2	.034	1	0	3	0	1	0	2
606			min	-92.365	3	-1.419	4	-.044	3	0	1	0	3	0	4
607		19	max	.677	13	0	2	.034	1	0	3	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
608			min	-92.294	3	-1.597	4	-.044	3	0	1	0	3	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	1	.009	2	.004	1	-1.44e-5	10	NC	3	NC	2
2			min	-.003	3	-.009	3	-.002	3	-3.99e-4	1	4338.682	2	8860.739	1
3		2	max	.002	1	.008	2	.004	1	-1.372e-5	10	NC	3	NC	2
4			min	-.003	3	-.009	3	-.002	3	-3.814e-4	1	4739.406	2	9536.247	1
5		3	max	.002	1	.008	2	.004	1	-1.304e-5	10	NC	1	NC	1
6			min	-.003	3	-.008	3	-.002	3	-3.637e-4	1	5216.833	2	NC	1
7		4	max	.002	1	.007	2	.003	1	-1.236e-5	10	NC	1	NC	1
8			min	-.003	3	-.008	3	-.001	3	-3.461e-4	1	5789.68	2	NC	1
9		5	max	.002	1	.006	2	.003	1	-1.168e-5	10	NC	1	NC	1
10			min	-.003	3	-.008	3	-.001	3	-3.285e-4	1	6482.961	2	NC	1
11		6	max	.001	1	.005	2	.003	1	-1.1e-5	10	NC	1	NC	1
12			min	-.002	3	-.007	3	-.001	3	-3.109e-4	1	7330.659	2	NC	1
13		7	max	.001	1	.005	2	.003	1	-1.032e-5	10	NC	1	NC	1
14			min	-.002	3	-.007	3	0	3	-2.933e-4	1	8379.835	2	NC	1
15		8	max	.001	1	.004	2	.002	1	-9.645e-6	10	NC	1	NC	1
16			min	-.002	3	-.006	3	0	3	-2.757e-4	1	9697.136	2	NC	1
17		9	max	.001	1	.003	2	.002	1	-8.966e-6	10	NC	1	NC	1
18			min	-.002	3	-.006	3	0	3	-2.581e-4	1	NC	1	NC	1
19		10	max	.001	1	.003	2	.002	1	-8.286e-6	10	NC	1	NC	1
20			min	-.002	3	-.006	3	0	3	-2.404e-4	1	NC	1	NC	1
21		11	max	0	1	.002	2	.001	1	-7.607e-6	10	NC	1	NC	1
22			min	-.002	3	-.005	3	0	3	-2.228e-4	1	NC	1	NC	1
23		12	max	0	1	.002	2	.001	1	-6.928e-6	10	NC	1	NC	1
24			min	-.001	3	-.004	3	0	3	-2.052e-4	1	NC	1	NC	1
25		13	max	0	1	.001	2	0	1	-6.248e-6	10	NC	1	NC	1
26			min	-.001	3	-.004	3	0	3	-1.876e-4	1	NC	1	NC	1
27		14	max	0	1	.001	2	0	1	-5.569e-6	10	NC	1	NC	1
28			min	0	3	-.003	3	0	3	-1.7e-4	1	NC	1	NC	1
29		15	max	0	1	0	2	0	1	-4.89e-6	10	NC	1	NC	1
30			min	0	3	-.003	3	0	3	-1.524e-4	1	NC	1	NC	1
31		16	max	0	1	0	2	0	1	-4.21e-6	10	NC	1	NC	1
32			min	0	3	-.002	3	0	3	-1.348e-4	1	NC	1	NC	1
33		17	max	0	1	0	2	0	1	-3.531e-6	10	NC	1	NC	1
34			min	0	3	-.001	3	0	3	-1.172e-4	1	NC	1	NC	1
35		18	max	0	1	0	2	0	1	-2.851e-6	10	NC	1	NC	1
36			min	0	3	0	3	0	3	-9.954e-5	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	-2.172e-6	10	NC	1	NC	1
38			min	0	1	0	1	0	1	-8.193e-5	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	3.869e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	1.03e-6	10	NC	1	NC	1
41		2	max	0	3	0	2	0	10	4.915e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	1	1.525e-6	10	NC	1	NC	1
43		3	max	0	3	0	2	0	10	5.961e-5	1	NC	1	NC	1
44			min	0	2	-.002	3	0	1	2.02e-6	10	NC	1	NC	1
45		4	max	0	3	0	2	0	3	7.006e-5	1	NC	1	NC	1
46			min	0	2	-.003	3	0	1	2.515e-6	10	NC	1	NC	1
47		5	max	0	3	0	2	0	3	8.052e-5	1	NC	1	NC	1
48			min	0	2	-.003	3	0	1	3.01e-6	10	NC	1	NC	1
49		6	max	0	3	0	2	0	3	9.097e-5	1	NC	1	NC	1
50			min	0	2	-.004	3	0	1	3.505e-6	10	NC	1	NC	1
51		7	max	0	3	0	2	0	3	1.014e-4	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
52			min	0	2	-.005	3	0	9	4.e-6	10	NC	1	NC	1
53		8	max	0	3	0	2	0	3	1.119e-4	1	NC	1	NC	1
54			min	0	2	-.006	3	0	9	4.496e-6	10	NC	1	NC	1
55		9	max	0	3	.001	2	0	3	1.223e-4	1	NC	1	NC	1
56			min	0	2	-.006	3	0	9	4.991e-6	10	NC	1	NC	1
57		10	max	0	3	.002	2	0	1	1.328e-4	1	NC	1	NC	1
58			min	0	2	-.007	3	0	15	5.486e-6	10	NC	1	NC	1
59		11	max	.001	3	.002	2	0	1	1.433e-4	1	NC	1	NC	1
60			min	-.001	2	-.007	3	0	15	5.981e-6	10	NC	1	NC	1
61		12	max	.001	3	.003	2	0	1	1.537e-4	1	NC	1	NC	1
62			min	-.001	2	-.007	3	0	15	6.456e-6	15	NC	1	NC	1
63		13	max	.001	3	.003	2	.001	1	1.642e-4	1	NC	1	NC	1
64			min	-.001	2	-.008	3	0	15	6.884e-6	15	NC	1	NC	1
65		14	max	.001	3	.004	2	.001	1	1.746e-4	1	NC	1	NC	1
66			min	-.001	2	-.008	3	0	15	7.311e-6	15	NC	1	NC	1
67		15	max	.002	3	.005	2	.002	1	1.851e-4	1	NC	1	NC	1
68			min	-.002	2	-.008	3	0	15	7.739e-6	15	9475.919	2	NC	1
69		16	max	.002	3	.006	2	.002	1	1.955e-4	1	NC	1	NC	1
70			min	-.002	2	-.008	3	0	15	8.166e-6	15	7984.906	2	NC	1
71		17	max	.002	3	.007	2	.002	1	2.06e-4	1	NC	1	NC	1
72			min	-.002	2	-.008	3	0	15	8.594e-6	15	6841.071	2	NC	1
73		18	max	.002	3	.008	2	.003	1	2.164e-4	1	NC	1	NC	1
74			min	-.002	2	-.008	3	0	15	9.021e-6	15	5952.335	2	NC	1
75		19	max	.002	3	.009	2	.003	1	2.269e-4	1	NC	3	NC	1
76			min	-.002	2	-.008	3	0	15	9.448e-6	15	5254.883	2	NC	1
77	M4	1	max	.001	1	.01	2	0	15	-1.089e-5	10	NC	1	NC	2
78			min	0	12	-.009	3	-.002	1	-3.116e-4	1	NC	1	9003.771	1
79		2	max	.001	1	.01	2	0	15	-1.089e-5	10	NC	1	NC	2
80			min	0	12	-.009	3	-.002	1	-3.116e-4	1	NC	1	9822.156	1
81		3	max	.001	1	.009	2	0	15	-1.089e-5	10	NC	1	NC	1
82			min	0	12	-.008	3	-.002	1	-3.116e-4	1	NC	1	NC	1
83		4	max	.001	1	.009	2	0	15	-1.089e-5	10	NC	1	NC	1
84			min	0	12	-.008	3	-.002	1	-3.116e-4	1	NC	1	NC	1
85		5	max	.001	1	.008	2	0	15	-1.089e-5	10	NC	1	NC	1
86			min	0	12	-.007	3	-.001	1	-3.116e-4	1	NC	1	NC	1
87		6	max	.001	1	.008	2	0	15	-1.089e-5	10	NC	1	NC	1
88			min	0	12	-.007	3	-.001	1	-3.116e-4	1	NC	1	NC	1
89		7	max	0	1	.007	2	0	15	-1.089e-5	10	NC	1	NC	1
90			min	0	12	-.006	3	-.001	1	-3.116e-4	1	NC	1	NC	1
91		8	max	0	1	.006	2	0	15	-1.089e-5	10	NC	1	NC	1
92			min	0	12	-.006	3	0	1	-3.116e-4	1	NC	1	NC	1
93		9	max	0	1	.006	2	0	15	-1.089e-5	10	NC	1	NC	1
94			min	0	12	-.005	3	0	1	-3.116e-4	1	NC	1	NC	1
95		10	max	0	1	.005	2	0	15	-1.089e-5	10	NC	1	NC	1
96			min	0	12	-.005	3	0	1	-3.116e-4	1	NC	1	NC	1
97		11	max	0	1	.005	2	0	15	-1.089e-5	10	NC	1	NC	1
98			min	0	12	-.004	3	0	1	-3.116e-4	1	NC	1	NC	1
99		12	max	0	1	.004	2	0	15	-1.089e-5	10	NC	1	NC	1
100			min	0	12	-.004	3	0	1	-3.116e-4	1	NC	1	NC	1
101		13	max	0	1	.003	2	0	15	-1.089e-5	10	NC	1	NC	1
102			min	0	12	-.003	3	0	1	-3.116e-4	1	NC	1	NC	1
103		14	max	0	1	.003	2	0	15	-1.089e-5	10	NC	1	NC	1
104			min	0	12	-.003	3	0	1	-3.116e-4	1	NC	1	NC	1
105		15	max	0	1	.002	2	0	15	-1.089e-5	10	NC	1	NC	1
106			min	0	12	-.002	3	0	1	-3.116e-4	1	NC	1	NC	1
107		16	max	0	1	.002	2	0	15	-1.089e-5	10	NC	1	NC	1
108			min	0	12	-.002	3	0	1	-3.116e-4	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
109		17	max	0	1	.001	2	0	15	-1.089e-5	10	NC	1	NC	1
110			min	0	12	-.001	3	0	1	-3.116e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	15	-1.089e-5	10	NC	1	NC	1
112			min	0	12	0	3	0	1	-3.116e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	-1.089e-5	10	NC	1	NC	1
114			min	0	1	0	1	0	1	-3.116e-4	1	NC	1	NC	1
115	M6	1	max	.006	1	.03	2	.001	1	4.384e-4	3	NC	3	NC	1
116			min	-.011	3	-.028	3	-.006	3	-8.019e-8	2	1309.377	2	6938.294	3
117		2	max	.006	1	.028	2	.001	1	4.249e-4	3	NC	3	NC	1
118			min	-.01	3	-.026	3	-.005	3	-3.452e-7	11	1401.762	2	7365.676	3
119		3	max	.006	1	.026	2	.001	1	4.113e-4	3	NC	3	NC	1
120			min	-.009	3	-.025	3	-.005	3	-2.194e-6	1	1507.717	2	7873.49	3
121		4	max	.005	1	.024	2	.001	1	3.978e-4	3	NC	3	NC	1
122			min	-.009	3	-.024	3	-.005	3	-4.442e-6	1	1629.965	2	8478.875	3
123		5	max	.005	1	.022	2	.001	1	3.842e-4	3	NC	3	NC	1
124			min	-.008	3	-.022	3	-.004	3	-6.69e-6	1	1772.015	2	9204.58	3
125		6	max	.005	1	.02	2	0	1	3.707e-4	3	NC	3	NC	1
126			min	-.008	3	-.021	3	-.004	3	-8.937e-6	1	1938.462	2	NC	1
127		7	max	.004	1	.018	2	0	1	3.571e-4	3	NC	3	NC	1
128			min	-.007	3	-.019	3	-.004	3	-1.119e-5	1	2135.438	2	NC	1
129		8	max	.004	1	.017	2	0	1	3.436e-4	3	NC	3	NC	1
130			min	-.006	3	-.018	3	-.003	3	-1.343e-5	1	2371.312	2	NC	1
131		9	max	.004	1	.015	2	0	1	3.3e-4	3	NC	3	NC	1
132			min	-.006	3	-.016	3	-.003	3	-1.568e-5	1	2657.799	2	NC	1
133		10	max	.003	1	.013	2	0	1	3.165e-4	3	NC	3	NC	1
134			min	-.005	3	-.014	3	-.002	3	-1.793e-5	1	3011.823	2	NC	1
135		11	max	.003	1	.011	2	0	1	3.029e-4	3	NC	3	NC	1
136			min	-.005	3	-.013	3	-.002	3	-2.018e-5	1	3458.764	2	NC	1
137		12	max	.003	1	.01	2	0	1	2.894e-4	3	NC	3	NC	1
138			min	-.004	3	-.011	3	-.002	3	-2.242e-5	1	4038.497	2	NC	1
139		13	max	.002	1	.008	2	0	1	2.758e-4	3	NC	3	NC	1
140			min	-.004	3	-.01	3	-.001	3	-2.467e-5	1	4817.462	2	NC	1
141		14	max	.002	1	.007	2	0	1	2.623e-4	3	NC	3	NC	1
142			min	-.003	3	-.008	3	-.001	3	-2.692e-5	1	5915.221	2	NC	1
143		15	max	.001	1	.005	2	0	1	2.487e-4	3	NC	1	NC	1
144			min	-.002	3	-.007	3	0	3	-2.917e-5	1	7570.842	2	NC	1
145		16	max	.001	1	.004	2	0	1	2.352e-4	3	NC	1	NC	1
146			min	-.002	3	-.005	3	0	3	-3.141e-5	1	NC	1	NC	1
147		17	max	0	1	.002	2	0	1	2.216e-4	3	NC	1	NC	1
148			min	-.001	3	-.003	3	0	3	-3.366e-5	1	NC	1	NC	1
149		18	max	0	1	.001	2	0	1	2.081e-4	3	NC	1	NC	1
150			min	0	3	-.002	3	0	3	-3.591e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.945e-4	3	NC	1	NC	1
152			min	0	1	0	1	0	1	-3.816e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	1.79e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-9.128e-5	3	NC	1	NC	1
155		2	max	0	3	.001	2	0	3	1.582e-5	1	NC	1	NC	1
156			min	0	2	-.002	3	0	1	-6.835e-5	3	NC	1	NC	1
157		3	max	0	3	.003	2	0	3	1.374e-5	1	NC	1	NC	1
158			min	0	2	-.004	3	0	1	-4.542e-5	3	NC	1	NC	1
159		4	max	0	3	.004	2	.001	3	1.166e-5	1	NC	1	NC	1
160			min	-.001	2	-.006	3	0	1	-2.248e-5	3	NC	1	NC	1
161		5	max	.001	3	.005	2	.002	3	9.578e-6	1	NC	1	NC	1
162			min	-.001	2	-.008	3	0	1	0	2	8948.368	2	NC	1
163		6	max	.002	3	.006	2	.002	3	2.338e-5	3	NC	1	NC	1
164			min	-.002	2	-.009	3	0	1	0	2	7168.021	2	NC	1
165		7	max	.002	3	.008	2	.002	3	4.631e-5	3	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
166			min	-.002	2	-.011	3	0	1	-1.018e-7	13	5949.835	2	NC	1
167		8	max	.002	3	.009	2	.002	3	6.924e-5	3	NC	3	NC	1
168			min	-.003	2	-.013	3	0	1	-1.245e-6	9	5056.41	2	NC	1
169		9	max	.003	3	.011	2	.003	3	9.217e-5	3	NC	3	NC	1
170			min	-.003	2	-.014	3	0	1	-3.153e-6	9	4369.467	2	NC	1
171		10	max	.003	3	.012	2	.003	3	1.151e-4	3	NC	3	NC	1
172			min	-.003	2	-.016	3	0	1	-5.062e-6	9	3823.436	2	NC	1
173		11	max	.003	3	.014	2	.003	3	1.38e-4	3	NC	3	NC	1
174			min	-.004	2	-.017	3	0	1	-6.97e-6	9	3378.917	2	NC	1
175		12	max	.003	3	.015	2	.003	3	1.61e-4	3	NC	3	NC	1
176			min	-.004	2	-.018	3	0	1	-8.878e-6	9	3010.672	2	NC	1
177		13	max	.004	3	.017	2	.003	3	1.839e-4	3	NC	3	NC	1
178			min	-.004	2	-.019	3	0	1	-1.079e-5	9	2701.65	2	NC	1
179		14	max	.004	3	.019	2	.003	3	2.068e-4	3	NC	3	NC	1
180			min	-.005	2	-.02	3	0	1	-1.269e-5	9	2439.813	2	NC	1
181		15	max	.004	3	.021	2	.003	3	2.298e-4	3	NC	3	NC	1
182			min	-.005	2	-.021	3	0	1	-1.46e-5	9	2216.339	2	NC	1
183		16	max	.005	3	.023	2	.003	3	2.527e-4	3	NC	3	NC	1
184			min	-.006	2	-.022	3	0	1	-1.651e-5	9	2024.567	2	NC	1
185		17	max	.005	3	.025	2	.003	3	2.756e-4	3	NC	3	NC	1
186			min	-.006	2	-.023	3	0	1	-1.842e-5	9	1859.339	2	NC	1
187		18	max	.005	3	.027	2	.003	3	2.986e-4	3	NC	3	NC	1
188			min	-.006	2	-.024	3	0	1	-2.033e-5	9	1716.588	2	NC	1
189		19	max	.006	3	.029	2	.003	3	3.215e-4	3	NC	3	NC	1
190			min	-.007	2	-.025	3	0	1	-2.224e-5	9	1593.061	2	NC	1
191	M8	1	max	.004	1	.034	2	0	1	-1.037e-7	10	NC	1	NC	1
192			min	0	3	-.028	3	-.002	3	-2.414e-4	3	NC	1	9975.813	3
193		2	max	.004	1	.032	2	0	1	-1.037e-7	10	NC	1	NC	1
194			min	0	3	-.026	3	-.002	3	-2.414e-4	3	NC	1	NC	1
195		3	max	.003	1	.031	2	0	1	-1.037e-7	10	NC	1	NC	1
196			min	0	3	-.025	3	-.002	3	-2.414e-4	3	NC	1	NC	1
197		4	max	.003	1	.029	2	0	1	-1.037e-7	10	NC	1	NC	1
198			min	0	3	-.023	3	-.001	3	-2.414e-4	3	NC	1	NC	1
199		5	max	.003	1	.027	2	0	1	-1.037e-7	10	NC	1	NC	1
200			min	0	3	-.022	3	-.001	3	-2.414e-4	3	NC	1	NC	1
201		6	max	.003	1	.025	2	0	1	-1.037e-7	10	NC	1	NC	1
202			min	0	3	-.02	3	-.001	3	-2.414e-4	3	NC	1	NC	1
203		7	max	.003	1	.023	2	0	1	-1.037e-7	10	NC	1	NC	1
204			min	0	3	-.019	3	-.001	3	-2.414e-4	3	NC	1	NC	1
205		8	max	.002	1	.021	2	0	1	-1.037e-7	10	NC	1	NC	1
206			min	0	3	-.017	3	0	3	-2.414e-4	3	NC	1	NC	1
207		9	max	.002	1	.019	2	0	1	-1.037e-7	10	NC	1	NC	1
208			min	0	3	-.015	3	0	3	-2.414e-4	3	NC	1	NC	1
209		10	max	.002	1	.017	2	0	1	-1.037e-7	10	NC	1	NC	1
210			min	0	3	-.014	3	0	3	-2.414e-4	3	NC	1	NC	1
211		11	max	.002	1	.015	2	0	1	-1.037e-7	10	NC	1	NC	1
212			min	0	3	-.012	3	0	3	-2.414e-4	3	NC	1	NC	1
213		12	max	.001	1	.013	2	0	1	-1.037e-7	10	NC	1	NC	1
214			min	0	3	-.011	3	0	3	-2.414e-4	3	NC	1	NC	1
215		13	max	.001	1	.011	2	0	1	-1.037e-7	10	NC	1	NC	1
216			min	0	3	-.009	3	0	3	-2.414e-4	3	NC	1	NC	1
217		14	max	.001	1	.01	2	0	1	-1.037e-7	10	NC	1	NC	1
218			min	0	3	-.008	3	0	3	-2.414e-4	3	NC	1	NC	1
219		15	max	0	1	.008	2	0	1	-1.037e-7	10	NC	1	NC	1
220			min	0	3	-.006	3	0	3	-2.414e-4	3	NC	1	NC	1
221		16	max	0	1	.006	2	0	1	-1.037e-7	10	NC	1	NC	1
222			min	0	3	-.005	3	0	3	-2.414e-4	3	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
223		17	max	0	1	.004	2	0	1	-1.037e-7	10	NC	1	NC	1
224			min	0	3	-.003	3	0	3	-2.414e-4	3	NC	1	NC	1
225		18	max	0	1	.002	2	0	1	-1.037e-7	10	NC	1	NC	1
226			min	0	3	-.002	3	0	3	-2.414e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	-1.037e-7	10	NC	1	NC	1
228			min	0	1	0	1	0	1	-2.414e-4	3	NC	1	NC	1
229	M10	1	max	.002	1	.009	2	0	3	3.984e-4	1	NC	3	NC	1
230			min	-.003	3	-.009	3	-.002	1	-5.114e-4	3	4343.431	2	NC	1
231		2	max	.002	1	.008	2	0	3	3.783e-4	1	NC	3	NC	1
232			min	-.003	3	-.009	3	-.001	1	-4.94e-4	3	4744.745	2	NC	1
233		3	max	.002	1	.008	2	0	3	3.582e-4	1	NC	1	NC	1
234			min	-.003	3	-.008	3	-.001	1	-4.766e-4	3	5222.905	2	NC	1
235		4	max	.002	1	.007	2	0	3	3.382e-4	1	NC	1	NC	1
236			min	-.002	3	-.008	3	-.001	1	-4.592e-4	3	5796.672	2	NC	1
237		5	max	.002	1	.006	2	0	3	3.181e-4	1	NC	1	NC	1
238			min	-.002	3	-.008	3	-.001	1	-4.418e-4	3	6491.118	2	NC	1
239		6	max	.001	1	.005	2	0	3	2.981e-4	1	NC	1	NC	1
240			min	-.002	3	-.007	3	-.001	1	-4.244e-4	3	7340.31	2	NC	1
241		7	max	.001	1	.005	2	0	3	2.78e-4	1	NC	1	NC	1
242			min	-.002	3	-.007	3	-.001	1	-4.07e-4	3	8391.434	2	NC	1
243		8	max	.001	1	.004	2	0	3	2.58e-4	1	NC	1	NC	1
244			min	-.002	3	-.006	3	0	1	-3.896e-4	3	9711.318	2	NC	1
245		9	max	.001	1	.003	2	0	3	2.379e-4	1	NC	1	NC	1
246			min	-.002	3	-.006	3	0	1	-3.722e-4	3	NC	1	NC	1
247		10	max	.001	1	.003	2	0	3	2.178e-4	1	NC	1	NC	1
248			min	-.001	3	-.006	3	0	1	-3.548e-4	3	NC	1	NC	1
249		11	max	0	1	.002	2	0	3	1.978e-4	1	NC	1	NC	1
250			min	-.001	3	-.005	3	0	1	-3.375e-4	3	NC	1	NC	1
251		12	max	0	1	.002	2	0	3	1.777e-4	1	NC	1	NC	1
252			min	-.001	3	-.005	3	0	1	-3.201e-4	3	NC	1	NC	1
253		13	max	0	1	.001	2	0	3	1.577e-4	1	NC	1	NC	1
254			min	0	3	-.004	3	0	1	-3.027e-4	3	NC	1	NC	1
255		14	max	0	1	.001	2	0	3	1.376e-4	1	NC	1	NC	1
256			min	0	3	-.003	3	0	1	-2.853e-4	3	NC	1	NC	1
257		15	max	0	1	0	2	0	3	1.175e-4	1	NC	1	NC	1
258			min	0	3	-.003	3	0	1	-2.679e-4	3	NC	1	NC	1
259		16	max	0	1	0	2	0	3	9.749e-5	1	NC	1	NC	1
260			min	0	3	-.002	3	0	1	-2.505e-4	3	NC	1	NC	1
261		17	max	0	1	0	2	0	3	7.743e-5	1	NC	1	NC	1
262			min	0	3	-.001	3	0	1	-2.331e-4	3	NC	1	NC	1
263		18	max	0	1	0	2	0	3	5.737e-5	1	NC	1	NC	1
264			min	0	3	0	3	0	1	-2.157e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	3.732e-5	1	NC	1	NC	1
266			min	0	1	0	1	0	1	-1.983e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	9.359e-5	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-1.788e-5	1	NC	1	NC	1
269		2	max	0	3	0	2	0	1	7.095e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-3.252e-5	1	NC	1	NC	1
271		3	max	0	3	0	2	0	1	4.831e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-4.715e-5	1	NC	1	NC	1
273		4	max	0	3	0	2	0	2	2.567e-5	3	NC	1	NC	1
274			min	0	2	-.003	3	-.001	3	-6.178e-5	1	NC	1	NC	1
275		5	max	0	3	0	2	0	2	3.027e-6	3	NC	1	NC	1
276			min	0	2	-.003	3	-.002	3	-7.641e-5	1	NC	1	NC	1
277		6	max	0	3	0	2	0	10	-3.459e-6	10	NC	1	NC	1
278			min	0	2	-.004	3	-.002	3	-9.105e-5	1	NC	1	NC	1
279		7	max	0	3	0	2	0	10	-3.945e-6	10	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
280			min	0	2	-.005	3	-.002	3	-1.057e-4	1	NC	1	NC	1
281		8	max	0	3	0	2	0	10	-4.43e-6	10	NC	1	NC	1
282			min	0	2	-.006	3	-.002	3	-1.203e-4	1	NC	1	NC	1
283		9	max	0	3	.001	2	0	10	-4.916e-6	10	NC	1	NC	1
284			min	0	2	-.006	3	-.002	3	-1.349e-4	1	NC	1	NC	1
285		10	max	0	3	.002	2	0	10	-5.402e-6	10	NC	1	NC	1
286			min	0	2	-.007	3	-.003	3	-1.496e-4	1	NC	1	NC	1
287		11	max	.001	3	.002	2	0	10	-5.887e-6	10	NC	1	NC	1
288			min	-.001	2	-.007	3	-.003	3	-1.642e-4	1	NC	1	NC	1
289		12	max	.001	3	.003	2	0	10	-6.373e-6	10	NC	1	NC	1
290			min	-.001	2	-.007	3	-.003	3	-1.788e-4	1	NC	1	NC	1
291		13	max	.001	3	.003	2	0	10	-6.859e-6	10	NC	1	NC	1
292			min	-.001	2	-.008	3	-.003	3	-1.935e-4	1	NC	1	NC	1
293		14	max	.001	3	.004	2	0	10	-7.345e-6	10	NC	1	NC	1
294			min	-.001	2	-.008	3	-.003	3	-2.081e-4	1	NC	1	NC	1
295		15	max	.002	3	.005	2	0	10	-7.83e-6	10	NC	1	NC	1
296			min	-.002	2	-.008	3	-.003	1	-2.234e-4	3	9490.633	2	NC	1
297		16	max	.002	3	.006	2	0	10	-8.316e-6	10	NC	1	NC	1
298			min	-.002	2	-.008	3	-.003	1	-2.46e-4	3	7996.049	2	NC	1
299		17	max	.002	3	.007	2	0	10	-8.802e-6	10	NC	1	NC	1
300			min	-.002	2	-.008	3	-.004	1	-2.687e-4	3	6849.759	2	NC	1
301		18	max	.002	3	.008	2	0	10	-9.287e-6	10	NC	1	NC	1
302			min	-.002	2	-.008	3	-.004	1	-2.913e-4	3	5959.296	2	NC	1
303		19	max	.002	3	.009	2	0	10	-9.773e-6	10	NC	3	NC	1
304			min	-.002	2	-.008	3	-.004	1	-3.14e-4	3	5260.607	2	NC	1
305	M12	1	max	.001	1	.01	2	.004	1	3.357e-4	3	NC	1	NC	2
306			min	0	12	-.009	3	0	10	1.068e-5	10	NC	1	5115.809	1
307		2	max	.001	1	.01	2	.003	1	3.357e-4	3	NC	1	NC	2
308			min	0	12	-.009	3	0	10	1.068e-5	10	NC	1	5579.446	1
309		3	max	.001	1	.009	2	.003	1	3.357e-4	3	NC	1	NC	2
310			min	0	12	-.008	3	0	10	1.068e-5	10	NC	1	6131.316	1
311		4	max	.001	1	.009	2	.003	1	3.357e-4	3	NC	1	NC	2
312			min	0	12	-.008	3	0	10	1.068e-5	10	NC	1	6794.68	1
313		5	max	.001	1	.008	2	.003	1	3.357e-4	3	NC	1	NC	2
314			min	0	12	-.007	3	0	10	1.068e-5	10	NC	1	7601.224	1
315		6	max	.001	1	.008	2	.002	1	3.357e-4	3	NC	1	NC	2
316			min	0	12	-.007	3	0	10	1.068e-5	10	NC	1	8595.021	1
317		7	max	0	1	.007	2	.002	1	3.357e-4	3	NC	1	NC	2
318			min	0	12	-.006	3	0	10	1.068e-5	10	NC	1	9838.851	1
319		8	max	0	1	.006	2	.002	1	3.357e-4	3	NC	1	NC	1
320			min	0	12	-.006	3	0	10	1.068e-5	10	NC	1	NC	1
321		9	max	0	1	.006	2	.001	1	3.357e-4	3	NC	1	NC	1
322			min	0	12	-.005	3	0	10	1.068e-5	10	NC	1	NC	1
323		10	max	0	1	.005	2	.001	1	3.357e-4	3	NC	1	NC	1
324			min	0	12	-.005	3	0	10	1.068e-5	10	NC	1	NC	1
325		11	max	0	1	.005	2	0	1	3.357e-4	3	NC	1	NC	1
326			min	0	12	-.004	3	0	10	1.068e-5	10	NC	1	NC	1
327		12	max	0	1	.004	2	0	1	3.357e-4	3	NC	1	NC	1
328			min	0	12	-.004	3	0	10	1.068e-5	10	NC	1	NC	1
329		13	max	0	1	.003	2	0	1	3.357e-4	3	NC	1	NC	1
330			min	0	12	-.003	3	0	10	1.068e-5	10	NC	1	NC	1
331		14	max	0	1	.003	2	0	1	3.357e-4	3	NC	1	NC	1
332			min	0	12	-.003	3	0	10	1.068e-5	10	NC	1	NC	1
333		15	max	0	1	.002	2	0	1	3.357e-4	3	NC	1	NC	1
334			min	0	12	-.002	3	0	10	1.068e-5	10	NC	1	NC	1
335		16	max	0	1	.002	2	0	1	3.357e-4	3	NC	1	NC	1
336			min	0	12	-.002	3	0	10	1.068e-5	10	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
337		17	max	0	1	.001	2	0	1	3.357e-4	3	NC	1	NC	1
338			min	0	12	-.001	3	0	10	1.068e-5	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	3.357e-4	3	NC	1	NC	1
340			min	0	12	0	3	0	10	1.068e-5	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	3.357e-4	3	NC	1	NC	1
342			min	0	1	0	1	0	1	1.068e-5	10	NC	1	NC	1
343	M1	1	max	.008	3	.024	3	.003	3	7.052e-3	2	NC	1	NC	1
344			min	-.008	2	-.02	2	-.001	1	-1.015e-2	3	NC	1	NC	1
345		2	max	.008	3	.014	3	.003	3	3.468e-3	2	NC	4	NC	1
346			min	-.008	2	-.012	2	-.003	1	-5.008e-3	3	4865.011	3	NC	1
347		3	max	.008	3	.005	3	.002	3	3.855e-5	3	NC	4	NC	1
348			min	-.008	2	-.004	2	-.004	1	-2.243e-4	1	2520.273	3	NC	1
349		4	max	.008	3	.003	2	.002	3	4.012e-5	3	NC	4	NC	1
350			min	-.008	2	-.003	3	-.005	1	-1.905e-4	1	1796.072	3	NC	1
351		5	max	.008	3	.01	2	.001	3	4.168e-5	3	NC	4	NC	1
352			min	-.008	2	-.009	3	-.005	1	-1.566e-4	1	1450.807	3	NC	1
353		6	max	.008	3	.015	2	0	3	4.325e-5	3	NC	4	NC	1
354			min	-.008	2	-.014	3	-.005	1	-1.228e-4	1	1257.687	2	NC	1
355		7	max	.008	3	.019	2	0	3	4.481e-5	3	NC	4	NC	1
356			min	-.008	2	-.018	3	-.004	1	-8.9e-5	1	1119.268	2	NC	1
357		8	max	.008	3	.022	2	0	3	4.637e-5	3	NC	4	NC	1
358			min	-.008	2	-.021	3	-.003	1	-5.518e-5	1	1032.181	2	NC	1
359		9	max	.008	3	.024	2	0	3	4.794e-5	3	NC	4	NC	1
360			min	-.008	2	-.022	3	-.002	1	-2.535e-5	9	980.204	2	NC	1
361		10	max	.008	3	.025	2	0	3	4.95e-5	3	NC	4	NC	1
362			min	-.008	2	-.023	3	-.001	1	-1.203e-6	9	955.571	2	NC	1
363		11	max	.008	3	.025	2	0	3	5.107e-5	3	NC	4	NC	1
364			min	-.008	2	-.022	3	0	9	1.618e-6	15	955.437	2	NC	1
365		12	max	.008	3	.023	2	.001	1	8.012e-5	1	NC	4	NC	1
366			min	-.008	2	-.02	3	0	15	3.096e-6	15	980.827	2	NC	1
367		13	max	.008	3	.02	2	.002	1	1.139e-4	1	NC	4	NC	1
368			min	-.008	2	-.017	3	0	15	4.575e-6	15	1037.222	2	NC	1
369		14	max	.008	3	.016	2	.003	1	1.478e-4	1	NC	4	NC	1
370			min	-.008	2	-.013	3	0	15	6.053e-6	15	1137.356	2	NC	1
371		15	max	.008	3	.01	2	.003	1	1.816e-4	1	NC	4	NC	1
372			min	-.008	2	-.009	3	0	15	7.532e-6	15	1309.271	2	NC	1
373		16	max	.008	3	.003	2	.003	1	2.055e-4	1	NC	4	NC	1
374			min	-.008	2	-.003	3	0	15	8.57e-6	15	1621.765	2	NC	1
375		17	max	.008	3	.004	3	.002	1	5.733e-5	3	NC	4	NC	1
376			min	-.008	2	-.006	2	0	15	-2.001e-5	9	2296.587	2	NC	1
377		18	max	.008	3	.012	3	0	1	5.053e-3	2	NC	4	NC	1
378			min	-.008	2	-.016	2	0	15	-2.56e-3	3	4450.423	2	NC	1
379		19	max	.008	3	.02	3	0	3	1.018e-2	2	NC	1	NC	1
380			min	-.008	2	-.027	2	0	1	-5.227e-3	3	NC	1	NC	1
381	M5	1	max	.025	3	.076	3	.003	3	5.891e-6	3	NC	1	NC	1
382			min	-.028	2	-.066	2	-.002	1	0	15	NC	1	NC	1
383		2	max	.025	3	.045	3	.005	3	1.226e-4	3	NC	4	NC	1
384			min	-.028	2	-.038	2	-.001	1	-2.468e-5	1	1533.258	3	NC	1
385		3	max	.025	3	.016	3	.006	3	2.371e-4	3	NC	5	NC	1
386			min	-.028	2	-.012	2	-.001	1	-4.895e-5	1	794.647	3	NC	1
387		4	max	.025	3	.011	2	.007	3	2.292e-4	3	NC	5	NC	1
388			min	-.028	2	-.009	3	-.001	1	-4.632e-5	1	566.919	3	NC	1
389		5	max	.025	3	.031	2	.007	3	2.214e-4	3	NC	5	NC	1
390			min	-.028	2	-.029	3	-.001	1	-4.39e-5	9	458.225	2	NC	1
391		6	max	.025	3	.048	2	.008	3	2.135e-4	3	NC	5	NC	1
392			min	-.028	2	-.045	3	-.001	1	-4.169e-5	9	388.724	2	9306.49	3
393		7	max	.025	3	.062	2	.008	3	2.057e-4	3	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
394			min	-.028	2	-.058	3	-.001	1	-3.949e-5	9	345.774	2	8835.295	3
395		8	max	.025	3	.072	2	.008	3	1.979e-4	3	NC	5	NC	1
396			min	-.028	2	-.066	3	-.001	1	-3.729e-5	9	318.736	2	8723.941	3
397		9	max	.024	3	.079	2	.007	3	1.9e-4	3	NC	5	NC	1
398			min	-.028	2	-.071	3	-.001	1	-3.509e-5	9	302.576	2	8903.027	3
399		10	max	.024	3	.082	2	.007	3	1.822e-4	3	NC	5	NC	1
400			min	-.028	2	-.072	3	-.001	1	-3.288e-5	9	294.884	2	9363.246	3
401		11	max	.024	3	.081	2	.006	3	1.743e-4	3	NC	5	NC	1
402			min	-.028	2	-.07	3	-.001	1	-3.068e-5	9	294.773	2	NC	1
403		12	max	.024	3	.075	2	.006	3	1.665e-4	3	NC	5	NC	1
404			min	-.028	2	-.064	3	-.001	1	-2.848e-5	9	302.556	2	NC	1
405		13	max	.024	3	.066	2	.005	3	1.587e-4	3	NC	5	NC	1
406			min	-.028	2	-.055	3	0	1	-2.628e-5	9	319.921	2	NC	1
407		14	max	.024	3	.052	2	.004	3	1.508e-4	3	NC	5	NC	1
408			min	-.028	2	-.042	3	0	1	-2.407e-5	9	350.802	2	NC	1
409		15	max	.024	3	.033	2	.003	3	1.43e-4	3	NC	5	NC	1
410			min	-.028	2	-.027	3	0	1	-2.187e-5	9	403.869	2	NC	1
411		16	max	.024	3	.009	2	.003	3	1.306e-4	3	NC	5	NC	1
412			min	-.028	2	-.008	3	0	1	-2.125e-5	9	500.41	2	NC	1
413		17	max	.024	3	.014	3	.002	3	1.055e-5	3	NC	5	NC	1
414			min	-.028	2	-.02	2	0	1	-6.341e-5	1	709.278	2	NC	1
415		18	max	.024	3	.037	3	.001	3	3.706e-6	3	NC	4	NC	1
416			min	-.028	2	-.053	2	0	1	-3.248e-5	1	1375.15	2	NC	1
417		19	max	.024	3	.062	3	0	3	-3.224e-8	15	NC	1	NC	1
418			min	-.028	2	-.088	2	0	1	-1.003e-6	3	NC	1	NC	1
419	M9	1	max	.008	3	.024	3	.003	3	1.016e-2	3	NC	1	NC	1
420			min	-.008	2	-.02	2	-.002	1	-7.052e-3	2	NC	1	NC	1
421		2	max	.008	3	.014	3	.001	3	5.005e-3	3	NC	4	NC	1
422			min	-.008	2	-.012	2	0	9	-3.468e-3	2	4866.837	3	NC	1
423		3	max	.008	3	.005	3	.002	1	1.125e-4	1	NC	4	NC	1
424			min	-.008	2	-.004	2	0	3	-5.643e-5	3	2521.234	3	NC	1
425		4	max	.008	3	.003	2	.002	1	8.331e-5	1	NC	4	NC	1
426			min	-.008	2	-.003	3	-.001	3	-6.126e-5	3	1796.734	3	NC	1
427		5	max	.008	3	.01	2	.002	1	5.412e-5	1	NC	4	NC	1
428			min	-.008	2	-.009	3	-.002	3	-6.608e-5	3	1451.294	3	NC	1
429		6	max	.008	3	.015	2	.002	1	2.493e-5	1	NC	4	NC	1
430			min	-.008	2	-.015	3	-.003	3	-7.091e-5	3	1258.026	2	8789.948	3
431		7	max	.008	3	.019	2	.002	1	1.275e-5	2	NC	4	NC	1
432			min	-.008	2	-.019	3	-.004	3	-7.574e-5	3	1119.582	2	8018.196	3
433		8	max	.008	3	.022	2	0	1	3.396e-6	2	NC	4	NC	1
434			min	-.008	2	-.021	3	-.004	3	-8.057e-5	3	1032.482	2	7586.222	3
435		9	max	.008	3	.024	2	0	2	-1.239e-6	10	NC	4	NC	1
436			min	-.008	2	-.023	3	-.005	3	-8.54e-5	3	980.5	2	7394.935	3
437		10	max	.008	3	.025	2	0	2	-2.376e-6	10	NC	4	NC	1
438			min	-.008	2	-.023	3	-.005	3	-9.184e-5	1	955.868	2	7401.799	3
439		11	max	.008	3	.025	2	0	10	-3.513e-6	10	NC	4	NC	1
440			min	-.008	2	-.022	3	-.005	3	-1.21e-4	1	955.743	2	7598.881	3
441		12	max	.008	3	.023	2	0	10	-4.649e-6	10	NC	4	NC	1
442			min	-.008	2	-.02	3	-.004	3	-1.502e-4	1	981.149	2	8008.173	3
443		13	max	.008	3	.02	2	0	10	-5.786e-6	10	NC	4	NC	1
444			min	-.008	2	-.018	3	-.004	3	-1.794e-4	1	1037.569	2	8689.516	3
445		14	max	.008	3	.016	2	0	10	-6.923e-6	10	NC	4	NC	1
446			min	-.008	2	-.014	3	-.004	1	-2.086e-4	1	1137.743	2	9767.409	3
447		15	max	.008	3	.01	2	0	10	-8.059e-6	10	NC	4	NC	1
448			min	-.008	2	-.009	3	-.005	1	-2.378e-4	1	1309.719	2	NC	1
449		16	max	.008	3	.003	2	0	10	-8.909e-6	10	NC	4	NC	1
450			min	-.008	2	-.003	3	-.004	1	-2.601e-4	1	1622.314	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
451		17	max	.008	3	.004	3	0	10	6.967e-5	3	NC	4	NC	1
452			min	-.008	2	-.006	2	-.004	1	-1.193e-4	1	2297.31	2	NC	1
453		18	max	.008	3	.012	3	0	10	2.625e-3	3	NC	4	NC	1
454			min	-.008	2	-.016	2	-.003	1	-5.053e-3	2	4451.779	2	NC	1
455		19	max	.008	3	.02	3	0	3	5.225e-3	3	NC	1	NC	1
456			min	-.008	2	-.027	2	0	1	-1.018e-2	2	NC	1	NC	1
457	M13	1	max	.002	1	.024	3	.008	3	3.72e-3	3	NC	1	NC	1
458			min	-.003	3	-.02	2	-.008	2	-3.261e-3	2	NC	1	NC	1
459		2	max	.002	1	.083	3	.006	3	4.625e-3	3	NC	4	NC	1
460			min	-.003	3	-.061	2	-.006	2	-4.068e-3	2	1832.453	3	NC	1
461		3	max	.002	1	.132	3	.013	1	5.531e-3	3	NC	5	NC	2
462			min	-.003	3	-.096	2	-.005	10	-4.875e-3	2	998.978	3	6132.838	1
463		4	max	.002	1	.165	3	.021	1	6.436e-3	3	NC	5	NC	2
464			min	-.003	3	-.119	2	-.005	10	-5.681e-3	2	766.571	3	4342.193	1
465		5	max	.002	1	.178	3	.023	1	7.341e-3	3	NC	5	NC	2
466			min	-.003	3	-.13	2	-.006	10	-6.488e-3	2	701.055	3	3968.445	1
467		6	max	.002	1	.172	3	.019	1	8.246e-3	3	NC	5	NC	2
468			min	-.003	3	-.127	2	-.008	10	-7.294e-3	2	730.649	3	4560.177	1
469		7	max	.002	1	.15	3	.016	3	9.151e-3	3	NC	5	NC	2
470			min	-.003	3	-.113	2	-.013	2	-8.101e-3	2	858.571	3	7250.734	1
471		8	max	.002	1	.119	3	.019	3	1.006e-2	3	NC	4	NC	1
472			min	-.003	3	-.094	2	-.02	2	-8.908e-3	2	1136.552	3	9495.324	2
473		9	max	.002	1	.09	3	.022	3	1.096e-2	3	NC	4	NC	1
474			min	-.003	3	-.075	2	-.025	2	-9.714e-3	2	1637.009	3	6331.985	2
475		10	max	.002	1	.076	3	.025	3	1.187e-2	3	NC	4	NC	4
476			min	-.003	3	-.066	2	-.028	2	-1.052e-2	2	2056.49	3	5514.799	2
477		11	max	.001	1	.09	3	.027	3	1.096e-2	3	NC	4	NC	1
478			min	-.003	3	-.075	2	-.025	2	-9.714e-3	2	1637.007	3	5762.991	3
479		12	max	.001	1	.119	3	.028	3	1.006e-2	3	NC	4	NC	1
480			min	-.003	3	-.094	2	-.02	2	-8.908e-3	2	1136.551	3	5586.61	3
481		13	max	.001	1	.15	3	.027	3	9.157e-3	3	NC	5	NC	2
482			min	-.003	3	-.113	2	-.013	2	-8.101e-3	2	858.57	3	5823.58	3
483		14	max	.001	1	.172	3	.025	3	8.254e-3	3	NC	5	NC	2
484			min	-.003	3	-.127	2	-.008	10	-7.294e-3	2	730.649	3	4556.447	1
485		15	max	.001	1	.178	3	.023	1	7.35e-3	3	NC	5	NC	2
486			min	-.003	3	-.13	2	-.007	10	-6.488e-3	2	701.055	3	3973.11	1
487		16	max	.001	1	.165	3	.02	1	6.447e-3	3	NC	5	NC	2
488			min	-.003	3	-.119	2	-.005	10	-5.681e-3	2	766.571	3	4355.32	1
489		17	max	.001	1	.132	3	.014	3	5.544e-3	3	NC	5	NC	2
490			min	-.003	3	-.096	2	-.005	10	-4.875e-3	2	998.977	3	6165.837	1
491		18	max	.001	1	.083	3	.011	3	4.641e-3	3	NC	4	NC	1
492			min	-.003	3	-.061	2	-.006	2	-4.068e-3	2	1832.451	3	NC	1
493		19	max	.001	1	.024	3	.008	3	3.738e-3	3	NC	1	NC	1
494			min	-.003	3	-.02	2	-.008	2	-3.262e-3	2	NC	1	NC	1
495	M16	1	max	0	1	.02	3	.008	3	4.131e-3	2	NC	1	NC	1
496			min	0	3	-.027	2	-.008	2	-3.025e-3	3	NC	1	NC	1
497		2	max	0	1	.05	3	.011	3	5.159e-3	2	NC	4	NC	1
498			min	0	3	-.086	2	-.006	2	-3.734e-3	3	1825.988	2	NC	1
499		3	max	0	1	.076	3	.014	3	6.187e-3	2	NC	5	NC	2
500			min	0	3	-.136	2	-.005	10	-4.443e-3	3	993.381	2	6145.598	1
501		4	max	0	1	.094	3	.02	1	7.215e-3	2	NC	5	NC	2
502			min	0	3	-.169	2	-.005	10	-5.152e-3	3	759.462	2	4351.329	1
503		5	max	0	1	.103	3	.023	1	8.243e-3	2	NC	5	NC	2
504			min	0	3	-.184	2	-.006	10	-5.861e-3	3	690.415	2	3978.168	1
505		6	max	0	1	.102	3	.023	3	9.271e-3	2	NC	5	NC	2
506			min	0	3	-.179	2	-.008	10	-6.57e-3	3	712.662	2	4575.58	1
507		7	max	0	1	.094	3	.025	3	1.03e-2	2	NC	5	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
508			min	0	3	-.158	2	-.013	2	-7.278e-3	3	824.094	2	6449.812	3
509		8	max	0	1	.081	3	.025	3	1.133e-2	2	NC	4	NC	1
510			min	0	3	-.129	2	-.02	2	-7.987e-3	3	1061.036	2	6207.41	3
511		9	max	0	1	.068	3	.025	3	1.235e-2	2	NC	4	NC	1
512			min	0	3	-.101	2	-.025	2	-8.696e-3	3	1461.07	2	6296.645	3
513		10	max	0	1	.062	3	.024	3	1.338e-2	2	NC	4	NC	4
514			min	0	3	-.088	2	-.028	2	-9.405e-3	3	1771.813	2	5539.192	2
515		11	max	0	1	.068	3	.023	3	1.235e-2	2	NC	4	NC	1
516			min	0	3	-.101	2	-.025	2	-8.694e-3	3	1461.07	2	6362.824	2
517		12	max	0	1	.081	3	.021	3	1.133e-2	2	NC	4	NC	1
518			min	0	3	-.129	2	-.02	2	-7.984e-3	3	1061.036	2	8055.4	3
519		13	max	0	1	.094	3	.02	3	1.03e-2	2	NC	5	NC	2
520			min	0	3	-.158	2	-.013	2	-7.273e-3	3	824.094	2	7288.115	1
521		14	max	0	1	.102	3	.019	1	9.271e-3	2	NC	5	NC	2
522			min	0	3	-.179	2	-.008	10	-6.562e-3	3	712.662	2	4582.163	1
523		15	max	0	1	.103	3	.023	1	8.244e-3	2	NC	5	NC	2
524			min	0	3	-.184	2	-.006	10	-5.852e-3	3	690.415	2	3990.71	1
525		16	max	0	1	.094	3	.02	1	7.216e-3	2	NC	5	NC	2
526			min	0	3	-.169	2	-.005	10	-5.141e-3	3	759.462	2	4373.012	1
527		17	max	0	1	.076	3	.013	1	6.188e-3	2	NC	5	NC	2
528			min	0	3	-.136	2	-.005	10	-4.43e-3	3	993.381	2	6192.006	1
529		18	max	0	1	.05	3	.009	3	5.161e-3	2	NC	4	NC	1
530			min	0	3	-.086	2	-.006	2	-3.719e-3	3	1825.988	2	NC	1
531		19	max	0	1	.02	3	.008	3	4.133e-3	2	NC	1	NC	1
532			min	0	3	-.027	2	-.008	2	-3.009e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	3.912e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-4.943e-5	2	NC	1	NC	1
535		2	max	0	3	0	15	0	1	8.152e-4	3	NC	1	NC	1
536			min	0	2	-.004	4	0	3	-4.708e-4	2	NC	1	NC	1
537		3	max	0	3	-.002	15	.003	1	1.239e-3	3	NC	1	NC	1
538			min	0	2	-.008	4	-.003	3	-8.922e-4	2	8800.218	4	NC	1
539		4	max	0	3	-.003	15	.006	1	1.663e-3	3	NC	3	NC	4
540			min	0	2	-.011	4	-.007	3	-1.314e-3	2	6037.463	4	5571.118	3
541		5	max	0	3	-.003	15	.009	2	2.087e-3	3	NC	5	NC	4
542			min	0	2	-.014	4	-.011	3	-1.735e-3	2	4711.094	4	3668.846	3
543		6	max	0	3	-.004	15	.014	2	2.512e-3	3	NC	5	NC	4
544			min	-.001	2	-.017	4	-.017	3	-2.156e-3	2	3964.884	4	2677.612	3
545		7	max	0	3	-.005	15	.018	2	2.936e-3	3	NC	15	NC	4
546			min	-.001	2	-.019	4	-.022	3	-2.578e-3	2	3516.136	4	2096.734	3
547		8	max	0	3	-.005	15	.022	2	3.36e-3	3	NC	15	NC	4
548			min	-.001	2	-.021	4	-.027	3	-2.999e-3	2	3246.821	4	1731.032	3
549		9	max	0	3	-.005	15	.026	2	3.784e-3	3	NC	15	NC	4
550			min	-.002	2	-.022	4	-.031	3	-3.42e-3	2	3101.859	4	1491.49	3
551		10	max	0	3	-.005	15	.028	2	4.208e-3	3	NC	15	NC	4
552			min	-.002	2	-.022	4	-.035	3	-3.842e-3	2	3056	4	1333.329	3
553		11	max	0	3	-.005	15	.03	2	4.632e-3	3	NC	15	NC	4
554			min	-.002	2	-.022	4	-.037	3	-4.263e-3	2	3101.859	4	1233.021	3
555		12	max	.001	3	-.005	15	.03	2	5.056e-3	3	NC	15	NC	5
556			min	-.002	2	-.021	4	-.038	3	-4.685e-3	2	3246.821	4	1178.911	3
557		13	max	.001	3	-.005	15	.029	2	5.48e-3	3	NC	15	NC	5
558			min	-.002	2	-.019	4	-.037	3	-5.106e-3	2	3516.136	4	1167.671	3
559		14	max	.001	3	-.004	15	.027	1	5.904e-3	3	NC	5	NC	4
560			min	-.003	2	-.017	4	-.034	3	-5.527e-3	2	3964.884	4	1204.47	3
561		15	max	.001	3	-.003	15	.022	1	6.328e-3	3	NC	5	NC	4
562			min	-.003	2	-.015	4	-.028	3	-5.949e-3	2	4711.094	4	1308.087	3
563		16	max	.001	3	-.003	15	.016	1	6.752e-3	3	NC	3	NC	4
564			min	-.003	2	-.012	4	-.018	3	-6.37e-3	2	6037.463	4	1529.429	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
565		17	max	.001	3	0	2	.006	1	7.176e-3	3	NC	1	NC	4
566			min	-.003	2	-.008	4	-.006	3	-6.791e-3	2	8800.218	4	2028.146	3
567		18	max	.002	3	.003	2	.01	3	7.6e-3	3	NC	1	NC	4
568			min	-.004	2	-.005	4	-.012	2	-7.213e-3	2	NC	1	3611.781	3
569		19	max	.002	3	.006	2	.03	3	8.025e-3	3	NC	1	NC	1
570			min	-.004	2	-.001	9	-.03	2	-7.634e-3	2	NC	1	NC	1
571	M16A	1	max	0	10	.001	2	.009	3	2.298e-3	3	NC	1	NC	1
572			min	-.002	3	-.001	3	-.009	2	-2.293e-3	2	NC	1	NC	1
573		2	max	0	10	0	15	.002	3	2.211e-3	3	NC	1	NC	1
574			min	-.002	3	-.004	4	-.004	2	-2.19e-3	2	NC	1	NC	1
575		3	max	0	10	-.002	15	.004	1	2.123e-3	3	NC	1	NC	4
576			min	-.001	3	-.008	4	-.003	3	-2.086e-3	2	8800.218	4	5753.566	3
577		4	max	0	10	-.003	15	.007	1	2.036e-3	3	NC	3	NC	4
578			min	-.001	3	-.011	4	-.008	3	-1.983e-3	2	6037.463	4	4381.621	3
579		5	max	0	10	-.003	15	.01	1	1.948e-3	3	NC	5	NC	4
580			min	-.001	3	-.015	4	-.01	3	-1.88e-3	2	4711.094	4	3789.744	3
581		6	max	0	10	-.004	15	.011	1	1.861e-3	3	NC	5	NC	4
582			min	-.001	3	-.017	4	-.012	3	-1.777e-3	2	3964.884	4	3534.872	3
583		7	max	0	10	-.005	15	.012	1	1.773e-3	3	NC	15	NC	4
584			min	-.001	3	-.019	4	-.013	3	-1.673e-3	2	3516.136	4	3478.73	3
585		8	max	0	10	-.005	15	.011	1	1.685e-3	3	NC	15	NC	4
586			min	-.001	3	-.021	4	-.013	3	-1.57e-3	2	3246.821	4	3574.94	3
587		9	max	0	10	-.005	15	.011	1	1.598e-3	3	NC	15	NC	4
588			min	0	3	-.022	4	-.012	3	-1.467e-3	2	3101.859	4	3819.047	3
589		10	max	0	10	-.005	15	.01	1	1.51e-3	3	NC	15	NC	4
590			min	0	3	-.022	4	-.011	3	-1.364e-3	2	3056	4	4237.632	3
591		11	max	0	10	-.005	15	.009	1	1.423e-3	3	NC	15	NC	4
592			min	0	3	-.022	4	-.01	3	-1.26e-3	2	3101.859	4	4895.013	3
593		12	max	0	10	-.005	15	.007	1	1.335e-3	3	NC	15	NC	4
594			min	0	3	-.021	4	-.008	3	-1.157e-3	2	3246.821	4	5919.615	3
595		13	max	0	10	-.004	15	.005	1	1.248e-3	3	NC	15	NC	2
596			min	0	3	-.019	4	-.006	3	-1.054e-3	2	3516.136	4	7572.3	3
597		14	max	0	10	-.004	15	.004	1	1.16e-3	3	NC	5	NC	1
598			min	0	3	-.017	4	-.004	3	-9.505e-4	2	3964.884	4	NC	1
599		15	max	0	10	-.003	15	.002	1	1.073e-3	3	NC	5	NC	1
600			min	0	3	-.014	4	-.002	3	-8.472e-4	2	4711.094	4	NC	1
601		16	max	0	10	-.003	15	.001	9	9.85e-4	3	NC	3	NC	1
602			min	0	3	-.011	4	0	3	-7.44e-4	2	6037.463	4	NC	1
603		17	max	0	10	-.002	15	0	4	8.975e-4	3	NC	1	NC	1
604			min	0	3	-.008	4	0	2	-6.407e-4	2	8800.218	4	NC	1
605		18	max	0	10	0	15	0	3	8.099e-4	3	NC	1	NC	1
606			min	0	3	-.004	4	0	2	-5.374e-4	2	NC	1	NC	1
607		19	max	0	1	0	1	0	1	7.224e-4	3	NC	1	NC	1
608			min	0	1	0	1	0	1	-4.342e-4	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

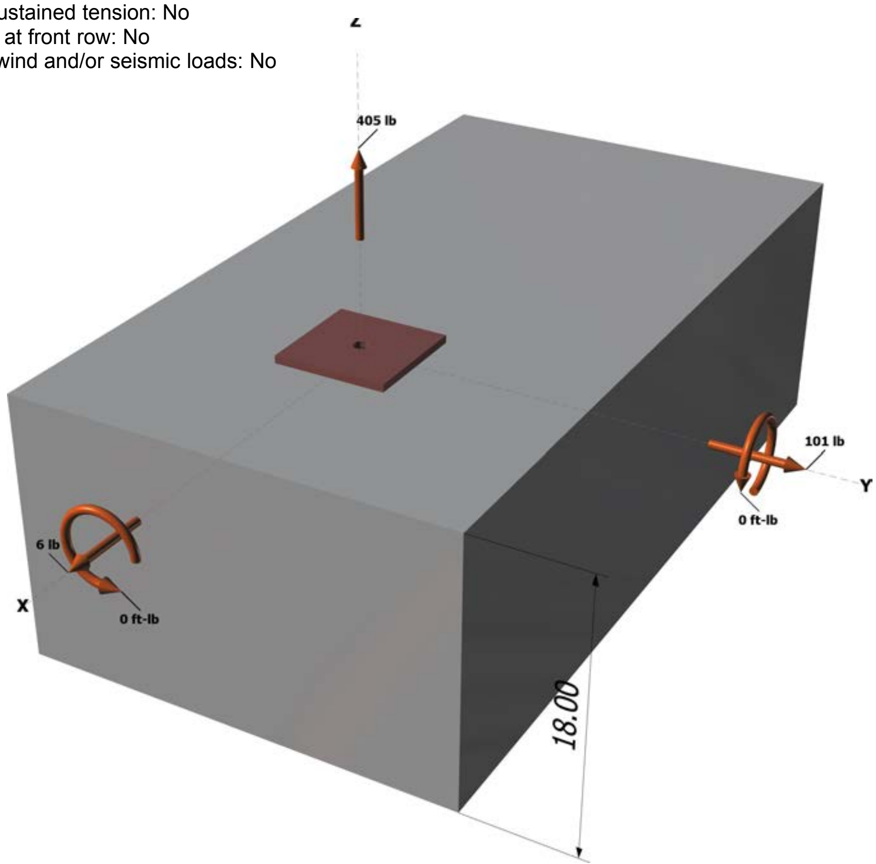
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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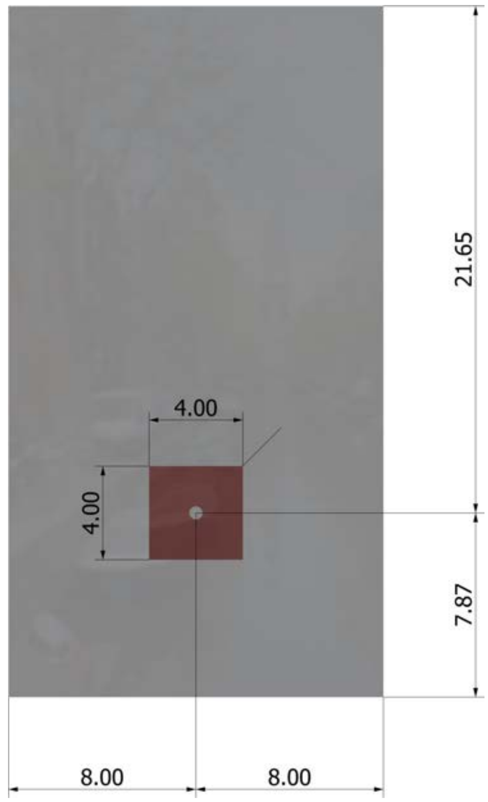


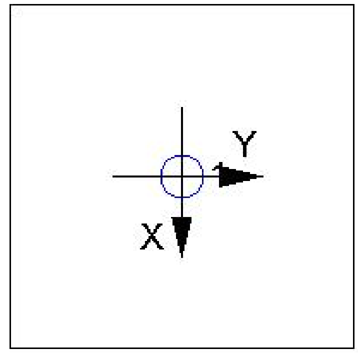
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\, (A_{Nc} / A_{Nco})\, \Psi_{ed,N}\, \Psi_{c,N}\, \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\, (A_{Na} / A_{Na0})\, \Psi_{ed,Na}\, \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\, (A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\, (A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\, (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\, (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi \min|k_{cp}N_a\,;\, k_{cp}N_{cb}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\, k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.

Anchor Designer™
Software
Version 2.4.5673.0

Company:	Schletter, Inc.	Date:	12/10/2015
Engineer:	HCV	Page:	1/5
Project:	Standard PVMini - Worst Case		
Address:			
Phone:			
E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

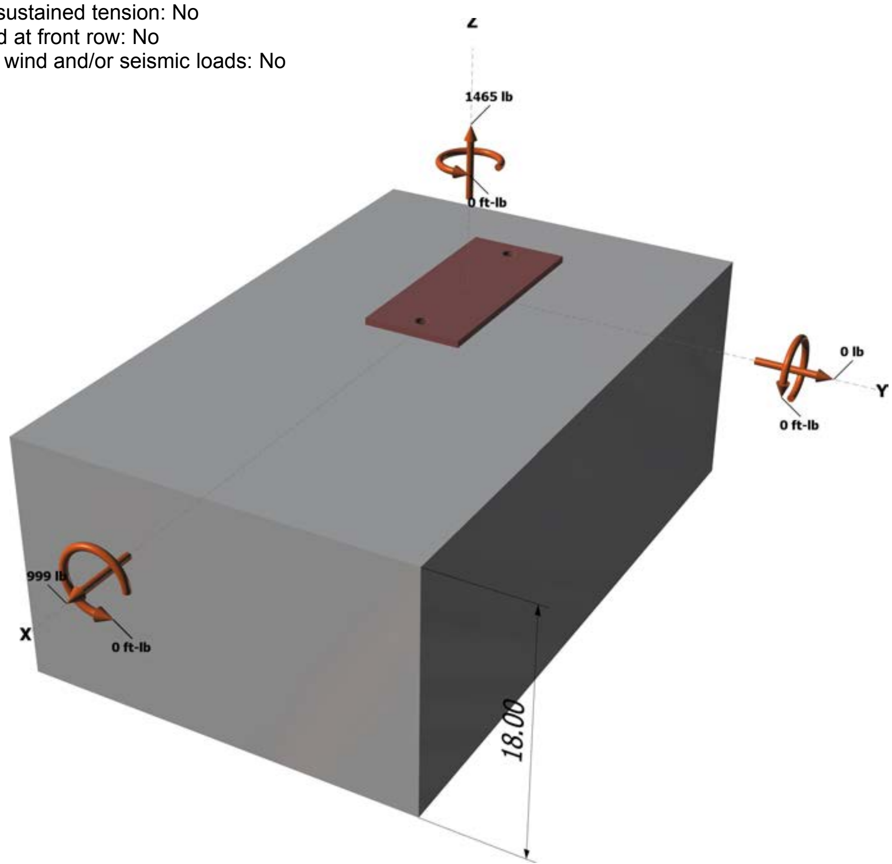
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



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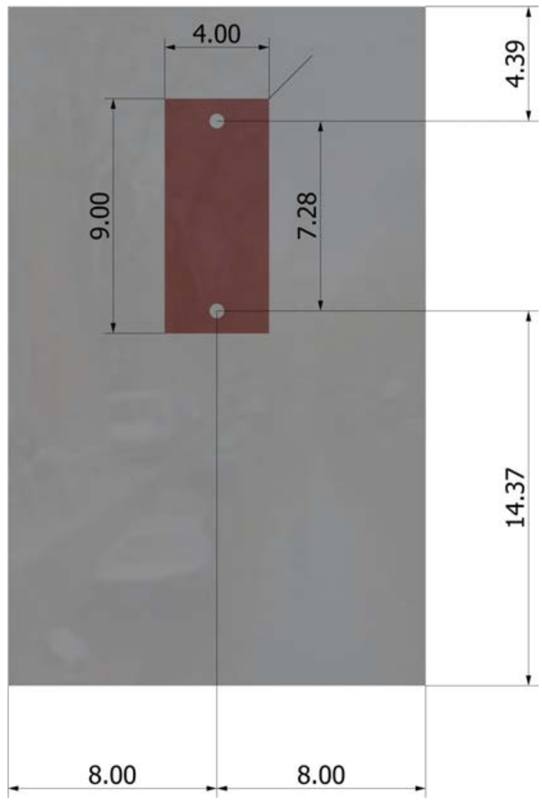


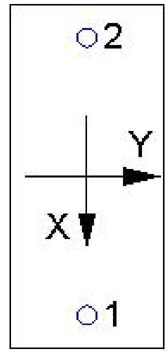
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\,\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\,\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.