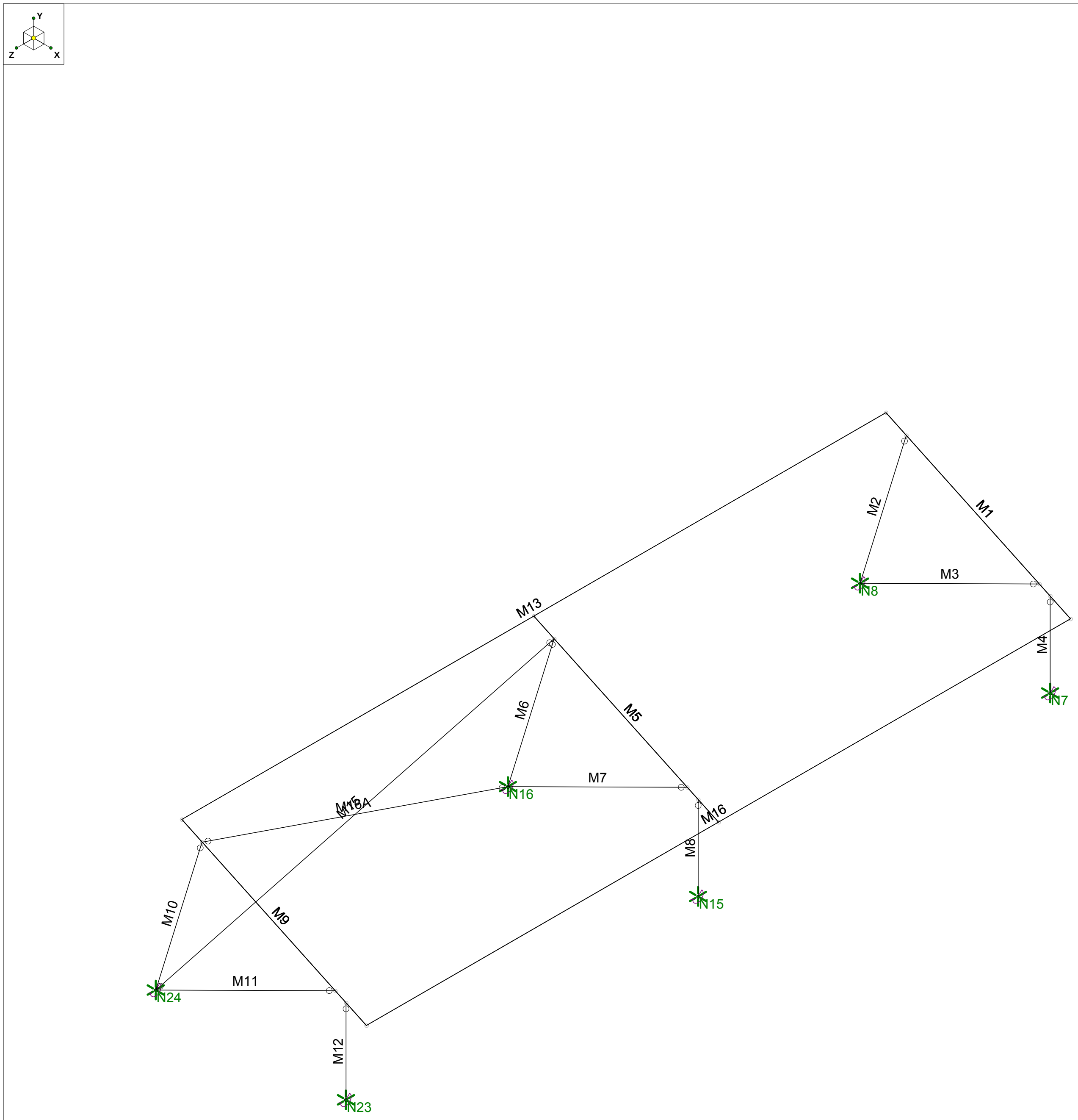


Schletter, Inc.	Standard PVMini Racking System	25° Tilt w/ Seismic Design
HCV	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

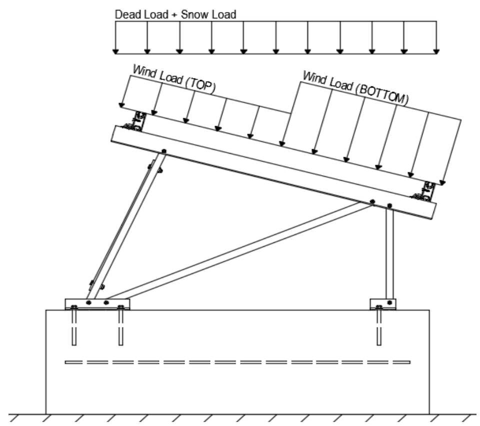
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

Maximum			Minimum		
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row = 1
Module Tilt = 25°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads

Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 18.56 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.82
C_e = 0.90
C_t = 1.20

2.3 Wind Loads

Design Wind Speed, V = 130 mph
Height ≤ 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 26.53 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.1	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.7	
$Cf-_{TOP}$	=	-2.2	*(Suction)*
$Cf-_{BOTTOM}$	=	-1	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

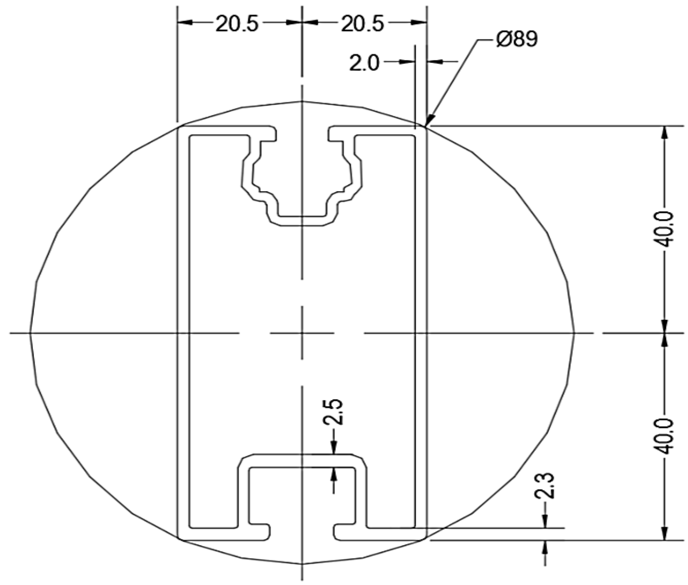
Purlins	Location	Diagonal Struts	Location	Front Reactions	Location
M13	Top	M3	Outer	N7	Outer
M16	Bottom	M7	Inner	N15	Inner
		M11	Outer	N23	Outer
Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer
Front Struts	Location	**Bracing**			
M4	Outer	M15			
M8	Inner	M16A			
M12	Outer				

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

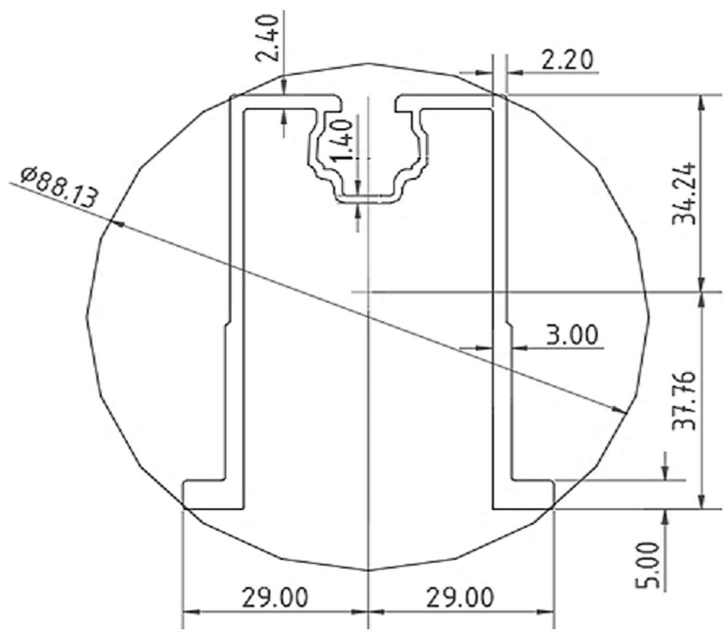
Purlin Type =	**ProfiPlusXT**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	69	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.48	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	22.71	ksi
S_y =	0.75	in^3
S_x =	0.44	in^3
E =	10100	ksi
I_y =	1.20	in^4
I_x =	0.36	in^4
A =	0.96	in^2
g =	1.15	lbs/ft
M_y =	0.581	k-ft
M_z =	0.127	k-ft
$M_{y\ allowable}$ =	1.831	k-ft
$M_{z\ allowable}$ =	0.838	k-ft
Utilization =	47%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

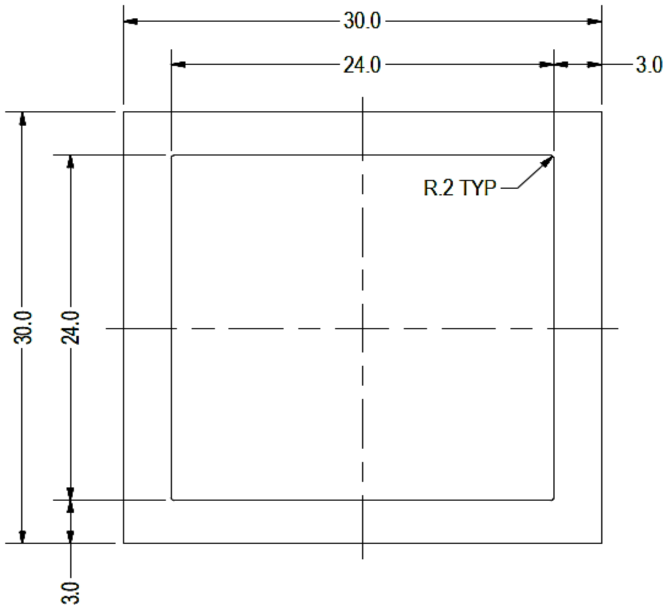
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.45	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	0.521	k-ft
M_z =	0.000	k-ft
P_n =	0.292	k
$M_{y\ allowable}$ =	1.445	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	38%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

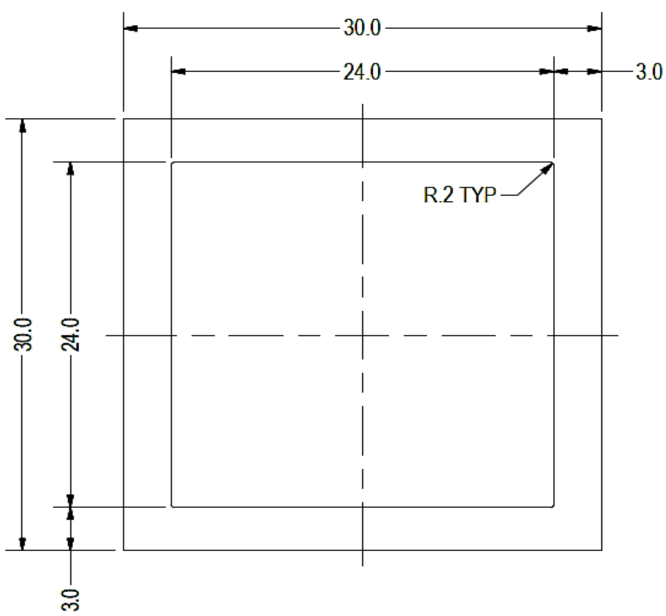
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.037	k-ft
P_n =	0.209	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	10%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

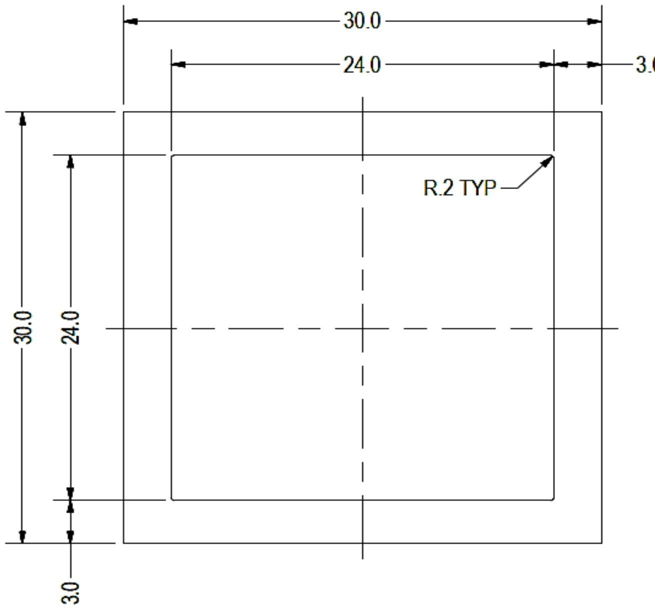
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.475	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	12%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

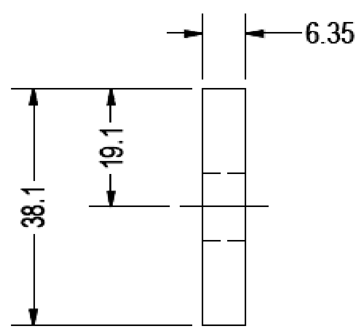
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	36.18	in
$\Phi F_{ty\ AXIAL}$ =	11.59	ksi
$\Phi F_{ty\ BENDING}$ =	30.23	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.882	k
$M_{y\ allowable}$ =	0.410	k-ft
$M_{z\ allowable}$ =	0.410	k-ft
$P_{n\ allowable}$ =	5.820	k
Utilization =	15%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.004	k-ft
P_n =	0.211	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	11%	



A cross brace kit is required every 18 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

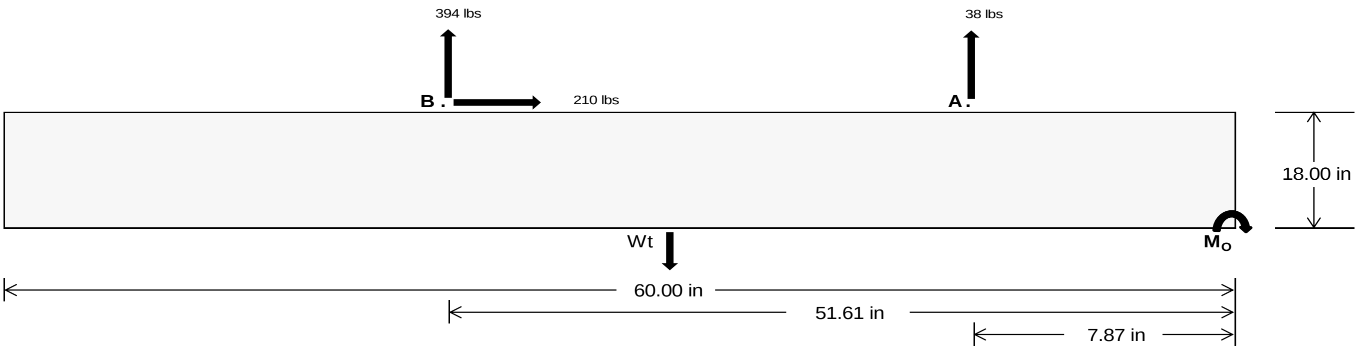
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	169.65	1711.20	k
Compressive Load =	1405.74	1225.47	k
Lateral Load =	30.61	911.42	k
Moment (Weak Axis) =	0.05	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



<u>Concrete Properties</u>
Weight of Concrete = 145 pcf
Compressive Strength = 2500 psi
Yield Strength = 60000 psi

<u>Footing Reinforcement</u>
Use fiber reinforcing with (1) #5 rebar.

<u>Overturning Check</u>
M_O = 24406.0 in-lbs
Resisting Force Required = 813.53 lbs
S.F. = 1.67
Weight Required = 1355.89 lbs
Minimum Width = 21 in in
Weight Provided = 1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.

<u>Sliding</u>
Force = 210.22 lbs
Friction = 0.4
Weight Required = 525.55 lbs
Resisting Weight = 1903.13 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

<u>Cohesion</u>
Sliding Force = 210.22 lbs
Cohesion = 130 psf
Area = 8.75 ft^2
Resisting = 951.56 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation. Cohesion is OK.

<u>Shear Key</u>
Additional Force = 0 lbs
Lateral Bearing Pressure = 200 psf/ft
Required Depth = 0.00 ft
f'_c = 2500 psi
Length = 8 in

Shear key is not required.

<u>Bearing Pressure</u>

	Ballast Width			
	21 in	22 in	23 in	24 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.75 ft) =	1903 lbs	1994 lbs	2084 lbs	2175 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in
F_A	504 lbs	504 lbs	504 lbs	504 lbs	453 lbs	453 lbs	453 lbs	453 lbs	676 lbs	676 lbs	676 lbs	676 lbs	-75 lbs	-75 lbs	-75 lbs	-75 lbs
F_B	357 lbs	357 lbs	357 lbs	357 lbs	494 lbs	494 lbs	494 lbs	494 lbs	608 lbs	608 lbs	608 lbs	608 lbs	-788 lbs	-788 lbs	-788 lbs	-788 lbs
F_V	47 lbs	47 lbs	47 lbs	47 lbs	378 lbs	378 lbs	378 lbs	378 lbs	315 lbs	315 lbs	315 lbs	315 lbs	-420 lbs	-420 lbs	-420 lbs	-420 lbs
P_{total}	2765 lbs	2855 lbs	2946 lbs	3037 lbs	2850 lbs	2940 lbs	3031 lbs	3121 lbs	3187 lbs	3278 lbs	3368 lbs	3459 lbs	279 lbs	334 lbs	388 lbs	442 lbs
M	356 lbs-ft	356 lbs-ft	356 lbs-ft	356 lbs-ft	512 lbs-ft	512 lbs-ft	512 lbs-ft	512 lbs-ft	625 lbs-ft	625 lbs-ft	625 lbs-ft	625 lbs-ft	650 lbs-ft	650 lbs-ft	650 lbs-ft	650 lbs-ft
e	0.13 ft	0.12 ft	0.12 ft	0.12 ft	0.18 ft	0.17 ft	0.17 ft	0.16 ft	0.20 ft	0.19 ft	0.19 ft	0.18 ft	2.33 ft	1.95 ft	1.67 ft	1.47 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	267.1 psf	264.8 psf	262.8 psf	260.9 psf	255.4 psf	253.7 psf	252.1 psf	250.7 psf	278.6 psf	275.8 psf	273.3 psf	270.9 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	364.9 psf	358.2 psf	352.0 psf	346.4 psf	395.9 psf	387.8 psf	380.4 psf	373.6 psf	449.9 psf	439.3 psf	429.7 psf	420.8 psf	614.3 psf	219.6 psf	163.5 psf	143.0 psf

Maximum Bearing Pressure = 614 psf
Allowable Bearing Pressure = 1500 psf

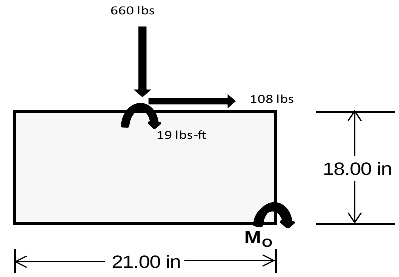
Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O =	396.6 ft-lbs
Resisting Force Required =	453.20 lbs
S.F. =	1.67
Weight Required =	755.34 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	21 in			21 in			21 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	128 lbs	115 lbs	70 lbs	287 lbs	660 lbs	243 lbs	79 lbs	-11 lbs	24 lbs
F_V	17 lbs	143 lbs	17 lbs	11 lbs	108 lbs	13 lbs	17 lbs	143 lbs	17 lbs
P_{total}	2484 lbs	2471 lbs	2426 lbs	2530 lbs	2903 lbs	2486 lbs	768 lbs	678 lbs	713 lbs
M	48 lbs-ft	240 lbs-ft	51 lbs-ft	33 lbs-ft	181 lbs-ft	39 lbs-ft	49 lbs-ft	239 lbs-ft	49 lbs-ft
e	0.02 ft	0.10 ft	0.02 ft	0.01 ft	0.06 ft	0.02 ft	0.06 ft	0.35 ft	0.07 ft
L/6	0.29 ft	1.56 ft	1.71 ft	1.72 ft	1.63 ft	1.72 ft	1.62 ft	1.04 ft	1.61 ft
f_{min}	265.0 sqft	188.5 sqft	257.5 sqft	276.2 sqft	260.8 sqft	268.9 sqft	68.7 sqft	-16.4 sqft	62.1 sqft
f_{max}	302.8 psf	376.3 psf	297.1 psf	302.2 psf	402.7 psf	299.3 psf	106.8 psf	171.2 psf	100.9 psf

Maximum Bearing Pressure = 403 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 21in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

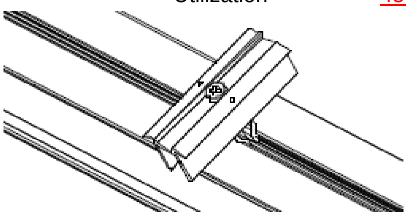
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

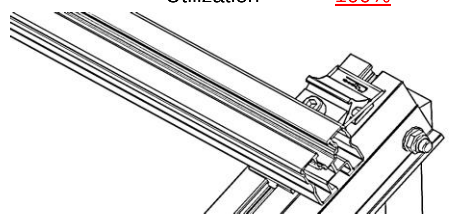
Fastening of Modules to Purlins

Maximum Uplifting Force =	0.546	k
Allowable Uplift =	1.214	k
Utilization =	45%	



Fastening of Purlins to Girders

Maximum Uplifting Force =	1.113	k
Allowable Uplift =	1.116	k
Utilization =	100%	



6.2 Bolted Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut

Maximum Axial Load =	1.081	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	19%	

Rear Strut

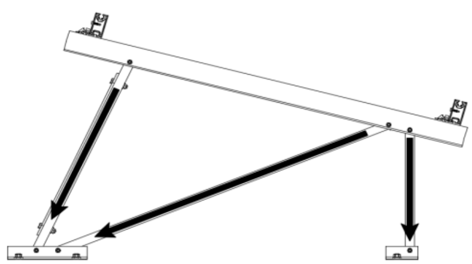
Maximum Axial Load =	1.170	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	21%	

Diagonal Strut

Maximum Axial Load =	0.475	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	8%	

Bracing

Maximum Axial Load =	0.211	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	3%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

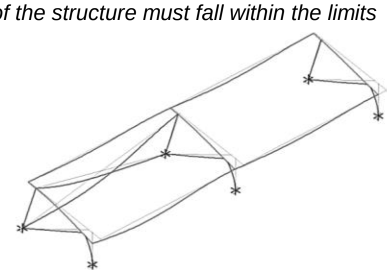
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	30.83	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	0.617	in
Max Drift, Δ_{MAX} =	0.078	in

$0.078 \leq 0.617$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus XT**

Strong Axis:

3.4.14

L_b = 69.00 in

J = 0.427

143.909

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.5 ksi

3.4.16

b/t = 6.6

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 69.00 in

J = 0.427

156.378

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.3

3.4.16

b/t = 37.95

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 22.7 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 37.95

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 38.1
m = 0.63
C_0 = 40.784
Cc = 39.216

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.7
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LSt= 29.5 ksi
Ix = 498305 mm^4
1.197 in^4
y = 40.784 mm
Sx = 0.746 in^3
M_{max}St = 1.831 k-ft

3.4.18

h/t = 6.6

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 20.5
Cc = 20.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LWk= 22.7 ksi
Iy = 148662 mm^4
0.357 in^4
x = 20.5 mm
Sy = 0.443 in^3
M_{max}Wk = 0.838 k-ft

<u>Compression</u>

3.4.9

b/t = 6.6
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 37.95
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.4 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.42 ksi
A = 620.02 mm^2
0.96 in^2
P_{max} = 20.59 kips

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in
ry = 1.374
Cb = 1.13
23.1669

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2
φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))
φF_L= 29.5 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in
ry = 1.374
Cb = 1.13
24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2
φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))
φF_L= 29.5 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7
F_{UT}= (φbk2*√(BpE))/(5.1b/t)
F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
F_{ST}= φb[Bp-1.6Dp*b/t]
F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = 1.17φyFcy

φF_L = 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT} = 9.37

F_{ST} = 28.24

φF_L = Fut + (Fst - Fut)ρst < Fst

φF_L = 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

φF_LSt = 29.5 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.445 k-ft

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

φF_LWk = 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L = φcc(Bc-Dc*λ)

φF_L = 30.1251 ksi

3.4.8

$b/t =$ 24.46
$S1 =$ 3.83
$S2 =$ 10.30
$\varphi F_L =$ (φck2*√(BpE))/(5.1b/t)
$\varphi F_L =$ 10.4 ksi

3.4.9

$b/t =$ 4.29
$S1 =$ 12.21 (See 3.4.16 above for formula)
$S2 =$ 32.70 (See 3.4.16 above for formula)
$\varphi F_L =$ φyFcy
$\varphi F_L =$ 33.3 ksi

$b/t =$ 24.46
$S1 =$ 12.21
$S2 =$ 32.70
$\varphi F_L =$ φc[Bp-1.6Dp*b/t]
$\varphi F_L =$ 28.2 ksi

3.4.9.1

$b/t =$ 24.46
$t =$ 2.6
$ds =$ 6.05
$rs =$ 3.49
$S =$ 21.70
$\rho st =$ 0.22
$F_{UT} =$ 10.43
$F_{ST} =$ 28.24
$\varphi F_L =$ Fut + (Fst - Fut)ρst < Fst
$\varphi F_L =$ 14.3 ksi

3.4.10

$Rb/t =$ 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

$S1 =$ 6.87
$S2 =$ 131.3
$\varphi F_L =$ φyFcy
$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 14.29 ksi
$A =$ 576.21 mm^2
0.89 in^2
$P_{max} =$ 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in
J = 0.16
47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 31.2 ksi
Ix = 39958.2 mm^4
0.096 in^4
y = 15 mm
Sx = 0.163 in^3
M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in
J = 0.16
47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.2 ksi
Iy = 39958.2 mm^4
0.096 in^4
x = 15 mm
Sy = 0.163 in^3
M_{max}Wk = 0.423 k-ft

Compression

3.4.7

$\lambda =$ 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.83792

$\varphi F_L = \varphi cc(Bc\text{-}Dc^*\lambda)$

$\varphi F_L =$ 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 24.52 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.404 k-ft

Weak Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.85841

φF_L= (φccFcy)/(λ²)

φF_L= 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 7.60 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 36.18 in

J = 0.16

94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.410 k-ft

Weak Axis:

3.4.14

L_b = 36.18 in

J = 0.16

94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.5514

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.7972

φF_L = (φccFcy)/(λ²)

φF_L = 11.5927 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L = φyFcy

φF_L = 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 11.59 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 5.82 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-51.748	-51.748	0	0
2	M16	Y	-51.748	-51.748	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-81.397	-81.397	0	0
2	M16	y	-125.796	-125.796	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	162.794	162.794	0	0
2	M16	y	73.997	73.997	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	181.179	2	284.623	2	-.008	10	0	1	0	1	0	1
2		min	-224.671	3	-408.436	3	-2.233	4	0	3	0	1	0	1
3	N7	max	0	5	389.294	1	-.1	10	0	10	0	1	0	1
4		min	-.161	2	-30.117	3	-23.131	4	-.037	4	0	1	0	1
5	N15	max	0	15	1081.335	1	.49	1	0	1	0	1	0	1
6		min	-1.432	2	-130.501	3	-23.547	5	-.037	4	0	1	0	1
7	N16	max	646.198	2	942.671	2	0	10	0	1	0	1	0	1
8		min	-701.09	3	-1316.31	3	-189.748	4	0	3	0	1	0	1
9	N23	max	0	15	389.099	1	1.974	1	.003	1	0	1	0	1
10		min	-.161	2	-29.639	3	-21.838	5	-.034	5	0	1	0	1
11	N24	max	181.358	2	287.893	2	55.56	3	0	4	0	1	0	1
12		min	-224.889	3	-406.577	3	-3.435	5	0	3	0	1	0	1
13	Totals:	max	1006.981	2	3287.323	1	0	9						
14		min	-1150.83	3	-2321.581	3	-262.829	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	275.744	1	.64	6	1.116	4	0	10	0	12	0	1
2			min	-369.152	3	.149	15	-.059	3	0	4	0	1	0	1
3		2	max	275.86	1	.594	6	1.01	4	0	10	0	5	0	15
4			min	-369.065	3	.139	15	-.059	3	0	4	0	1	0	6
5		3	max	275.976	1	.548	6	.905	4	0	10	0	4	0	15
6			min	-368.978	3	.128	15	-.059	3	0	4	0	3	0	6
7		4	max	276.093	1	.503	6	.799	4	0	10	0	4	0	15
8			min	-368.89	3	.117	15	-.059	3	0	4	0	3	0	6
9		5	max	276.209	1	.457	6	.694	4	0	10	0	4	0	15
10			min	-368.803	3	.106	15	-.059	3	0	4	0	3	0	6
11		6	max	276.326	1	.411	6	.588	4	0	10	0	4	0	15
12			min	-368.716	3	.096	15	-.059	3	0	4	0	3	0	6
13		7	max	276.442	1	.366	6	.483	4	0	10	0	4	0	15
14			min	-368.629	3	.085	15	-.059	3	0	4	0	3	0	6
15		8	max	276.558	1	.32	6	.377	4	0	10	0	4	0	15
16			min	-368.541	3	.074	15	-.059	3	0	4	0	3	0	6
17		9	max	276.675	1	.274	6	.36	1	0	10	0	4	0	15
18			min	-368.454	3	.063	15	-.059	3	0	4	0	3	0	6
19		10	max	276.791	1	.229	6	.36	1	0	10	0	4	0	15
20			min	-368.367	3	.053	15	-.059	3	0	4	0	3	0	6
21		11	max	276.908	1	.183	6	.36	1	0	10	0	4	0	15
22			min	-368.279	3	.042	15	-.059	3	0	4	0	3	0	6
23		12	max	277.024	1	.138	2	.36	1	0	10	0	4	0	15
24			min	-368.192	3	.031	15	-.129	5	0	4	0	3	0	6
25		13	max	277.14	1	.102	2	.36	1	0	10	0	4	0	15
26			min	-368.105	3	.018	12	-.234	5	0	4	0	3	0	6
27		14	max	277.257	1	.067	2	.36	1	0	10	0	4	0	15
28			min	-368.017	3	-.003	3	-.34	5	0	4	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	277.373	1	.031	2	.36	1	0	10	0	4	0	15
30			min	-367.93	3	-.03	3	-.445	5	0	4	0	3	0	6
31		16	max	277.49	1	-.004	2	.36	1	0	10	0	1	0	15
32			min	-367.843	3	-.056	3	-.551	5	0	4	0	3	0	6
33		17	max	277.606	1	-.022	15	.36	1	0	10	0	1	0	15
34			min	-367.756	3	-.091	4	-.656	5	0	4	0	3	0	6
35		18	max	277.722	1	-.033	15	.36	1	0	10	0	1	0	15
36			min	-367.668	3	-.137	4	-.762	5	0	4	0	3	0	6
37		19	max	277.839	1	-.044	15	.36	1	0	10	0	1	0	15
38			min	-367.581	3	-.182	4	-.867	5	0	4	0	3	0	6
39	M3	1	max	125.58	2	1.775	6	-.027	10	0	5	.001	1	0	6
40			min	-130.137	3	.417	15	-1.398	4	0	1	0	10	0	15
41		2	max	125.511	2	1.598	6	-.027	10	0	5	.001	1	0	2
42			min	-130.189	3	.375	15	-1.264	4	0	1	0	10	0	15
43		3	max	125.443	2	1.421	6	-.027	10	0	5	0	1	0	2
44			min	-130.24	3	.333	15	-1.13	4	0	1	0	15	0	3
45		4	max	125.374	2	1.244	6	-.027	10	0	5	0	1	0	15
46			min	-130.292	3	.292	15	-.997	4	0	1	0	5	0	4
47		5	max	125.305	2	1.067	6	-.027	10	0	5	0	1	0	15
48			min	-130.343	3	.25	15	-.863	4	0	1	0	5	0	4
49		6	max	125.237	2	.889	6	-.027	10	0	5	0	1	0	15
50			min	-130.394	3	.208	15	-.73	4	0	1	0	5	0	4
51		7	max	125.168	2	.712	6	-.027	10	0	5	0	1	0	15
52			min	-130.446	3	.167	15	-.596	4	0	1	0	5	0	4
53		8	max	125.1	2	.535	6	-.027	10	0	5	0	1	0	15
54			min	-130.497	3	.125	15	-.462	4	0	1	0	5	-.001	4
55		9	max	125.031	2	.358	6	-.027	10	0	5	0	1	0	15
56			min	-130.549	3	.083	15	-.347	1	0	1	0	5	-.001	4
57		10	max	124.962	2	.181	6	-.027	10	0	5	0	1	0	15
58			min	-130.6	3	.042	15	-.347	1	0	1	0	5	-.001	4
59		11	max	124.894	2	.027	2	.013	5	0	5	0	1	0	15
60			min	-130.652	3	-.022	3	-.347	1	0	1	0	5	-.001	4
61		12	max	124.825	2	-.042	15	.147	5	0	5	0	1	0	15
62			min	-130.703	3	-.174	4	-.347	1	0	1	0	5	-.001	4
63		13	max	124.757	2	-.083	15	.28	5	0	5	0	1	0	15
64			min	-130.755	3	-.351	4	-.347	1	0	1	0	5	-.001	4
65		14	max	124.688	2	-.125	15	.414	5	0	5	0	1	0	15
66			min	-130.806	3	-.528	4	-.347	1	0	1	0	5	-.001	4
67		15	max	124.619	2	-.167	15	.548	5	0	5	0	1	0	15
68			min	-130.858	3	-.705	4	-.347	1	0	1	0	5	0	4
69		16	max	124.551	2	-.208	15	.681	5	0	5	0	12	0	15
70			min	-130.909	3	-.883	4	-.347	1	0	1	0	4	0	4
71		17	max	124.482	2	-.25	15	.815	5	0	5	0	12	0	15
72			min	-130.96	3	-1.06	4	-.347	1	0	1	0	4	0	4
73		18	max	124.414	2	-.292	15	.948	5	0	5	0	12	0	15
74			min	-131.012	3	-1.237	4	-.347	1	0	1	0	1	0	4
75		19	max	124.345	2	-.333	15	1.082	5	0	5	0	5	0	1
76			min	-131.063	3	-1.414	4	-.347	1	0	1	0	1	0	1
77	M4	1	max	388.13	1	0	1	-.102	10	0	1	0	5	0	1
78			min	-30.991	3	0	1	-22.486	4	0	1	0	2	0	1
79		2	max	388.194	1	0	1	-.102	10	0	1	0	12	0	1
80			min	-30.942	3	0	1	-22.543	4	0	1	-.002	4	0	1
81		3	max	388.259	1	0	1	-.102	10	0	1	0	12	0	1
82			min	-30.894	3	0	1	-22.599	4	0	1	-.004	4	0	1
83		4	max	388.324	1	0	1	-.102	10	0	1	0	10	0	1
84			min	-30.845	3	0	1	-22.655	4	0	1	-.006	4	0	1
85		5	max	388.388	1	0	1	-.102	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	-30.797	3	0	1	-22.711	4	0	1	-.008	4	0	1
87		6	max	388.453	1	0	1	-.102	10	0	1	0	10	0	1
88			min	-30.748	3	0	1	-22.767	4	0	1	-.01	4	0	1
89		7	max	388.518	1	0	1	-.102	10	0	1	0	10	0	1
90			min	-30.7	3	0	1	-22.823	4	0	1	-.012	4	0	1
91		8	max	388.583	1	0	1	-.102	10	0	1	0	10	0	1
92			min	-30.651	3	0	1	-22.879	4	0	1	-.014	4	0	1
93		9	max	388.647	1	0	1	-.102	10	0	1	0	10	0	1
94			min	-30.603	3	0	1	-22.935	4	0	1	-.016	4	0	1
95		10	max	388.712	1	0	1	-.102	10	0	1	0	10	0	1
96			min	-30.554	3	0	1	-22.991	4	0	1	-.018	4	0	1
97		11	max	388.777	1	0	1	-.102	10	0	1	0	10	0	1
98			min	-30.506	3	0	1	-23.047	4	0	1	-.02	4	0	1
99		12	max	388.841	1	0	1	-.102	10	0	1	0	10	0	1
100			min	-30.457	3	0	1	-23.103	4	0	1	-.022	4	0	1
101		13	max	388.906	1	0	1	-.102	10	0	1	0	10	0	1
102			min	-30.409	3	0	1	-23.159	4	0	1	-.024	4	0	1
103		14	max	388.971	1	0	1	-.102	10	0	1	0	10	0	1
104			min	-30.36	3	0	1	-23.216	4	0	1	-.027	4	0	1
105		15	max	389.036	1	0	1	-.102	10	0	1	0	10	0	1
106			min	-30.312	3	0	1	-23.272	4	0	1	-.029	4	0	1
107		16	max	389.1	1	0	1	-.102	10	0	1	0	10	0	1
108			min	-30.263	3	0	1	-23.328	4	0	1	-.031	4	0	1
109		17	max	389.165	1	0	1	-.102	10	0	1	0	10	0	1
110			min	-30.215	3	0	1	-23.384	4	0	1	-.033	4	0	1
111		18	max	389.23	1	0	1	-.102	10	0	1	0	10	0	1
112			min	-30.166	3	0	1	-23.44	4	0	1	-.035	4	0	1
113		19	max	389.294	1	0	1	-.102	10	0	1	0	10	0	1
114			min	-30.117	3	0	1	-23.496	4	0	1	-.037	4	0	1
115	M6	1	max	880.356	1	.629	6	1.053	4	0	3	0	3	0	1
116			min	-1170.202	3	.142	15	-.182	3	0	5	0	9	0	1
117		2	max	880.472	1	.583	6	.947	4	0	3	0	4	0	15
118			min	-1170.114	3	.131	15	-.182	3	0	5	0	9	0	6
119		3	max	880.588	1	.537	6	.842	4	0	3	0	4	0	15
120			min	-1170.027	3	.121	15	-.182	3	0	5	0	10	0	6
121		4	max	880.705	1	.492	6	.736	4	0	3	0	4	0	15
122			min	-1169.94	3	.11	15	-.182	3	0	5	0	10	0	6
123		5	max	880.821	1	.449	2	.631	4	0	3	0	4	0	15
124			min	-1169.852	3	.099	15	-.182	3	0	5	0	10	0	6
125		6	max	880.938	1	.413	2	.525	4	0	3	0	4	0	15
126			min	-1169.765	3	.088	15	-.182	3	0	5	0	3	0	6
127		7	max	881.054	1	.377	2	.42	4	0	3	0	4	0	15
128			min	-1169.678	3	.078	15	-.182	3	0	5	0	3	0	6
129		8	max	881.17	1	.342	2	.314	4	0	3	0	4	0	15
130			min	-1169.591	3	.067	15	-.182	3	0	5	0	3	0	6
131		9	max	881.287	1	.306	2	.209	4	0	3	0	4	0	15
132			min	-1169.503	3	.05	12	-.182	3	0	5	0	3	0	2
133		10	max	881.403	1	.271	2	.12	1	0	3	0	4	0	15
134			min	-1169.416	3	.032	12	-.182	3	0	5	0	3	0	2
135		11	max	881.52	1	.235	2	.12	1	0	3	0	4	0	15
136			min	-1169.329	3	.012	3	-.182	3	0	5	0	3	0	2
137		12	max	881.636	1	.2	2	.12	1	0	3	0	4	0	15
138			min	-1169.241	3	-.014	3	-.182	3	0	5	0	3	0	2
139		13	max	881.752	1	.164	2	.12	1	0	3	0	4	0	15
140			min	-1169.154	3	-.041	3	-.247	5	0	5	0	3	0	2
141		14	max	881.869	1	.128	2	.12	1	0	3	0	4	0	15
142			min	-1169.067	3	-.068	3	-.353	5	0	5	0	3	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	881.985	1	.093	2	.12	1	0	3	0	4	0	15
144			min	-1168.979	3	-.094	3	-.458	5	0	5	0	3	0	2
145		16	max	882.102	1	.057	2	.12	1	0	3	0	4	0	12
146			min	-1168.892	3	-.121	3	-.564	5	0	5	0	3	0	2
147		17	max	882.218	1	.022	2	.12	1	0	3	0	4	0	12
148			min	-1168.805	3	-.148	3	-.669	5	0	5	0	3	0	2
149		18	max	882.334	1	-.014	2	.12	1	0	3	0	4	0	12
150			min	-1168.718	3	-.175	3	-.775	5	0	5	0	3	0	2
151		19	max	882.451	1	-.05	2	.12	1	0	3	0	1	0	12
152			min	-1168.63	3	-.201	3	-.88	5	0	5	0	3	0	2
153	M7	1	max	474.621	2	1.789	4	.015	3	0	1	0	4	0	2
154			min	-390.419	3	.425	15	-1.383	4	0	3	0	3	0	12
155		2	max	474.553	2	1.612	4	.015	3	0	1	0	4	0	2
156			min	-390.471	3	.384	15	-1.249	4	0	3	0	3	0	3
157		3	max	474.484	2	1.435	4	.015	3	0	1	0	1	0	2
158			min	-390.522	3	.342	15	-1.116	4	0	3	0	3	0	3
159		4	max	474.416	2	1.258	4	.015	3	0	1	0	1	0	2
160			min	-390.574	3	.3	15	-.982	4	0	3	0	3	0	3
161		5	max	474.347	2	1.081	4	.015	3	0	1	0	1	0	15
162			min	-390.625	3	.259	15	-.848	4	0	3	0	5	0	3
163		6	max	474.278	2	.903	4	.015	3	0	1	0	1	0	15
164			min	-390.677	3	.217	15	-.715	4	0	3	0	5	0	6
165		7	max	474.21	2	.726	4	.015	3	0	1	0	1	0	15
166			min	-390.728	3	.175	15	-.581	4	0	3	0	5	0	6
167		8	max	474.141	2	.549	4	.015	3	0	1	0	1	0	15
168			min	-390.779	3	.134	15	-.448	4	0	3	0	5	0	6
169		9	max	474.073	2	.372	4	.015	3	0	1	0	1	0	15
170			min	-390.831	3	.09	12	-.314	4	0	3	0	5	-.001	6
171		10	max	474.004	2	.223	2	.015	3	0	1	0	1	0	15
172			min	-390.882	3	.021	12	-.18	4	0	3	0	5	-.001	6
173		11	max	473.935	2	.085	2	.015	3	0	1	0	1	0	15
174			min	-390.934	3	-.081	3	-.047	4	0	3	0	5	-.001	6
175		12	max	473.867	2	-.033	15	.087	5	0	1	0	1	0	15
176			min	-390.985	3	-.184	3	-.014	2	0	3	0	5	-.001	6
177		13	max	473.798	2	-.075	15	.221	5	0	1	0	1	0	15
178			min	-391.037	3	-.337	6	-.014	2	0	3	0	5	-.001	6
179		14	max	473.73	2	-.116	15	.354	5	0	1	0	1	0	15
180			min	-391.088	3	-.515	6	-.014	2	0	3	0	5	-.001	6
181		15	max	473.661	2	-.158	15	.488	5	0	1	0	1	0	15
182			min	-391.14	3	-.692	6	-.014	2	0	3	0	5	0	6
183		16	max	473.592	2	-.2	15	.621	5	0	1	0	1	0	15
184			min	-391.191	3	-.869	6	-.014	2	0	3	0	5	0	6
185		17	max	473.524	2	-.241	15	.755	5	0	1	0	1	0	15
186			min	-391.243	3	-1.046	6	-.014	2	0	3	0	5	0	6
187		18	max	473.455	2	-.283	15	.889	5	0	1	0	1	0	15
188			min	-391.294	3	-1.223	6	-.014	2	0	3	0	5	0	6
189		19	max	473.387	2	-.324	15	1.022	5	0	1	0	1	0	1
190			min	-391.345	3	-1.401	6	-.014	2	0	3	0	3	0	1
191	M8	1	max	1080.171	1	0	1	.595	1	0	1	0	4	0	1
192			min	-131.375	3	0	1	-22.764	4	0	1	0	1	0	1
193		2	max	1080.235	1	0	1	.595	1	0	1	0	1	0	1
194			min	-131.326	3	0	1	-22.82	4	0	1	-.002	4	0	1
195		3	max	1080.3	1	0	1	.595	1	0	1	0	1	0	1
196			min	-131.278	3	0	1	-22.876	4	0	1	-.004	4	0	1
197		4	max	1080.365	1	0	1	.595	1	0	1	0	1	0	1
198			min	-131.229	3	0	1	-22.932	4	0	1	-.006	4	0	1
199		5	max	1080.43	1	0	1	.595	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	-131.181	3	0	1	-22.988	4	0	1	-.008	4	0	1
201		6	max	1080.494	1	0	1	.595	1	0	1	0	1	0	1
202			min	-131.132	3	0	1	-23.044	4	0	1	-.01	4	0	1
203		7	max	1080.559	1	0	1	.595	1	0	1	0	1	0	1
204			min	-131.084	3	0	1	-23.1	4	0	1	-.012	4	0	1
205		8	max	1080.624	1	0	1	.595	1	0	1	0	1	0	1
206			min	-131.035	3	0	1	-23.157	4	0	1	-.014	4	0	1
207		9	max	1080.688	1	0	1	.595	1	0	1	0	1	0	1
208			min	-130.987	3	0	1	-23.213	4	0	1	-.016	4	0	1
209		10	max	1080.753	1	0	1	.595	1	0	1	0	1	0	1
210			min	-130.938	3	0	1	-23.269	4	0	1	-.019	4	0	1
211		11	max	1080.818	1	0	1	.595	1	0	1	0	1	0	1
212			min	-130.89	3	0	1	-23.325	4	0	1	-.021	4	0	1
213		12	max	1080.883	1	0	1	.595	1	0	1	0	1	0	1
214			min	-130.841	3	0	1	-23.381	4	0	1	-.023	4	0	1
215		13	max	1080.947	1	0	1	.595	1	0	1	0	1	0	1
216			min	-130.793	3	0	1	-23.437	4	0	1	-.025	4	0	1
217		14	max	1081.012	1	0	1	.595	1	0	1	0	1	0	1
218			min	-130.744	3	0	1	-23.493	4	0	1	-.027	4	0	1
219		15	max	1081.077	1	0	1	.595	1	0	1	0	1	0	1
220			min	-130.696	3	0	1	-23.549	4	0	1	-.029	4	0	1
221		16	max	1081.141	1	0	1	.595	1	0	1	0	1	0	1
222			min	-130.647	3	0	1	-23.605	4	0	1	-.031	4	0	1
223		17	max	1081.206	1	0	1	.595	1	0	1	0	1	0	1
224			min	-130.599	3	0	1	-23.661	4	0	1	-.033	4	0	1
225		18	max	1081.271	1	0	1	.595	1	0	1	0	1	0	1
226			min	-130.55	3	0	1	-23.717	4	0	1	-.035	4	0	1
227		19	max	1081.335	1	0	1	.595	1	0	1	0	1	0	1
228			min	-130.501	3	0	1	-23.773	4	0	1	-.037	4	0	1
229	M10	1	max	278.299	1	.668	4	1.203	5	0	1	0	1	0	1
230			min	-338.975	3	.169	15	-.126	1	-.001	5	0	3	0	1
231		2	max	278.416	1	.623	4	1.097	5	0	1	0	4	0	15
232			min	-338.888	3	.158	15	-.126	1	-.001	5	0	3	0	4
233		3	max	278.532	1	.577	4	.992	5	0	1	0	4	0	15
234			min	-338.801	3	.147	15	-.126	1	-.001	5	0	3	0	4
235		4	max	278.649	1	.531	4	.886	5	0	1	0	4	0	15
236			min	-338.714	3	.136	15	-.126	1	-.001	5	0	3	0	4
237		5	max	278.765	1	.486	4	.781	5	0	1	0	4	0	15
238			min	-338.626	3	.126	15	-.126	1	-.001	5	0	3	0	4
239		6	max	278.881	1	.44	4	.675	5	0	1	0	4	0	15
240			min	-338.539	3	.115	15	-.126	1	-.001	5	0	3	0	4
241		7	max	278.998	1	.394	4	.57	5	0	1	0	4	0	15
242			min	-338.452	3	.104	15	-.126	1	-.001	5	0	3	0	4
243		8	max	279.114	1	.349	4	.464	5	0	1	0	4	0	15
244			min	-338.364	3	.093	15	-.126	1	-.001	5	0	3	0	4
245		9	max	279.231	1	.303	4	.359	5	0	1	0	4	0	15
246			min	-338.277	3	.083	15	-.126	1	-.001	5	0	3	0	4
247		10	max	279.347	1	.257	4	.253	5	0	1	.001	4	0	15
248			min	-338.19	3	.072	15	-.126	1	-.001	5	0	3	0	4
249		11	max	279.463	1	.212	4	.148	5	0	1	.001	4	0	15
250			min	-338.102	3	.061	15	-.126	1	-.001	5	0	3	0	4
251		12	max	279.58	1	.166	4	.042	5	0	1	.001	4	0	15
252			min	-338.015	3	.051	15	-.126	1	-.001	5	0	3	0	4
253		13	max	279.696	1	.12	4	-.016	12	0	1	.001	5	0	15
254			min	-337.928	3	.035	12	-.126	1	-.001	5	0	3	0	4
255		14	max	279.813	1	.075	4	-.016	12	0	1	.001	5	0	15
256			min	-337.841	3	.012	9	-.185	4	-.001	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	279.929	1	.031	2	-.016	12	0	1	.001	5	0	15
258			min	-337.753	3	-.018	9	-.291	4	-.001	5	0	3	0	4
259		16	max	280.045	1	.011	5	-.016	12	0	1	0	5	0	15
260			min	-337.666	3	-.048	9	-.396	4	-.001	5	0	3	0	4
261		17	max	280.162	1	-.003	15	-.016	12	0	1	0	5	0	15
262			min	-337.579	3	-.077	9	-.502	4	-.001	5	0	1	0	4
263		18	max	280.278	1	-.014	15	-.016	12	0	1	0	5	0	15
264			min	-337.491	3	-.109	6	-.607	4	-.001	5	0	1	0	4
265		19	max	280.395	1	-.025	15	-.016	12	0	1	0	5	0	15
266			min	-337.404	3	-.155	6	-.713	4	-.001	5	0	1	0	4
267	M11	1	max	125.206	2	1.77	6	.386	1	.001	4	.001	5	0	6
268			min	-130.762	3	.412	15	-1.244	5	0	10	-.001	1	0	15
269		2	max	125.137	2	1.592	6	.386	1	.001	4	0	5	0	2
270			min	-130.813	3	.371	15	-1.11	5	0	10	-.001	1	0	12
271		3	max	125.068	2	1.415	6	.386	1	.001	4	0	5	0	2
272			min	-130.865	3	.329	15	-.977	5	0	10	0	1	0	3
273		4	max	125	2	1.238	6	.386	1	.001	4	0	5	0	15
274			min	-130.916	3	.287	15	-.843	5	0	10	0	1	0	4
275		5	max	124.931	2	1.061	6	.386	1	.001	4	0	3	0	15
276			min	-130.968	3	.246	15	-.71	5	0	10	0	1	0	4
277		6	max	124.863	2	.884	6	.386	1	.001	4	0	3	0	15
278			min	-131.019	3	.204	15	-.576	5	0	10	0	1	0	4
279		7	max	124.794	2	.706	6	.386	1	.001	4	0	3	0	15
280			min	-131.071	3	.162	15	-.442	5	0	10	0	1	0	4
281		8	max	124.725	2	.529	6	.386	1	.001	4	0	3	0	15
282			min	-131.122	3	.121	15	-.309	5	0	10	0	1	-.001	4
283		9	max	124.657	2	.352	6	.386	1	.001	4	0	3	0	15
284			min	-131.173	3	.079	15	-.175	5	0	10	0	1	-.001	4
285		10	max	124.588	2	.175	6	.386	1	.001	4	0	3	0	15
286			min	-131.225	3	.037	15	-.041	5	0	10	0	1	-.001	4
287		11	max	124.52	2	.027	2	.386	1	.001	4	0	3	0	15
288			min	-131.276	3	-.038	3	-.015	3	0	10	0	1	-.001	4
289		12	max	124.451	2	-.046	15	.386	1	.001	4	0	3	0	15
290			min	-131.328	3	-.18	4	-.015	3	0	10	0	4	-.001	4
291		13	max	124.382	2	-.087	15	.442	4	.001	4	0	3	0	15
292			min	-131.379	3	-.357	4	-.015	3	0	10	0	4	-.001	4
293		14	max	124.314	2	-.129	15	.576	4	.001	4	0	3	0	15
294			min	-131.431	3	-.534	4	-.015	3	0	10	0	1	-.001	4
295		15	max	124.245	2	-.171	15	.709	4	.001	4	0	3	0	15
296			min	-131.482	3	-.712	4	-.015	3	0	10	0	10	0	4
297		16	max	124.177	2	-.212	15	.843	4	.001	4	0	4	0	15
298			min	-131.534	3	-.889	4	-.015	3	0	10	0	10	0	4
299		17	max	124.108	2	-.254	15	.977	4	.001	4	0	4	0	15
300			min	-131.585	3	-1.066	4	-.015	3	0	10	0	10	0	4
301		18	max	124.039	2	-.296	15	1.11	4	.001	4	0	4	0	15
302			min	-131.637	3	-1.243	4	-.015	3	0	10	0	10	0	4
303		19	max	123.971	2	-.337	15	1.244	4	.001	4	0	4	0	1
304			min	-131.688	3	-1.42	4	-.015	3	0	10	0	10	0	1
305	M12	1	max	387.934	1	0	1	2.109	1	0	1	0	4	0	1
306			min	-30.513	3	0	1	-20.855	5	0	1	0	3	0	1
307		2	max	387.999	1	0	1	2.109	1	0	1	0	1	0	1
308			min	-30.464	3	0	1	-20.911	5	0	1	-.002	5	0	1
309		3	max	388.064	1	0	1	2.109	1	0	1	0	1	0	1
310			min	-30.416	3	0	1	-20.967	5	0	1	-.004	5	0	1
311		4	max	388.128	1	0	1	2.109	1	0	1	0	1	0	1
312			min	-30.367	3	0	1	-21.023	5	0	1	-.006	5	0	1
313		5	max	388.193	1	0	1	2.109	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	-30.319	3	0	1	-21.079	5	0	1	-.007	5	0	1
315		6	max	388.258	1	0	1	2.109	1	0	1	0	1	0	1
316			min	-30.27	3	0	1	-21.135	5	0	1	-.009	5	0	1
317		7	max	388.323	1	0	1	2.109	1	0	1	.001	1	0	1
318			min	-30.222	3	0	1	-21.192	5	0	1	-.011	5	0	1
319		8	max	388.387	1	0	1	2.109	1	0	1	.001	1	0	1
320			min	-30.173	3	0	1	-21.248	5	0	1	-.013	5	0	1
321		9	max	388.452	1	0	1	2.109	1	0	1	.002	1	0	1
322			min	-30.125	3	0	1	-21.304	5	0	1	-.015	5	0	1
323		10	max	388.517	1	0	1	2.109	1	0	1	.002	1	0	1
324			min	-30.076	3	0	1	-21.36	5	0	1	-.017	5	0	1
325		11	max	388.581	1	0	1	2.109	1	0	1	.002	1	0	1
326			min	-30.028	3	0	1	-21.416	5	0	1	-.019	5	0	1
327		12	max	388.646	1	0	1	2.109	1	0	1	.002	1	0	1
328			min	-29.979	3	0	1	-21.472	5	0	1	-.021	5	0	1
329		13	max	388.711	1	0	1	2.109	1	0	1	.002	1	0	1
330			min	-29.931	3	0	1	-21.528	5	0	1	-.023	5	0	1
331		14	max	388.775	1	0	1	2.109	1	0	1	.002	1	0	1
332			min	-29.882	3	0	1	-21.584	5	0	1	-.025	5	0	1
333		15	max	388.84	1	0	1	2.109	1	0	1	.003	1	0	1
334			min	-29.834	3	0	1	-21.64	5	0	1	-.027	5	0	1
335		16	max	388.905	1	0	1	2.109	1	0	1	.003	1	0	1
336			min	-29.785	3	0	1	-21.696	5	0	1	-.029	5	0	1
337		17	max	388.97	1	0	1	2.109	1	0	1	.003	1	0	1
338			min	-29.737	3	0	1	-21.752	5	0	1	-.03	5	0	1
339		18	max	389.034	1	0	1	2.109	1	0	1	.003	1	0	1
340			min	-29.688	3	0	1	-21.808	5	0	1	-.032	5	0	1
341		19	max	389.099	1	0	1	2.109	1	0	1	.003	1	0	1
342			min	-29.639	3	0	1	-21.865	5	0	1	-.034	5	0	1
343	M1	1	max	106.525	1	346.524	3	-2.607	12	0	1	.081	1	.013	1
344			min	5.35	12	-277.133	1	-41.025	1	0	3	.006	10	-.014	3
345		2	max	106.643	1	346.334	3	-2.607	12	0	1	.072	1	.073	1
346			min	5.409	12	-277.386	1	-41.025	1	0	3	.005	10	-.089	3
347		3	max	68.83	1	5.699	14	-2.646	12	0	12	.062	1	.133	1
348			min	-5.565	10	-20.229	2	-40.856	1	0	1	.004	10	-.163	3
349		4	max	68.948	1	5.45	14	-2.646	12	0	12	.053	1	.133	1
350			min	-5.466	10	-20.482	2	-40.856	1	0	1	.004	10	-.158	3
351		5	max	69.066	1	5.211	9	-2.646	12	0	12	.044	1	.134	1
352			min	-5.368	10	-20.735	2	-40.856	1	0	1	.003	10	-.154	3
353		6	max	69.184	1	5	9	-2.646	12	0	12	.036	1	.136	2
354			min	-5.27	10	-20.988	2	-40.856	1	0	1	.003	10	-.15	3
355		7	max	69.302	1	4.789	9	-2.646	12	0	12	.027	1	.14	2
356			min	-5.171	10	-21.241	2	-40.856	1	0	1	.002	10	-.146	3
357		8	max	69.42	1	4.579	9	-2.646	12	0	12	.018	1	.145	2
358			min	-5.073	10	-21.494	2	-40.856	1	0	1	.001	10	-.141	3
359		9	max	69.538	1	4.368	9	-2.646	12	0	12	.009	1	.15	2
360			min	-4.975	10	-21.747	2	-40.856	1	0	1	0	10	-.137	3
361		10	max	69.656	1	4.157	9	-2.646	12	0	12	.001	4	.154	2
362			min	-4.876	10	-22	2	-40.856	1	0	1	0	10	-.132	3
363		11	max	69.774	1	3.946	9	-2.646	12	0	12	0	3	.159	2
364			min	-4.778	10	-22.254	2	-40.856	1	0	1	-.009	1	-.128	3
365		12	max	69.892	1	3.735	9	-2.646	12	0	12	0	12	.164	2
366			min	-4.68	10	-22.507	2	-40.856	1	0	1	-.018	1	-.123	3
367		13	max	70.01	1	3.524	9	-2.646	12	0	12	0	12	.169	2
368			min	-4.581	10	-22.76	2	-40.856	1	0	1	-.026	1	-.119	3
369		14	max	70.128	1	3.313	9	-2.646	12	0	12	-.002	12	.174	2
370			min	-4.483	10	-23.013	2	-40.856	1	0	1	-.035	1	-.114	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	70.246	1	3.102	9	-2.646	12	0	12	-.002	12	.179	2
372			min	-4.385	10	-23.266	2	-40.856	1	0	1	-.044	1	-.109	3
373		16	max	88.638	2	73.374	2	-2.675	12	0	1	-.003	12	.183	2
374			min	-19.831	3	-124.796	3	-41.159	1	0	5	-.053	1	-.104	3
375		17	max	88.756	2	73.121	2	-2.675	12	0	1	-.003	12	.167	2
376			min	-19.743	3	-124.986	3	-41.159	1	0	5	-.062	1	-.077	3
377		18	max	-4.331	12	350.422	2	-2.831	12	0	5	-.004	12	.092	2
378			min	-106.624	1	-153.304	3	-42.118	1	0	2	-.071	1	-.043	3
379		19	max	-4.272	12	350.168	2	-2.831	12	0	5	-.005	12	.016	2
380			min	-106.506	1	-153.494	3	-42.118	1	0	2	-.081	1	-.01	3
381	M5	1	max	245.261	1	1126.707	3	0	10	0	1	.039	4	.028	3
382			min	4.976	15	-899.198	1	-49.813	3	0	5	0	10	-.027	1
383		2	max	245.379	1	1126.517	3	0	10	0	1	.034	4	.169	1
384			min	5.012	15	-899.451	1	-49.813	3	0	5	-.004	3	-.216	3
385		3	max	175.699	3	6.459	9	5.482	3	0	3	.028	4	.36	1
386			min	-24.092	10	-68.609	2	-21.56	4	0	4	-.014	3	-.456	3
387		4	max	175.787	3	6.248	9	5.482	3	0	3	.024	4	.366	1
388			min	-23.994	10	-68.862	2	-21.318	4	0	4	-.013	3	-.442	3
389		5	max	175.876	3	6.037	9	5.482	3	0	3	.019	4	.372	1
390			min	-23.895	10	-69.115	2	-21.076	4	0	4	-.012	3	-.428	3
391		6	max	175.964	3	5.826	9	5.482	3	0	3	.015	4	.378	1
392			min	-23.797	10	-69.368	2	-20.834	4	0	4	-.011	3	-.415	3
393		7	max	176.053	3	5.616	9	5.482	3	0	3	.01	4	.386	2
394			min	-23.699	10	-69.621	2	-20.592	4	0	4	-.01	3	-.401	3
395		8	max	176.141	3	5.405	9	5.482	3	0	3	.006	4	.401	2
396			min	-23.6	10	-69.874	2	-20.35	4	0	4	-.008	3	-.387	3
397		9	max	176.23	3	5.194	9	5.482	3	0	3	.001	4	.417	2
398			min	-23.502	10	-70.127	2	-20.108	4	0	4	-.007	3	-.373	3
399		10	max	176.318	3	4.983	9	5.482	3	0	3	0	10	.432	2
400			min	-23.404	10	-70.38	2	-19.866	4	0	4	-.006	3	-.359	3
401		11	max	176.407	3	4.772	9	5.482	3	0	3	0	10	.447	2
402			min	-23.305	10	-70.633	2	-19.624	4	0	4	-.007	4	-.346	3
403		12	max	176.495	3	4.561	9	5.482	3	0	3	0	10	.462	2
404			min	-23.207	10	-70.887	2	-19.382	4	0	4	-.012	4	-.332	3
405		13	max	176.584	3	4.35	9	5.482	3	0	3	0	10	.478	2
406			min	-23.109	10	-71.14	2	-19.14	4	0	4	-.016	4	-.318	3
407		14	max	176.672	3	4.139	9	5.482	3	0	3	0	10	.493	2
408			min	-23.01	10	-71.393	2	-18.898	4	0	4	-.02	4	-.304	3
409		15	max	176.761	3	3.928	9	5.482	3	0	3	0	10	.509	2
410			min	-22.912	10	-71.646	2	-18.656	4	0	4	-.024	4	-.29	3
411		16	max	292.247	2	300.872	2	5.455	3	0	1	0	3	.521	2
412			min	-66.631	3	-371.163	3	-17.399	4	0	4	-.028	4	-.273	3
413		17	max	292.365	2	300.619	2	5.455	3	0	1	.002	3	.456	2
414			min	-66.542	3	-371.353	3	-17.157	4	0	4	-.032	4	-.192	3
415		18	max	-7.519	12	1133.641	2	5.024	3	0	4	.003	3	.213	2
416			min	-245.411	1	-491.084	3	-39.031	5	0	1	-.04	4	-.086	3
417		19	max	-7.46	12	1133.388	2	5.024	3	0	4	.004	3	.02	3
418			min	-245.292	1	-491.274	3	-38.789	5	0	1	-.049	4	-.033	2
419	M9	1	max	106.139	1	346.489	3	163.756	4	0	3	-.001	15	.013	1
420			min	1.978	15	-277.131	1	2.938	10	0	1	-.079	1	-.014	3
421		2	max	106.257	1	346.299	3	163.998	4	0	3	.032	5	.073	1
422			min	2.013	15	-277.384	1	2.938	10	0	1	-.07	1	-.089	3
423		3	max	68.941	1	5.606	9	39.824	1	0	1	.063	5	.132	1
424			min	-5.137	10	-20.244	2	-27.408	5	0	5	-.061	1	-.163	3
425		4	max	69.059	1	5.395	9	39.824	1	0	1	.057	5	.133	1
426			min	-5.039	10	-20.497	2	-27.166	5	0	5	-.052	1	-.158	3
427		5	max	69.177	1	5.184	9	39.824	1	0	1	.052	5	.134	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-4.94	10	-20.75	2	-26.924	5	0	5	-.043	1	-.154	3
429		6	max	69.295	1	4.973	9	39.824	1	0	1	.046	5	.136	2
430			min	-4.842	10	-21.003	2	-26.682	5	0	5	-.035	1	-.15	3
431		7	max	69.413	1	4.762	9	39.824	1	0	1	.04	5	.14	2
432			min	-4.744	10	-21.256	2	-26.44	5	0	5	-.026	1	-.146	3
433		8	max	69.531	1	4.551	9	39.824	1	0	1	.034	5	.145	2
434			min	-4.645	10	-21.509	2	-26.198	5	0	5	-.017	1	-.141	3
435		9	max	69.649	1	4.34	9	39.824	1	0	1	.029	5	.149	2
436			min	-4.547	10	-21.763	2	-25.956	5	0	5	-.009	1	-.137	3
437		10	max	69.767	1	4.129	9	39.824	1	0	1	.023	4	.154	2
438			min	-4.449	10	-22.016	2	-25.714	5	0	5	0	1	-.132	3
439		11	max	69.885	1	3.919	9	39.824	1	0	1	.019	4	.159	2
440			min	-4.35	10	-22.269	2	-25.472	5	0	5	0	10	-.128	3
441		12	max	70.003	1	3.708	9	39.824	1	0	1	.017	1	.164	2
442			min	-4.252	10	-22.522	2	-25.23	5	0	5	.001	10	-.123	3
443		13	max	70.121	1	3.497	9	39.824	1	0	1	.026	1	.169	2
444			min	-4.154	10	-22.775	2	-24.988	5	0	5	.002	10	-.119	3
445		14	max	70.239	1	3.286	9	39.824	1	0	1	.034	1	.174	2
446			min	-4.055	10	-23.028	2	-24.746	5	0	5	0	15	-.114	3
447		15	max	70.357	1	3.075	9	39.824	1	0	1	.043	1	.179	2
448			min	-3.957	10	-23.281	2	-24.504	5	0	5	-.004	5	-.109	3
449		16	max	88.843	2	73.067	2	40.169	1	0	10	.052	1	.183	2
450			min	-20.2	3	-125.226	3	-23.104	5	0	4	-.008	5	-.104	3
451		17	max	88.961	2	72.814	2	40.169	1	0	10	.061	1	.167	2
452			min	-20.111	3	-125.416	3	-22.862	5	0	4	-.013	5	-.077	3
453		18	max	4.855	5	350.422	2	42.277	1	0	2	.07	1	.092	2
454			min	-106.245	1	-153.3	3	-43.441	5	0	3	-.022	5	-.043	3
455		19	max	4.91	5	350.169	2	42.277	1	0	2	.079	1	.016	2
456			min	-106.127	1	-153.489	3	-43.199	5	0	3	-.032	5	-.01	3
457	M13	1	max	163.758	4	276.755	1	-1.977	15	.013	1	.079	1	0	1
458			min	2.939	10	-346.493	3	-106.132	1	-.014	3	.001	15	0	3
459		2	max	157.432	4	196.196	1	-1.047	15	.013	1	.02	1	.189	3
460			min	2.939	10	-245.406	3	-80.692	1	-.014	3	0	15	-.151	1
461		3	max	151.106	4	115.638	1	-.116	15	.013	1	.006	3	.314	3
462			min	2.939	10	-144.319	3	-55.251	1	-.014	3	-.024	1	-.251	1
463		4	max	144.78	4	35.079	1	1.148	5	.013	1	.003	3	.373	3
464			min	2.939	10	-43.233	3	-29.811	1	-.014	3	-.051	1	-.299	1
465		5	max	138.454	4	57.854	3	2.587	5	.013	1	0	5	.369	3
466			min	2.939	10	-45.48	1	-4.371	1	-.014	3	-.062	1	-.296	1
467		6	max	132.128	4	158.94	3	21.07	1	.013	1	.003	5	.3	3
468			min	2.939	10	-126.039	1	-1.055	3	-.014	3	-.056	1	-.241	1
469		7	max	125.802	4	260.027	3	46.51	1	.013	1	.006	5	.166	3
470			min	2.939	10	-206.598	1	.307	3	-.014	3	-.035	1	-.134	1
471		8	max	119.476	4	361.114	3	71.95	1	.013	1	.011	4	.023	1
472			min	2.939	10	-287.157	1	1.255	12	-.014	3	0	3	-.033	3
473		9	max	113.15	4	462.2	3	97.391	1	.013	1	.057	1	.232	1
474			min	2.939	10	-367.716	1	2.163	12	-.014	3	.001	12	-.296	3
475		10	max	106.824	4	563.287	3	122.831	1	.013	1	.127	1	.493	1
476			min	2.939	10	-448.274	1	3.071	12	-.014	3	.003	12	-.623	3
477		11	max	75.888	4	367.716	1	3.287	5	.014	3	.056	1	.232	1
478			min	2.607	12	-462.2	3	-97.005	1	-.013	1	-.016	5	-.296	3
479		12	max	69.562	4	287.157	1	4.727	5	.014	3	.003	2	.023	1
480			min	2.607	12	-361.114	3	-71.564	1	-.013	1	-.014	5	-.033	3
481		13	max	63.235	4	206.598	1	6.166	5	.014	3	-.003	10	.166	3
482			min	2.607	12	-260.027	3	-46.124	1	-.013	1	-.035	1	-.134	1
483		14	max	56.909	4	126.039	1	7.606	5	.014	3	-.004	15	.3	3
484			min	2.607	12	-158.94	3	-20.684	1	-.013	1	-.057	1	-.241	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	50.583	4	45.48	1	10.297	4	.014	3	0	15	.369	3
486			min	2.607	12	-57.854	3	-.406	10	-.013	1	-.062	1	-.296	1
487		16	max	44.257	4	43.233	3	30.197	1	.014	3	.006	5	.373	3
488			min	2.607	12	-35.079	1	2.164	10	-.013	1	-.05	1	-.299	1
489		17	max	41.128	1	144.319	3	55.637	1	.014	3	.013	5	.314	3
490			min	2.607	12	-115.638	1	3.535	12	-.013	1	-.023	1	-.251	1
491		18	max	41.128	1	245.406	3	81.078	1	.014	3	.026	4	.189	3
492			min	2.607	12	-196.196	1	4.443	12	-.013	1	0	10	-.151	1
493		19	max	41.128	1	346.493	3	106.518	1	.014	3	.081	1	0	1
494			min	2.607	12	-276.755	1	5.351	12	-.013	1	.006	10	0	3
495	M16	1	max	43.189	5	350.347	2	4.91	5	.01	3	.079	1	0	2
496			min	-42.169	1	-153.512	3	-106.135	1	-.016	2	-.032	5	0	3
497		2	max	36.863	5	248.38	2	6.35	5	.01	3	.02	1	.084	3
498			min	-42.169	1	-109.157	3	-80.694	1	-.016	2	-.028	5	-.191	2
499		3	max	30.537	5	146.414	2	7.789	5	.01	3	0	12	.139	3
500			min	-42.169	1	-64.802	3	-55.254	1	-.016	2	-.029	4	-.317	2
501		4	max	24.211	5	44.447	2	9.229	5	.01	3	-.002	12	.167	3
502			min	-42.169	1	-20.447	3	-29.814	1	-.016	2	-.051	1	-.378	2
503		5	max	17.885	5	23.908	3	10.668	5	.01	3	-.003	12	.166	3
504			min	-42.169	1	-57.52	2	-4.373	1	-.016	2	-.062	1	-.374	2
505		6	max	11.559	5	68.264	3	21.067	1	.01	3	-.003	15	.136	3
506			min	-42.169	1	-159.486	2	-.241	3	-.016	2	-.056	1	-.305	2
507		7	max	5.233	5	112.619	3	46.507	1	.01	3	.004	5	.078	3
508			min	-42.169	1	-261.453	2	.836	12	-.016	2	-.035	1	-.17	2
509		8	max	.569	3	156.974	3	71.948	1	.01	3	.013	4	.029	2
510			min	-42.169	1	-363.42	2	1.744	12	-.016	2	-.004	3	-.008	3
511		9	max	.569	3	201.329	3	97.388	1	.01	3	.057	1	.294	2
512			min	-42.169	1	-465.386	2	2.652	12	-.016	2	-.002	3	-.122	3
513		10	max	25.058	5	-11.097	15	122.829	1	.004	14	.127	1	.624	2
514			min	-42.169	1	-567.353	2	-5.778	3	-.016	2	.003	12	-.265	3
515		11	max	18.732	5	465.386	2	2.811	5	.016	2	.056	1	.294	2
516			min	-42.016	1	-201.329	3	-97.009	1	-.01	3	-.013	5	-.122	3
517		12	max	12.406	5	363.42	2	4.251	5	.016	2	.003	2	.029	2
518			min	-42.016	1	-156.974	3	-71.568	1	-.01	3	-.011	5	-.008	3
519		13	max	6.08	5	261.453	2	5.69	5	.016	2	-.001	12	.078	3
520			min	-42.016	1	-112.619	3	-46.128	1	-.01	3	-.035	1	-.17	2
521		14	max	-.103	15	159.486	2	7.13	5	.016	2	-.002	12	.136	3
522			min	-42.016	1	-68.264	3	-20.688	1	-.01	3	-.056	1	-.305	2
523		15	max	-2.831	12	57.52	2	9.796	4	.016	2	.001	5	.166	3
524			min	-42.016	1	-23.908	3	-.399	10	-.01	3	-.062	1	-.374	2
525		16	max	-2.831	12	20.447	3	30.193	1	.016	2	.007	5	.167	3
526			min	-42.016	1	-44.447	2	1.548	12	-.01	3	-.05	1	-.378	2
527		17	max	-2.831	12	64.802	3	55.634	1	.016	2	.014	5	.139	3
528			min	-42.016	1	-146.414	2	2.456	12	-.01	3	-.023	1	-.317	2
529		18	max	-2.831	12	109.157	3	81.074	1	.016	2	.027	4	.084	3
530			min	-42.016	1	-248.381	2	3.364	12	-.01	3	0	10	-.191	2
531		19	max	-2.831	12	153.512	3	106.514	1	.016	2	.081	1	0	2
532			min	-42.016	1	-350.347	2	4.272	12	-.01	3	.005	12	0	5
533	M15	1	max	0	1	1.309	9	.062	3	0	9	0	9	0	1
534			min	-62.246	3	0	1	-.022	9	0	3	0	3	0	1
535		2	max	0	1	1.164	9	.062	3	0	9	0	9	0	1
536			min	-62.311	3	0	1	-.022	9	0	3	0	3	0	9
537		3	max	0	1	1.018	9	.062	3	0	9	0	9	0	1
538			min	-62.376	3	0	1	-.022	9	0	3	0	3	0	9
539		4	max	0	1	.873	9	.062	3	0	9	0	9	0	1
540			min	-62.441	3	0	1	-.022	9	0	3	0	3	-.001	9
541		5	max	0	1	.727	9	.062	3	0	9	0	9	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-62.507	3	0	1	-.022	9	0	3	0	3	-.001	9
543		6	max	0	1	.582	9	.062	3	0	9	0	9	0	1
544			min	-62.572	3	0	1	-.022	9	0	3	0	3	-.002	9
545		7	max	0	1	.436	9	.062	3	0	9	0	3	0	1
546			min	-62.637	3	0	1	-.022	9	0	3	0	9	-.002	9
547		8	max	0	1	.291	9	.062	3	0	9	0	3	0	1
548			min	-62.702	3	0	1	-.022	9	0	3	0	9	-.002	9
549		9	max	0	1	.145	9	.062	3	0	9	0	3	0	1
550			min	-62.767	3	0	1	-.022	9	0	3	0	9	-.002	9
551		10	max	0	1	0	1	.062	3	0	9	0	3	0	1
552			min	-62.833	3	0	1	-.022	9	0	3	0	9	-.002	9
553		11	max	0	1	0	1	.062	3	0	9	0	3	0	1
554			min	-62.898	3	-.145	9	-.022	9	0	3	0	9	-.002	9
555		12	max	0	1	0	1	.062	3	0	9	0	3	0	1
556			min	-62.963	3	-.291	9	-.022	9	0	3	0	9	-.002	9
557		13	max	0	1	0	1	.062	3	0	9	0	3	0	1
558			min	-63.028	3	-.436	9	-.022	9	0	3	0	9	-.002	9
559		14	max	0	1	0	1	.062	3	0	9	0	3	0	1
560			min	-63.093	3	-.582	9	-.022	9	0	3	0	9	-.002	9
561		15	max	0	1	0	1	.062	3	0	9	0	3	0	1
562			min	-63.158	3	-.727	9	-.022	9	0	3	0	9	-.001	9
563		16	max	0	1	0	1	.062	3	0	9	0	3	0	1
564			min	-63.224	3	-.873	9	-.022	9	0	3	0	9	-.001	9
565		17	max	0	1	0	1	.062	3	0	9	0	3	0	1
566			min	-63.289	3	-1.018	9	-.022	9	0	3	0	9	0	9
567		18	max	0	1	0	1	.062	3	0	9	0	3	0	1
568			min	-63.354	3	-1.164	9	-.022	9	0	3	0	9	0	9
569		19	max	0	1	0	1	.062	3	0	9	0	3	0	1
570			min	-63.419	3	-1.309	9	-.022	9	0	3	0	9	0	1
571	M16A	1	max	0	10	2.686	4	.263	4	0	3	0	3	0	1
572			min	-209.906	4	0	10	-.028	3	0	2	0	4	0	1
573		2	max	0	10	2.387	4	.237	4	0	3	0	3	0	10
574			min	-209.944	4	0	10	-.028	3	0	2	0	4	0	4
575		3	max	0	10	2.089	4	.212	4	0	3	0	3	0	10
576			min	-209.982	4	0	10	-.028	3	0	2	0	4	-.002	4
577		4	max	0	10	1.791	4	.186	4	0	3	0	3	0	10
578			min	-210.02	4	0	10	-.028	3	0	2	0	1	-.002	4
579		5	max	0	10	1.492	4	.16	4	0	3	0	3	0	10
580			min	-210.058	4	0	10	-.028	3	0	2	0	1	-.003	4
581		6	max	0	10	1.194	4	.135	4	0	3	0	3	0	10
582			min	-210.096	4	0	10	-.028	3	0	2	0	1	-.004	4
583		7	max	0	10	.895	4	.109	4	0	3	0	5	0	10
584			min	-210.134	4	0	10	-.028	3	0	2	0	1	-.004	4
585		8	max	0	10	.597	4	.083	4	0	3	0	5	0	10
586			min	-210.172	4	0	10	-.028	3	0	2	0	1	-.004	4
587		9	max	0	10	.298	4	.057	4	0	3	0	5	0	10
588			min	-210.21	4	0	10	-.028	3	0	2	0	1	-.004	4
589		10	max	0	10	0	1	.032	4	0	3	0	5	0	10
590			min	-210.248	4	0	1	-.028	3	0	2	0	1	-.004	4
591		11	max	0	10	0	10	.031	1	0	3	0	5	0	10
592			min	-210.286	4	-.298	4	-.028	3	0	2	0	1	-.004	4
593		12	max	0	10	0	10	.031	1	0	3	0	5	0	10
594			min	-210.324	4	-.597	4	-.028	3	0	2	0	1	-.004	4
595		13	max	0	10	0	10	.031	1	0	3	0	5	0	10
596			min	-210.362	4	-.895	4	-.049	5	0	2	0	3	-.004	4
597		14	max	.011	2	0	10	.031	1	0	3	0	4	0	10
598			min	-210.4	4	-1.194	4	-.075	5	0	2	0	3	-.004	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.098	2	0	10	.031	1	0	3	0	4	0	10
600			min	-210.438	4	-1.492	4	-.101	5	0	2	0	3	-.003	4
601		16	max	.185	2	0	10	.031	1	0	3	0	4	0	10
602			min	-210.475	4	-1.791	4	-.127	5	0	2	0	3	-.002	4
603		17	max	.272	2	0	10	.031	1	0	3	0	1	0	10
604			min	-210.513	4	-2.089	4	-.152	5	0	2	0	3	-.002	4
605		18	max	.359	2	0	10	.031	1	0	3	0	1	0	10
606			min	-210.551	4	-2.387	4	-.178	5	0	2	0	5	0	4
607		19	max	.446	2	0	10	.031	1	0	3	0	1	0	1
608			min	-210.589	4	-2.686	4	-.204	5	0	2	0	5	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	1	.009	2	.008	1	1.276e-3	5	NC	3	NC	2
2			min	-.003	3	-.008	3	-.013	5	-6.235e-4	1	4105.946	2	4392.654	1
3		2	max	.002	1	.008	2	.008	1	1.299e-3	5	NC	3	NC	2
4			min	-.003	3	-.008	3	-.012	5	-5.976e-4	1	4460.241	2	4746.502	1
5		3	max	.002	1	.007	2	.007	1	1.322e-3	5	NC	3	NC	2
6			min	-.003	3	-.008	3	-.012	5	-5.717e-4	1	4877.905	2	5163.797	1
7		4	max	.002	1	.007	2	.006	1	1.346e-3	5	NC	3	NC	2
8			min	-.003	3	-.007	3	-.012	5	-5.457e-4	1	5373.53	2	5659.893	1
9		5	max	.002	1	.006	2	.006	1	1.369e-3	5	NC	1	NC	2
10			min	-.003	3	-.007	3	-.011	5	-5.198e-4	1	5966.366	2	6255.297	1
11		6	max	.002	1	.005	2	.005	1	1.392e-3	5	NC	1	NC	2
12			min	-.002	3	-.007	3	-.011	5	-4.939e-4	1	6682.212	2	6977.894	1
13		7	max	.002	1	.005	2	.005	1	1.415e-3	5	NC	1	NC	2
14			min	-.002	3	-.006	3	-.01	5	-4.68e-4	1	7556.29	2	7866.404	1
15		8	max	.002	1	.004	2	.004	1	1.438e-3	5	NC	1	NC	2
16			min	-.002	3	-.006	3	-.009	5	-4.42e-4	1	8637.739	2	8975.889	1
17		9	max	.001	1	.004	2	.004	1	1.461e-3	5	NC	1	NC	1
18			min	-.002	3	-.005	3	-.009	5	-4.161e-4	1	9996.874	2	NC	1
19		10	max	.001	1	.003	2	.003	1	1.484e-3	5	NC	1	NC	1
20			min	-.002	3	-.005	3	-.008	5	-3.902e-4	1	NC	1	NC	1
21		11	max	.001	1	.003	2	.002	1	1.507e-3	5	NC	1	NC	1
22			min	-.001	3	-.004	3	-.007	5	-3.643e-4	1	NC	1	NC	1
23		12	max	0	1	.002	2	.002	1	1.531e-3	5	NC	1	NC	1
24			min	-.001	3	-.004	3	-.007	5	-3.383e-4	1	NC	1	NC	1
25		13	max	0	1	.002	2	.002	1	1.554e-3	5	NC	1	NC	1
26			min	-.001	3	-.003	3	-.006	5	-3.124e-4	1	NC	1	NC	1
27		14	max	0	1	.001	2	.001	1	1.577e-3	5	NC	1	NC	1
28			min	0	3	-.003	3	-.005	5	-2.865e-4	1	NC	1	NC	1
29		15	max	0	1	0	2	0	1	1.6e-3	5	NC	1	NC	1
30			min	0	3	-.002	3	-.004	5	-2.606e-4	1	NC	1	NC	1
31		16	max	0	1	0	2	0	1	1.623e-3	5	NC	1	NC	1
32			min	0	3	-.002	3	-.003	5	-2.346e-4	1	NC	1	NC	1
33		17	max	0	1	0	2	0	1	1.646e-3	5	NC	1	NC	1
34			min	0	3	-.001	3	-.002	5	-2.087e-4	1	NC	1	NC	1
35		18	max	0	1	0	2	0	1	1.669e-3	5	NC	1	NC	1
36			min	0	3	0	3	-.001	5	-1.828e-4	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	1.692e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-1.569e-4	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	7.296e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-7.874e-4	5	NC	1	NC	1
41		2	max	0	3	0	2	.004	5	9.026e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	1	-7.927e-4	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	3	0	2	.008	5	1.076e-4	1	NC	1	NC	1
44			min	0	2	-.002	3	0	1	-7.98e-4	5	NC	1	NC	1
45		4	max	0	3	0	2	.012	5	1.248e-4	1	NC	1	NC	1
46			min	0	2	-.003	3	0	1	-8.034e-4	5	NC	1	NC	1
47		5	max	0	3	0	2	.016	5	1.421e-4	1	NC	1	NC	1
48			min	0	2	-.003	3	0	1	-8.087e-4	5	NC	1	NC	1
49		6	max	0	3	0	2	.02	4	1.594e-4	1	NC	1	NC	1
50			min	0	2	-.004	3	0	1	-8.14e-4	5	NC	1	NC	1
51		7	max	0	3	0	2	.025	4	1.767e-4	1	NC	1	NC	1
52			min	0	2	-.005	3	0	1	-8.194e-4	5	NC	1	NC	1
53		8	max	0	3	.001	2	.029	4	1.94e-4	1	NC	1	NC	1
54			min	0	2	-.005	3	0	1	-8.247e-4	5	NC	1	NC	1
55		9	max	0	3	.002	2	.033	4	2.113e-4	1	NC	1	NC	1
56			min	0	2	-.006	3	0	1	-8.3e-4	5	NC	1	NC	1
57		10	max	0	3	.002	2	.036	4	2.286e-4	1	NC	1	NC	1
58			min	0	2	-.007	3	0	10	-8.354e-4	5	NC	1	NC	1
59		11	max	0	3	.003	2	.04	4	2.459e-4	1	NC	1	NC	1
60			min	0	2	-.007	3	0	10	-8.407e-4	5	NC	1	NC	1
61		12	max	0	3	.003	2	.044	4	2.632e-4	1	NC	1	NC	1
62			min	0	2	-.007	3	0	10	-8.46e-4	5	NC	1	NC	1
63		13	max	0	3	.004	2	.048	4	2.805e-4	1	NC	1	NC	1
64			min	0	2	-.008	3	0	10	-8.513e-4	5	NC	1	NC	1
65		14	max	.001	3	.005	2	.051	4	2.978e-4	1	NC	1	NC	1
66			min	-.001	2	-.008	3	0	10	-8.567e-4	5	9624.879	2	NC	1
67		15	max	.001	3	.006	2	.055	4	3.151e-4	1	NC	1	NC	1
68			min	-.001	2	-.008	3	0	10	-8.62e-4	5	8123.978	2	NC	1
69		16	max	.001	3	.007	2	.058	4	3.324e-4	1	NC	1	NC	1
70			min	-.001	2	-.008	3	0	10	-8.673e-4	5	6954.635	2	NC	1
71		17	max	.001	3	.008	2	.062	4	3.497e-4	1	NC	3	NC	1
72			min	-.001	2	-.008	3	0	10	-8.727e-4	5	6034.719	2	NC	1
73		18	max	.001	3	.009	2	.065	4	3.669e-4	1	NC	3	NC	1
74			min	-.001	2	-.008	3	0	10	-8.78e-4	5	5304.913	2	NC	1
75		19	max	.001	3	.01	2	.068	4	3.842e-4	1	NC	3	NC	1
76			min	-.001	2	-.008	3	0	10	-8.833e-4	5	4722.106	2	NC	1
77	M4	1	max	.002	1	.01	2	0	10	4.065e-3	5	NC	1	NC	2
78			min	0	3	-.008	3	-.072	4	-5.21e-4	1	NC	1	267.862	4
79		2	max	.002	1	.01	2	0	10	4.065e-3	5	NC	1	NC	2
80			min	0	3	-.008	3	-.066	4	-5.21e-4	1	NC	1	291.993	4
81		3	max	.002	1	.009	2	0	10	4.065e-3	5	NC	1	NC	2
82			min	0	3	-.007	3	-.06	4	-5.21e-4	1	NC	1	320.714	4
83		4	max	.002	1	.008	2	0	10	4.065e-3	5	NC	1	NC	2
84			min	0	3	-.007	3	-.054	4	-5.21e-4	1	NC	1	355.233	4
85		5	max	.001	1	.008	2	0	10	4.065e-3	5	NC	1	NC	1
86			min	0	3	-.006	3	-.049	4	-5.21e-4	1	NC	1	397.197	4
87		6	max	.001	1	.007	2	0	10	4.065e-3	5	NC	1	NC	1
88			min	0	3	-.006	3	-.043	4	-5.21e-4	1	NC	1	448.894	4
89		7	max	.001	1	.007	2	0	10	4.065e-3	5	NC	1	NC	1
90			min	0	3	-.006	3	-.038	4	-5.21e-4	1	NC	1	513.588	4
91		8	max	.001	1	.006	2	0	10	4.065e-3	5	NC	1	NC	1
92			min	0	3	-.005	3	-.032	4	-5.21e-4	1	NC	1	596.051	4
93		9	max	.001	1	.006	2	0	10	4.065e-3	5	NC	1	NC	1
94			min	0	3	-.005	3	-.027	4	-5.21e-4	1	NC	1	703.507	4
95		10	max	0	1	.005	2	0	10	4.065e-3	5	NC	1	NC	1
96			min	0	3	-.004	3	-.023	4	-5.21e-4	1	NC	1	847.309	4
97		11	max	0	1	.004	2	0	10	4.065e-3	5	NC	1	NC	1
98			min	0	3	-.004	3	-.018	4	-5.21e-4	1	NC	1	1046.154	4
99		12	max	0	1	.004	2	0	10	4.065e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	3	-.003	3	-.015	4	-5.21e-4	1	NC	1	1332.655	4
101		13	max	0	1	.003	2	0	10	4.065e-3	5	NC	1	NC	1
102			min	0	3	-.003	3	-.011	4	-5.21e-4	1	NC	1	1767.987	4
103		14	max	0	1	.003	2	0	10	4.065e-3	5	NC	1	NC	1
104			min	0	3	-.002	3	-.008	4	-5.21e-4	1	NC	1	2478.33	4
105		15	max	0	1	.002	2	0	10	4.065e-3	5	NC	1	NC	1
106			min	0	3	-.002	3	-.005	4	-5.21e-4	1	NC	1	3760.121	4
107		16	max	0	1	.002	2	0	10	4.065e-3	5	NC	1	NC	1
108			min	0	3	-.001	3	-.003	4	-5.21e-4	1	NC	1	6456.046	4
109		17	max	0	1	.001	2	0	10	4.065e-3	5	NC	1	NC	1
110			min	0	3	0	3	-.001	4	-5.21e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	10	4.065e-3	5	NC	1	NC	1
112			min	0	3	0	3	0	4	-5.21e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	4.065e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-5.21e-4	1	NC	1	NC	1
115	M6	1	max	.008	1	.026	2	.003	1	1.386e-3	4	NC	3	NC	1
116			min	-.01	3	-.023	3	-.013	5	-6.189e-8	10	1378.654	2	8959.052	3
117		2	max	.007	1	.025	2	.003	1	1.407e-3	4	NC	3	NC	1
118			min	-.01	3	-.022	3	-.013	5	-5.849e-8	10	1474.358	2	9561.844	3
119		3	max	.007	1	.023	2	.003	1	1.429e-3	4	NC	3	NC	1
120			min	-.009	3	-.02	3	-.012	5	-1.238e-6	2	1583.921	2	NC	1
121		4	max	.007	1	.021	2	.003	1	1.45e-3	4	NC	3	NC	1
122			min	-.009	3	-.019	3	-.012	5	-2.78e-6	2	1710.125	2	NC	1
123		5	max	.006	1	.02	2	.002	1	1.471e-3	4	NC	3	NC	1
124			min	-.008	3	-.018	3	-.011	5	-5.314e-6	1	1856.555	2	NC	1
125		6	max	.006	1	.018	2	.002	1	1.493e-3	4	NC	3	NC	1
126			min	-.008	3	-.017	3	-.011	5	-1.002e-5	1	2027.906	2	NC	1
127		7	max	.005	1	.016	2	.002	1	1.514e-3	4	NC	3	NC	1
128			min	-.007	3	-.016	3	-.01	5	-1.473e-5	1	2230.442	2	NC	1
129		8	max	.005	1	.015	2	.002	1	1.536e-3	4	NC	3	NC	1
130			min	-.006	3	-.014	3	-.01	5	-1.944e-5	1	2472.715	2	NC	1
131		9	max	.004	1	.013	2	.001	1	1.557e-3	4	NC	3	NC	1
132			min	-.006	3	-.013	3	-.009	5	-2.415e-5	1	2766.699	2	NC	1
133		10	max	.004	1	.012	2	.001	1	1.578e-3	4	NC	3	NC	1
134			min	-.005	3	-.012	3	-.008	5	-2.886e-5	1	3129.697	2	NC	1
135		11	max	.004	1	.01	2	.001	1	1.6e-3	4	NC	3	NC	1
136			min	-.005	3	-.011	3	-.008	5	-3.357e-5	1	3587.663	2	NC	1
137		12	max	.003	1	.009	2	0	1	1.621e-3	4	NC	3	NC	1
138			min	-.004	3	-.009	3	-.007	5	-3.828e-5	1	4181.383	2	NC	1
139		13	max	.003	1	.007	2	0	1	1.642e-3	4	NC	3	NC	1
140			min	-.003	3	-.008	3	-.006	5	-4.299e-5	1	4978.831	2	NC	1
141		14	max	.002	1	.006	2	0	1	1.664e-3	4	NC	3	NC	1
142			min	-.003	3	-.007	3	-.005	5	-4.77e-5	1	6102.347	2	NC	1
143		15	max	.002	1	.005	2	0	1	1.685e-3	4	NC	1	NC	1
144			min	-.002	3	-.005	3	-.004	5	-5.241e-5	1	7796.59	2	NC	1
145		16	max	.001	1	.003	2	0	1	1.707e-3	4	NC	1	NC	1
146			min	-.002	3	-.004	3	-.003	5	-5.711e-5	1	NC	1	NC	1
147		17	max	0	1	.002	2	0	1	1.728e-3	4	NC	1	NC	1
148			min	-.001	3	-.003	3	-.002	5	-6.182e-5	1	NC	1	NC	1
149		18	max	0	1	.001	2	0	1	1.75e-3	5	NC	1	NC	1
150			min	0	3	-.001	3	-.001	5	-6.653e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.772e-3	5	NC	1	NC	1
152			min	0	1	0	1	0	1	-7.124e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	3.285e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-8.245e-4	5	NC	1	NC	1
155		2	max	0	3	.001	2	.004	5	2.792e-5	1	NC	1	NC	1
156			min	0	2	-.002	3	0	1	-8.149e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	3	.003	2	.009	5	2.298e-5	1	NC	1	NC	1
158			min	0	2	-.003	3	0	1	-8.06e-4	4	NC	1	NC	1
159		4	max	0	3	.004	2	.013	5	1.805e-5	1	NC	1	NC	1
160			min	0	2	-.005	3	0	1	-7.971e-4	4	NC	1	NC	1
161		5	max	0	3	.005	2	.017	5	1.311e-5	1	NC	1	NC	1
162			min	-.001	2	-.007	3	0	1	-7.882e-4	4	9234.078	2	NC	1
163		6	max	.001	3	.006	2	.021	5	1.564e-5	3	NC	1	NC	1
164			min	-.001	2	-.008	3	0	1	-7.793e-4	4	7407.832	2	NC	1
165		7	max	.001	3	.007	2	.026	5	3.274e-5	3	NC	3	NC	1
166			min	-.002	2	-.01	3	0	1	-7.704e-4	4	6156.463	2	NC	1
167		8	max	.002	3	.009	2	.03	4	4.983e-5	3	NC	3	NC	1
168			min	-.002	2	-.011	3	-.001	1	-7.615e-4	4	5237.179	2	NC	1
169		9	max	.002	3	.01	2	.034	4	6.693e-5	3	NC	3	NC	1
170			min	-.002	2	-.013	3	-.001	1	-7.527e-4	4	4529.106	2	NC	1
171		10	max	.002	3	.012	2	.038	4	8.402e-5	3	NC	3	NC	1
172			min	-.003	2	-.014	3	-.001	1	-7.438e-4	4	3965.295	2	NC	1
173		11	max	.002	3	.013	2	.042	4	1.011e-4	3	NC	3	NC	1
174			min	-.003	2	-.015	3	-.001	1	-7.349e-4	4	3505.554	2	NC	1
175		12	max	.003	3	.015	2	.045	4	1.182e-4	3	NC	3	NC	1
176			min	-.003	2	-.017	3	-.001	1	-7.26e-4	4	3124.149	2	NC	1
177		13	max	.003	3	.016	2	.049	4	1.353e-4	3	NC	3	NC	1
178			min	-.004	2	-.018	3	-.002	1	-7.171e-4	4	2803.695	2	NC	1
179		14	max	.003	3	.018	2	.053	4	1.524e-4	3	NC	3	NC	1
180			min	-.004	2	-.019	3	-.002	1	-7.082e-4	4	2531.907	2	NC	1
181		15	max	.003	3	.02	2	.056	4	1.695e-4	3	NC	3	NC	1
182			min	-.004	2	-.019	3	-.002	1	-6.993e-4	4	2299.77	2	NC	1
183		16	max	.004	3	.022	2	.06	4	1.866e-4	3	NC	3	NC	1
184			min	-.004	2	-.02	3	-.002	1	-6.905e-4	4	2100.462	2	NC	1
185		17	max	.004	3	.024	2	.063	4	2.037e-4	3	NC	3	NC	1
186			min	-.005	2	-.021	3	-.002	1	-6.816e-4	4	1928.694	2	NC	1
187		18	max	.004	3	.026	2	.066	4	2.208e-4	3	NC	3	NC	1
188			min	-.005	2	-.022	3	-.002	1	-6.727e-4	4	1780.282	2	NC	1
189		19	max	.004	3	.028	2	.07	4	2.379e-4	3	NC	3	NC	1
190			min	-.005	2	-.023	3	-.002	1	-6.638e-4	4	1651.873	2	NC	1
191	M8	1	max	.005	1	.03	2	.002	1	3.86e-3	4	NC	1	NC	1
192			min	0	3	-.023	3	-.073	4	-1.81e-4	3	NC	1	264.666	4
193		2	max	.005	1	.028	2	.002	1	3.86e-3	4	NC	1	NC	1
194			min	0	3	-.022	3	-.067	4	-1.81e-4	3	NC	1	288.509	4
195		3	max	.005	1	.027	2	.002	1	3.86e-3	4	NC	1	NC	1
196			min	0	3	-.02	3	-.061	4	-1.81e-4	3	NC	1	316.888	4
197		4	max	.004	1	.025	2	.001	1	3.86e-3	4	NC	1	NC	1
198			min	0	3	-.019	3	-.055	4	-1.81e-4	3	NC	1	350.995	4
199		5	max	.004	1	.023	2	.001	1	3.86e-3	4	NC	1	NC	1
200			min	0	3	-.018	3	-.049	4	-1.81e-4	3	NC	1	392.459	4
201		6	max	.004	1	.022	2	.001	1	3.86e-3	4	NC	1	NC	1
202			min	0	3	-.016	3	-.044	4	-1.81e-4	3	NC	1	443.541	4
203		7	max	.003	1	.02	2	0	1	3.86e-3	4	NC	1	NC	1
204			min	0	3	-.015	3	-.038	4	-1.81e-4	3	NC	1	507.463	4
205		8	max	.003	1	.018	2	0	1	3.86e-3	4	NC	1	NC	1
206			min	0	3	-.014	3	-.033	4	-1.81e-4	3	NC	1	588.945	4
207		9	max	.003	1	.017	2	0	1	3.86e-3	4	NC	1	NC	1
208			min	0	3	-.013	3	-.028	4	-1.81e-4	3	NC	1	695.122	4
209		10	max	.003	1	.015	2	0	1	3.86e-3	4	NC	1	NC	1
210			min	0	3	-.011	3	-.023	4	-1.81e-4	3	NC	1	837.211	4
211		11	max	.002	1	.013	2	0	1	3.86e-3	4	NC	1	NC	1
212			min	0	3	-.01	3	-.019	4	-1.81e-4	3	NC	1	1033.689	4
213		12	max	.002	1	.012	2	0	1	3.86e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	3	-.009	3	-.015	4	-1.81e-4	3	NC	1	1316.781	4
215		13	max	.002	1	.01	2	0	1	3.86e-3	4	NC	1	NC	1
216			min	0	3	-.008	3	-.011	4	-1.81e-4	3	NC	1	1746.933	4
217		14	max	.001	1	.008	2	0	1	3.86e-3	4	NC	1	NC	1
218			min	0	3	-.006	3	-.008	4	-1.81e-4	3	NC	1	2448.824	4
219		15	max	.001	1	.007	2	0	1	3.86e-3	4	NC	1	NC	1
220			min	0	3	-.005	3	-.005	4	-1.81e-4	3	NC	1	3715.367	4
221		16	max	0	1	.005	2	0	1	3.86e-3	4	NC	1	NC	1
222			min	0	3	-.004	3	-.003	4	-1.81e-4	3	NC	1	6379.227	4
223		17	max	0	1	.003	2	0	1	3.86e-3	4	NC	1	NC	1
224			min	0	3	-.003	3	-.001	4	-1.81e-4	3	NC	1	NC	1
225		18	max	0	1	.002	2	0	1	3.86e-3	4	NC	1	NC	1
226			min	0	3	-.001	3	0	4	-1.81e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	3.86e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-1.81e-4	3	NC	1	NC	1
229	M10	1	max	.003	1	.009	2	0	3	6.436e-4	1	NC	3	NC	1
230			min	-.003	3	-.008	3	-.006	4	-3.634e-4	3	4110.754	2	NC	1
231		2	max	.002	1	.008	2	0	3	6.105e-4	1	NC	3	NC	1
232			min	-.003	3	-.008	3	-.006	4	-3.517e-4	3	4465.585	2	NC	1
233		3	max	.002	1	.007	2	0	3	5.773e-4	1	NC	3	NC	1
234			min	-.003	3	-.008	3	-.006	4	-3.4e-4	3	4883.903	2	NC	1
235		4	max	.002	1	.007	2	0	3	5.442e-4	1	NC	3	NC	1
236			min	-.003	3	-.007	3	-.006	4	-3.284e-4	3	5380.332	2	NC	1
237		5	max	.002	1	.006	2	0	3	5.364e-4	4	NC	1	NC	1
238			min	-.002	3	-.007	3	-.006	4	-3.167e-4	3	5974.166	2	NC	1
239		6	max	.002	1	.005	2	0	3	5.952e-4	4	NC	1	NC	1
240			min	-.002	3	-.007	3	-.006	4	-3.05e-4	3	6691.263	2	NC	1
241		7	max	.002	1	.005	2	0	3	6.541e-4	4	NC	1	NC	1
242			min	-.002	3	-.006	3	-.006	4	-2.933e-4	3	7566.931	2	NC	1
243		8	max	.002	1	.004	2	0	3	7.13e-4	4	NC	1	NC	1
244			min	-.002	3	-.006	3	-.006	4	-2.816e-4	3	8650.429	2	NC	1
245		9	max	.001	1	.004	2	0	3	7.718e-4	4	NC	1	NC	1
246			min	-.002	3	-.005	3	-.005	4	-2.699e-4	3	NC	1	NC	1
247		10	max	.001	1	.003	2	0	3	8.307e-4	4	NC	1	NC	1
248			min	-.002	3	-.005	3	-.005	4	-2.582e-4	3	NC	1	NC	1
249		11	max	.001	1	.003	2	0	3	8.895e-4	4	NC	1	NC	1
250			min	-.001	3	-.005	3	-.005	4	-2.465e-4	3	NC	1	NC	1
251		12	max	0	1	.002	2	0	3	9.484e-4	4	NC	1	NC	1
252			min	-.001	3	-.004	3	-.004	4	-2.348e-4	3	NC	1	NC	1
253		13	max	0	1	.002	2	0	3	1.007e-3	4	NC	1	NC	1
254			min	-.001	3	-.004	3	-.004	4	-2.231e-4	3	NC	1	NC	1
255		14	max	0	1	.001	2	0	3	1.066e-3	4	NC	1	NC	1
256			min	0	3	-.003	3	-.004	4	-2.114e-4	3	NC	1	NC	1
257		15	max	0	1	0	2	0	3	1.125e-3	4	NC	1	NC	1
258			min	0	3	-.003	3	-.003	4	-1.997e-4	3	NC	1	NC	1
259		16	max	0	1	0	2	0	3	1.184e-3	4	NC	1	NC	1
260			min	0	3	-.002	3	-.002	4	-1.88e-4	3	NC	1	NC	1
261		17	max	0	1	0	2	0	3	1.243e-3	4	NC	1	NC	1
262			min	0	3	-.001	3	-.002	4	-1.763e-4	3	NC	1	NC	1
263		18	max	0	1	0	2	0	3	1.302e-3	4	NC	1	NC	1
264			min	0	3	0	3	0	4	-1.646e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.36e-3	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-1.529e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	7.124e-5	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-6.336e-4	4	NC	1	NC	1
269		2	max	0	3	0	2	.003	4	5.358e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-6.998e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	3	0	2	.007	4	3.593e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-7.66e-4	4	NC	1	NC	1
273		4	max	0	3	0	2	.01	4	1.828e-5	3	NC	1	NC	1
274			min	0	2	-.003	3	0	3	-8.322e-4	4	NC	1	NC	1
275		5	max	0	3	0	2	.013	4	6.249e-7	3	NC	1	NC	1
276			min	0	2	-.003	3	-.001	3	-8.984e-4	4	NC	1	NC	1
277		6	max	0	3	0	2	.017	5	-1.09e-5	12	NC	1	NC	1
278			min	0	2	-.004	3	-.001	3	-9.646e-4	4	NC	1	NC	1
279		7	max	0	3	0	2	.02	5	-1.32e-5	10	NC	1	NC	1
280			min	0	2	-.005	3	-.002	3	-1.031e-3	4	NC	1	NC	1
281		8	max	0	3	.001	2	.024	5	-1.482e-5	10	NC	1	NC	1
282			min	0	2	-.006	3	-.002	3	-1.097e-3	4	NC	1	NC	1
283		9	max	0	3	.002	2	.027	5	-1.644e-5	10	NC	1	NC	1
284			min	0	2	-.006	3	-.002	3	-1.163e-3	4	NC	1	NC	1
285		10	max	0	3	.002	2	.031	5	-1.806e-5	10	NC	1	NC	1
286			min	0	2	-.007	3	-.002	1	-1.229e-3	4	NC	1	NC	1
287		11	max	0	3	.003	2	.034	5	-1.968e-5	10	NC	1	NC	1
288			min	0	2	-.007	3	-.003	1	-1.295e-3	4	NC	1	NC	1
289		12	max	0	3	.003	2	.037	5	-2.13e-5	10	NC	1	NC	1
290			min	0	2	-.008	3	-.004	1	-1.362e-3	4	NC	1	NC	1
291		13	max	0	3	.004	2	.041	5	-2.292e-5	10	NC	1	NC	1
292			min	0	2	-.008	3	-.004	1	-1.428e-3	4	NC	1	NC	1
293		14	max	.001	3	.005	2	.044	5	-2.453e-5	10	NC	1	NC	2
294			min	-.001	2	-.008	3	-.005	1	-1.494e-3	4	9640.454	2	9385.562	1
295		15	max	.001	3	.006	2	.047	5	-2.615e-5	10	NC	1	NC	2
296			min	-.001	2	-.008	3	-.006	1	-1.56e-3	4	8135.856	2	8319.457	1
297		16	max	.001	3	.007	2	.051	5	-2.777e-5	10	NC	1	NC	2
298			min	-.001	2	-.008	3	-.006	1	-1.626e-3	4	6963.91	2	7478.029	1
299		17	max	.001	3	.008	2	.054	5	-2.939e-5	10	NC	3	NC	2
300			min	-.001	2	-.008	3	-.007	1	-1.693e-3	4	6042.13	2	6805.51	1
301		18	max	.001	3	.009	2	.058	5	-3.101e-5	10	NC	3	NC	2
302			min	-.001	2	-.008	3	-.007	1	-1.759e-3	4	5310.969	2	6263.21	1
303		19	max	.001	3	.01	2	.061	5	-3.263e-5	10	NC	3	NC	2
304			min	-.001	2	-.008	3	-.008	1	-1.825e-3	4	4727.165	2	5823.713	1
305	M12	1	max	.002	1	.01	2	.007	1	4.873e-3	4	NC	1	NC	3
306			min	0	3	-.008	3	-.067	5	3.5e-5	10	NC	1	288.511	5
307		2	max	.002	1	.01	2	.006	1	4.873e-3	4	NC	1	NC	2
308			min	0	3	-.008	3	-.061	5	3.5e-5	10	NC	1	314.497	5
309		3	max	.002	1	.009	2	.006	1	4.873e-3	4	NC	1	NC	2
310			min	0	3	-.007	3	-.056	5	3.5e-5	10	NC	1	345.425	5
311		4	max	.002	1	.008	2	.005	1	4.873e-3	4	NC	1	NC	2
312			min	0	3	-.007	3	-.051	5	3.5e-5	10	NC	1	382.595	5
313		5	max	.001	1	.008	2	.005	1	4.873e-3	4	NC	1	NC	2
314			min	0	3	-.007	3	-.045	5	3.5e-5	10	NC	1	427.78	5
315		6	max	.001	1	.007	2	.004	1	4.873e-3	4	NC	1	NC	2
316			min	0	3	-.006	3	-.04	5	3.5e-5	10	NC	1	483.447	5
317		7	max	.001	1	.007	2	.003	1	4.873e-3	4	NC	1	NC	2
318			min	0	3	-.006	3	-.035	5	3.5e-5	10	NC	1	553.105	5
319		8	max	.001	1	.006	2	.003	1	4.873e-3	4	NC	1	NC	2
320			min	0	3	-.005	3	-.03	5	3.5e-5	10	NC	1	641.897	5
321		9	max	.001	1	.006	2	.003	1	4.873e-3	4	NC	1	NC	2
322			min	0	3	-.005	3	-.026	5	3.5e-5	10	NC	1	757.597	5
323		10	max	0	1	.005	2	.002	1	4.873e-3	4	NC	1	NC	2
324			min	0	3	-.004	3	-.021	5	3.5e-5	10	NC	1	912.429	5
325		11	max	0	1	.004	2	.002	1	4.873e-3	4	NC	1	NC	1
326			min	0	3	-.004	3	-.017	5	3.5e-5	10	NC	1	1126.523	5
327		12	max	0	1	.004	2	.001	1	4.873e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	3	-.003	3	-.013	5	3.5e-5	10	NC	1	1434.991	5
329		13	max	0	1	.003	2	.001	1	4.873e-3	4	NC	1	NC	1
330			min	0	3	-.003	3	-.01	5	3.5e-5	10	NC	1	1903.693	5
331		14	max	0	1	.003	2	0	1	4.873e-3	4	NC	1	NC	1
332			min	0	3	-.002	3	-.007	5	3.5e-5	10	NC	1	2668.475	5
333		15	max	0	1	.002	2	0	1	4.873e-3	4	NC	1	NC	1
334			min	0	3	-.002	3	-.005	5	3.5e-5	10	NC	1	4048.478	5
335		16	max	0	1	.002	2	0	1	4.873e-3	4	NC	1	NC	1
336			min	0	3	-.001	3	-.003	5	3.5e-5	10	NC	1	6950.917	5
337		17	max	0	1	.001	2	0	1	4.873e-3	4	NC	1	NC	1
338			min	0	3	0	3	-.001	5	3.5e-5	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	4.873e-3	4	NC	1	NC	1
340			min	0	3	0	3	0	5	3.5e-5	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	4.873e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	3.5e-5	10	NC	1	NC	1
343	M1	1	max	.008	3	.025	3	.007	5	6.889e-3	1	NC	1	NC	1
344			min	-.008	2	-.023	2	-.003	1	-8.488e-3	3	NC	1	NC	1
345		2	max	.008	3	.014	3	.01	5	3.217e-3	1	NC	4	NC	1
346			min	-.008	2	-.013	2	-.006	1	-4.188e-3	3	4372.756	2	NC	1
347		3	max	.008	3	.004	3	.013	5	3.929e-4	5	NC	4	NC	2
348			min	-.008	2	-.003	2	-.008	1	-3.868e-4	1	2252.651	2	8253.711	5
349		4	max	.008	3	.005	2	.016	5	3.967e-4	5	NC	4	NC	2
350			min	-.008	2	-.004	3	-.009	1	-3.29e-4	1	1579.642	2	5165.92	5
351		5	max	.008	3	.013	2	.02	5	4.004e-4	5	NC	5	NC	2
352			min	-.008	2	-.011	3	-.009	1	-2.713e-4	1	1254.147	2	3671.374	5
353		6	max	.008	3	.019	2	.024	5	4.042e-4	5	NC	5	NC	2
354			min	-.008	2	-.017	3	-.009	1	-2.136e-4	1	1068.476	2	2804.779	5
355		7	max	.008	3	.024	2	.028	5	4.08e-4	5	NC	5	NC	2
356			min	-.008	2	-.021	3	-.008	1	-1.558e-4	1	954.316	2	2247.072	5
357		8	max	.008	3	.027	2	.032	5	4.117e-4	5	NC	5	NC	1
358			min	-.008	2	-.024	3	-.006	1	-9.812e-5	1	883.131	2	1862.726	5
359		9	max	.008	3	.03	2	.037	5	4.155e-4	5	NC	5	NC	1
360			min	-.008	2	-.026	3	-.005	1	-4.039e-5	1	841.472	2	1583.379	4
361		10	max	.008	3	.031	2	.041	5	4.249e-4	4	NC	5	NC	1
362			min	-.008	2	-.026	3	-.003	1	8.439e-6	10	822.958	2	1357.278	4
363		11	max	.008	3	.03	2	.046	4	4.415e-4	4	NC	5	NC	1
364			min	-.008	2	-.025	3	0	1	1.219e-5	10	825.348	2	1187.04	4
365		12	max	.008	3	.028	2	.051	4	4.58e-4	4	NC	5	NC	1
366			min	-.008	2	-.023	3	0	10	1.594e-5	10	849.693	2	1055.981	4
367		13	max	.008	3	.025	2	.056	4	4.746e-4	4	NC	5	NC	2
368			min	-.009	2	-.02	3	0	10	1.969e-5	10	900.873	2	953.39	4
369		14	max	.008	3	.02	2	.06	4	4.911e-4	4	NC	5	NC	2
370			min	-.009	2	-.015	3	0	10	2.344e-5	10	990.037	2	872.138	4
371		15	max	.008	3	.013	2	.065	4	5.077e-4	4	NC	4	NC	2
372			min	-.009	2	-.01	3	0	10	2.719e-5	10	1141.54	2	807.341	4
373		16	max	.008	3	.005	2	.069	4	7.589e-4	4	NC	4	NC	2
374			min	-.009	2	-.004	3	0	10	2.998e-5	10	1414.625	2	755.579	4
375		17	max	.008	3	.004	3	.072	4	6.594e-3	4	NC	4	NC	2
376			min	-.009	2	-.005	2	0	10	-1.297e-5	1	1996.329	2	714.469	4
377		18	max	.008	3	.012	3	.075	4	4.334e-3	2	NC	4	NC	1
378			min	-.009	2	-.017	2	0	10	-1.969e-3	3	3852.882	2	682.192	4
379		19	max	.008	3	.02	3	.078	4	8.729e-3	2	NC	1	NC	1
380			min	-.009	2	-.03	2	-.002	1	-4.016e-3	3	NC	1	658.265	4
381	M5	1	max	.021	3	.071	3	.007	5	9.443e-6	4	NC	1	NC	1
382			min	-.025	2	-.065	2	-.004	1	3.427e-8	2	NC	1	NC	1
383		2	max	.021	3	.041	3	.01	5	1.952e-4	5	NC	4	NC	1
384			min	-.025	2	-.037	2	-.004	1	-6.538e-5	1	1597.916	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.021	3	.013	3	.013	5	3.78e-4	5	NC	5	NC	1
386			min	-.025	2	-.01	1	-.003	1	-1.296e-4	1	818.586	2	NC	1
387		4	max	.021	3	.014	2	.017	5	3.946e-4	5	NC	5	NC	1
388			min	-.025	2	-.01	3	-.003	1	-1.234e-4	1	572.579	2	NC	1
389		5	max	.021	3	.034	2	.021	5	4.112e-4	5	NC	5	NC	1
390			min	-.025	2	-.03	3	-.003	1	-1.172e-4	1	453.631	2	NC	1
391		6	max	.021	3	.051	2	.025	5	4.278e-4	5	NC	5	NC	1
392			min	-.025	2	-.045	3	-.003	1	-1.109e-4	1	385.737	2	NC	1
393		7	max	.021	3	.065	2	.03	5	4.444e-4	5	NC	5	NC	1
394			min	-.025	2	-.056	3	-.003	1	-1.047e-4	1	343.92	2	NC	1
395		8	max	.021	3	.075	2	.034	5	4.61e-4	5	NC	5	NC	1
396			min	-.025	2	-.064	3	-.003	1	-9.851e-5	1	317.752	2	NC	1
397		9	max	.021	3	.082	2	.039	5	4.776e-4	5	NC	15	NC	1
398			min	-.025	2	-.069	3	-.003	1	-9.229e-5	1	302.312	2	NC	1
399		10	max	.021	3	.084	2	.044	5	4.942e-4	5	NC	15	NC	1
400			min	-.025	2	-.069	3	-.003	1	-8.608e-5	1	295.257	2	NC	1
401		11	max	.021	3	.083	2	.049	5	5.108e-4	5	NC	15	NC	1
402			min	-.025	2	-.067	3	-.003	1	-7.986e-5	1	295.75	2	NC	1
403		12	max	.021	3	.078	2	.053	5	5.274e-4	5	NC	5	NC	1
404			min	-.025	2	-.061	3	-.002	1	-7.365e-5	1	304.146	2	NC	1
405		13	max	.021	3	.068	2	.058	5	5.44e-4	5	NC	5	NC	1
406			min	-.025	2	-.053	3	-.002	1	-6.743e-5	1	322.178	2	NC	1
407		14	max	.02	3	.054	2	.062	4	5.606e-4	5	NC	5	NC	1
408			min	-.025	2	-.041	3	-.002	1	-6.122e-5	1	353.84	2	NC	1
409		15	max	.02	3	.035	2	.066	4	5.772e-4	5	NC	5	NC	1
410			min	-.025	2	-.027	3	-.002	1	-5.5e-5	1	407.887	2	NC	1
411		16	max	.02	3	.012	2	.07	4	8.251e-4	5	NC	5	NC	1
412			min	-.025	2	-.01	3	-.002	1	-5.275e-5	1	505.725	2	NC	1
413		17	max	.02	3	.01	3	.073	4	6.601e-3	4	NC	5	NC	1
414			min	-.025	2	-.016	2	-.002	1	-1.448e-4	1	715.763	2	NC	1
415		18	max	.02	3	.031	3	.076	4	3.387e-3	4	NC	4	NC	1
416			min	-.025	2	-.049	2	-.002	1	-7.396e-5	1	1389.66	2	NC	1
417		19	max	.02	3	.054	3	.078	4	3.197e-6	5	NC	1	NC	1
418			min	-.025	2	-.084	2	-.002	1	-3.761e-7	3	NC	1	NC	1
419	M9	1	max	.008	3	.025	3	.006	5	8.493e-3	3	NC	1	NC	1
420			min	-.008	2	-.023	2	-.004	1	-6.889e-3	1	NC	1	NC	1
421		2	max	.008	3	.014	3	.005	5	4.197e-3	3	NC	4	NC	1
422			min	-.008	2	-.013	2	0	1	-3.354e-3	1	4375.14	2	NC	1
423		3	max	.008	3	.004	3	.006	4	1.143e-4	1	NC	4	NC	1
424			min	-.008	2	-.003	2	0	3	-2.033e-5	3	2253.92	2	NC	1
425		4	max	.008	3	.005	2	.007	4	6.779e-5	1	NC	4	NC	1
426			min	-.008	2	-.004	3	-.001	3	-2.737e-5	3	1580.552	2	NC	1
427		5	max	.008	3	.013	2	.009	4	2.637e-5	2	NC	4	NC	1
428			min	-.008	2	-.011	3	-.002	3	-3.442e-5	3	1254.868	2	NC	1
429		6	max	.008	3	.019	2	.011	4	9.211e-6	2	NC	5	NC	1
430			min	-.008	2	-.017	3	-.002	3	-4.146e-5	3	1069.084	2	7603.449	4
431		7	max	.008	3	.024	2	.015	4	2.94e-6	10	NC	5	NC	1
432			min	-.008	2	-.021	3	-.003	3	-7.182e-5	1	954.85	2	5019.354	4
433		8	max	.008	3	.027	2	.018	4	-8.169e-7	10	NC	5	NC	1
434			min	-.008	2	-.024	3	-.003	3	-1.184e-4	1	883.616	2	3592.553	4
435		9	max	.008	3	.03	2	.022	5	-2.03e-6	15	NC	5	NC	1
436			min	-.008	2	-.026	3	-.003	3	-1.649e-4	1	841.925	2	2720.271	4
437		10	max	.008	3	.03	2	.027	5	-2.833e-7	15	NC	5	NC	1
438			min	-.008	2	-.026	3	-.004	3	-2.114e-4	1	823.391	2	2147.15	4
439		11	max	.008	3	.03	2	.033	5	1.829e-6	5	NC	5	NC	1
440			min	-.008	2	-.025	3	-.004	1	-2.58e-4	1	825.773	2	1749.859	4
441		12	max	.008	3	.028	2	.038	5	4.347e-6	5	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.008	2	-.023	3	-.006	1	-3.045e-4	1	850.119	2	1462.839	4
443		13	max	.008	3	.025	2	.044	5	6.864e-6	5	NC	5	NC	2
444			min	-.008	2	-.02	3	-.007	1	-3.51e-4	1	901.313	2	1241.581	5
445		14	max	.008	3	.019	2	.05	5	9.382e-6	5	NC	5	NC	2
446			min	-.008	2	-.016	3	-.008	1	-3.976e-4	1	990.507	2	1075.79	5
447		15	max	.008	3	.013	2	.055	5	1.19e-5	5	NC	5	NC	2
448			min	-.008	2	-.01	3	-.008	1	-4.441e-4	1	1142.064	2	948.703	5
449		16	max	.008	3	.005	2	.061	5	2.674e-4	5	NC	4	NC	2
450			min	-.008	2	-.004	3	-.008	1	-4.806e-4	1	1415.247	2	849.448	5
451		17	max	.008	3	.004	3	.067	5	6.543e-3	5	NC	4	NC	2
452			min	-.009	2	-.005	2	-.007	1	-2.784e-4	1	1997.144	2	770.186	4
453		18	max	.008	3	.012	3	.072	5	3.23e-3	5	NC	4	NC	1
454			min	-.009	2	-.017	2	-.005	1	-4.36e-3	2	3854.393	2	701.823	4
455		19	max	.008	3	.02	3	.078	4	4.015e-3	3	NC	1	NC	1
456			min	-.009	2	-.03	2	-.001	1	-8.729e-3	2	NC	1	645.642	4
457	M13	1	max	.004	1	.025	3	.008	3	4.167e-3	3	NC	1	NC	1
458			min	-.006	5	-.023	2	-.008	2	-3.961e-3	2	NC	1	NC	1
459		2	max	.004	1	.088	3	.012	1	4.961e-3	3	NC	4	NC	2
460			min	-.006	5	-.074	1	-.004	10	-4.708e-3	2	2194.81	3	8177.808	1
461		3	max	.004	1	.14	3	.033	1	5.755e-3	3	NC	5	NC	2
462			min	-.006	5	-.116	1	-.003	5	-5.455e-3	2	1199.358	3	3643.17	1
463		4	max	.004	1	.174	3	.049	1	6.55e-3	3	NC	5	NC	3
464			min	-.006	5	-.144	1	-.005	5	-6.203e-3	2	924.235	3	2531.292	1
465		5	max	.004	1	.187	3	.056	1	7.344e-3	3	NC	5	NC	3
466			min	-.006	5	-.155	1	-.006	5	-6.95e-3	2	851.103	3	2244.814	1
467		6	max	.004	1	.179	3	.052	1	8.138e-3	3	NC	5	NC	3
468			min	-.007	5	-.15	1	-.008	5	-7.698e-3	2	897.137	3	2437.497	1
469		7	max	.004	1	.154	3	.036	1	8.932e-3	3	NC	5	NC	2
470			min	-.007	5	-.13	1	-.009	5	-8.445e-3	2	1074.906	3	3367.305	1
471		8	max	.004	1	.119	3	.017	3	9.727e-3	3	NC	4	NC	2
472			min	-.007	5	-.103	1	-.011	2	-9.192e-3	2	1474.146	3	7340.951	1
473		9	max	.004	1	.086	3	.019	3	1.052e-2	3	NC	4	NC	1
474			min	-.007	5	-.077	1	-.021	2	-9.94e-3	2	2260.063	3	NC	1
475		10	max	.004	1	.071	3	.021	3	1.132e-2	3	NC	4	NC	1
476			min	-.007	5	-.065	2	-.025	2	-1.069e-2	2	2998.09	3	8280.897	2
477		11	max	.004	1	.086	3	.023	3	1.052e-2	3	NC	4	NC	1
478			min	-.007	5	-.077	1	-.021	2	-9.94e-3	2	2260.061	3	8868.128	3
479		12	max	.004	1	.119	3	.025	3	9.729e-3	3	NC	4	NC	2
480			min	-.007	5	-.103	1	-.011	2	-9.193e-3	2	1474.146	3	7238.16	1
481		13	max	.003	1	.154	3	.036	1	8.935e-3	3	NC	5	NC	2
482			min	-.007	5	-.13	1	-.007	10	-8.446e-3	2	1074.905	3	3351.072	1
483		14	max	.003	1	.179	3	.052	1	8.142e-3	3	NC	5	NC	5
484			min	-.007	5	-.15	1	-.004	10	-7.698e-3	2	897.137	3	2434.927	1
485		15	max	.003	1	.187	3	.056	1	7.349e-3	3	NC	5	NC	3
486			min	-.007	5	-.155	1	-.002	10	-6.951e-3	2	851.103	3	2248.509	1
487		16	max	.003	1	.175	3	.049	1	6.555e-3	3	NC	5	NC	3
488			min	-.007	5	-.144	1	-.002	5	-6.204e-3	2	924.234	3	2542.281	1
489		17	max	.003	1	.14	3	.033	1	5.762e-3	3	NC	5	NC	2
490			min	-.007	5	-.116	1	-.004	5	-5.457e-3	2	1199.358	3	3671.848	1
491		18	max	.003	1	.088	3	.012	1	4.969e-3	3	NC	4	NC	2
492			min	-.007	5	-.074	1	-.004	5	-4.71e-3	2	2194.809	3	8292.49	1
493		19	max	.003	1	.025	3	.008	3	4.175e-3	3	NC	1	NC	1
494			min	-.007	5	-.023	2	-.008	2	-3.962e-3	2	NC	1	NC	1
495	M16	1	max	.001	1	.02	3	.008	3	4.774e-3	2	NC	1	NC	1
496			min	-.078	4	-.03	2	-.009	2	-3.246e-3	3	NC	1	NC	1
497		2	max	.001	1	.05	3	.014	4	5.699e-3	2	NC	4	NC	2
498			min	-.078	4	-.094	2	-.004	10	-3.823e-3	3	2133.538	2	8188.751	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	.002	1	.075	3	.033	1	6.624e-3	2	NC	5	NC	2
500			min	-.078	4	-.148	2	-.002	10	-4.401e-3	3	1164.078	2	3647.571	1
501		4	max	.002	1	.092	3	.049	1	7.549e-3	2	NC	5	NC	3
502			min	-.078	4	-.184	2	-.002	10	-4.979e-3	3	894.577	2	2534.537	1
503		5	max	.002	1	.1	3	.056	1	8.474e-3	2	NC	5	NC	3
504			min	-.078	4	-.198	2	-.002	10	-5.556e-3	3	820.083	2	2248.293	1
505		6	max	.002	1	.098	3	.051	1	9.399e-3	2	NC	5	NC	5
506			min	-.078	4	-.19	2	-.004	10	-6.134e-3	3	858.048	2	2442.766	1
507		7	max	.002	1	.088	3	.036	1	1.032e-2	2	NC	5	NC	2
508			min	-.078	4	-.166	2	-.007	10	-6.712e-3	3	1015.002	2	3379.758	1
509		8	max	.002	1	.074	3	.023	3	1.125e-2	2	NC	5	NC	2
510			min	-.078	4	-.131	2	-.011	2	-7.289e-3	3	1359.715	2	7412.788	1
511		9	max	.002	1	.06	3	.022	3	1.217e-2	2	NC	4	NC	1
512			min	-.078	4	-.099	2	-.021	2	-7.867e-3	3	1998.807	2	9709.524	3
513		10	max	.002	1	.054	3	.02	3	1.31e-2	2	NC	4	NC	1
514			min	-.078	4	-.084	2	-.025	2	-8.445e-3	3	2554.793	2	8276.096	2
515		11	max	.002	1	.06	3	.019	3	1.217e-2	2	NC	4	NC	1
516			min	-.078	4	-.099	2	-.021	2	-7.866e-3	3	1998.807	2	NC	1
517		12	max	.002	1	.074	3	.019	3	1.125e-2	2	NC	5	NC	2
518			min	-.078	4	-.131	2	-.011	2	-7.287e-3	3	1359.715	2	7352.92	1
519		13	max	.002	1	.088	3	.036	1	1.032e-2	2	NC	5	NC	2
520			min	-.078	4	-.166	2	-.007	10	-6.709e-3	3	1015.002	2	3375.409	1
521		14	max	.002	1	.098	3	.051	1	9.4e-3	2	NC	5	NC	3
522			min	-.078	4	-.19	2	-.004	10	-6.13e-3	3	858.048	2	2447.082	1
523		15	max	.002	1	.099	3	.056	1	8.475e-3	2	NC	5	NC	3
524			min	-.078	4	-.198	2	-.002	5	-5.552e-3	3	820.083	2	2257.773	1
525		16	max	.002	1	.092	3	.049	1	7.55e-3	2	NC	5	NC	3
526			min	-.078	4	-.184	2	-.005	5	-4.973e-3	3	894.577	2	2552.078	1
527		17	max	.002	1	.075	3	.032	1	6.625e-3	2	NC	5	NC	2
528			min	-.078	4	-.148	2	-.007	5	-4.395e-3	3	1164.078	2	3686.719	1
529		18	max	.002	1	.05	3	.011	1	5.701e-3	2	NC	4	NC	2
530			min	-.078	4	-.094	2	-.005	5	-3.816e-3	3	2133.538	2	8333.542	1
531		19	max	.002	1	.02	3	.008	3	4.776e-3	2	NC	1	NC	1
532			min	-.078	4	-.03	2	-.009	2	-3.238e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	3.693e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-5.601e-4	5	NC	1	NC	1
535		2	max	0	3	0	15	.007	4	8.232e-4	3	NC	1	NC	1
536			min	0	5	-.006	1	0	3	-5.805e-4	5	NC	1	NC	1
537		3	max	0	3	0	15	.014	4	1.277e-3	3	NC	5	NC	1
538			min	-.001	5	-.012	1	-.003	3	-1.021e-3	2	6575.021	2	5374.339	4
539		4	max	0	3	0	15	.022	4	1.731e-3	3	NC	5	NC	9
540			min	-.002	5	-.018	1	-.006	3	-1.49e-3	2	4510.848	2	3466.932	4
541		5	max	0	3	0	15	.03	4	2.185e-3	3	NC	5	NC	9
542			min	-.003	5	-.023	1	-.011	3	-1.959e-3	2	3519.861	2	2601.877	4
543		6	max	0	3	0	15	.036	4	2.639e-3	3	NC	5	9094.413	9
544			min	-.003	5	-.027	1	-.015	3	-2.428e-3	2	2962.335	2	2144.227	4
545		7	max	0	3	0	15	.041	4	3.092e-3	3	NC	5	7162.601	9
546			min	-.004	5	-.03	1	-.02	3	-2.897e-3	2	2627.057	2	1890.947	4
547		8	max	0	3	0	15	.044	4	3.546e-3	3	NC	5	5939.599	9
548			min	-.005	5	-.033	1	-.025	3	-3.367e-3	2	2425.839	2	1761.36	4
549		9	max	0	3	.001	15	.045	4	4.e-3	3	NC	5	5135.701	9
550			min	-.005	5	-.035	1	-.029	3	-3.836e-3	2	2317.532	2	1721.774	4
551		10	max	0	3	.001	5	.044	4	4.454e-3	3	NC	5	4604.241	9
552			min	-.006	5	-.035	1	-.033	3	-4.305e-3	2	2283.269	2	1730.392	3
553		11	max	0	3	.002	5	.041	4	4.908e-3	3	NC	5	4267.96	9
554			min	-.006	5	-.035	1	-.035	3	-4.774e-3	2	2317.532	2	1598.744	3
555		12	max	0	3	.002	5	.036	4	5.362e-3	3	NC	5	4088.816	9

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.007	5	-.033	1	-.036	3	-5.244e-3	2	2425.839	2	1527.406	3
557		13	max	0	3	.003	5	.034	1	5.816e-3	3	NC	5	4859.776	15
558			min	-.008	5	-.031	1	-.035	3	-5.713e-3	2	2627.057	2	1511.85	3
559		14	max	0	3	.003	5	.031	1	6.269e-3	3	NC	5	6816.109	15
560			min	-.008	5	-.028	1	-.032	3	-6.182e-3	2	2962.335	2	1558.614	3
561		15	max	.001	3	.003	5	.026	1	6.723e-3	3	NC	5	NC	15
562			min	-.009	5	-.024	1	-.027	3	-6.651e-3	2	3519.861	2	1691.862	3
563		16	max	.001	3	.004	5	.019	1	7.177e-3	3	NC	5	NC	5
564			min	-.01	5	-.019	1	-.018	3	-7.121e-3	2	4510.848	2	1977.286	3
565		17	max	.001	3	.004	5	.009	1	7.631e-3	3	NC	5	NC	4
566			min	-.01	5	-.014	1	-.007	3	-7.59e-3	2	6575.021	2	2621.035	3
567		18	max	.001	3	.005	5	.007	3	8.085e-3	3	NC	1	NC	4
568			min	-.011	5	-.008	1	-.01	2	-8.059e-3	2	NC	1	4666.018	3
569		19	max	.001	3	.006	5	.025	3	8.539e-3	3	NC	1	NC	1
570			min	-.012	5	-.002	9	-.027	2	-8.528e-3	2	NC	1	NC	1
571	M16A	1	max	0	10	0	10	.009	3	2.97e-3	3	NC	1	NC	1
572			min	-.004	4	-.003	4	-.009	2	-2.981e-3	2	NC	1	NC	1
573		2	max	0	10	-.003	12	.002	9	2.842e-3	3	NC	1	NC	1
574			min	-.004	4	-.014	4	-.003	5	-2.842e-3	2	7556.517	4	NC	1
575		3	max	0	10	-.006	12	.008	1	2.715e-3	3	NC	12	NC	4
576			min	-.004	4	-.023	4	-.007	5	-2.703e-3	2	3845.253	4	5836.426	1
577		4	max	0	10	-.009	12	.013	1	2.587e-3	3	9021.697	12	NC	10
578			min	-.004	4	-.032	4	-.014	5	-2.564e-3	2	2638.068	4	4428.676	1
579		5	max	0	10	-.011	12	.016	1	2.46e-3	3	7039.721	12	NC	14
580			min	-.003	4	-.041	4	-.022	5	-2.424e-3	2	2058.512	4	3805.422	5
581		6	max	0	10	-.013	12	.018	1	2.332e-3	3	5924.67	12	NC	14
582			min	-.003	4	-.048	4	-.03	5	-2.285e-3	2	1732.455	4	2730.139	5
583		7	max	0	10	-.015	12	.018	1	2.205e-3	3	5254.113	12	8983.405	10
584			min	-.003	4	-.053	4	-.037	5	-2.146e-3	2	1536.375	4	2158.012	5
585		8	max	0	10	-.016	12	.018	1	2.077e-3	3	4851.678	12	9236.15	10
586			min	-.003	4	-.057	4	-.044	5	-2.007e-3	2	1418.698	4	1830.409	5
587		9	max	0	10	-.017	12	.017	1	1.949e-3	3	4635.064	12	9872.426	10
588			min	-.002	4	-.059	4	-.048	5	-1.868e-3	2	1355.357	4	1642.008	5
589		10	max	0	10	-.017	12	.016	1	1.822e-3	3	4566.538	12	NC	10
590			min	-.002	4	-.06	4	-.051	5	-1.729e-3	2	1335.319	4	1545.444	5
591		11	max	0	10	-.017	12	.014	1	1.694e-3	3	4635.064	12	NC	10
592			min	-.002	4	-.059	4	-.052	5	-1.59e-3	2	1355.357	4	1520.21	5
593		12	max	0	10	-.016	12	.012	1	1.567e-3	3	4851.678	12	NC	9
594			min	-.002	4	-.056	4	-.051	5	-1.451e-3	2	1418.698	4	1561.881	5
595		13	max	0	10	-.015	12	.009	1	1.439e-3	3	5254.113	12	NC	9
596			min	-.001	4	-.052	4	-.047	5	-1.311e-3	2	1536.375	4	1680.299	5
597		14	max	0	10	-.013	12	.007	1	1.311e-3	3	5924.67	12	NC	2
598			min	-.001	4	-.046	4	-.041	5	-1.172e-3	2	1732.455	4	1905.268	5
599		15	max	0	10	-.011	12	.004	1	1.184e-3	3	7039.721	12	NC	1
600			min	0	4	-.039	4	-.034	5	-1.033e-3	2	2058.512	4	2306.484	5
601		16	max	0	10	-.009	12	.002	1	1.056e-3	3	9021.697	12	NC	1
602			min	0	4	-.03	4	-.026	5	-8.941e-4	2	2638.068	4	3057.614	5
603		17	max	0	10	-.006	12	0	9	9.287e-4	3	NC	12	NC	1
604			min	0	4	-.021	4	-.017	5	-7.55e-4	2	3845.253	4	4697.957	5
605		18	max	0	10	-.003	12	0	9	8.702e-4	4	NC	1	NC	1
606			min	0	4	-.011	4	-.008	5	-6.159e-4	2	7556.517	4	9980.006	5
607		19	max	0	1	0	1	0	1	9.418e-4	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-4.767e-4	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

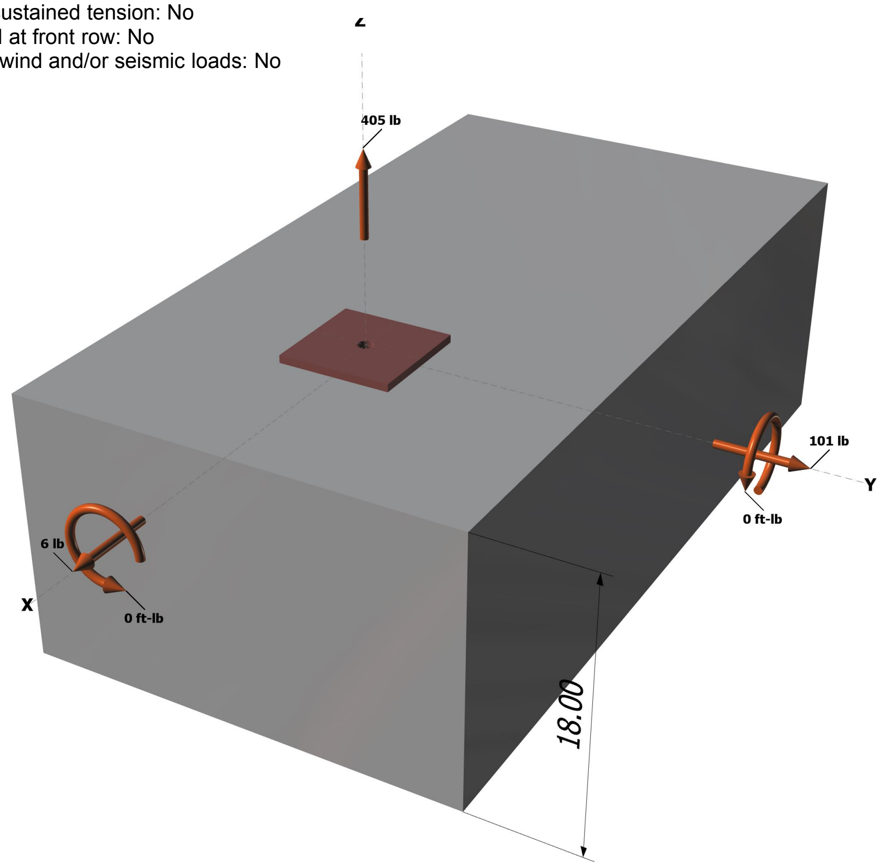
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

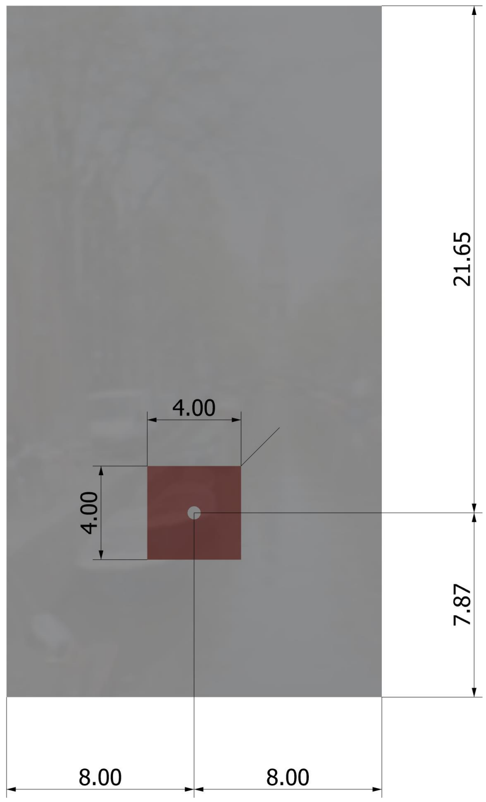
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>



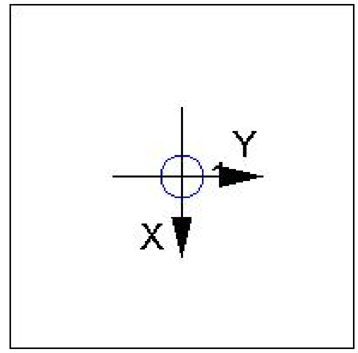
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\, (A_{Nc} / A_{Nco})\, \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\, (A_{Na} / A_{Na0})\, \Psi_{ed,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi (A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi (A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\ (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\ (2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi \min|k_{cp}N_a\ ;\ k_{cp}N_{cb}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

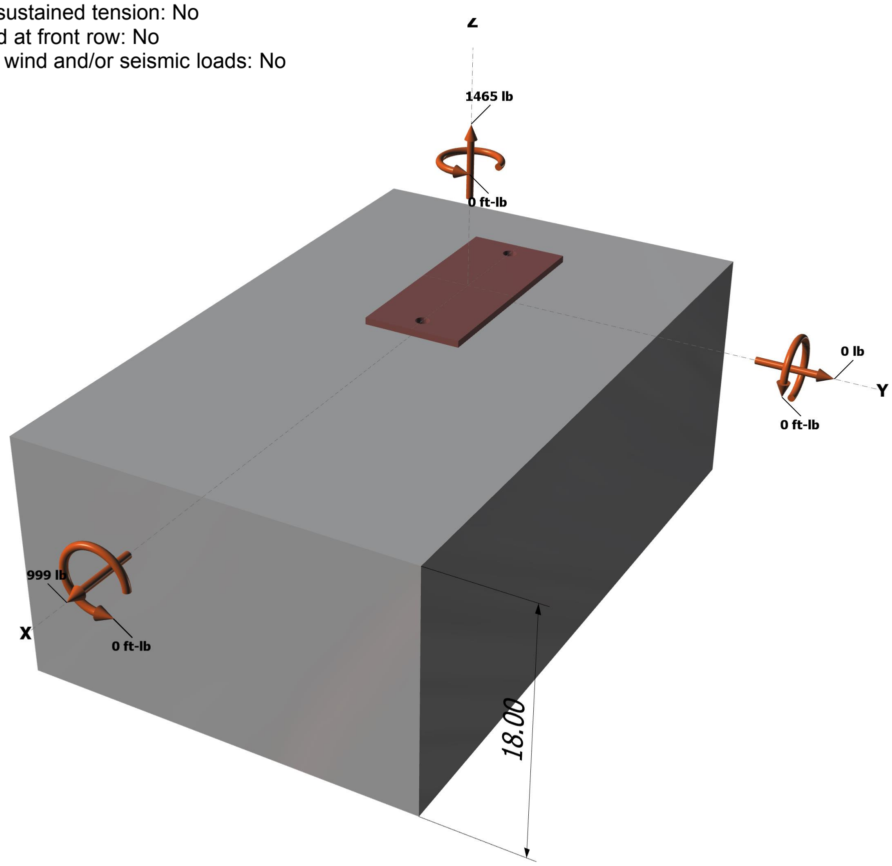
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

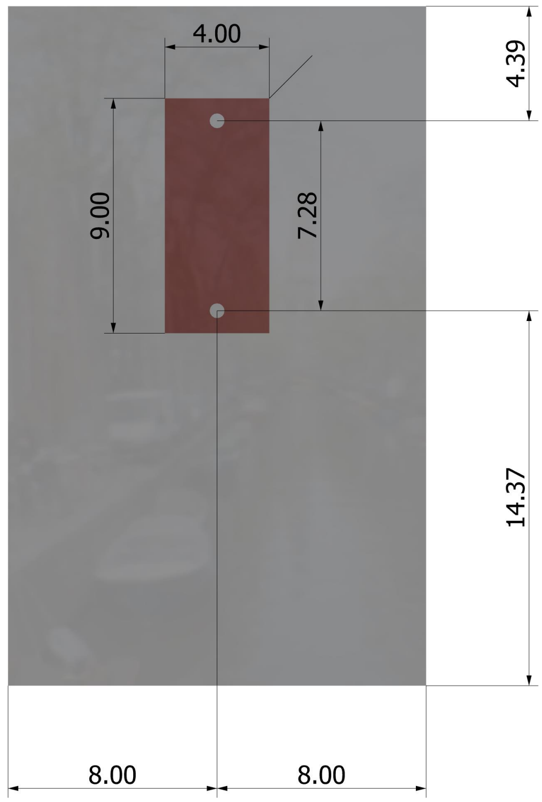
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>



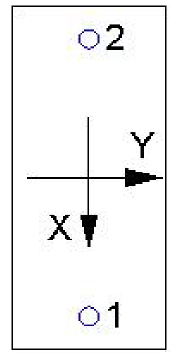
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\, (A_{Nc} / A_{Nco})\, \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\, (A_{Na} / A_{Na0})\, \Psi_{ed,Na} \Psi_{g,Na} \Psi_{ec,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.