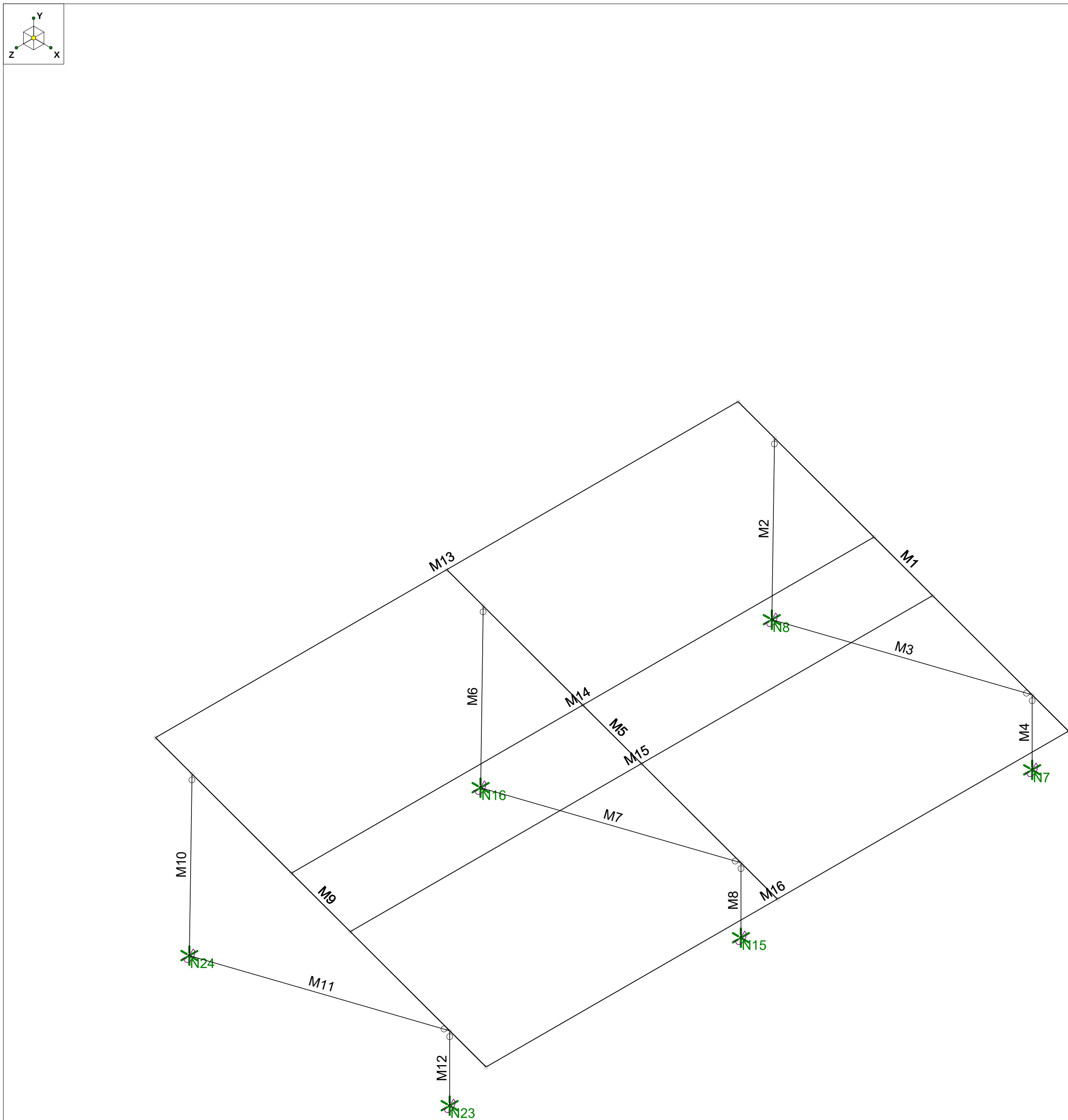


Schletter, Inc.		20° Tilt w/ Seismic Design
HCV	Standard PVMax Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

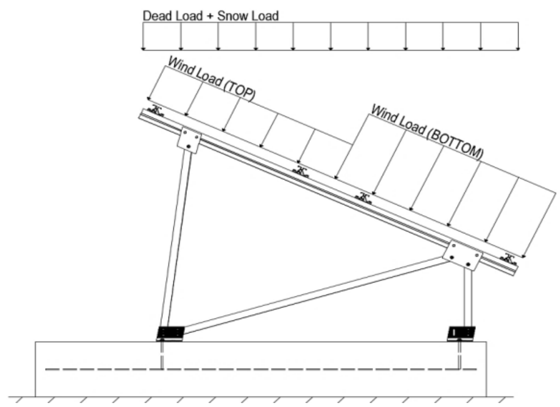
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	2000 mm	Height =	1900 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 2
Module Tilt = 20°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 20.62 psf *(ASCE 7-05, Eq. 7-2)*
I_s = 1.00
C_s = 0.91
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 120 mph
Height < 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 22.61 psf *Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.050	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.650	
$Cf-_{TOP, OUTER PURLIN}$	=	-2.400	
$Cf-_{TOP, INNER PURLIN}$	=	-1.840	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.000	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.06	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W
1.2D + 1.6W + 0.5S
0.9D + 1.6W ^{M}
1.54D + 1.3E + 0.2S ^{R}
0.56D + 1.3E ^{R}
1.54D + 1.25E + 0.2S ^{O}
0.56D + 1.25E ^{O}

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 1.0W
1.0D + 0.75L + 0.75W + 0.75S
0.6D + 1.0W ^{M}
1.238D + 0.875E ^{O}
1.1785D + 0.65625E + 0.75S ^{O}
0.362D + 0.875E ^{O}

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

^{M} *Uses the minimum allowable module dead load.*
^{R} *Include redundancy factor of 1.3.*
^{O} *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	Diagonal Struts	Location	Front Reactions	Location
M13	Top	M3	Outer	N7	Outer
M14	Mid-Top	M7	Inner	N15	Inner
M15	Mid-Bottom	M11	Outer	N23	Outer
M16	Bottom				

Girders	Location	Rear Struts	Location	Rear Reactions	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

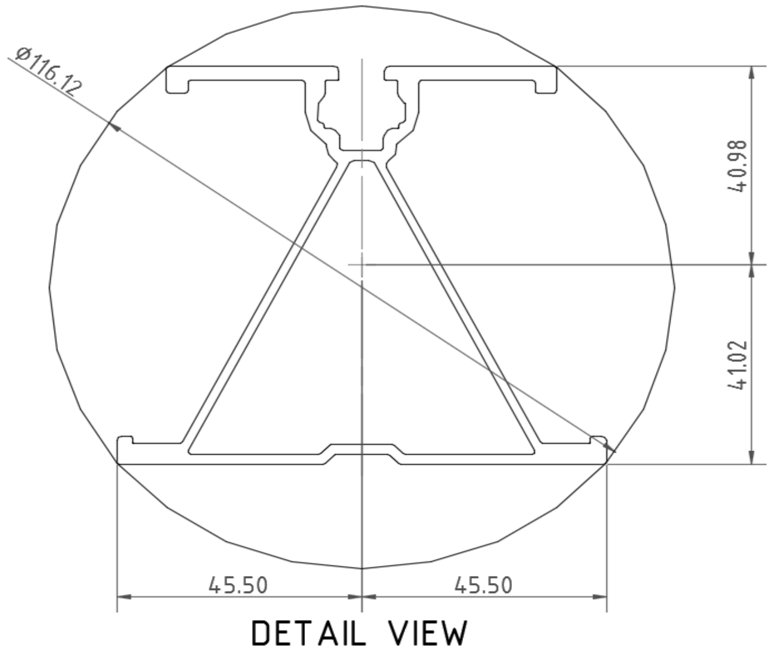
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

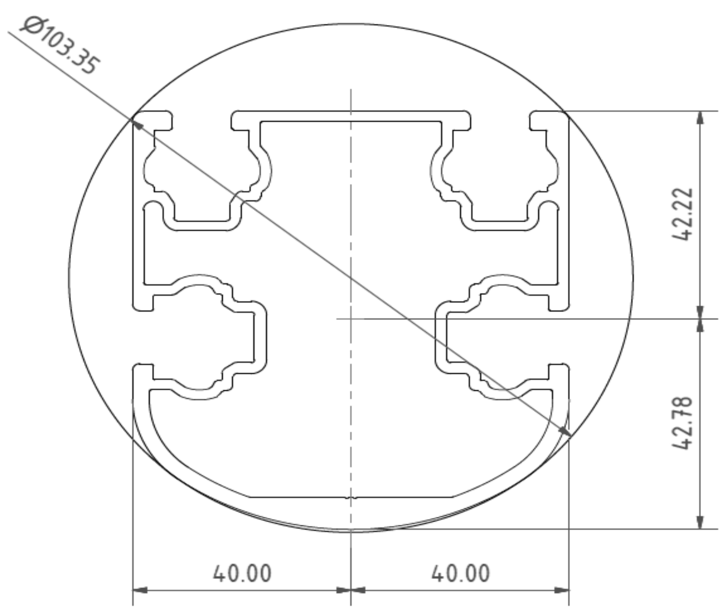
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	87	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.424	k-ft
M_z =	0.195	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	68%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

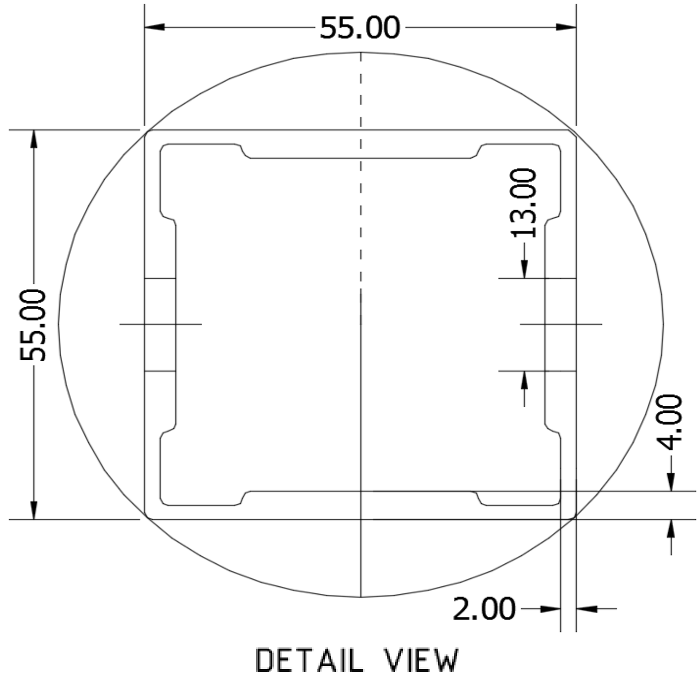
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	104.56	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.00	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-3.380	k-ft
M_z =	0.000	k-ft
P_n =	-0.819	k
$M_{y\ allowable}$ =	3.422	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	100%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

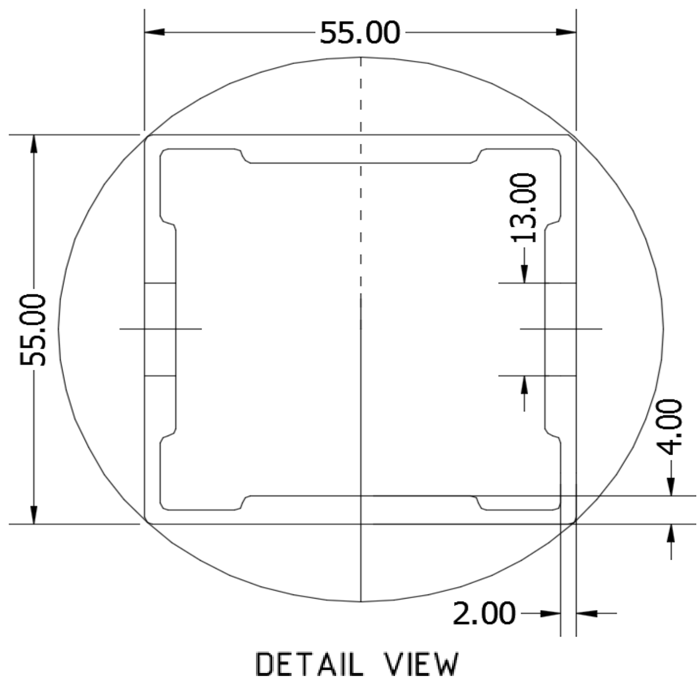
Strut Type =	55x55	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	24.80	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.446	k-ft
P_n =	0.536	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	34%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

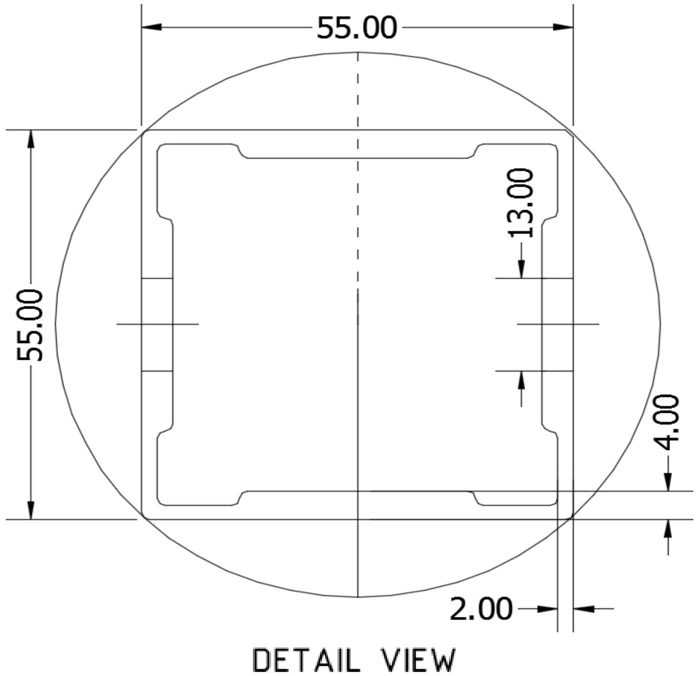
Strut Type =	55x55	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	98.03	in
$\Phi F_{ty\ AXIAL}$ =	6.11	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.013	k-ft
M_z =	0.000	k-ft
P_n =	1.987	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	6.000	k
Utilization =	34%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.10	in
$\Phi F_{ty\ AXIAL}$ =	13.63	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.013	k-ft
M_z =	0.000	k-ft
P_n =	3.276	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.386	k
Utilization =	25%	



5. FOUNDATION DESIGN CALCULATIONS

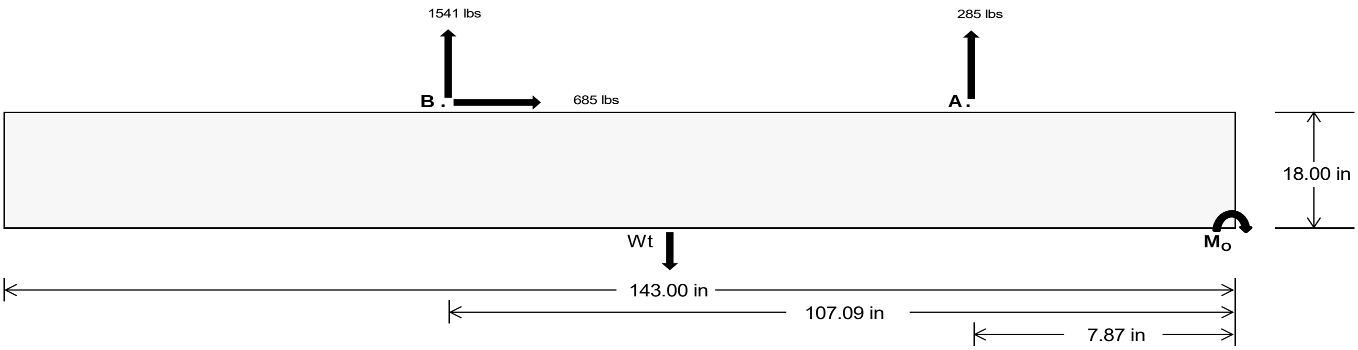
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	1197.69	6419.39	k
Compressive Load =	4070.39	4894.76	k
Lateral Load =	296.88	2848.59	k
Moment (Weak Axis) =	0.60	0.31	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC tables 1804.2 (2003, 2006) & 1806.2 (2009).



Concrete Properties

Weight of Concrete = 145 pcf
Compressive Strength = 2500 psi
Yield Strength = 60000 psi

Footing Reinforcement

Use fiber reinforcing with (2) #5 rebar.

Overturning Check

M_O = 179599.9 in-lbs
Resisting Force Required = 2511.89 lbs
S.F. = 1.67
Weight Required = 4186.48 lbs
Minimum Width = 35 in in
Weight Provided = 7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.

Sliding

Force = 684.91 lbs
Friction = 0.4
Weight Required = 1712.29 lbs
Resisting Weight = 7559.64 lbs
Additional Weight Required = 0 lbs

Use a 143in long x 35in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion

Sliding Force = 684.91 lbs
Cohesion = 130 psf
Area = 34.76 ft^2
Resisting = 3779.82 lbs
Additional Weight Required = 0 lbs

Use a 143in long x 35in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key

Additional Force = 0 lbs
Lateral Bearing Pressure = 200 psf/ft
Required Depth = 0.00 ft
f'_c = 2500 psi
Length = 8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	35 in	36 in	37 in	38 in
P_{ftg} = (145 pcf)(11.92 ft)(1.5 ft)(2.92 ft) =	7560 lbs	7776 lbs	7992 lbs	8208 lbs

ASD LC	1.0D + 1.0S				1.0D + 1.0W				1.0D + 0.75L + 0.75W + 0.75S				0.6D + 1.0W			
Width	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in
F_A	1270 lbs	1270 lbs	1270 lbs	1270 lbs	1679 lbs	1679 lbs	1679 lbs	1679 lbs	2106 lbs	2106 lbs	2106 lbs	2106 lbs	-571 lbs	-571 lbs	-571 lbs	-571 lbs
F_B	1353 lbs	1353 lbs	1353 lbs	1353 lbs	2055 lbs	2055 lbs	2055 lbs	2055 lbs	2445 lbs	2445 lbs	2445 lbs	2445 lbs	-3082 lbs	-3082 lbs	-3082 lbs	-3082 lbs
F_V	121 lbs	121 lbs	121 lbs	121 lbs	1209 lbs	1209 lbs	1209 lbs	1209 lbs	988 lbs	988 lbs	988 lbs	988 lbs	-1370 lbs	-1370 lbs	-1370 lbs	-1370 lbs
P_{total}	10183 lbs	10399 lbs	10615 lbs	10831 lbs	11293 lbs	11509 lbs	11725 lbs	11941 lbs	12110 lbs	12326 lbs	12542 lbs	12758 lbs	883 lbs	1012 lbs	1142 lbs	1272 lbs
M	2902 lbs-ft	2902 lbs-ft	2902 lbs-ft	2902 lbs-ft	4621 lbs-ft	4621 lbs-ft	4621 lbs-ft	4621 lbs-ft	5399 lbs-ft	5399 lbs-ft	5399 lbs-ft	5399 lbs-ft	4058 lbs-ft	4058 lbs-ft	4058 lbs-ft	4058 lbs-ft
e	0.28 ft	0.28 ft	0.27 ft	0.27 ft	0.41 ft	0.40 ft	0.39 ft	0.39 ft	0.45 ft	0.44 ft	0.43 ft	0.42 ft	4.60 ft	4.01 ft	3.55 ft	3.19 ft
L/6	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft
f_{min}	250.9 psf	250.0 psf	249.1 psf	248.3 psf	258.0 psf	256.9 psf	255.8 psf	254.8 psf	270.2 psf	268.8 psf	267.4 psf	266.1 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	335.0 psf	331.7 psf	328.7 psf	325.7 psf	391.9 psf	387.0 psf	382.4 psf	378.1 psf	426.6 psf	420.8 psf	415.3 psf	410.1 psf	148.2 psf	115.4 psf	102.7 psf	96.8 psf

Maximum Bearing Pressure = 427 psf
Allowable Bearing Pressure = 1500 psf

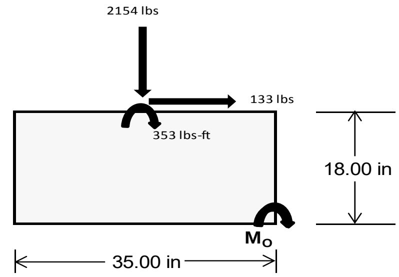
Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 2588.6 ft-lbs
Resisting Force Required = 1775.04 lbs
S.F. = 1.67
Weight Required = 2958.41 lbs
Minimum Width = 35 in in
Weight Provided = 7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	35 in			35 in			35 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	257 lbs	539 lbs	185 lbs	800 lbs	2154 lbs	745 lbs	100 lbs	158 lbs	29 lbs
F_V	185 lbs	181 lbs	188 lbs	137 lbs	133 lbs	145 lbs	186 lbs	182 lbs	186 lbs
P_{total}	9616 lbs	9898 lbs	9544 lbs	9709 lbs	11063 lbs	9654 lbs	2837 lbs	2894 lbs	2766 lbs
M	740 lbs-ft	730 lbs-ft	747 lbs-ft	557 lbs-ft	553 lbs-ft	582 lbs-ft	739 lbs-ft	728 lbs-ft	742 lbs-ft
e	0.08 ft	0.07 ft	0.08 ft	0.06 ft	0.05 ft	0.06 ft	0.26 ft	0.25 ft	0.27 ft
L/6	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft
f_{min}	232.8 psf	241.6 psf	230.4 psf	246.4 psf	285.6 psf	243.3 psf	37.9 psf	40.2 psf	35.7 psf
f_{max}	320.5 psf	328.0 psf	318.8 psf	312.3 psf	351.0 psf	312.2 psf	125.4 psf	126.4 psf	123.5 psf

Maximum Bearing Pressure = 351 psf
Allowable Bearing Pressure = 1500 psf

Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 143in long x 34in wide x 18in tall ballast foundation and fiber reinforcing with (2) #5 rebar.

5.3 Foundation Anchors

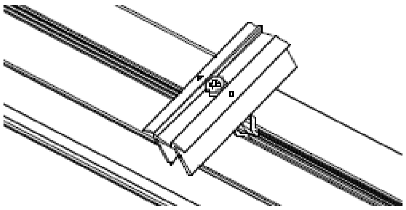
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

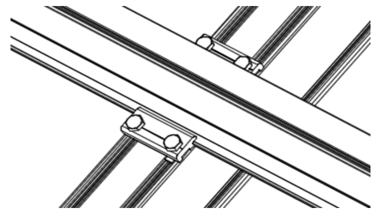
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.963	k
Allowable Uplift =	1.214	k
Utilization =	79%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	2.493	k
Allowable Uplift =	4.357	k
Utilization =	57%	



6.2 Strut Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	3.131	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	42%	

Rear Strut		
Maximum Axial Load =	4.420	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	60%	

Diagonal Strut		
Maximum Axial Load =	2.183	k
M12 Bolt Shear Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	29%	

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

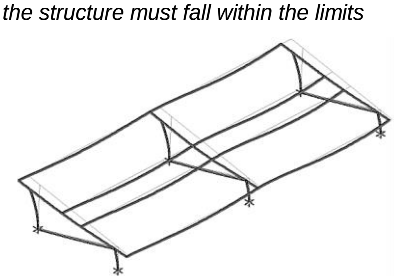
Mean Height, h_{sx} = 51.89 in

Allowable Story Drift for All Other Structures, Δ = { $0.020h_{sx}$; 1.038 in

Max Drift, Δ_{MAX} = 0.531 in

$0.531 \leq 1.038$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 87 in

J = 0.432

240.683

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.3 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

$\varphi F_L St$= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

$M_{max}St$ = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 87

J = 0.432

153.06

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

$M_{max}Wk$ = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:
3.4.14

L_b = 104.56 in
J = 1.08
179.85

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.0 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

Weak Axis:
3.4.14

L_b = 104.56
J = 1.08
190.335

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 28.9

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Used

Rb/t = 18.1

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 31.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 35.2

m = 0.68

C_0 = 41.067

Cc = 43.717

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 73.8

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.0 ksi

Ix = 984962 mm^4

2.366 in^4

y = 43.717 mm

Sx = 1.375 in^3

M_{max}St = 3.323 k-ft

3.4.18

h/t = 16.2

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40

Cc = 40

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 923544 mm^4

2.219 in^4

x = 40 mm

Sy = 1.409 in^3

M_{max}Wk = 3.904 k-ft

Compression

3.4.9

b/t = 16.2

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

b/t = 7.4

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 31.09 ksi

φF_L= 31.09 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.87952

φF_L= φcc(Bc-Dc*λ)

φF_L= 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 98.03 in

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4 ksi

Weak Axis:

3.4.14

L_b = 98.03

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 2.26776

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.89749

φF_L= (φccFcy)/(λ²)

φF_L= 6.10803 ksi

3.4.9

b/t = 24.5
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

b/t = 24.5
S1 = 12.21
S2 = 32.70
$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
$\varphi F_L = \varphi yFcy$
$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 6.11 ksi
A = 663.99 mm^2
1.03 in^2
$P_{max} =$ 6.29 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **<u>55x55</u>**

<u>Strong Axis:</u>

3.4.14

$L_b =$ 61.10 in
J = 0.942
95.3524

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)/2}))}]$
$\varphi F_L =$ 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

<u>Weak Axis:</u>

3.4.14

$L_b =$ 61.1
J = 0.942
95.3524

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)/2}))}]$
$\varphi F_L =$ 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.41345

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.77788

φF_L= (φccFcy)/(λ²)

φF_L= 13.6277 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt} \right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 13.63 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 14.03 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-9.843	-9.843	0	0
2	M14	Y	-9.843	-9.843	0	0
3	M15	Y	-9.843	-9.843	0	0
4	M16	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-5.454	-5.454	0	0
2	M14	Y	-5.454	-5.454	0	0
3	M15	Y	-5.454	-5.454	0	0
4	M16	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-63.565	-63.565	0	0
2	M14	Y	-63.565	-63.565	0	0
3	M15	Y	-63.565	-63.565	0	0
4	M16	Y	-63.565	-63.565	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-77.887	-77.887	0	0
2	M14	y	-77.887	-77.887	0	0
3	M15	y	-122.393	-122.393	0	0
4	M16	y	-122.393	-122.393	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	178.027	178.027	0	0
2	M14	y	136.487	136.487	0	0
3	M15	y	74.178	74.178	0	0
4	M16	y	74.178	74.178	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	7.874	7.874	0	0
2	M14	Z	7.874	7.874	0	0
3	M15	Z	7.874	7.874	0	0
4	M16	Z	7.874	7.874	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8														
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6														
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	600.548	2	1249.079	2	.592	1	.003	1	0	1	0	1
2		min	-740.311	3	-1596.142	3	-52.579	5	-.239	4	0	1	0	1
3	N7	max	.02	9	1127.577	1	-.55	12	-.001	12	0	1	0	1
4		min	-.233	2	-277.88	3	-228.367	4	-.46	4	0	1	0	1
5	N15	max	0	15	3131.066	2	0	3	0	3	0	1	0	1
6		min	-2.305	2	-921.297	3	-218.088	4	-.446	4	0	1	0	1
7	N16	max	1980.066	2	3765.197	2	0	1	0	1	0	1	0	1
8		min	-2191.222	3	-4937.989	3	-52.67	5	-.242	4	0	1	0	1
9	N23	max	.03	14	1127.577	1	7.59	1	.016	1	0	1	0	1
10		min	-.233	2	-277.88	3	-222.923	4	-.452	4	0	1	0	1
11	N24	max	600.548	2	1249.079	2	-.045	10	0	10	0	1	0	1
12		min	-740.311	3	-1596.142	3	-53.147	5	-.241	4	0	1	0	1
13	Totals:	max	3178.39	2	11526.266	2	0	2						
14		min	-3672.812	3	-9607.33	3	-823.585	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	61.091	4	452.571	1	-6.764	12	0	15	.131	1	0	4
2			min	3.166	10	-763.966	3	-133.888	1	-.014	2	.009	10	0	3
3		2	max	51.585	4	315.083	1	-5.613	12	0	15	.083	4	.525	3
4			min	3.166	10	-539.25	3	-102.115	1	-.014	2	0	10	-.309	1
5		3	max	46.984	1	177.594	1	-4.463	12	0	15	.051	5	.869	3
6			min	3.166	10	-314.533	3	-70.343	1	-.014	2	-.034	1	-.508	1
7		4	max	46.984	1	40.105	1	-2.579	10	0	15	.029	5	1.032	3
8			min	3.166	10	-89.816	3	-38.57	1	-.014	2	-.078	1	-.595	1
9		5	max	46.984	1	134.9	3	.547	10	0	15	.009	5	1.013	3
10			min	3.166	10	-97.404	2	-26.257	4	-.014	2	-.096	1	-.572	1
11		6	max	46.984	1	359.617	3	24.975	1	0	15	-.004	12	.814	3
12			min	2.097	15	-234.872	1	-22.421	5	-.014	2	-.089	1	-.438	1
13		7	max	46.984	1	584.333	3	56.748	1	0	15	-.004	10	.434	3
14			min	-6.27	5	-372.36	1	-20.671	5	-.014	2	-.056	1	-.194	1
15		8	max	46.984	1	809.05	3	88.521	1	0	15	.005	2	.169	2
16			min	-15.776	5	-509.849	1	-18.92	5	-.014	2	-.044	4	-.127	3
17		9	max	46.984	1	1033.767	3	120.294	1	0	15	.087	1	.628	2
18			min	-25.282	5	-647.338	1	-17.169	5	-.014	2	-.058	5	-.869	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	49.638	4	1258.483	3	152.066	1	.004	12	.197	1	1.204	1
20			min	3.166	10	-784.826	1	-92.439	14	-.014	2	-.001	3	-1.793	3
21		11	max	46.984	1	647.338	1	-2.438	12	.014	2	.087	1	.628	2
22			min	3.166	10	-1033.767	3	-120.294	1	0	15	-.005	3	-.869	3
23		12	max	46.984	1	509.849	1	-1.288	12	.014	2	.044	4	.169	2
24			min	3.166	10	-809.05	3	-88.521	1	0	15	-.007	3	-.127	3
25		13	max	46.984	1	372.36	1	-.024	3	.014	2	.021	5	.434	3
26			min	3.166	10	-584.333	3	-56.748	1	0	15	-.056	1	-.194	1
27		14	max	46.984	1	234.872	1	1.701	3	.014	2	0	15	.814	3
28			min	1.298	15	-359.617	3	-30.458	4	0	15	-.089	1	-.438	1
29		15	max	46.984	1	97.404	2	6.797	1	.014	2	-.003	12	1.013	3
30			min	-7.52	5	-134.9	3	-23.306	5	0	15	-.096	1	-.572	1
31		16	max	46.984	1	89.816	3	38.57	1	.014	2	0	12	1.032	3
32			min	-17.026	5	-40.105	1	-21.555	5	0	15	-.078	1	-.595	1
33		17	max	46.984	1	314.533	3	70.343	1	.014	2	.004	3	.869	3
34			min	-26.532	5	-177.594	1	-19.804	5	0	15	-.062	4	-.508	1
35		18	max	46.984	1	539.25	3	102.115	1	.014	2	.036	1	.525	3
36			min	-36.037	5	-315.083	1	-18.053	5	0	15	-.07	5	-.309	1
37		19	max	46.984	1	763.966	3	133.888	1	.014	2	.131	1	0	1
38			min	-45.543	5	-452.571	1	-16.303	5	0	15	-.083	5	0	3
39	M14	1	max	41.212	4	532.424	1	-7.042	12	.015	3	.189	4	0	1
40			min	2.166	12	-631.848	3	-140.004	1	-.016	2	.011	10	0	3
41		2	max	31.706	4	394.936	1	-5.892	12	.015	3	.131	4	.44	3
42			min	2.166	12	-460.671	3	-108.231	1	-.016	2	.002	10	-.374	1
43		3	max	31.336	1	257.974	2	-4.741	12	.015	3	.08	5	.742	3
44			min	2.166	12	-289.495	3	-76.459	1	-.016	2	-.014	1	-.636	1
45		4	max	31.336	1	123.221	2	-3.109	10	.015	3	.046	5	.906	3
46			min	2.166	12	-118.319	3	-51.947	4	-.016	2	-.063	1	-.788	1
47		5	max	31.336	1	52.857	3	.018	10	.015	3	.013	5	.933	3
48			min	-3.351	5	-17.53	1	-43.629	4	-.016	2	-.086	1	-.831	2
49		6	max	31.336	1	224.033	3	18.859	1	.015	3	-.004	12	.821	3
50			min	-12.857	5	-155.019	1	-38.185	5	-.016	2	-.084	1	-.768	2
51		7	max	31.336	1	395.209	3	50.632	1	.015	3	-.004	10	.572	3
52			min	-22.363	5	-292.507	1	-36.435	5	-.016	2	-.062	4	-.596	2
53		8	max	31.336	1	566.385	3	82.405	1	.015	3	.003	2	.185	3
54			min	-31.869	5	-429.996	1	-34.684	5	-.016	2	-.08	4	-.315	2
55		9	max	31.336	1	737.562	3	114.177	1	.015	3	.077	1	.113	1
56			min	-41.375	5	-567.484	1	-32.933	5	-.016	2	-.105	5	-.341	3
57		10	max	60.734	4	908.738	3	145.95	1	.015	3	.19	4	.625	1
58			min	2.166	12	-704.973	1	-97.329	14	-.016	2	-.002	3	-1.004	3
59		11	max	51.228	4	567.484	1	-2.16	12	.016	2	.13	4	.113	1
60			min	2.166	12	-737.562	3	-114.177	1	-.015	3	-.005	3	-.341	3
61		12	max	41.723	4	429.996	1	-1.01	12	.016	2	.078	4	.185	3
62			min	2.166	12	-566.385	3	-82.405	1	-.015	3	-.007	3	-.315	2
63		13	max	32.217	4	292.507	1	.398	3	.016	2	.043	5	.572	3
64			min	2.166	12	-395.209	3	-52.917	4	-.015	3	-.056	1	-.596	2
65		14	max	31.336	1	155.019	1	2.124	3	.016	2	.01	5	.821	3
66			min	2.166	12	-224.033	3	-44.6	4	-.015	3	-.084	1	-.768	2
67		15	max	31.336	1	17.53	1	12.913	1	.016	2	-.002	12	.933	3
68			min	2.166	12	-52.857	3	-38.391	5	-.015	3	-.086	1	-.831	2
69		16	max	31.336	1	118.319	3	44.686	1	.016	2	0	3	.906	3
70			min	-3.005	5	-123.221	2	-36.64	5	-.015	3	-.066	4	-.788	1
71		17	max	31.336	1	289.495	3	76.459	1	.016	2	.005	3	.742	3
72			min	-12.511	5	-257.974	2	-34.889	5	-.015	3	-.085	4	-.636	1
73		18	max	31.336	1	460.671	3	108.231	1	.016	2	.06	1	.44	3
74			min	-22.017	5	-394.936	1	-33.139	5	-.015	3	-.109	5	-.374	1
75		19	max	31.336	1	631.848	3	140.004	1	.016	2	.16	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-31.523	5	-532.424	1	-31.388	5	-.015	3	-.135	5	0	3
77	M15	1	max	74.264	5	721.291	2	-6.876	12	.017	2	.253	4	0	2
78			min	-32.816	1	-361.977	3	-140.02	1	-.012	3	.011	10	0	3
79		2	max	64.758	5	529.174	2	-5.726	12	.017	2	.181	4	.255	3
80			min	-32.816	1	-271.11	3	-108.248	1	-.012	3	.003	10	-.504	2
81		3	max	55.252	5	337.057	2	-4.576	12	.017	2	.116	5	.437	3
82			min	-32.816	1	-180.243	3	-77.402	4	-.012	3	-.014	1	-.853	2
83		4	max	45.746	5	144.94	2	-3.191	10	.017	2	.068	5	.545	3
84			min	-32.816	1	-89.377	3	-69.085	4	-.012	3	-.063	1	-1.047	2
85		5	max	36.24	5	1.625	12	-.065	10	.017	2	.021	5	.581	3
86			min	-32.816	1	-47.177	2	-60.768	4	-.012	3	-.086	1	-1.086	2
87		6	max	26.734	5	92.357	3	18.843	1	.017	2	-.004	12	.543	3
88			min	-32.816	1	-239.294	2	-55.304	5	-.012	3	-.084	1	-.971	2
89		7	max	17.228	5	183.224	3	50.616	1	.017	2	-.004	10	.432	3
90			min	-32.816	1	-431.411	2	-53.554	5	-.012	3	-.081	4	-.701	2
91		8	max	7.722	5	274.09	3	82.388	1	.017	2	.002	2	.248	3
92			min	-32.816	1	-623.528	2	-51.803	5	-.012	3	-.113	4	-.276	2
93		9	max	-1.138	15	364.957	3	114.161	1	.017	2	.077	1	.304	2
94			min	-32.816	1	-815.645	2	-50.052	5	-.012	3	-.151	5	-.01	12
95		10	max	-2.189	10	455.824	3	145.934	1	.012	3	.25	4	1.038	2
96			min	-32.816	1	-1007.762	2	-106.029	14	-.017	2	0	3	-.34	3
97		11	max	-1.461	15	815.645	2	-2.326	12	.012	3	.177	4	.304	2
98			min	-32.816	1	-364.957	3	-114.161	1	-.017	2	-.004	3	-.01	12
99		12	max	-2.189	10	623.528	2	-1.175	12	.012	3	.11	4	.248	3
100			min	-32.816	1	-274.09	3	-82.388	1	-.017	2	-.006	3	-.276	2
101		13	max	-2.189	10	431.411	2	.134	3	.012	3	.062	5	.432	3
102			min	-32.816	1	-183.224	3	-70.077	4	-.017	2	-.056	1	-.701	2
103		14	max	-2.189	10	239.294	2	1.86	3	.012	3	.015	5	.543	3
104			min	-38.376	4	-92.357	3	-61.76	4	-.017	2	-.084	1	-.971	2
105		15	max	-2.189	10	47.177	2	12.93	1	.012	3	-.002	12	.581	3
106			min	-47.882	4	-1.625	12	-55.509	5	-.017	2	-.086	1	-1.086	2
107		16	max	-2.189	10	89.377	3	44.702	1	.012	3	0	3	.545	3
108			min	-57.387	4	-144.94	2	-53.758	5	-.017	2	-.089	4	-1.047	2
109		17	max	-2.189	10	180.243	3	76.475	1	.012	3	.005	3	.437	3
110			min	-66.893	4	-337.057	2	-52.007	5	-.017	2	-.122	4	-.853	2
111		18	max	-2.189	10	271.11	3	108.248	1	.012	3	.06	1	.255	3
112			min	-76.399	4	-529.174	2	-50.256	5	-.017	2	-.158	5	-.504	2
113		19	max	-2.189	10	361.977	3	140.02	1	.012	3	.16	1	0	2
114			min	-85.905	4	-721.291	2	-48.506	5	-.017	2	-.198	5	0	5
115	M16	1	max	69.706	5	640.025	2	-6.243	12	.008	1	.174	4	0	2
116			min	-52.503	1	-294.168	3	-134.476	1	-.012	3	.009	12	0	3
117		2	max	60.2	5	447.908	2	-5.093	12	.008	1	.119	4	.2	3
118			min	-52.503	1	-203.302	3	-102.703	1	-.012	3	.001	10	-.438	2
119		3	max	50.694	5	255.792	2	-3.943	12	.008	1	.077	5	.328	3
120			min	-52.503	1	-112.435	3	-70.931	1	-.012	3	-.032	1	-.722	2
121		4	max	41.189	5	63.675	2	-2.792	12	.008	1	.046	5	.382	3
122			min	-52.503	1	-21.568	3	-46.704	4	-.012	3	-.077	1	-.85	2
123		5	max	31.683	5	69.299	3	.229	10	.008	1	.016	5	.362	3
124			min	-52.503	1	-128.442	2	-38.387	4	-.012	3	-.096	1	-.824	2
125		6	max	22.177	5	160.165	3	24.387	1	.008	1	-.004	12	.27	3
126			min	-52.503	1	-320.559	2	-34.408	5	-.012	3	-.089	1	-.643	2
127		7	max	12.671	5	251.032	3	56.16	1	.008	1	-.004	12	.104	3
128			min	-52.503	1	-512.676	2	-32.657	5	-.012	3	-.056	1	-.308	2
129		8	max	3.165	5	341.899	3	87.933	1	.008	1	.004	2	.183	2
130			min	-52.503	1	-704.793	2	-30.906	5	-.012	3	-.066	4	-.135	3
131		9	max	-3.8	12	432.766	3	119.706	1	.008	1	.085	1	.828	2
132			min	-52.503	1	-896.91	2	-29.156	5	-.012	3	-.09	5	-.447	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-3.8	12	523.633	3	151.478	1	.008	1	.195	1	1.628	2
134			min	-52.503	1	-1089.027	2	-98.37	14	-.012	3	.002	12	-.832	3
135		11	max	.558	5	896.91	2	-2.959	12	.012	3	.117	4	.828	2
136			min	-52.503	1	-432.766	3	-119.706	1	-.008	1	-.002	3	-.447	3
137		12	max	-3.8	12	704.793	2	-1.809	12	.012	3	.066	4	.183	2
138			min	-52.503	1	-341.899	3	-87.933	1	-.008	1	-.005	3	-.135	3
139		13	max	-3.8	12	512.676	2	-.658	12	.012	3	.033	5	.104	3
140			min	-52.503	1	-251.032	3	-56.16	1	-.008	1	-.056	1	-.308	2
141		14	max	-3.8	12	320.559	2	.868	3	.012	3	.003	5	.27	3
142			min	-52.503	1	-160.165	3	-42.417	4	-.008	1	-.089	1	-.643	2
143		15	max	-3.8	12	128.442	2	7.385	1	.012	3	-.003	12	.362	3
144			min	-52.503	1	-69.299	3	-35.27	5	-.008	1	-.096	1	-.824	2
145		16	max	-3.8	12	21.568	3	39.158	1	.012	3	-.001	12	.382	3
146			min	-58.693	4	-63.675	2	-33.52	5	-.008	1	-.077	1	-.85	2
147		17	max	-3.8	12	112.435	3	70.931	1	.012	3	.002	3	.328	3
148			min	-68.199	4	-255.792	2	-31.769	5	-.008	1	-.088	4	-.722	2
149		18	max	-3.8	12	203.302	3	102.703	1	.012	3	.037	1	.2	3
150			min	-77.705	4	-447.908	2	-30.018	5	-.008	1	-.105	5	-.438	2
151		19	max	-3.8	12	294.168	3	134.476	1	.012	3	.133	1	0	2
152			min	-87.211	4	-640.025	2	-28.267	5	-.008	1	-.129	5	0	5
153	M2	1	max	1089.048	2	2.217	4	.551	1	0	3	0	3	0	1
154			min	-1427.791	3	.546	15	-44.399	4	0	1	0	1	0	1
155		2	max	1089.464	2	2.208	4	.551	1	0	3	0	1	0	15
156			min	-1427.479	3	.544	15	-44.759	4	0	1	-.012	4	0	4
157		3	max	1089.88	2	2.199	4	.551	1	0	3	0	1	0	15
158			min	-1427.167	3	.542	15	-45.12	4	0	1	-.025	4	-.001	4
159		4	max	1090.296	2	2.19	4	.551	1	0	3	0	1	0	15
160			min	-1426.855	3	.54	15	-45.48	4	0	1	-.038	4	-.002	4
161		5	max	1090.712	2	2.182	4	.551	1	0	3	0	1	0	15
162			min	-1426.543	3	.538	15	-45.841	4	0	1	-.051	4	-.002	4
163		6	max	1091.127	2	2.173	4	.551	1	0	3	0	1	0	15
164			min	-1426.231	3	.536	15	-46.201	4	0	1	-.063	4	-.003	4
165		7	max	1091.543	2	2.164	4	.551	1	0	3	0	1	0	15
166			min	-1425.92	3	.534	15	-46.562	4	0	1	-.077	4	-.004	4
167		8	max	1091.959	2	2.156	4	.551	1	0	3	.001	1	-.001	15
168			min	-1425.608	3	.532	15	-46.922	4	0	1	-.09	4	-.004	4
169		9	max	1092.375	2	2.147	4	.551	1	0	3	.001	1	-.001	15
170			min	-1425.296	3	.53	15	-47.283	4	0	1	-.103	4	-.005	4
171		10	max	1092.791	2	2.138	4	.551	1	0	3	.001	1	-.001	15
172			min	-1424.984	3	.528	15	-47.643	4	0	1	-.116	4	-.005	4
173		11	max	1093.207	2	2.129	4	.551	1	0	3	.002	1	-.002	15
174			min	-1424.672	3	.525	15	-48.004	4	0	1	-.13	4	-.006	4
175		12	max	1093.623	2	2.121	4	.551	1	0	3	.002	1	-.002	15
176			min	-1424.36	3	.523	15	-48.364	4	0	1	-.143	4	-.007	4
177		13	max	1094.039	2	2.112	4	.551	1	0	3	.002	1	-.002	15
178			min	-1424.048	3	.521	15	-48.724	4	0	1	-.157	4	-.007	4
179		14	max	1094.455	2	2.103	4	.551	1	0	3	.002	1	-.002	15
180			min	-1423.736	3	.519	15	-49.085	4	0	1	-.17	4	-.008	4
181		15	max	1094.87	2	2.095	4	.551	1	0	3	.002	1	-.002	15
182			min	-1423.424	3	.517	15	-49.445	4	0	1	-.184	4	-.008	4
183		16	max	1095.286	2	2.086	4	.551	1	0	3	.002	1	-.002	15
184			min	-1423.112	3	.515	15	-49.806	4	0	1	-.198	4	-.009	4
185		17	max	1095.702	2	2.077	4	.551	1	0	3	.002	1	-.002	15
186			min	-1422.801	3	.513	15	-50.166	4	0	1	-.212	4	-.01	4
187		18	max	1096.118	2	2.068	4	.551	1	0	3	.003	1	-.003	15
188			min	-1422.489	3	.511	15	-50.527	4	0	1	-.226	4	-.01	4
189		19	max	1096.534	2	2.06	4	.551	1	0	3	.003	1	-.003	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-1422.177	3	.509	15	-50.887	4	0	1	-.24	4	-.011	4
191	M3	1	max	600.629	2	9.136	4	.137	1	0	3	0	1	.011	4
192			min	-738.36	3	2.162	15	-2.93	5	0	4	-.004	4	.003	15
193		2	max	600.458	2	8.262	4	.137	1	0	3	0	1	.007	4
194			min	-738.488	3	1.957	15	-2.321	5	0	4	-.005	4	.001	12
195		3	max	600.288	2	7.387	4	.137	1	0	3	0	1	.003	2
196			min	-738.616	3	1.751	15	-1.712	5	0	4	-.006	4	0	3
197		4	max	600.118	2	6.513	4	.137	1	0	3	0	1	0	2
198			min	-738.744	3	1.546	15	-1.104	5	0	4	-.007	5	-.002	3
199		5	max	599.947	2	5.638	4	.137	1	0	3	0	1	0	15
200			min	-738.871	3	1.34	15	-.495	5	0	4	-.007	5	-.004	3
201		6	max	599.777	2	4.764	4	.168	4	0	3	0	1	-.001	15
202			min	-738.999	3	1.135	15	.01	10	0	4	-.007	5	-.006	6
203		7	max	599.606	2	3.89	4	.776	4	0	3	0	1	-.002	15
204			min	-739.127	3	.929	15	.01	10	0	4	-.007	5	-.008	6
205		8	max	599.436	2	3.015	4	1.385	4	0	3	0	1	-.002	15
206			min	-739.255	3	.724	15	.01	10	0	4	-.007	5	-.009	6
207		9	max	599.266	2	2.141	4	1.994	4	0	3	0	1	-.002	15
208			min	-739.382	3	.518	15	.01	10	0	4	-.006	5	-.011	6
209		10	max	599.095	2	1.266	4	2.602	4	0	3	0	1	-.003	15
210			min	-739.51	3	.312	15	.01	10	0	4	-.005	5	-.011	6
211		11	max	598.925	2	.455	2	3.211	4	0	3	0	1	-.003	15
212			min	-739.638	3	-.035	3	.01	10	0	4	-.003	5	-.012	6
213		12	max	598.755	2	-.099	15	3.82	4	0	3	0	1	-.003	15
214			min	-739.766	3	-.546	3	.01	10	0	4	-.002	5	-.012	6
215		13	max	598.584	2	-.304	15	4.429	4	0	3	0	1	-.003	15
216			min	-739.893	3	-1.358	6	.01	10	0	4	0	10	-.011	6
217		14	max	598.414	2	-.51	15	5.037	4	0	3	.003	4	-.002	15
218			min	-740.021	3	-2.233	6	.01	10	0	4	0	10	-.01	6
219		15	max	598.244	2	-.715	15	5.646	4	0	3	.005	4	-.002	15
220			min	-740.149	3	-3.107	6	.01	10	0	4	0	10	-.009	6
221		16	max	598.073	2	-.921	15	6.255	4	0	3	.008	4	-.002	15
222			min	-740.277	3	-3.982	6	.01	10	0	4	0	10	-.008	6
223		17	max	597.903	2	-1.126	15	6.863	4	0	3	.011	4	-.001	15
224			min	-740.404	3	-4.856	6	.01	10	0	4	0	10	-.005	6
225		18	max	597.733	2	-1.332	15	7.472	4	0	3	.014	4	0	15
226			min	-740.532	3	-5.731	6	.01	10	0	4	0	10	-.003	6
227		19	max	597.562	2	-1.538	15	8.081	4	0	3	.018	4	0	1
228			min	-740.66	3	-6.605	6	.01	10	0	4	0	10	0	1
229	M4	1	max	1124.511	1	0	1	-.547	12	0	1	.011	4	0	1
230			min	-280.18	3	0	1	-226.603	4	0	1	0	10	0	1
231		2	max	1124.681	1	0	1	-.547	12	0	1	0	12	0	1
232			min	-280.052	3	0	1	-226.75	4	0	1	-.015	4	0	1
233		3	max	1124.852	1	0	1	-.547	12	0	1	0	12	0	1
234			min	-279.924	3	0	1	-226.898	4	0	1	-.041	4	0	1
235		4	max	1125.022	1	0	1	-.547	12	0	1	0	12	0	1
236			min	-279.797	3	0	1	-227.046	4	0	1	-.067	4	0	1
237		5	max	1125.192	1	0	1	-.547	12	0	1	0	12	0	1
238			min	-279.669	3	0	1	-227.193	4	0	1	-.093	4	0	1
239		6	max	1125.363	1	0	1	-.547	12	0	1	0	12	0	1
240			min	-279.541	3	0	1	-227.341	4	0	1	-.12	4	0	1
241		7	max	1125.533	1	0	1	-.547	12	0	1	0	12	0	1
242			min	-279.413	3	0	1	-227.488	4	0	1	-.146	4	0	1
243		8	max	1125.703	1	0	1	-.547	12	0	1	0	12	0	1
244			min	-279.286	3	0	1	-227.636	4	0	1	-.172	4	0	1
245		9	max	1125.874	1	0	1	-.547	12	0	1	0	12	0	1
246			min	-279.158	3	0	1	-227.784	4	0	1	-.198	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	1126.044	1	0	1	-.547	12	0	1	0	12	0	1
248			min	-279.03	3	0	1	-227.931	4	0	1	-.224	4	0	1
249		11	max	1126.214	1	0	1	-.547	12	0	1	0	12	0	1
250			min	-278.902	3	0	1	-228.079	4	0	1	-.25	4	0	1
251		12	max	1126.385	1	0	1	-.547	12	0	1	0	12	0	1
252			min	-278.775	3	0	1	-228.227	4	0	1	-.276	4	0	1
253		13	max	1126.555	1	0	1	-.547	12	0	1	0	12	0	1
254			min	-278.647	3	0	1	-228.374	4	0	1	-.303	4	0	1
255		14	max	1126.725	1	0	1	-.547	12	0	1	0	12	0	1
256			min	-278.519	3	0	1	-228.522	4	0	1	-.329	4	0	1
257		15	max	1126.896	1	0	1	-.547	12	0	1	0	12	0	1
258			min	-278.391	3	0	1	-228.67	4	0	1	-.355	4	0	1
259		16	max	1127.066	1	0	1	-.547	12	0	1	0	12	0	1
260			min	-278.264	3	0	1	-228.817	4	0	1	-.381	4	0	1
261		17	max	1127.236	1	0	1	-.547	12	0	1	0	12	0	1
262			min	-278.136	3	0	1	-228.965	4	0	1	-.408	4	0	1
263		18	max	1127.407	1	0	1	-.547	12	0	1	-.001	12	0	1
264			min	-278.008	3	0	1	-229.112	4	0	1	-.434	4	0	1
265		19	max	1127.577	1	0	1	-.547	12	0	1	-.001	12	0	1
266			min	-277.88	3	0	1	-229.26	4	0	1	-.46	4	0	1
267	M6	1	max	3268.948	2	2.648	2	0	1	0	4	0	4	0	1
268			min	-4419.961	3	.03	3	-44.849	4	0	1	0	1	0	1
269		2	max	3269.364	2	2.642	2	0	1	0	4	0	1	0	3
270			min	-4419.649	3	.025	3	-45.21	4	0	1	-.013	4	0	2
271		3	max	3269.78	2	2.635	2	0	1	0	4	0	1	0	3
272			min	-4419.337	3	.02	3	-45.57	4	0	1	-.025	4	-.001	2
273		4	max	3270.195	2	2.628	2	0	1	0	4	0	1	0	3
274			min	-4419.025	3	.015	3	-45.931	4	0	1	-.038	4	-.002	2
275		5	max	3270.611	2	2.621	2	0	1	0	4	0	1	0	3
276			min	-4418.713	3	.01	3	-46.291	4	0	1	-.051	4	-.003	2
277		6	max	3271.027	2	2.614	2	0	1	0	4	0	1	0	3
278			min	-4418.401	3	.004	3	-46.651	4	0	1	-.064	4	-.004	2
279		7	max	3271.443	2	2.608	2	0	1	0	4	0	1	0	3
280			min	-4418.089	3	0	3	-47.012	4	0	1	-.077	4	-.004	2
281		8	max	3271.859	2	2.601	2	0	1	0	4	0	1	0	3
282			min	-4417.777	3	-.006	3	-47.372	4	0	1	-.09	4	-.005	2
283		9	max	3272.275	2	2.594	2	0	1	0	4	0	1	0	3
284			min	-4417.465	3	-.011	3	-47.733	4	0	1	-.104	4	-.006	2
285		10	max	3272.691	2	2.587	2	0	1	0	4	0	1	0	3
286			min	-4417.153	3	-.016	3	-48.093	4	0	1	-.117	4	-.007	2
287		11	max	3273.107	2	2.58	2	0	1	0	4	0	1	0	3
288			min	-4416.841	3	-.021	3	-48.454	4	0	1	-.131	4	-.007	2
289		12	max	3273.522	2	2.574	2	0	1	0	4	0	1	0	3
290			min	-4416.53	3	-.026	3	-48.814	4	0	1	-.144	4	-.008	2
291		13	max	3273.938	2	2.567	2	0	1	0	4	0	1	0	3
292			min	-4416.218	3	-.031	3	-49.175	4	0	1	-.158	4	-.009	2
293		14	max	3274.354	2	2.56	2	0	1	0	4	0	1	0	3
294			min	-4415.906	3	-.036	3	-49.535	4	0	1	-.172	4	-.009	2
295		15	max	3274.77	2	2.553	2	0	1	0	4	0	1	0	3
296			min	-4415.594	3	-.041	3	-49.896	4	0	1	-.186	4	-.01	2
297		16	max	3275.186	2	2.546	2	0	1	0	4	0	1	0	3
298			min	-4415.282	3	-.047	3	-50.256	4	0	1	-.2	4	-.011	2
299		17	max	3275.602	2	2.54	2	0	1	0	4	0	1	0	3
300			min	-4414.97	3	-.052	3	-50.617	4	0	1	-.214	4	-.012	2
301		18	max	3276.018	2	2.533	2	0	1	0	4	0	1	0	3
302			min	-4414.658	3	-.057	3	-50.977	4	0	1	-.228	4	-.012	2
303		19	max	3276.434	2	2.526	2	0	1	0	4	0	1	0	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-4414.346	3	-.062	3	-51.338	4	0	1	-.243	4	-.013	2
305	M7	1	max	1986.655	2	9.132	6	0	1	0	1	0	1	.013	2
306			min	-2180.277	3	2.144	15	-3.121	5	0	4	-.004	4	0	3
307		2	max	1986.485	2	8.257	6	0	1	0	1	0	1	.01	2
308			min	-2180.405	3	1.938	15	-2.512	5	0	4	-.005	4	-.002	3
309		3	max	1986.315	2	7.383	6	0	1	0	1	0	1	.006	2
310			min	-2180.533	3	1.732	15	-1.903	5	0	4	-.006	4	-.004	3
311		4	max	1986.144	2	6.508	6	0	1	0	1	0	1	.004	2
312			min	-2180.66	3	1.527	15	-1.295	5	0	4	-.007	4	-.006	3
313		5	max	1985.974	2	5.634	6	0	1	0	1	0	1	.001	2
314			min	-2180.788	3	1.321	15	-.686	5	0	4	-.008	4	-.007	3
315		6	max	1985.804	2	4.759	6	0	1	0	1	0	1	-.001	2
316			min	-2180.916	3	1.116	15	-.077	5	0	4	-.008	4	-.008	3
317		7	max	1985.633	2	3.885	6	.552	4	0	1	0	1	-.002	15
318			min	-2181.044	3	.91	15	0	1	0	4	-.008	4	-.009	3
319		8	max	1985.463	2	3.011	6	1.16	4	0	1	0	1	-.002	15
320			min	-2181.171	3	.705	15	0	1	0	4	-.007	5	-.009	4
321		9	max	1985.293	2	2.214	2	1.769	4	0	1	0	1	-.003	15
322			min	-2181.299	3	.365	12	0	1	0	4	-.007	5	-.011	4
323		10	max	1985.122	2	1.532	2	2.378	4	0	1	0	1	-.003	15
324			min	-2181.427	3	-.009	3	0	1	0	4	-.006	5	-.011	4
325		11	max	1984.952	2	.851	2	2.987	4	0	1	0	1	-.003	15
326			min	-2181.555	3	-.52	3	0	1	0	4	-.004	5	-.012	4
327		12	max	1984.782	2	.169	2	3.595	4	0	1	0	1	-.003	15
328			min	-2181.683	3	-1.032	3	0	1	0	4	-.003	5	-.012	4
329		13	max	1984.611	2	-.323	15	4.204	4	0	1	0	1	-.003	15
330			min	-2181.81	3	-1.543	3	0	1	0	4	-.001	5	-.011	4
331		14	max	1984.441	2	-.529	15	4.813	4	0	1	.001	4	-.002	15
332			min	-2181.938	3	-2.236	4	0	1	0	4	0	1	-.01	4
333		15	max	1984.271	2	-.734	15	5.421	4	0	1	.004	4	-.002	15
334			min	-2182.066	3	-3.111	4	0	1	0	4	0	1	-.009	4
335		16	max	1984.1	2	-.94	15	6.03	4	0	1	.006	4	-.002	15
336			min	-2182.194	3	-3.985	4	0	1	0	4	0	1	-.008	4
337		17	max	1983.93	2	-1.145	15	6.639	4	0	1	.009	4	-.001	15
338			min	-2182.321	3	-4.859	4	0	1	0	4	0	1	-.005	4
339		18	max	1983.76	2	-1.351	15	7.247	4	0	1	.013	4	0	15
340			min	-2182.449	3	-5.734	4	0	1	0	4	0	1	-.003	4
341		19	max	1983.589	2	-1.556	15	7.856	4	0	1	.016	4	0	1
342			min	-2182.577	3	-6.608	4	0	1	0	4	0	1	0	1
343	M8	1	max	3128	2	0	1	0	1	0	1	.01	4	0	1
344			min	-923.596	3	0	1	-219.01	4	0	1	0	1	0	1
345		2	max	3128.17	2	0	1	0	1	0	1	0	1	0	1
346			min	-923.469	3	0	1	-219.157	4	0	1	-.016	4	0	1
347		3	max	3128.34	2	0	1	0	1	0	1	0	1	0	1
348			min	-923.341	3	0	1	-219.305	4	0	1	-.041	4	0	1
349		4	max	3128.511	2	0	1	0	1	0	1	0	1	0	1
350			min	-923.213	3	0	1	-219.453	4	0	1	-.066	4	0	1
351		5	max	3128.681	2	0	1	0	1	0	1	0	1	0	1
352			min	-923.085	3	0	1	-219.6	4	0	1	-.091	4	0	1
353		6	max	3128.851	2	0	1	0	1	0	1	0	1	0	1
354			min	-922.958	3	0	1	-219.748	4	0	1	-.116	4	0	1
355		7	max	3129.022	2	0	1	0	1	0	1	0	1	0	1
356			min	-922.83	3	0	1	-219.895	4	0	1	-.142	4	0	1
357		8	max	3129.192	2	0	1	0	1	0	1	0	1	0	1
358			min	-922.702	3	0	1	-220.043	4	0	1	-.167	4	0	1
359		9	max	3129.362	2	0	1	0	1	0	1	0	1	0	1
360			min	-922.574	3	0	1	-220.191	4	0	1	-.192	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	3129.533	2	0	1	0	1	0	1	0	1	0	1
362			min	-922.447	3	0	1	-220.338	4	0	1	-.217	4	0	1
363		11	max	3129.703	2	0	1	0	1	0	1	0	1	0	1
364			min	-922.319	3	0	1	-220.486	4	0	1	-.243	4	0	1
365		12	max	3129.873	2	0	1	0	1	0	1	0	1	0	1
366			min	-922.191	3	0	1	-220.634	4	0	1	-.268	4	0	1
367		13	max	3130.044	2	0	1	0	1	0	1	0	1	0	1
368			min	-922.063	3	0	1	-220.781	4	0	1	-.293	4	0	1
369		14	max	3130.214	2	0	1	0	1	0	1	0	1	0	1
370			min	-921.936	3	0	1	-220.929	4	0	1	-.319	4	0	1
371		15	max	3130.384	2	0	1	0	1	0	1	0	1	0	1
372			min	-921.808	3	0	1	-221.077	4	0	1	-.344	4	0	1
373		16	max	3130.555	2	0	1	0	1	0	1	0	1	0	1
374			min	-921.68	3	0	1	-221.224	4	0	1	-.369	4	0	1
375		17	max	3130.725	2	0	1	0	1	0	1	0	1	0	1
376			min	-921.552	3	0	1	-221.372	4	0	1	-.395	4	0	1
377		18	max	3130.895	2	0	1	0	1	0	1	0	1	0	1
378			min	-921.424	3	0	1	-221.519	4	0	1	-.42	4	0	1
379		19	max	3131.066	2	0	1	0	1	0	1	0	1	0	1
380			min	-921.297	3	0	1	-221.667	4	0	1	-.446	4	0	1
381	M10	1	max	1089.048	2	2.102	6	-.037	10	0	1	0	4	0	1
382			min	-1427.791	3	.468	15	-44.695	4	0	3	0	3	0	1
383		2	max	1089.464	2	2.093	6	-.037	10	0	1	0	10	0	15
384			min	-1427.479	3	.466	15	-45.056	4	0	3	-.013	4	0	6
385		3	max	1089.88	2	2.084	6	-.037	10	0	1	0	10	0	15
386			min	-1427.167	3	.464	15	-45.416	4	0	3	-.025	4	-.001	6
387		4	max	1090.296	2	2.075	6	-.037	10	0	1	0	10	0	15
388			min	-1426.855	3	.462	15	-45.776	4	0	3	-.038	4	-.002	6
389		5	max	1090.712	2	2.067	6	-.037	10	0	1	0	10	0	15
390			min	-1426.543	3	.46	15	-46.137	4	0	3	-.051	4	-.002	6
391		6	max	1091.127	2	2.058	6	-.037	10	0	1	0	10	0	15
392			min	-1426.231	3	.458	15	-46.497	4	0	3	-.064	4	-.003	6
393		7	max	1091.543	2	2.049	6	-.037	10	0	1	0	10	0	15
394			min	-1425.92	3	.456	15	-46.858	4	0	3	-.077	4	-.003	6
395		8	max	1091.959	2	2.041	6	-.037	10	0	1	0	10	0	15
396			min	-1425.608	3	.454	15	-47.218	4	0	3	-.09	4	-.004	6
397		9	max	1092.375	2	2.032	6	-.037	10	0	1	0	10	-.001	15
398			min	-1425.296	3	.452	15	-47.579	4	0	3	-.103	4	-.005	6
399		10	max	1092.791	2	2.023	6	-.037	10	0	1	0	10	-.001	15
400			min	-1424.984	3	.45	15	-47.939	4	0	3	-.117	4	-.005	6
401		11	max	1093.207	2	2.014	6	-.037	10	0	1	0	10	-.001	15
402			min	-1424.672	3	.448	15	-48.3	4	0	3	-.13	4	-.006	6
403		12	max	1093.623	2	2.006	6	-.037	10	0	1	0	10	-.001	15
404			min	-1424.36	3	.446	15	-48.66	4	0	3	-.144	4	-.006	6
405		13	max	1094.039	2	1.997	6	-.037	10	0	1	0	10	-.002	15
406			min	-1424.048	3	.444	15	-49.021	4	0	3	-.158	4	-.007	6
407		14	max	1094.455	2	1.988	6	-.037	10	0	1	0	10	-.002	15
408			min	-1423.736	3	.442	15	-49.381	4	0	3	-.171	4	-.007	6
409		15	max	1094.87	2	1.98	6	-.037	10	0	1	0	10	-.002	15
410			min	-1423.424	3	.44	15	-49.742	4	0	3	-.185	4	-.008	6
411		16	max	1095.286	2	1.971	6	-.037	10	0	1	0	10	-.002	15
412			min	-1423.112	3	.438	15	-50.102	4	0	3	-.199	4	-.009	6
413		17	max	1095.702	2	1.962	6	-.037	10	0	1	0	10	-.002	15
414			min	-1422.801	3	.436	15	-50.463	4	0	3	-.213	4	-.009	6
415		18	max	1096.118	2	1.953	6	-.037	10	0	1	0	10	-.002	15
416			min	-1422.489	3	.434	15	-50.823	4	0	3	-.228	4	-.01	6
417		19	max	1096.534	2	1.945	6	-.037	10	0	1	0	10	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-1422.177	3	.432	15	-51.184	4	0	3	-.242	4	-.01	6
419	M11	1	max	600.629	2	9.068	6	-.01	10	0	1	0	10	.01	6
420			min	-738.36	3	2.116	15	-2.949	4	0	4	-.004	4	.002	15
421		2	max	600.458	2	8.194	6	-.01	10	0	1	0	10	.006	2
422			min	-738.488	3	1.911	15	-2.34	4	0	4	-.005	4	.001	12
423		3	max	600.288	2	7.319	6	-.01	10	0	1	0	10	.003	2
424			min	-738.616	3	1.705	15	-1.732	4	0	4	-.006	4	0	3
425		4	max	600.118	2	6.445	6	-.01	10	0	1	0	10	0	2
426			min	-738.744	3	1.5	15	-1.123	4	0	4	-.007	4	-.002	3
427		5	max	599.947	2	5.57	6	-.01	10	0	1	0	10	0	15
428			min	-738.871	3	1.294	15	-.514	4	0	4	-.007	4	-.004	4
429		6	max	599.777	2	4.696	6	.099	5	0	1	0	10	-.002	15
430			min	-738.999	3	1.089	15	-.137	1	0	4	-.007	4	-.006	4
431		7	max	599.606	2	3.821	6	.707	5	0	1	0	10	-.002	15
432			min	-739.127	3	.883	15	-.137	1	0	4	-.007	4	-.008	4
433		8	max	599.436	2	2.947	6	1.316	5	0	1	0	10	-.002	15
434			min	-739.255	3	.678	15	-.137	1	0	4	-.007	4	-.01	4
435		9	max	599.266	2	2.073	6	1.925	5	0	1	0	10	-.003	15
436			min	-739.382	3	.472	15	-.137	1	0	4	-.006	4	-.011	4
437		10	max	599.095	2	1.198	6	2.534	5	0	1	0	10	-.003	15
438			min	-739.51	3	.267	15	-.137	1	0	4	-.005	4	-.012	4
439		11	max	598.925	2	.455	2	3.142	5	0	1	0	10	-.003	15
440			min	-739.638	3	-.035	3	-.137	1	0	4	-.004	4	-.012	4
441		12	max	598.755	2	-.145	15	3.751	5	0	1	0	10	-.003	15
442			min	-739.766	3	-.552	4	-.137	1	0	4	-.002	4	-.012	4
443		13	max	598.584	2	-.35	15	4.36	5	0	1	0	5	-.003	15
444			min	-739.893	3	-1.427	4	-.137	1	0	4	0	1	-.012	4
445		14	max	598.414	2	-.556	15	4.968	5	0	1	.002	5	-.003	15
446			min	-740.021	3	-2.301	4	-.137	1	0	4	0	1	-.011	4
447		15	max	598.244	2	-.761	15	5.577	5	0	1	.005	5	-.002	15
448			min	-740.149	3	-3.175	4	-.137	1	0	4	0	1	-.009	4
449		16	max	598.073	2	-.967	15	6.186	5	0	1	.008	5	-.002	15
450			min	-740.277	3	-4.05	4	-.137	1	0	4	-.001	1	-.008	4
451		17	max	597.903	2	-1.172	15	6.795	5	0	1	.011	5	-.001	15
452			min	-740.404	3	-4.924	4	-.137	1	0	4	-.001	1	-.005	4
453		18	max	597.733	2	-1.378	15	7.403	5	0	1	.014	5	0	15
454			min	-740.532	3	-5.799	4	-.137	1	0	4	-.001	1	-.003	4
455		19	max	597.562	2	-1.583	15	8.012	5	0	1	.018	5	0	1
456			min	-740.66	3	-6.673	4	-.137	1	0	4	-.001	1	0	1
457	M12	1	max	1124.511	1	0	1	7.851	1	0	1	.01	5	0	1
458			min	-280.18	3	0	1	-222.376	4	0	1	0	1	0	1
459		2	max	1124.681	1	0	1	7.851	1	0	1	0	1	0	1
460			min	-280.052	3	0	1	-222.524	4	0	1	-.015	4	0	1
461		3	max	1124.852	1	0	1	7.851	1	0	1	.001	1	0	1
462			min	-279.924	3	0	1	-222.671	4	0	1	-.041	4	0	1
463		4	max	1125.022	1	0	1	7.851	1	0	1	.002	1	0	1
464			min	-279.797	3	0	1	-222.819	4	0	1	-.066	4	0	1
465		5	max	1125.192	1	0	1	7.851	1	0	1	.003	1	0	1
466			min	-279.669	3	0	1	-222.967	4	0	1	-.092	4	0	1
467		6	max	1125.363	1	0	1	7.851	1	0	1	.004	1	0	1
468			min	-279.541	3	0	1	-223.114	4	0	1	-.117	4	0	1
469		7	max	1125.533	1	0	1	7.851	1	0	1	.005	1	0	1
470			min	-279.413	3	0	1	-223.262	4	0	1	-.143	4	0	1
471		8	max	1125.703	1	0	1	7.851	1	0	1	.006	1	0	1
472			min	-279.286	3	0	1	-223.41	4	0	1	-.169	4	0	1
473		9	max	1125.874	1	0	1	7.851	1	0	1	.006	1	0	1
474			min	-279.158	3	0	1	-223.557	4	0	1	-.194	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	1126.044	1	0	1	7.851	1	0	1	.007	1	0	1
476			min	-279.03	3	0	1	-223.705	4	0	1	-.22	4	0	1
477		11	max	1126.214	1	0	1	7.851	1	0	1	.008	1	0	1
478			min	-278.902	3	0	1	-223.852	4	0	1	-.246	4	0	1
479		12	max	1126.385	1	0	1	7.851	1	0	1	.009	1	0	1
480			min	-278.775	3	0	1	-224	4	0	1	-.271	4	0	1
481		13	max	1126.555	1	0	1	7.851	1	0	1	.01	1	0	1
482			min	-278.647	3	0	1	-224.148	4	0	1	-.297	4	0	1
483		14	max	1126.725	1	0	1	7.851	1	0	1	.011	1	0	1
484			min	-278.519	3	0	1	-224.295	4	0	1	-.323	4	0	1
485		15	max	1126.896	1	0	1	7.851	1	0	1	.012	1	0	1
486			min	-278.391	3	0	1	-224.443	4	0	1	-.349	4	0	1
487		16	max	1127.066	1	0	1	7.851	1	0	1	.013	1	0	1
488			min	-278.264	3	0	1	-224.591	4	0	1	-.375	4	0	1
489		17	max	1127.236	1	0	1	7.851	1	0	1	.014	1	0	1
490			min	-278.136	3	0	1	-224.738	4	0	1	-.4	4	0	1
491		18	max	1127.407	1	0	1	7.851	1	0	1	.015	1	0	1
492			min	-278.008	3	0	1	-224.886	4	0	1	-.426	4	0	1
493		19	max	1127.577	1	0	1	7.851	1	0	1	.016	1	0	1
494			min	-277.88	3	0	1	-225.033	4	0	1	-.452	4	0	1
495	M1	1	max	133.892	1	763.905	3	45.512	5	0	1	.131	1	0	15
496			min	-16.303	5	-450.653	1	-46.926	1	0	3	-.083	5	-.014	2
497		2	max	134.468	1	762.718	3	46.972	5	0	1	.102	1	.268	1
498			min	-16.034	5	-452.236	1	-46.926	1	0	3	-.055	5	-.48	3
499		3	max	478.071	3	580.212	2	5.003	5	0	3	.072	1	.538	1
500			min	-301.822	2	-592.827	3	-46.508	1	0	2	-.026	5	-.938	3
501		4	max	478.504	3	578.629	2	6.463	5	0	3	.044	1	.189	1
502			min	-301.246	2	-594.015	3	-46.508	1	0	2	-.022	5	-.57	3
503		5	max	478.936	3	577.045	2	7.923	5	0	3	.015	1	-.005	15
504			min	-300.67	2	-595.202	3	-46.508	1	0	2	-.018	5	-.201	3
505		6	max	479.368	3	575.462	2	9.383	5	0	3	-.001	10	.169	3
506			min	-300.093	2	-596.39	3	-46.508	1	0	2	-.015	4	-.552	2
507		7	max	479.8	3	573.879	2	10.843	5	0	3	-.003	10	.539	3
508			min	-299.517	2	-597.577	3	-46.508	1	0	2	-.043	1	-.908	2
509		8	max	480.232	3	572.296	2	12.303	5	0	3	.001	5	.91	3
510			min	-298.941	2	-598.764	3	-46.508	1	0	2	-.072	1	-1.264	2
511		9	max	491.414	3	48.238	2	45.173	5	0	9	.048	1	1.06	3
512			min	-245.049	2	.474	15	-77.879	1	0	3	-.113	5	-1.441	2
513		10	max	491.847	3	46.655	2	46.634	5	0	9	0	10	1.038	3
514			min	-244.473	2	-.008	5	-77.879	1	0	3	-.086	4	-1.47	2
515		11	max	492.279	3	45.072	2	48.094	5	0	9	-.003	10	1.016	3
516			min	-243.896	2	-2.007	4	-77.879	1	0	3	-.066	4	-1.499	2
517		12	max	503.198	3	401.058	3	127.667	5	0	2	.071	1	.891	3
518			min	-189.887	2	-674.819	2	-45.072	1	0	3	-.204	5	-1.33	2
519		13	max	503.63	3	399.871	3	129.127	5	0	2	.043	1	.643	3
520			min	-189.311	2	-676.402	2	-45.072	1	0	3	-.124	5	-.911	2
521		14	max	504.063	3	398.683	3	130.587	5	0	2	.015	1	.395	3
522			min	-188.735	2	-677.985	2	-45.072	1	0	3	-.044	5	-.491	2
523		15	max	504.495	3	397.496	3	132.048	5	0	2	.038	5	.148	3
524			min	-188.159	2	-679.568	2	-45.072	1	0	3	-.013	1	-.097	1
525		16	max	504.927	3	396.308	3	133.508	5	0	2	.12	5	.353	2
526			min	-187.582	2	-681.152	2	-45.072	1	0	3	-.041	1	-.098	3
527		17	max	505.359	3	395.121	3	134.968	5	0	2	.203	5	.776	2
528			min	-187.006	2	-682.735	2	-45.072	1	0	3	-.069	1	-.344	3
529		18	max	27.998	5	642.325	2	-3.8	12	0	5	.176	5	.391	2
530			min	-135.049	1	-293.083	3	-88.671	4	0	2	-.1	1	-.17	3
531		19	max	28.267	5	640.742	2	-3.8	12	0	5	.129	5	.012	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-134.472	1	-294.271	3	-87.211	4	0	2	-.133	1	-.008	1
533	M5	1	max	304.124	1	2516.935	3	74.827	5	0	1	0	1	.028	2
534			min	7.178	12	-1562.253	1	0	1	0	4	-.166	4	0	15
535		2	max	304.7	1	2515.748	3	76.287	5	0	1	0	1	.993	1
536			min	7.467	12	-1563.836	1	0	1	0	4	-.119	4	-1.549	3
537		3	max	1452.371	3	1512.621	2	36.714	4	0	4	0	1	1.931	1
538			min	-942.33	2	-1698.014	3	0	1	0	1	-.072	4	-3.064	3
539		4	max	1452.803	3	1511.037	2	38.174	4	0	4	0	1	1.012	1
540			min	-941.754	2	-1699.201	3	0	1	0	1	-.049	4	-2.009	3
541		5	max	1453.235	3	1509.454	2	39.634	4	0	4	0	1	.093	1
542			min	-941.178	2	-1700.389	3	0	1	0	1	-.025	4	-.955	3
543		6	max	1453.667	3	1507.871	2	41.094	4	0	4	0	4	.101	3
544			min	-940.601	2	-1701.576	3	0	1	0	1	0	1	-.906	2
545		7	max	1454.1	3	1506.288	2	42.554	4	0	4	.026	4	1.158	3
546			min	-940.025	2	-1702.764	3	0	1	0	1	0	1	-1.841	2
547		8	max	1454.532	3	1504.705	2	44.014	4	0	4	.053	4	2.215	3
548			min	-939.449	2	-1703.951	3	0	1	0	1	0	1	-2.775	2
549		9	max	1464.521	3	164.303	2	150.736	4	0	1	0	1	2.556	3
550			min	-820.357	2	.477	15	0	1	0	1	-.166	4	-3.178	2
551		10	max	1464.953	3	162.72	2	152.197	4	0	1	0	1	2.466	3
552			min	-819.781	2	0	15	0	1	0	1	-.072	5	-3.279	2
553		11	max	1465.385	3	161.137	2	153.657	4	0	1	.023	4	2.377	3
554			min	-819.205	2	-1.854	6	0	1	0	1	0	1	-3.38	2
555		12	max	1475.899	3	1091.202	3	172.894	4	0	1	0	1	2.077	3
556			min	-700.347	2	-1831.807	2	0	1	0	4	-.285	4	-3.018	2
557		13	max	1476.331	3	1090.015	3	174.354	4	0	1	0	1	1.4	3
558			min	-699.771	2	-1833.391	2	0	1	0	4	-.177	4	-1.881	2
559		14	max	1476.763	3	1088.828	3	175.814	4	0	1	0	1	.724	3
560			min	-699.195	2	-1834.974	2	0	1	0	4	-.068	4	-.742	2
561		15	max	1477.196	3	1087.64	3	177.274	4	0	1	.041	4	.397	2
562			min	-698.619	2	-1836.557	2	0	1	0	4	0	1	0	15
563		16	max	1477.628	3	1086.453	3	178.735	4	0	1	.152	4	1.537	2
564			min	-698.042	2	-1838.14	2	0	1	0	4	0	1	-.626	3
565		17	max	1478.06	3	1085.266	3	180.195	4	0	1	.263	4	2.679	2
566			min	-697.466	2	-1839.723	2	0	1	0	4	0	1	-1.3	3
567		18	max	-8.506	12	2182.209	2	0	1	0	4	.265	4	1.368	2
568			min	-303.54	1	-1046.349	3	-27.419	5	0	1	0	1	-.675	3
569		19	max	-8.218	12	2180.626	2	0	1	0	4	.25	4	.017	1
570			min	-302.963	1	-1047.536	3	-25.959	5	0	1	0	1	-.025	3
571	M9	1	max	133.892	1	763.905	3	61.202	4	0	3	-.009	10	0	15
572			min	6.763	12	-450.653	1	3.166	10	0	4	-.131	1	-.014	2
573		2	max	134.468	1	762.718	3	62.662	4	0	3	-.007	10	.268	1
574			min	7.051	12	-452.236	1	3.166	10	0	4	-.102	1	-.48	3
575		3	max	478.071	3	580.212	2	46.508	1	0	2	-.005	10	.538	1
576			min	-301.822	2	-592.827	3	3.131	10	0	3	-.072	1	-.938	3
577		4	max	478.504	3	578.629	2	46.508	1	0	2	-.003	10	.189	1
578			min	-301.246	2	-594.015	3	3.131	10	0	3	-.044	1	-.57	3
579		5	max	478.936	3	577.045	2	46.508	1	0	2	0	10	-.006	15
580			min	-300.67	2	-595.202	3	3.131	10	0	3	-.023	4	-.201	3
581		6	max	479.368	3	575.462	2	46.508	1	0	2	.014	1	.169	3
582			min	-300.093	2	-596.39	3	3.131	10	0	3	-.011	5	-.552	2
583		7	max	479.8	3	573.879	2	46.508	1	0	2	.043	1	.539	3
584			min	-299.517	2	-597.577	3	3.131	10	0	3	-.001	5	-.908	2
585		8	max	480.232	3	572.296	2	46.508	1	0	2	.072	1	.91	3
586			min	-298.941	2	-598.764	3	3.131	10	0	3	.005	10	-1.264	2
587		9	max	491.414	3	48.238	2	77.879	1	0	3	-.003	10	1.06	3
588			min	-245.049	2	.489	15	5.498	10	0	9	-.13	4	-1.441	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	491.847	3	46.655	2	77.879	1	0	3	0	1	1.038	3
590			min	-244.473	2	.011	15	5.498	10	0	9	-.085	4	-1.47	2
591		11	max	492.279	3	45.072	2	77.879	1	0	3	.049	1	1.016	3
592			min	-243.896	2	-1.891	6	5.498	10	0	9	-.05	5	-1.499	2
593		12	max	503.198	3	401.058	3	143.963	4	0	3	-.005	10	.891	3
594			min	-189.887	2	-674.819	2	3.262	12	0	2	-.229	4	-1.33	2
595		13	max	503.63	3	399.871	3	145.424	4	0	3	-.003	10	.643	3
596			min	-189.311	2	-676.402	2	3.262	12	0	2	-.14	4	-.911	2
597		14	max	504.063	3	398.683	3	146.884	4	0	3	-.001	10	.395	3
598			min	-188.735	2	-677.985	2	3.262	12	0	2	-.049	4	-.491	2
599		15	max	504.495	3	397.496	3	148.344	4	0	3	.043	4	.148	3
600			min	-188.159	2	-679.568	2	3.262	12	0	2	0	12	-.097	1
601		16	max	504.927	3	396.308	3	149.804	4	0	3	.135	4	.353	2
602			min	-187.582	2	-681.152	2	3.262	12	0	2	.003	12	-.098	3
603		17	max	505.359	3	395.121	3	151.264	4	0	3	.229	4	.776	2
604			min	-187.006	2	-682.735	2	3.262	12	0	2	.005	12	-.344	3
605		18	max	-6.532	12	642.325	2	52.559	1	0	2	.211	4	.391	2
606			min	-135.049	1	-293.083	3	-71.299	5	0	3	.007	12	-.17	3
607		19	max	-6.243	12	640.742	2	52.559	1	0	2	.174	4	.012	3
608			min	-134.472	1	-294.271	3	-69.839	5	0	3	.009	12	-.008	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.229	2	.009	3	1.553e-2	2	NC	1	NC	1
2			min	-.552	4	-.067	3	-.006	2	-4.291e-3	3	NC	1	NC	1
3		2	max	0	1	.169	2	.013	1	1.65e-2	2	NC	4	NC	1
4			min	-.552	4	.005	15	-.009	5	-3.832e-3	3	1195.936	3	NC	1
5		3	max	0	1	.198	3	.03	1	1.748e-2	2	NC	5	NC	2
6			min	-.552	4	.003	15	-.012	5	-3.373e-3	3	657.267	3	5629.205	1
7		4	max	0	1	.273	3	.044	1	1.845e-2	2	NC	5	NC	2
8			min	-.552	4	.003	15	-.009	5	-2.914e-3	3	511.747	3	3863.43	1
9		5	max	0	1	.296	3	.051	1	1.943e-2	2	NC	5	NC	2
10			min	-.552	4	.003	15	-.004	5	-2.455e-3	3	479.415	3	3388.815	1
11		6	max	0	1	.267	3	.047	1	2.04e-2	2	NC	5	NC	2
12			min	-.552	4	.004	15	-.004	10	-1.996e-3	3	520.24	3	3629.342	1
13		7	max	0	1	.212	2	.035	1	2.138e-2	2	NC	2	NC	2
14			min	-.552	4	.005	15	-.006	10	-1.538e-3	3	657.042	3	4889.446	1
15		8	max	0	1	.28	2	.027	3	2.235e-2	2	NC	4	NC	2
16			min	-.552	4	.006	15	-.009	10	-1.079e-3	3	1002.255	3	9760.961	14
17		9	max	0	1	.339	2	.027	3	2.333e-2	2	NC	4	NC	1
18			min	-.552	4	.007	15	-.015	2	-6.197e-4	3	1583.044	2	9625.824	3
19		10	max	0	1	.365	2	.028	3	2.431e-2	2	NC	4	NC	1
20			min	-.552	4	-.016	3	-.019	2	-1.608e-4	3	1280.245	2	9556.644	3
21		11	max	0	10	.339	2	.027	3	2.333e-2	2	NC	4	NC	1
22			min	-.552	4	.007	15	-.015	2	-6.197e-4	3	1583.044	2	9625.824	3
23		12	max	0	10	.28	2	.027	3	2.235e-2	2	NC	4	NC	2
24			min	-.552	4	.006	15	-.009	10	-1.079e-3	3	1002.255	3	9839.348	1
25		13	max	0	10	.212	2	.035	1	2.138e-2	2	NC	2	NC	2
26			min	-.552	4	.004	15	-.006	10	-1.538e-3	3	657.042	3	4889.446	1
27		14	max	0	10	.267	3	.047	1	2.04e-2	2	NC	5	NC	2
28			min	-.552	4	.003	15	-.004	10	-1.996e-3	3	520.24	3	3629.342	1
29		15	max	0	10	.296	3	.051	1	1.943e-2	2	NC	5	NC	2
30			min	-.552	4	.002	15	-.002	10	-2.455e-3	3	479.415	3	3388.815	1
31		16	max	0	10	.273	3	.044	1	1.845e-2	2	NC	5	NC	2
32			min	-.552	4	.002	15	-.002	10	-2.914e-3	3	511.747	3	3863.43	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	10	.198	3	.03	1	1.748e-2	2	NC	5	NC	2
34			min	-.552	4	.003	15	-.002	10	-3.373e-3	3	657.267	3	5629.205	1
35		18	max	0	10	.169	2	.014	4	1.65e-2	2	NC	4	NC	1
36			min	-.552	4	.004	15	-.003	10	-3.832e-3	3	1195.936	3	NC	1
37		19	max	0	10	.229	2	.009	3	1.553e-2	2	NC	1	NC	1
38			min	-.552	4	-.067	3	-.006	2	-4.291e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.443	3	.008	3	8.573e-3	2	NC	1	NC	1
40			min	-.427	4	-.667	2	-.005	2	-6.675e-3	3	NC	1	NC	1
41		2	max	0	1	.637	3	.009	3	9.742e-3	2	NC	5	NC	1
42			min	-.427	4	-.871	2	-.014	5	-7.705e-3	3	855.3	2	NC	1
43		3	max	0	1	.81	3	.023	1	1.091e-2	2	NC	5	NC	2
44			min	-.427	4	-1.056	2	-.017	5	-8.735e-3	3	448.159	2	7576.632	1
45		4	max	0	1	.944	3	.036	1	1.208e-2	2	NC	15	NC	2
46			min	-.427	4	-1.208	2	-.013	5	-9.765e-3	3	321.653	2	4780.15	1
47		5	max	0	1	1.033	3	.043	1	1.325e-2	2	NC	15	NC	2
48			min	-.427	4	-1.321	2	-.003	5	-1.079e-2	3	266.204	2	3997.89	1
49		6	max	0	1	1.074	3	.042	1	1.442e-2	2	NC	15	NC	2
50			min	-.427	4	-1.391	2	-.003	10	-1.182e-2	3	240.34	2	4149.558	1
51		7	max	0	1	1.074	3	.031	1	1.559e-2	2	NC	15	NC	2
52			min	-.427	4	-1.423	2	-.005	10	-1.285e-2	3	230.388	2	5458.654	1
53		8	max	0	1	1.044	3	.025	4	1.676e-2	2	NC	15	NC	1
54			min	-.427	4	-1.424	2	-.008	10	-1.388e-2	3	230.062	2	6638.616	4
55		9	max	0	1	1.006	3	.024	3	1.793e-2	2	NC	15	NC	1
56			min	-.427	4	-1.409	2	-.014	2	-1.491e-2	3	234.616	2	9327.632	4
57		10	max	0	1	.986	3	.024	3	1.91e-2	2	NC	15	NC	1
58			min	-.427	4	-1.399	2	-.017	2	-1.594e-2	3	237.948	2	NC	1
59		11	max	0	12	1.006	3	.024	3	1.793e-2	2	NC	15	NC	1
60			min	-.427	4	-1.409	2	-.014	5	-1.491e-2	3	234.616	2	NC	1
61		12	max	0	12	1.044	3	.024	3	1.676e-2	2	NC	15	NC	1
62			min	-.427	4	-1.424	2	-.017	5	-1.388e-2	3	230.062	2	NC	1
63		13	max	0	12	1.074	3	.031	1	1.559e-2	2	NC	15	NC	2
64			min	-.427	4	-1.423	2	-.012	5	-1.285e-2	3	230.388	2	5458.654	1
65		14	max	0	12	1.074	3	.042	1	1.442e-2	2	NC	15	NC	2
66			min	-.427	4	-1.391	2	-.003	10	-1.182e-2	3	240.34	2	4149.558	1
67		15	max	0	12	1.033	3	.043	1	1.325e-2	2	NC	15	NC	2
68			min	-.427	4	-1.321	2	-.002	10	-1.079e-2	3	266.204	2	3997.89	1
69		16	max	0	12	.944	3	.036	1	1.208e-2	2	NC	15	NC	2
70			min	-.427	4	-1.208	2	-.002	10	-9.765e-3	3	321.653	2	4780.15	1
71		17	max	0	12	.81	3	.026	4	1.091e-2	2	NC	5	NC	2
72			min	-.427	4	-1.056	2	-.002	10	-8.735e-3	3	448.159	2	6387.247	4
73		18	max	0	12	.637	3	.017	4	9.742e-3	2	NC	5	NC	1
74			min	-.427	4	-.871	2	-.003	10	-7.705e-3	3	855.3	2	9330.617	4
75		19	max	0	12	.443	3	.008	3	8.573e-3	2	NC	1	NC	1
76			min	-.427	4	-.667	2	-.005	2	-6.675e-3	3	NC	1	NC	1
77	M15	1	max	0	10	.453	3	.008	3	5.642e-3	3	NC	1	NC	1
78			min	-.354	4	-.666	2	-.005	2	-8.869e-3	2	NC	1	NC	1
79		2	max	0	10	.601	3	.009	3	6.495e-3	3	NC	5	NC	1
80			min	-.354	4	-.905	2	-.021	5	-1.008e-2	2	729.398	2	8986.221	5
81		3	max	0	10	.736	3	.023	1	7.348e-3	3	NC	5	NC	2
82			min	-.354	4	-1.118	2	-.027	5	-1.13e-2	2	385.097	2	6902.618	5
83		4	max	0	10	.849	3	.036	1	8.201e-3	3	NC	15	NC	2
84			min	-.354	4	-1.288	2	-.021	5	-1.252e-2	2	279.798	2	4748.094	1
85		5	max	0	10	.934	3	.044	1	9.054e-3	3	NC	15	NC	2
86			min	-.354	4	-1.405	2	-.007	5	-1.373e-2	2	235.553	2	3969.282	1
87		6	max	0	10	.989	3	.042	1	9.907e-3	3	NC	15	NC	2
88			min	-.354	4	-1.466	2	-.003	10	-1.495e-2	2	217.437	2	4113.037	1
89		7	max	0	10	1.017	3	.032	1	1.076e-2	3	NC	15	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.354	4	-1.479	2	-.005	10	-1.616e-2	2	214.165	2	5387.612	1
91		8	max	0	10	1.022	3	.032	4	1.161e-2	3	NC	15	NC	1
92			min	-.354	4	-1.455	2	-.007	10	-1.738e-2	2	220.457	2	5234.272	4
93		9	max	0	10	1.016	3	.023	4	1.247e-2	3	NC	15	NC	1
94			min	-.354	4	-1.419	2	-.013	2	-1.859e-2	2	231.212	2	7084.027	4
95		10	max	0	1	1.01	3	.023	3	1.332e-2	3	NC	15	NC	1
96			min	-.354	4	-1.398	2	-.016	2	-1.981e-2	2	237.653	2	NC	1
97		11	max	0	1	1.016	3	.023	3	1.247e-2	3	NC	15	NC	1
98			min	-.354	4	-1.419	2	-.02	5	-1.859e-2	2	231.212	2	9365.253	5
99		12	max	0	1	1.022	3	.022	3	1.161e-2	3	NC	15	NC	1
100			min	-.354	4	-1.455	2	-.024	5	-1.738e-2	2	220.457	2	7765.692	5
101		13	max	0	1	1.017	3	.032	1	1.076e-2	3	NC	15	NC	2
102			min	-.354	4	-1.479	2	-.017	5	-1.616e-2	2	214.165	2	5387.612	1
103		14	max	0	1	.989	3	.042	1	9.907e-3	3	NC	15	NC	2
104			min	-.354	4	-1.466	2	-.003	10	-1.495e-2	2	217.437	2	4113.037	1
105		15	max	0	1	.934	3	.044	1	9.054e-3	3	NC	15	NC	2
106			min	-.354	4	-1.405	2	-.002	10	-1.373e-2	2	235.553	2	3969.282	1
107		16	max	0	1	.849	3	.036	1	8.201e-3	3	NC	15	NC	2
108			min	-.354	4	-1.288	2	-.001	10	-1.252e-2	2	279.798	2	4748.094	1
109		17	max	0	1	.736	3	.036	4	7.348e-3	3	NC	5	NC	2
110			min	-.354	4	-1.118	2	-.002	10	-1.13e-2	2	385.097	2	4722.633	4
111		18	max	0	1	.601	3	.025	4	6.495e-3	3	NC	5	NC	1
112			min	-.354	4	-.905	2	-.003	10	-1.008e-2	2	729.398	2	6681.288	4
113		19	max	0	1	.453	3	.008	3	5.642e-3	3	NC	1	NC	1
114			min	-.354	4	-.666	2	-.005	2	-8.869e-3	2	NC	1	NC	1
115	M16	1	max	0	12	.204	2	.007	3	1.083e-2	3	NC	1	NC	1
116			min	-.124	4	-.162	3	-.004	2	-1.325e-2	2	NC	1	NC	1
117		2	max	0	12	.115	1	.013	1	1.172e-2	3	NC	4	NC	1
118			min	-.124	4	-.128	3	-.014	5	-1.374e-2	2	1698.857	2	NC	1
119		3	max	0	12	.049	1	.031	1	1.26e-2	3	NC	5	NC	2
120			min	-.124	4	-.104	3	-.019	5	-1.423e-2	2	951.115	2	5621.742	1
121		4	max	0	12	.024	9	.045	1	1.348e-2	3	NC	5	NC	2
122			min	-.124	4	-.096	3	-.016	5	-1.48e-2	1	766.626	2	3837.742	1
123		5	max	0	12	.026	9	.052	1	1.436e-2	3	NC	5	NC	2
124			min	-.124	4	-.108	3	-.008	5	-1.539e-2	1	763.586	2	3346.034	1
125		6	max	0	12	.055	1	.049	1	1.525e-2	3	NC	4	NC	2
126			min	-.124	4	-.138	3	-.002	10	-1.598e-2	1	930.496	2	3551.047	1
127		7	max	0	12	.121	1	.037	1	1.613e-2	3	NC	4	NC	2
128			min	-.124	4	-.182	3	-.004	10	-1.656e-2	1	1530.934	2	4697.488	1
129		8	max	0	12	.2	1	.021	14	1.701e-2	3	NC	1	NC	2
130			min	-.124	4	-.231	3	-.006	10	-1.715e-2	1	2540.393	3	8260.267	4
131		9	max	0	12	.269	1	.02	3	1.789e-2	3	NC	4	NC	1
132			min	-.124	4	-.272	3	-.011	2	-1.774e-2	1	1581.927	3	NC	1
133		10	max	0	1	.299	1	.02	3	1.878e-2	3	NC	5	NC	1
134			min	-.125	4	-.29	3	-.015	2	-1.833e-2	1	1357.465	3	NC	1
135		11	max	0	1	.269	1	.02	3	1.789e-2	3	NC	4	NC	1
136			min	-.124	4	-.272	3	-.011	2	-1.774e-2	1	1581.927	3	NC	1
137		12	max	0	1	.2	1	.019	3	1.701e-2	3	NC	1	NC	2
138			min	-.124	4	-.231	3	-.011	5	-1.715e-2	1	2540.393	3	8930.85	1
139		13	max	0	1	.121	1	.037	1	1.613e-2	3	NC	4	NC	2
140			min	-.124	4	-.182	3	-.005	5	-1.656e-2	1	1530.934	2	4697.488	1
141		14	max	0	1	.055	1	.049	1	1.525e-2	3	NC	4	NC	2
142			min	-.124	4	-.138	3	-.002	10	-1.598e-2	1	930.496	2	3551.047	1
143		15	max	0	1	.026	9	.052	1	1.436e-2	3	NC	5	NC	2
144			min	-.124	4	-.108	3	0	10	-1.539e-2	1	763.586	2	3346.034	1
145		16	max	0	1	.024	9	.045	1	1.348e-2	3	NC	5	NC	2
146			min	-.124	4	-.096	3	0	10	-1.48e-2	1	766.626	2	3837.742	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.049	1	.031	1	1.26e-2	3	NC	5	NC	2
148			min	-.124	4	-.104	3	0	10	-1.423e-2	2	951.115	2	5594.806	4
149		18	max	0	1	.115	1	.02	4	1.172e-2	3	NC	4	NC	1
150			min	-.124	4	-.128	3	-.002	10	-1.374e-2	2	1698.857	2	8440.653	4
151		19	max	0	1	.204	2	.007	3	1.083e-2	3	NC	1	NC	1
152			min	-.124	4	-.162	3	-.004	2	-1.325e-2	2	NC	1	NC	1
153	M2	1	max	.006	2	.008	2	.006	1	2.107e-3	5	NC	1	NC	2
154			min	-.008	3	-.013	3	-.522	4	-1.315e-4	1	7464.909	2	116.082	4
155		2	max	.006	2	.007	2	.006	1	2.106e-3	5	NC	1	NC	1
156			min	-.008	3	-.012	3	-.479	4	-1.233e-4	1	8563.978	2	126.49	4
157		3	max	.006	2	.006	2	.005	1	2.105e-3	5	NC	1	NC	1
158			min	-.007	3	-.012	3	-.436	4	-1.15e-4	1	NC	1	138.869	4
159		4	max	.005	2	.005	2	.005	1	2.104e-3	5	NC	1	NC	1
160			min	-.007	3	-.011	3	-.394	4	-1.067e-4	1	NC	1	153.735	4
161		5	max	.005	2	.004	2	.004	1	2.103e-3	5	NC	1	NC	1
162			min	-.006	3	-.011	3	-.353	4	-9.845e-5	1	NC	1	171.796	4
163		6	max	.005	2	.003	2	.004	1	2.102e-3	5	NC	1	NC	1
164			min	-.006	3	-.01	3	-.312	4	-9.018e-5	1	NC	1	194.033	4
165		7	max	.004	2	.002	2	.003	1	2.103e-3	4	NC	1	NC	1
166			min	-.006	3	-.01	3	-.273	4	-8.191e-5	1	NC	1	221.84	4
167		8	max	.004	2	.001	2	.003	1	2.105e-3	4	NC	1	NC	1
168			min	-.005	3	-.009	3	-.235	4	-7.364e-5	1	NC	1	257.261	4
169		9	max	.004	2	0	2	.002	1	2.106e-3	4	NC	1	NC	1
170			min	-.005	3	-.009	3	-.2	4	-6.537e-5	1	NC	1	303.384	4
171		10	max	.003	2	0	2	.002	1	2.107e-3	4	NC	1	NC	1
172			min	-.004	3	-.008	3	-.166	4	-5.71e-5	1	NC	1	365.06	4
173		11	max	.003	2	0	2	.002	1	2.108e-3	4	NC	1	NC	1
174			min	-.004	3	-.007	3	-.135	4	-4.883e-5	1	NC	1	450.268	4
175		12	max	.002	2	0	15	.001	1	2.109e-3	4	NC	1	NC	1
176			min	-.003	3	-.007	3	-.106	4	-4.056e-5	1	NC	1	572.914	4
177		13	max	.002	2	0	15	0	1	2.11e-3	4	NC	1	NC	1
178			min	-.003	3	-.006	3	-.08	4	-3.229e-5	1	NC	1	759.049	4
179		14	max	.002	2	0	15	0	1	2.112e-3	4	NC	1	NC	1
180			min	-.002	3	-.005	3	-.057	4	-2.402e-5	1	NC	1	1062.316	4
181		15	max	.001	2	0	15	0	1	2.113e-3	4	NC	1	NC	1
182			min	-.002	3	-.004	3	-.038	4	-1.575e-5	1	NC	1	1608.457	4
183		16	max	.001	2	0	15	0	1	2.114e-3	4	NC	1	NC	1
184			min	-.001	3	-.003	3	-.022	4	-7.485e-6	1	NC	1	2753.774	4
185		17	max	0	2	0	15	0	1	2.115e-3	4	NC	1	NC	1
186			min	0	3	-.002	3	-.01	4	-9.852e-7	3	NC	1	5874.591	4
187		18	max	0	2	0	15	0	1	2.116e-3	4	NC	1	NC	1
188			min	0	3	-.001	3	-.003	4	1.177e-7	12	NC	1	NC	1
189		19	max	0	1	0	1	0	1	2.117e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	8.513e-7	12	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	-3.099e-7	12	NC	1	NC	1
192			min	0	1	0	1	0	1	-4.1e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.012	4	1.625e-4	4	NC	1	NC	1
194			min	0	2	-.002	6	0	12	8.773e-7	12	NC	1	NC	1
195		3	max	0	3	-.001	15	.023	4	7.349e-4	4	NC	1	NC	1
196			min	0	2	-.005	6	0	12	2.064e-6	12	NC	1	NC	1
197		4	max	.001	3	-.002	15	.034	4	1.307e-3	4	NC	1	NC	1
198			min	0	2	-.008	6	0	12	3.252e-6	12	NC	1	NC	1
199		5	max	.002	3	-.002	15	.045	4	1.88e-3	4	NC	1	NC	1
200			min	-.001	2	-.011	6	0	12	4.439e-6	12	9491.893	6	NC	1
201		6	max	.002	3	-.003	15	.055	4	2.452e-3	4	NC	1	NC	1
202			min	-.002	2	-.013	6	0	12	5.626e-6	12	7600.834	6	NC	1
203		7	max	.002	3	-.003	15	.065	4	3.025e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.002	2	-.016	6	0	12	6.813e-6	12	6467.399	6	NC	1
205		8	max	.003	3	-.004	15	.074	4	3.597e-3	4	NC	5	NC	1
206			min	-.002	2	-.018	6	0	12	8.e-6	12	5767.734	6	NC	1
207		9	max	.003	3	-.004	15	.083	4	4.17e-3	4	NC	5	NC	1
208			min	-.003	2	-.019	6	0	12	9.188e-6	12	5349.885	6	NC	1
209		10	max	.004	3	-.004	15	.092	4	4.742e-3	4	NC	5	NC	1
210			min	-.003	2	-.02	6	0	12	1.037e-5	12	5139.706	6	NC	1
211		11	max	.004	3	-.004	15	.101	4	5.315e-3	4	NC	5	NC	1
212			min	-.003	2	-.02	6	0	12	1.156e-5	12	5105.726	6	NC	1
213		12	max	.004	3	-.004	15	.109	4	5.887e-3	4	NC	5	NC	1
214			min	-.004	2	-.02	6	0	12	1.275e-5	12	5246.998	6	NC	1
215		13	max	.005	3	-.004	15	.117	4	6.46e-3	4	NC	5	NC	1
216			min	-.004	2	-.018	6	0	12	1.394e-5	12	5594.218	6	NC	1
217		14	max	.005	3	-.004	15	.125	4	7.032e-3	4	NC	5	NC	1
218			min	-.004	2	-.016	6	0	12	1.512e-5	12	6226.066	6	NC	1
219		15	max	.006	3	-.003	15	.134	4	7.604e-3	4	NC	2	NC	1
220			min	-.005	2	-.014	6	0	12	1.631e-5	12	7318.593	6	NC	1
221		16	max	.006	3	-.002	15	.142	4	8.177e-3	4	NC	1	NC	1
222			min	-.005	2	-.011	6	0	12	1.75e-5	12	9299.452	6	NC	1
223		17	max	.006	3	-.001	15	.151	4	8.749e-3	4	NC	1	NC	1
224			min	-.005	2	-.008	1	0	12	1.869e-5	12	NC	1	NC	1
225		18	max	.007	3	0	15	.161	4	9.322e-3	4	NC	1	NC	1
226			min	-.006	2	-.005	1	0	12	1.987e-5	12	NC	1	NC	1
227		19	max	.007	3	0	5	.172	4	9.894e-3	4	NC	1	NC	1
228			min	-.006	2	-.002	1	0	12	2.106e-5	12	NC	1	NC	1
229	M4	1	max	.003	1	.005	2	0	12	5.201e-5	1	NC	1	NC	2
230			min	0	3	-.007	3	-.172	4	-5.171e-4	5	NC	1	144.424	4
231		2	max	.003	1	.005	2	0	12	5.201e-5	1	NC	1	NC	2
232			min	0	3	-.007	3	-.158	4	-5.171e-4	5	NC	1	157.205	4
233		3	max	.002	1	.005	2	0	12	5.201e-5	1	NC	1	NC	2
234			min	0	3	-.007	3	-.144	4	-5.171e-4	5	NC	1	172.405	4
235		4	max	.002	1	.005	2	0	12	5.201e-5	1	NC	1	NC	2
236			min	0	3	-.006	3	-.13	4	-5.171e-4	5	NC	1	190.656	4
237		5	max	.002	1	.004	2	0	12	5.201e-5	1	NC	1	NC	2
238			min	0	3	-.006	3	-.117	4	-5.171e-4	5	NC	1	212.814	4
239		6	max	.002	1	.004	2	0	12	5.201e-5	1	NC	1	NC	2
240			min	0	3	-.005	3	-.103	4	-5.171e-4	5	NC	1	240.067	4
241		7	max	.002	1	.004	2	0	12	5.201e-5	1	NC	1	NC	2
242			min	0	3	-.005	3	-.09	4	-5.171e-4	5	NC	1	274.1	4
243		8	max	.002	1	.003	2	0	12	5.201e-5	1	NC	1	NC	2
244			min	0	3	-.004	3	-.078	4	-5.171e-4	5	NC	1	317.373	4
245		9	max	.001	1	.003	2	0	12	5.201e-5	1	NC	1	NC	1
246			min	0	3	-.004	3	-.066	4	-5.171e-4	5	NC	1	373.588	4
247		10	max	.001	1	.003	2	0	12	5.201e-5	1	NC	1	NC	1
248			min	0	3	-.004	3	-.055	4	-5.171e-4	5	NC	1	448.532	4
249		11	max	.001	1	.002	2	0	12	5.201e-5	1	NC	1	NC	1
250			min	0	3	-.003	3	-.045	4	-5.171e-4	5	NC	1	551.675	4
251		12	max	.001	1	.002	2	0	12	5.201e-5	1	NC	1	NC	1
252			min	0	3	-.003	3	-.035	4	-5.171e-4	5	NC	1	699.4	4
253		13	max	0	1	.002	2	0	12	5.201e-5	1	NC	1	NC	1
254			min	0	3	-.002	3	-.027	4	-5.171e-4	5	NC	1	922.116	4
255		14	max	0	1	.002	2	0	12	5.201e-5	1	NC	1	NC	1
256			min	0	3	-.002	3	-.019	4	-5.171e-4	5	NC	1	1281.699	4
257		15	max	0	1	.001	2	0	12	5.201e-5	1	NC	1	NC	1
258			min	0	3	-.002	3	-.013	4	-5.171e-4	5	NC	1	1920.807	4
259		16	max	0	1	0	2	0	12	5.201e-5	1	NC	1	NC	1
260			min	0	3	-.001	3	-.008	4	-5.171e-4	5	NC	1	3233.878	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	5.201e-5	1	NC	1	NC	1
262			min	0	3	0	3	-.004	4	-5.171e-4	5	NC	1	6683.805	4
263		18	max	0	1	0	2	0	12	5.201e-5	1	NC	1	NC	1
264			min	0	3	0	3	-.001	4	-5.171e-4	5	NC	1	NC	1
265		19	max	0	1	0	1	0	1	5.201e-5	1	NC	1	NC	1
266			min	0	1	0	1	0	1	-5.171e-4	5	NC	1	NC	1
267	M6	1	max	.019	2	.027	2	0	1	2.186e-3	4	NC	3	NC	1
268			min	-.026	3	-.038	3	-.527	4	0	1	2258.288	2	114.98	4
269		2	max	.018	2	.025	2	0	1	2.183e-3	4	NC	3	NC	1
270			min	-.024	3	-.036	3	-.483	4	0	1	2468.427	2	125.29	4
271		3	max	.017	2	.022	2	0	1	2.179e-3	4	NC	3	NC	1
272			min	-.023	3	-.034	3	-.44	4	0	1	2719.867	2	137.552	4
273		4	max	.016	2	.02	2	0	1	2.176e-3	4	NC	3	NC	1
274			min	-.021	3	-.032	3	-.398	4	0	1	3023.845	2	152.279	4
275		5	max	.015	2	.018	2	0	1	2.173e-3	4	NC	3	NC	1
276			min	-.02	3	-.03	3	-.356	4	0	1	3395.817	2	170.17	4
277		6	max	.014	2	.016	2	0	1	2.17e-3	4	NC	3	NC	1
278			min	-.019	3	-.028	3	-.315	4	0	1	3857.512	2	192.197	4
279		7	max	.013	2	.014	2	0	1	2.166e-3	4	NC	3	NC	1
280			min	-.017	3	-.025	3	-.276	4	0	1	4440.267	2	219.743	4
281		8	max	.012	2	.012	2	0	1	2.163e-3	4	NC	1	NC	1
282			min	-.016	3	-.023	3	-.238	4	0	1	5190.646	2	254.832	4
283		9	max	.011	2	.01	2	0	1	2.16e-3	4	NC	1	NC	1
284			min	-.014	3	-.021	3	-.202	4	0	1	6180.312	2	300.523	4
285		10	max	.01	2	.008	2	0	1	2.156e-3	4	NC	1	NC	1
286			min	-.013	3	-.019	3	-.167	4	0	1	7524.299	2	361.621	4
287		11	max	.008	2	.006	2	0	1	2.153e-3	4	NC	1	NC	1
288			min	-.011	3	-.017	3	-.136	4	0	1	9417.007	2	446.032	4
289		12	max	.007	2	.005	2	0	1	2.15e-3	4	NC	1	NC	1
290			min	-.01	3	-.015	3	-.107	4	0	1	NC	1	567.532	4
291		13	max	.006	2	.004	2	0	1	2.147e-3	4	NC	1	NC	1
292			min	-.009	3	-.013	3	-.081	4	0	1	NC	1	751.93	4
293		14	max	.005	2	.003	2	0	1	2.143e-3	4	NC	1	NC	1
294			min	-.007	3	-.011	3	-.058	4	0	1	NC	1	1052.37	4
295		15	max	.004	2	.002	2	0	1	2.14e-3	4	NC	1	NC	1
296			min	-.006	3	-.008	3	-.038	4	0	1	NC	1	1593.433	4
297		16	max	.003	2	0	2	0	1	2.137e-3	4	NC	1	NC	1
298			min	-.004	3	-.006	3	-.022	4	0	1	NC	1	2728.127	4
299		17	max	.002	2	0	2	0	1	2.134e-3	4	NC	1	NC	1
300			min	-.003	3	-.004	3	-.01	4	0	1	NC	1	5820.132	4
301		18	max	.001	2	0	2	0	1	2.13e-3	4	NC	1	NC	1
302			min	-.001	3	-.002	3	-.003	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	2.127e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-4.114e-4	4	NC	1	NC	1
307		2	max	.001	3	0	2	.012	4	1.463e-4	4	NC	1	NC	1
308			min	-.001	2	-.004	3	0	1	0	1	NC	1	NC	1
309		3	max	.002	3	-.001	15	.023	4	7.04e-4	4	NC	1	NC	1
310			min	-.002	2	-.007	3	0	1	0	1	NC	1	NC	1
311		4	max	.004	3	-.002	15	.034	4	1.262e-3	4	NC	1	NC	1
312			min	-.003	2	-.01	3	0	1	0	1	NC	1	NC	1
313		5	max	.005	3	-.003	15	.045	4	1.819e-3	4	NC	1	NC	1
314			min	-.004	2	-.013	3	0	1	0	1	8276.466	3	NC	1
315		6	max	.006	3	-.003	15	.055	4	2.377e-3	4	NC	1	NC	1
316			min	-.005	2	-.016	3	0	1	0	1	6967.833	3	NC	1
317		7	max	.007	3	-.004	15	.065	4	2.935e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.007	2	-.018	3	0	1	0	1	6180.997	3	NC	1
319		8	max	.008	3	-.004	15	.074	4	3.493e-3	4	NC	2	NC	1
320			min	-.008	2	-.019	3	0	1	0	1	5709.011	3	NC	1
321		9	max	.01	3	-.005	15	.083	4	4.05e-3	4	NC	2	NC	1
322			min	-.009	2	-.02	3	0	1	0	1	5340.636	4	NC	1
323		10	max	.011	3	-.005	15	.092	4	4.608e-3	4	NC	2	NC	1
324			min	-.01	2	-.021	3	0	1	0	1	5131.37	4	NC	1
325		11	max	.012	3	-.005	15	.1	4	5.166e-3	4	NC	5	NC	1
326			min	-.011	2	-.021	4	0	1	0	1	5097.902	4	NC	1
327		12	max	.013	3	-.005	15	.108	4	5.723e-3	4	NC	5	NC	1
328			min	-.012	2	-.02	4	0	1	0	1	5239.35	4	NC	1
329		13	max	.014	3	-.004	15	.116	4	6.281e-3	4	NC	2	NC	1
330			min	-.013	2	-.019	4	0	1	0	1	5586.414	4	NC	1
331		14	max	.016	3	-.004	15	.124	4	6.839e-3	4	NC	2	NC	1
332			min	-.014	2	-.017	4	0	1	0	1	6217.702	4	NC	1
333		15	max	.017	3	-.003	15	.131	4	7.396e-3	4	NC	1	NC	1
334			min	-.015	2	-.015	4	0	1	0	1	7309.069	4	NC	1
335		16	max	.018	3	-.003	15	.139	4	7.954e-3	4	NC	1	NC	1
336			min	-.016	2	-.012	3	0	1	0	1	9287.657	4	NC	1
337		17	max	.019	3	-.002	15	.148	4	8.512e-3	4	NC	1	NC	1
338			min	-.017	2	-.009	3	0	1	0	1	NC	1	NC	1
339		18	max	.02	3	-.001	15	.157	4	9.07e-3	4	NC	1	NC	1
340			min	-.018	2	-.007	1	0	1	0	1	NC	1	NC	1
341		19	max	.021	3	0	15	.166	4	9.627e-3	4	NC	1	NC	1
342			min	-.02	2	-.005	1	0	1	0	1	NC	1	NC	1
343	M8	1	max	.007	2	.018	2	0	1	0	1	NC	1	NC	1
344			min	-.002	3	-.022	3	-.166	4	-6.107e-4	4	NC	1	149.008	4
345		2	max	.007	2	.017	2	0	1	0	1	NC	1	NC	1
346			min	-.002	3	-.02	3	-.153	4	-6.107e-4	4	NC	1	162.206	4
347		3	max	.007	2	.016	2	0	1	0	1	NC	1	NC	1
348			min	-.002	3	-.019	3	-.139	4	-6.107e-4	4	NC	1	177.903	4
349		4	max	.006	2	.015	2	0	1	0	1	NC	1	NC	1
350			min	-.002	3	-.018	3	-.126	4	-6.107e-4	4	NC	1	196.749	4
351		5	max	.006	2	.014	2	0	1	0	1	NC	1	NC	1
352			min	-.002	3	-.017	3	-.113	4	-6.107e-4	4	NC	1	219.628	4
353		6	max	.005	2	.013	2	0	1	0	1	NC	1	NC	1
354			min	-.002	3	-.016	3	-.1	4	-6.107e-4	4	NC	1	247.768	4
355		7	max	.005	2	.012	2	0	1	0	1	NC	1	NC	1
356			min	-.001	3	-.014	3	-.088	4	-6.107e-4	4	NC	1	282.909	4
357		8	max	.005	2	.011	2	0	1	0	1	NC	1	NC	1
358			min	-.001	3	-.013	3	-.076	4	-6.107e-4	4	NC	1	327.59	4
359		9	max	.004	2	.01	2	0	1	0	1	NC	1	NC	1
360			min	-.001	3	-.012	3	-.064	4	-6.107e-4	4	NC	1	385.633	4
361		10	max	.004	2	.009	2	0	1	0	1	NC	1	NC	1
362			min	-.001	3	-.011	3	-.054	4	-6.107e-4	4	NC	1	463.017	4
363		11	max	.003	2	.008	2	0	1	0	1	NC	1	NC	1
364			min	0	3	-.01	3	-.044	4	-6.107e-4	4	NC	1	569.518	4
365		12	max	.003	2	.007	2	0	1	0	1	NC	1	NC	1
366			min	0	3	-.008	3	-.034	4	-6.107e-4	4	NC	1	722.052	4
367		13	max	.002	2	.006	2	0	1	0	1	NC	1	NC	1
368			min	0	3	-.007	3	-.026	4	-6.107e-4	4	NC	1	952.024	4
369		14	max	.002	2	.005	2	0	1	0	1	NC	1	NC	1
370			min	0	3	-.006	3	-.019	4	-6.107e-4	4	NC	1	1323.327	4
371		15	max	.002	2	.004	2	0	1	0	1	NC	1	NC	1
372			min	0	3	-.005	3	-.013	4	-6.107e-4	4	NC	1	1983.28	4
373		16	max	.001	2	.003	2	0	1	0	1	NC	1	NC	1
374			min	0	3	-.004	3	-.007	4	-6.107e-4	4	NC	1	3339.213	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	2	.002	2	0	1	0	1	NC	1	NC	1
376			min	0	3	-.002	3	-.004	4	-6.107e-4	4	NC	1	6901.886	4
377		18	max	0	2	.001	2	0	1	0	1	NC	1	NC	1
378			min	0	3	-.001	3	-.001	4	-6.107e-4	4	NC	1	NC	1
379		19	max	0	1	0	1	0	1	0	1	NC	1	NC	1
380			min	0	1	0	1	0	1	-6.107e-4	4	NC	1	NC	1
381	M10	1	max	.006	2	.008	2	0	10	2.167e-3	4	NC	1	NC	2
382			min	-.008	3	-.013	3	-.525	4	8.241e-6	10	7464.909	2	115.36	4
383		2	max	.006	2	.007	2	0	10	2.164e-3	4	NC	1	NC	1
384			min	-.008	3	-.012	3	-.482	4	7.703e-6	10	8563.978	2	125.703	4
385		3	max	.006	2	.006	2	0	10	2.161e-3	4	NC	1	NC	1
386			min	-.007	3	-.012	3	-.439	4	7.165e-6	10	NC	1	138.005	4
387		4	max	.005	2	.005	2	0	10	2.157e-3	4	NC	1	NC	1
388			min	-.007	3	-.011	3	-.396	4	6.627e-6	10	NC	1	152.78	4
389		5	max	.005	2	.004	2	0	10	2.154e-3	4	NC	1	NC	1
390			min	-.006	3	-.011	3	-.355	4	6.089e-6	10	NC	1	170.73	4
391		6	max	.005	2	.003	2	0	10	2.151e-3	4	NC	1	NC	1
392			min	-.006	3	-.01	3	-.314	4	5.551e-6	10	NC	1	192.83	4
393		7	max	.004	2	.002	2	0	10	2.148e-3	4	NC	1	NC	1
394			min	-.006	3	-.01	3	-.275	4	5.012e-6	10	NC	1	220.466	4
395		8	max	.004	2	.001	2	0	10	2.144e-3	4	NC	1	NC	1
396			min	-.005	3	-.009	3	-.237	4	4.474e-6	10	NC	1	255.671	4
397		9	max	.004	2	0	2	0	10	2.141e-3	4	NC	1	NC	1
398			min	-.005	3	-.009	3	-.201	4	3.936e-6	10	NC	1	301.512	4
399		10	max	.003	2	0	2	0	10	2.138e-3	4	NC	1	NC	1
400			min	-.004	3	-.008	3	-.167	4	3.398e-6	10	NC	1	362.81	4
401		11	max	.003	2	0	2	0	10	2.134e-3	4	NC	1	NC	1
402			min	-.004	3	-.007	3	-.135	4	2.86e-6	10	NC	1	447.499	4
403		12	max	.002	2	0	2	0	10	2.131e-3	4	NC	1	NC	1
404			min	-.003	3	-.007	3	-.106	4	2.322e-6	10	NC	1	569.399	4
405		13	max	.002	2	-.001	2	0	10	2.128e-3	4	NC	1	NC	1
406			min	-.003	3	-.006	3	-.08	4	1.784e-6	10	NC	1	754.406	4
407		14	max	.002	2	-.001	15	0	10	2.124e-3	4	NC	1	NC	1
408			min	-.002	3	-.005	3	-.057	4	1.245e-6	10	NC	1	1055.84	4
409		15	max	.001	2	-.001	15	0	10	2.121e-3	4	NC	1	NC	1
410			min	-.002	3	-.004	3	-.038	4	7.073e-7	10	NC	1	1598.7	4
411		16	max	.001	2	0	15	0	10	2.118e-3	4	NC	1	NC	1
412			min	-.001	3	-.003	3	-.022	4	1.692e-7	10	NC	1	2737.191	4
413		17	max	0	2	0	15	0	10	2.114e-3	4	NC	1	NC	1
414			min	0	3	-.002	4	-.01	4	-7.842e-7	1	NC	1	5839.674	4
415		18	max	0	2	0	15	0	10	2.111e-3	4	NC	1	NC	1
416			min	0	3	-.001	4	-.003	4	-9.054e-6	1	NC	1	NC	1
417		19	max	0	1	0	1	0	1	2.108e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	-1.732e-5	1	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	5.398e-6	1	NC	1	NC	1
420			min	0	1	0	1	0	1	-4.07e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.012	4	1.56e-4	4	NC	1	NC	1
422			min	0	2	-.003	4	0	1	-1.211e-5	1	NC	1	NC	1
423		3	max	0	3	-.001	15	.023	4	7.19e-4	4	NC	1	NC	1
424			min	0	2	-.006	4	0	1	-2.962e-5	1	NC	1	NC	1
425		4	max	.001	3	-.002	15	.034	4	1.282e-3	4	NC	1	NC	1
426			min	0	2	-.009	4	0	1	-4.713e-5	1	NC	1	NC	1
427		5	max	.002	3	-.003	15	.045	4	1.845e-3	4	NC	1	NC	1
428			min	-.001	2	-.012	4	0	1	-6.464e-5	1	9029.695	4	NC	1
429		6	max	.002	3	-.004	15	.055	4	2.408e-3	4	NC	1	NC	1
430			min	-.002	2	-.014	4	0	1	-8.215e-5	1	7265.952	4	NC	1
431		7	max	.002	3	-.004	15	.064	4	2.971e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.002	2	-.017	4	0	1	-9.967e-5	1	6206.487	4	NC	1
433		8	max	.003	3	-.005	15	.074	4	3.534e-3	4	NC	5	NC	1
434			min	-.002	2	-.019	4	0	1	-1.172e-4	1	5552.531	4	NC	1
435		9	max	.003	3	-.005	15	.083	4	4.097e-3	4	NC	5	NC	1
436			min	-.003	2	-.02	4	-.001	1	-1.347e-4	1	5163.67	4	NC	1
437		10	max	.004	3	-.005	15	.091	4	4.66e-3	4	NC	5	NC	1
438			min	-.003	2	-.021	4	-.001	1	-1.522e-4	1	4971.538	4	NC	1
439		11	max	.004	3	-.005	15	.1	4	5.223e-3	4	NC	5	NC	1
440			min	-.003	2	-.021	4	-.002	1	-1.697e-4	1	4947.608	4	NC	1
441		12	max	.004	3	-.005	15	.108	4	5.786e-3	4	NC	5	NC	1
442			min	-.004	2	-.021	4	-.002	1	-1.872e-4	1	5092.219	4	NC	1
443		13	max	.005	3	-.005	15	.116	4	6.349e-3	4	NC	5	NC	1
444			min	-.004	2	-.02	4	-.002	1	-2.047e-4	1	5436.082	4	NC	1
445		14	max	.005	3	-.004	15	.124	4	6.912e-3	4	NC	5	NC	1
446			min	-.004	2	-.018	4	-.003	1	-2.222e-4	1	6056.424	4	NC	1
447		15	max	.006	3	-.004	15	.132	4	7.475e-3	4	NC	2	NC	1
448			min	-.005	2	-.015	4	-.003	1	-2.397e-4	1	7125.262	4	NC	1
449		16	max	.006	3	-.003	15	.14	4	8.038e-3	4	NC	1	NC	1
450			min	-.005	2	-.012	4	-.004	1	-2.573e-4	1	9059.859	4	NC	1
451		17	max	.006	3	-.002	15	.149	4	8.601e-3	4	NC	1	NC	1
452			min	-.005	2	-.009	4	-.004	1	-2.748e-4	1	NC	1	NC	1
453		18	max	.007	3	-.001	15	.158	4	9.164e-3	4	NC	1	NC	1
454			min	-.006	2	-.005	4	-.005	1	-2.923e-4	1	NC	1	NC	1
455		19	max	.007	3	0	10	.169	4	9.727e-3	4	NC	1	NC	1
456			min	-.006	2	-.002	1	-.006	1	-3.098e-4	1	NC	1	NC	1
457	M12	1	max	.003	1	.005	2	.006	1	-3.624e-6	10	NC	1	NC	2
458			min	0	3	-.007	3	-.169	4	-5.372e-4	4	NC	1	147.068	4
459		2	max	.003	1	.005	2	.005	1	-3.624e-6	10	NC	1	NC	2
460			min	0	3	-.007	3	-.155	4	-5.372e-4	4	NC	1	160.085	4
461		3	max	.002	1	.005	2	.005	1	-3.624e-6	10	NC	1	NC	2
462			min	0	3	-.007	3	-.141	4	-5.372e-4	4	NC	1	175.567	4
463		4	max	.002	1	.005	2	.004	1	-3.624e-6	10	NC	1	NC	2
464			min	0	3	-.006	3	-.128	4	-5.372e-4	4	NC	1	194.155	4
465		5	max	.002	1	.004	2	.004	1	-3.624e-6	10	NC	1	NC	2
466			min	0	3	-.006	3	-.114	4	-5.372e-4	4	NC	1	216.723	4
467		6	max	.002	1	.004	2	.003	1	-3.624e-6	10	NC	1	NC	2
468			min	0	3	-.005	3	-.101	4	-5.372e-4	4	NC	1	244.479	4
469		7	max	.002	1	.004	2	.003	1	-3.624e-6	10	NC	1	NC	2
470			min	0	3	-.005	3	-.089	4	-5.372e-4	4	NC	1	279.141	4
471		8	max	.002	1	.003	2	.003	1	-3.624e-6	10	NC	1	NC	2
472			min	0	3	-.004	3	-.077	4	-5.372e-4	4	NC	1	323.213	4
473		9	max	.001	1	.003	2	.002	1	-3.624e-6	10	NC	1	NC	1
474			min	0	3	-.004	3	-.065	4	-5.372e-4	4	NC	1	380.467	4
475		10	max	.001	1	.003	2	.002	1	-3.624e-6	10	NC	1	NC	1
476			min	0	3	-.004	3	-.054	4	-5.372e-4	4	NC	1	456.795	4
477		11	max	.001	1	.002	2	.002	1	-3.624e-6	10	NC	1	NC	1
478			min	0	3	-.003	3	-.044	4	-5.372e-4	4	NC	1	561.844	4
479		12	max	.001	1	.002	2	.001	1	-3.624e-6	10	NC	1	NC	1
480			min	0	3	-.003	3	-.035	4	-5.372e-4	4	NC	1	712.298	4
481		13	max	0	1	.002	2	0	1	-3.624e-6	10	NC	1	NC	1
482			min	0	3	-.002	3	-.026	4	-5.372e-4	4	NC	1	939.13	4
483		14	max	0	1	.002	2	0	1	-3.624e-6	10	NC	1	NC	1
484			min	0	3	-.002	3	-.019	4	-5.372e-4	4	NC	1	1305.36	4
485		15	max	0	1	.001	2	0	1	-3.624e-6	10	NC	1	NC	1
486			min	0	3	-.002	3	-.013	4	-5.372e-4	4	NC	1	1956.283	4
487		16	max	0	1	0	2	0	1	-3.624e-6	10	NC	1	NC	1
488			min	0	3	-.001	3	-.008	4	-5.372e-4	4	NC	1	3293.636	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	-3.624e-6	10	NC	1	NC	1
490			min	0	3	0	3	-.004	4	-5.372e-4	4	NC	1	6807.388	4
491		18	max	0	1	0	2	0	1	-3.624e-6	10	NC	1	NC	1
492			min	0	3	0	3	-.001	4	-5.372e-4	4	NC	1	NC	1
493		19	max	0	1	0	1	0	1	-3.624e-6	10	NC	1	NC	1
494			min	0	1	0	1	0	1	-5.372e-4	4	NC	1	NC	1
495	M1	1	max	.009	3	.229	2	.552	4	6.97e-3	1	NC	1	NC	1
496			min	-.006	2	-.067	3	0	10	-1.561e-2	3	NC	1	NC	1
497		2	max	.009	3	.112	2	.537	4	7.025e-3	4	NC	5	NC	1
498			min	-.006	2	-.034	3	-.004	1	-7.748e-3	3	1167.024	2	NC	1
499		3	max	.009	3	.013	3	.521	4	1.271e-2	4	NC	5	NC	1
500			min	-.006	2	-.011	2	-.006	1	-1.159e-4	1	565.737	2	7559.307	5
501		4	max	.009	3	.083	3	.505	4	1.097e-2	4	NC	15	NC	1
502			min	-.005	2	-.147	2	-.006	1	-3.883e-3	3	360.568	2	5373.849	5
503		5	max	.009	3	.17	3	.488	4	9.231e-3	4	NC	15	NC	1
504			min	-.005	2	-.288	2	-.004	1	-7.673e-3	3	262.251	2	4254.868	5
505		6	max	.009	3	.261	3	.471	4	1.19e-2	2	8355.187	15	NC	1
506			min	-.005	2	-.423	2	-.002	1	-1.146e-2	3	207.774	2	3570.201	5
507		7	max	.009	3	.348	3	.453	4	1.586e-2	2	7071.264	15	NC	1
508			min	-.005	2	-.543	2	0	3	-1.525e-2	3	175.47	2	3094.437	4
509		8	max	.008	3	.42	3	.435	4	1.983e-2	2	6309.737	15	NC	1
510			min	-.005	2	-.639	2	0	12	-1.904e-2	3	156.304	2	2738.445	4
511		9	max	.008	3	.467	3	.416	4	2.212e-2	2	5910.404	15	NC	1
512			min	-.005	2	-.699	2	0	1	-1.962e-2	3	146.294	2	2498.294	4
513		10	max	.008	3	.485	3	.394	4	2.33e-2	2	5788.118	15	NC	1
514			min	-.005	2	-.719	2	0	10	-1.805e-2	3	143.357	2	2415.121	4
515		11	max	.008	3	.474	3	.369	4	2.448e-2	2	5910.13	15	NC	1
516			min	-.005	2	-.698	2	0	10	-1.648e-2	3	146.787	2	2445.567	4
517		12	max	.008	3	.434	3	.343	4	2.333e-2	2	6309.079	15	NC	1
518			min	-.005	2	-.636	2	0	1	-1.438e-2	3	157.74	2	2590.536	4
519		13	max	.007	3	.37	3	.311	4	1.871e-2	2	7069.974	15	NC	1
520			min	-.005	2	-.537	2	0	1	-1.151e-2	3	178.836	2	3054.026	4
521		14	max	.007	3	.288	3	.276	4	1.408e-2	2	8352.829	15	NC	1
522			min	-.004	2	-.413	2	0	12	-8.635e-3	3	214.772	2	4114.646	4
523		15	max	.007	3	.196	3	.239	4	9.454e-3	2	NC	15	NC	1
524			min	-.004	2	-.276	2	0	12	-5.762e-3	3	276.298	2	6685.736	4
525		16	max	.007	3	.099	3	.204	4	8.166e-3	4	NC	15	NC	1
526			min	-.004	2	-.136	2	0	12	-2.889e-3	3	389.387	2	NC	1
527		17	max	.007	3	.005	3	.172	4	9.27e-3	4	NC	5	NC	1
528			min	-.004	2	-.006	2	0	12	-1.534e-5	3	629.043	2	NC	1
529		18	max	.007	3	.104	2	.146	4	5.544e-3	2	NC	5	NC	1
530			min	-.004	2	-.081	3	0	12	-1.84e-3	3	1325.528	2	NC	1
531		19	max	.007	3	.204	2	.124	4	1.107e-2	2	NC	1	NC	1
532			min	-.004	2	-.162	3	0	1	-3.748e-3	3	NC	1	NC	1
533	M5	1	max	.028	3	.365	2	.552	4	0	1	NC	1	NC	1
534			min	-.019	2	-.016	3	0	1	-9.904e-6	4	NC	1	NC	1
535		2	max	.028	3	.18	2	.541	4	6.497e-3	4	NC	5	NC	1
536			min	-.019	2	-.01	3	0	1	0	1	744.014	2	NC	1
537		3	max	.028	3	.038	3	.526	4	1.285e-2	4	NC	5	NC	1
538			min	-.019	2	-.031	2	0	1	0	1	345.863	2	6222.182	4
539		4	max	.027	3	.164	3	.509	4	1.047e-2	4	9403.637	15	NC	1
540			min	-.019	2	-.29	2	0	1	0	1	208.643	2	4731.479	4
541		5	max	.026	3	.346	3	.491	4	8.089e-3	4	6518.273	15	NC	1
542			min	-.018	2	-.576	2	0	1	0	1	145.052	2	3981.134	4
543		6	max	.026	3	.554	3	.472	4	5.71e-3	4	4983.768	15	NC	1
544			min	-.018	2	-.862	2	0	1	0	1	111.091	2	3501.703	4
545		7	max	.025	3	.759	3	.453	4	3.33e-3	4	4103.953	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.018	2	-1.124	2	0	1	0	1	91.554	2	3124.335	4
547		8	max	.025	3	.932	3	.434	4	9.508e-4	4	3595.275	15	NC	1
548			min	-.017	2	-1.334	2	0	1	0	1	80.232	2	2774.582	4
549		9	max	.024	3	1.044	3	.416	4	0	1	3335.168	15	NC	1
550			min	-.017	2	-1.468	2	0	1	-5.314e-6	5	74.434	2	2492.748	4
551		10	max	.024	3	1.085	3	.393	4	4.12e-8	14	3256.851	15	NC	1
552			min	-.017	2	-1.514	2	0	1	-5.041e-6	5	72.74	2	2439.05	4
553		11	max	.023	3	1.058	3	.369	4	1.932e-7	14	3335.369	15	NC	1
554			min	-.016	2	-1.47	2	0	1	-4.768e-6	5	74.714	2	2482.518	4
555		12	max	.022	3	.965	3	.344	4	6.618e-4	4	3595.741	15	NC	1
556			min	-.016	2	-1.331	2	0	1	0	1	81.166	2	2542.403	4
557		13	max	.022	3	.814	3	.312	4	2.318e-3	4	4104.87	15	NC	1
558			min	-.016	2	-1.109	2	0	1	0	1	94.022	2	2967.062	4
559		14	max	.021	3	.625	3	.276	4	3.975e-3	4	4985.512	15	NC	1
560			min	-.015	2	-.835	2	0	1	0	1	116.775	2	4139.179	4
561		15	max	.021	3	.416	3	.237	4	5.631e-3	4	6521.663	15	NC	1
562			min	-.015	2	-.541	2	0	1	0	1	157.774	2	7624.886	5
563		16	max	.02	3	.206	3	.2	4	7.287e-3	4	9410.688	15	NC	1
564			min	-.015	2	-.258	2	0	1	0	1	238.4	2	NC	1
565		17	max	.02	3	.013	3	.167	4	8.944e-3	4	NC	5	NC	1
566			min	-.015	2	-.017	2	0	1	0	1	422.282	2	NC	1
567		18	max	.02	3	.159	1	.142	4	4.524e-3	4	NC	5	NC	1
568			min	-.015	2	-.148	3	0	1	0	1	945.402	1	NC	1
569		19	max	.02	3	.299	1	.125	4	0	1	NC	1	NC	1
570			min	-.015	2	-.29	3	0	1	-4.745e-6	4	NC	1	NC	1
571	M9	1	max	.009	3	.229	2	.552	4	1.561e-2	3	NC	1	NC	1
572			min	-.006	2	-.067	3	0	1	-6.97e-3	1	NC	1	NC	1
573		2	max	.009	3	.112	2	.54	4	7.748e-3	3	NC	5	NC	1
574			min	-.006	2	-.034	3	0	10	-3.361e-3	1	1167.024	2	NC	1
575		3	max	.009	3	.013	3	.525	4	1.279e-2	4	NC	5	NC	1
576			min	-.006	2	-.011	2	0	10	-2.6e-5	10	565.737	2	6723.827	4
577		4	max	.009	3	.083	3	.508	4	1.011e-2	5	NC	15	NC	1
578			min	-.005	2	-.147	2	0	10	-3.97e-3	2	360.568	2	4965.607	4
579		5	max	.009	3	.17	3	.49	4	7.673e-3	3	NC	15	NC	1
580			min	-.005	2	-.288	2	0	10	-7.934e-3	2	262.251	2	4067.318	4
581		6	max	.009	3	.261	3	.472	4	1.146e-2	3	8323.08	15	NC	1
582			min	-.005	2	-.423	2	0	10	-1.19e-2	2	207.774	2	3504.418	4
583		7	max	.009	3	.348	3	.453	4	1.525e-2	3	7044.778	15	NC	1
584			min	-.005	2	-.543	2	0	1	-1.586e-2	2	175.47	2	3093.59	4
585		8	max	.008	3	.42	3	.435	4	1.904e-2	3	6286.515	15	NC	1
586			min	-.005	2	-.639	2	0	1	-1.983e-2	2	156.304	2	2753.505	5
587		9	max	.008	3	.467	3	.416	4	1.962e-2	3	5888.845	15	NC	1
588			min	-.005	2	-.699	2	0	10	-2.212e-2	2	146.294	2	2492.087	4
589		10	max	.008	3	.485	3	.394	4	1.805e-2	3	5767.018	15	NC	1
590			min	-.005	2	-.719	2	0	1	-2.33e-2	2	143.357	2	2415.853	4
591		11	max	.008	3	.474	3	.369	4	1.648e-2	3	5888.49	15	NC	1
592			min	-.005	2	-.698	2	0	1	-2.448e-2	2	146.787	2	2452.595	4
593		12	max	.008	3	.434	3	.343	4	1.438e-2	3	6285.813	15	NC	1
594			min	-.005	2	-.636	2	0	10	-2.333e-2	2	157.74	2	2576.61	4
595		13	max	.007	3	.37	3	.311	4	1.151e-2	3	7043.647	15	NC	1
596			min	-.005	2	-.537	2	0	10	-1.871e-2	2	178.836	2	3050.912	4
597		14	max	.007	3	.288	3	.275	4	8.635e-3	3	8321.308	15	NC	1
598			min	-.004	2	-.413	2	-.001	1	-1.408e-2	2	214.772	2	4185.616	5
599		15	max	.007	3	.196	3	.238	4	5.762e-3	3	NC	15	NC	1
600			min	-.004	2	-.276	2	-.004	1	-9.454e-3	2	276.298	2	7095.838	5
601		16	max	.007	3	.099	3	.201	4	7.22e-3	5	NC	15	NC	1
602			min	-.004	2	-.136	2	-.005	1	-4.828e-3	2	389.387	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.007	3	.005	3	.169	4	9.072e-3	4	NC	5	NC	1
604			min	-.004	2	-.006	2	-.006	1	-4.029e-4	1	629.043	2	NC	1
605		18	max	.007	3	.104	2	.144	4	4.441e-3	5	NC	5	NC	1
606			min	-.004	2	-.081	3	-.004	1	-5.544e-3	2	1325.528	2	NC	1
607		19	max	.007	3	.204	2	.124	4	3.748e-3	3	NC	1	NC	1
608			min	-.004	2	-.162	3	0	12	-1.107e-2	2	NC	1	NC	1

SIMPSON Strong-Tie	Anchor Designer™ Software Version 2.4.6025.0

Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	1/5
Project:	Standard PVMax - Worst Case, 14-40 Inch Width		
Address:			
Phone:			
E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

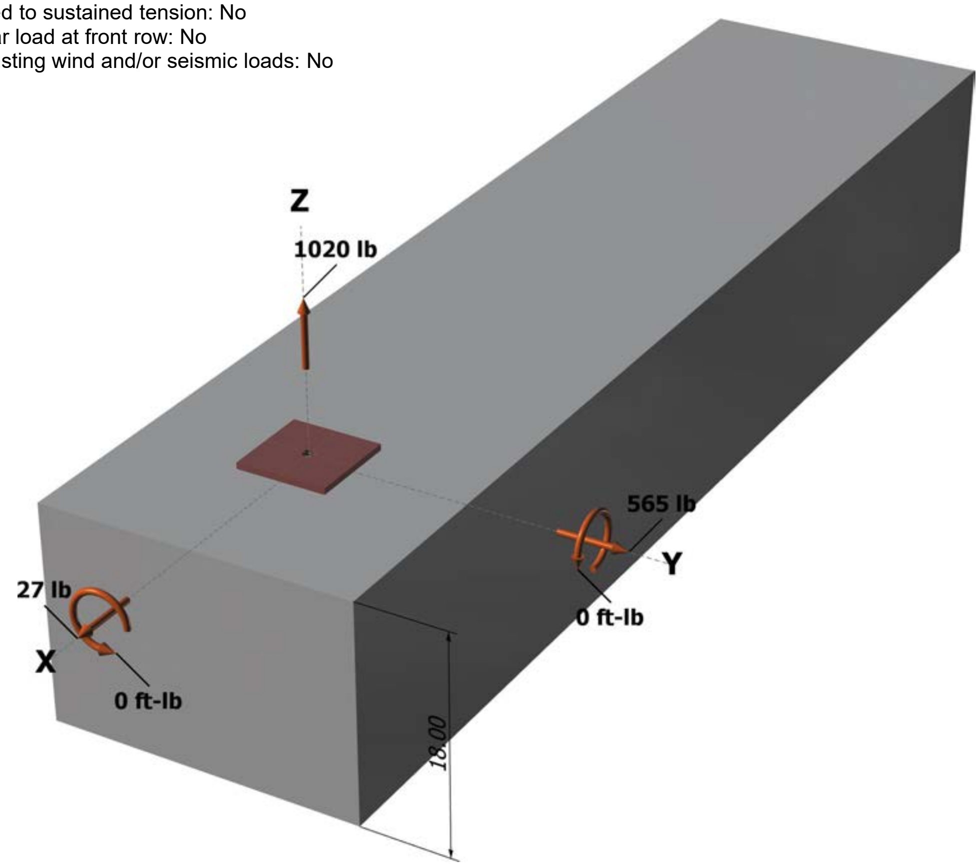
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



Company:	Schletter, Inc.	Date:	8/1/2016
Engineer:	HCV	Page:	2/5
Project:	Standard PVMax - Worst Case, 14-40 Inch Width		
Address:			
Phone:			
E-mail:			

<Figure 2>

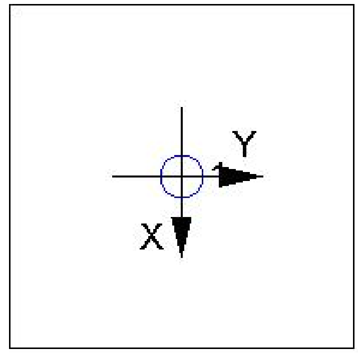
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1020.0	27.0	565.0	565.6
Sum	1020.0	27.0	565.0	565.6

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1020
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi\, (A_{Nc} / A_{Nco})\, \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\, (A_{Na} / A_{Na0})\, \Psi_{ed,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi \min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	1020	6071	0.17	Pass
Concrete breakout	1020	5710	0.18	Pass
Adhesive	**1020**	**5365**	**0.19**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**566**	**3156**	**0.18**	**Pass (Governs)**
T Concrete breakout y+	565	3934	0.14	Pass
T Concrete breakout x+	27	3018	0.01	Pass
|| Concrete breakout y+	27	8508	0.00	Pass
|| Concrete breakout x+	565	6875	0.08	Pass
Concrete breakout, combined	-	-	0.14	Pass
Pryout	566	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.19	0.00	19.0 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

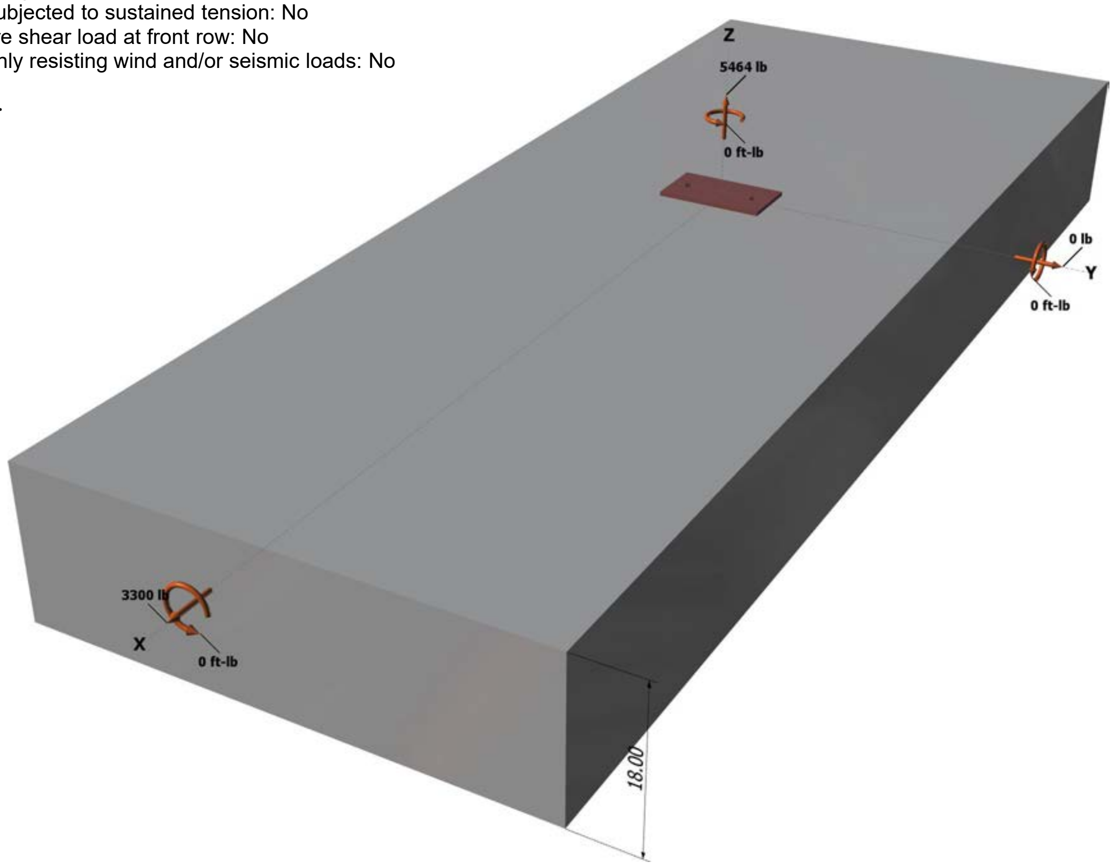
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

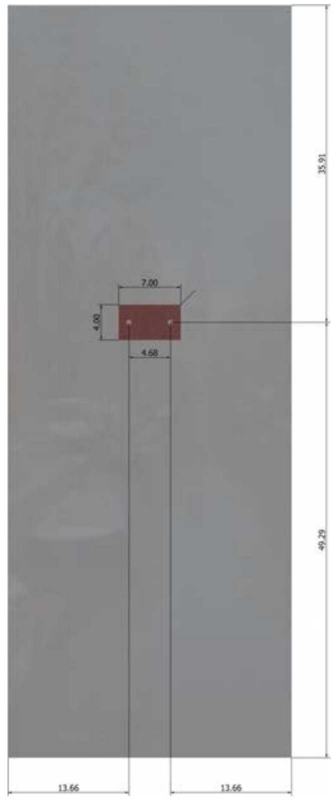
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



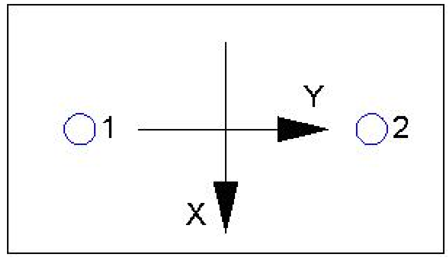
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2732.0	1650.0	0.0	1650.0
2	2732.0	1650.0	0.0	1650.0
Sum	5464.0	3300.0	0.0	3300.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 5464
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
408.24	324.00	1.000	1.000	1.00	1.000	12492	0.65	10231

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\ (A_{Vc} / A_{Vco})\,\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
576.00	648.00	1.000	0.928	1.000	1.000	15593	0.70	9001

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	13.66	18939

$\phi V_{cbx} = \phi\ (2)(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
737.64	839.68	1.000	1.000	1.000	18939	0.70	23292

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\ \min|k_{cp}N_{ag}\ ;\ k_{cp}N_{cbg}| = \phi\ \min|k_{cp}(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
408.24	324.00	1.000	1.000	1.000	1.000	12492	15740	0.70

ϕV_{cpg} (lb)
20601

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	2732	6071	0.45	Pass
Concrete breakout	5464	10231	0.53	Pass
Adhesive	**5464**	**8093**	**0.68**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	**1650**	**3156**	**0.52**	**Pass (Governs)**
T Concrete breakout x+	3300	9001	0.37	Pass

|| Concrete breakout y-	1650	23292	0.07	Pass
Pryout	3300	20601	0.16	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.3	0.68	0.52	119.8 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.