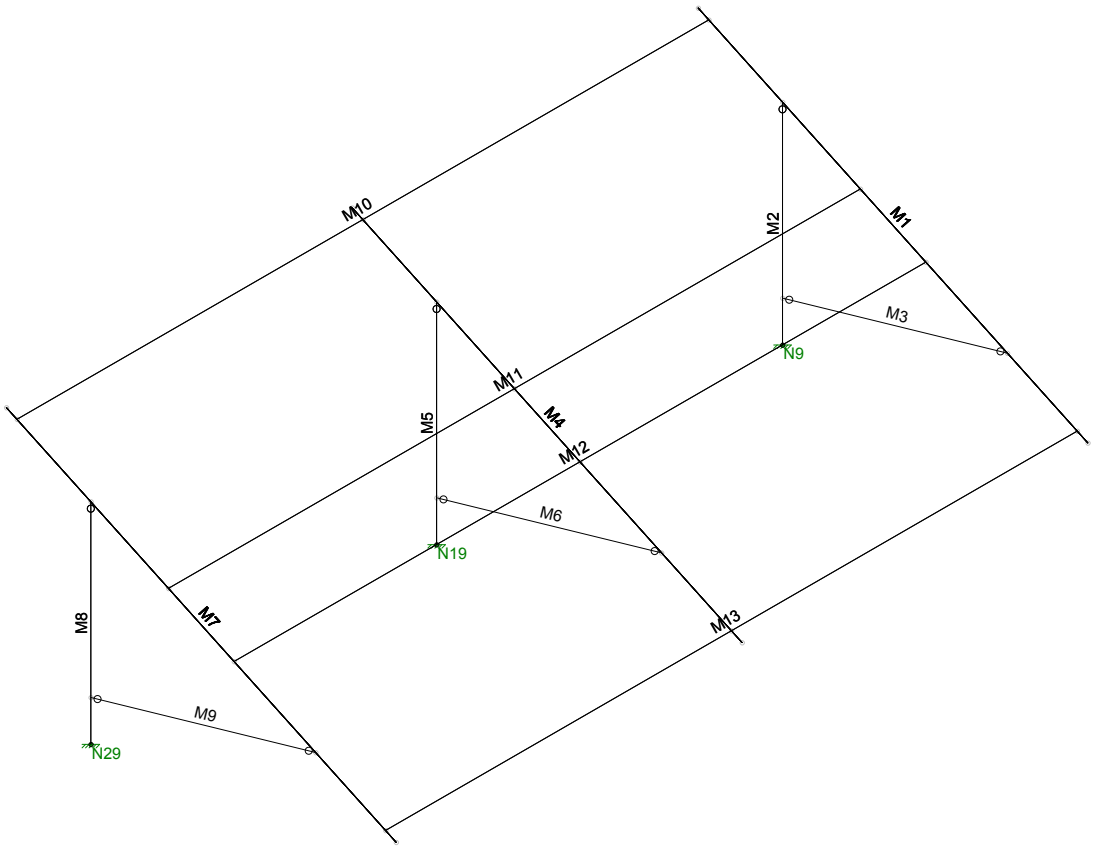


Schletter, Inc.		25° Tilt w/ Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

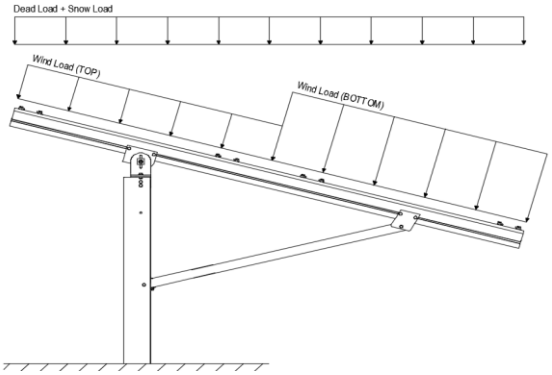
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum	
Height =	2000	mm	1900	mm
Width =	1050	mm	970	mm
Dead Load =	3.00	psf	1.75	psf

Modules Per Row =	2
Module Tilt =	25°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	18.56	psf	*(ASCE 7-05, Eq. 7-2)*
I_s =	1.00		
C_s =	0.82		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	120	mph	Exposure Category = C
Height <	15	ft	Importance Category = II
Peak Velocity Pressure, q_z =	22.61	psf	*Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.1	*(Pressure)*	*Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.*
$Cf+_{BOTTOM}$ =	1.7		
$Cf-_{TOP}$ =	-2.2	*(Suction)*	
$Cf-_{BOTTOM}$ =	-1		

2.4 Seismic Loads

S_S =	2.50	R =	1.25	*ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.*
S_{DS} =	1.67	C_S =	0.8	
S_1 =	1.00	ρ =	1.3	
S_{D1} =	1.00	Ω =	1.25	
T_a =	0.08	C_d =	1.25	

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W
1.2D + 1.6W + 0.5S
0.9D + 1.6W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 1.0W
1.0D + 0.75L + 0.75W + 0.75S
0.6D + 1.0W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

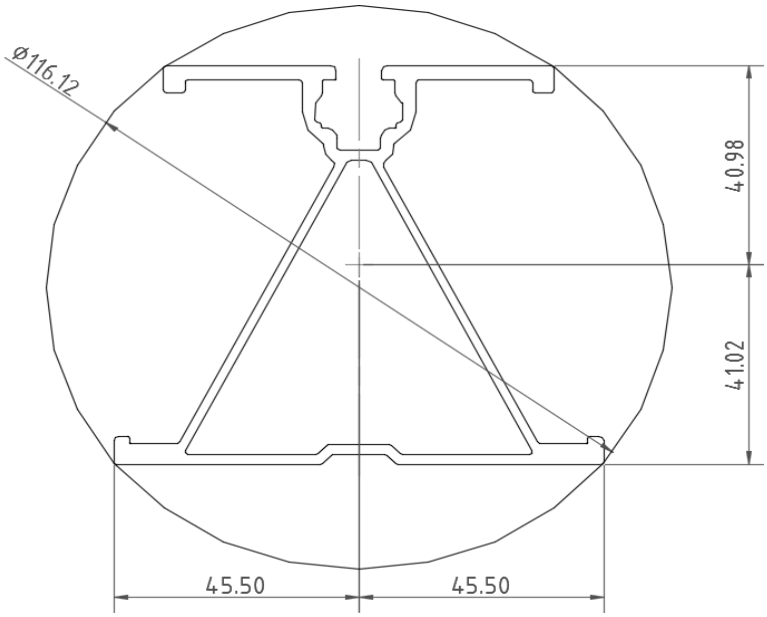
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	78	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.6	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.040	k-ft
M_z =	0.170	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	52%	

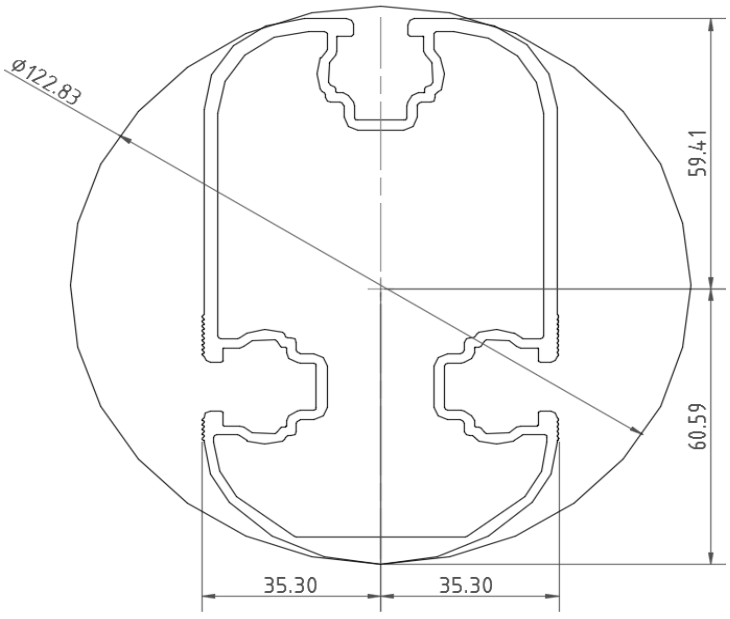


DETAIL VIEW

4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

Girder Type =	**T5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	81.77	in
$\Phi F_{ty\ AXIAL}$ =	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	30.06	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	31.56	ksi
S_y =	1.98	in^3
S_x =	1.32	in^3
E =	10100	ksi
I_y =	4.74	in^4
I_x =	1.83	in^4
A =	1.93	in^2
g =	2.32	lbs/ft
M_y =	4.023	k-ft
M_z =	0.000	k-ft
P_n =	1.937	k
$M_{y\ allowable}$ =	4.960	k-ft
$M_{z\ allowable}$ =	3.472	k-ft
$P_{n\ allowable}$ =	59.439	k
Utilization =	84%	

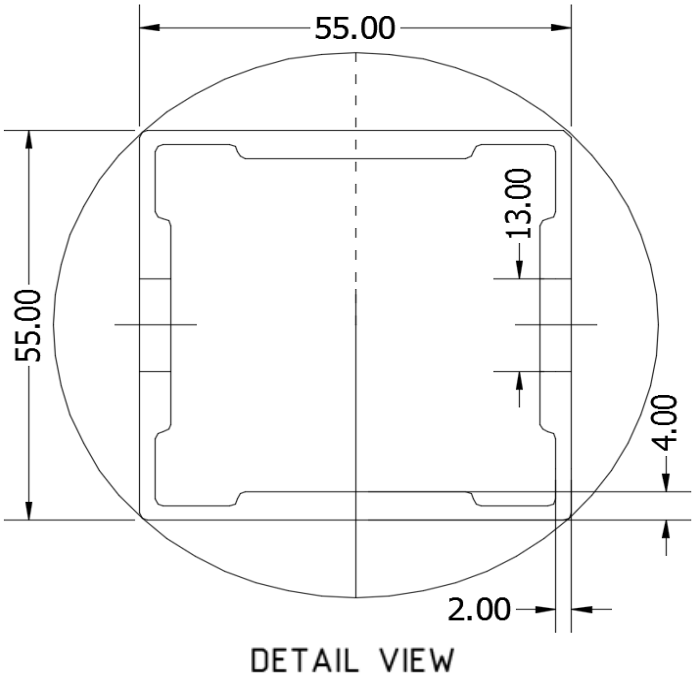


DETAIL VIEW

4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

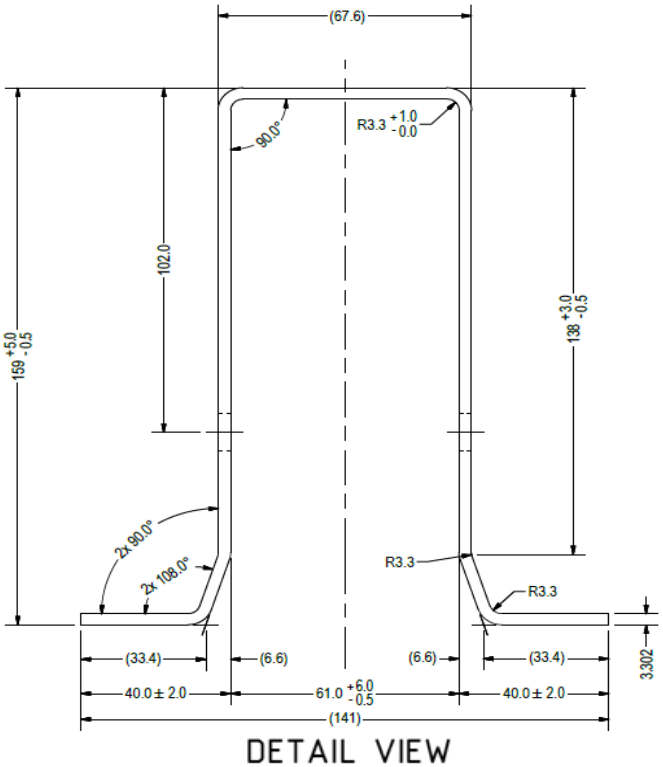
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	74.80	in
$\Phi F_{ty\ AXIAL}$ =	9.61	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.007	k-ft
M_z =	0.000	k-ft
P_n =	5.207	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	9.441	k
Utilization =	56%	



4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	81.31	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	11.268	k-ft
M_z =	0.000	k-ft
P_r =	5.707	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	30.879	k
Utilization =	78%	



5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	6.50	k
Maximum Lateral Load =	3.45	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

Lateral Force @ Top of Pole, P =	1.06	k
Height of Pole Above Grade, H =	5.78	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

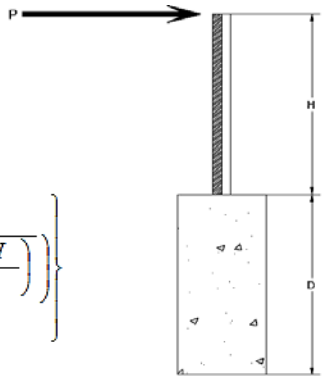
Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1+\sqrt{1+\left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Non-Constrained

Lateral Force @ Top of Pole, P =	1.06	k
Height of Pole Above Grade, H =	5.78	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	5.74	
Required Footing Depth, D =	9.53	ft

2nd Trial @ D_2 =	6.39	ft
Lateral Soil Bearing @ D/3, S_1 =	0.43	ksf
Lateral Soil Bearing @ D, S_3 =	1.28	ksf
Constant 2.34P/(S_1B), A =	2.92	
Required Footing Depth, D =	5.99	ft

3rd Trial @ D_3 =	6.19	ft
Lateral Soil Bearing @ D/3, S_1 =	0.41	ksf
Lateral Soil Bearing @ D, S_3 =	1.24	ksf
Constant 2.34P/(S_1B), A =	3.01	
Required Footing Depth, D =	6.12	ft

4th Trial @ D_4 =	6.15	ft
Lateral Soil Bearing @ D/3, S_1 =	0.41	ksf
Lateral Soil Bearing @ D, S_3 =	1.23	ksf
Constant 2.34P/(S_1B), A =	3.03	
Required Footing Depth, D =	6.14	ft

5th Trial @ D_5 =	6.15	ft
Lateral Soil Bearing @ D/3, S_1 =	0.41	ksf
Lateral Soil Bearing @ D, S_3 =	1.23	ksf
Constant 2.34P/(S_1B), A =	3.04	
Required Footing Depth, D =	6.25	ft

A 2ft diameter x 6.25ft deep footing unrestrained at ground level is required for the racking structure.

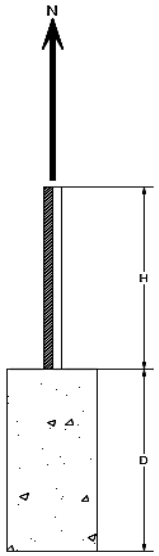
5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	3.11	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	2.03	k
Required Concrete Volume, V =	13.98	ft^3
Required Footing Depth, D =	4.50	ft

Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	6.73
2	0.4	0.2	118.10	6.63
3	0.6	0.2	118.10	6.52
4	0.8	0.2	118.10	6.42
5	1	0.2	118.10	6.32
6	1.2	0.2	118.10	6.21
7	1.4	0.2	118.10	6.11
8	1.6	0.2	118.10	6.01
9	1.8	0.2	118.10	5.90
10	2	0.2	118.10	5.80
11	2.2	0.2	118.10	5.70
12	2.4	0.2	118.10	5.59
13	2.6	0.2	118.10	5.49
14	2.8	0.2	118.10	5.38
15	3	0.2	118.10	5.28
16	3.2	0.2	118.10	5.18
17	3.4	0.2	118.10	5.07
18	3.6	0.2	118.10	4.97
19	3.8	0.2	118.10	4.87
20	4	0.2	118.10	4.76
21	4.2	0.2	118.10	4.66
22	4.4	0.2	118.10	4.55
23	4.6	0.2	118.10	4.45
24	0	0.0	0.00	4.45
25	0	0.0	0.00	4.45
26	0	0.0	0.00	4.45
27	0	0.0	0.00	4.45
28	0	0.0	0.00	4.45
29	0	0.0	0.00	4.45
30	0	0.0	0.00	4.45
31	0	0.0	0.00	4.45
32	0	0.0	0.00	4.45
33	0	0.0	0.00	4.45
34	0	0.0	0.00	4.45
Max	4.6	Sum	1.09	

A 2ft diameter x 4.5ft deep footing unrestrained at ground level is required for the racking structure.



5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	6.25	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	3.67	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	20.42	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

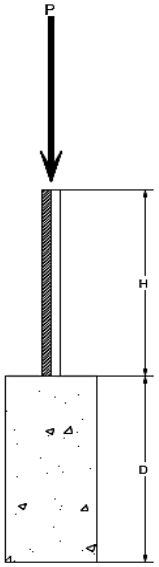
Weight of Concrete

Footing Volume	19.63	ft^3
Weight	2.85	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	3.06	k
1/3 Increase for Wind =	1.33	
Total Resistance =	10.37	k
Applied Force =	6.51	k
Utilization =	63%	

A 2ft diameter footing passes at a depth of 6.25ft.



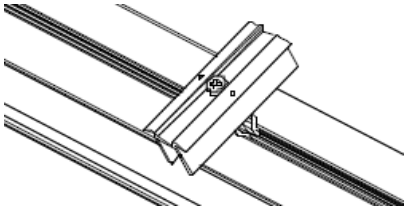
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

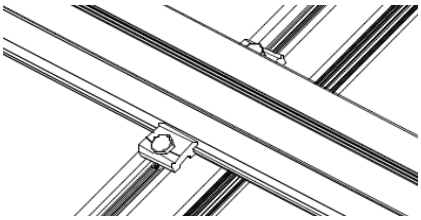
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.882 k
Allowable Uplift	=	1.214 k
Utilization	=	73%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	2.045 k
Allowable Uplift	=	2.180 k
Utilization	=	94%

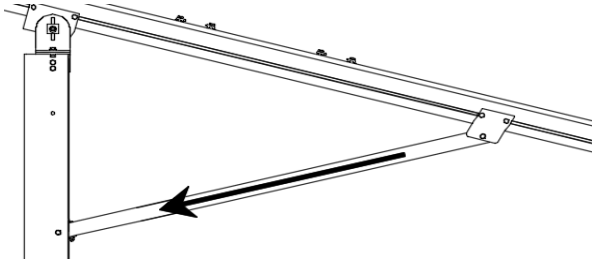


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load	=	5.207 k
M10 Bolt Shear Capacity	=	8.894 k
Utilization	=	59%

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

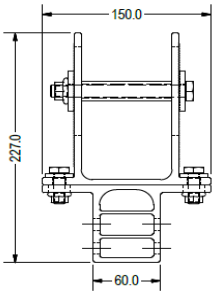


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

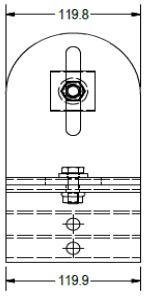
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

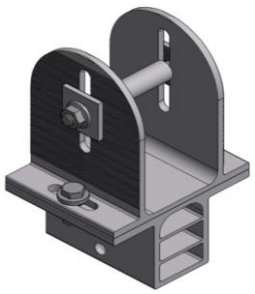
Maximum Tensile Load	=	4.202 k
Allowable Load	=	5.649 k
Utilization	=	74%



FRONT VIEW



SIDE VIEW



7. SEISMIC DESIGN

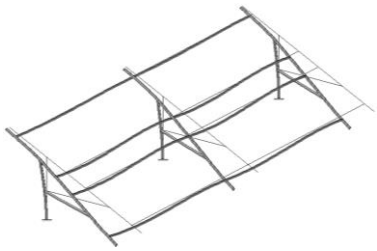
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	74.39 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.488 in
Max Drift, Δ_{MAX}	=	0.701 in

0.701 ≤ 1.488, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:		Weak Axis:	
3.4.14		**3.4.14**	
L_b =	78 in	L_b =	78
J =	0.432	J =	0.432
	215.785		137.226
$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$		$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$	
S1 =	0.51461	S1 =	0.51461
$S2 = \left(\frac{C_c}{1.6}\right)^2$		$S2 = \left(\frac{C_c}{1.6}\right)^2$	
S2 =	1701.56	S2 =	1701.56
φF_L=	φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]	φF_L=	φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L=	28.6 ksi	φF_L=	29.6
3.4.16		**3.4.16**	
b/t =	32.195	b/t =	37.0588
$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$		$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$	
S1 =	12.2	S1 =	12.2
$S2 = \frac{k_1 Bp}{1.6Dp}$		$S2 = \frac{k_1 Bp}{1.6Dp}$	
S2 =	46.7	S2 =	46.7
φF_L=	φb[Bp-1.6Dp*b/t]	φF_L=	φb[Bp-1.6Dp*b/t]
φF_L=	25.1 ksi	φF_L=	23.1 ksi
3.4.16.1	Not Used	**3.4.16.1**	
Rb/t =		N/A for Weak Direction	
$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$			
S1 =	1.1		
$S2 = C_t$			
S2 =	141.0		
φF_L=	1.17φyFcy		
φF_L=	38.9 ksi		
3.4.18		**3.4.18**	
h/t =	37.0588	h/t =	32.195
$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$		$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$	
S1 =	36.9	S1 =	36.9
m =	0.65	m =	0.65
C_0 =	40.985	C_0 =	45.5
Cc =	41.015	Cc =	45.5
$S2 = \frac{k_1 Bbr}{mDbr}$		$S2 = \frac{k_1 Bbr}{mDbr}$	
S2 =	77.2	S2 =	77.3
φF_L=	φb[Bbr-mDbr*h/t]	φF_L=	1.3φyFcy
φF_L=	43.2 ksi	φF_L=	43.2 ksi
φF_LSt=	25.1 ksi	φF_LWk=	23.1 ksi
Ix =	897074 mm^4	Iy =	446476 mm^4
	2.155 in^4		1.073 in^4
y =	41.015 mm	x =	45.5 mm
Sx =	1.335 in^3	Sy =	0.599 in^3
M_{max}St =	2.788 k-ft	M_{max}Wk =	1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 81.7717 in
J = 1.98
105.231

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.1 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 81.7717
J = 1.98
114.202

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 29.9

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 30.1 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 4.935 k-ft

$\varphi F_L Wk$= 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 30.80 ksi

φF_L= 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:	Weak Axis:
3.4.14	**3.4.14**
L_b = 74.8031 in	L_b = 74.8031
J = 0.942	J = 0.942
116.737	116.737
$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$	$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$
S1 = 0.51461	S1 = 0.51461
$S2 = \left(\frac{C_c}{1.6}\right)^2$	$S2 = \left(\frac{C_c}{1.6}\right)^2$
S2 = 1701.56	S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]	φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.9 ksi	φF_L= 29.9
3.4.16	**3.4.16**
b/t = 24.5	b/t = 24.5
$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$	$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$
S1 = 12.2	S1 = 12.2
$S2 = \frac{k_1 Bp}{1.6Dp}$	$S2 = \frac{k_1 Bp}{1.6Dp}$
S2 = 46.7	S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]	φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi	φF_L= 28.2 ksi
3.4.16.1 Not Used	**3.4.16.1**
Rb/t = 0.0	N/A for Weak Direction
$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$	
S1 = 1.1	
$S2 = C_t$	
S2 = 141.0	
φF_L= 1.17φyFcy	
φF_L= 38.9 ksi	
3.4.18	**3.4.18**
h/t = 24.5	h/t = 24.5
$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$	$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$
S1 = 36.9	S1 = 36.9
m = 0.65	m = 0.65
C_0 = 27.5	C_0 = 27.5
Cc = 27.5	Cc = 27.5
$S2 = \frac{k_1 Bbr}{mDbr}$	$S2 = \frac{k_1 Bbr}{mDbr}$
S2 = 77.3	S2 = 77.3
φF_L= 1.3φyFcy	φF_L= 1.3φyFcy
φF_L= 43.2 ksi	φF_L= 43.2 ksi
φF_LSt= 28.2 ksi	φF_LWk= 28.2 ksi
Ix = 279836 mm^4	Iy = 279836 mm^4
0.672 in^4	0.672 in^4
y = 27.5 mm	x = 27.5 mm
Sx = 0.621 in^3	Sy = 0.621 in^3
M_{max}St = 1.460 k-ft	M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.73045

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.82226

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

φF_L = 9.61085 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

φF_L = 33.25 ksi

φF_L = 9.61 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 9.89 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	81.31	in	
Pr =	5.71	k	(LRFD Factored Load)
Mr (Strong) =	11.27	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	116.99			
4.71√(E/Fy) =	103.55	=>	kL/r	> 4.71√(E/Fy)
Fcr =	18.34	ksi		
Fe =	20.91	ksi		
Pn =	40.9	k		

Torsional/Flexural Torsional Buckling:

Fcr =	13.8471	ksi
Fey =	53.3447	ksi
Fez =	17.7356	ksi
Pn =	30.879	k

Bending (Strong Axis):

Yielding:

Mn =	21.95	k-ft

Flange Local Buckling:

Mn =	19.207	k-ft

Pr/Pc =	0.2054	≥	0.2	
Utilization =	0.78	<	1.0	OK

Bending (Weak Axis):

Yielding:

Mn =	14.65	k-ft

Flange Local Buckling:

Mn =	14.39	k-ft

Pr/Pc =	0.205	≥	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 78%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-9.843	-9.843	0	0
2	M11	Y	-9.843	-9.843	0	0
3	M12	Y	-9.843	-9.843	0	0
4	M13	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-5.454	-5.454	0	0
2	M11	Y	-5.454	-5.454	0	0
3	M12	Y	-5.454	-5.454	0	0
4	M13	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-55.176	-55.176	0	0
2	M11	Y	-55.176	-55.176	0	0
3	M12	Y	-55.176	-55.176	0	0
4	M13	Y	-55.176	-55.176	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-81.596	-81.596	0	0
2	M11	y	-81.596	-81.596	0	0
3	M12	y	-126.102	-126.102	0	0
4	M13	y	-126.102	-126.102	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	163.191	163.191	0	0
2	M11	y	163.191	163.191	0	0
3	M12	y	74.178	74.178	0	0
4	M13	y	74.178	74.178	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Z	7.874	7.874	0	0
2	M11	Z	7.874	7.874	0	0
3	M12	Z	7.874	7.874	0	0
4	M13	Z	7.874	7.874	0	0
5	M10	Z	0	0	0	0
6	M11	Z	0	0	0	0
7	M12	Z	0	0	0	0
8	M13	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8														
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6														
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	508.87	2	2274.925	2	97.476	2	.152	1	.006	5	7.143	1
2		min	-849.713	3	-1709.496	3	-280.32	5	-1.246	5	-.004	2	.7	12
3	N19	max	2633.781	2	5708.672	2	0	2	0	3	.007	4	9.586	1
4		min	-2473.738	3	-4990.852	3	-293.785	5	-1.291	4	0	12	.302	15
5	N29	max	508.87	2	2274.925	2	114.066	3	.156	3	.007	4	7.143	1
6		min	-849.713	3	-1709.496	3	-298.825	4	-1.291	4	-.002	3	-.519	5
7	Totals:	max	3651.522	2	10258.521	2	0	1						
8		min	-4173.165	3	-8409.845	3	-860.773	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.004	2	0	4	0	1	0	1	0	1
2			min	0	1	0	3	0	1	0	1	0	1	0	1
3		2	max	-3.403	12	306.454	3	6.84	3	.043	3	.234	1	.264	2
4			min	-185.995	1	-711.141	2	-112.04	1	-.167	2	-.002	3	-.112	3
5		3	max	-3.79	12	305.21	3	6.84	3	.043	3	.161	1	.731	2
6			min	-186.768	1	-712.799	2	-112.04	1	-.167	2	.002	12	-.313	3
7		4	max	-4.176	12	303.967	3	6.84	3	.043	3	.087	1	1.199	2
8			min	-187.541	1	-714.457	2	-112.04	1	-.167	2	.005	12	-.513	3
9		5	max	633.881	3	644.324	2	17.545	3	-.007	9	.109	1	1.418	2
10			min	-1690.612	2	-258.935	3	-135.301	1	-.023	2	-.031	3	-.609	3
11		6	max	633.301	3	642.666	2	17.545	3	-.007	9	.03	2	.996	2
12			min	-1691.385	2	-260.178	3	-135.301	1	-.023	2	-.027	5	-.438	3
13		7	max	632.721	3	641.008	2	17.545	3	-.007	9	-.005	12	.575	2
14			min	-1692.158	2	-261.422	3	-135.301	1	-.023	2	-.071	4	-.267	3
15		8	max	632.141	3	639.35	2	17.545	3	-.007	9	.004	3	.155	2
16			min	-1692.931	2	-262.666	3	-135.301	1	-.023	2	-.157	1	-.095	3
17		9	max	628.793	3	8.583	1	32.449	3	.015	5	.094	1	-.001	15
18			min	-1817.733	2	.193	15	-182.45	1	-.117	2	.006	12	-.044	2
19		10	max	628.213	3	7.253	3	32.449	3	.015	5	.031	3	-.001	15
20			min	-1818.507	2	-.449	5	-182.45	1	-.117	2	-.028	2	-.046	2
21		11	max	627.633	3	6.009	3	32.449	3	.015	5	.052	3	-.001	15
22			min	-1819.28	2	-1.532	13	-182.45	1	-.117	2	-.145	1	-.048	2
23		12	max	618.804	3	677.341	3	.605	10	.147	3	.118	1	.098	2
24			min	-1938.296	2	-423.387	2	-168.292	4	-.141	2	.027	12	-.246	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
25		13	max	618.225	3	676.097	3	.605	10	.147	3	.095	1	.377	2
26			min	-1939.069	2	-425.045	2	-169.878	4	-.141	2	-.026	3	-.69	3
27		14	max	617.645	3	674.853	3	.605	10	.147	3	.073	1	.656	2
28			min	-1939.842	2	-426.703	2	-171.463	4	-.141	2	-.12	5	-1.133	3
29		15	max	617.065	3	673.61	3	.605	10	.147	3	.067	2	.937	2
30			min	-1940.615	2	-428.361	2	-173.049	4	-.141	2	-.228	5	-1.575	3
31		16	max	187.605	1	429.974	2	55.9	5	.091	2	.015	3	.713	2
32			min	3.025	12	-714.903	3	-101.719	1	-.252	3	-.148	4	-1.202	3
33		17	max	186.831	1	428.316	2	54.314	5	.091	2	.015	3	.432	2
34			min	2.638	12	-716.147	3	-101.719	1	-.252	3	-.176	1	-.733	3
35		18	max	186.058	1	426.658	2	52.729	5	.091	2	.014	3	.151	2
36			min	2.252	12	-717.39	3	-101.719	1	-.252	3	-.243	1	-.262	3
37		19	max	0	1	0	15	0	1	0	1	0	1	0	1
38			min	0	1	-.002	3	0	4	0	1	0	1	0	1
39	M4	1	max	0	1	.006	2	0	4	0	1	0	1	0	1
40			min	0	1	-.001	3	0	1	0	1	0	1	0	1
41		2	max	25.776	10	852.2	3	0	1	.029	4	.205	4	.513	2
42			min	-190.162	1	-1686.963	2	-76.944	5	0	1	0	1	-.266	3
43		3	max	25.132	10	850.956	3	0	1	.029	4	.154	4	1.621	2
44			min	-190.935	1	-1688.622	2	-78.529	5	0	1	0	1	-.825	3
45		4	max	24.488	10	849.713	3	0	1	.029	4	.102	4	2.729	2
46			min	-191.708	1	-1690.28	2	-80.115	5	0	1	0	1	-1.383	3
47		5	max	1989.424	3	1725.6	2	0	1	0	1	.014	4	3.211	2
48			min	-3986.39	2	-914.015	3	-77.978	4	-.013	4	0	1	-1.616	3
49		6	max	1988.844	3	1723.941	2	0	1	0	1	0	1	2.079	2
50			min	-3987.163	2	-915.259	3	-79.564	4	-.013	4	-.037	5	-1.016	3
51		7	max	1988.264	3	1722.283	2	0	1	0	1	0	1	.949	2
52			min	-3987.936	2	-916.503	3	-81.15	4	-.013	4	-.09	4	-.415	3
53		8	max	1987.684	3	1720.625	2	0	1	0	1	0	1	.187	3
54			min	-3988.71	2	-917.746	3	-82.735	4	-.013	4	-.144	4	-.181	2
55		9	max	1958.234	3	5.224	3	0	1	.012	4	.127	4	.476	3
56			min	-3967.804	2	-128.889	2	-186.954	4	0	1	0	1	-.698	2
57		10	max	1957.654	3	3.98	3	0	1	.012	4	.005	5	.473	3
58			min	-3968.578	2	-130.547	2	-188.539	4	0	1	0	1	-.613	2
59		11	max	1957.074	3	2.737	3	0	1	.012	4	0	1	.471	3
60			min	-3969.351	2	-132.205	2	-190.125	4	0	1	-.12	4	-.527	2
61		12	max	1938.585	3	1970.439	3	0	1	.107	4	.133	5	.016	9
62			min	-3960.018	2	-1472.562	2	-183.154	5	0	1	0	1	-.148	3
63		13	max	1938.005	3	1969.195	3	0	1	.107	4	.012	5	.928	2
64			min	-3960.791	2	-1474.22	2	-184.739	5	0	1	0	1	-1.44	3
65		14	max	1937.425	3	1967.952	3	0	1	.107	4	0	1	1.896	2
66			min	-3961.564	2	-1475.879	2	-186.325	5	0	1	-.11	4	-2.732	3
67		15	max	1936.845	3	1966.708	3	0	1	.107	4	0	1	2.865	2
68			min	-3962.338	2	-1477.537	2	-187.91	5	0	1	-.232	4	-4.023	3
69		16	max	191.582	1	1336.938	2	45.635	5	0	1	0	1	2.182	2
70			min	-24.698	10	-1880.271	3	0	1	-.097	4	-.124	5	-3.055	3
71		17	max	190.809	1	1335.28	2	44.049	5	0	1	0	1	1.305	2
72			min	-25.342	10	-1881.515	3	0	1	-.097	4	-.095	5	-1.82	3
73		18	max	190.035	1	1333.622	2	42.464	5	0	1	0	1	.429	2
74			min	-25.987	10	-1882.758	3	0	1	-.097	4	-.067	4	-.585	3
75		19	max	0	1	0	2	0	1	0	1	0	1	0	1
76			min	0	1	-.003	3	0	4	0	1	0	1	0	1
77	M7	1	max	0	1	.004	2	0	4	0	1	0	1	0	1
78			min	0	1	0	3	0	3	0	1	0	1	0	1
79		2	max	27.524	5	306.454	3	112.04	1	.167	2	.108	5	.264	2
80			min	-185.995	1	-711.141	2	-35.4	5	-.043	3	-.234	1	-.112	3
81		3	max	27.163	5	305.21	3	112.04	1	.167	2	.084	5	.731	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
82			min	-186.768	1	-712.799	2	-36.986	5	-.043	3	-.161	1	-.313	3
83		4	max	26.802	5	303.967	3	112.04	1	.167	2	.059	5	1.199	2
84			min	-187.541	1	-714.457	2	-38.571	5	-.043	3	-.087	1	-.513	3
85		5	max	633.881	3	644.324	2	135.301	1	.023	2	.031	3	1.418	2
86			min	-1690.612	2	-258.935	3	-34.717	5	-.011	5	-.109	1	-.609	3
87		6	max	633.301	3	642.666	2	135.301	1	.023	2	.019	3	.996	2
88			min	-1691.385	2	-260.178	3	-36.303	5	-.011	5	-.03	2	-.438	3
89		7	max	632.721	3	641.008	2	135.301	1	.023	2	.068	1	.575	2
90			min	-1692.158	2	-261.422	3	-37.888	5	-.011	5	-.052	5	-.267	3
91		8	max	632.141	3	639.35	2	135.301	1	.023	2	.157	1	.155	2
92			min	-1692.931	2	-262.666	3	-39.474	5	-.011	5	-.077	5	-.095	3
93		9	max	628.793	3	8.583	1	182.45	1	.117	2	.057	5	-.003	15
94			min	-1817.733	2	1.204	15	-63.52	5	.013	15	-.094	1	-.044	2
95		10	max	628.213	3	7.253	3	182.45	1	.117	2	.028	2	-.003	15
96			min	-1818.507	2	.704	15	-65.105	5	.013	15	-.031	3	-.046	2
97		11	max	627.633	3	6.009	3	182.45	1	.117	2	.145	1	-.004	15
98			min	-1819.28	2	-.513	13	-66.691	5	.013	15	-.052	3	-.048	2
99		12	max	618.804	3	677.341	3	104.338	3	.141	2	.079	5	.098	2
100			min	-1938.296	2	-423.387	2	-155.403	5	-.147	3	-.118	1	-.246	3
101		13	max	618.225	3	676.097	3	104.338	3	.141	2	.026	3	.377	2
102			min	-1939.069	2	-425.045	2	-156.988	5	-.147	3	-.095	1	-.69	3
103		14	max	617.645	3	674.853	3	104.338	3	.141	2	.095	3	.656	2
104			min	-1939.842	2	-426.703	2	-158.574	5	-.147	3	-.137	4	-1.133	3
105		15	max	617.065	3	673.61	3	104.338	3	.141	2	.163	3	.937	2
106			min	-1940.615	2	-428.361	2	-160.16	5	-.147	3	-.237	4	-1.575	3
107		16	max	187.605	1	429.974	2	101.719	1	.252	3	.11	1	.713	2
108			min	1.793	15	-714.903	3	.646	12	-.095	4	-.12	5	-1.202	3
109		17	max	186.831	1	428.316	2	101.719	1	.252	3	.176	1	.432	2
110			min	1.56	15	-716.147	3	.646	12	-.095	4	-.077	5	-.733	3
111		18	max	186.058	1	426.658	2	101.719	1	.252	3	.243	1	.151	2
112			min	1.327	15	-717.39	3	.646	12	-.095	4	-.035	5	-.262	3
113		19	max	0	1	0	4	0	12	0	1	0	1	0	1
114			min	0	1	-.002	3	0	1	0	1	0	1	0	1
115	M10	1	max	101.756	1	425.314	2	-1.101	15	.009	2	.277	1	.095	4
116			min	.647	12	-718.602	3	-185.603	1	-.022	3	-.014	5	-.252	3
117		2	max	101.756	1	304.054	2	.153	15	.009	2	.154	1	.2	3
118			min	.647	12	-534.125	3	-154.501	1	-.022	3	-.015	3	-.173	2
119		3	max	101.756	1	182.795	2	1.834	5	.009	2	.076	2	.519	3
120			min	.647	12	-349.648	3	-123.4	1	-.022	3	-.015	3	-.349	2
121		4	max	101.756	1	61.535	2	3.773	5	.009	2	.02	2	.705	3
122			min	.647	12	-165.171	3	-92.298	1	-.022	3	-.028	9	-.437	2
123		5	max	101.756	1	19.306	3	5.713	5	.009	2	-.006	10	.758	3
124			min	.647	12	-59.724	2	-61.196	1	-.022	3	-.079	1	-.437	2
125		6	max	101.756	1	203.783	3	7.652	5	.009	2	-.002	15	.677	3
126			min	.647	12	-180.983	2	-46.245	2	-.022	3	-.112	1	-.351	2
127		7	max	101.756	1	388.26	3	16.419	14	.009	2	.002	5	.463	3
128			min	.647	12	-302.243	2	-33.668	2	-.022	3	-.123	1	-.176	2
129		8	max	101.756	1	572.737	3	35.146	9	.009	2	.01	5	.116	3
130			min	.647	12	-423.502	2	-21.092	2	-.022	3	-.114	2	-.017	5
131		9	max	101.756	1	757.214	3	63.211	1	.009	2	.019	5	.436	2
132			min	-6.852	5	-544.762	2	-16.842	10	-.022	3	-.125	2	-.364	3
133		10	max	101.756	1	207.067	14	94.313	1	-.002	15	.044	14	.873	2
134			min	.647	12	-941.691	3	-58.19	14	-.022	3	-.126	2	-.977	3
135		11	max	101.756	1	544.762	2	16.842	10	.022	3	.017	3	.436	2
136			min	.647	12	-757.214	3	-63.211	1	-.009	2	-.125	2	-.364	3
137		12	max	101.756	1	423.502	2	21.092	2	.022	3	.008	3	.116	3
138			min	.647	12	-572.737	3	-35.146	9	-.009	2	-.114	2	.015	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
139		13	max	101.756	1	302.243	2	33.668	2	.022	3	0	3	.463	3
140			min	-.191	15	-388.26	3	-14.842	9	-.009	2	-.123	1	-.176	2
141		14	max	101.756	1	180.983	2	46.245	2	.022	3	-.003	12	.677	3
142			min	-8.561	5	-203.783	3	-7.235	3	-.009	2	-.112	1	-.351	2
143		15	max	101.756	1	59.724	2	61.196	1	.022	3	0	15	.758	3
144			min	-17.084	5	-19.306	3	-5.323	3	-.009	2	-.079	1	-.437	2
145		16	max	101.756	1	165.171	3	92.298	1	.022	3	.02	2	.705	3
146			min	-25.606	5	-61.535	2	-3.412	3	-.009	2	-.028	9	-.437	2
147		17	max	101.756	1	349.648	3	123.4	1	.022	3	.076	2	.519	3
148			min	-34.129	5	-182.795	2	-1.5	3	-.009	2	-.015	3	-.349	2
149		18	max	101.756	1	534.125	3	154.501	1	.022	3	.154	1	.2	3
150			min	-42.652	5	-304.054	2	.411	3	-.009	2	-.015	3	-.173	2
151		19	max	101.756	1	718.602	3	185.603	1	.022	3	.277	1	.091	2
152			min	-51.174	5	-425.314	2	1.865	12	-.009	2	-.014	3	-.252	3
153	M11	1	max	147.317	1	422.956	2	48.079	5	.005	3	.336	1	.085	4
154			min	-136.613	3	-673.737	3	-199.323	1	-.012	2	-.18	5	-.205	3
155		2	max	147.317	1	301.697	2	50.018	5	.005	3	.203	1	.215	3
156			min	-136.613	3	-489.26	3	-168.221	1	-.012	2	-.145	5	-.238	2
157		3	max	147.317	1	180.437	2	51.958	5	.005	3	.102	2	.502	3
158			min	-136.613	3	-304.783	3	-137.12	1	-.012	2	-.108	5	-.412	2
159		4	max	147.317	1	59.178	2	53.897	5	.005	3	.039	2	.656	3
160			min	-136.613	3	-120.306	3	-106.018	1	-.012	2	-.074	4	-.498	2
161		5	max	147.317	1	64.171	3	55.837	5	.005	3	0	10	.676	3
162			min	-136.613	3	-62.081	2	-74.916	1	-.012	2	-.06	1	-.497	2
163		6	max	147.317	1	248.648	3	57.776	5	.005	3	.011	5	.563	3
164			min	-136.613	3	-183.341	2	-55.792	2	-.012	2	-.103	1	-.408	2
165		7	max	147.317	1	433.125	3	62.472	4	.005	3	.053	5	.317	3
166			min	-136.613	3	-304.6	2	-43.215	2	-.012	2	-.123	1	-.232	2
167		8	max	147.317	1	617.602	3	71.174	4	.005	3	.097	5	.031	2
168			min	-136.613	3	-425.859	2	-30.638	2	-.012	2	-.122	2	-.063	3
169		9	max	147.317	1	802.079	3	79.875	4	.005	3	.143	5	.383	2
170			min	-136.613	3	-547.119	2	-21.136	10	-.012	2	-.139	2	-.575	3
171		10	max	147.317	1	668.378	2	52.402	5	-.001	15	.197	4	.822	2
172			min	-136.613	3	-986.556	3	-80.593	1	-.012	2	-.148	2	-1.221	3
173		11	max	147.317	1	547.119	2	54.341	5	.012	2	.009	3	.383	2
174			min	-136.613	3	-802.079	3	-49.491	1	-.005	3	-.154	4	-.575	3
175		12	max	147.317	1	425.859	2	56.281	5	.012	2	.004	3	.031	2
176			min	-136.613	3	-617.602	3	-27.869	9	-.005	3	-.123	4	-.063	3
177		13	max	147.317	1	304.6	2	58.22	5	.012	2	.001	3	.317	3
178			min	-136.613	3	-433.125	3	-7.565	9	-.005	3	-.123	1	-.232	2
179		14	max	147.317	1	183.341	2	64.58	4	.012	2	0	3	.563	3
180			min	-136.613	3	-248.648	3	-1.282	3	-.005	3	-.103	1	-.408	2
181		15	max	147.317	1	62.081	2	74.916	1	.012	2	.022	5	.676	3
182			min	-136.613	3	-64.171	3	.517	12	-.005	3	-.06	1	-.497	2
183		16	max	147.317	1	120.306	3	106.018	1	.012	2	.067	5	.656	3
184			min	-136.613	3	-59.178	2	1.791	12	-.005	3	-.012	9	-.498	2
185		17	max	147.317	1	304.783	3	137.12	1	.012	2	.126	4	.502	3
186			min	-136.613	3	-180.437	2	3.065	12	-.005	3	.002	12	-.412	2
187		18	max	147.317	1	489.26	3	168.221	1	.012	2	.203	1	.215	3
188			min	-136.613	3	-301.697	2	4.34	12	-.005	3	.005	12	-.238	2
189		19	max	147.317	1	673.737	3	199.323	1	.012	2	.336	1	.037	1
190			min	-136.613	3	-422.956	2	5.614	12	-.005	3	.008	12	-.205	3
191	M12	1	max	22.289	5	631.035	2	45.002	5	0	12	.356	1	.094	2
192			min	-46.284	1	-272.956	3	-204.117	1	-.007	1	-.168	5	.019	9
193		2	max	14.971	3	458.346	2	46.941	5	0	12	.22	1	.211	3
194			min	-46.284	1	-191.339	3	-173.015	1	-.007	1	-.135	5	-.299	2
195		3	max	14.971	3	285.658	2	48.881	5	0	12	.117	2	.32	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
196			min	-46.284	1	-109.721	3	-141.914	1	-.007	1	-.1	5	-.568	2
197		4	max	14.971	3	112.969	2	50.821	5	0	12	.05	2	.37	3
198			min	-46.284	1	-28.104	3	-110.812	1	-.007	1	-.068	4	-.712	2
199		5	max	14.971	3	53.514	3	52.76	5	0	12	.004	10	.361	3
200			min	-46.284	1	-59.719	2	-79.71	1	-.007	1	-.054	1	-.731	2
201		6	max	14.971	3	135.131	3	54.7	5	0	12	.012	5	.293	3
202			min	-46.284	1	-232.408	2	-61.073	2	-.007	1	-.1	1	-.626	2
203		7	max	14.971	3	216.749	3	58.904	4	0	12	.052	5	.165	3
204			min	-46.284	1	-405.097	2	-48.496	2	-.007	1	-.124	1	-.396	2
205		8	max	14.971	3	298.366	3	67.606	4	0	12	.094	5	-.003	15
206			min	-46.95	4	-577.785	2	-35.919	2	-.007	1	-.126	2	-.048	1
207		9	max	14.971	3	379.984	3	76.308	4	0	12	.137	5	.439	2
208			min	-55.472	4	-750.474	2	-24.055	10	-.007	1	-.148	2	-.266	3
209		10	max	14.971	3	923.162	2	85.01	4	0	12	.188	4	1.043	2
210			min	-63.995	4	-187.152	14	-75.799	1	-.007	1	-.16	2	-.569	3
211		11	max	39.626	5	750.474	2	51.63	5	.007	1	.017	3	.439	2
212			min	-46.284	1	-379.984	3	-46.409	9	-.001	5	-.15	4	-.266	3
213		12	max	31.104	5	577.785	2	53.569	5	.007	1	.009	3	0	5
214			min	-46.284	1	-298.366	3	-26.104	9	-.001	5	-.126	2	-.048	1
215		13	max	22.581	5	405.097	2	55.509	5	.007	1	.002	3	.165	3
216			min	-46.284	1	-216.749	3	-8.704	3	-.001	5	-.124	1	-.396	2
217		14	max	14.971	3	232.408	2	62.554	4	.007	1	-.003	12	.293	3
218			min	-46.284	1	-135.131	3	-6.792	3	-.001	5	-.1	1	-.626	2
219		15	max	14.971	3	59.719	2	79.71	1	.007	1	.019	5	.361	3
220			min	-46.284	1	-53.514	3	-4.881	3	-.001	5	-.054	1	-.731	2
221		16	max	14.971	3	28.104	3	110.812	1	.007	1	.063	5	.37	3
222			min	-46.284	1	-112.969	2	-2.969	3	-.001	5	-.011	3	-.712	2
223		17	max	14.971	3	109.721	3	141.914	1	.007	1	.121	4	.32	3
224			min	-46.284	1	-285.658	2	-1.058	3	-.001	5	-.012	3	-.568	2
225		18	max	14.971	3	191.339	3	173.015	1	.007	1	.22	1	.211	3
226			min	-46.284	1	-458.346	2	.854	3	-.001	5	-.012	3	-.299	2
227		19	max	14.971	3	272.956	3	204.117	1	.007	1	.356	1	.094	2
228			min	-46.284	1	-631.035	2	2.176	12	-.001	5	-.011	3	-.027	5
229	M13	1	max	33.715	5	710.628	2	27.888	5	.01	3	.272	1	.167	2
230			min	-111.922	1	-307.733	3	-184.861	1	-.026	2	-.119	5	-.043	3
231		2	max	25.193	5	537.939	2	29.828	5	.01	3	.149	1	.15	3
232			min	-111.922	1	-226.116	3	-153.759	1	-.026	2	-.099	5	-.284	2
233		3	max	16.67	5	365.251	2	31.767	5	.01	3	.072	2	.283	3
234			min	-111.922	1	-144.498	3	-122.657	1	-.026	2	-.076	5	-.61	2
235		4	max	8.148	5	192.562	2	33.707	5	.01	3	.016	10	.358	3
236			min	-111.922	1	-62.881	3	-91.556	1	-.026	2	-.063	4	-.811	2
237		5	max	6.839	3	25.297	1	35.646	5	.01	3	-.003	12	.374	3
238			min	-111.922	1	5.163	15	-60.454	1	-.026	2	-.083	1	-.888	2
239		6	max	6.839	3	100.354	3	37.586	5	.01	3	0	15	.331	3
240			min	-111.922	1	-152.815	2	-45.721	2	-.026	2	-.115	1	-.84	2
241		7	max	6.839	3	181.972	3	44.752	4	.01	3	.027	5	.229	3
242			min	-111.922	1	-325.504	2	-33.145	2	-.026	2	-.125	1	-.667	2
243		8	max	6.839	3	263.589	3	53.454	4	.01	3	.056	5	.068	3
244			min	-111.922	1	-498.192	2	-20.568	2	-.026	2	-.116	2	-.37	2
245		9	max	6.839	3	345.207	3	65.331	14	.01	3	.087	5	.052	2
246			min	-111.922	1	-670.881	2	-16.594	10	-.026	2	-.127	2	-.151	3
247		10	max	6.839	3	426.824	3	95.055	1	.01	3	.131	4	.599	2
248			min	-111.922	1	-843.569	2	-13.13	10	-.026	2	-.128	2	-.43	3
249		11	max	23.901	5	670.881	2	32.72	5	.026	2	.016	3	.052	2
250			min	-111.922	1	-345.207	3	-63.953	1	-.01	3	-.127	2	-.151	3
251		12	max	15.379	5	498.192	2	34.66	5	.026	2	.008	3	.068	3
252			min	-111.922	1	-263.589	3	-35.542	9	-.01	3	-.116	2	-.37	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
253		13	max	6.856	5	325.504	2	36.599	5	.026	2	.003	3	.229	3
254			min	-111.922	1	-181.972	3	-15.238	9	-.01	3	-.125	1	-.667	2
255		14	max	6.839	3	152.815	2	45.721	2	.026	2	-.002	12	.331	3
256			min	-111.922	1	-100.354	3	-5.392	3	-.01	3	-.115	1	-.84	2
257		15	max	6.839	3	5.363	5	60.454	1	.026	2	.017	5	.374	3
258			min	-111.922	1	-25.297	1	-3.48	3	-.01	3	-.083	1	-.888	2
259		16	max	6.839	3	62.881	3	91.556	1	.026	2	.047	5	.358	3
260			min	-111.922	1	-192.562	2	-1.569	3	-.01	3	-.029	9	-.811	2
261		17	max	6.839	3	144.498	3	122.657	1	.026	2	.082	4	.283	3
262			min	-111.922	1	-365.251	2	.343	3	-.01	3	-.008	3	-.61	2
263		18	max	6.839	3	226.116	3	153.759	1	.026	2	.149	1	.15	3
264			min	-111.922	1	-537.939	2	1.741	12	-.01	3	-.007	3	-.284	2
265		19	max	6.839	3	307.733	3	184.861	1	.026	2	.272	1	.167	2
266			min	-111.922	1	-710.628	2	3.016	12	-.01	3	-.004	3	-.043	3
267	M2	1	max	2274.925	2	849.318	3	97.644	2	.006	5	1.246	5	7.143	1
268			min	-1709.496	3	-505.1	2	-280.422	5	-.004	2	-.152	1	.7	12
269		2	max	2272.003	2	849.318	3	97.644	2	.006	5	1.157	5	7.174	1
270			min	-1711.688	3	-505.1	2	-277.89	5	-.004	2	-.123	1	.53	12
271		3	max	2269.081	2	849.318	3	97.644	2	.006	5	1.068	5	7.204	1
272			min	-1713.879	3	-505.1	2	-275.358	5	-.004	2	-.094	1	.359	12
273		4	max	2266.16	2	849.318	3	97.644	2	.006	5	.98	5	7.235	1
274			min	-1716.07	3	-505.1	2	-272.826	5	-.004	2	-.065	1	.189	12
275		5	max	1701.599	2	1556.161	1	69.582	2	.001	2	.899	5	6.99	1
276			min	-1486.444	3	22.889	12	-258.375	5	0	3	-.067	1	.103	12
277		6	max	1698.678	2	1556.161	1	69.582	2	.001	2	.818	4	6.491	1
278			min	-1488.635	3	22.889	12	-255.843	5	0	3	-.046	1	.095	12
279		7	max	1695.756	2	1556.161	1	69.582	2	.001	2	.738	4	5.992	1
280			min	-1490.827	3	22.889	12	-253.311	5	0	3	-.042	3	.088	12
281		8	max	1692.834	2	1556.161	1	69.582	2	.001	2	.659	4	5.492	1
282			min	-1493.018	3	22.889	12	-250.779	5	0	3	-.075	3	.081	12
283		9	max	1689.912	2	1556.161	1	69.582	2	.001	2	.581	4	4.993	1
284			min	-1495.209	3	22.889	12	-248.247	5	0	3	-.108	3	.073	12
285		10	max	1686.991	2	1556.161	1	69.582	2	.001	2	.504	4	4.494	1
286			min	-1497.401	3	22.889	12	-245.714	5	0	3	-.141	3	.066	12
287		11	max	1684.069	2	1556.161	1	69.582	2	.001	2	.427	4	3.995	1
288			min	-1499.592	3	22.889	12	-243.182	5	0	3	-.175	3	.059	12
289		12	max	1681.147	2	1556.161	1	69.582	2	.001	2	.352	4	3.495	1
290			min	-1501.783	3	22.889	12	-240.65	5	0	3	-.208	3	.051	12
291		13	max	1678.225	2	1556.161	1	69.582	2	.001	2	.277	4	2.996	1
292			min	-1503.974	3	22.889	12	-238.118	5	0	3	-.241	3	.044	12
293		14	max	1675.304	2	1556.161	1	69.582	2	.001	2	.203	4	2.497	1
294			min	-1506.166	3	22.889	12	-235.586	5	0	3	-.274	3	.037	12
295		15	max	1672.382	2	1556.161	1	69.582	2	.001	2	.166	2	1.997	1
296			min	-1508.357	3	22.889	12	-233.054	5	0	3	-.308	3	.029	12
297		16	max	1669.46	2	1556.161	1	69.582	2	.001	2	.188	2	1.498	1
298			min	-1510.548	3	22.889	12	-230.521	5	0	3	-.341	3	.022	12
299		17	max	1666.539	2	1556.161	1	69.582	2	.001	2	.211	2	.999	1
300			min	-1512.74	3	22.889	12	-227.989	5	0	3	-.374	3	.015	12
301		18	max	1663.617	2	1556.161	1	69.582	2	.001	2	.233	2	.499	1
302			min	-1514.931	3	22.889	12	-225.457	5	0	3	-.408	3	.007	12
303		19	max	1660.695	2	1556.161	1	69.582	2	.001	2	.255	2	0	1
304			min	-1517.122	3	22.889	12	-222.925	5	0	3	-.441	3	0	1
305	M5	1	max	5708.672	2	2471.509	3	0	1	.007	4	1.291	4	9.586	1
306			min	-4990.852	3	-2620.736	2	-293.956	5	0	1	0	1	.302	15
307		2	max	5705.75	2	2471.509	3	0	1	.007	4	1.197	4	10.104	1
308			min	-4993.044	3	-2620.736	2	-291.423	5	0	1	0	1	.307	15
309		3	max	5702.828	2	2471.509	3	0	1	.007	4	1.104	4	10.622	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
310			min	-4995.235	3	-2620.736	2	-288.891	5	0	1	0	1	.312	15
311		4	max	5699.906	2	2471.509	3	0	1	.007	4	1.012	4	11.139	1
312			min	-4997.426	3	-2620.736	2	-286.359	5	0	1	0	1	-.09	3
313		5	max	4321.873	2	2445.253	2	0	1	0	1	.929	4	10.984	2
314			min	-4260.645	3	-101.13	3	-274.634	4	0	4	0	1	-.454	3
315		6	max	4318.951	2	2445.253	2	0	1	0	1	.841	4	10.2	2
316			min	-4262.837	3	-101.13	3	-272.102	4	0	4	0	1	-.422	3
317		7	max	4316.029	2	2445.253	2	0	1	0	1	.754	4	9.415	2
318			min	-4265.028	3	-101.13	3	-269.569	4	0	4	0	1	-.389	3
319		8	max	4313.108	2	2445.253	2	0	1	0	1	.668	4	8.631	2
320			min	-4267.219	3	-101.13	3	-267.037	4	0	4	0	1	-.357	3
321		9	max	4310.186	2	2445.253	2	0	1	0	1	.583	4	7.846	2
322			min	-4269.41	3	-101.13	3	-264.505	4	0	4	0	1	-.324	3
323		10	max	4307.264	2	2445.253	2	0	1	0	1	.498	4	7.061	2
324			min	-4271.602	3	-101.13	3	-261.973	4	0	4	0	1	-.292	3
325		11	max	4304.342	2	2445.253	2	0	1	0	1	.415	4	6.277	2
326			min	-4273.793	3	-101.13	3	-259.441	4	0	4	0	1	-.26	3
327		12	max	4301.421	2	2445.253	2	0	1	0	1	.332	4	5.492	2
328			min	-4275.984	3	-101.13	3	-256.909	4	0	4	0	1	-.227	3
329		13	max	4298.499	2	2445.253	2	0	1	0	1	.25	4	4.708	2
330			min	-4278.176	3	-101.13	3	-254.376	4	0	4	0	1	-.195	3
331		14	max	4295.577	2	2445.253	2	0	1	0	1	.168	4	3.923	2
332			min	-4280.367	3	-101.13	3	-251.844	4	0	4	0	1	-.162	3
333		15	max	4292.655	2	2445.253	2	0	1	0	1	.088	4	3.138	2
334			min	-4282.558	3	-101.13	3	-249.312	4	0	4	0	1	-.13	3
335		16	max	4289.734	2	2445.253	2	0	1	0	1	.008	4	2.354	2
336			min	-4284.75	3	-101.13	3	-246.78	4	0	4	0	1	-.097	3
337		17	max	4286.812	2	2445.253	2	0	1	0	1	0	1	1.569	2
338			min	-4286.941	3	-101.13	3	-244.248	4	0	4	-.07	4	-.065	3
339		18	max	4283.89	2	2445.253	2	0	1	0	1	0	1	.785	2
340			min	-4289.132	3	-101.13	3	-241.716	4	0	4	-.148	4	-.032	3
341		19	max	4280.969	2	2445.253	2	0	1	0	1	0	1	0	1
342			min	-4291.323	3	-101.13	3	-239.183	4	0	4	-.225	4	0	1
343	M8	1	max	2274.925	2	849.318	3	113.934	3	.007	4	1.291	4	7.143	1
344			min	-1709.496	3	-505.1	2	-299.156	4	-.002	3	-.156	3	-.519	5
345		2	max	2272.003	2	849.318	3	113.934	3	.007	4	1.196	4	7.174	1
346			min	-1711.688	3	-505.1	2	-296.623	4	-.002	3	-.119	3	-.469	5
347		3	max	2269.081	2	849.318	3	113.934	3	.007	4	1.101	4	7.204	1
348			min	-1713.879	3	-505.1	2	-294.091	4	-.002	3	-.083	3	-.419	5
349		4	max	2266.16	2	849.318	3	113.934	3	.007	4	1.007	4	7.235	1
350			min	-1716.07	3	-505.1	2	-291.559	4	-.002	3	-.046	3	-.369	5
351		5	max	1701.599	2	1556.161	1	103.697	3	0	3	.925	4	6.99	1
352			min	-1486.444	3	-73.993	5	-274.602	4	-.001	2	-.025	3	-.332	5
353		6	max	1698.678	2	1556.161	1	103.697	3	0	3	.837	4	6.491	1
354			min	-1488.635	3	-73.993	5	-272.07	4	-.001	2	.005	12	-.309	5
355		7	max	1695.756	2	1556.161	1	103.697	3	0	3	.75	4	5.992	1
356			min	-1490.827	3	-73.993	5	-269.538	4	-.001	2	.005	10	-.285	5
357		8	max	1692.834	2	1556.161	1	103.697	3	0	3	.664	4	5.492	1
358			min	-1493.018	3	-73.993	5	-267.006	4	-.001	2	-.01	2	-.261	5
359		9	max	1689.912	2	1556.161	1	103.697	3	0	3	.579	4	4.993	1
360			min	-1495.209	3	-73.993	5	-264.474	4	-.001	2	-.032	2	-.237	5
361		10	max	1686.991	2	1556.161	1	103.697	3	0	3	.494	4	4.494	1
362			min	-1497.401	3	-73.993	5	-261.941	4	-.001	2	-.054	2	-.214	5
363		11	max	1684.069	2	1556.161	1	103.697	3	0	3	.412	5	3.995	1
364			min	-1499.592	3	-73.993	5	-259.409	4	-.001	2	-.077	2	-.19	5
365		12	max	1681.147	2	1556.161	1	103.697	3	0	3	.333	5	3.495	1
366			min	-1501.783	3	-73.993	5	-256.877	4	-.001	2	-.099	2	-.166	5

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
367		13	max	1678.225	2	1556.161	1	103.697	3	0	3	.255	5	2.996	1
368			min	-1503.974	3	-73.993	5	-254.345	4	-.001	2	-.121	2	-.142	5
369		14	max	1675.304	2	1556.161	1	103.697	3	0	3	.274	3	2.497	1
370			min	-1506.166	3	-73.993	5	-251.813	4	-.001	2	-.144	2	-.119	5
371		15	max	1672.382	2	1556.161	1	103.697	3	0	3	.308	3	1.997	1
372			min	-1508.357	3	-73.993	5	-249.281	4	-.001	2	-.166	2	-.095	5
373		16	max	1669.46	2	1556.161	1	103.697	3	0	3	.341	3	1.498	1
374			min	-1510.548	3	-73.993	5	-246.748	4	-.001	2	-.188	2	-.071	5
375		17	max	1666.539	2	1556.161	1	103.697	3	0	3	.374	3	.999	1
376			min	-1512.74	3	-73.993	5	-244.216	4	-.001	2	-.211	2	-.047	5
377		18	max	1663.617	2	1556.161	1	103.697	3	0	3	.408	3	.499	1
378			min	-1514.931	3	-73.993	5	-241.684	4	-.001	2	-.233	2	-.024	5
379		19	max	1660.695	2	1556.161	1	103.697	3	0	3	.441	3	0	1
380			min	-1517.122	3	-73.993	5	-239.152	4	-.001	2	-.255	2	0	1
381	M3	1	max	2076.599	2	5.879	4	27.544	2	.014	3	.006	4	0	1
382			min	-850.207	3	1.382	15	-12.406	5	-.033	2	-.002	3	0	1
383		2	max	2076.453	2	5.226	4	27.544	2	.014	3	.014	2	0	15
384			min	-850.317	3	1.228	15	-11.947	5	-.033	2	-.006	3	-.002	4
385		3	max	2076.306	2	4.572	4	27.544	2	.014	3	.024	2	0	15
386			min	-850.427	3	1.075	15	-11.488	5	-.033	2	-.009	3	-.004	4
387		4	max	2076.16	2	3.919	4	27.544	2	.014	3	.034	2	-.001	15
388			min	-850.537	3	.921	15	-11.029	5	-.033	2	-.013	3	-.005	4
389		5	max	2076.013	2	3.266	4	27.544	2	.014	3	.044	2	-.002	15
390			min	-850.647	3	.768	15	-10.695	3	-.033	2	-.017	3	-.007	4
391		6	max	2075.866	2	2.613	4	27.544	2	.014	3	.053	2	-.002	15
392			min	-850.757	3	.614	15	-10.695	3	-.033	2	-.021	3	-.008	4
393		7	max	2075.72	2	1.96	4	27.544	2	.014	3	.063	2	-.002	15
394			min	-850.867	3	.461	15	-10.695	3	-.033	2	-.025	3	-.008	4
395		8	max	2075.573	2	1.306	4	27.544	2	.014	3	.073	2	-.002	15
396			min	-850.976	3	.307	15	-10.695	3	-.033	2	-.029	3	-.009	4
397		9	max	2075.426	2	.653	4	27.544	2	.014	3	.083	2	-.002	15
398			min	-851.086	3	.154	15	-10.695	3	-.033	2	-.032	3	-.009	4
399		10	max	2075.28	2	0	1	27.544	2	.014	3	.093	2	-.002	15
400			min	-851.196	3	0	1	-10.695	3	-.033	2	-.036	3	-.009	4
401		11	max	2075.133	2	-.154	15	27.544	2	.014	3	.103	2	-.002	15
402			min	-851.306	3	-.653	6	-10.695	3	-.033	2	-.04	3	-.009	4
403		12	max	2074.987	2	-.307	15	27.544	2	.014	3	.113	2	-.002	15
404			min	-851.416	3	-1.306	6	-10.695	3	-.033	2	-.044	3	-.009	4
405		13	max	2074.84	2	-.461	15	27.544	2	.014	3	.122	2	-.002	15
406			min	-851.526	3	-1.96	6	-10.695	3	-.033	2	-.048	3	-.008	4
407		14	max	2074.693	2	-.614	15	27.544	2	.014	3	.132	2	-.002	15
408			min	-851.636	3	-2.613	6	-10.695	3	-.033	2	-.051	3	-.008	4
409		15	max	2074.547	2	-.768	15	27.544	2	.014	3	.142	2	-.002	15
410			min	-851.746	3	-3.266	6	-10.695	3	-.033	2	-.055	3	-.007	4
411		16	max	2074.4	2	-.921	15	27.544	2	.014	3	.152	2	-.001	15
412			min	-851.856	3	-3.919	6	-10.695	3	-.033	2	-.059	3	-.005	4
413		17	max	2074.254	2	-1.075	15	27.544	2	.014	3	.162	2	0	15
414			min	-851.966	3	-4.572	6	-10.695	3	-.033	2	-.063	3	-.004	4
415		18	max	2074.107	2	-1.228	15	27.544	2	.014	3	.172	2	0	15
416			min	-852.076	3	-5.226	6	-10.695	3	-.033	2	-.067	3	-.002	4
417		19	max	2073.96	2	-1.382	15	27.544	2	.014	3	.181	2	0	1
418			min	-852.186	3	-5.879	6	-10.695	3	-.033	2	-.071	3	0	1
419	M6	1	max	5206.809	2	5.879	4	0	1	.008	4	.005	4	0	1
420			min	-2678.298	3	1.382	15	-13.428	4	0	1	0	1	0	1
421		2	max	5206.663	2	5.226	4	0	1	.008	4	0	4	0	15
422			min	-2678.408	3	1.228	15	-12.969	4	0	1	0	1	-.002	4
423		3	max	5206.516	2	4.572	4	0	1	.008	4	0	1	0	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
424			min	-2678.517	3	1.075	15	-12.51	4	0	1	-.004	4	-.004	4
425		4	max	5206.369	2	3.919	4	0	1	.008	4	0	1	-.001	15
426			min	-2678.627	3	.921	15	-12.051	4	0	1	-.008	4	-.005	4
427		5	max	5206.223	2	3.266	4	0	1	.008	4	0	1	-.002	15
428			min	-2678.737	3	.768	15	-11.592	4	0	1	-.013	4	-.007	4
429		6	max	5206.076	2	2.613	4	0	1	.008	4	0	1	-.002	15
430			min	-2678.847	3	.614	15	-11.133	4	0	1	-.017	4	-.008	4
431		7	max	5205.93	2	1.96	4	0	1	.008	4	0	1	-.002	15
432			min	-2678.957	3	.461	15	-10.673	4	0	1	-.021	4	-.008	4
433		8	max	5205.783	2	1.306	4	0	1	.008	4	0	1	-.002	15
434			min	-2679.067	3	.307	15	-10.214	4	0	1	-.024	4	-.009	4
435		9	max	5205.636	2	.653	4	0	1	.008	4	0	1	-.002	15
436			min	-2679.177	3	.154	15	-9.755	4	0	1	-.028	4	-.009	4
437		10	max	5205.49	2	0	1	0	1	.008	4	0	1	-.002	15
438			min	-2679.287	3	0	1	-9.296	4	0	1	-.031	4	-.009	4
439		11	max	5205.343	2	-.154	15	0	1	.008	4	0	1	-.002	15
440			min	-2679.397	3	-.653	6	-8.837	4	0	1	-.034	4	-.009	4
441		12	max	5205.197	2	-.307	15	0	1	.008	4	0	1	-.002	15
442			min	-2679.507	3	-1.306	6	-8.378	4	0	1	-.038	4	-.009	4
443		13	max	5205.05	2	-.461	15	0	1	.008	4	0	1	-.002	15
444			min	-2679.617	3	-1.96	6	-7.919	4	0	1	-.04	4	-.008	4
445		14	max	5204.903	2	-.614	15	0	1	.008	4	0	1	-.002	15
446			min	-2679.727	3	-2.613	6	-7.46	4	0	1	-.043	4	-.008	4
447		15	max	5204.757	2	-.768	15	0	1	.008	4	0	1	-.002	15
448			min	-2679.837	3	-3.266	6	-7.001	4	0	1	-.046	4	-.007	4
449		16	max	5204.61	2	-.921	15	0	1	.008	4	0	1	-.001	15
450			min	-2679.947	3	-3.919	6	-6.542	4	0	1	-.048	4	-.005	4
451		17	max	5204.464	2	-1.075	15	0	1	.008	4	0	1	0	15
452			min	-2680.057	3	-4.572	6	-6.083	4	0	1	-.05	4	-.004	4
453		18	max	5204.317	2	-1.228	15	0	1	.008	4	0	1	0	15
454			min	-2680.167	3	-5.226	6	-5.624	4	0	1	-.053	4	-.002	4
455		19	max	5204.17	2	-1.382	15	0	1	.008	4	0	1	0	1
456			min	-2680.277	3	-5.879	6	-5.165	4	0	1	-.054	4	0	1
457	M9	1	max	2076.599	2	5.879	6	10.695	3	.033	2	.005	5	0	1
458			min	-850.207	3	1.382	15	-27.544	2	-.014	3	-.004	2	0	1
459		2	max	2076.453	2	5.226	6	10.695	3	.033	2	.006	3	0	15
460			min	-850.317	3	1.228	15	-27.544	2	-.014	3	-.014	2	-.002	6
461		3	max	2076.306	2	4.572	6	10.695	3	.033	2	.009	3	0	15
462			min	-850.427	3	1.075	15	-27.544	2	-.014	3	-.024	2	-.004	6
463		4	max	2076.16	2	3.919	6	10.695	3	.033	2	.013	3	-.001	15
464			min	-850.537	3	.921	15	-27.544	2	-.014	3	-.034	2	-.005	6
465		5	max	2076.013	2	3.266	6	10.695	3	.033	2	.017	3	-.002	15
466			min	-850.647	3	.768	15	-27.544	2	-.014	3	-.044	2	-.007	6
467		6	max	2075.866	2	2.613	6	10.695	3	.033	2	.021	3	-.002	15
468			min	-850.757	3	.614	15	-27.544	2	-.014	3	-.053	2	-.008	6
469		7	max	2075.72	2	1.96	6	10.695	3	.033	2	.025	3	-.002	15
470			min	-850.867	3	.461	15	-27.544	2	-.014	3	-.063	2	-.008	6
471		8	max	2075.573	2	1.306	6	10.695	3	.033	2	.029	3	-.002	15
472			min	-850.976	3	.307	15	-27.544	2	-.014	3	-.073	2	-.009	6
473		9	max	2075.426	2	.653	6	10.695	3	.033	2	.032	3	-.002	15
474			min	-851.086	3	.154	15	-27.544	2	-.014	3	-.083	2	-.009	6
475		10	max	2075.28	2	0	1	10.695	3	.033	2	.036	3	-.002	15
476			min	-851.196	3	0	1	-27.544	2	-.014	3	-.093	2	-.009	6
477		11	max	2075.133	2	-.154	15	10.695	3	.033	2	.04	3	-.002	15
478			min	-851.306	3	-.653	4	-27.544	2	-.014	3	-.103	2	-.009	6
479		12	max	2074.987	2	-.307	15	10.695	3	.033	2	.044	3	-.002	15
480			min	-851.416	3	-1.306	4	-27.544	2	-.014	3	-.113	2	-.009	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
481		13	max	2074.84	2	-.461	15	10.695	3	.033	2	.048	3	-.002	15
482			min	-851.526	3	-1.96	4	-27.544	2	-.014	3	-.122	2	-.008	6
483		14	max	2074.693	2	-.614	15	10.695	3	.033	2	.051	3	-.002	15
484			min	-851.636	3	-2.613	4	-27.544	2	-.014	3	-.132	2	-.008	6
485		15	max	2074.547	2	-.768	15	10.695	3	.033	2	.055	3	-.002	15
486			min	-851.746	3	-3.266	4	-27.544	2	-.014	3	-.142	2	-.007	6
487		16	max	2074.4	2	-.921	15	10.695	3	.033	2	.059	3	-.001	15
488			min	-851.856	3	-3.919	4	-27.544	2	-.014	3	-.152	2	-.005	6
489		17	max	2074.254	2	-1.075	15	10.695	3	.033	2	.063	3	0	15
490			min	-851.966	3	-4.572	4	-27.544	2	-.014	3	-.162	2	-.004	6
491		18	max	2074.107	2	-1.228	15	10.695	3	.033	2	.067	3	0	15
492			min	-852.076	3	-5.226	4	-27.544	2	-.014	3	-.172	2	-.002	6
493		19	max	2073.96	2	-1.382	15	10.695	3	.033	2	.071	3	0	1
494			min	-852.186	3	-5.879	4	-27.544	2	-.014	3	-.181	2	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	-.014	12	.112	3	.009	1	6.926e-3	3	NC	3	NC	1
2			min	-.477	1	-1.025	2	-.587	4	-1.972e-2	2	105.574	1	307.923	5
3		2	max	-.014	12	.075	3	0	3	6.645e-3	3	6137.697	12	NC	2
4			min	-.477	1	-.876	2	-.568	4	-1.863e-2	2	117.624	1	322.072	4
5		3	max	-.014	12	.039	3	0	3	6.095e-3	3	3137.235	12	NC	3
6			min	-.477	1	-.737	1	-.543	4	-1.651e-2	2	132.392	1	341.579	4
7		4	max	-.014	12	.008	3	.001	3	5.544e-3	3	2205.925	12	NC	3
8			min	-.477	1	-.612	1	-.513	4	-1.438e-2	2	149.915	1	368.434	4
9		5	max	-.014	12	-.01	12	.002	3	5.197e-3	3	1810.248	12	NC	3
10			min	-.477	1	-.502	1	-.479	4	-1.277e-2	2	169.579	1	403.686	4
11		6	max	-.014	12	-.018	12	.002	3	5.37e-3	3	1639.864	12	NC	1
12			min	-.476	1	-.411	1	-.445	4	-1.247e-2	2	190.418	1	447.799	4
13		7	max	-.014	12	-.022	12	.001	3	5.544e-3	3	1689.181	15	NC	1
14			min	-.475	1	-.332	1	-.411	4	-1.218e-2	2	212.968	1	500.913	4
15		8	max	-.014	12	-.024	12	0	1	5.718e-3	3	1839.407	15	NC	1
16			min	-.475	1	-.261	1	-.38	4	-1.188e-2	2	238.592	1	560.529	5
17		9	max	-.015	12	-.021	15	0	10	6.178e-3	3	2018.431	15	NC	1
18			min	-.474	1	-.191	1	-.353	4	-1.098e-2	2	270.258	1	628.752	5
19		10	max	-.015	12	-.014	15	0	2	6.907e-3	3	2236.898	15	NC	1
20			min	-.474	1	-.121	1	-.324	4	-9.486e-3	2	312.077	1	722.116	5
21		11	max	-.015	12	-.007	15	0	1	7.637e-3	3	2509.371	15	NC	1
22			min	-.473	1	-.05	1	-.294	4	-7.996e-3	2	369.753	1	850.612	5
23		12	max	-.015	12	.023	2	.003	3	7.103e-3	3	2858.44	15	NC	1
24			min	-.472	1	-.04	3	-.265	4	-6.357e-3	2	454.657	1	1029.58	5
25		13	max	-.015	12	.092	1	.007	3	5.229e-3	3	3322.761	15	NC	1
26			min	-.471	1	-.037	3	-.234	4	-4.56e-3	2	586.954	1	1334.779	5
27		14	max	-.015	12	.157	1	.011	3	3.354e-3	3	3972.746	15	NC	1
28			min	-.471	1	-.023	3	-.202	4	-4.057e-3	4	802.088	1	1882.623	5
29		15	max	-.016	12	.212	1	.01	3	1.479e-3	3	4949.533	15	NC	1
30			min	-.47	1	.006	12	-.175	4	-4.998e-3	4	1166.763	1	2879.388	5
31		16	max	-.016	12	.254	1	.01	1	4.158e-3	3	6584.511	15	NC	2
32			min	-.47	1	.028	15	-.156	5	-4.337e-3	4	1779.879	1	4634.256	5
33		17	max	-.016	12	.285	1	.011	1	7.371e-3	3	9866.982	15	NC	2
34			min	-.47	1	.035	15	-.142	5	-3.487e-3	4	2938.981	1	8038.302	1
35		18	max	-.016	12	.31	1	.006	1	1.058e-2	3	NC	5	NC	1
36			min	-.47	1	.042	15	-.133	4	-4.115e-3	2	1280.905	3	NC	1
37		19	max	-.016	12	.333	1	0	12	1.222e-2	3	NC	1	NC	1
38			min	-.47	1	.05	15	-.128	4	-4.703e-3	2	709.237	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
39	M4	1	max	-.002	3	.295	3	0	1	9.098e-4	4	NC	3	NC	1
40			min	-.729	1	-1.728	2	-.587	4	0	1	69.253	2	308.206	4
41		2	max	-.002	3	.213	3	0	1	7.228e-4	4	2898.157	15	NC	1
42			min	-.729	1	-1.464	2	-.569	4	0	1	79.533	2	320.2	4
43		3	max	-.002	3	.136	3	0	1	3.566e-4	5	3254.027	15	NC	1
44			min	-.728	1	-1.207	2	-.545	4	0	1	92.938	2	338.831	4
45		4	max	-.002	3	.071	3	0	1	0	1	3672.422	15	NC	1
46			min	-.728	1	-.975	2	-.514	4	-1.06e-5	4	107.764	1	365.503	4
47		5	max	-.002	3	.029	3	0	1	0	1	4131.91	15	NC	1
48			min	-.728	1	-.79	1	-.48	4	-2.281e-4	4	124.12	1	401.282	4
49		6	max	-.003	3	.011	3	0	1	0	1	4603.464	15	NC	1
50			min	-.727	1	-.657	1	-.444	4	-6.2e-5	4	140.558	1	446.157	4
51		7	max	-.003	3	.009	3	0	1	1.052e-4	5	5106.311	15	NC	1
52			min	-.725	1	-.548	1	-.41	4	0	1	157.451	1	499.672	4
53		8	max	-.004	12	.014	3	0	1	2.702e-4	4	5687.139	15	NC	1
54			min	-.724	1	-.451	1	-.38	4	0	1	176.435	1	559.663	4
55		9	max	-.005	12	.016	3	0	1	2.746e-4	4	6444.286	15	NC	1
56			min	-.722	1	-.354	2	-.353	4	0	1	201.534	1	625.208	4
57		10	max	-.005	12	.009	3	0	1	1.266e-4	4	7521.854	15	NC	1
58			min	-.721	1	-.247	2	-.323	4	0	1	238.75	1	720.402	4
59		11	max	-.005	12	-.003	12	0	1	0	1	9144.427	15	NC	1
60			min	-.72	1	-.131	2	-.293	4	-2.137e-5	4	297.749	1	850.619	4
61		12	max	-.006	12	.003	9	0	1	0	1	NC	15	NC	1
62			min	-.718	1	-.026	3	-.266	4	-7.605e-4	4	403.744	1	1015.635	4
63		13	max	-.006	12	.126	1	0	1	0	1	NC	5	NC	1
64			min	-.717	1	-.045	3	-.236	4	-2.128e-3	4	416.882	3	1298.537	4
65		14	max	-.007	12	.237	1	0	1	0	1	NC	5	NC	1
66			min	-.715	1	-.043	3	-.205	4	-3.494e-3	4	419.943	3	1811.03	4
67		15	max	-.007	12	.321	1	0	1	0	1	NC	2	NC	1
68			min	-.714	1	.002	12	-.178	4	-4.861e-3	4	484.118	3	2737.582	4
69		16	max	-.007	12	.364	1	0	1	0	1	NC	1	NC	1
70			min	-.714	1	.011	15	-.159	4	-3.898e-3	4	758.889	3	4351.866	4
71		17	max	-.008	12	.374	1	0	1	0	1	NC	4	NC	1
72			min	-.714	1	.012	15	-.145	4	-2.661e-3	4	3745.918	2	7713.773	4
73		18	max	-.008	12	.443	3	0	1	0	1	NC	1	NC	1
74			min	-.714	1	.012	15	-.135	4	-1.424e-3	4	952.801	3	NC	1
75		19	max	-.008	12	.634	3	0	1	0	1	NC	1	NC	1
76			min	-.714	1	.012	15	-.127	4	-7.935e-4	4	417.95	3	NC	1
77	M7	1	max	.025	5	.112	3	0	3	1.972e-2	2	NC	3	NC	1
78			min	-.477	1	-1.025	2	-.591	4	-6.926e-3	3	105.574	1	303.616	4
79		2	max	.025	5	.075	3	.007	1	1.863e-2	2	NC	5	NC	2
80			min	-.477	1	-.876	2	-.565	4	-6.645e-3	3	117.624	1	321.596	4
81		3	max	.025	5	.039	3	.015	1	1.651e-2	2	NC	5	NC	3
82			min	-.477	1	-.737	1	-.537	4	-6.095e-3	3	132.392	1	343.835	4
83		4	max	.025	5	.027	5	.016	1	1.438e-2	2	NC	5	NC	3
84			min	-.477	1	-.612	1	-.506	4	-5.544e-3	3	149.915	1	371.59	4
85		5	max	.025	5	.025	5	.014	1	1.277e-2	2	NC	5	NC	3
86			min	-.477	1	-.502	1	-.474	4	-5.197e-3	3	169.579	1	406.169	4
87		6	max	.025	5	.022	5	.009	1	1.247e-2	2	NC	5	NC	1
88			min	-.476	1	-.411	1	-.441	4	-5.37e-3	3	190.418	1	447.51	4
89		7	max	.025	5	.019	5	.003	2	1.218e-2	2	NC	5	NC	1
90			min	-.475	1	-.332	1	-.41	4	-5.544e-3	3	212.968	1	496.17	4
91		8	max	.025	5	.015	5	0	10	1.188e-2	2	NC	5	NC	1
92			min	-.475	1	-.261	1	-.381	4	-5.718e-3	3	238.592	1	553.174	4
93		9	max	.025	5	.011	5	0	3	1.098e-2	2	NC	5	NC	1
94			min	-.474	1	-.191	1	-.353	4	-6.178e-3	3	270.258	1	620.811	4
95		10	max	.025	5	.008	5	.001	3	9.486e-3	2	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
96			min	-.474	1	-.121	1	-.324	4	-6.907e-3	3	312.077	1	711.18	4
97		11	max	.025	5	.004	5	0	3	7.996e-3	2	NC	5	NC	1
98			min	-.473	1	-.05	1	-.294	4	-7.637e-3	3	369.753	1	835.805	4
99		12	max	.025	5	.023	2	.003	1	6.357e-3	2	NC	4	NC	1
100			min	-.472	1	-.04	3	-.264	4	-7.103e-3	3	454.657	1	1015.917	4
101		13	max	.025	5	.092	1	.005	2	4.56e-3	2	NC	4	NC	1
102			min	-.471	1	-.037	3	-.232	4	-5.229e-3	3	586.954	1	1315.354	4
103		14	max	.025	5	.157	1	.003	2	2.763e-3	2	NC	4	NC	1
104			min	-.471	1	-.023	3	-.202	4	-3.54e-3	5	802.088	1	1827.735	4
105		15	max	.025	5	.212	1	0	10	9.659e-4	2	NC	4	NC	1
106			min	-.47	1	-.011	5	-.177	4	-4.777e-3	5	1166.763	1	2681.995	4
107		16	max	.025	5	.254	1	-.003	10	1.809e-3	2	NC	4	NC	2
108			min	-.47	1	-.017	5	-.16	4	-4.158e-3	3	1779.879	1	3983.472	4
109		17	max	.025	5	.285	1	-.002	12	2.962e-3	2	NC	4	NC	2
110			min	-.47	1	-.024	5	-.147	4	-7.371e-3	3	2938.981	1	6312.086	4
111		18	max	.025	5	.31	1	0	12	4.115e-3	2	NC	4	NC	1
112			min	-.47	1	-.031	5	-.136	4	-1.058e-2	3	1280.905	3	NC	1
113		19	max	.025	5	.333	1	.008	1	4.703e-3	2	NC	1	NC	1
114			min	-.47	1	-.039	5	-.125	4	-1.222e-2	3	709.237	3	NC	1
115	M10	1	max	0	1	.322	1	.47	1	1.13e-2	3	NC	1	NC	1
116			min	-.13	4	-.035	5	-.025	5	-9.45e-4	5	NC	1	NC	1
117		2	max	0	1	.376	3	.497	1	1.272e-2	3	NC	4	NC	3
118			min	-.13	4	-.025	5	-.016	5	-8.364e-4	5	1449.768	3	5814.314	1
119		3	max	0	1	.476	3	.537	1	1.414e-2	3	NC	4	NC	3
120			min	-.13	4	-.018	5	-.008	5	-7.279e-4	5	752.203	3	2340.184	1
121		4	max	0	1	.555	3	.581	1	1.556e-2	3	NC	4	NC	3
122			min	-.13	4	-.012	5	-.002	15	-6.193e-4	5	545.164	3	1403.548	1
123		5	max	0	1	.605	3	.624	1	1.698e-2	3	NC	4	NC	3
124			min	-.13	4	-.008	5	.002	15	-5.107e-4	5	464.019	3	1014.247	1
125		6	max	0	1	.624	3	.66	1	1.841e-2	3	NC	4	NC	3
126			min	-.13	4	-.003	5	.005	15	-5.695e-4	2	439.025	3	820.893	1
127		7	max	0	1	.615	3	.687	1	1.983e-2	3	NC	4	NC	3
128			min	-.13	4	0	15	.009	15	-1.112e-3	2	449.69	3	718.597	1
129		8	max	0	1	.588	3	.704	1	2.125e-2	3	NC	1	NC	3
130			min	-.13	4	.004	15	.01	12	-1.654e-3	2	487.863	3	666.401	1
131		9	max	0	1	.557	3	.712	1	2.267e-2	3	NC	4	NC	3
132			min	-.13	4	.008	15	.008	12	-2.197e-3	2	541.17	3	639.283	2
133		10	max	0	1	.541	3	.714	1	2.409e-2	3	NC	4	NC	3
134			min	-.13	4	.012	15	.008	12	-2.739e-3	2	572.913	3	625.55	2
135		11	max	0	12	.557	3	.712	1	2.267e-2	3	NC	4	NC	3
136			min	-.13	4	.016	15	.008	12	-2.197e-3	2	541.17	3	639.283	2
137		12	max	0	12	.588	3	.704	1	2.125e-2	3	NC	1	NC	3
138			min	-.13	4	.018	15	.01	12	-1.654e-3	2	487.863	3	666.401	1
139		13	max	0	12	.615	3	.687	1	1.983e-2	3	NC	4	NC	3
140			min	-.13	4	.019	15	.012	12	-1.112e-3	2	449.69	3	718.597	1
141		14	max	0	12	.624	3	.66	1	1.841e-2	3	NC	5	NC	3
142			min	-.13	4	.021	15	.014	12	-5.695e-4	2	439.025	3	820.893	1
143		15	max	0	12	.605	3	.624	1	1.698e-2	3	NC	5	NC	3
144			min	-.13	4	.023	15	.015	12	-1.898e-4	10	464.019	3	1014.247	1
145		16	max	0	12	.555	3	.581	1	1.556e-2	3	NC	5	NC	3
146			min	-.13	4	.027	15	.016	12	1.074e-4	10	545.164	3	1403.548	1
147		17	max	0	12	.476	3	.537	1	1.414e-2	3	NC	5	NC	3
148			min	-.13	4	.031	15	.017	12	4.047e-4	10	752.203	3	2340.184	1
149		18	max	0	12	.376	3	.497	1	1.272e-2	3	NC	4	NC	3
150			min	-.13	4	.038	15	.017	12	7.019e-4	10	1449.768	3	5814.314	1
151		19	max	0	12	.322	1	.47	1	1.13e-2	3	NC	1	NC	1
152			min	-.13	4	.046	15	.016	12	9.113e-4	15	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
153	M11	1	max	0	1	.003	5	.472	1	9.079e-3	1	NC	1	NC	1
154			min	-.279	4	-.04	3	-.025	5	-4.299e-4	5	NC	1	NC	1
155		2	max	0	1	.03	3	.491	1	9.827e-3	1	NC	4	NC	2
156			min	-.279	4	-.072	2	-.001	15	-3.234e-4	3	2220.256	3	7107.59	4
157		3	max	0	1	.092	3	.527	1	1.058e-2	1	NC	4	NC	3
158			min	-.279	4	-.123	2	.007	15	-6.151e-4	3	1181.202	3	2878.935	1
159		4	max	0	1	.134	3	.57	1	1.132e-2	1	NC	4	NC	3
160			min	-.279	4	-.158	2	.009	15	-9.068e-4	3	898.869	3	1596.66	1
161		5	max	0	1	.149	3	.614	1	1.207e-2	1	NC	5	NC	3
162			min	-.279	4	-.172	2	.007	15	-1.199e-3	3	828.219	3	1100.053	1
163		6	max	0	1	.136	3	.654	1	1.282e-2	1	NC	5	NC	3
164			min	-.279	4	-.166	2	.004	15	-1.49e-3	3	888.162	3	861.522	1
165		7	max	0	1	.1	3	.684	1	1.357e-2	1	NC	5	NC	3
166			min	-.279	4	-.144	2	.001	15	-1.782e-3	3	1113.57	3	736.097	1
167		8	max	0	1	.052	3	.705	1	1.432e-2	1	NC	4	NC	3
168			min	-.279	4	-.112	2	.001	15	-2.074e-3	3	1539.9	2	670.463	1
169		9	max	0	1	.007	3	.716	1	1.507e-2	1	NC	4	NC	3
170			min	-.279	4	-.082	2	.006	12	-2.365e-3	3	2193.976	2	633.454	2
171		10	max	0	1	-.002	15	.719	1	1.582e-2	1	NC	4	NC	3
172			min	-.279	4	-.068	2	.006	12	-2.657e-3	3	2734.39	2	617.959	2
173		11	max	0	3	.007	3	.716	1	1.507e-2	1	NC	4	NC	3
174			min	-.279	4	-.082	2	.006	12	-2.365e-3	3	2193.976	2	633.454	2
175		12	max	0	3	.052	3	.705	1	1.432e-2	1	NC	4	NC	3
176			min	-.279	4	-.112	2	.007	12	-2.074e-3	3	1539.9	2	670.463	1
177		13	max	0	3	.1	3	.684	1	1.357e-2	1	NC	5	NC	3
178			min	-.279	4	-.144	2	.008	12	-1.782e-3	3	1113.57	3	736.097	1
179		14	max	0	3	.136	3	.654	1	1.282e-2	1	NC	5	NC	3
180			min	-.279	4	-.166	2	.009	12	-1.49e-3	3	888.162	3	861.522	1
181		15	max	0	3	.149	3	.614	1	1.207e-2	1	NC	5	NC	3
182			min	-.279	4	-.172	2	.01	12	-1.199e-3	3	828.219	3	1100.053	1
183		16	max	0	3	.134	3	.57	1	1.132e-2	1	NC	5	NC	3
184			min	-.279	4	-.158	2	.011	12	-9.068e-4	3	898.869	3	1596.66	1
185		17	max	0	3	.092	3	.527	1	1.058e-2	1	NC	5	NC	3
186			min	-.279	4	-.123	2	.012	12	-6.151e-4	3	1181.202	3	2878.935	1
187		18	max	0	3	.03	3	.491	1	9.827e-3	1	NC	4	NC	2
188			min	-.279	4	-.072	2	.013	12	-3.234e-4	3	2220.256	3	8404.309	1
189		19	max	0	3	-.003	15	.472	1	9.079e-3	1	NC	1	NC	1
190			min	-.279	4	-.04	3	.015	12	-3.174e-5	3	NC	1	NC	1
191	M12	1	max	0	3	.013	5	.475	1	8.863e-3	1	NC	1	NC	1
192			min	-.367	4	-.227	1	-.025	5	-4.601e-4	5	NC	1	NC	1
193		2	max	0	3	.01	3	.491	1	9.293e-3	1	NC	4	NC	2
194			min	-.367	4	-.315	2	-.002	5	-3.449e-4	5	1551.996	2	7730.763	4
195		3	max	0	3	.05	3	.525	1	9.724e-3	1	NC	5	NC	3
196			min	-.367	4	-.403	2	.006	15	-2.298e-4	5	825.099	2	3098.034	1
197		4	max	0	3	.076	3	.568	1	1.015e-2	1	NC	5	NC	3
198			min	-.367	4	-.469	2	.008	15	-1.147e-4	5	612.878	2	1664.047	1
199		5	max	0	3	.087	3	.613	1	1.058e-2	1	NC	5	NC	3
200			min	-.367	4	-.505	2	.006	15	-1.26e-5	15	536.151	2	1126.021	1
201		6	max	0	3	.084	3	.654	1	1.102e-2	1	NC	5	NC	3
202			min	-.367	4	-.512	2	.003	15	2.581e-5	3	524.28	2	871.444	1
203		7	max	0	3	.069	3	.686	1	1.145e-2	1	NC	5	NC	3
204			min	-.367	4	-.493	2	0	15	5.977e-5	3	559.807	2	738.251	1
205		8	max	0	3	.047	3	.708	1	1.188e-2	1	NC	5	NC	3
206			min	-.367	4	-.458	2	.001	15	8.566e-5	12	639.762	2	668.248	1
207		9	max	0	3	.026	3	.72	1	1.231e-2	1	NC	5	NC	5
208			min	-.367	4	-.422	2	.005	12	1.077e-4	12	750.857	2	627.941	2
209		10	max	0	1	.016	3	.723	1	1.274e-2	1	NC	5	NC	5

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
210			min	-.367	4	-.404	2	.004	12	1.297e-4	12	819.818	2	611.597	2
211		11	max	0	1	.026	3	.72	1	1.231e-2	1	NC	5	NC	12
212			min	-.367	4	-.422	2	.005	12	1.077e-4	12	750.857	2	627.941	2
213		12	max	0	1	.047	3	.708	1	1.188e-2	1	NC	5	NC	3
214			min	-.367	4	-.458	2	.006	12	8.566e-5	12	639.762	2	668.248	1
215		13	max	0	1	.069	3	.686	1	1.145e-2	1	NC	5	NC	3
216			min	-.367	4	-.493	2	.008	12	5.977e-5	3	559.807	2	738.251	1
217		14	max	0	1	.084	3	.654	1	1.102e-2	1	NC	5	NC	3
218			min	-.367	4	-.512	2	.01	12	2.581e-5	3	524.28	2	871.444	1
219		15	max	0	1	.087	3	.613	1	1.058e-2	1	NC	5	NC	3
220			min	-.367	4	-.505	2	.012	12	-8.149e-6	3	536.151	2	1126.021	1
221		16	max	0	1	.076	3	.568	1	1.015e-2	1	NC	5	NC	3
222			min	-.367	4	-.469	2	.014	12	-4.211e-5	3	612.878	2	1664.047	1
223		17	max	0	1	.05	3	.525	1	9.724e-3	1	NC	5	NC	3
224			min	-.367	4	-.403	2	.015	12	-7.607e-5	3	825.099	2	3098.034	1
225		18	max	0	1	.01	3	.491	1	9.293e-3	1	NC	4	NC	2
226			min	-.367	4	-.315	2	.015	12	-1.1e-4	3	1551.996	2	9778.972	1
227		19	max	0	1	-.024	12	.475	1	8.863e-3	1	NC	1	NC	1
228			min	-.367	4	-.227	1	.015	12	-1.44e-4	3	NC	1	NC	1
229	M13	1	max	0	3	.094	3	.477	1	1.884e-2	2	NC	1	NC	1
230			min	-.579	4	-.952	2	-.025	5	-4.737e-3	3	NC	1	NC	1
231		2	max	0	3	.153	3	.506	1	2.047e-2	2	NC	5	NC	3
232			min	-.579	4	-1.123	2	-.005	5	-5.352e-3	3	912.828	2	5393.523	1
233		3	max	0	3	.207	3	.547	1	2.21e-2	2	NC	5	NC	3
234			min	-.579	4	-1.282	2	.004	15	-5.967e-3	3	472.041	2	2214.822	1
235		4	max	0	3	.249	3	.593	1	2.373e-2	2	NC	5	NC	3
236			min	-.579	4	-1.417	2	.008	15	-6.582e-3	3	335.306	2	1342.153	1
237		5	max	0	3	.276	3	.637	1	2.536e-2	2	NC	5	NC	3
238			min	-.579	4	-1.519	2	.009	15	-7.198e-3	3	275.2	2	975.733	1
239		6	max	0	3	.288	3	.674	1	2.699e-2	2	NC	15	NC	3
240			min	-.579	4	-1.584	2	.008	12	-7.813e-3	3	246.779	2	792.621	1
241		7	max	0	3	.286	3	.701	1	2.862e-2	2	NC	15	NC	3
242			min	-.579	4	-1.615	2	.006	12	-8.428e-3	3	235.263	2	695.372	1
243		8	max	0	3	.275	3	.719	1	3.025e-2	2	NC	15	NC	5
244			min	-.579	4	-1.619	2	.004	12	-9.043e-3	3	233.939	2	645.627	1
245		9	max	0	3	.262	3	.727	1	3.188e-2	2	NC	15	NC	5
246			min	-.579	4	-1.608	2	.002	3	-9.658e-3	3	237.909	2	616.606	2
247		10	max	0	1	.255	3	.729	1	3.351e-2	2	NC	15	NC	5
248			min	-.579	4	-1.599	2	.002	3	-1.027e-2	3	241.046	2	603.66	2
249		11	max	0	1	.262	3	.727	1	3.188e-2	2	NC	15	NC	12
250			min	-.579	4	-1.608	2	.002	3	-9.658e-3	3	237.909	2	616.606	2
251		12	max	0	1	.275	3	.719	1	3.025e-2	2	NC	15	NC	12
252			min	-.579	4	-1.619	2	.004	12	-9.043e-3	3	233.939	2	645.627	1
253		13	max	0	1	.286	3	.701	1	2.862e-2	2	NC	15	NC	3
254			min	-.579	4	-1.615	2	.006	12	-8.428e-3	3	235.263	2	695.372	1
255		14	max	0	1	.288	3	.674	1	2.699e-2	2	NC	15	NC	3
256			min	-.579	4	-1.584	2	.008	12	-7.813e-3	3	246.779	2	792.621	1
257		15	max	0	1	.276	3	.637	1	2.536e-2	2	NC	15	NC	3
258			min	-.579	4	-1.519	2	.01	12	-7.198e-3	3	275.2	2	975.733	1
259		16	max	0	1	.249	3	.593	1	2.373e-2	2	NC	15	NC	3
260			min	-.579	4	-1.417	2	.012	12	-6.582e-3	3	335.306	2	1342.153	1
261		17	max	0	1	.207	3	.547	1	2.21e-2	2	NC	5	NC	3
262			min	-.579	4	-1.282	2	.013	12	-5.967e-3	3	472.041	2	2214.822	1
263		18	max	0	1	.153	3	.506	1	2.047e-2	2	NC	5	NC	3
264			min	-.579	4	-1.123	2	.013	12	-5.352e-3	3	912.828	2	5393.523	1
265		19	max	0	1	.094	3	.477	1	1.884e-2	2	NC	1	NC	1
266			min	-.579	4	-.952	2	.014	12	-4.737e-3	3	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	5	1.225e-3	2	NC	1	NC	1
270			min	0	2	-.002	1	0	1	-2.054e-3	5	NC	1	NC	1
271		3	max	0	3	0	12	.003	5	2.451e-3	2	NC	3	NC	1
272			min	0	2	-.008	1	0	1	-4.109e-3	5	8658.254	1	NC	1
273		4	max	0	3	-.002	12	.008	5	3.676e-3	2	NC	3	NC	1
274			min	0	2	-.018	1	0	1	-6.163e-3	5	3838.003	1	9194.618	5
275		5	max	0	3	-.002	12	.013	5	4.076e-3	2	NC	3	NC	1
276			min	0	2	-.032	1	-.001	1	-7.056e-3	5	2145.575	1	5328.041	5
277		6	max	0	3	-.003	12	.02	5	3.712e-3	2	NC	3	NC	1
278			min	0	2	-.051	1	-.002	1	-6.875e-3	5	1370.284	1	3508.758	5
279		7	max	0	3	-.004	12	.028	5	3.348e-3	2	NC	3	NC	1
280			min	0	2	-.072	1	-.003	1	-6.694e-3	5	956.08	1	2505.876	5
281		8	max	0	3	-.005	12	.037	5	2.984e-3	2	NC	12	NC	1
282			min	0	2	-.098	1	-.003	1	-6.513e-3	5	708.952	1	1893.233	5
283		9	max	0	3	-.006	12	.046	5	2.621e-3	2	NC	12	NC	1
284			min	0	2	-.126	1	-.004	1	-6.332e-3	5	549.586	1	1490.857	5
285		10	max	0	3	-.007	12	.057	5	2.257e-3	2	9690.2	12	NC	1
286			min	-.001	2	-.157	1	-.005	1	-6.15e-3	5	440.7	1	1211.915	5
287		11	max	0	3	-.008	12	.069	5	1.893e-3	2	8423.091	12	NC	1
288			min	-.001	2	-.191	1	-.005	1	-5.969e-3	5	362.977	1	1010.441	5
289		12	max	.001	3	-.009	12	.081	5	1.529e-3	2	7422.786	12	NC	1
290			min	-.001	2	-.227	1	-.006	1	-5.788e-3	5	305.516	1	860.046	5
291		13	max	.001	3	-.01	12	.093	5	1.165e-3	2	6616.604	12	NC	1
292			min	-.001	2	-.265	1	-.006	1	-5.607e-3	5	261.81	1	744.748	5
293		14	max	.001	3	-.012	12	.106	4	8.016e-4	2	5955.715	12	NC	1
294			min	-.001	2	-.304	1	-.007	1	-5.426e-3	4	227.779	1	654.237	4
295		15	max	.001	3	-.013	12	.119	4	4.378e-4	2	5406.129	12	NC	1
296			min	-.002	2	-.345	1	-.007	1	-5.282e-3	4	200.757	1	581.701	4
297		16	max	.001	3	-.014	12	.133	4	4.427e-4	3	4943.599	12	NC	1
298			min	-.002	2	-.387	1	-.007	1	-5.138e-3	4	178.949	1	522.916	4
299		17	max	.001	3	-.015	12	.146	4	6.27e-4	3	4550.287	12	NC	1
300			min	-.002	2	-.43	1	-.006	1	-4.994e-3	4	161.099	1	474.657	4
301		18	max	.002	3	-.016	12	.159	4	8.113e-4	3	4212.838	12	NC	1
302			min	-.002	2	-.474	1	-.007	3	-4.85e-3	4	146.315	1	434.608	4
303		19	max	.002	3	-.018	12	.173	4	9.955e-4	3	3921.067	12	NC	1
304			min	-.002	2	-.517	1	-.01	3	-4.706e-3	4	133.943	1	401.071	4
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	4	0	1	NC	1	NC	1
308			min	0	2	-.002	1	0	1	-2.127e-3	4	NC	1	NC	1
309		3	max	0	3	0	15	.004	4	0	1	NC	3	NC	1
310			min	0	2	-.011	1	0	1	-4.254e-3	4	6514.099	1	NC	1
311		4	max	0	3	0	15	.008	4	0	1	NC	3	NC	1
312			min	-.001	2	-.025	1	0	1	-6.381e-3	4	2800.496	1	8884.536	4
313		5	max	.001	3	-.001	15	.013	4	0	1	NC	3	NC	1
314			min	-.001	2	-.045	1	0	1	-7.302e-3	4	1525.756	1	5149.736	4
315		6	max	.001	3	-.002	15	.02	4	0	1	NC	3	NC	1
316			min	-.002	2	-.073	1	0	1	-7.108e-3	4	955.447	1	3392.032	4
317		7	max	.002	3	-.003	15	.029	4	0	1	NC	3	NC	1
318			min	-.002	2	-.105	1	0	1	-6.913e-3	4	657.785	1	2423.183	4
319		8	max	.002	3	-.004	15	.038	4	0	1	NC	3	NC	1
320			min	-.002	2	-.143	1	0	1	-6.719e-3	4	483.102	1	1831.431	4
321		9	max	.002	3	-.005	15	.048	4	0	1	NC	3	NC	1
322			min	-.002	2	-.186	1	0	1	-6.525e-3	4	371.825	1	1442.849	4
323		10	max	.002	3	-.007	15	.059	4	0	1	NC	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
324			min	-.003	2	-.234	1	0	1	-6.331e-3	4	296.506	1	1173.524	4
325		11	max	.003	3	-.008	15	.071	4	0	1	NC	3	NC	1
326			min	-.003	2	-.285	1	0	1	-6.137e-3	4	243.142	1	979.039	4
327		12	max	.003	3	-.009	12	.083	4	0	1	NC	3	NC	1
328			min	-.003	2	-.34	1	0	1	-5.943e-3	4	203.926	1	833.898	4
329		13	max	.003	3	-.009	12	.096	4	0	1	NC	3	NC	1
330			min	-.003	2	-.398	1	0	1	-5.749e-3	4	174.245	1	722.662	4
331		14	max	.003	3	-.009	12	.109	4	0	1	NC	3	NC	1
332			min	-.004	2	-.458	1	0	1	-5.554e-3	4	151.231	1	635.532	4
333		15	max	.004	3	-.009	12	.122	4	0	1	NC	3	NC	1
334			min	-.004	2	-.521	1	0	1	-5.36e-3	4	133.02	1	566.036	4
335		16	max	.004	3	-.009	12	.136	4	0	1	NC	3	NC	1
336			min	-.004	2	-.586	1	0	1	-5.166e-3	4	118.368	1	509.772	4
337		17	max	.004	3	-.01	12	.149	4	0	1	NC	3	NC	1
338			min	-.004	2	-.651	1	0	1	-4.972e-3	4	106.408	1	463.645	4
339		18	max	.004	3	-.01	12	.163	4	0	1	NC	3	NC	1
340			min	-.005	2	-.718	1	0	1	-4.778e-3	4	96.525	1	425.433	4
341		19	max	.005	3	-.01	12	.176	4	0	1	NC	3	NC	1
342			min	-.005	2	-.785	1	0	1	-4.584e-3	4	88.272	1	393.51	4
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	5	0	4	4.827e-4	3	NC	1	NC	1
346			min	0	2	-.002	1	0	3	-2.249e-3	4	NC	1	NC	1
347		3	max	0	3	0	5	.004	4	9.654e-4	3	NC	3	NC	1
348			min	0	2	-.008	1	0	3	-4.498e-3	4	8658.254	1	NC	1
349		4	max	0	3	.001	5	.008	4	1.448e-3	3	NC	3	NC	1
350			min	0	2	-.018	1	0	3	-6.747e-3	4	3838.003	1	8892.03	4
351		5	max	0	3	.002	5	.013	4	1.584e-3	3	NC	3	NC	1
352			min	0	2	-.032	1	-.001	3	-7.701e-3	4	2145.575	1	5157.49	4
353		6	max	0	3	.003	5	.02	4	1.4e-3	3	NC	3	NC	1
354			min	0	2	-.051	1	-.002	3	-7.457e-3	4	1370.284	1	3398.698	4
355		7	max	0	3	.004	5	.029	4	1.216e-3	3	NC	3	NC	1
356			min	0	2	-.072	1	-.002	3	-7.214e-3	4	956.08	1	2428.725	4
357		8	max	0	3	.006	5	.038	4	1.031e-3	3	NC	5	NC	1
358			min	0	2	-.098	1	-.003	3	-6.97e-3	4	708.952	1	1836.079	4
359		9	max	0	3	.007	5	.048	4	8.472e-4	3	NC	7	NC	1
360			min	0	2	-.126	1	-.003	3	-6.727e-3	4	549.586	1	1446.814	4
361		10	max	0	3	.009	5	.059	4	6.629e-4	3	NC	13	NC	1
362			min	-.001	2	-.157	1	-.003	3	-6.483e-3	4	440.7	1	1176.968	4
363		11	max	0	3	.011	5	.071	4	4.786e-4	3	9874.075	13	NC	1
364			min	-.001	2	-.191	1	-.003	3	-6.24e-3	4	362.977	1	982.082	4
365		12	max	.001	3	.013	5	.083	4	2.944e-4	3	8243.562	13	NC	1
366			min	-.001	2	-.227	1	-.003	3	-5.996e-3	4	305.516	1	836.626	4
367		13	max	.001	3	.015	5	.096	4	1.101e-4	3	7017.467	13	NC	1
368			min	-.001	2	-.265	1	-.002	3	-5.752e-3	4	261.81	1	725.143	4
369		14	max	.001	3	.017	5	.109	4	-4.67e-5	12	6071.869	13	NC	1
370			min	-.001	2	-.304	1	-.001	3	-5.509e-3	4	227.779	1	637.815	4
371		15	max	.001	3	.019	5	.122	4	1.912e-5	9	5406.129	12	NC	1
372			min	-.002	2	-.345	1	0	3	-5.265e-3	4	200.757	1	568.161	4
373		16	max	.001	3	.021	5	.135	4	1.352e-4	9	4943.599	12	NC	1
374			min	-.002	2	-.387	1	.001	12	-5.038e-3	5	178.949	1	511.77	4
375		17	max	.001	3	.023	5	.149	4	4.525e-4	1	4550.287	12	NC	1
376			min	-.002	2	-.43	1	.002	10	-4.834e-3	5	161.099	1	465.541	4
377		18	max	.002	3	.025	5	.162	4	7.767e-4	1	4212.838	12	NC	1
378			min	-.002	2	-.474	1	.001	10	-4.631e-3	5	146.315	1	427.248	4
379		19	max	.002	3	.028	5	.175	4	1.101e-3	1	3921.067	12	NC	1
380			min	-.002	2	-.517	1	0	10	-4.428e-3	5	133.943	1	395.261	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
381	M3	1	max	.023	1	0	12	.01	5	1.069e-3	2	NC	1	NC	1
382			min	.002	12	-.007	1	-.001	1	-6.3e-4	5	NC	1	NC	1
383		2	max	.023	1	-.002	12	.041	5	1.543e-3	2	NC	1	NC	3
384			min	.002	12	-.048	1	-.019	2	-7.122e-4	5	NC	1	4196.69	2
385		3	max	.022	1	-.003	12	.072	5	2.018e-3	2	NC	1	NC	4
386			min	.002	12	-.088	1	-.036	2	-7.944e-4	5	NC	1	2124.914	2
387		4	max	.021	1	-.005	12	.104	5	2.492e-3	2	NC	1	NC	13
388			min	.003	15	-.129	1	-.052	2	-9.529e-4	3	NC	1	1443.348	2
389		5	max	.02	1	-.006	12	.134	5	2.966e-3	2	NC	1	7711.876	13
390			min	.003	15	-.169	1	-.067	2	-1.153e-3	3	NC	1	1110.096	2
391		6	max	.02	1	-.007	12	.165	5	3.441e-3	2	NC	1	6297.711	13
392			min	.003	15	-.21	1	-.081	2	-1.354e-3	3	9670.313	4	917.064	2
393		7	max	.019	1	-.009	12	.195	5	3.915e-3	2	NC	1	5411.875	13
394			min	.003	15	-.25	1	-.093	2	-1.554e-3	3	8575.823	4	795.206	2
395		8	max	.018	1	-.01	12	.225	5	4.39e-3	2	NC	1	4835.1	13
396			min	.003	15	-.289	1	-.103	2	-1.755e-3	3	7918.965	4	715.317	2
397		9	max	.018	1	-.011	12	.253	5	4.864e-3	2	NC	3	4461.528	13
398			min	.003	15	-.329	1	-.111	2	-1.956e-3	3	7565.404	4	663.291	2
399		10	max	.017	1	-.011	12	.281	5	5.339e-3	2	NC	3	4237.251	13
400			min	.002	15	-.368	1	-.116	2	-2.156e-3	3	7453.555	4	631.969	2
401		11	max	.016	1	-.012	12	.309	5	5.813e-3	2	NC	3	4136.864	13
402			min	.002	15	-.408	1	-.118	2	-2.357e-3	3	7565.404	4	604.999	14
403		12	max	.016	1	-.013	12	.335	5	6.288e-3	2	NC	1	4154.848	13
404			min	.002	15	-.446	1	-.117	2	-2.557e-3	3	7918.965	4	545.789	14
405		13	max	.015	1	-.013	12	.36	5	6.762e-3	2	NC	1	4305.274	13
406			min	.002	15	-.485	1	-.112	2	-2.758e-3	3	8575.823	4	496.223	14
407		14	max	.014	1	-.014	12	.384	5	7.237e-3	2	NC	1	4630.55	13
408			min	.002	15	-.524	1	-.103	2	-2.958e-3	3	9670.313	4	454.065	14
409		15	max	.013	1	-.014	12	.406	5	7.711e-3	2	NC	1	5229.115	13
410			min	.002	15	-.562	1	-.089	2	-3.159e-3	3	NC	1	417.716	14
411		16	max	.013	1	-.014	12	.428	5	8.186e-3	2	NC	1	6342.671	13
412			min	.002	15	-.6	1	-.072	2	-3.359e-3	3	NC	1	386.009	14
413		17	max	.012	1	-.014	12	.448	5	8.66e-3	2	NC	1	8708.622	13
414			min	.002	15	-.638	1	-.049	2	-3.56e-3	3	NC	1	358.069	14
415		18	max	.011	1	-.014	12	.468	4	9.135e-3	2	NC	1	NC	4
416			min	.002	15	-.676	1	-.021	2	-3.76e-3	3	NC	1	333.228	14
417		19	max	.011	1	-.014	12	.489	4	9.609e-3	2	NC	1	NC	1
418			min	.002	10	-.714	1	-.002	3	-3.961e-3	3	NC	1	310.969	14
419	M6	1	max	.032	1	0	15	.01	4	0	1	NC	1	NC	1
420			min	0	15	-.01	1	0	1	-6.543e-4	5	NC	1	NC	1
421		2	max	.03	1	0	3	.043	4	0	1	NC	1	NC	1
422			min	0	15	-.073	1	0	1	-7.695e-4	4	NC	1	NC	1
423		3	max	.029	1	0	3	.075	4	0	1	NC	1	NC	1
424			min	0	15	-.135	1	0	1	-8.851e-4	4	NC	1	6834.71	4
425		4	max	.027	1	0	3	.107	4	0	1	NC	1	NC	1
426			min	0	15	-.197	1	0	1	-1.001e-3	4	NC	1	4589.059	4
427		5	max	.025	1	.002	3	.139	4	0	1	NC	1	NC	1
428			min	0	15	-.259	1	0	1	-1.116e-3	4	NC	1	3496.688	4
429		6	max	.024	1	.002	3	.17	4	0	1	NC	1	NC	1
430			min	0	15	-.321	1	0	1	-1.232e-3	4	9670.313	4	2867.289	4
431		7	max	.022	1	.003	3	.201	4	0	1	NC	1	NC	1
432			min	0	15	-.383	1	0	1	-1.347e-3	4	8575.823	4	2471.991	4
433		8	max	.02	1	.005	3	.232	4	0	1	NC	1	NC	1
434			min	0	15	-.444	1	0	1	-1.463e-3	4	7918.965	4	2214.062	4
435		9	max	.018	1	.006	3	.261	4	0	1	NC	3	NC	1
436			min	0	15	-.506	1	0	1	-1.579e-3	4	7565.404	4	2046.785	4
437		10	max	.017	1	.007	3	.29	4	0	1	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
438			min	0	15	-.567	1	0	1	-1.694e-3	4	7453.555	4	1946.398	4
439		11	max	.017	3	.009	3	.317	4	0	1	NC	5	NC	1
440			min	0	15	-.628	1	0	1	-1.81e-3	4	7565.404	4	1901.782	4
441		12	max	.018	3	.011	3	.344	4	0	1	NC	1	NC	1
442			min	0	15	-.688	1	0	1	-1.925e-3	4	6721.428	3	1910.703	4
443		13	max	.019	3	.013	3	.369	4	0	1	NC	1	NC	1
444			min	0	10	-.749	1	0	1	-2.041e-3	4	5725.251	3	1979.763	4
445		14	max	.02	3	.015	3	.393	4	0	1	NC	1	NC	1
446			min	-.001	10	-.809	1	0	1	-2.156e-3	4	4935.541	3	2128.436	4
447		15	max	.021	3	.017	3	.415	4	0	1	NC	1	NC	1
448			min	-.002	10	-.869	1	0	1	-2.272e-3	4	4302.579	3	2401.74	4
449		16	max	.023	3	.02	3	.436	4	0	1	NC	1	NC	1
450			min	-.003	10	-.928	1	0	1	-2.388e-3	4	3790.365	3	2910.08	4
451		17	max	.024	3	.022	3	.456	4	0	1	NC	1	NC	1
452			min	-.005	2	-.988	1	0	1	-2.503e-3	4	3372.445	3	3990.169	4
453		18	max	.025	3	.025	3	.474	4	0	1	NC	1	NC	1
454			min	-.007	2	-1.048	1	0	1	-2.619e-3	4	3029.13	3	7333.273	4
455		19	max	.026	3	.027	3	.49	4	0	1	NC	1	NC	1
456			min	-.01	2	-1.107	1	0	1	-2.734e-3	4	2745.612	3	NC	1
457	M9	1	max	.023	1	0	5	.01	4	3.513e-4	3	NC	1	NC	1
458			min	-.002	5	-.007	1	-.001	3	-1.069e-3	2	NC	1	NC	1
459		2	max	.023	1	.002	5	.044	4	5.518e-4	3	NC	1	NC	3
460			min	-.002	5	-.048	1	-.008	3	-1.543e-3	2	NC	1	4196.69	2
461		3	max	.022	1	.003	5	.078	4	7.523e-4	3	NC	1	9699.104	15
462			min	-.002	5	-.088	1	-.015	3	-2.018e-3	2	NC	1	2124.914	2
463		4	max	.021	1	.004	5	.112	4	9.529e-4	3	NC	1	6512.491	15
464			min	-.002	5	-.129	1	-.021	3	-2.492e-3	2	NC	1	1443.348	2
465		5	max	.02	1	.006	5	.145	4	1.153e-3	3	NC	1	4962.142	15
466			min	-.002	5	-.169	1	-.028	3	-2.966e-3	2	NC	1	1110.096	2
467		6	max	.02	1	.007	5	.178	4	1.354e-3	3	NC	1	4068.672	15
468			min	-.002	5	-.21	1	-.033	3	-3.441e-3	2	9670.313	6	917.064	2
469		7	max	.019	1	.009	5	.21	4	1.554e-3	3	NC	1	3507.358	15
470			min	-.002	5	-.25	1	-.038	3	-3.915e-3	2	8575.823	6	795.206	2
471		8	max	.018	1	.011	5	.242	4	1.755e-3	3	NC	1	3140.941	15
472			min	-.002	5	-.289	1	-.042	3	-4.39e-3	2	7623.406	5	715.317	2
473		9	max	.018	1	.012	5	.272	4	1.956e-3	3	NC	3	2903.125	15
474			min	-.002	5	-.329	1	-.045	3	-4.864e-3	2	6479.697	5	663.291	2
475		10	max	.017	1	.014	5	.3	4	2.156e-3	3	NC	3	2760.174	15
476			min	-.002	5	-.368	1	-.047	3	-5.339e-3	2	5589.523	5	631.969	2
477		11	max	.016	1	.016	5	.328	4	2.357e-3	3	NC	3	2696.287	15
478			min	-.002	5	-.408	1	-.048	3	-5.813e-3	2	4879.794	5	618.045	2
479		12	max	.016	1	.018	5	.354	4	2.557e-3	3	NC	1	2708.25	15
480			min	-.002	5	-.446	1	-.048	3	-6.288e-3	2	4303.446	5	620.946	2
481		13	max	.015	1	.021	5	.378	4	2.758e-3	3	NC	1	2805.366	15
482			min	-.002	5	-.485	1	-.046	3	-6.762e-3	2	3828.655	5	642.864	2
483		14	max	.014	1	.023	5	.401	4	2.958e-3	3	NC	1	3015.15	15
484			min	-.002	5	-.524	1	-.042	3	-7.237e-3	2	3433.044	5	690.062	2
485		15	max	.013	1	.025	5	.422	4	3.159e-3	3	NC	1	3401.247	15
486			min	-.002	5	-.562	1	-.037	3	-7.711e-3	2	3100.371	5	776.926	2
487		16	max	.013	1	.028	5	.44	4	3.359e-3	3	NC	1	4119.769	15
488			min	-.002	5	-.6	1	-.031	3	-8.186e-3	2	2818.538	5	938.669	2
489		17	max	.012	1	.03	5	.457	4	3.56e-3	3	NC	1	5646.863	15
490			min	-.002	5	-.638	1	-.022	3	-8.66e-3	2	2578.344	5	1282.629	2
491		18	max	.011	1	.033	5	.471	4	3.76e-3	3	NC	1	NC	15
492			min	-.002	5	-.676	1	-.011	3	-9.135e-3	2	2372.672	5	2347.885	2
493		19	max	.011	1	.036	5	.483	4	3.961e-3	3	NC	1	NC	1
494			min	-.002	5	-.714	1	-.015	1	-9.609e-3	2	2195.938	5	NC	1