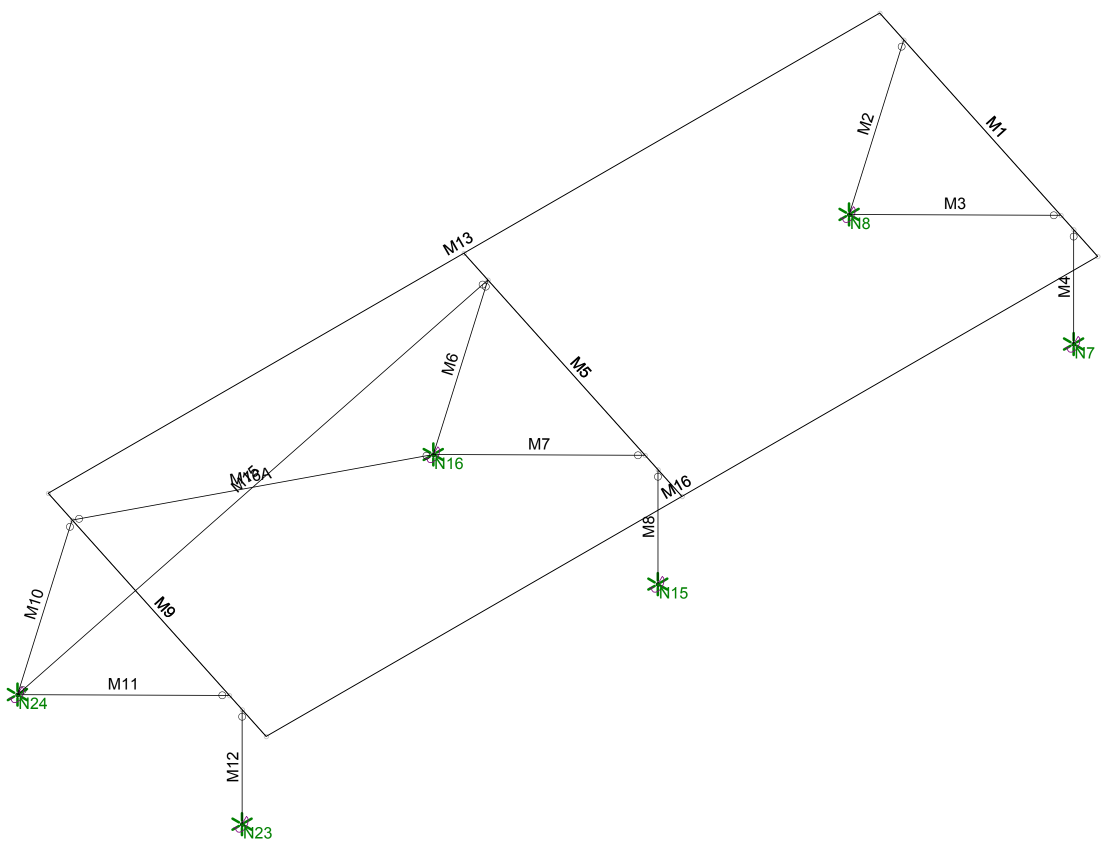


Schletter, Inc.		25° Tilt w/ Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

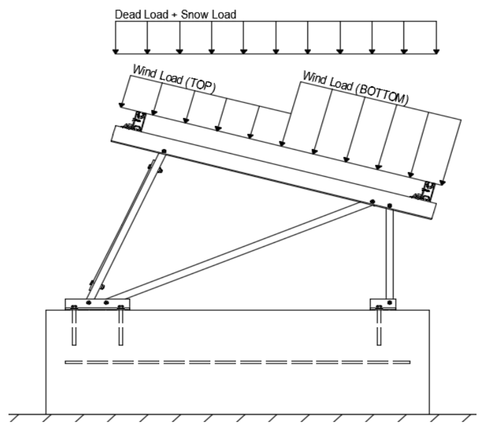
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 1
Module Tilt = 25°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 18.56 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.82
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 150 mph
Height ≤ 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 35.33 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.1	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.7	
$Cf-_{TOP}$	=	-2.2	*(Suction)*
$Cf-_{BOTTOM}$	=	-1	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

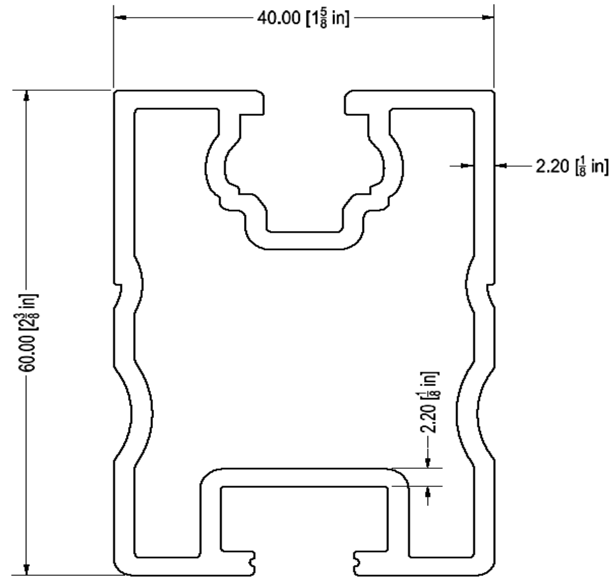
Purlins	Location	**Diagonal Struts**	Location	**Front Reactions**	Location
M13	Top	M3	Outer	N7	Outer
M16	Bottom	M7	Inner	N15	Inner
		M11	Outer	N23	Outer
Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer
Front Struts	Location	**Bracing**			
M4	Outer	M15			
M8	Inner	M16A			
M12	Outer				

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

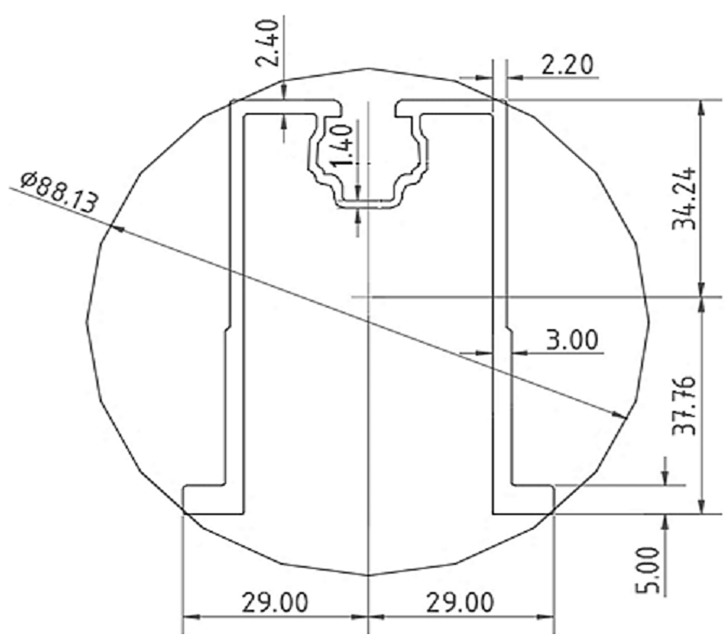
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	51	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.63	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	0.420	k-ft
M_z =	0.035	k-ft
$M_{y\ allowable}$ =	1.261	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	37%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

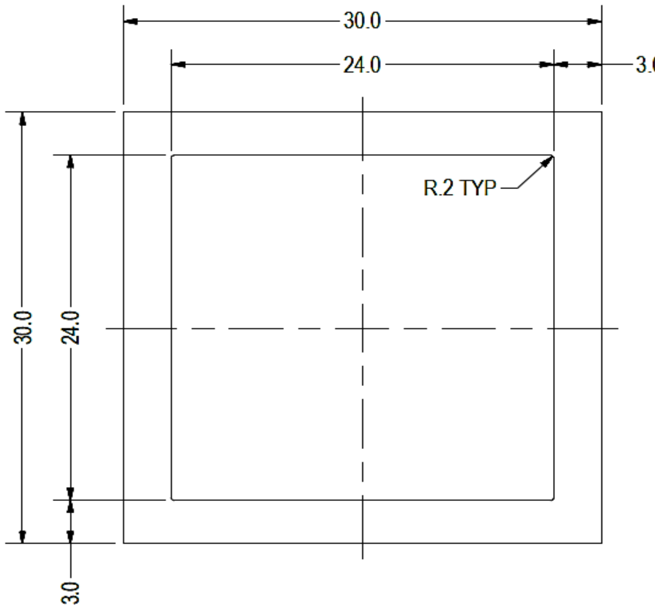
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.77	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	-0.477	k-ft
M_z =	-0.019	k-ft
P_n =	0.166	k
$M_{y\ allowable}$ =	1.461	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	38%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

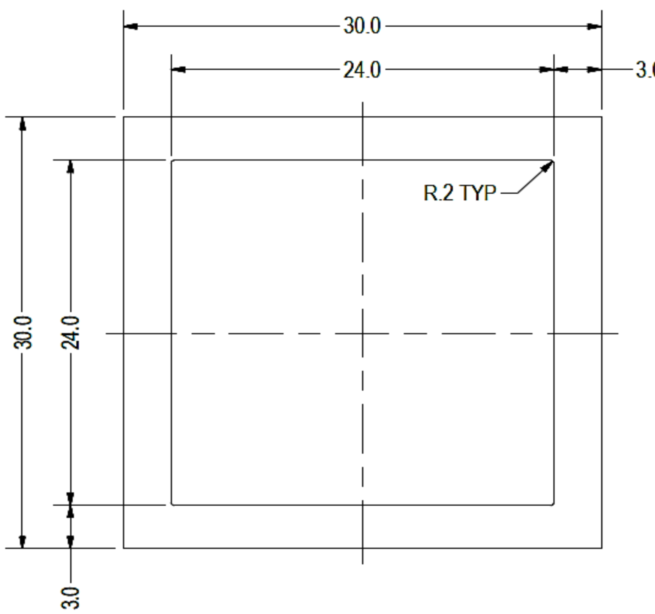
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.028	k-ft
P_n =	0.155	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	8%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

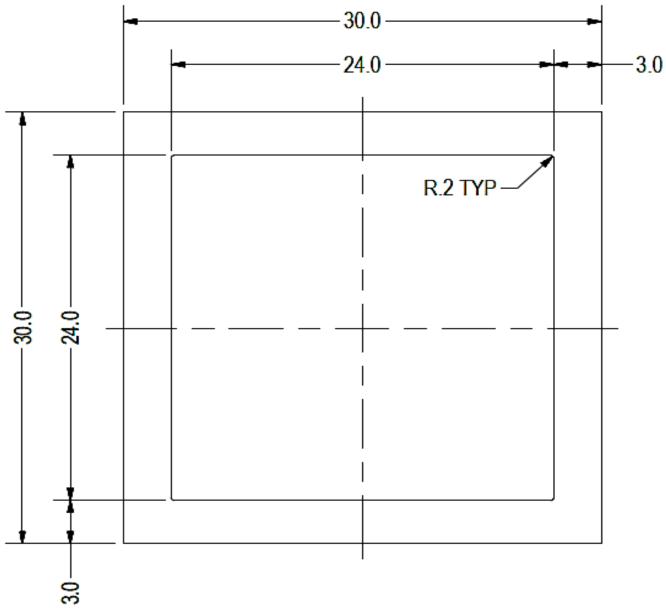
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.468	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	12%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

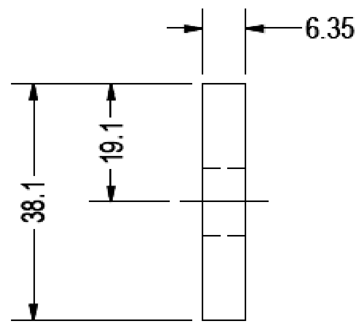
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	36.18	in
$\Phi F_{ty\ AXIAL}$ =	11.59	ksi
$\Phi F_{ty\ BENDING}$ =	30.23	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.712	k
$M_{y\ allowable}$ =	0.410	k-ft
$M_{z\ allowable}$ =	0.410	k-ft
$P_{n\ allowable}$ =	5.820	k
Utilization =	12%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.003	k-ft
P_n =	0.173	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	8%	



A cross brace kit is required every 24 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

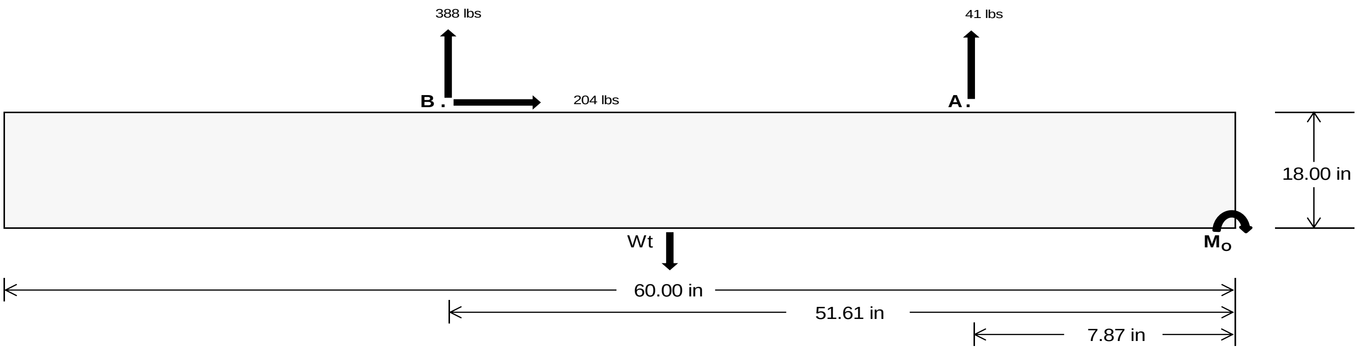
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	183.62	1686.23	k
Compressive Load =	1144.30	1124.58	k
Lateral Load =	22.97	885.47	k
Moment (Weak Axis) =	0.04	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

Footing Reinforcement

Use fiber reinforcing with (1) #5 rebar.

Overturning Check

M_O =	24044.7 in-lbs
Resisting Force Required =	801.49 lbs
S.F. =	1.67
Weight Required =	1335.81 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.

Sliding

Force =	204.28 lbs
Friction =	0.4
Weight Required =	510.69 lbs
Resisting Weight =	1903.13 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion

Sliding Force =	204.28 lbs
Cohesion =	130 psf
Area =	8.75 ft^2
Resisting =	951.56 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	21 in	22 in	23 in	24 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.75 ft) =	1903 lbs	1994 lbs	2084 lbs	2175 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in
F_A	375 lbs	375 lbs	375 lbs	375 lbs	429 lbs	429 lbs	429 lbs	429 lbs	572 lbs	572 lbs	572 lbs	572 lbs	-82 lbs	-82 lbs	-82 lbs	-82 lbs
F_B	263 lbs	263 lbs	263 lbs	263 lbs	466 lbs	466 lbs	466 lbs	466 lbs	524 lbs	524 lbs	524 lbs	524 lbs	-777 lbs	-777 lbs	-777 lbs	-777 lbs
F_V	31 lbs	31 lbs	31 lbs	31 lbs	364 lbs	364 lbs	364 lbs	364 lbs	294 lbs	294 lbs	294 lbs	294 lbs	-409 lbs	-409 lbs	-409 lbs	-409 lbs
P_{total}	2541 lbs	2631 lbs	2722 lbs	2813 lbs	2799 lbs	2890 lbs	2980 lbs	3071 lbs	2999 lbs	3090 lbs	3181 lbs	3271 lbs	283 lbs	337 lbs	392 lbs	446 lbs
M	265 lbs-ft	265 lbs-ft	265 lbs-ft	265 lbs-ft	497 lbs-ft	497 lbs-ft	497 lbs-ft	497 lbs-ft	551 lbs-ft	551 lbs-ft	551 lbs-ft	551 lbs-ft	634 lbs-ft	634 lbs-ft	634 lbs-ft	634 lbs-ft
e	0.10 ft	0.10 ft	0.10 ft	0.09 ft	0.18 ft	0.17 ft	0.17 ft	0.16 ft	0.18 ft	0.18 ft	0.17 ft	0.17 ft	2.24 ft	1.88 ft	1.62 ft	1.42 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	254.0 psf	252.4 psf	250.9 psf	249.5 psf	251.7 psf	250.2 psf	248.7 psf	247.4 psf	267.2 psf	264.9 psf	262.9 psf	261.0 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	326.7 psf	321.7 psf	317.2 psf	313.0 psf	388.0 psf	380.3 psf	373.2 psf	366.7 psf	418.4 psf	409.2 psf	400.9 psf	393.3 psf	418.4 psf	198.1 psf	154.8 psf	138.0 psf

Maximum Bearing Pressure =	418 psf
Allowable Bearing Pressure =	1500 psf

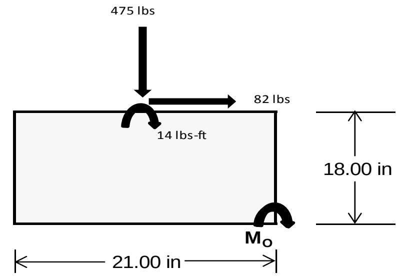
Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 279.0 ft-lbs
Resisting Force Required = 318.88 lbs
S.F. = 1.67
Weight Required = 531.47 lbs
Minimum Width = 21 in in
Weight Provided = 1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	21 in			21 in			21 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	114 lbs	69 lbs	56 lbs	228 lbs	475 lbs	184 lbs	76 lbs	-26 lbs	20 lbs
F_V	13 lbs	109 lbs	13 lbs	9 lbs	82 lbs	10 lbs	13 lbs	109 lbs	13 lbs
P_{total}	2470 lbs	2425 lbs	2412 lbs	2471 lbs	2718 lbs	2427 lbs	765 lbs	663 lbs	709 lbs
M	37 lbs-ft	182 lbs-ft	38 lbs-ft	26 lbs-ft	137 lbs-ft	29 lbs-ft	37 lbs-ft	182 lbs-ft	38 lbs-ft
e	0.01 ft	0.08 ft	0.02 ft	0.01 ft	0.05 ft	0.01 ft	0.05 ft	0.28 ft	0.05 ft
L/6	0.29 ft	1.60 ft	1.72 ft	1.73 ft	1.65 ft	1.73 ft	1.65 ft	1.20 ft	1.64 ft
f_{min}	268.0 sqft	205.6 sqft	260.9 sqft	272.2 sqft	257.0 sqft	265.9 sqft	73.0 sqft	4.3 sqft	66.3 sqft
f_{max}	296.7 psf	348.6 psf	290.5 psf	292.6 psf	364.3 psf	288.7 psf	101.9 psf	147.2 psf	95.8 psf

Maximum Bearing Pressure = 364 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 21in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

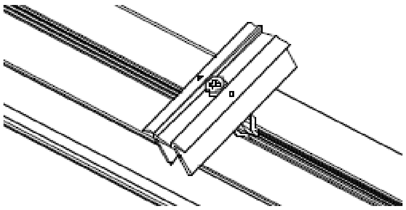
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

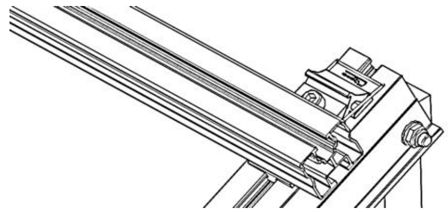
<u>Fastening of Modules to Purlins</u>

Maximum Uplifting Force =	0.732	k
Allowable Uplift =	1.214	k
Utilization =	60%	



<u>Fastening of Purlins to Girders</u>

Maximum Uplifting Force =	1.109	k
Allowable Uplift =	1.116	k
Utilization =	99%	



6.2 Bolted Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

<u>Front Strut</u>

Maximum Axial Load =	0.880	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	15%	

<u>Rear Strut</u>

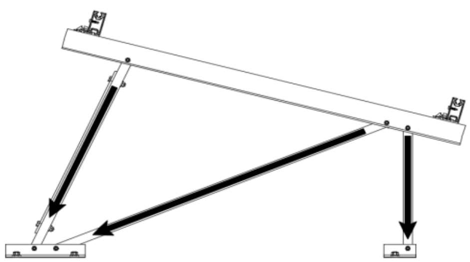
Maximum Axial Load =	1.135	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	20%	

<u>Diagonal Strut</u>

Maximum Axial Load =	0.468	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	8%	

<u>Bracing</u>

Maximum Axial Load =	0.173	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	2%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

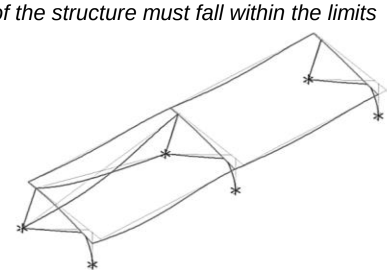
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	30.83 in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$ 0.617 in
Max Drift, Δ_{MAX} =	0.058 in

<u>*0.058 ≤ 0.617, OK.*</u>

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus**

Strong Axis:

3.4.14

L_b = 51.00 in

J = 0.255

132.801

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 51.00 in

J = 0.255

137.906

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 30

Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 29.6 ksi

Ix = 250988 mm^4

0.603 in^4

y = 30 mm

Sx = 0.511 in^3

$M_{max}St$ = 1.261 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 20

Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi

Iy = 120291 mm^4

0.289 in^4

x = 20 mm

Sy = 0.367 in^3

$M_{max}Wk$ = 0.871 k-ft

<u>Compression</u>

3.4.9

b/t = 7.4

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 23.9

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.47 ksi

A = 578.06 mm^2

0.90 in^2

P_{max} = 25.51 kips

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.33

21.3453

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.8 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.33

24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.8 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7

F_{UT}= (φbk2*√(BpE))/(5.1b/t)

F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

F_{ST}= φb[Bp-1.6Dp*b/t]

F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.461 k-ft

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.8

$b/t =$ 24.46
$S1 =$ 3.83
$S2 =$ 10.30
$\varphi F_L = (\varphi ck2^*\sqrt{(BpE)})/(5.1b/t)$
$\varphi F_L =$ 10.4 ksi

3.4.9

$b/t =$ 4.29
$S1 =$ 12.21 (See 3.4.16 above for formula)
$S2 =$ 32.70 (See 3.4.16 above for formula)
$\varphi F_L = \varphi yFcy$
$\varphi F_L =$ 33.3 ksi

$b/t =$ 24.46
$S1 =$ 12.21
$S2 =$ 32.70
$\varphi F_L = \varphi c[Bp-1.6Dp^*b/t]$
$\varphi F_L =$ 28.2 ksi

3.4.9.1

$b/t =$ 24.46
$t =$ 2.6
$ds =$ 6.05
$rs =$ 3.49
$S =$ 21.70
$\rho st =$ 0.22
$F_{UT} =$ 10.43
$F_{ST} =$ 28.24
$\varphi F_L = Fut + (Fst - Fut)\rho st < Fst$
$\varphi F_L =$ 14.3 ksi

3.4.10

$Rb/t =$ 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

$S1 =$ 6.87
$S2 =$ 131.3
$\varphi F_L = \varphi yFcy$
$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 14.29 ksi
$A =$ 576.21 mm^2
0.89 in^2
$P_{max} =$ 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 31.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.2 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.423 k-ft

Compression

3.4.7

λ = 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83792

φF_L = φcc(Bc-Dc*λ)

φF_L = 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L = φyFcy

φF_L = 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 24.52 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

$L_b =$ 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

$\varphi F_L = \varphi b[Bc-1.6Dc^*\sqrt{((LbSc)/(Cb^*\sqrt{(IyJ)/2}))}]$

$\varphi F_L =$ 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

$\varphi F_L = 1.17\varphi yFcy$

$\varphi F_L =$ 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

$C_0 =$ 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L St =$ 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

$M_{max}St =$ 0.404 k-ft

Weak Axis:

3.4.14

$L_b =$ 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

$\varphi F_L = \varphi b[Bc-1.6Dc^*\sqrt{((LbSc)/(Cb^*\sqrt{(IyJ)/2}))}]$

$\varphi F_L =$ 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

$C_0 =$ 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L Wk =$ 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

$M_{max}Wk =$ 0.450 k-ft

Compression

3.4.7

λ = 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.85841

φF_L = (φccFcy)/(λ²)

φF_L = 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L = φyFcy

φF_L = 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 7.60 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 36.18 in

J = 0.16

94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.410 k-ft

Weak Axis:

3.4.14

L_b = 36.18 in

J = 0.16

94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.5514

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.7972

φF_L= $(\varphi ccFcy)/(\lambda^2)$

φF_L= 11.5927 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= $\varphi yFcy$

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= $\varphi yFcy$

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= $\varphi yFcy$

φF_L= 33.25 ksi

φF_L= 11.59 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 5.82 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-51.748	-51.748	0	0
2	M16	Y	-51.748	-51.748	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-108.369	-108.369	0	0
2	M16	y	-167.479	-167.479	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	216.738	216.738	0	0
2	M16	y	98.517	98.517	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	187.411	2	271.142	2	.002	10	0	10	0	1	0	1
2		min	-225.361	3	-406.535	3	-2.253	4	0	3	0	1	0	1
3	N7	max	0	4	309.778	1	0	10	0	10	0	1	0	1
4		min	-.128	2	-32.422	3	-17.299	4	-.027	4	0	1	0	1
5	N15	max	0	15	880.228	1	.167	9	0	9	0	1	0	1
6		min	-1.295	2	-141.243	3	-17.668	5	-.028	4	0	1	0	1
7	N16	max	617.646	2	865.059	2	0	2	0	9	0	1	0	1
8		min	-681.127	3	-1297.098	3	-144.52	4	0	3	0	1	0	1
9	N23	max	0	15	309.893	1	.867	1	.001	1	0	1	0	1
10		min	-.128	2	-31.894	3	-16.428	5	-.026	5	0	1	0	1
11	N24	max	187.411	2	273.618	2	74.388	3	0	4	0	1	0	1
12		min	-225.789	3	-405.506	3	-3.253	5	0	3	0	1	0	1
13	Totals:	max	990.916	2	2796.644	2	0	10						
14		min	-1132.476	3	-2314.699	3	-200.862	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	225.137	1	.641	6	1.022	4	0	10	0	10	0	1
2			min	-366.377	3	.149	15	-.087	3	0	4	0	4	0	1
3		2	max	225.254	1	.595	6	.917	4	0	10	0	5	0	15
4			min	-366.29	3	.139	15	-.087	3	0	4	0	3	0	6
5		3	max	225.37	1	.55	6	.811	4	0	10	0	4	0	15
6			min	-366.203	3	.128	15	-.087	3	0	4	0	3	0	6
7		4	max	225.487	1	.504	6	.706	4	0	10	0	4	0	15
8			min	-366.115	3	.117	15	-.087	3	0	4	0	3	0	6
9		5	max	225.603	1	.458	6	.6	4	0	10	0	4	0	15
10			min	-366.028	3	.106	15	-.087	3	0	4	0	3	0	6
11		6	max	225.719	1	.413	6	.495	4	0	10	0	4	0	15
12			min	-365.941	3	.096	15	-.087	3	0	4	0	3	0	6
13		7	max	225.836	1	.367	6	.389	4	0	10	0	4	0	15
14			min	-365.854	3	.085	15	-.087	3	0	4	0	3	0	6
15		8	max	225.952	1	.321	6	.284	4	0	10	0	4	0	15
16			min	-365.766	3	.074	15	-.087	3	0	4	0	3	0	6
17		9	max	226.069	1	.276	6	.178	4	0	10	0	4	0	15
18			min	-365.679	3	.064	15	-.087	3	0	4	0	3	0	6
19		10	max	226.185	1	.23	6	.153	1	0	10	0	4	0	15
20			min	-365.592	3	.053	15	-.087	3	0	4	0	3	0	6
21		11	max	226.301	1	.184	6	.153	1	0	10	0	4	0	15
22			min	-365.504	3	.042	15	-.087	3	0	4	0	3	0	6
23		12	max	226.418	1	.14	2	.153	1	0	10	0	4	0	15
24			min	-365.417	3	.031	15	-.179	5	0	4	0	3	0	6
25		13	max	226.534	1	.105	2	.153	1	0	10	0	4	0	15
26			min	-365.33	3	.018	12	-.284	5	0	4	0	3	0	6
27		14	max	226.651	1	.069	2	.153	1	0	10	0	4	0	15
28			min	-365.242	3	-.003	3	-.39	5	0	4	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	226.767	1	.034	2	.153	1	0	10	0	4	0	15
30			min	-365.155	3	-.03	3	-.495	5	0	4	0	3	0	6
31		16	max	226.883	1	-.002	2	.153	1	0	10	0	4	0	15
32			min	-365.068	3	-.057	3	-.601	5	0	4	0	3	0	6
33		17	max	227	1	-.022	15	.153	1	0	10	0	4	0	15
34			min	-364.981	3	-.09	4	-.706	5	0	4	0	3	0	6
35		18	max	227.116	1	-.033	15	.153	1	0	10	0	1	0	15
36			min	-364.893	3	-.135	4	-.812	5	0	4	0	3	0	6
37		19	max	227.233	1	-.044	15	.153	1	0	10	0	1	0	15
38			min	-364.806	3	-.181	4	-.917	5	0	4	0	3	0	6
39	M3	1	max	139.194	2	1.776	6	-.002	10	0	5	0	4	0	6
40			min	-131.821	3	.417	15	-1.343	4	0	1	0	10	0	15
41		2	max	139.126	2	1.599	6	-.002	10	0	5	0	1	0	2
42			min	-131.872	3	.375	15	-1.209	4	0	1	0	10	0	15
43		3	max	139.057	2	1.422	6	-.002	10	0	5	0	1	0	2
44			min	-131.924	3	.333	15	-1.076	4	0	1	0	5	0	3
45		4	max	138.989	2	1.245	6	-.002	10	0	5	0	1	0	15
46			min	-131.975	3	.292	15	-.942	4	0	1	0	5	0	4
47		5	max	138.92	2	1.068	6	-.002	10	0	5	0	1	0	15
48			min	-132.026	3	.25	15	-.809	4	0	1	0	5	0	4
49		6	max	138.851	2	.89	6	-.002	10	0	5	0	1	0	15
50			min	-132.078	3	.208	15	-.675	4	0	1	0	5	0	4
51		7	max	138.783	2	.713	6	-.002	10	0	5	0	1	0	15
52			min	-132.129	3	.167	15	-.541	4	0	1	0	5	0	4
53		8	max	138.714	2	.536	6	-.002	10	0	5	0	1	0	15
54			min	-132.181	3	.125	15	-.408	4	0	1	0	5	-.001	4
55		9	max	138.646	2	.359	6	-.002	10	0	5	0	1	0	15
56			min	-132.232	3	.083	15	-.274	4	0	1	0	5	-.001	4
57		10	max	138.577	2	.182	6	-.002	10	0	5	0	1	0	15
58			min	-132.284	3	.042	15	-.175	1	0	1	0	5	-.001	4
59		11	max	138.508	2	.029	2	.032	5	0	5	0	1	0	15
60			min	-132.335	3	-.022	3	-.175	1	0	1	0	5	-.001	4
61		12	max	138.44	2	-.042	15	.166	5	0	5	0	1	0	15
62			min	-132.387	3	-.173	4	-.175	1	0	1	0	5	-.001	4
63		13	max	138.371	2	-.083	15	.3	5	0	5	0	1	0	15
64			min	-132.438	3	-.35	4	-.175	1	0	1	0	5	-.001	4
65		14	max	138.303	2	-.125	15	.433	5	0	5	0	1	0	15
66			min	-132.49	3	-.527	4	-.175	1	0	1	0	5	-.001	4
67		15	max	138.234	2	-.167	15	.567	5	0	5	0	9	0	15
68			min	-132.541	3	-.705	4	-.175	1	0	1	0	5	0	4
69		16	max	138.165	2	-.208	15	.701	5	0	5	0	10	0	15
70			min	-132.592	3	-.882	4	-.175	1	0	1	0	4	0	4
71		17	max	138.097	2	-.25	15	.834	5	0	5	0	10	0	15
72			min	-132.644	3	-1.059	4	-.175	1	0	1	0	4	0	4
73		18	max	138.028	2	-.292	15	.968	5	0	5	0	10	0	15
74			min	-132.695	3	-1.236	4	-.175	1	0	1	0	4	0	4
75		19	max	137.96	2	-.333	15	1.101	5	0	5	0	5	0	1
76			min	-132.747	3	-1.413	4	-.175	1	0	1	0	1	0	1
77	M4	1	max	308.614	1	0	1	0	10	0	1	0	5	0	1
78			min	-33.296	3	0	1	-16.505	4	0	1	0	2	0	1
79		2	max	308.678	1	0	1	0	10	0	1	0	10	0	1
80			min	-33.247	3	0	1	-16.561	4	0	1	-.001	4	0	1
81		3	max	308.743	1	0	1	0	10	0	1	0	10	0	1
82			min	-33.199	3	0	1	-16.617	4	0	1	-.003	4	0	1
83		4	max	308.808	1	0	1	0	10	0	1	0	10	0	1
84			min	-33.15	3	0	1	-16.673	4	0	1	-.004	4	0	1
85		5	max	308.873	1	0	1	0	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	-33.102	3	0	1	-16.729	4	0	1	-.006	4	0	1
87		6	max	308.937	1	0	1	0	10	0	1	0	10	0	1
88			min	-33.053	3	0	1	-16.785	4	0	1	-.007	4	0	1
89		7	max	309.002	1	0	1	0	10	0	1	0	10	0	1
90			min	-33.005	3	0	1	-16.841	4	0	1	-.009	4	0	1
91		8	max	309.067	1	0	1	0	10	0	1	0	10	0	1
92			min	-32.956	3	0	1	-16.897	4	0	1	-.01	4	0	1
93		9	max	309.131	1	0	1	0	10	0	1	0	10	0	1
94			min	-32.908	3	0	1	-16.953	4	0	1	-.012	4	0	1
95		10	max	309.196	1	0	1	0	10	0	1	0	10	0	1
96			min	-32.859	3	0	1	-17.01	4	0	1	-.013	4	0	1
97		11	max	309.261	1	0	1	0	10	0	1	0	10	0	1
98			min	-32.811	3	0	1	-17.066	4	0	1	-.015	4	0	1
99		12	max	309.326	1	0	1	0	10	0	1	0	10	0	1
100			min	-32.762	3	0	1	-17.122	4	0	1	-.017	4	0	1
101		13	max	309.39	1	0	1	0	10	0	1	0	10	0	1
102			min	-32.714	3	0	1	-17.178	4	0	1	-.018	4	0	1
103		14	max	309.455	1	0	1	0	10	0	1	0	10	0	1
104			min	-32.665	3	0	1	-17.234	4	0	1	-.02	4	0	1
105		15	max	309.52	1	0	1	0	10	0	1	0	10	0	1
106			min	-32.617	3	0	1	-17.29	4	0	1	-.021	4	0	1
107		16	max	309.584	1	0	1	0	10	0	1	0	10	0	1
108			min	-32.568	3	0	1	-17.346	4	0	1	-.023	4	0	1
109		17	max	309.649	1	0	1	0	10	0	1	0	10	0	1
110			min	-32.52	3	0	1	-17.402	4	0	1	-.024	4	0	1
111		18	max	309.714	1	0	1	0	10	0	1	0	10	0	1
112			min	-32.471	3	0	1	-17.458	4	0	1	-.026	4	0	1
113		19	max	309.778	1	0	1	0	10	0	1	0	10	0	1
114			min	-32.422	3	0	1	-17.514	4	0	1	-.027	4	0	1
115	M6	1	max	709.746	1	.629	6	.98	4	0	3	0	3	0	1
116			min	-1135.021	3	.142	15	-.261	3	0	5	0	2	0	1
117		2	max	709.863	1	.583	6	.875	4	0	3	0	4	0	15
118			min	-1134.934	3	.131	15	-.261	3	0	5	0	2	0	6
119		3	max	709.979	1	.537	6	.769	4	0	3	0	4	0	15
120			min	-1134.846	3	.12	15	-.261	3	0	5	0	2	0	6
121		4	max	710.095	1	.492	6	.664	4	0	3	0	4	0	15
122			min	-1134.759	3	.109	15	-.261	3	0	5	0	2	0	6
123		5	max	710.212	1	.453	2	.558	4	0	3	0	4	0	15
124			min	-1134.672	3	.099	15	-.261	3	0	5	0	2	0	6
125		6	max	710.328	1	.417	2	.453	4	0	3	0	4	0	15
126			min	-1134.585	3	.088	15	-.261	3	0	5	0	3	0	6
127		7	max	710.445	1	.382	2	.347	4	0	3	0	4	0	15
128			min	-1134.497	3	.077	15	-.261	3	0	5	0	3	0	6
129		8	max	710.561	1	.346	2	.242	4	0	3	0	4	0	15
130			min	-1134.41	3	.066	15	-.261	3	0	5	0	3	0	2
131		9	max	710.677	1	.311	2	.136	4	0	3	0	4	0	15
132			min	-1134.323	3	.05	12	-.261	3	0	5	0	3	0	2
133		10	max	710.794	1	.275	2	.039	14	0	3	0	4	0	15
134			min	-1134.235	3	.032	12	-.261	3	0	5	0	3	0	2
135		11	max	710.91	1	.239	2	.036	9	0	3	0	4	0	15
136			min	-1134.148	3	.011	3	-.261	3	0	5	0	3	0	2
137		12	max	711.027	1	.204	2	.036	9	0	3	0	4	0	15
138			min	-1134.061	3	-.016	3	-.261	3	0	5	0	3	0	2
139		13	max	711.143	1	.168	2	.036	9	0	3	0	4	0	15
140			min	-1133.973	3	-.042	3	-.3	5	0	5	0	3	0	2
141		14	max	711.259	1	.133	2	.036	9	0	3	0	4	0	15
142			min	-1133.886	3	-.069	3	-.405	5	0	5	0	3	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	711.376	1	.097	2	.036	9	0	3	0	4	0	15
144			min	-1133.799	3	-.096	3	-.511	5	0	5	0	3	0	2
145		16	max	711.492	1	.062	2	.036	9	0	3	0	4	0	12
146			min	-1133.712	3	-.122	3	-.616	5	0	5	0	3	0	2
147		17	max	711.609	1	.026	2	.036	9	0	3	0	4	0	12
148			min	-1133.624	3	-.149	3	-.721	5	0	5	0	3	0	2
149		18	max	711.725	1	-.01	2	.036	9	0	3	0	4	0	12
150			min	-1133.537	3	-.176	3	-.827	5	0	5	0	3	0	2
151		19	max	711.841	1	-.045	2	.036	9	0	3	0	14	0	12
152			min	-1133.45	3	-.202	3	-.932	5	0	5	0	3	0	2
153	M7	1	max	467.999	2	1.791	4	.021	3	0	9	0	4	0	2
154			min	-371.993	3	.426	15	-1.355	4	0	3	0	3	0	12
155		2	max	467.93	2	1.613	4	.021	3	0	9	0	4	0	2
156			min	-372.044	3	.384	15	-1.222	4	0	3	0	3	0	3
157		3	max	467.862	2	1.436	4	.021	3	0	9	0	1	0	2
158			min	-372.095	3	.342	15	-1.088	4	0	3	0	3	0	3
159		4	max	467.793	2	1.259	4	.021	3	0	9	0	1	0	2
160			min	-372.147	3	.301	15	-.954	4	0	3	0	3	0	3
161		5	max	467.724	2	1.082	4	.021	3	0	9	0	1	0	15
162			min	-372.198	3	.259	15	-.821	4	0	3	0	5	0	3
163		6	max	467.656	2	.905	4	.021	3	0	9	0	1	0	15
164			min	-372.25	3	.218	15	-.687	4	0	3	0	5	0	6
165		7	max	467.587	2	.727	4	.021	3	0	9	0	1	0	15
166			min	-372.301	3	.176	15	-.553	4	0	3	0	5	0	6
167		8	max	467.519	2	.55	4	.021	3	0	9	0	1	0	15
168			min	-372.353	3	.134	15	-.42	4	0	3	0	5	0	6
169		9	max	467.45	2	.373	4	.021	3	0	9	0	1	0	15
170			min	-372.404	3	.093	15	-.286	4	0	3	0	5	-.001	6
171		10	max	467.381	2	.217	2	.021	3	0	9	0	1	0	15
172			min	-372.456	3	.025	12	-.153	4	0	3	0	5	-.001	6
173		11	max	467.313	2	.079	2	.021	3	0	9	0	1	0	15
174			min	-372.507	3	-.073	3	-.019	4	0	3	0	5	-.001	6
175		12	max	467.244	2	-.032	15	.116	5	0	9	0	1	0	15
176			min	-372.559	3	-.177	3	-.013	1	0	3	0	5	-.001	6
177		13	max	467.176	2	-.074	15	.249	5	0	9	0	1	0	15
178			min	-372.61	3	-.336	6	-.013	1	0	3	0	5	-.001	6
179		14	max	467.107	2	-.116	15	.383	5	0	9	0	1	0	15
180			min	-372.661	3	-.513	6	-.013	1	0	3	0	5	-.001	6
181		15	max	467.038	2	-.157	15	.517	5	0	9	0	1	0	15
182			min	-372.713	3	-.691	6	-.013	1	0	3	0	5	0	6
183		16	max	466.97	2	-.199	15	.65	5	0	9	0	1	0	15
184			min	-372.764	3	-.868	6	-.013	1	0	3	0	5	0	6
185		17	max	466.901	2	-.241	15	.784	5	0	9	0	1	0	15
186			min	-372.816	3	-1.045	6	-.013	1	0	3	0	5	0	6
187		18	max	466.832	2	-.282	15	.918	5	0	9	0	1	0	15
188			min	-372.867	3	-1.222	6	-.013	1	0	3	0	3	0	6
189		19	max	466.764	2	-.324	15	1.051	5	0	9	0	9	0	1
190			min	-372.919	3	-1.399	6	-.013	1	0	3	0	3	0	1
191	M8	1	max	879.063	1	0	1	.178	9	0	1	0	4	0	1
192			min	-142.117	3	0	1	-16.799	4	0	1	0	3	0	1
193		2	max	879.128	1	0	1	.178	9	0	1	0	9	0	1
194			min	-142.068	3	0	1	-16.855	4	0	1	-.001	4	0	1
195		3	max	879.192	1	0	1	.178	9	0	1	0	9	0	1
196			min	-142.02	3	0	1	-16.911	4	0	1	-.003	4	0	1
197		4	max	879.257	1	0	1	.178	9	0	1	0	9	0	1
198			min	-141.971	3	0	1	-16.967	4	0	1	-.005	4	0	1
199		5	max	879.322	1	0	1	.178	9	0	1	0	9	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	-141.923	3	0	1	-17.023	4	0	1	-.006	4	0	1
201		6	max	879.386	1	0	1	.178	9	0	1	0	9	0	1
202			min	-141.874	3	0	1	-17.079	4	0	1	-.008	4	0	1
203		7	max	879.451	1	0	1	.178	9	0	1	0	9	0	1
204			min	-141.826	3	0	1	-17.136	4	0	1	-.009	4	0	1
205		8	max	879.516	1	0	1	.178	9	0	1	0	9	0	1
206			min	-141.777	3	0	1	-17.192	4	0	1	-.011	4	0	1
207		9	max	879.58	1	0	1	.178	9	0	1	0	9	0	1
208			min	-141.729	3	0	1	-17.248	4	0	1	-.012	4	0	1
209		10	max	879.645	1	0	1	.178	9	0	1	0	9	0	1
210			min	-141.68	3	0	1	-17.304	4	0	1	-.014	4	0	1
211		11	max	879.71	1	0	1	.178	9	0	1	0	9	0	1
212			min	-141.632	3	0	1	-17.36	4	0	1	-.015	4	0	1
213		12	max	879.775	1	0	1	.178	9	0	1	0	9	0	1
214			min	-141.583	3	0	1	-17.416	4	0	1	-.017	4	0	1
215		13	max	879.839	1	0	1	.178	9	0	1	0	9	0	1
216			min	-141.534	3	0	1	-17.472	4	0	1	-.018	4	0	1
217		14	max	879.904	1	0	1	.178	9	0	1	0	9	0	1
218			min	-141.486	3	0	1	-17.528	4	0	1	-.02	4	0	1
219		15	max	879.969	1	0	1	.178	9	0	1	0	9	0	1
220			min	-141.437	3	0	1	-17.584	4	0	1	-.022	4	0	1
221		16	max	880.033	1	0	1	.178	9	0	1	0	9	0	1
222			min	-141.389	3	0	1	-17.64	4	0	1	-.023	4	0	1
223		17	max	880.098	1	0	1	.178	9	0	1	0	9	0	1
224			min	-141.34	3	0	1	-17.696	4	0	1	-.025	4	0	1
225		18	max	880.163	1	0	1	.178	9	0	1	0	9	0	1
226			min	-141.292	3	0	1	-17.752	4	0	1	-.026	4	0	1
227		19	max	880.228	1	0	1	.178	9	0	1	0	9	0	1
228			min	-141.243	3	0	1	-17.808	4	0	1	-.028	4	0	1
229	M10	1	max	226.777	1	.671	4	1.1	5	0	1	0	1	0	1
230			min	-312.981	3	.17	15	-.109	1	-.001	5	0	3	0	1
231		2	max	226.893	1	.626	4	.994	5	0	1	0	4	0	15
232			min	-312.894	3	.159	15	-.109	1	-.001	5	0	3	0	4
233		3	max	227.01	1	.58	4	.889	5	0	1	0	4	0	15
234			min	-312.807	3	.148	15	-.109	1	-.001	5	0	3	0	4
235		4	max	227.126	1	.534	4	.783	5	0	1	0	4	0	15
236			min	-312.719	3	.138	15	-.109	1	-.001	5	0	3	0	4
237		5	max	227.243	1	.489	4	.678	5	0	1	0	4	0	15
238			min	-312.632	3	.127	15	-.109	1	-.001	5	0	3	0	4
239		6	max	227.359	1	.443	4	.572	5	0	1	0	4	0	15
240			min	-312.545	3	.116	15	-.109	1	-.001	5	0	3	0	4
241		7	max	227.475	1	.397	4	.467	5	0	1	0	4	0	15
242			min	-312.457	3	.105	15	-.109	1	-.001	5	0	3	0	4
243		8	max	227.592	1	.352	4	.361	5	0	1	0	4	0	15
244			min	-312.37	3	.095	15	-.109	1	-.001	5	0	3	0	4
245		9	max	227.708	1	.306	4	.256	5	0	1	0	5	0	15
246			min	-312.283	3	.084	15	-.109	1	-.001	5	0	3	0	4
247		10	max	227.825	1	.26	4	.15	5	0	1	0	5	0	15
248			min	-312.195	3	.073	15	-.109	1	-.001	5	0	3	0	4
249		11	max	227.941	1	.215	4	.045	5	0	1	0	5	0	15
250			min	-312.108	3	.063	15	-.109	1	-.001	5	0	3	0	4
251		12	max	228.057	1	.169	4	-.004	10	0	1	0	5	0	15
252			min	-312.021	3	.049	12	-.109	1	-.001	5	0	3	0	4
253		13	max	228.174	1	.123	4	-.004	10	0	1	0	5	0	15
254			min	-311.934	3	.031	12	-.18	4	-.001	5	0	3	0	4
255		14	max	228.29	1	.078	4	-.004	10	0	1	0	5	0	15
256			min	-311.846	3	.014	12	-.285	4	-.001	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	228.407	1	.034	2	-.004	10	0	1	0	5	0	15
258			min	-311.759	3	-.007	3	-.391	4	-.001	5	0	3	0	4
259		16	max	228.523	1	.013	5	-.004	10	0	1	0	5	0	15
260			min	-311.672	3	-.034	3	-.496	4	-.001	5	0	3	0	4
261		17	max	228.639	1	-.002	15	-.004	10	0	1	0	5	0	15
262			min	-311.584	3	-.062	9	-.602	4	-.001	5	0	3	0	4
263		18	max	228.756	1	-.013	15	-.004	10	0	1	0	5	0	15
264			min	-311.497	3	-.106	6	-.707	4	-.001	5	0	3	0	4
265		19	max	228.872	1	-.023	15	-.004	10	0	1	0	5	0	15
266			min	-311.41	3	-.152	6	-.813	4	-.001	5	0	3	0	4
267	M11	1	max	138.766	2	1.77	6	.187	1	0	4	0	5	0	6
268			min	-132.544	3	.412	15	-1.255	5	0	10	0	1	0	15
269		2	max	138.697	2	1.593	6	.187	1	0	4	0	5	0	2
270			min	-132.595	3	.37	15	-1.122	5	0	10	0	1	0	12
271		3	max	138.628	2	1.416	6	.187	1	0	4	0	3	0	2
272			min	-132.647	3	.329	15	-.988	5	0	10	0	1	0	3
273		4	max	138.56	2	1.238	6	.187	1	0	4	0	3	0	15
274			min	-132.698	3	.287	15	-.854	5	0	10	0	1	0	4
275		5	max	138.491	2	1.061	6	.187	1	0	4	0	3	0	15
276			min	-132.75	3	.245	15	-.721	5	0	10	0	1	0	4
277		6	max	138.423	2	.884	6	.187	1	0	4	0	3	0	15
278			min	-132.801	3	.204	15	-.587	5	0	10	0	1	0	4
279		7	max	138.354	2	.707	6	.187	1	0	4	0	3	0	15
280			min	-132.852	3	.162	15	-.453	5	0	10	0	4	0	4
281		8	max	138.285	2	.529	6	.187	1	0	4	0	3	0	15
282			min	-132.904	3	.12	15	-.32	5	0	10	0	4	-.001	4
283		9	max	138.217	2	.352	6	.187	1	0	4	0	3	0	15
284			min	-132.955	3	.079	15	-.186	5	0	10	0	4	-.001	4
285		10	max	138.148	2	.175	6	.187	1	0	4	0	3	0	15
286			min	-133.007	3	.037	15	-.053	5	0	10	0	4	-.001	4
287		11	max	138.08	2	.029	2	.187	1	0	4	0	3	0	15
288			min	-133.058	3	-.034	3	-.04	3	0	10	0	4	-.001	4
289		12	max	138.011	2	-.046	15	.257	4	0	4	0	3	0	15
290			min	-133.11	3	-.18	4	-.04	3	0	10	0	4	-.001	4
291		13	max	137.942	2	-.088	15	.391	4	0	4	0	3	0	15
292			min	-133.161	3	-.357	4	-.04	3	0	10	0	4	-.001	4
293		14	max	137.874	2	-.129	15	.524	4	0	4	0	3	0	15
294			min	-133.213	3	-.534	4	-.04	3	0	10	0	4	-.001	4
295		15	max	137.805	2	-.171	15	.658	4	0	4	0	3	0	15
296			min	-133.264	3	-.711	4	-.04	3	0	10	0	5	0	4
297		16	max	137.737	2	-.213	15	.791	4	0	4	0	3	0	15
298			min	-133.316	3	-.888	4	-.04	3	0	10	0	10	0	4
299		17	max	137.668	2	-.254	15	.925	4	0	4	0	3	0	15
300			min	-133.367	3	-1.066	4	-.04	3	0	10	0	10	0	4
301		18	max	137.599	2	-.296	15	1.059	4	0	4	0	4	0	15
302			min	-133.418	3	-1.243	4	-.04	3	0	10	0	10	0	4
303		19	max	137.531	2	-.338	15	1.192	4	0	4	0	4	0	1
304			min	-133.47	3	-1.42	4	-.04	3	0	10	0	10	0	1
305	M12	1	max	308.728	1	0	1	.913	1	0	1	0	4	0	1
306			min	-32.767	3	0	1	-15.426	5	0	1	0	3	0	1
307		2	max	308.793	1	0	1	.913	1	0	1	0	1	0	1
308			min	-32.719	3	0	1	-15.482	5	0	1	-.001	5	0	1
309		3	max	308.858	1	0	1	.913	1	0	1	0	1	0	1
310			min	-32.67	3	0	1	-15.538	5	0	1	-.003	5	0	1
311		4	max	308.923	1	0	1	.913	1	0	1	0	1	0	1
312			min	-32.622	3	0	1	-15.594	5	0	1	-.004	5	0	1
313		5	max	308.987	1	0	1	.913	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	-32.573	3	0	1	-15.65	5	0	1	-.006	5	0	1
315		6	max	309.052	1	0	1	.913	1	0	1	0	1	0	1
316			min	-32.524	3	0	1	-15.706	5	0	1	-.007	5	0	1
317		7	max	309.117	1	0	1	.913	1	0	1	0	1	0	1
318			min	-32.476	3	0	1	-15.762	5	0	1	-.008	5	0	1
319		8	max	309.181	1	0	1	.913	1	0	1	0	1	0	1
320			min	-32.427	3	0	1	-15.818	5	0	1	-.01	5	0	1
321		9	max	309.246	1	0	1	.913	1	0	1	0	1	0	1
322			min	-32.379	3	0	1	-15.874	5	0	1	-.011	5	0	1
323		10	max	309.311	1	0	1	.913	1	0	1	0	1	0	1
324			min	-32.33	3	0	1	-15.931	5	0	1	-.013	5	0	1
325		11	max	309.376	1	0	1	.913	1	0	1	0	1	0	1
326			min	-32.282	3	0	1	-15.987	5	0	1	-.014	5	0	1
327		12	max	309.44	1	0	1	.913	1	0	1	0	1	0	1
328			min	-32.233	3	0	1	-16.043	5	0	1	-.015	5	0	1
329		13	max	309.505	1	0	1	.913	1	0	1	0	1	0	1
330			min	-32.185	3	0	1	-16.099	5	0	1	-.017	5	0	1
331		14	max	309.57	1	0	1	.913	1	0	1	.001	1	0	1
332			min	-32.136	3	0	1	-16.155	5	0	1	-.018	5	0	1
333		15	max	309.634	1	0	1	.913	1	0	1	.001	1	0	1
334			min	-32.088	3	0	1	-16.211	5	0	1	-.02	5	0	1
335		16	max	309.699	1	0	1	.913	1	0	1	.001	1	0	1
336			min	-32.039	3	0	1	-16.267	5	0	1	-.021	5	0	1
337		17	max	309.764	1	0	1	.913	1	0	1	.001	1	0	1
338			min	-31.991	3	0	1	-16.323	5	0	1	-.023	5	0	1
339		18	max	309.829	1	0	1	.913	1	0	1	.001	1	0	1
340			min	-31.942	3	0	1	-16.379	5	0	1	-.024	5	0	1
341		19	max	309.893	1	0	1	.913	1	0	1	.001	1	0	1
342			min	-31.894	3	0	1	-16.435	5	0	1	-.026	5	0	1
343	M1	1	max	76.594	1	345.479	3	-.189	10	0	2	.04	1	0	2
344			min	5.84	10	-232.724	2	-20.15	1	0	3	0	10	0	3
345		2	max	76.712	1	345.29	3	-.189	10	0	2	.035	1	.051	2
346			min	5.907	12	-232.977	2	-20.15	1	0	3	0	10	-.075	3
347		3	max	60.729	3	4.78	14	-.186	10	0	5	.031	1	.1	2
348			min	-8.842	10	-19.894	2	-20.063	1	0	1	0	10	-.149	3
349		4	max	60.818	3	4.532	14	-.186	10	0	5	.026	1	.105	2
350			min	-8.744	10	-20.147	2	-20.063	1	0	1	0	10	-.145	3
351		5	max	60.906	3	4.283	14	-.186	10	0	5	.022	1	.109	2
352			min	-8.646	10	-20.4	2	-20.063	1	0	1	0	10	-.141	3
353		6	max	60.995	3	4.034	14	-.186	10	0	5	.018	1	.114	2
354			min	-8.547	10	-20.653	2	-20.063	1	0	1	0	10	-.137	3
355		7	max	61.083	3	3.786	14	-.186	10	0	5	.013	1	.118	2
356			min	-8.449	10	-20.906	2	-20.063	1	0	1	0	10	-.133	3
357		8	max	61.172	3	3.537	14	-.186	10	0	5	.009	1	.123	2
358			min	-8.351	10	-21.159	2	-20.063	1	0	1	0	10	-.129	3
359		9	max	61.26	3	3.288	14	-.186	10	0	5	.004	1	.127	2
360			min	-8.252	10	-21.412	2	-20.063	1	0	1	0	10	-.125	3
361		10	max	61.349	3	3.04	14	-.186	10	0	5	.002	3	.132	2
362			min	-8.154	10	-21.665	2	-20.063	1	0	1	0	10	-.121	3
363		11	max	61.437	3	2.791	14	-.186	10	0	5	0	3	.137	2
364			min	-8.056	10	-21.918	2	-20.063	1	0	1	-.004	1	-.117	3
365		12	max	61.526	3	2.572	9	-.186	10	0	5	0	10	.142	2
366			min	-7.957	10	-22.171	2	-20.063	1	0	1	-.009	1	-.112	3
367		13	max	61.614	3	2.361	9	-.186	10	0	5	0	10	.146	2
368			min	-7.859	10	-22.425	2	-20.063	1	0	1	-.013	1	-.108	3
369		14	max	61.703	3	2.15	9	-.186	10	0	5	0	10	.151	2
370			min	-7.761	10	-22.678	2	-20.063	1	0	1	-.017	1	-.104	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	61.791	3	1.939	9	-.186	10	0	5	0	10	.156	2
372			min	-7.662	10	-22.931	2	-20.063	1	0	1	-.022	1	-.1	3
373		16	max	86.69	2	84.298	2	-.188	10	0	1	0	10	.16	2
374			min	-20.253	3	-124.414	3	-20.22	1	0	5	-.026	1	-.094	3
375		17	max	86.808	2	84.045	2	-.188	10	0	1	0	10	.142	2
376			min	-20.164	3	-124.604	3	-20.22	1	0	5	-.031	1	-.067	3
377		18	max	-3.894	12	328.871	2	-.187	10	0	3	0	10	.072	2
378			min	-76.697	1	-155.01	3	-27.601	4	0	2	-.035	1	-.034	3
379		19	max	-3.835	12	328.618	2	-.187	10	0	3	0	10	0	2
380			min	-76.579	1	-155.2	3	-27.359	4	0	2	-.04	1	0	3
381	M5	1	max	185.084	1	1113.127	3	0	2	0	9	.031	4	0	3
382			min	.045	3	-743.315	2	-66.769	3	0	5	0	10	0	2
383		2	max	185.202	1	1112.937	3	0	2	0	9	.026	4	.161	2
384			min	.133	3	-743.568	2	-66.769	3	0	5	-.005	3	-.241	3
385		3	max	165.703	3	5.401	9	7.271	3	0	3	.022	4	.319	2
386			min	-25.064	10	-69.435	2	-16.979	4	0	4	-.019	3	-.477	3
387		4	max	165.791	3	5.191	9	7.271	3	0	3	.018	4	.334	2
388			min	-24.965	10	-69.689	2	-16.737	4	0	4	-.017	3	-.463	3
389		5	max	165.88	3	4.98	9	7.271	3	0	3	.015	4	.35	2
390			min	-24.867	10	-69.942	2	-16.495	4	0	4	-.016	3	-.449	3
391		6	max	165.968	3	4.769	9	7.271	3	0	3	.011	4	.365	2
392			min	-24.769	10	-70.195	2	-16.253	4	0	4	-.014	3	-.435	3
393		7	max	166.057	3	4.558	9	7.271	3	0	3	.008	4	.38	2
394			min	-24.67	10	-70.448	2	-16.011	4	0	4	-.013	3	-.421	3
395		8	max	166.145	3	4.347	9	7.271	3	0	3	.004	4	.395	2
396			min	-24.572	10	-70.701	2	-15.769	4	0	4	-.011	3	-.406	3
397		9	max	166.234	3	4.136	9	7.271	3	0	3	0	4	.411	2
398			min	-24.474	10	-70.954	2	-15.527	4	0	4	-.009	3	-.392	3
399		10	max	166.322	3	3.925	9	7.271	3	0	3	0	2	.426	2
400			min	-24.375	10	-71.207	2	-15.285	4	0	4	-.008	3	-.378	3
401		11	max	166.411	3	3.714	9	7.271	3	0	3	0	2	.442	2
402			min	-24.277	10	-71.46	2	-15.043	4	0	4	-.006	3	-.364	3
403		12	max	166.499	3	3.503	9	7.271	3	0	3	0	2	.457	2
404			min	-24.179	10	-71.713	2	-14.801	4	0	4	-.009	4	-.349	3
405		13	max	166.588	3	3.292	9	7.271	3	0	3	0	2	.473	2
406			min	-24.08	10	-71.966	2	-14.559	4	0	4	-.012	4	-.335	3
407		14	max	166.676	3	3.082	9	7.271	3	0	3	0	2	.488	2
408			min	-23.982	10	-72.219	2	-14.317	4	0	4	-.015	4	-.32	3
409		15	max	166.765	3	2.871	9	7.271	3	0	3	0	3	.504	2
410			min	-23.884	10	-72.472	2	-14.075	4	0	4	-.019	4	-.306	3
411		16	max	277.785	2	294.666	2	7.238	3	0	3	.001	3	.517	2
412			min	-65.141	3	-358.678	3	-12.788	4	0	4	-.022	4	-.289	3
413		17	max	277.903	2	294.413	2	7.238	3	0	3	.003	3	.453	2
414			min	-65.053	3	-358.868	3	-12.546	4	0	4	-.024	4	-.211	3
415		18	max	-3.679	12	1051.979	2	6.667	3	0	4	.004	3	.227	2
416			min	-185.237	1	-488.406	3	-28.75	5	0	9	-.031	4	-.106	3
417		19	max	-3.62	12	1051.726	2	6.667	3	0	4	.006	3	0	3
418			min	-185.119	1	-488.595	3	-28.508	5	0	9	-.037	4	0	2
419	M9	1	max	76.457	1	345.41	3	120.648	4	0	3	0	15	0	2
420			min	.816	15	-232.724	2	.189	10	0	2	-.039	1	0	3
421		2	max	76.575	1	345.22	3	120.89	4	0	3	.025	5	.051	2
422			min	.851	15	-232.977	2	.189	10	0	2	-.035	1	-.075	3
423		3	max	60.35	3	4.455	9	19.769	1	0	1	.049	5	.1	2
424			min	-8.499	10	-19.869	2	-21.93	5	0	5	-.03	1	-.148	3
425		4	max	60.438	3	4.244	9	19.769	1	0	1	.044	5	.105	2
426			min	-8.401	10	-20.122	2	-21.688	5	0	5	-.026	1	-.145	3
427		5	max	60.527	3	4.033	9	19.769	1	0	1	.039	5	.109	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-8.302	10	-20.375	2	-21.446	5	0	5	-.022	1	-.141	3
429		6	max	60.615	3	3.822	9	19.769	1	0	1	.034	5	.114	2
430			min	-8.204	10	-20.628	2	-21.204	5	0	5	-.017	1	-.137	3
431		7	max	60.704	3	3.611	9	19.769	1	0	1	.03	5	.118	2
432			min	-8.106	10	-20.881	2	-20.962	5	0	5	-.013	1	-.133	3
433		8	max	60.792	3	3.4	9	19.769	1	0	1	.025	5	.123	2
434			min	-8.007	10	-21.134	2	-20.72	5	0	5	-.009	1	-.129	3
435		9	max	60.881	3	3.189	9	19.769	1	0	1	.021	5	.127	2
436			min	-7.909	10	-21.387	2	-20.478	5	0	5	-.004	1	-.125	3
437		10	max	60.969	3	2.978	9	19.769	1	0	1	.017	4	.132	2
438			min	-7.811	10	-21.64	2	-20.236	5	0	5	0	1	-.121	3
439		11	max	61.058	3	2.768	9	19.769	1	0	1	.013	4	.137	2
440			min	-7.712	10	-21.893	2	-19.994	5	0	5	0	10	-.117	3
441		12	max	61.146	3	2.557	9	19.769	1	0	1	.01	4	.141	2
442			min	-7.614	10	-22.146	2	-19.752	5	0	5	0	10	-.112	3
443		13	max	61.235	3	2.346	9	19.769	1	0	1	.013	1	.146	2
444			min	-7.516	10	-22.399	2	-19.51	5	0	5	0	10	-.108	3
445		14	max	61.323	3	2.135	9	19.769	1	0	1	.017	1	.151	2
446			min	-7.417	10	-22.652	2	-19.268	5	0	5	0	5	-.104	3
447		15	max	61.412	3	1.924	9	19.769	1	0	1	.021	1	.156	2
448			min	-7.319	10	-22.905	2	-19.026	5	0	5	-.005	5	-.1	3
449		16	max	86.835	2	83.989	2	19.937	1	0	10	.026	1	.16	2
450			min	-21.074	3	-124.886	3	-17.635	5	0	4	-.008	5	-.094	3
451		17	max	86.953	2	83.736	2	19.937	1	0	10	.03	1	.142	2
452			min	-20.986	3	-125.076	3	-17.393	5	0	4	-.012	5	-.067	3
453		18	max	6.963	5	328.871	2	20.852	1	0	2	.035	1	.072	2
454			min	-76.555	1	-155.002	3	-32.567	5	0	3	-.019	5	-.034	3
455		19	max	7.018	5	328.618	2	20.852	1	0	2	.039	1	0	2
456			min	-76.437	1	-155.192	3	-32.325	5	0	3	-.026	5	0	3
457	M13	1	max	120.648	4	232.638	2	-.816	15	0	2	.039	1	0	2
458			min	.189	10	-345.449	3	-76.452	1	0	3	0	15	0	3
459		2	max	116.01	4	165.54	2	-.133	15	0	2	.012	3	.139	3
460			min	.189	10	-245.229	3	-57.667	1	0	3	-.002	10	-.094	2
461		3	max	111.372	4	98.442	2	.73	5	0	2	.009	3	.232	3
462			min	.189	10	-145.01	3	-38.881	1	0	3	-.015	1	-.156	2
463		4	max	106.734	4	31.345	2	1.786	5	0	2	.006	3	.276	3
464			min	.189	10	-44.791	3	-20.096	1	0	3	-.029	1	-.187	2
465		5	max	102.096	4	55.429	3	2.841	5	0	2	.004	3	.274	3
466			min	.189	10	-35.753	2	-4.593	3	0	3	-.034	1	-.186	2
467		6	max	97.458	4	155.648	3	17.475	1	0	2	.003	5	.224	3
468			min	.189	10	-102.851	2	-3.6	3	0	3	-.03	1	-.153	2
469		7	max	92.82	4	255.867	3	36.26	1	0	2	.005	5	.127	3
470			min	.189	10	-169.949	2	-2.607	3	0	3	-.018	1	-.089	2
471		8	max	88.182	4	356.087	3	55.045	1	0	2	.008	4	.009	1
472			min	.189	10	-237.047	2	-1.614	3	0	3	0	3	-.018	3
473		9	max	83.544	4	456.306	3	73.831	1	0	2	.034	1	.135	2
474			min	.189	10	-304.144	2	-.621	3	0	3	-.001	3	-.209	3
475		10	max	78.906	4	556.526	3	92.616	1	0	2	.074	1	.295	2
476			min	.189	10	-371.242	2	.372	3	0	3	-.016	5	-.449	3
477		11	max	54.604	4	304.144	2	5.277	5	0	3	.034	1	.135	2
478			min	.189	10	-456.306	3	-73.693	1	0	2	-.013	5	-.209	3
479		12	max	49.966	4	237.047	2	6.333	5	0	3	.005	2	.009	1
480			min	.189	10	-356.087	3	-54.908	1	0	2	-.011	5	-.018	3
481		13	max	45.328	4	169.949	2	7.388	5	0	3	0	10	.127	3
482			min	.189	10	-255.867	3	-36.123	1	0	2	-.018	1	-.089	2
483		14	max	40.69	4	102.851	2	8.444	5	0	3	-.002	10	.224	3
484			min	.189	10	-155.648	3	-17.337	1	0	2	-.03	1	-.153	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	36.052	4	35.753	2	10.228	4	0	3	0	5	.274	3
486			min	.189	10	-55.429	3	-2.144	2	0	2	-.034	1	-.186	2
487		16	max	31.414	4	44.791	3	20.233	1	0	3	.005	5	.276	3
488			min	.189	10	-31.345	2	.186	10	0	2	-.029	1	-.187	2
489		17	max	26.776	4	145.01	3	39.019	1	0	3	.011	5	.232	3
490			min	.189	10	-98.442	2	2.071	10	0	2	-.015	1	-.156	2
491		18	max	22.138	4	245.229	3	57.804	1	0	3	.019	4	.139	3
492			min	.189	10	-165.54	2	3.955	10	0	2	-.002	10	-.094	2
493		19	max	20.187	1	345.449	3	76.589	1	0	3	.04	1	0	2
494			min	.189	10	-232.638	2	5.84	10	0	2	0	10	0	3
495	M16	1	max	32.315	5	328.723	2	7.018	5	0	3	.039	1	0	2
496			min	-20.815	1	-155.214	3	-76.442	1	0	2	-.026	5	0	3
497		2	max	27.677	5	233.712	2	8.074	5	0	3	.008	1	.063	3
498			min	-20.815	1	-110.821	3	-57.657	1	0	2	-.022	5	-.133	2
499		3	max	23.039	5	138.701	2	9.129	5	0	3	0	3	.105	3
500			min	-20.815	1	-66.428	3	-38.871	1	0	2	-.021	4	-.221	2
501		4	max	18.401	5	43.69	2	10.185	5	0	3	-.001	12	.126	3
502			min	-20.815	1	-22.035	3	-20.086	1	0	2	-.029	1	-.264	2
503		5	max	13.763	5	22.357	3	11.24	5	0	3	-.002	12	.125	3
504			min	-20.815	1	-51.321	2	-3.002	3	0	2	-.034	1	-.262	2
505		6	max	9.125	5	66.75	3	17.485	1	0	3	-.002	15	.104	3
506			min	-20.815	1	-146.331	2	-2.009	3	0	2	-.03	1	-.215	2
507		7	max	4.487	5	111.143	3	36.27	1	0	3	.003	5	.062	3
508			min	-20.815	1	-241.342	2	-1.016	3	0	2	-.018	1	-.124	2
509		8	max	2.14	3	155.536	3	55.055	1	0	3	.01	4	.013	2
510			min	-20.815	1	-336.353	2	-.023	3	0	2	-.006	3	0	3
511		9	max	2.14	3	199.928	3	73.841	1	0	3	.034	1	.194	2
512			min	-20.815	1	-431.364	2	.836	12	0	2	-.006	3	-.084	3
513		10	max	19.089	5	-8.093	15	92.626	1	0	14	.074	1	.42	2
514			min	-20.815	1	-526.375	2	-3.009	3	0	2	-.005	3	-.189	3
515		11	max	14.451	5	431.364	2	4.472	5	0	2	.034	1	.194	2
516			min	-20.769	1	-199.928	3	-73.698	1	0	3	-.01	5	-.084	3
517		12	max	9.813	5	336.353	2	5.527	5	0	2	.005	2	.013	2
518			min	-20.769	1	-155.536	3	-54.913	1	0	3	-.008	5	0	3
519		13	max	5.175	5	241.342	2	6.582	5	0	2	0	10	.062	3
520			min	-20.769	1	-111.143	3	-36.128	1	0	3	-.018	1	-.124	2
521		14	max	.537	5	146.331	2	7.638	5	0	2	0	12	.104	3
522			min	-20.769	1	-66.75	3	-17.342	1	0	3	-.03	1	-.215	2
523		15	max	-.187	10	51.321	2	9.4	4	0	2	.002	5	.125	3
524			min	-20.769	1	-22.357	3	-2.134	2	0	3	-.034	1	-.262	2
525		16	max	-.187	10	22.035	3	20.228	1	0	2	.006	5	.126	3
526			min	-20.769	1	-43.69	2	.191	10	0	3	-.029	1	-.264	2
527		17	max	-.187	10	66.428	3	39.014	1	0	2	.011	5	.105	3
528			min	-20.769	1	-138.701	2	2.075	10	0	3	-.015	1	-.221	2
529		18	max	-.187	10	110.821	3	57.799	1	0	2	.019	4	.063	3
530			min	-22.745	4	-233.712	2	3.173	12	0	3	-.002	10	-.133	2
531		19	max	-.187	10	155.214	3	76.584	1	0	2	.04	1	0	2
532			min	-27.383	4	-328.723	2	3.835	12	0	3	0	10	0	3
533	M15	1	max	0	1	.879	3	.124	3	0	1	0	1	0	1
534			min	-90.83	3	0	1	0	1	0	3	0	3	0	1
535		2	max	0	1	.781	3	.124	3	0	1	0	1	0	1
536			min	-90.895	3	0	1	0	1	0	3	0	3	0	3
537		3	max	0	1	.684	3	.124	3	0	1	0	1	0	1
538			min	-90.961	3	0	1	0	1	0	3	0	3	0	3
539		4	max	0	1	.586	3	.124	3	0	1	0	1	0	1
540			min	-91.026	3	0	1	0	1	0	3	0	3	0	3
541		5	max	0	1	.488	3	.124	3	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-91.091	3	0	1	0	1	0	3	0	3	0	3
543		6	max	0	1	.391	3	.124	3	0	1	0	1	0	1
544			min	-91.156	3	0	1	0	1	0	3	0	3	0	3
545		7	max	0	1	.293	3	.124	3	0	1	0	3	0	1
546			min	-91.221	3	0	1	0	1	0	3	0	1	-.001	3
547		8	max	0	1	.195	3	.124	3	0	1	0	3	0	1
548			min	-91.287	3	0	1	0	1	0	3	0	1	-.001	3
549		9	max	0	1	.098	3	.124	3	0	1	0	3	0	1
550			min	-91.352	3	0	1	0	1	0	3	0	1	-.001	3
551		10	max	0	1	0	1	.124	3	0	1	0	3	0	1
552			min	-91.417	3	0	1	0	1	0	3	0	1	-.001	3
553		11	max	0	1	0	1	.124	3	0	1	0	3	0	1
554			min	-91.482	3	-.098	3	0	1	0	3	0	1	-.001	3
555		12	max	0	1	0	1	.124	3	0	1	0	3	0	1
556			min	-91.547	3	-.195	3	0	1	0	3	0	1	-.001	3
557		13	max	0	1	0	1	.124	3	0	1	0	3	0	1
558			min	-91.613	3	-.293	3	0	1	0	3	0	1	-.001	3
559		14	max	0	1	0	1	.124	3	0	1	0	3	0	1
560			min	-91.678	3	-.391	3	0	1	0	3	0	1	0	3
561		15	max	0	1	0	1	.124	3	0	1	0	3	0	1
562			min	-91.743	3	-.488	3	0	1	0	3	0	1	0	3
563		16	max	0	1	0	1	.124	3	0	1	0	3	0	1
564			min	-91.808	3	-.586	3	0	1	0	3	0	1	0	3
565		17	max	0	1	0	1	.124	3	0	1	0	3	0	1
566			min	-91.873	3	-.684	3	0	1	0	3	0	1	0	3
567		18	max	0	1	0	1	.124	3	0	1	0	3	0	1
568			min	-91.938	3	-.781	3	0	1	0	3	0	1	0	3
569		19	max	0	1	0	1	.124	3	0	1	0	3	0	1
570			min	-92.004	3	-.879	3	0	1	0	3	0	1	0	1
571	M16A	1	max	0	2	2.168	4	.283	4	0	3	0	3	0	1
572			min	-173.207	4	0	2	-.05	3	0	1	0	4	0	1
573		2	max	0	2	1.927	4	.255	4	0	3	0	3	0	2
574			min	-173.206	4	0	2	-.05	3	0	1	0	4	0	4
575		3	max	0	2	1.686	4	.227	4	0	3	0	3	0	2
576			min	-173.205	4	0	2	-.05	3	0	1	0	4	-.001	4
577		4	max	0	2	1.445	4	.2	4	0	3	0	3	0	2
578			min	-173.204	4	0	2	-.05	3	0	1	0	1	-.002	4
579		5	max	0	2	1.204	4	.172	4	0	3	0	3	0	2
580			min	-173.203	4	0	2	-.05	3	0	1	0	1	-.002	4
581		6	max	0	2	.964	4	.144	4	0	3	0	3	0	2
582			min	-173.202	4	0	2	-.05	3	0	1	0	1	-.002	4
583		7	max	0	2	.723	4	.117	4	0	3	0	3	0	2
584			min	-173.201	4	0	2	-.05	3	0	1	0	1	-.003	4
585		8	max	0	2	.482	4	.089	4	0	3	0	5	0	2
586			min	-173.2	4	0	2	-.05	3	0	1	0	1	-.003	4
587		9	max	0	2	.241	4	.061	4	0	3	0	5	0	2
588			min	-173.199	4	0	2	-.05	3	0	1	0	1	-.003	4
589		10	max	0	2	0	1	.039	1	0	3	0	5	0	2
590			min	-173.198	4	0	1	-.05	3	0	1	0	1	-.003	4
591		11	max	0	2	0	2	.039	1	0	3	0	5	0	2
592			min	-173.197	4	-.241	4	-.05	3	0	1	0	1	-.003	4
593		12	max	.013	11	0	2	.039	1	0	3	0	5	0	2
594			min	-173.196	4	-.482	4	-.05	3	0	1	0	1	-.003	4
595		13	max	.085	11	0	2	.039	1	0	3	0	5	0	2
596			min	-173.195	4	-.723	4	-.053	5	0	1	0	3	-.003	4
597		14	max	.158	11	0	2	.039	1	0	3	0	5	0	2
598			min	-173.194	4	-.964	4	-.081	5	0	1	0	3	-.002	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.23	11	0	2	.039	1	0	3	0	5	0	2
600			min	-173.193	4	-1.204	4	-.108	5	0	1	0	3	-.002	4
601		16	max	.302	11	0	2	.039	1	0	3	0	4	0	2
602			min	-173.191	4	-1.445	4	-.136	5	0	1	0	3	-.002	4
603		17	max	.375	11	0	2	.039	1	0	3	0	1	0	2
604			min	-173.19	4	-1.686	4	-.164	5	0	1	0	3	-.001	4
605		18	max	.447	11	0	2	.039	1	0	3	0	1	0	2
606			min	-173.189	4	-1.927	4	-.191	5	0	1	0	3	0	4
607		19	max	.52	11	0	2	.039	1	0	3	0	1	0	1
608			min	-173.232	5	-2.168	4	-.219	5	0	1	0	5	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	1	.008	2	.003	1	9.535e-4	5	NC	3	NC	1
2			min	-.003	3	-.008	3	-.01	5	-3.111e-4	1	4524.743	2	NC	1
3		2	max	.002	1	.007	2	.003	1	9.739e-4	5	NC	3	NC	1
4			min	-.003	3	-.007	3	-.009	5	-2.975e-4	1	4929.118	2	NC	1
5		3	max	.002	1	.007	2	.003	1	9.942e-4	5	NC	3	NC	1
6			min	-.003	3	-.007	3	-.009	5	-2.839e-4	1	5408.483	2	NC	1
7		4	max	.002	1	.006	2	.003	1	1.015e-3	5	NC	1	NC	1
8			min	-.003	3	-.007	3	-.009	5	-2.703e-4	1	5980.745	2	NC	1
9		5	max	.002	1	.005	2	.002	1	1.035e-3	5	NC	1	NC	1
10			min	-.003	3	-.006	3	-.009	5	-2.566e-4	1	6669.722	2	NC	1
11		6	max	.001	1	.005	2	.002	1	1.055e-3	5	NC	1	NC	1
12			min	-.002	3	-.006	3	-.008	5	-2.43e-4	1	7507.614	2	NC	1
13		7	max	.001	1	.004	2	.002	1	1.076e-3	5	NC	1	NC	1
14			min	-.002	3	-.006	3	-.008	5	-2.294e-4	1	8538.79	2	NC	1
15		8	max	.001	1	.004	2	.002	1	1.096e-3	5	NC	1	NC	1
16			min	-.002	3	-.005	3	-.007	5	-2.158e-4	1	9825.769	2	NC	1
17		9	max	.001	1	.003	2	.001	1	1.116e-3	5	NC	1	NC	1
18			min	-.002	3	-.005	3	-.007	5	-2.021e-4	1	NC	1	NC	1
19		10	max	.001	1	.003	2	.001	1	1.137e-3	5	NC	1	NC	1
20			min	-.002	3	-.005	3	-.006	5	-1.885e-4	1	NC	1	NC	1
21		11	max	0	1	.002	2	.001	1	1.157e-3	5	NC	1	NC	1
22			min	-.001	3	-.004	3	-.006	5	-1.749e-4	1	NC	1	NC	1
23		12	max	0	1	.002	2	0	1	1.177e-3	5	NC	1	NC	1
24			min	-.001	3	-.004	3	-.005	5	-1.613e-4	1	NC	1	NC	1
25		13	max	0	1	.001	2	0	1	1.198e-3	5	NC	1	NC	1
26			min	-.001	3	-.003	3	-.005	5	-1.477e-4	1	NC	1	NC	1
27		14	max	0	1	.001	2	0	1	1.218e-3	5	NC	1	NC	1
28			min	0	3	-.003	3	-.004	5	-1.34e-4	1	NC	1	NC	1
29		15	max	0	1	0	2	0	1	1.239e-3	5	NC	1	NC	1
30			min	0	3	-.002	3	-.003	5	-1.204e-4	1	NC	1	NC	1
31		16	max	0	1	0	2	0	1	1.259e-3	5	NC	1	NC	1
32			min	0	3	-.002	3	-.002	5	-1.068e-4	1	NC	1	NC	1
33		17	max	0	1	0	2	0	1	1.279e-3	5	NC	1	NC	1
34			min	0	3	-.001	3	-.002	5	-9.316e-5	1	NC	1	NC	1
35		18	max	0	1	0	2	0	1	1.3e-3	5	NC	1	NC	1
36			min	0	3	0	3	0	5	-7.954e-5	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	1.32e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-6.592e-5	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	3.073e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-6.14e-4	5	NC	1	NC	1
41		2	max	0	3	0	2	.003	5	4.028e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	1	-6.179e-4	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	3	0	2	.006	5	4.982e-5	1	NC	1	NC	1
44			min	0	2	-.002	3	0	1	-6.218e-4	5	NC	1	NC	1
45		4	max	0	3	0	2	.01	5	5.937e-5	1	NC	1	NC	1
46			min	0	2	-.002	3	0	1	-6.257e-4	5	NC	1	NC	1
47		5	max	0	3	0	2	.013	5	6.891e-5	1	NC	1	NC	1
48			min	0	2	-.003	3	0	1	-6.296e-4	5	NC	1	NC	1
49		6	max	0	3	0	2	.016	4	7.846e-5	1	NC	1	NC	1
50			min	0	2	-.004	3	0	9	-6.335e-4	5	NC	1	NC	1
51		7	max	0	3	0	2	.019	4	8.8e-5	1	NC	1	NC	1
52			min	0	2	-.005	3	0	9	-6.374e-4	5	NC	1	NC	1
53		8	max	0	3	0	2	.022	4	9.755e-5	1	NC	1	NC	1
54			min	0	2	-.005	3	0	9	-6.413e-4	5	NC	1	NC	1
55		9	max	0	3	.001	2	.025	4	1.071e-4	1	NC	1	NC	1
56			min	0	2	-.006	3	0	10	-6.452e-4	5	NC	1	NC	1
57		10	max	0	3	.002	2	.028	4	1.166e-4	1	NC	1	NC	1
58			min	0	2	-.006	3	0	10	-6.491e-4	5	NC	1	NC	1
59		11	max	0	3	.002	2	.031	4	1.262e-4	1	NC	1	NC	1
60			min	0	2	-.007	3	0	10	-6.53e-4	5	NC	1	NC	1
61		12	max	0	3	.003	2	.033	4	1.357e-4	1	NC	1	NC	1
62			min	0	2	-.007	3	0	10	-6.569e-4	5	NC	1	NC	1
63		13	max	.001	3	.003	2	.036	4	1.453e-4	1	NC	1	NC	1
64			min	-.001	2	-.007	3	0	10	-6.608e-4	5	NC	1	NC	1
65		14	max	.001	3	.004	2	.039	4	1.548e-4	1	NC	1	NC	1
66			min	-.001	2	-.007	3	0	10	-6.647e-4	5	NC	1	NC	1
67		15	max	.001	3	.005	2	.041	4	1.644e-4	1	NC	1	NC	1
68			min	-.001	2	-.008	3	0	10	-6.686e-4	5	9674.547	2	NC	1
69		16	max	.001	3	.006	2	.043	4	1.739e-4	1	NC	1	NC	1
70			min	-.001	2	-.008	3	0	10	-6.725e-4	5	8156.831	2	NC	1
71		17	max	.001	3	.007	2	.046	4	1.835e-4	1	NC	1	NC	1
72			min	-.001	2	-.008	3	0	10	-6.764e-4	5	6990.62	2	NC	1
73		18	max	.001	3	.008	2	.048	4	1.93e-4	1	NC	3	NC	1
74			min	-.001	2	-.008	3	0	10	-6.803e-4	5	6083.569	2	NC	1
75		19	max	.002	3	.009	2	.05	4	2.026e-4	1	NC	3	NC	1
76			min	-.002	2	-.008	3	0	10	-6.842e-4	5	5371.337	2	NC	1
77	M4	1	max	.001	1	.009	2	0	10	2.991e-3	5	NC	1	NC	1
78			min	0	3	-.008	3	-.053	4	-2.478e-4	1	NC	1	362.753	4
79		2	max	.001	1	.009	2	0	10	2.991e-3	5	NC	1	NC	1
80			min	0	3	-.007	3	-.049	4	-2.478e-4	1	NC	1	395.41	4
81		3	max	.001	1	.008	2	0	10	2.991e-3	5	NC	1	NC	1
82			min	0	3	-.007	3	-.045	4	-2.478e-4	1	NC	1	434.274	4
83		4	max	.001	1	.008	2	0	10	2.991e-3	5	NC	1	NC	1
84			min	0	3	-.006	3	-.04	4	-2.478e-4	1	NC	1	480.98	4
85		5	max	.001	1	.007	2	0	10	2.991e-3	5	NC	1	NC	1
86			min	0	3	-.006	3	-.036	4	-2.478e-4	1	NC	1	537.754	4
87		6	max	.001	1	.007	2	0	10	2.991e-3	5	NC	1	NC	1
88			min	0	3	-.006	3	-.032	4	-2.478e-4	1	NC	1	607.693	4
89		7	max	0	1	.006	2	0	10	2.991e-3	5	NC	1	NC	1
90			min	0	3	-.005	3	-.028	4	-2.478e-4	1	NC	1	695.206	4
91		8	max	0	1	.006	2	0	10	2.991e-3	5	NC	1	NC	1
92			min	0	3	-.005	3	-.024	4	-2.478e-4	1	NC	1	806.75	4
93		9	max	0	1	.005	2	0	10	2.991e-3	5	NC	1	NC	1
94			min	0	3	-.004	3	-.02	4	-2.478e-4	1	NC	1	952.091	4
95		10	max	0	1	.005	2	0	10	2.991e-3	5	NC	1	NC	1
96			min	0	3	-.004	3	-.017	4	-2.478e-4	1	NC	1	1146.579	4
97		11	max	0	1	.004	2	0	10	2.991e-3	5	NC	1	NC	1
98			min	0	3	-.003	3	-.014	4	-2.478e-4	1	NC	1	1415.494	4
99		12	max	0	1	.004	2	0	10	2.991e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	3	-.003	3	-.011	4	-2.478e-4	1	NC	1	1802.929	4
101		13	max	0	1	.003	2	0	10	2.991e-3	5	NC	1	NC	1
102			min	0	3	-.003	3	-.008	4	-2.478e-4	1	NC	1	2391.59	4
103		14	max	0	1	.003	2	0	10	2.991e-3	5	NC	1	NC	1
104			min	0	3	-.002	3	-.006	4	-2.478e-4	1	NC	1	3352.062	4
105		15	max	0	1	.002	2	0	10	2.991e-3	5	NC	1	NC	1
106			min	0	3	-.002	3	-.004	4	-2.478e-4	1	NC	1	5085.087	4
107		16	max	0	1	.002	2	0	10	2.991e-3	5	NC	1	NC	1
108			min	0	3	-.001	3	-.002	4	-2.478e-4	1	NC	1	8729.826	4
109		17	max	0	1	.001	2	0	10	2.991e-3	5	NC	1	NC	1
110			min	0	3	0	3	-.001	4	-2.478e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	10	2.991e-3	5	NC	1	NC	1
112			min	0	3	0	3	0	4	-2.478e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	2.991e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-2.478e-4	1	NC	1	NC	1
115	M6	1	max	.006	1	.026	2	.001	9	1.016e-3	4	NC	3	NC	1
116			min	-.01	3	-.023	3	-.01	5	-8.236e-8	2	1380.738	2	6747.974	3
117		2	max	.006	1	.025	2	0	9	1.036e-3	4	NC	3	NC	1
118			min	-.01	3	-.022	3	-.009	5	-3.755e-7	11	1476.759	2	7189.562	3
119		3	max	.006	1	.023	2	0	9	1.056e-3	4	NC	3	NC	1
120			min	-.009	3	-.021	3	-.009	5	-1.262e-6	11	1586.71	2	7711.135	3
121		4	max	.005	1	.021	2	0	9	1.076e-3	4	NC	3	NC	1
122			min	-.008	3	-.02	3	-.009	5	-2.837e-6	1	1713.389	2	8330.186	3
123		5	max	.005	1	.02	2	0	9	1.096e-3	4	NC	3	NC	1
124			min	-.008	3	-.018	3	-.009	5	-4.828e-6	1	1860.405	2	9069.861	3
125		6	max	.005	1	.018	2	0	9	1.116e-3	4	NC	3	NC	1
126			min	-.007	3	-.017	3	-.008	5	-6.819e-6	1	2032.481	2	9961.257	3
127		7	max	.004	1	.016	2	0	9	1.136e-3	4	NC	3	NC	1
128			min	-.007	3	-.016	3	-.008	5	-8.811e-6	1	2235.923	2	NC	1
129		8	max	.004	1	.015	2	0	9	1.156e-3	4	NC	3	NC	1
130			min	-.006	3	-.015	3	-.008	5	-1.08e-5	1	2479.337	2	NC	1
131		9	max	.004	1	.013	2	0	9	1.176e-3	4	NC	3	NC	1
132			min	-.006	3	-.013	3	-.007	5	-1.279e-5	1	2774.779	2	NC	1
133		10	max	.003	1	.012	2	0	9	1.196e-3	4	NC	3	NC	1
134			min	-.005	3	-.012	3	-.007	5	-1.478e-5	1	3139.666	2	NC	1
135		11	max	.003	1	.01	2	0	9	1.216e-3	4	NC	3	NC	1
136			min	-.005	3	-.011	3	-.006	5	-1.678e-5	1	3600.128	2	NC	1
137		12	max	.002	1	.009	2	0	1	1.237e-3	4	NC	3	NC	1
138			min	-.004	3	-.01	3	-.005	5	-1.877e-5	1	4197.227	2	NC	1
139		13	max	.002	1	.007	2	0	1	1.257e-3	4	NC	3	NC	1
140			min	-.003	3	-.008	3	-.005	5	-2.076e-5	1	4999.401	2	NC	1
141		14	max	.002	1	.006	2	0	1	1.277e-3	4	NC	3	NC	1
142			min	-.003	3	-.007	3	-.004	5	-2.275e-5	1	6129.825	2	NC	1
143		15	max	.001	1	.005	2	0	1	1.297e-3	4	NC	1	NC	1
144			min	-.002	3	-.006	3	-.003	5	-2.474e-5	1	7834.837	2	NC	1
145		16	max	.001	1	.003	2	0	1	1.317e-3	4	NC	1	NC	1
146			min	-.002	3	-.004	3	-.002	5	-2.673e-5	1	NC	1	NC	1
147		17	max	0	1	.002	2	0	1	1.337e-3	4	NC	1	NC	1
148			min	-.001	3	-.003	3	-.002	5	-2.872e-5	1	NC	1	NC	1
149		18	max	0	1	.001	2	0	1	1.357e-3	4	NC	1	NC	1
150			min	0	3	-.001	3	0	5	-3.071e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.377e-3	4	NC	1	NC	1
152			min	0	1	0	1	0	1	-3.271e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	1.516e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-6.404e-4	4	NC	1	NC	1
155		2	max	0	3	.001	2	.003	4	1.375e-5	1	NC	1	NC	1
156			min	0	2	-.002	3	0	1	-6.331e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	3	.003	2	.007	4	1.234e-5	1	NC	1	NC	1
158			min	0	2	-.004	3	0	1	-6.259e-4	4	NC	1	NC	1
159		4	max	0	3	.004	2	.01	4	1.094e-5	1	NC	1	NC	1
160			min	0	2	-.005	3	0	1	-6.186e-4	4	NC	1	NC	1
161		5	max	0	3	.005	2	.013	4	9.526e-6	1	NC	1	NC	1
162			min	-.001	2	-.007	3	0	1	-6.114e-4	4	9270.493	2	NC	1
163		6	max	.001	3	.006	2	.017	4	1.938e-5	3	NC	1	NC	1
164			min	-.001	2	-.009	3	0	1	-6.041e-4	4	7431.354	2	NC	1
165		7	max	.001	3	.007	2	.02	4	4.159e-5	3	NC	1	NC	1
166			min	-.002	2	-.01	3	0	1	-5.969e-4	4	6171.395	2	NC	1
167		8	max	.002	3	.009	2	.023	4	6.38e-5	3	NC	3	NC	1
168			min	-.002	2	-.012	3	0	1	-5.896e-4	4	5246.116	2	NC	1
169		9	max	.002	3	.01	2	.026	4	8.6e-5	3	NC	3	NC	1
170			min	-.002	2	-.013	3	0	1	-5.824e-4	4	4533.765	2	NC	1
171		10	max	.002	3	.012	2	.029	4	1.082e-4	3	NC	3	NC	1
172			min	-.003	2	-.015	3	0	1	-5.751e-4	4	3966.879	2	NC	1
173		11	max	.002	3	.013	2	.032	4	1.304e-4	3	NC	3	NC	1
174			min	-.003	2	-.016	3	0	1	-5.679e-4	4	3504.933	2	NC	1
175		12	max	.003	3	.015	2	.035	4	1.526e-4	3	NC	3	NC	1
176			min	-.003	2	-.017	3	0	1	-5.606e-4	4	3121.964	2	NC	1
177		13	max	.003	3	.016	2	.037	4	1.748e-4	3	NC	3	NC	1
178			min	-.004	2	-.018	3	0	1	-5.534e-4	4	2800.42	2	NC	1
179		14	max	.003	3	.018	2	.04	4	1.97e-4	3	NC	3	NC	1
180			min	-.004	2	-.019	3	0	1	-5.461e-4	4	2527.895	2	NC	1
181		15	max	.003	3	.02	2	.042	4	2.192e-4	3	NC	3	NC	1
182			min	-.004	2	-.02	3	0	1	-5.389e-4	4	2295.28	2	NC	1
183		16	max	.004	3	.022	2	.045	4	2.414e-4	3	NC	3	NC	1
184			min	-.004	2	-.021	3	0	1	-5.316e-4	4	2095.685	2	NC	1
185		17	max	.004	3	.024	2	.047	4	2.637e-4	3	NC	3	NC	1
186			min	-.005	2	-.022	3	0	9	-5.244e-4	4	1923.765	2	NC	1
187		18	max	.004	3	.026	2	.049	4	2.859e-4	3	NC	3	NC	1
188			min	-.005	2	-.023	3	0	9	-5.171e-4	4	1775.297	2	NC	1
189		19	max	.004	3	.028	2	.052	4	3.081e-4	3	NC	3	NC	1
190			min	-.005	2	-.024	3	0	9	-5.099e-4	4	1646.898	2	NC	1
191	M8	1	max	.004	1	.03	2	0	9	2.829e-3	4	NC	1	NC	1
192			min	0	3	-.024	3	-.054	4	-2.313e-4	3	NC	1	356.563	4
193		2	max	.004	1	.028	2	0	9	2.829e-3	4	NC	1	NC	1
194			min	0	3	-.022	3	-.05	4	-2.313e-4	3	NC	1	388.664	4
195		3	max	.004	1	.026	2	0	9	2.829e-3	4	NC	1	NC	1
196			min	0	3	-.021	3	-.045	4	-2.313e-4	3	NC	1	426.866	4
197		4	max	.003	1	.025	2	0	9	2.829e-3	4	NC	1	NC	1
198			min	0	3	-.02	3	-.041	4	-2.313e-4	3	NC	1	472.776	4
199		5	max	.003	1	.023	2	0	9	2.829e-3	4	NC	1	NC	1
200			min	0	3	-.018	3	-.037	4	-2.313e-4	3	NC	1	528.584	4
201		6	max	.003	1	.021	2	0	9	2.829e-3	4	NC	1	NC	1
202			min	0	3	-.017	3	-.032	4	-2.313e-4	3	NC	1	597.333	4
203		7	max	.003	1	.02	2	0	9	2.829e-3	4	NC	1	NC	1
204			min	0	3	-.016	3	-.028	4	-2.313e-4	3	NC	1	683.357	4
205		8	max	.003	1	.018	2	0	9	2.829e-3	4	NC	1	NC	1
206			min	0	3	-.014	3	-.024	4	-2.313e-4	3	NC	1	793.004	4
207		9	max	.002	1	.017	2	0	9	2.829e-3	4	NC	1	NC	1
208			min	0	3	-.013	3	-.021	4	-2.313e-4	3	NC	1	935.874	4
209		10	max	.002	1	.015	2	0	9	2.829e-3	4	NC	1	NC	1
210			min	0	3	-.012	3	-.017	4	-2.313e-4	3	NC	1	1127.056	4
211		11	max	.002	1	.013	2	0	9	2.829e-3	4	NC	1	NC	1
212			min	0	3	-.01	3	-.014	4	-2.313e-4	3	NC	1	1391.401	4
213		12	max	.002	1	.012	2	0	9	2.829e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	3	-.009	3	-.011	4	-2.313e-4	3	NC	1	1772.254	4
215		13	max	.001	1	.01	2	0	9	2.829e-3	4	NC	1	NC	1
216			min	0	3	-.008	3	-.008	4	-2.313e-4	3	NC	1	2350.916	4
217		14	max	.001	1	.008	2	0	9	2.829e-3	4	NC	1	NC	1
218			min	0	3	-.007	3	-.006	4	-2.313e-4	3	NC	1	3295.076	4
219		15	max	0	1	.007	2	0	9	2.829e-3	4	NC	1	NC	1
220			min	0	3	-.005	3	-.004	4	-2.313e-4	3	NC	1	4998.676	4
221		16	max	0	1	.005	2	0	9	2.829e-3	4	NC	1	NC	1
222			min	0	3	-.004	3	-.002	4	-2.313e-4	3	NC	1	8581.546	4
223		17	max	0	1	.003	2	0	9	2.829e-3	4	NC	1	NC	1
224			min	0	3	-.003	3	-.001	4	-2.313e-4	3	NC	1	NC	1
225		18	max	0	1	.002	2	0	9	2.829e-3	4	NC	1	NC	1
226			min	0	3	-.001	3	0	4	-2.313e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	2.829e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-2.313e-4	3	NC	1	NC	1
229	M10	1	max	.002	1	.008	2	0	3	3.139e-4	1	NC	3	NC	1
230			min	-.003	3	-.008	3	-.004	4	-4.953e-4	3	4530.212	2	NC	1
231		2	max	.002	1	.007	2	0	3	2.985e-4	1	NC	3	NC	1
232			min	-.003	3	-.007	3	-.005	4	-4.793e-4	3	4935.224	2	NC	1
233		3	max	.002	1	.007	2	0	3	2.83e-4	1	NC	3	NC	1
234			min	-.002	3	-.007	3	-.005	4	-4.633e-4	3	5415.372	2	NC	1
235		4	max	.002	1	.006	2	0	3	3.312e-4	4	NC	1	NC	1
236			min	-.002	3	-.007	3	-.005	4	-4.473e-4	3	5988.605	2	NC	1
237		5	max	.002	1	.005	2	0	3	3.808e-4	4	NC	1	NC	1
238			min	-.002	3	-.007	3	-.005	4	-4.313e-4	3	6678.798	2	NC	1
239		6	max	.001	1	.005	2	0	3	4.304e-4	4	NC	1	NC	1
240			min	-.002	3	-.006	3	-.005	4	-4.153e-4	3	7518.231	2	NC	1
241		7	max	.001	1	.004	2	0	3	4.8e-4	4	NC	1	NC	1
242			min	-.002	3	-.006	3	-.005	4	-3.993e-4	3	8551.39	2	NC	1
243		8	max	.001	1	.004	2	0	3	5.296e-4	4	NC	1	NC	1
244			min	-.002	3	-.006	3	-.005	4	-3.833e-4	3	9840.963	2	NC	1
245		9	max	.001	1	.003	2	0	3	5.792e-4	4	NC	1	NC	1
246			min	-.002	3	-.005	3	-.004	4	-3.673e-4	3	NC	1	NC	1
247		10	max	.001	1	.003	2	0	3	6.288e-4	4	NC	1	NC	1
248			min	-.001	3	-.005	3	-.004	4	-3.513e-4	3	NC	1	NC	1
249		11	max	0	1	.002	2	0	3	6.784e-4	4	NC	1	NC	1
250			min	-.001	3	-.004	3	-.004	4	-3.353e-4	3	NC	1	NC	1
251		12	max	0	1	.002	2	0	3	7.28e-4	4	NC	1	NC	1
252			min	-.001	3	-.004	3	-.004	4	-3.193e-4	3	NC	1	NC	1
253		13	max	0	1	.001	2	0	3	7.776e-4	4	NC	1	NC	1
254			min	0	3	-.003	3	-.003	4	-3.033e-4	3	NC	1	NC	1
255		14	max	0	1	.001	2	0	3	8.272e-4	4	NC	1	NC	1
256			min	0	3	-.003	3	-.003	4	-2.873e-4	3	NC	1	NC	1
257		15	max	0	1	0	2	0	3	8.768e-4	4	NC	1	NC	1
258			min	0	3	-.002	3	-.002	4	-2.713e-4	3	NC	1	NC	1
259		16	max	0	1	0	2	0	3	9.264e-4	4	NC	1	NC	1
260			min	0	3	-.002	3	-.002	4	-2.553e-4	3	NC	1	NC	1
261		17	max	0	1	0	2	0	3	9.76e-4	4	NC	1	NC	1
262			min	0	3	-.001	3	-.001	4	-2.393e-4	3	NC	1	NC	1
263		18	max	0	1	0	2	0	3	1.026e-3	4	NC	1	NC	1
264			min	0	3	0	3	0	4	-2.233e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.075e-3	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-2.073e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	9.662e-5	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-5.006e-4	4	NC	1	NC	1
269		2	max	0	3	0	2	.003	4	7.467e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-5.466e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	3	0	2	.005	4	5.272e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-5.926e-4	4	NC	1	NC	1
273		4	max	0	3	0	2	.008	4	3.077e-5	3	NC	1	NC	1
274			min	0	2	-.002	3	-.001	3	-6.387e-4	4	NC	1	NC	1
275		5	max	0	3	0	2	.011	4	8.819e-6	3	NC	1	NC	1
276			min	0	2	-.003	3	-.002	3	-6.847e-4	4	NC	1	NC	1
277		6	max	0	3	0	2	.013	4	-7.827e-7	10	NC	1	NC	1
278			min	0	2	-.004	3	-.002	3	-7.307e-4	4	NC	1	NC	1
279		7	max	0	3	0	2	.016	5	-8.912e-7	10	NC	1	NC	1
280			min	0	2	-.005	3	-.002	3	-7.768e-4	4	NC	1	NC	1
281		8	max	0	3	0	2	.019	5	-9.998e-7	10	NC	1	NC	1
282			min	0	2	-.005	3	-.002	3	-8.228e-4	4	NC	1	NC	1
283		9	max	0	3	.001	2	.021	5	-1.108e-6	10	NC	1	NC	1
284			min	0	2	-.006	3	-.003	3	-8.688e-4	4	NC	1	NC	1
285		10	max	0	3	.002	2	.024	5	-1.217e-6	10	NC	1	NC	1
286			min	0	2	-.006	3	-.003	3	-9.148e-4	4	NC	1	NC	1
287		11	max	0	3	.002	2	.026	5	-1.325e-6	10	NC	1	NC	1
288			min	0	2	-.007	3	-.003	3	-9.609e-4	4	NC	1	NC	1
289		12	max	0	3	.003	2	.029	5	-1.434e-6	10	NC	1	NC	1
290			min	0	2	-.007	3	-.003	3	-1.007e-3	4	NC	1	NC	1
291		13	max	.001	3	.003	2	.031	5	-1.542e-6	10	NC	1	NC	1
292			min	-.001	2	-.007	3	-.003	3	-1.053e-3	4	NC	1	NC	1
293		14	max	.001	3	.004	2	.034	5	-1.651e-6	10	NC	1	NC	1
294			min	-.001	2	-.008	3	-.003	3	-1.099e-3	4	NC	1	NC	1
295		15	max	.001	3	.005	2	.036	5	-1.76e-6	10	NC	1	NC	1
296			min	-.001	2	-.008	3	-.003	3	-1.145e-3	4	9688.504	2	NC	1
297		16	max	.001	3	.006	2	.038	5	-1.868e-6	10	NC	1	NC	1
298			min	-.001	2	-.008	3	-.003	1	-1.191e-3	4	8167.362	2	NC	1
299		17	max	.001	3	.007	2	.041	5	-1.977e-6	10	NC	1	NC	1
300			min	-.001	2	-.008	3	-.003	1	-1.237e-3	4	6998.799	2	NC	1
301		18	max	.001	3	.008	2	.043	5	-2.085e-6	10	NC	3	NC	1
302			min	-.001	2	-.008	3	-.003	1	-1.283e-3	4	6090.098	2	NC	1
303		19	max	.002	3	.009	2	.046	5	-2.194e-6	10	NC	3	NC	1
304			min	-.002	2	-.008	3	-.003	1	-1.329e-3	4	5376.688	2	NC	1
305	M12	1	max	.001	1	.009	2	.003	1	3.538e-3	4	NC	1	NC	2
306			min	0	3	-.008	3	-.05	5	1.977e-6	10	NC	1	387.613	5
307		2	max	.001	1	.009	2	.003	1	3.538e-3	4	NC	1	NC	2
308			min	0	3	-.007	3	-.046	5	1.977e-6	10	NC	1	422.499	5
309		3	max	.001	1	.008	2	.002	1	3.538e-3	4	NC	1	NC	2
310			min	0	3	-.007	3	-.042	5	1.977e-6	10	NC	1	464.015	5
311		4	max	.001	1	.008	2	.002	1	3.538e-3	4	NC	1	NC	2
312			min	0	3	-.007	3	-.038	5	1.977e-6	10	NC	1	513.906	5
313		5	max	.001	1	.007	2	.002	1	3.538e-3	4	NC	1	NC	2
314			min	0	3	-.006	3	-.034	5	1.977e-6	10	NC	1	574.551	5
315		6	max	.001	1	.007	2	.002	1	3.538e-3	4	NC	1	NC	1
316			min	0	3	-.006	3	-.03	5	1.977e-6	10	NC	1	649.256	5
317		7	max	0	1	.006	2	.002	1	3.538e-3	4	NC	1	NC	1
318			min	0	3	-.005	3	-.026	5	1.977e-6	10	NC	1	742.733	5
319		8	max	0	1	.006	2	.001	1	3.538e-3	4	NC	1	NC	1
320			min	0	3	-.005	3	-.022	5	1.977e-6	10	NC	1	861.876	5
321		9	max	0	1	.005	2	.001	1	3.538e-3	4	NC	1	NC	1
322			min	0	3	-.004	3	-.019	5	1.977e-6	10	NC	1	1017.115	5
323		10	max	0	1	.005	2	0	1	3.538e-3	4	NC	1	NC	1
324			min	0	3	-.004	3	-.016	5	1.977e-6	10	NC	1	1224.845	5
325		11	max	0	1	.004	2	0	1	3.538e-3	4	NC	1	NC	1
326			min	0	3	-.003	3	-.013	5	1.977e-6	10	NC	1	1512.064	5
327		12	max	0	1	.004	2	0	1	3.538e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	3	-.003	3	-.01	5	1.977e-6	10	NC	1	1925.864	5
329		13	max	0	1	.003	2	0	1	3.538e-3	4	NC	1	NC	1
330			min	0	3	-.003	3	-.008	5	1.977e-6	10	NC	1	2554.57	5
331		14	max	0	1	.003	2	0	1	3.538e-3	4	NC	1	NC	1
332			min	0	3	-.002	3	-.005	5	1.977e-6	10	NC	1	3580.362	5
333		15	max	0	1	.002	2	0	1	3.538e-3	4	NC	1	NC	1
334			min	0	3	-.002	3	-.004	5	1.977e-6	10	NC	1	5431.212	5
335		16	max	0	1	.002	2	0	1	3.538e-3	4	NC	1	NC	1
336			min	0	3	-.001	3	-.002	5	1.977e-6	10	NC	1	9323.672	5
337		17	max	0	1	.001	2	0	1	3.538e-3	4	NC	1	NC	1
338			min	0	3	0	3	0	5	1.977e-6	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	3.538e-3	4	NC	1	NC	1
340			min	0	3	0	3	0	5	1.977e-6	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	3.538e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	1.977e-6	10	NC	1	NC	1
343	M1	1	max	.007	3	.023	3	.006	5	6.681e-3	2	NC	1	NC	1
344			min	-.008	2	-.02	2	-.001	9	-9.542e-3	3	NC	1	NC	1
345		2	max	.007	3	.013	3	.008	5	3.293e-3	2	NC	4	NC	1
346			min	-.008	2	-.011	2	-.002	1	-4.699e-3	3	4835.977	3	NC	1
347		3	max	.007	3	.004	3	.01	5	2.728e-4	5	NC	4	NC	1
348			min	-.008	2	-.003	2	-.003	1	-1.625e-4	1	2508.32	3	NC	1
349		4	max	.007	3	.004	2	.012	5	2.717e-4	5	NC	4	NC	1
350			min	-.008	2	-.004	3	-.004	1	-1.352e-4	1	1792.041	3	6888.377	5
351		5	max	.007	3	.011	2	.015	5	2.705e-4	5	NC	4	NC	1
352			min	-.008	2	-.01	3	-.004	1	-1.079e-4	1	1451.421	3	4900.972	5
353		6	max	.007	3	.016	2	.018	5	2.694e-4	5	NC	4	NC	1
354			min	-.008	2	-.015	3	-.004	1	-8.061e-5	1	1258.068	2	3748.425	5
355		7	max	.007	3	.02	2	.021	5	2.683e-4	5	NC	4	NC	1
356			min	-.008	2	-.019	3	-.003	1	-5.331e-5	1	1121.846	2	3006.543	5
357		8	max	.007	3	.023	2	.024	5	2.672e-4	5	NC	4	NC	1
358			min	-.008	2	-.022	3	-.003	1	-3.007e-5	9	1036.56	2	2495.164	5
359		9	max	.007	3	.025	2	.028	5	2.661e-4	5	NC	4	NC	1
360			min	-.008	2	-.023	3	-.002	1	-1.023e-5	9	986.194	2	2125.198	5
361		10	max	.007	3	.026	2	.031	5	2.705e-4	4	NC	4	NC	1
362			min	-.008	2	-.023	3	0	9	1.023e-6	10	963.121	2	1831.303	4
363		11	max	.007	3	.026	2	.034	4	2.759e-4	4	NC	4	NC	1
364			min	-.008	2	-.023	3	0	9	1.212e-6	10	964.607	2	1608.084	4
365		12	max	.007	3	.024	2	.038	4	2.812e-4	4	NC	4	NC	1
366			min	-.008	2	-.021	3	0	10	1.401e-6	10	991.796	2	1435.067	4
367		13	max	.007	3	.021	2	.041	4	2.866e-4	4	NC	4	NC	1
368			min	-.008	2	-.018	3	0	10	1.591e-6	10	1050.315	2	1298.73	4
369		14	max	.007	3	.017	2	.045	4	2.92e-4	4	NC	4	NC	1
370			min	-.008	2	-.014	3	0	10	1.78e-6	10	1153.119	2	1190.004	4
371		15	max	.007	3	.011	2	.048	4	2.974e-4	4	NC	4	NC	1
372			min	-.008	2	-.009	3	0	10	1.97e-6	10	1328.608	2	1102.631	4
373		16	max	.007	3	.004	2	.051	4	4.795e-4	4	NC	4	NC	1
374			min	-.008	2	-.003	3	0	10	2.117e-6	10	1646.138	2	1032.191	4
375		17	max	.007	3	.003	3	.053	4	4.869e-3	4	NC	4	NC	1
376			min	-.008	2	-.005	2	0	10	1.265e-6	10	2326.663	2	975.573	4
377		18	max	.007	3	.011	3	.056	4	4.622e-3	2	NC	4	NC	1
378			min	-.008	2	-.015	2	0	10	-2.299e-3	3	4505.275	2	930.329	4
379		19	max	.007	3	.018	3	.058	4	9.313e-3	2	NC	1	NC	1
380			min	-.008	2	-.026	2	0	1	-4.698e-3	3	NC	1	895.784	4
381	M5	1	max	.022	3	.074	3	.005	5	1.329e-5	4	NC	1	NC	1
382			min	-.025	2	-.064	2	-.001	9	0	11	NC	1	NC	1
383		2	max	.022	3	.042	3	.007	5	1.354e-4	5	NC	4	NC	1
384			min	-.025	2	-.036	2	-.001	9	-1.975e-5	9	1529.063	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.022	3	.013	3	.01	5	2.555e-4	5	NC	5	NC	1
386			min	-.025	2	-.009	2	-.001	9	-3.921e-5	9	793.46	3	NC	1
387		4	max	.022	3	.014	2	.012	5	2.648e-4	5	NC	5	NC	1
388			min	-.025	2	-.012	3	-.001	9	-3.728e-5	9	567.516	3	NC	1
389		5	max	.022	3	.034	2	.015	5	2.742e-4	5	NC	5	NC	1
390			min	-.025	2	-.032	3	0	9	-3.535e-5	9	460.161	2	NC	1
391		6	max	.022	3	.051	2	.019	5	2.835e-4	5	NC	5	NC	1
392			min	-.025	2	-.048	3	0	9	-3.342e-5	9	391.198	2	9718.469	3
393		7	max	.021	3	.064	2	.022	5	2.928e-4	5	NC	5	NC	1
394			min	-.025	2	-.06	3	0	9	-3.149e-5	9	348.697	2	9231.653	3
395		8	max	.021	3	.075	2	.026	5	3.022e-4	5	NC	5	NC	1
396			min	-.025	2	-.068	3	0	9	-2.957e-5	9	322.076	2	9121.321	3
397		9	max	.021	3	.081	2	.029	5	3.115e-4	5	NC	5	NC	1
398			min	-.025	2	-.073	3	0	9	-2.764e-5	9	306.337	2	9315.619	3
399		10	max	.021	3	.084	2	.033	5	3.209e-4	5	NC	5	NC	1
400			min	-.025	2	-.074	3	0	9	-2.571e-5	9	299.1	2	9805.662	3
401		11	max	.021	3	.082	2	.036	5	3.302e-4	5	NC	5	NC	1
402			min	-.025	2	-.071	3	0	9	-2.378e-5	9	299.509	2	NC	1
403		12	max	.021	3	.077	2	.04	4	3.396e-4	5	NC	5	NC	1
404			min	-.025	2	-.065	3	0	9	-2.185e-5	9	307.917	2	NC	1
405		13	max	.021	3	.067	2	.043	4	3.489e-4	5	NC	5	NC	1
406			min	-.025	2	-.056	3	0	9	-1.992e-5	9	326.07	2	NC	1
407		14	max	.021	3	.054	2	.046	4	3.582e-4	5	NC	5	NC	1
408			min	-.025	2	-.044	3	0	9	-1.799e-5	9	357.995	2	NC	1
409		15	max	.021	3	.035	2	.049	4	3.676e-4	5	NC	5	NC	1
410			min	-.025	2	-.029	3	0	9	-1.606e-5	9	412.527	2	NC	1
411		16	max	.021	3	.012	2	.052	4	5.511e-4	4	NC	5	NC	1
412			min	-.025	2	-.011	3	0	9	-1.533e-5	9	511.255	2	NC	1
413		17	max	.021	3	.01	3	.054	4	4.882e-3	4	NC	5	NC	1
414			min	-.025	2	-.016	2	0	9	-4.331e-5	9	723.136	2	NC	1
415		18	max	.021	3	.033	3	.056	4	2.506e-3	4	NC	4	NC	1
416			min	-.025	2	-.048	2	0	9	-2.214e-5	9	1400.849	2	NC	1
417		19	max	.021	3	.057	3	.058	4	4.755e-6	5	NC	1	NC	1
418			min	-.025	2	-.083	2	0	9	-8.688e-7	3	NC	1	NC	1
419	M9	1	max	.007	3	.023	3	.005	5	9.553e-3	3	NC	1	NC	1
420			min	-.008	2	-.02	2	-.001	9	-6.681e-3	2	NC	1	NC	1
421		2	max	.007	3	.013	3	.004	5	4.719e-3	3	NC	4	NC	1
422			min	-.008	2	-.011	2	0	9	-3.293e-3	2	4838.109	3	NC	1
423		3	max	.007	3	.004	3	.004	4	8.18e-5	1	NC	4	NC	1
424			min	-.008	2	-.003	2	0	3	-3.489e-5	5	2509.448	3	NC	1
425		4	max	.007	3	.004	2	.005	4	5.797e-5	1	NC	4	NC	1
426			min	-.008	2	-.004	3	-.001	3	-3.538e-5	5	1792.831	3	NC	1
427		5	max	.007	3	.011	2	.007	4	3.415e-5	1	NC	4	NC	1
428			min	-.008	2	-.01	3	-.002	3	-4.05e-5	3	1452.019	3	NC	1
429		6	max	.007	3	.016	2	.009	4	1.208e-5	2	NC	4	NC	1
430			min	-.008	2	-.016	3	-.003	3	-4.806e-5	3	1258.363	2	9049.828	3
431		7	max	.007	3	.02	2	.011	4	5.359e-6	2	NC	4	NC	1
432			min	-.008	2	-.019	3	-.004	3	-5.561e-5	3	1122.121	2	7083.163	4
433		8	max	.007	3	.023	2	.014	4	-5.093e-7	10	NC	4	NC	1
434			min	-.008	2	-.022	3	-.004	3	-6.317e-5	3	1036.825	2	4957.437	4
435		9	max	.007	3	.025	2	.017	4	-7.064e-7	10	NC	4	NC	1
436			min	-.008	2	-.023	3	-.004	3	-7.072e-5	3	986.455	2	3703.726	4
437		10	max	.007	3	.026	2	.021	5	-9.036e-7	10	NC	4	NC	1
438			min	-.008	2	-.024	3	-.005	3	-8.5e-5	1	963.384	2	2899.701	4
439		11	max	.007	3	.026	2	.025	5	-1.101e-6	10	NC	4	NC	1
440			min	-.008	2	-.023	3	-.004	3	-1.088e-4	1	964.879	2	2352.01	4
441		12	max	.007	3	.024	2	.029	5	-1.298e-6	10	NC	4	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.008	2	-.021	3	-.004	3	-1.327e-4	1	992.083	2	1959.056	5
443		13	max	.007	3	.021	2	.033	5	-1.495e-6	10	NC	4	NC	1
444			min	-.008	2	-.018	3	-.004	3	-1.565e-4	1	1050.625	2	1664.521	5
445		14	max	.007	3	.017	2	.037	5	-1.692e-6	10	NC	4	NC	1
446			min	-.008	2	-.014	3	-.003	3	-1.803e-4	1	1153.465	2	1444.514	5
447		15	max	.007	3	.011	2	.042	5	-1.89e-6	10	NC	4	NC	1
448			min	-.008	2	-.009	3	-.004	1	-2.041e-4	1	1329.01	2	1276.211	5
449		16	max	.007	3	.004	2	.046	5	1.481e-4	5	NC	4	NC	1
450			min	-.008	2	-.003	3	-.003	1	-2.225e-4	1	1646.631	2	1145.086	5
451		17	max	.007	3	.003	3	.05	5	4.843e-3	4	NC	4	NC	1
452			min	-.008	2	-.005	2	-.003	1	-1.104e-4	1	2327.31	2	1041.406	5
453		18	max	.007	3	.011	3	.054	5	2.378e-3	5	NC	4	NC	1
454			min	-.008	2	-.015	2	-.002	1	-4.622e-3	2	4506.486	2	954.16	4
455		19	max	.007	3	.018	3	.058	4	4.696e-3	3	NC	1	NC	1
456			min	-.008	2	-.026	2	0	9	-9.313e-3	2	NC	1	882.688	4
457	M13	1	max	.001	9	.023	3	.007	3	3.76e-3	3	NC	1	NC	1
458			min	-.005	5	-.02	2	-.008	2	-3.302e-3	2	NC	1	NC	1
459		2	max	.001	9	.075	3	.005	3	4.67e-3	3	NC	4	NC	1
460			min	-.005	5	-.056	2	-.006	2	-4.112e-3	2	1949.082	3	NC	1
461		3	max	.001	9	.119	3	.009	9	5.58e-3	3	NC	5	NC	2
462			min	-.005	5	-.087	2	-.005	2	-4.922e-3	2	1061.336	3	7912.701	1
463		4	max	.001	9	.148	3	.014	1	6.49e-3	3	NC	5	NC	2
464			min	-.005	5	-.109	2	-.005	10	-5.732e-3	2	812.757	3	5670.633	1
465		5	max	.001	9	.161	3	.015	1	7.4e-3	3	NC	5	NC	2
466			min	-.005	5	-.118	2	-.007	10	-6.542e-3	2	740.836	3	5273.049	1
467		6	max	.001	9	.156	3	.014	9	8.31e-3	3	NC	5	NC	2
468			min	-.005	5	-.116	2	-.009	2	-7.352e-3	2	767.99	3	6260.694	1
469		7	max	.001	9	.137	3	.014	3	9.22e-3	3	NC	5	NC	1
470			min	-.005	5	-.105	2	-.014	2	-8.162e-3	2	894.402	3	NC	1
471		8	max	.001	9	.111	3	.016	3	1.013e-2	3	NC	4	NC	1
472			min	-.005	5	-.088	2	-.019	2	-8.972e-3	2	1165.646	3	9149.272	2
473		9	max	.001	9	.085	3	.019	3	1.104e-2	3	NC	4	NC	1
474			min	-.005	5	-.071	2	-.023	2	-9.782e-3	2	1636.5	3	6552.551	2
475		10	max	.001	9	.074	3	.022	3	1.195e-2	3	NC	4	NC	4
476			min	-.005	5	-.064	2	-.025	2	-1.059e-2	2	2014.703	3	5824.413	2
477		11	max	.001	9	.086	3	.023	3	1.104e-2	3	NC	4	NC	1
478			min	-.005	5	-.071	2	-.023	2	-9.782e-3	2	1636.498	3	6280.576	3
479		12	max	.001	9	.111	3	.024	3	1.013e-2	3	NC	4	NC	1
480			min	-.005	5	-.088	2	-.019	2	-8.972e-3	2	1165.645	3	6107.53	3
481		13	max	.001	9	.137	3	.023	3	9.225e-3	3	NC	5	NC	1
482			min	-.005	5	-.105	2	-.014	2	-8.162e-3	2	894.401	3	6398.315	3
483		14	max	.001	9	.156	3	.021	3	8.317e-3	3	NC	5	NC	2
484			min	-.005	5	-.116	2	-.009	2	-7.352e-3	2	767.99	3	6255.933	1
485		15	max	.001	9	.161	3	.019	3	7.408e-3	3	NC	5	NC	2
486			min	-.005	5	-.118	2	-.007	10	-6.542e-3	2	740.836	3	5277.448	1
487		16	max	.001	9	.149	3	.016	3	6.5e-3	3	NC	5	NC	2
488			min	-.005	5	-.109	2	-.005	10	-5.732e-3	2	812.756	3	5683.328	1
489		17	max	.001	9	.119	3	.012	3	5.592e-3	3	NC	5	NC	2
490			min	-.005	5	-.087	2	-.005	2	-4.922e-3	2	1061.335	3	7944.266	1
491		18	max	.001	9	.076	3	.009	3	4.684e-3	3	NC	4	NC	1
492			min	-.006	5	-.056	2	-.006	2	-4.112e-3	2	1949.081	3	NC	1
493		19	max	.001	9	.023	3	.007	3	3.775e-3	3	NC	1	NC	1
494			min	-.006	5	-.02	2	-.008	2	-3.303e-3	2	NC	1	NC	1
495	M16	1	max	0	9	.018	3	.007	3	4.063e-3	2	NC	1	NC	1
496			min	-.058	4	-.026	2	-.008	2	-2.917e-3	3	NC	1	NC	1
497		2	max	0	9	.044	3	.01	3	5.065e-3	2	NC	4	NC	1
498			min	-.058	4	-.077	2	-.006	2	-3.597e-3	3	1996.432	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	0	9	.066	3	.012	3	6.066e-3	2	NC	5	NC	2
500			min	-.058	4	-.12	2	-.005	2	-4.276e-3	3	1084.747	2	7947.561	1
501		4	max	0	9	.082	3	.015	3	7.068e-3	2	NC	5	NC	2
502			min	-.058	4	-.149	2	-.005	10	-4.956e-3	3	827.48	2	5697.196	1
503		5	max	0	9	.089	3	.018	3	8.069e-3	2	NC	5	NC	2
504			min	-.058	4	-.162	2	-.007	10	-5.635e-3	3	749.586	2	5303.132	1
505		6	max	0	9	.089	3	.02	3	9.07e-3	2	NC	5	NC	2
506			min	-.058	4	-.158	2	-.009	2	-6.314e-3	3	769.39	2	6312.416	1
507		7	max	0	9	.082	3	.021	3	1.007e-2	2	NC	5	NC	1
508			min	-.058	4	-.141	2	-.014	2	-6.994e-3	3	881.543	2	7079.823	3
509		8	max	0	9	.072	3	.022	3	1.107e-2	2	NC	4	NC	1
510			min	-.058	4	-.117	2	-.019	2	-7.673e-3	3	1117.715	2	6766.841	3
511		9	max	0	9	.062	3	.022	3	1.207e-2	2	NC	4	NC	1
512			min	-.058	4	-.093	2	-.023	2	-8.353e-3	3	1503.479	2	6549.596	2
513		10	max	0	9	.057	3	.021	3	1.308e-2	2	NC	4	NC	4
514			min	-.058	4	-.083	2	-.025	2	-9.032e-3	3	1792.27	2	5822.328	2
515		11	max	0	9	.062	3	.02	3	1.207e-2	2	NC	4	NC	1
516			min	-.058	4	-.093	2	-.023	2	-8.351e-3	3	1503.479	2	6549.608	2
517		12	max	0	9	.072	3	.019	3	1.107e-2	2	NC	4	NC	1
518			min	-.058	4	-.117	2	-.019	2	-7.67e-3	3	1117.715	2	8849.946	3
519		13	max	0	9	.082	3	.017	3	1.007e-2	2	NC	5	NC	1
520			min	-.058	4	-.141	2	-.014	2	-6.989e-3	3	881.543	2	NC	1
521		14	max	0	9	.089	3	.015	3	9.071e-3	2	NC	5	NC	2
522			min	-.058	4	-.158	2	-.009	2	-6.308e-3	3	769.39	2	6320.59	1
523		15	max	0	9	.089	3	.015	1	8.07e-3	2	NC	5	NC	2
524			min	-.058	4	-.162	2	-.007	10	-5.627e-3	3	749.586	2	5317.077	1
525		16	max	0	1	.082	3	.013	1	7.069e-3	2	NC	5	NC	2
526			min	-.058	4	-.149	2	-.005	10	-4.946e-3	3	827.48	2	5720.199	1
527		17	max	0	1	.066	3	.01	3	6.067e-3	2	NC	5	NC	2
528			min	-.058	4	-.12	2	-.005	2	-4.265e-3	3	1084.747	2	7995.33	1
529		18	max	0	1	.044	3	.008	3	5.066e-3	2	NC	4	NC	1
530			min	-.058	4	-.077	2	-.006	2	-3.584e-3	3	1996.432	2	NC	1
531		19	max	0	1	.018	3	.007	3	4.065e-3	2	NC	1	NC	1
532			min	-.058	4	-.026	2	-.008	2	-2.903e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	3.793e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-5.562e-4	5	NC	1	NC	1
535		2	max	0	3	0	5	.004	4	8.102e-4	3	NC	1	NC	1
536			min	0	4	-.002	1	0	3	-5.694e-4	5	NC	1	NC	1
537		3	max	0	3	.001	5	.009	4	1.241e-3	3	NC	1	NC	1
538			min	0	4	-.004	1	-.003	3	-9.039e-4	2	NC	1	7159.401	4
539		4	max	0	3	.002	5	.014	4	1.672e-3	3	NC	3	NC	9
540			min	-.001	4	-.007	1	-.007	3	-1.33e-3	2	9373.639	2	4630.809	4
541		5	max	0	3	.002	5	.018	4	2.103e-3	3	NC	4	NC	9
542			min	-.002	4	-.008	1	-.011	3	-1.756e-3	2	7314.345	2	3477.988	4
543		6	max	0	3	.002	5	.022	4	2.534e-3	3	NC	5	9283.262	9
544			min	-.002	4	-.01	1	-.016	3	-2.182e-3	2	6155.795	2	2705.251	3
545		7	max	0	3	.003	5	.025	4	2.964e-3	3	NC	5	7315.936	9
546			min	-.003	4	-.011	1	-.021	3	-2.607e-3	2	5459.079	2	2115.56	3
547		8	max	0	3	.003	5	.027	4	3.395e-3	3	NC	5	6069.708	9
548			min	-.003	4	-.012	1	-.026	3	-3.033e-3	2	5040.945	2	1744.798	3
549		9	max	0	3	.004	5	.028	4	3.826e-3	3	NC	5	5250.238	9
550			min	-.004	4	-.013	1	-.03	3	-3.459e-3	2	4815.881	2	1502.144	3
551		10	max	0	3	.004	5	.027	4	4.257e-3	3	NC	5	4708.416	9
552			min	-.004	4	-.013	1	-.034	3	-3.885e-3	2	4744.681	2	1341.979	3
553		11	max	0	3	.004	5	.029	1	4.688e-3	3	NC	5	4523.961	15
554			min	-.005	4	-.013	1	-.036	3	-4.311e-3	2	4815.881	2	1240.354	3
555		12	max	0	3	.004	5	.03	1	5.119e-3	3	NC	5	5235.71	15

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.005	4	-.012	1	-.037	3	-4.737e-3	2	5040.945	2	1185.386	3
557		13	max	.001	3	.005	5	.029	1	5.55e-3	3	NC	5	6515.449	15
558			min	-.006	4	-.011	1	-.036	3	-5.163e-3	2	5459.079	2	1173.633	3
559		14	max	.001	3	.005	5	.027	1	5.981e-3	3	NC	5	8961.653	15
560			min	-.006	4	-.01	1	-.033	3	-5.589e-3	2	6155.795	2	1210.218	3
561		15	max	.001	3	.005	5	.022	1	6.411e-3	3	NC	4	NC	13
562			min	-.006	4	-.008	9	-.028	3	-6.015e-3	2	7314.345	2	1313.95	3
563		16	max	.001	3	.005	5	.016	1	6.842e-3	3	NC	3	NC	5
564			min	-.007	4	-.007	9	-.019	3	-6.441e-3	2	9373.639	2	1535.894	3
565		17	max	.001	3	.005	5	.007	1	7.273e-3	3	NC	1	NC	4
566			min	-.007	4	-.005	9	-.008	3	-6.866e-3	2	NC	1	2036.26	3
567		18	max	.001	3	.005	5	.007	3	7.704e-3	3	NC	1	NC	4
568			min	-.008	4	-.003	9	-.01	2	-7.292e-3	2	NC	1	3625.504	3
569		19	max	.002	3	.005	5	.026	3	8.135e-3	3	NC	1	NC	1
570			min	-.008	4	-.001	9	-.026	2	-7.718e-3	2	NC	1	NC	1
571	M16A	1	max	0	2	0	2	.008	3	2.35e-3	3	NC	1	NC	1
572			min	-.003	4	-.003	4	-.008	2	-2.355e-3	2	NC	1	NC	1
573		2	max	0	2	-.001	10	.001	3	2.257e-3	3	NC	1	NC	1
574			min	-.003	4	-.007	4	-.003	2	-2.247e-3	2	NC	1	NC	1
575		3	max	0	2	-.003	12	.004	1	2.165e-3	3	NC	1	NC	4
576			min	-.003	4	-.011	4	-.005	5	-2.14e-3	2	7387.166	4	5741.39	3
577		4	max	0	2	-.004	12	.007	1	2.072e-3	3	NC	3	NC	4
578			min	-.002	4	-.015	4	-.008	5	-2.033e-3	2	5068.027	4	4367.818	3
579		5	max	0	2	-.005	12	.009	1	1.979e-3	3	NC	12	NC	9
580			min	-.002	4	-.018	4	-.013	5	-1.926e-3	2	3954.633	4	3773.299	3
581		6	max	0	2	-.005	12	.01	1	1.887e-3	3	NC	12	NC	9
582			min	-.002	4	-.021	4	-.017	5	-1.819e-3	2	3328.242	4	3514.647	3
583		7	max	0	2	-.006	12	.011	1	1.794e-3	3	NC	12	NC	9
584			min	-.002	4	-.023	4	-.021	5	-1.711e-3	2	2951.55	4	3075.848	5
585		8	max	0	2	-.006	12	.011	1	1.701e-3	3	NC	12	NC	9
586			min	-.002	4	-.025	4	-.025	5	-1.604e-3	2	2725.478	4	2610.609	5
587		9	max	0	2	-.007	12	.01	1	1.609e-3	3	9631.762	12	NC	9
588			min	-.002	4	-.026	4	-.028	5	-1.497e-3	2	2603.793	4	2342.749	5
589		10	max	0	2	-.007	12	.009	1	1.516e-3	3	9489.363	12	NC	9
590			min	-.001	4	-.026	4	-.029	5	-1.39e-3	2	2565.298	4	2205.301	5
591		11	max	0	2	-.007	12	.008	1	1.424e-3	3	9631.762	12	NC	9
592			min	-.001	4	-.025	4	-.03	5	-1.283e-3	2	2603.793	4	2169.227	5
593		12	max	0	2	-.006	12	.006	1	1.331e-3	3	NC	12	NC	9
594			min	-.001	4	-.024	4	-.029	5	-1.175e-3	2	2725.478	4	2228.258	5
595		13	max	0	2	-.006	12	.005	1	1.238e-3	3	NC	12	NC	2
596			min	0	4	-.022	4	-.027	5	-1.068e-3	2	2951.55	4	2396.331	5
597		14	max	0	2	-.005	12	.003	1	1.146e-3	3	NC	12	NC	1
598			min	0	4	-.02	4	-.023	5	-9.609e-4	2	3328.242	4	2715.667	5
599		15	max	0	2	-.004	12	.002	1	1.053e-3	3	NC	12	NC	1
600			min	0	4	-.017	4	-.019	5	-8.536e-4	2	3954.633	4	3284.957	5
601		16	max	0	2	-.003	12	.001	9	9.603e-4	3	NC	3	NC	1
602			min	0	4	-.013	4	-.015	5	-7.464e-4	2	5068.027	4	4349.96	5
603		17	max	0	2	-.002	12	0	9	8.677e-4	3	NC	1	NC	1
604			min	0	4	-.009	4	-.01	5	-6.392e-4	2	7387.166	4	6673.302	5
605		18	max	0	2	-.001	12	0	3	8.526e-4	4	NC	1	NC	1
606			min	0	4	-.004	4	-.005	5	-5.32e-4	2	NC	1	NC	1
607		19	max	0	1	0	1	0	1	9.146e-4	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-4.248e-4	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

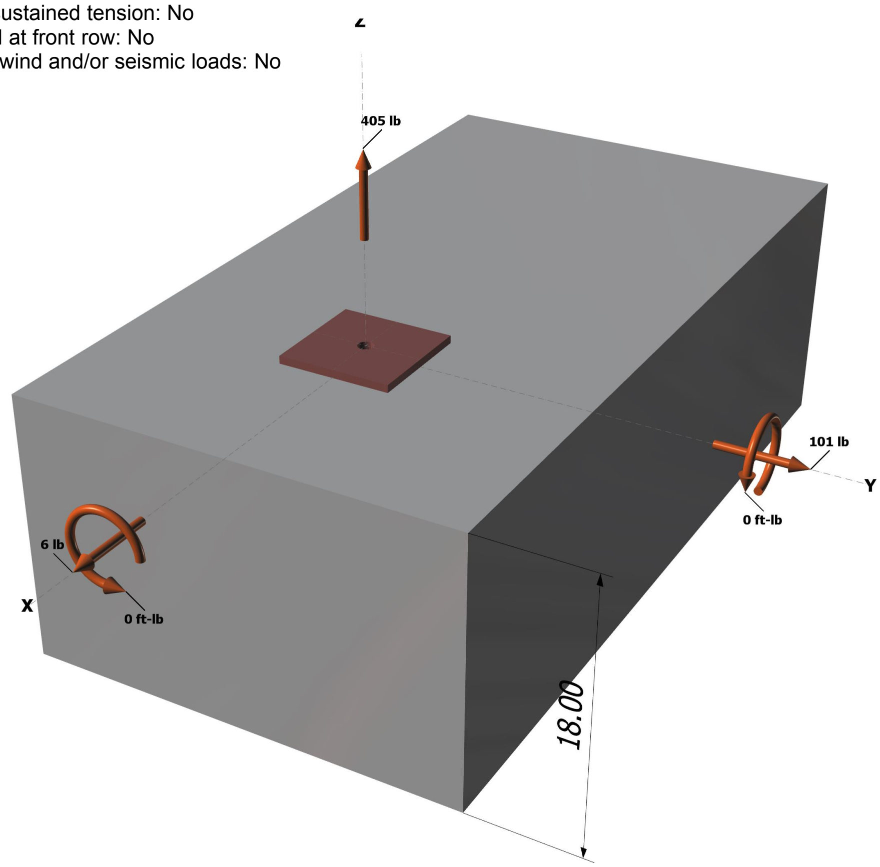
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'$_c$ (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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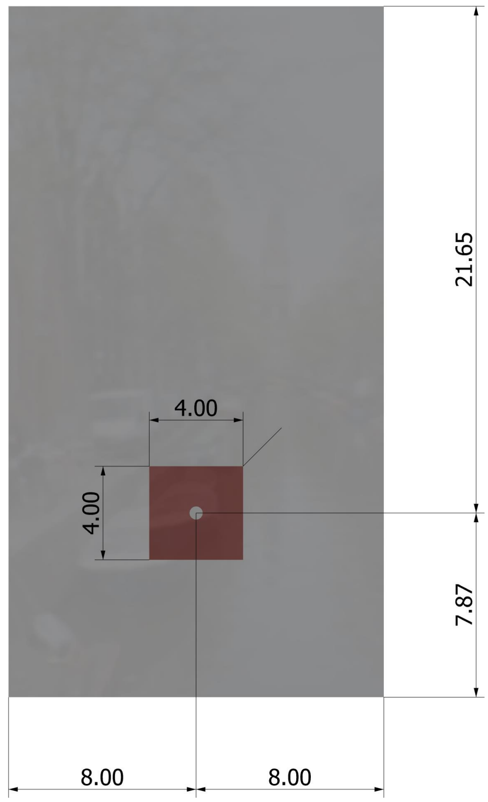


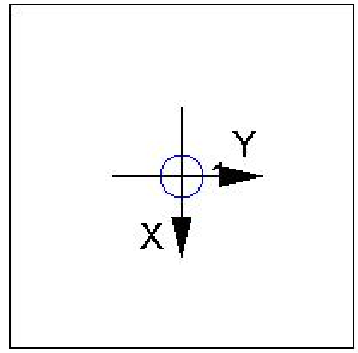
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\,\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\,\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

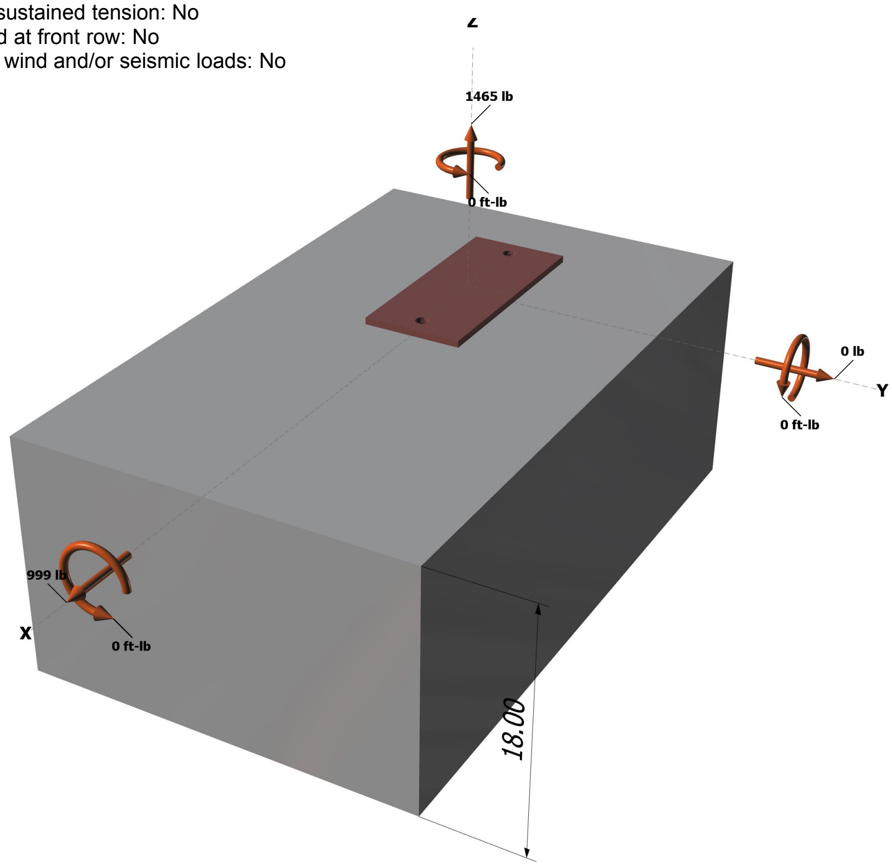
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

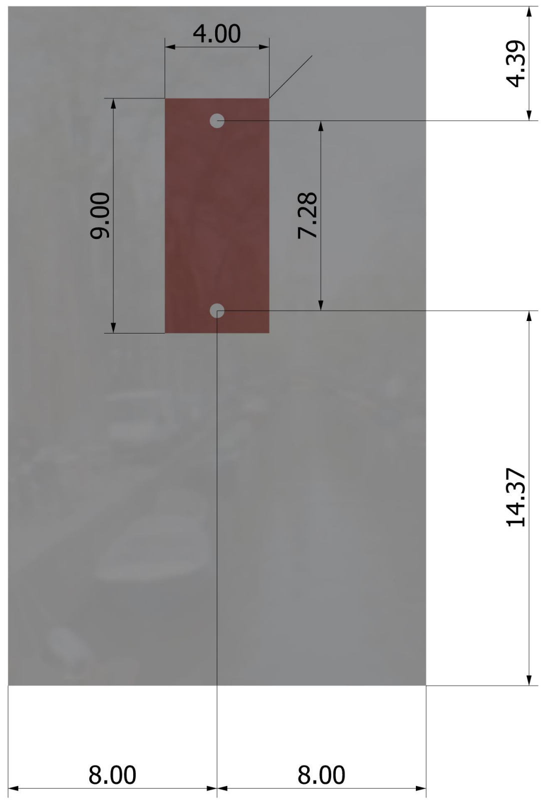
Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>



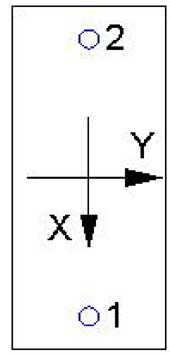
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.