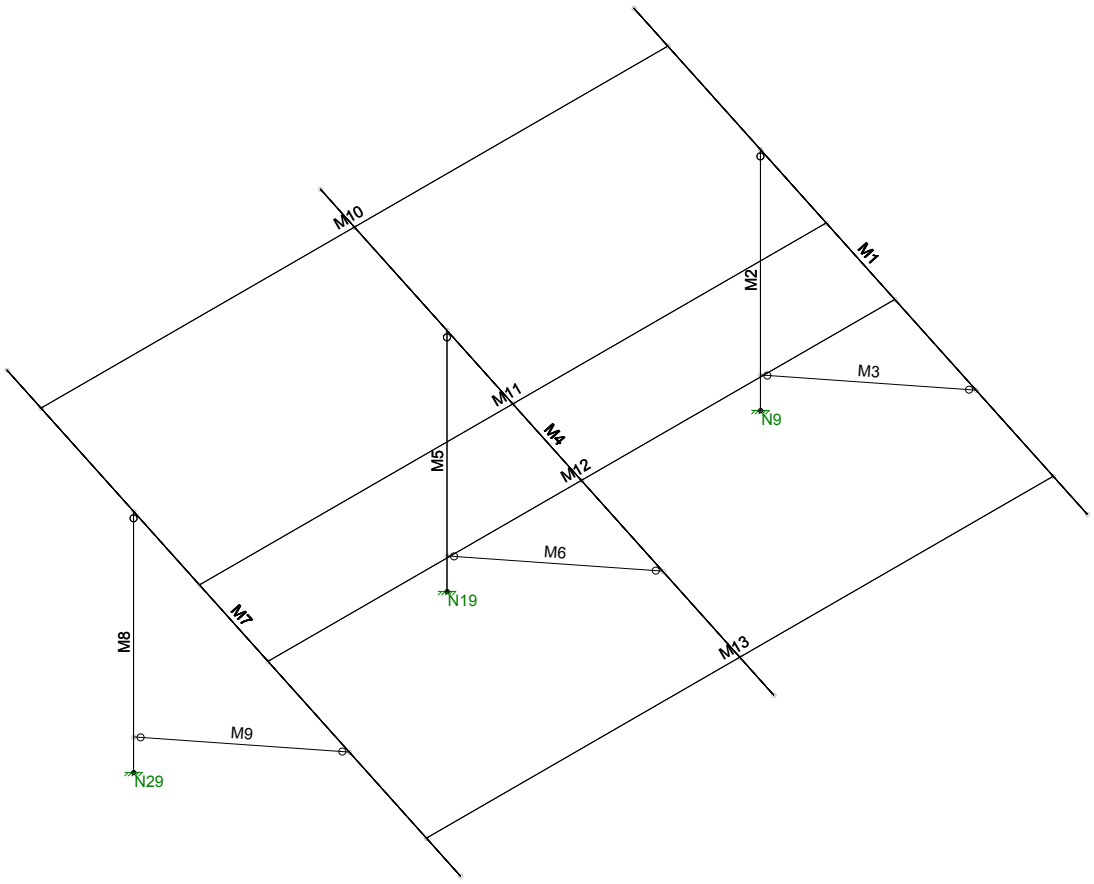


Schletter, Inc.		25° Tilt w/ Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

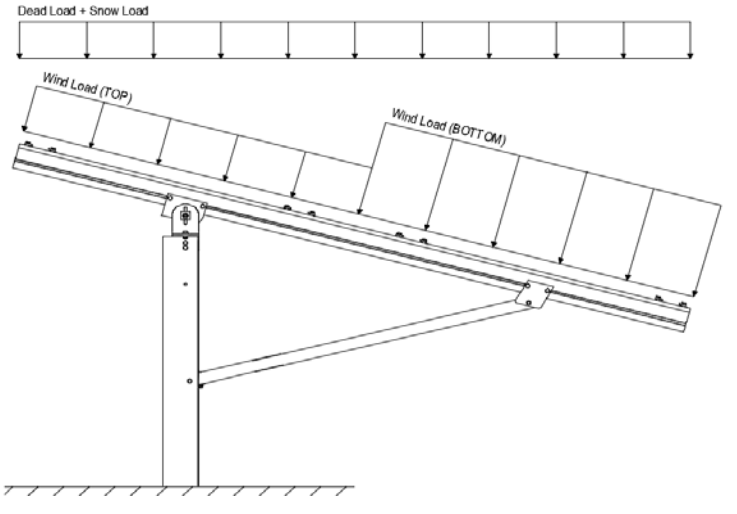
PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row =	2
Module Tilt =	25°
Maximum Height Above Grade =	3 ft

1.3 Technical Codes

- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	18.56	psf	*(ASCE 7-05, Eq. 7-2)*
I_s =	1.00		
C_s =	0.82		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	110	mph	Exposure Category = C
Height <	15	ft	Importance Category = II
Peak Velocity Pressure, q_z =	19.00	psf	*Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.1	*(Pressure)*	*Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.*
$Cf+_{BOTTOM}$ =	1.7		
$Cf-_{TOP}$ =	-2.2	*(Suction)*	
$Cf-_{BOTTOM}$ =	-1		

2.4 Seismic Loads

S_S =	2.50	R =	1.25	*ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.*
S_{DS} =	1.67	C_S =	0.8	
S_1 =	1.00	ρ =	1.3	
S_{D1} =	1.00	Ω =	1.25	
T_a =	0.08	C_d =	1.25	

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W	
1.2D + 1.6W + 0.5S	
0.9D + 1.6W [M]	
1.54D + 1.3E + 0.2S [R]	*(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)*
0.56D + 1.3E [R]	
1.54D + 1.25E + 0.2S [O]	
0.56D + 1.25E [O]	

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S	
1.0D + 1.0W	
1.0D + 0.75L + 0.75W + 0.75S	
0.6D + 1.0W [M]	*(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)*
1.238D + 0.875E [O]	
1.1785D + 0.65625E + 0.75S [O]	
0.362D + 0.875E [O]	

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

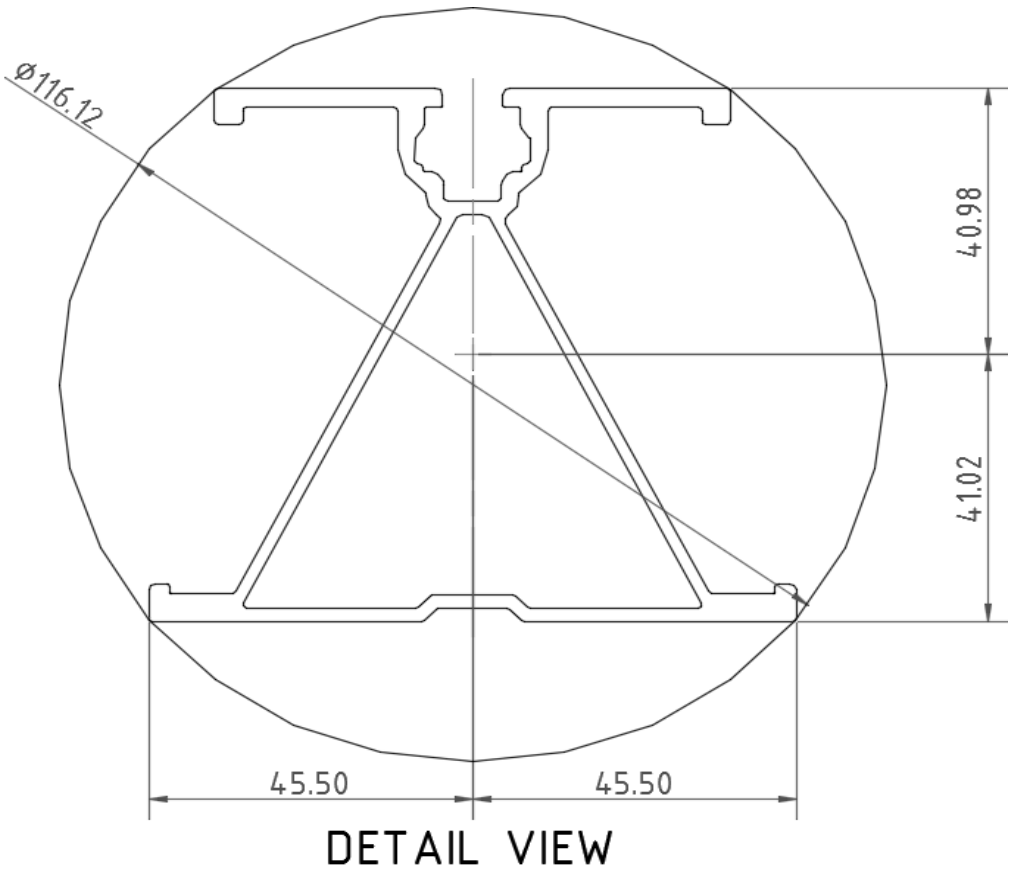
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

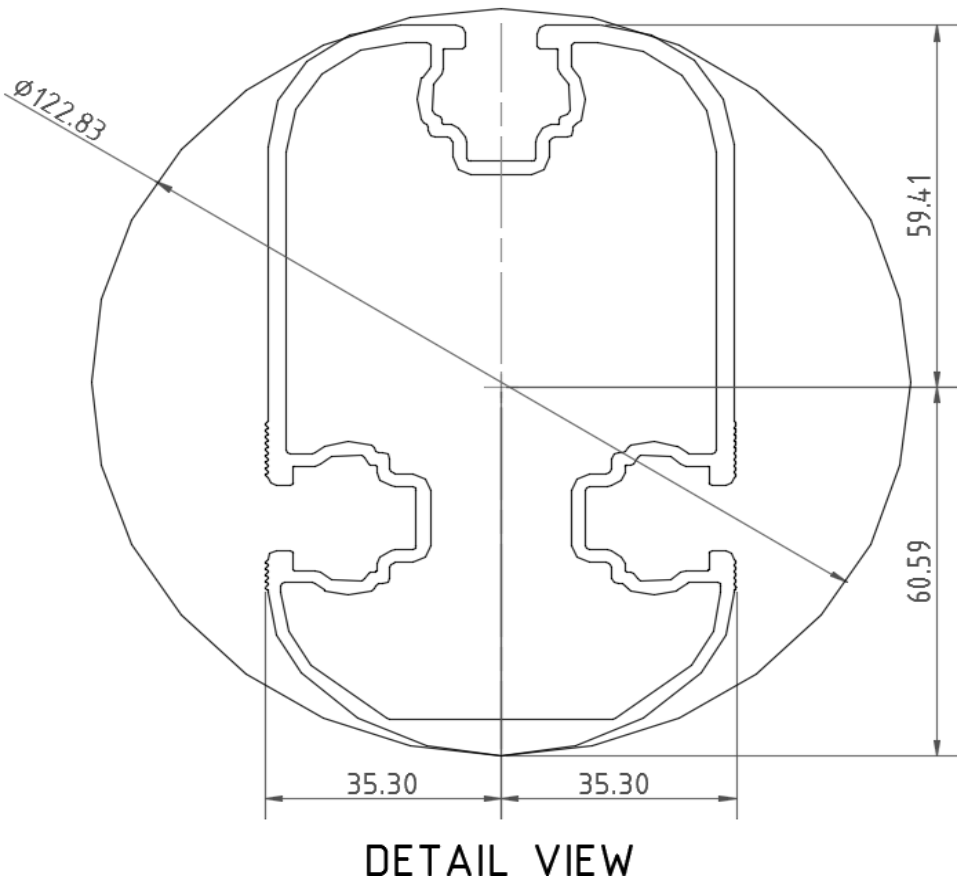
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	114	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.6	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.586	k-ft
M_z =	0.171	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	72%	



4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

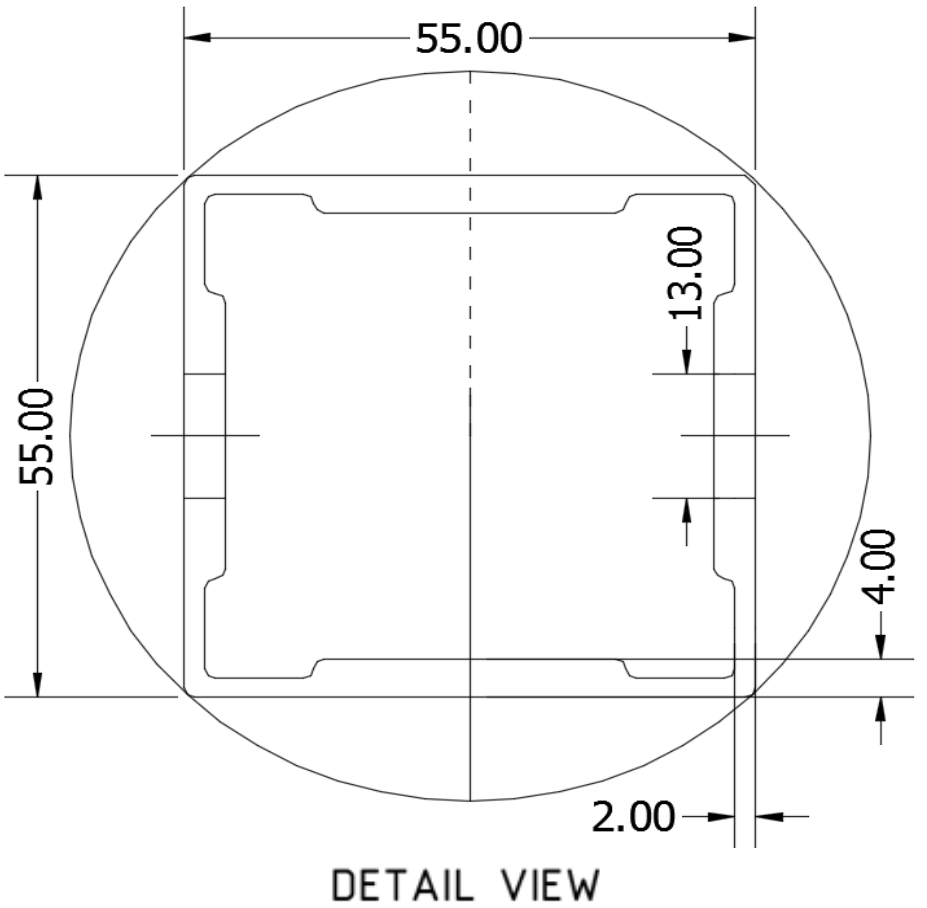
Girder Type =	**T5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	63.82	in
$\Phi F_{ty\ AXIAL}$ =	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	30.46	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	31.56	ksi
S_y =	1.98	in^3
S_x =	1.32	in^3
E =	10100	ksi
I_y =	4.74	in^4
I_x =	1.83	in^4
A =	1.93	in^2
g =	2.32	lbs/ft
M_y =	4.443	k-ft
M_z =	0.000	k-ft
P_n =	0.019	k
$M_{y\ allowable}$ =	5.026	k-ft
$M_{z\ allowable}$ =	3.472	k-ft
$P_{n\ allowable}$ =	59.439	k
Utilization =	88%	



4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.00	in
$\Phi F_{ty\ AXIAL}$ =	13.67	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.005	k-ft
M_z =	0.000	k-ft
P_n =	5.002	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.425	k
Utilization =	38%	

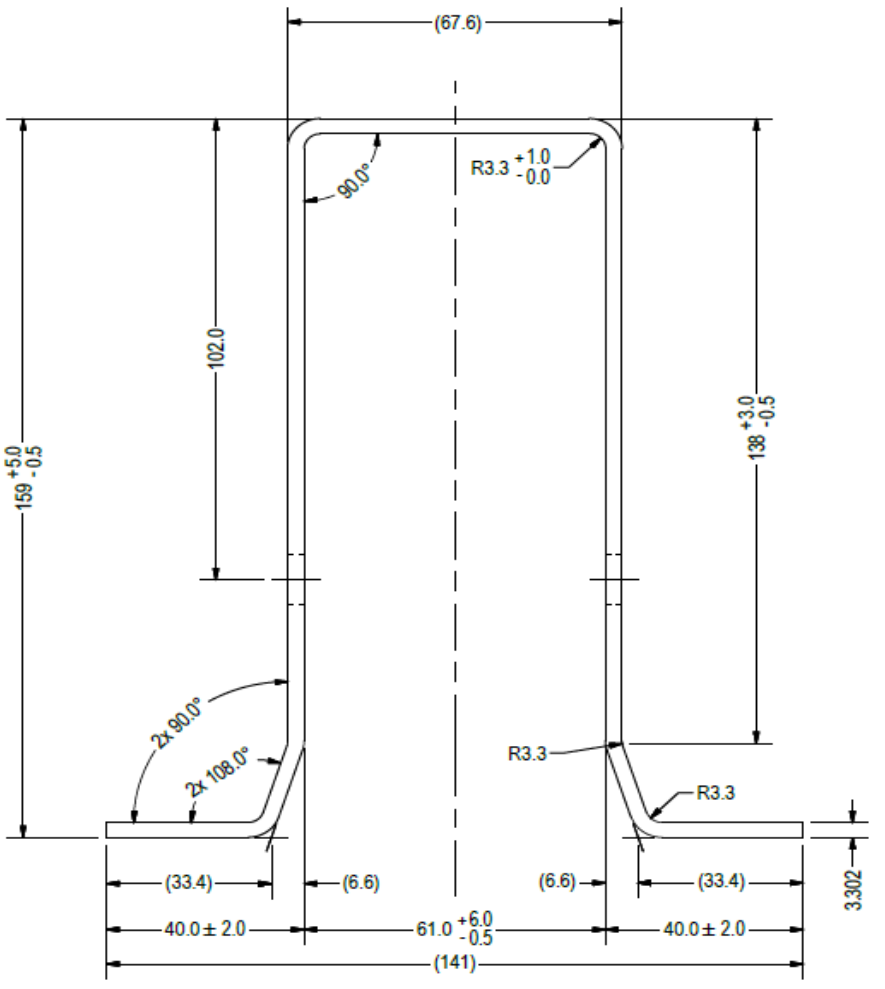


DETAIL VIEW

4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	72.60	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	10.425	k-ft
M_z =	0.000	k-ft
P_r =	6.264	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	38.073	k
Utilization =	69%	



DETAIL VIEW

5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	6.83	k
Maximum Lateral Load =	3.29	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

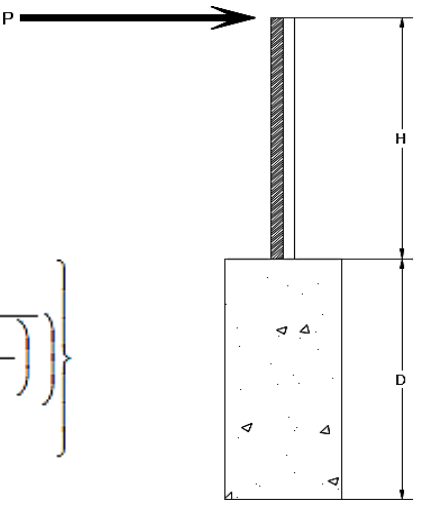
Lateral Force @ Top of Pole, P =	1.18	k
Height of Pole Above Grade, H =	5.05	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1 + \sqrt{1 + \left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

Non-Constrained

Lateral Force @ Top of Pole, P =	1.18	k
Height of Pole Above Grade, H =	5.05	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	6.35	
Required Footing Depth, D =	9.88	ft

2nd Trial @ D_2 =	6.57	ft
Lateral Soil Bearing @ D/3, S_1 =	0.44	ksf
Lateral Soil Bearing @ D, S_3 =	1.31	ksf
Constant 2.34P/(S_1B), A =	3.14	
Required Footing Depth, D =	6.02	ft

3rd Trial @ D_3 =	6.29	ft
Lateral Soil Bearing @ D/3, S_1 =	0.42	ksf
Lateral Soil Bearing @ D, S_3 =	1.26	ksf
Constant 2.34P/(S_1B), A =	3.28	
Required Footing Depth, D =	6.19	ft

4th Trial @ D_4 =	6.24	ft
Lateral Soil Bearing @ D/3, S_1 =	0.42	ksf
Lateral Soil Bearing @ D, S_3 =	1.25	ksf
Constant 2.34P/(S_1B), A =	3.30	
Required Footing Depth, D =	6.23	ft

5th Trial @ D_5 =	6.23	ft
Lateral Soil Bearing @ D/3, S_1 =	0.42	ksf
Lateral Soil Bearing @ D, S_3 =	1.25	ksf
Constant 2.34P/(S_1B), A =	3.31	
Required Footing Depth, D =	6.25	ft

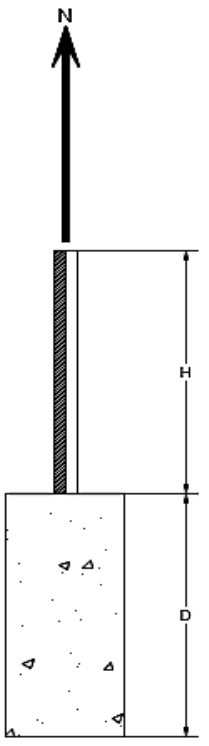
A 2ft diameter x 6.25ft deep footing unrestrained at ground level is required for the racking structure.

5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	3.27	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	2.14	k
Required Concrete Volume, V =	14.75	ft^3
Required Footing Depth, D =	4.75	ft

A 2ft diameter x 4.75ft deep footing unrestrained at ground level is required for the racking structure.



Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	7.08
2	0.4	0.2	118.10	6.98
3	0.6	0.2	118.10	6.87
4	0.8	0.2	118.10	6.77
5	1	0.2	118.10	6.67
6	1.2	0.2	118.10	6.56
7	1.4	0.2	118.10	6.46
8	1.6	0.2	118.10	6.35
9	1.8	0.2	118.10	6.25
10	2	0.2	118.10	6.15
11	2.2	0.2	118.10	6.04
12	2.4	0.2	118.10	5.94
13	2.6	0.2	118.10	5.84
14	2.8	0.2	118.10	5.73
15	3	0.2	118.10	5.63
16	3.2	0.2	118.10	5.52
17	3.4	0.2	118.10	5.42
18	3.6	0.2	118.10	5.32
19	3.8	0.2	118.10	5.21
20	4	0.2	118.10	5.11
21	4.2	0.2	118.10	5.01
22	4.4	0.2	118.10	4.90
23	4.6	0.2	118.10	4.80
24	4.8	0.2	118.10	4.69
25	0	0.0	0.00	4.69
26	0	0.0	0.00	4.69
27	0	0.0	0.00	4.69
28	0	0.0	0.00	4.69
29	0	0.0	0.00	4.69
30	0	0.0	0.00	4.69
31	0	0.0	0.00	4.69
32	0	0.0	0.00	4.69
33	0	0.0	0.00	4.69
34	0	0.0	0.00	4.69
Max	4.8	Sum	1.13	

5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	6.25	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	4.30	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	20.42	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

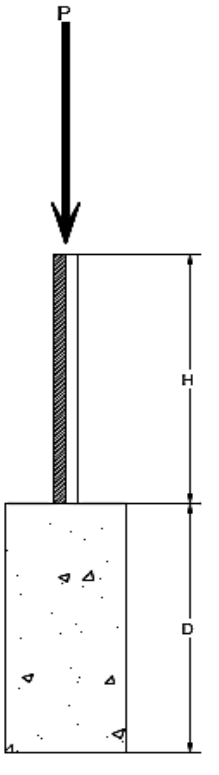
Weight of Concrete

Footing Volume	19.63	ft^3
Weight	2.85	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	3.06	k
1/3 Increase for Wind =	1.33	
Total Resistance =	10.37	k
Applied Force =	7.15	k
Utilization =	69%	

A 2ft diameter footing passes at a depth of 6.25ft.



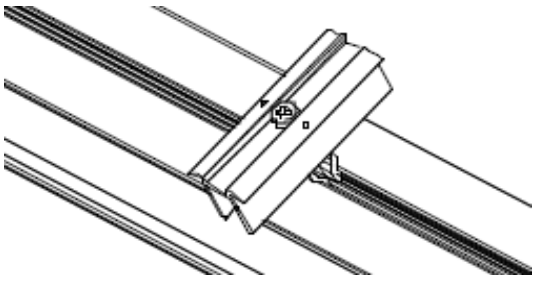
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

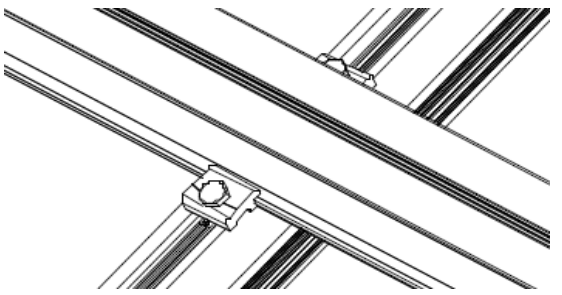
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.627 k
Allowable Uplift	=	1.214 k
Utilization	=	52%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	2.120 k
Allowable Uplift	=	2.180 k
Utilization	=	97%

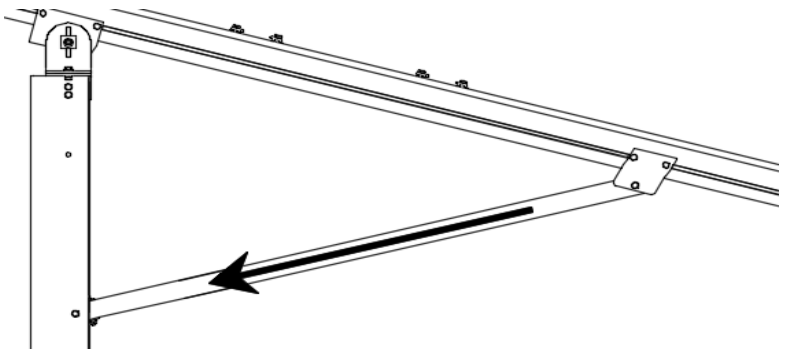


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load	=	5.002 k
M10 Bolt Shear Capacity	=	8.894 k
Utilization	=	56%

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

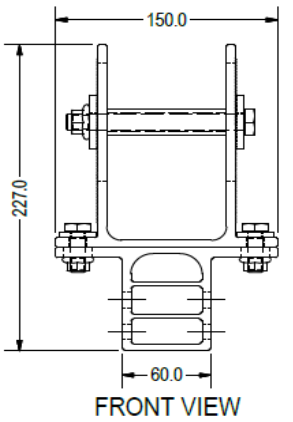


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

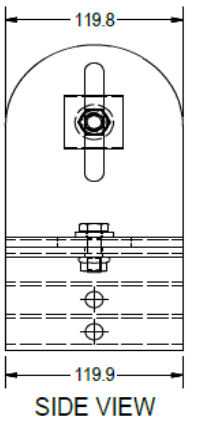
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

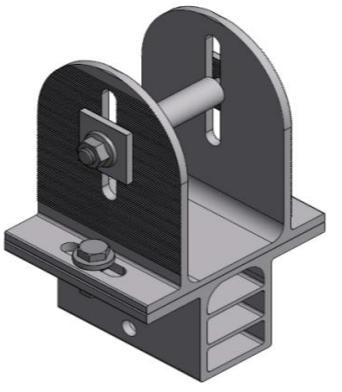
Maximum Tensile Load	=	4.498 k
Allowable Load	=	5.649 k
Utilization	=	80%



FRONT VIEW



SIDE VIEW



7. SEISMIC DESIGN

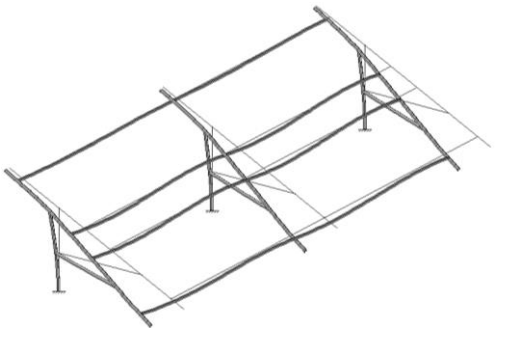
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	58.15 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.163 in
Max Drift, Δ_{MAX}	=	0.492 in

0.492 ≤ 1.163, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 114 in

J = 0.432

315.377

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 27.5 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 114

J = 0.432

200.561

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.8

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 63.8189 in
J = 1.98
82.1278

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.5 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 63.8189
J = 1.98
89.1294

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.3

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 30.5 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 5.001 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 30.80 ksi

φF_L= 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 61 in

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St$ = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 61

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk$ = 1.460 k-ft

Compression

3.4.7

λ = 1.41113

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

S1* = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

S2* = 1.23671

φcc = 0.77756

φF_L = (φccFcy)/(λ²)

φF_L = 13.6667 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 13.67 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 14.07 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	72.60	in	
Pr =	6.26	k	(LRFD Factored Load)
Mr (Strong) =	10.43	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	104.47		
4.71√(E/Fy) =	103.55	=> kL/r	> 4.71√(E/Fy)
Fcr =	23.00	ksi	
Fe =	26.23	ksi	
Pn =	51.291	k	

Torsional/Flexural Torsional Buckling:

Fcr =	17.0733	ksi
Fey =	66.8981	ksi
Fez =	21.7595	ksi
Pn =	38.0734	k

Bending (Strong Axis):

Yielding:

Mn =	21.95	k-ft

Flange Local Buckling:

Mn =	19.207	k-ft

Pr/Pc =	0.1828	<	0.2	
Utilization =	0.69	<	1.0	OK

Bending (Weak Axis):

Yielding:

Mn =	14.65	k-ft

Flange Local Buckling:

Mn =	14.39	k-ft

Pr/Pc =	0.183	<	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 69%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-8.366	-8.366	0	0
2	M11	Y	-8.366	-8.366	0	0
3	M12	Y	-8.366	-8.366	0	0
4	M13	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-4.45	-4.45	0	0
2	M11	Y	-4.45	-4.45	0	0
3	M12	Y	-4.45	-4.45	0	0
4	M13	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-46.9	-46.9	0	0
2	M11	Y	-46.9	-46.9	0	0
3	M12	Y	-46.9	-46.9	0	0
4	M13	Y	-46.9	-46.9	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-58.278	-58.278	0	0
2	M11	y	-58.278	-58.278	0	0
3	M12	y	-90.067	-90.067	0	0
4	M13	y	-90.067	-90.067	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	116.557	116.557	0	0
2	M11	y	116.557	116.557	0	0
3	M12	y	52.98	52.98	0	0
4	M13	y	52.98	52.98	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Z	6.693	6.693	0	0
2	M11	Z	6.693	6.693	0	0
3	M12	Z	6.693	6.693	0	0
4	M13	Z	6.693	6.693	0	0
5	M10	Z	0	0	0	0
6	M11	Z	0	0	0	0
7	M12	Z	0	0	0	0
8	M13	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8														
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6														
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	656.432	2	2329.191	1	238.457	2	.292	1	.01	5	4.969	1
2		min	-911.046	3	-1747.625	3	-319.013	5	-1.285	5	-.01	2	.5	15
3	N19	max	2498.889	2	6457.813	2	0	10	0	1	.01	4	9.627	1
4		min	-2534.193	3	-5248.446	3	-345.446	5	-1.346	4	0	1	.32	15
5	N29	max	656.432	2	2329.191	1	264.491	3	.336	3	.012	4	4.969	1
6		min	-911.046	3	-1747.625	3	-367.874	4	-1.361	4	-.004	3	-.185	5
7	Totals:	max	3811.753	2	11111.521	2	0	1						
8		min	-4356.285	3	-8743.696	3	-1001.011	4						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.006	2	.002	4	0	1	0	1	0	1
2			min	0	1	-.001	3	-.001	1	0	1	0	1	0	1
3		2	max	-.221	15	-.473	15	0	12	0	1	0	12	0	6
4			min	-.939	4	-2.011	6	-1.499	5	0	1	0	5	0	15
5		3	max	-10.104	12	297.491	3	-1.452	12	.065	3	.252	1	.304	2
6			min	-188.186	1	-694.423	2	-156.909	1	-.235	2	.02	12	-.128	3
7		4	max	-10.47	12	296.315	3	-1.452	12	.065	3	.154	1	.735	2
8			min	-188.917	1	-695.992	2	-156.909	1	-.235	2	.019	12	-.312	3
9		5	max	-10.835	12	295.138	3	-1.452	12	.065	3	.065	4	1.168	2
10			min	-189.648	1	-697.56	2	-156.909	1	-.235	2	-.004	10	-.496	3
11		6	max	392.546	3	608.305	2	25.116	3	.037	2	.109	2	1.122	2
12			min	-1247.319	2	-174.668	3	-211.165	1	-.055	3	-.042	3	-.507	3
13		7	max	391.998	3	606.737	2	25.116	3	.037	2	.011	10	.745	2
14			min	-1248.051	2	-175.844	3	-211.165	1	-.055	3	-.06	4	-.398	3
15		8	max	391.449	3	605.169	2	25.116	3	.037	2	-.007	12	.368	2
16			min	-1248.782	2	-177.02	3	-211.165	1	-.055	3	-.156	1	-.289	3
17		9	max	376.412	3	93.96	3	23.777	3	.016	5	.088	1	.154	1
18			min	-1380.316	1	-64.004	2	-220.885	1	-.187	2	.005	10	-.239	3
19		10	max	375.864	3	92.784	3	23.777	3	.016	5	.052	3	.191	1
20			min	-1381.047	1	-65.572	2	-220.885	1	-.187	2	-.051	2	-.297	3
21		11	max	375.315	3	91.608	3	23.777	3	.016	5	.067	3	.231	2
22			min	-1381.779	1	-67.14	2	-220.885	1	-.187	2	-.186	1	-.355	3
23		12	max	356.628	3	809.455	3	116.367	2	.361	3	.142	1	.465	2
24			min	-1574.668	1	-537.842	1	-271.833	3	-.331	2	-.017	5	-.695	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
25		13	max	356.08	3	808.279	3	116.367	2	.361	3	.175	1	.799	2
26			min	-1575.399	1	-539.41	1	-271.833	3	-.331	2	-.149	3	-1.197	3
27		14	max	190.334	1	492.609	2	69.646	5	.231	2	.051	3	1.12	2
28			min	10.303	15	-728.303	3	-121.606	1	-.424	3	-.19	4	-1.677	3
29		15	max	189.603	1	491.04	2	68.147	5	.231	2	.03	3	.815	2
30			min	10.083	15	-729.48	3	-121.606	1	-.424	3	-.163	4	-1.224	3
31		16	max	188.871	1	489.472	2	66.647	5	.231	2	.009	3	.511	2
32			min	9.862	15	-730.656	3	-121.606	1	-.424	3	-.195	1	-.771	3
33		17	max	188.14	1	487.904	2	65.147	5	.231	2	-.008	12	.207	2
34			min	9.57	12	-731.832	3	-121.606	1	-.424	3	-.271	1	-.318	3
35		18	max	.939	6	2.012	6	1.5	4	0	1	0	12	0	6
36			min	.221	15	.473	15	0	12	0	1	0	4	0	15
37		19	max	0	1	.002	2	0	1	0	1	0	1	0	1
38			min	0	1	-.005	3	0	5	0	1	0	1	0	1
39	M4	1	max	0	1	.015	2	.002	4	0	1	0	1	0	1
40			min	0	1	-.004	3	0	1	0	1	0	1	0	1
41		2	max	-.221	15	-.473	15	0	1	0	1	0	1	0	4
42			min	-.939	4	-2.009	4	-1.499	5	0	1	0	5	0	15
43		3	max	-10.672	12	916.04	3	0	1	.027	4	.206	4	.75	2
44			min	-325.674	1	-1961.113	2	-99.327	5	0	1	0	1	-.353	3
45		4	max	-11.037	12	914.864	3	0	1	.027	4	.144	4	1.967	2
46			min	-326.405	1	-1962.681	2	-100.827	5	0	1	0	1	-.922	3
47		5	max	-11.403	12	913.688	3	0	1	.027	4	.081	4	3.186	2
48			min	-327.137	1	-1964.249	2	-102.326	5	0	1	0	1	-1.489	3
49		6	max	1399.278	3	1799.085	2	0	1	0	1	0	1	3.024	2
50			min	-3452.814	2	-693.976	3	-95.06	4	-.022	4	-.017	5	-1.466	3
51		7	max	1398.729	3	1797.517	2	0	1	0	1	0	1	1.908	2
52			min	-3453.545	2	-695.152	3	-96.56	4	-.022	4	-.076	4	-1.035	3
53		8	max	1398.181	3	1795.948	2	0	1	0	1	0	1	.793	2
54			min	-3454.276	2	-696.328	3	-98.06	4	-.022	4	-.136	4	-.603	3
55		9	max	1383.581	3	270.43	3	0	1	.013	4	.103	4	.144	1
56			min	-3554.471	2	-235.48	1	-205.492	4	0	1	0	1	-.388	3
57		10	max	1383.032	3	269.253	3	0	1	.013	4	0	1	.29	1
58			min	-3555.203	2	-237.048	1	-206.991	4	0	1	-.025	4	-.555	3
59		11	max	1382.484	3	268.077	3	0	1	.013	4	0	1	.438	1
60			min	-3555.934	2	-238.616	1	-208.491	4	0	1	-.154	4	-.722	3
61		12	max	1375.183	3	2269.507	3	0	1	.129	4	.009	5	1.148	1
62			min	-3775.123	1	-1697.348	2	-222.494	5	0	1	0	1	-1.685	3
63		13	max	1374.635	3	2268.331	3	0	1	.129	4	0	1	2.198	1
64			min	-3775.854	1	-1698.916	2	-223.994	5	0	1	-.13	4	-3.093	3
65		14	max	327.959	1	1424.499	1	63.516	5	0	1	0	1	3.205	1
66			min	12.838	12	-1977.621	3	0	1	-.091	4	-.165	5	-4.443	3
67		15	max	327.228	1	1422.931	1	62.016	5	0	1	0	1	2.322	1
68			min	12.472	12	-1978.797	3	0	1	-.091	4	-.126	5	-3.215	3
69		16	max	326.497	1	1421.362	1	60.517	5	0	1	0	1	1.439	1
70			min	12.106	12	-1979.973	3	0	1	-.091	4	-.088	5	-1.986	3
71		17	max	325.765	1	1419.794	1	59.017	5	0	1	0	1	.557	1
72			min	11.741	12	-1981.15	3	0	1	-.091	4	-.051	4	-.757	3
73		18	max	.939	6	2.014	6	1.5	5	0	1	0	1	0	6
74			min	.221	15	.473	15	0	1	0	1	0	5	0	15
75		19	max	0	1	.006	2	0	1	0	1	0	1	0	1
76			min	0	1	-.012	3	0	4	0	1	0	1	0	1
77	M7	1	max	0	1	.006	2	.002	4	0	1	0	1	0	1
78			min	0	1	-.001	3	0	12	0	1	0	1	0	1
79		2	max	-.221	15	-.473	15	.001	1	0	1	0	1	0	4
80			min	-.939	4	-2.011	4	-1.499	5	0	1	0	5	0	15
81		3	max	15.032	5	297.491	3	156.909	1	.235	2	.098	5	.304	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
82			min	-188.186	1	-694.423	2	-43.773	5	-.065	3	-.252	1	-.128	3
83		4	max	14.691	5	296.315	3	156.909	1	.235	2	.071	5	.735	2
84			min	-188.917	1	-695.992	2	-45.273	5	-.065	3	-.154	1	-.312	3
85		5	max	14.349	5	295.138	3	156.909	1	.235	2	.042	5	1.168	2
86			min	-189.648	1	-697.56	2	-46.773	5	-.065	3	-.057	1	-.496	3
87		6	max	392.546	3	608.305	2	211.165	1	.055	3	.042	3	1.122	2
88			min	-1247.319	2	-174.668	3	-37.323	5	-.037	2	-.109	2	-.507	3
89		7	max	391.998	3	606.737	2	211.165	1	.055	3	.027	3	.745	2
90			min	-1248.051	2	-175.844	3	-38.822	5	-.037	2	-.047	5	-.398	3
91		8	max	391.449	3	605.169	2	211.165	1	.055	3	.156	1	.368	2
92			min	-1248.782	2	-177.02	3	-40.322	5	-.037	2	-.072	5	-.289	3
93		9	max	376.412	3	93.96	3	220.885	1	.187	2	.036	5	.154	1
94			min	-1380.316	1	-64.004	2	-84.188	5	.015	15	-.088	1	-.239	3
95		10	max	375.864	3	92.784	3	220.885	1	.187	2	.051	2	.191	1
96			min	-1381.047	1	-65.572	2	-85.688	5	.015	15	-.052	3	-.297	3
97		11	max	375.315	3	91.608	3	220.885	1	.187	2	.186	1	.231	2
98			min	-1381.779	1	-67.14	2	-87.188	5	.015	15	-.07	5	-.355	3
99		12	max	356.628	3	809.455	3	271.833	3	.331	2	-.013	12	.465	2
100			min	-1574.668	1	-537.842	1	-191.87	5	-.361	3	-.142	1	-.695	3
101		13	max	356.08	3	808.279	3	271.833	3	.331	2	.149	3	.799	2
102			min	-1575.399	1	-539.41	1	-193.369	5	-.361	3	-.182	4	-1.197	3
103		14	max	190.334	1	492.609	2	121.606	1	.424	3	.044	1	1.12	2
104			min	6.709	15	-728.303	3	21.551	10	-.231	2	-.18	5	-1.677	3
105		15	max	189.603	1	491.04	2	121.606	1	.424	3	.12	1	.815	2
106			min	6.489	15	-729.48	3	21.551	10	-.231	2	-.128	5	-1.224	3
107		16	max	188.871	1	489.472	2	121.606	1	.424	3	.195	1	.511	2
108			min	6.268	15	-730.656	3	21.551	10	-.231	2	-.077	5	-.771	3
109		17	max	188.14	1	487.904	2	121.606	1	.424	3	.271	1	.207	2
110			min	6.047	15	-731.832	3	21.551	10	-.231	2	-.027	5	-.318	3
111		18	max	.939	4	2.013	4	1.5	5	0	1	0	1	0	4
112			min	.221	15	.473	15	0	1	0	1	0	5	0	15
113		19	max	0	1	.002	2	0	15	0	1	0	1	0	1
114			min	0	1	-.005	3	0	1	0	1	0	1	0	1
115	M10	1	max	121.604	1	484.572	2	-5.609	15	.009	2	.32	1	.231	2
116			min	21.548	10	-734.152	3	-186.953	1	-.022	3	.004	15	-.424	3
117		2	max	121.604	1	352.383	2	-4.015	15	.009	2	.143	1	.249	3
118			min	21.548	10	-542.427	3	-148.194	1	-.022	3	-.002	5	-.213	1
119		3	max	121.604	1	220.193	2	-2.422	15	.009	2	.029	2	.721	3
120			min	21.548	10	-350.701	3	-109.435	1	-.022	3	-.01	4	-.515	1
121		4	max	121.604	1	88.004	2	-.828	15	.009	2	0	10	.99	3
122			min	21.548	10	-158.976	3	-70.677	1	-.022	3	-.088	1	-.676	1
123		5	max	121.604	1	32.749	3	1.077	5	.009	2	-.007	15	1.056	3
124			min	21.548	10	-45.564	1	-31.918	1	-.022	3	-.142	1	-.699	2
125		6	max	121.604	1	224.475	3	8.931	9	.009	2	-.005	15	.921	3
126			min	15.022	15	-177.895	1	-7.802	2	-.022	3	-.156	1	-.582	2
127		7	max	121.604	1	416.2	3	45.6	1	.009	2	-.002	15	.582	3
128			min	7.729	15	-310.226	1	-2.224	10	-.022	3	-.128	1	-.326	2
129		8	max	121.604	1	607.925	3	84.359	1	.009	2	.005	5	.075	1
130			min	.436	15	-442.557	1	2.179	10	-.022	3	-.059	1	-.016	5
131		9	max	121.604	1	799.651	3	123.117	1	.009	2	.05	1	.612	1
132			min	-9.851	5	-574.888	1	3.904	12	-.022	3	-.023	10	-.701	3
133		10	max	121.604	1	707.219	1	-5.145	15	.009	2	.201	1	1.289	1
134			min	21.548	10	-991.376	3	-161.876	1	-.022	3	-.014	10	-1.646	3
135		11	max	121.604	1	574.888	1	-3.551	15	.022	3	.05	1	.612	1
136			min	16.305	15	-799.651	3	-123.117	1	-.009	2	-.023	10	-.701	3
137		12	max	121.604	1	442.557	1	-1.957	15	.022	3	-.007	15	.075	1
138			min	9.012	15	-607.925	3	-84.359	1	-.009	2	-.059	1	.015	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
139		13	max	121.604	1	310.226	1	2.224	10	.022	3	-.008	15	.582	3
140			min	1.719	15	-416.2	3	-45.6	1	-.009	2	-.128	1	-.326	2
141		14	max	121.604	1	177.895	1	7.802	2	.022	3	-.007	15	.921	3
142			min	-7.986	5	-224.475	3	-8.931	9	-.009	2	-.156	1	-.582	2
143		15	max	121.604	1	45.564	1	31.918	1	.022	3	-.005	15	1.056	3
144			min	-18.821	5	-32.749	3	2.47	12	-.009	2	-.142	1	-.699	2
145		16	max	121.604	1	158.976	3	70.677	1	.022	3	0	10	.99	3
146			min	-29.657	5	-88.004	2	4.064	12	-.009	2	-.088	1	-.676	1
147		17	max	121.604	1	350.701	3	109.435	1	.022	3	.029	2	.721	3
148			min	-40.492	5	-220.193	2	5.658	12	-.009	2	-.007	9	-.515	1
149		18	max	121.604	1	542.427	3	148.194	1	.022	3	.143	1	.249	3
150			min	-51.328	5	-352.383	2	7.251	12	-.009	2	.009	12	-.213	1
151		19	max	121.604	1	734.152	3	186.953	1	.022	3	.32	1	.231	2
152			min	-62.163	5	-484.572	2	8.845	12	-.009	2	.017	12	-.424	3
153	M11	1	max	274.166	1	472.033	1	19.763	5	0	15	.356	1	.174	1
154			min	-295.504	3	-720.088	3	-192.784	1	-.006	1	-.132	5	-.475	3
155		2	max	274.166	1	339.702	1	22.229	5	0	15	.173	1	.183	3
156			min	-295.504	3	-528.362	3	-154.025	1	-.006	1	-.109	5	-.28	2
157		3	max	274.166	1	207.371	1	24.694	5	0	15	.037	2	.64	3
158			min	-295.504	3	-336.637	3	-115.266	1	-.006	1	-.085	5	-.563	2
159		4	max	274.166	1	75.04	1	27.16	5	0	15	.01	3	.894	3
160			min	-295.504	3	-144.911	3	-76.507	1	-.006	1	-.075	4	-.707	2
161		5	max	274.166	1	46.814	3	29.626	5	0	15	0	3	.946	3
162			min	-295.504	3	-62.005	2	-37.749	1	-.006	1	-.13	1	-.711	2
163		6	max	274.166	1	238.539	3	33.875	4	0	15	.005	5	.795	3
164			min	-295.504	3	-194.194	2	-9.77	2	-.006	1	-.15	1	-.576	2
165		7	max	274.166	1	430.265	3	44.84	4	0	15	.04	5	.442	3
166			min	-295.504	3	-326.384	2	-3.658	3	-.006	1	-.128	1	-.301	2
167		8	max	274.166	1	621.99	3	78.528	1	0	15	.078	5	.113	2
168			min	-295.504	3	-458.573	2	-1.268	3	-.006	1	-.066	1	-.113	3
169		9	max	274.166	1	813.715	3	117.287	1	0	15	.133	4	.667	2
170			min	-295.504	3	-590.763	2	.986	12	-.006	1	-.025	2	-.871	3
171		10	max	274.166	1	722.952	2	21.24	5	.006	1	.209	4	1.36	2
172			min	-295.504	3	-1005.441	3	-156.045	1	-.003	14	-.015	10	-1.831	3
173		11	max	274.166	1	590.763	2	23.706	5	.006	1	.042	9	.667	2
174			min	-295.504	3	-813.715	3	-117.287	1	0	5	-.11	5	-.871	3
175		12	max	274.166	1	458.573	2	26.171	5	.006	1	-.01	12	.113	2
176			min	-295.504	3	-621.99	3	-78.528	1	0	5	-.095	4	-.113	3
177		13	max	274.166	1	326.384	2	28.637	5	.006	1	-.008	12	.442	3
178			min	-295.504	3	-430.265	3	-39.769	1	0	5	-.128	1	-.301	2
179		14	max	274.166	1	194.194	2	31.103	5	.006	1	-.005	12	.795	3
180			min	-295.504	3	-238.539	3	-4.973	9	0	5	-.15	1	-.576	2
181		15	max	274.166	1	62.005	2	40.486	4	.006	1	.01	5	.946	3
182			min	-295.504	3	-46.814	3	5.388	12	0	5	-.13	1	-.711	2
183		16	max	274.166	1	144.911	3	76.507	1	.006	1	.047	5	.894	3
184			min	-295.504	3	-75.04	1	6.982	12	0	5	-.07	1	-.707	2
185		17	max	274.166	1	336.637	3	115.266	1	.006	1	.09	4	.64	3
186			min	-295.504	3	-207.371	1	8.576	12	0	5	.01	9	-.563	2
187		18	max	274.166	1	528.362	3	154.025	1	.006	1	.173	1	.183	3
188			min	-295.504	3	-339.702	1	10.17	12	0	5	.024	12	-.28	2
189		19	max	274.166	1	720.088	3	192.784	1	.006	1	.356	1	.174	1
190			min	-295.504	3	-472.033	1	11.763	12	0	5	.036	12	-.475	3
191	M12	1	max	42.271	5	665.581	2	22.428	5	0	3	.378	1	.225	2
192			min	-20.89	9	-272.787	3	-196.171	1	-.007	1	-.143	5	.028	15
193		2	max	33.066	2	479.704	2	24.894	5	0	3	.191	1	.303	3
194			min	-20.89	9	-188.436	3	-157.413	1	-.007	1	-.118	5	-.38	2
195		3	max	33.066	2	293.826	2	27.36	5	0	3	.052	2	.457	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
196			min	-20.89	9	-104.085	3	-118.654	1	-.007	1	-.091	5	-.788	2
197		4	max	33.066	2	107.948	2	29.826	5	0	3	.007	10	.522	3
198			min	-20.89	9	-19.734	3	-79.895	1	-.007	1	-.077	4	-1	2
199		5	max	33.066	2	64.617	3	32.291	5	0	3	-.005	12	.499	3
200			min	-20.89	9	-77.929	2	-41.136	1	-.007	1	-.123	1	-1.016	2
201		6	max	33.066	2	148.967	3	36.132	4	0	3	.008	5	.386	3
202			min	-22.138	14	-263.807	2	-13.317	2	-.007	1	-.146	1	-.835	2
203		7	max	33.066	2	233.318	3	47.097	4	0	3	.046	5	.184	3
204			min	-29.744	4	-449.685	2	-4.514	10	-.007	1	-.128	1	-.459	2
205		8	max	33.066	2	317.669	3	75.14	1	0	3	.086	5	.114	2
206			min	-40.579	4	-635.562	2	-.111	10	-.007	1	-.07	1	-.107	3
207		9	max	33.066	2	402.02	3	113.899	1	0	3	.143	4	.883	2
208			min	-51.415	4	-821.44	2	3.177	12	-.007	1	-.033	2	-.486	3
209		10	max	33.066	2	1007.317	2	104.948	9	.007	1	.222	4	1.848	2
210			min	-62.25	4	-486.371	3	-152.658	1	-.003	14	-.021	10	-.955	3
211		11	max	39.901	5	821.44	2	26.635	5	.007	1	.039	9	.883	2
212			min	-20.89	9	-402.02	3	-113.899	1	0	5	-.122	5	-.486	3
213		12	max	33.066	2	635.562	2	29.1	5	.007	1	-.008	12	.114	2
214			min	-20.89	9	-317.669	3	-75.14	1	0	5	-.103	4	-.107	3
215		13	max	33.066	2	449.685	2	31.566	5	.007	1	-.008	12	.184	3
216			min	-20.89	9	-233.318	3	-36.381	1	0	5	-.128	1	-.459	2
217		14	max	33.066	2	263.807	2	34.032	5	.007	1	-.008	12	.386	3
218			min	-20.89	9	-148.967	3	-3.648	9	0	5	-.146	1	-.835	2
219		15	max	33.066	2	77.929	2	43.896	4	.007	1	.012	5	.499	3
220			min	-20.89	9	-64.617	3	3.198	12	0	5	-.123	1	-1.016	2
221		16	max	33.066	2	19.734	3	79.895	1	.007	1	.051	5	.522	3
222			min	-23.369	14	-107.948	2	4.791	12	0	5	-.06	1	-1	2
223		17	max	33.066	2	104.085	3	118.654	1	.007	1	.099	4	.457	3
224			min	-32.141	4	-293.826	2	6.385	12	0	5	.005	12	-.788	2
225		18	max	33.066	2	188.436	3	157.413	1	.007	1	.191	1	.303	3
226			min	-42.976	4	-479.704	2	7.979	12	0	5	.013	12	-.38	2
227		19	max	33.066	2	272.787	3	196.171	1	.007	1	.378	1	.225	2
228			min	-53.812	4	-665.581	2	9.572	12	0	5	.022	12	-.032	5
229	M13	1	max	40.714	5	691.766	2	15.717	5	.008	3	.315	1	.235	2
230			min	-156.787	1	-299.887	3	-186.359	1	-.022	2	-.117	5	-.065	3
231		2	max	29.879	5	505.888	2	18.182	5	.008	3	.139	1	.207	3
232			min	-156.787	1	-215.537	3	-147.6	1	-.022	2	-.099	5	-.397	2
233		3	max	19.043	5	320.01	2	20.648	5	.008	3	.026	2	.39	3
234			min	-156.787	1	-131.186	3	-108.841	1	-.022	2	-.081	4	-.833	2
235		4	max	8.208	5	134.133	2	23.114	5	.008	3	0	10	.484	3
236			min	-156.787	1	-46.835	3	-70.083	1	-.022	2	-.091	1	-1.073	2
237		5	max	-1.452	12	37.516	3	25.58	5	.008	3	-.005	12	.488	3
238			min	-156.787	1	-51.745	2	-31.324	1	-.022	2	-.145	1	-1.117	2
239		6	max	-1.452	12	121.867	3	31.203	4	.008	3	0	15	.404	3
240			min	-156.787	1	-237.622	2	-7.259	2	-.022	2	-.157	1	-.964	2
241		7	max	-1.452	12	206.218	3	46.194	1	.008	3	.03	5	.231	3
242			min	-156.787	1	-423.5	2	-1.939	10	-.022	2	-.129	1	-.615	2
243		8	max	-1.452	12	290.569	3	84.952	1	.008	3	.063	5	-.006	15
244			min	-156.787	1	-609.378	2	1.783	12	-.022	2	-.06	1	-.084	1
245		9	max	-1.452	12	374.919	3	123.711	1	.008	3	.116	4	.672	2
246			min	-156.787	1	-795.255	2	3.377	12	-.022	2	-.023	10	-.382	3
247		10	max	-1.452	12	981.133	2	110.498	9	.02	1	.202	1	1.609	2
248			min	-156.787	1	-459.27	3	-162.47	1	-.022	2	-.013	10	-.822	3
249		11	max	28.774	5	795.255	2	18.846	5	.022	2	.051	1	.672	2
250			min	-156.787	1	-374.919	3	-123.711	1	-.008	3	-.089	5	-.382	3
251		12	max	17.939	5	609.378	2	21.311	5	.022	2	-.007	12	0	5
252			min	-156.787	1	-290.569	3	-84.952	1	-.008	3	-.077	4	-.084	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
253		13	max	7.103	5	423.5	2	23.777	5	.022	2	-.008	12	.231	3
254			min	-156.787	1	-206.218	3	-46.194	1	-.008	3	-.129	1	-.615	2
255		14	max	-1.452	12	237.622	2	26.243	5	.022	2	-.008	12	.404	3
256			min	-156.787	1	-121.867	3	-9.198	9	-.008	3	-.157	1	-.964	2
257		15	max	-1.452	12	51.745	2	34.168	4	.022	2	.011	5	.488	3
258			min	-156.787	1	-37.516	3	2.998	12	-.008	3	-.145	1	-1.117	2
259		16	max	-1.452	12	46.835	3	70.083	1	.022	2	.043	5	.484	3
260			min	-156.787	1	-134.133	2	4.591	12	-.008	3	-.091	1	-1.073	2
261		17	max	-1.452	12	131.186	3	108.841	1	.022	2	.077	5	.39	3
262			min	-156.787	1	-320.01	2	6.185	12	-.008	3	-.008	9	-.833	2
263		18	max	-1.452	12	215.537	3	147.6	1	.022	2	.139	4	.207	3
264			min	-156.787	1	-505.888	2	7.779	12	-.008	3	.012	12	-.397	2
265		19	max	-1.452	12	299.887	3	186.359	1	.022	2	.315	1	.235	2
266			min	-156.787	1	-691.766	2	9.372	12	-.008	3	.021	12	-.065	3
267	M2	1	max	2329.191	1	910.465	3	238.685	2	.01	5	1.285	5	4.969	1
268			min	-1747.625	3	-655.103	2	-319.079	5	-.01	2	-.292	1	.5	15
269		2	max	2326.636	1	910.465	3	238.685	2	.01	5	1.195	5	5.026	1
270			min	-1749.541	3	-655.103	2	-316.865	5	-.01	2	-.227	1	.479	15
271		3	max	2324.081	1	910.465	3	238.685	2	.01	5	1.107	5	5.084	1
272			min	-1751.457	3	-655.103	2	-314.651	5	-.01	2	-.163	1	.458	15
273		4	max	1725.416	1	1170.893	1	176.991	2	.002	2	1.019	5	4.928	1
274			min	-1507.389	3	102.803	15	-298.832	5	-.001	3	-.14	1	.433	15
275		5	max	1722.861	1	1170.893	1	176.991	2	.002	2	.935	5	4.599	1
276			min	-1509.305	3	102.803	15	-296.617	5	-.001	3	-.091	1	.404	15
277		6	max	1720.306	1	1170.893	1	176.991	2	.002	2	.852	5	4.271	1
278			min	-1511.221	3	102.803	15	-294.403	5	-.001	3	-.042	1	.375	15
279		7	max	1717.751	1	1170.893	1	176.991	2	.002	2	.776	4	3.942	1
280			min	-1513.137	3	102.803	15	-292.189	5	-.001	3	-.064	3	.346	15
281		8	max	1715.196	1	1170.893	1	176.991	2	.002	2	.7	4	3.614	1
282			min	-1515.054	3	102.803	15	-289.975	5	-.001	3	-.131	3	.317	15
283		9	max	1712.642	1	1170.893	1	176.991	2	.002	2	.625	4	3.285	1
284			min	-1516.97	3	102.803	15	-287.761	5	-.001	3	-.198	3	.288	15
285		10	max	1710.087	1	1170.893	1	176.991	2	.002	2	.55	4	2.957	1
286			min	-1518.886	3	102.803	15	-285.546	5	-.001	3	-.265	3	.26	15
287		11	max	1707.532	1	1170.893	1	176.991	2	.002	2	.477	4	2.628	1
288			min	-1520.802	3	102.803	15	-283.332	5	-.001	3	-.331	3	.231	15
289		12	max	1704.977	1	1170.893	1	176.991	2	.002	2	.403	4	2.3	1
290			min	-1522.718	3	102.803	15	-281.118	5	-.001	3	-.398	3	.202	15
291		13	max	1702.422	1	1170.893	1	176.991	2	.002	2	.331	4	1.971	1
292			min	-1524.634	3	102.803	15	-278.904	5	-.001	3	-.465	3	.173	15
293		14	max	1699.867	1	1170.893	1	176.991	2	.002	2	.37	2	1.643	1
294			min	-1526.551	3	102.803	15	-276.689	5	-.001	3	-.532	3	.144	15
295		15	max	1697.312	1	1170.893	1	176.991	2	.002	2	.42	2	1.314	1
296			min	-1528.467	3	102.803	15	-274.475	5	-.001	3	-.599	3	.115	15
297		16	max	1694.757	1	1170.893	1	176.991	2	.002	2	.47	2	.986	1
298			min	-1530.383	3	102.803	15	-272.261	5	-.001	3	-.665	3	.087	15
299		17	max	1692.202	1	1170.893	1	176.991	2	.002	2	.519	2	.657	1
300			min	-1532.299	3	102.803	15	-270.047	5	-.001	3	-.732	3	.058	15
301		18	max	1689.648	1	1170.893	1	176.991	2	.002	2	.569	2	.329	1
302			min	-1534.215	3	102.803	15	-267.832	5	-.001	3	-.799	3	.029	15
303		19	max	1687.093	1	1170.893	1	176.991	2	.002	2	.619	2	0	1
304			min	-1536.131	3	102.803	15	-265.618	5	-.001	3	-.866	3	0	1
305	M5	1	max	6457.813	2	2530.716	3	0	1	.01	4	1.346	4	9.627	1
306			min	-5248.446	3	-2491.296	2	-345.589	5	0	1	0	1	.32	15
307		2	max	6455.258	2	2530.716	3	0	1	.01	4	1.25	4	10.044	1
308			min	-5250.362	3	-2491.296	2	-343.375	5	0	1	0	1	.323	15
309		3	max	6452.703	2	2530.716	3	0	1	.01	4	1.154	4	10.46	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
310			min	-5252.279	3	-2491.296	2	-341.161	5	0	1	0	1	.327	15
311		4	max	4619.447	1	2439.982	1	0	1	0	1	1.061	4	10.269	1
312			min	-4400.491	3	75.218	15	-326.243	4	0	4	0	1	.317	15
313		5	max	4616.893	1	2439.982	1	0	1	0	1	.97	4	9.584	1
314			min	-4402.408	3	75.218	15	-324.029	4	0	4	0	1	.295	15
315		6	max	4614.338	1	2439.982	1	0	1	0	1	.879	4	8.9	1
316			min	-4404.324	3	75.218	15	-321.815	4	0	4	0	1	.274	15
317		7	max	4611.783	1	2439.982	1	0	1	0	1	.789	4	8.215	1
318			min	-4406.24	3	75.218	15	-319.6	4	0	4	0	1	.253	15
319		8	max	4609.228	1	2439.982	1	0	1	0	1	.7	4	7.531	1
320			min	-4408.156	3	75.218	15	-317.386	4	0	4	0	1	.232	15
321		9	max	4606.673	1	2439.982	1	0	1	0	1	.611	4	6.846	1
322			min	-4410.072	3	75.218	15	-315.172	4	0	4	0	1	.211	15
323		10	max	4604.118	1	2439.982	1	0	1	0	1	.523	4	6.161	1
324			min	-4411.988	3	75.218	15	-312.958	4	0	4	0	1	.19	15
325		11	max	4601.563	1	2439.982	1	0	1	0	1	.436	4	5.477	1
326			min	-4413.905	3	75.218	15	-310.743	4	0	4	0	1	.169	15
327		12	max	4599.008	1	2439.982	1	0	1	0	1	.349	4	4.792	1
328			min	-4415.821	3	75.218	15	-308.529	4	0	4	0	1	.148	15
329		13	max	4596.453	1	2439.982	1	0	1	0	1	.262	4	4.108	1
330			min	-4417.737	3	75.218	15	-306.315	4	0	4	0	1	.127	15
331		14	max	4593.899	1	2439.982	1	0	1	0	1	.177	4	3.423	1
332			min	-4419.653	3	75.218	15	-304.101	4	0	4	0	1	.106	15
333		15	max	4591.344	1	2439.982	1	0	1	0	1	.092	4	2.738	1
334			min	-4421.569	3	75.218	15	-301.886	4	0	4	0	1	.084	15
335		16	max	4588.789	1	2439.982	1	0	1	0	1	.007	4	2.054	1
336			min	-4423.485	3	75.218	15	-299.672	4	0	4	0	1	.063	15
337		17	max	4586.234	1	2439.982	1	0	1	0	1	0	1	1.369	1
338			min	-4425.402	3	75.218	15	-297.458	4	0	4	-.076	4	.042	15
339		18	max	4583.679	1	2439.982	1	0	1	0	1	0	1	.685	1
340			min	-4427.318	3	75.218	15	-295.244	4	0	4	-.16	4	.021	15
341		19	max	4581.124	1	2439.982	1	0	1	0	1	0	1	0	1
342			min	-4429.234	3	75.218	15	-293.03	4	0	4	-.242	4	0	1
343	M8	1	max	2329.191	1	910.465	3	264.282	3	.012	4	1.361	4	4.969	1
344			min	-1747.625	3	-655.103	2	-368.132	4	-.004	3	-.336	3	-.185	5
345		2	max	2326.636	1	910.465	3	264.282	3	.012	4	1.258	4	5.026	1
346			min	-1749.541	3	-655.103	2	-365.918	4	-.004	3	-.262	3	-.159	5
347		3	max	2324.081	1	910.465	3	264.282	3	.012	4	1.156	4	5.084	1
348			min	-1751.457	3	-655.103	2	-363.704	4	-.004	3	-.187	3	-.133	5
349		4	max	1725.416	1	1170.893	1	238.063	3	.001	3	1.061	4	4.928	1
350			min	-1507.389	3	-27.814	5	-338.998	4	-.002	2	-.136	3	-.117	5
351		5	max	1722.861	1	1170.893	1	238.063	3	.001	3	.966	4	4.599	1
352			min	-1509.305	3	-27.814	5	-336.783	4	-.002	2	-.069	3	-.109	5
353		6	max	1720.306	1	1170.893	1	238.063	3	.001	3	.872	4	4.271	1
354			min	-1511.221	3	-27.814	5	-334.569	4	-.002	2	-.003	3	-.101	5
355		7	max	1717.751	1	1170.893	1	238.063	3	.001	3	.779	4	3.942	1
356			min	-1513.137	3	-27.814	5	-332.355	4	-.002	2	-.023	2	-.094	5
357		8	max	1715.196	1	1170.893	1	238.063	3	.001	3	.686	4	3.614	1
358			min	-1515.054	3	-27.814	5	-330.141	4	-.002	2	-.072	2	-.086	5
359		9	max	1712.642	1	1170.893	1	238.063	3	.001	3	.6	5	3.285	1
360			min	-1516.97	3	-27.814	5	-327.926	4	-.002	2	-.122	2	-.078	5
361		10	max	1710.087	1	1170.893	1	238.063	3	.001	3	.516	5	2.957	1
362			min	-1518.886	3	-27.814	5	-325.712	4	-.002	2	-.172	2	-.07	5
363		11	max	1707.532	1	1170.893	1	238.063	3	.001	3	.432	5	2.628	1
364			min	-1520.802	3	-27.814	5	-323.498	4	-.002	2	-.221	2	-.062	5
365		12	max	1704.977	1	1170.893	1	238.063	3	.001	3	.398	3	2.3	1
366			min	-1522.718	3	-27.814	5	-321.284	4	-.002	2	-.271	2	-.055	5

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
367		13	max	1702.422	1	1170.893	1	238.063	3	.001	3	.465	3	1.971	1
368			min	-1524.634	3	-27.814	5	-319.069	4	-.002	2	-.321	2	-.047	5
369		14	max	1699.867	1	1170.893	1	238.063	3	.001	3	.532	3	1.643	1
370			min	-1526.551	3	-27.814	5	-316.855	4	-.002	2	-.37	2	-.039	5
371		15	max	1697.312	1	1170.893	1	238.063	3	.001	3	.599	3	1.314	1
372			min	-1528.467	3	-27.814	5	-314.641	4	-.002	2	-.42	2	-.031	5
373		16	max	1694.757	1	1170.893	1	238.063	3	.001	3	.665	3	.986	1
374			min	-1530.383	3	-27.814	5	-312.427	4	-.002	2	-.47	2	-.023	5
375		17	max	1692.202	1	1170.893	1	238.063	3	.001	3	.732	3	.657	1
376			min	-1532.299	3	-27.814	5	-310.212	4	-.002	2	-.519	2	-.016	5
377		18	max	1689.648	1	1170.893	1	238.063	3	.001	3	.799	3	.329	1
378			min	-1534.215	3	-27.814	5	-307.998	4	-.002	2	-.569	2	-.008	5
379		19	max	1687.093	1	1170.893	1	238.063	3	.001	3	.866	3	0	1
380			min	-1536.131	3	-27.814	5	-305.784	4	-.002	2	-.619	2	0	1
381	M3	1	max	1744.424	2	4.588	4	61.029	2	.019	3	.011	4	0	1
382			min	-620.13	3	1.079	15	-26.797	3	-.04	2	-.003	3	0	1
383		2	max	1744.249	2	4.078	4	61.029	2	.019	3	.023	2	0	15
384			min	-620.261	3	.959	15	-26.797	3	-.04	2	-.011	3	-.001	4
385		3	max	1744.075	2	3.569	4	61.029	2	.019	3	.041	2	0	15
386			min	-620.391	3	.839	15	-26.797	3	-.04	2	-.018	3	-.002	4
387		4	max	1743.901	2	3.059	4	61.029	2	.019	3	.059	2	0	15
388			min	-620.522	3	.719	15	-26.797	3	-.04	2	-.026	3	-.003	4
389		5	max	1743.726	2	2.549	4	61.029	2	.019	3	.077	2	0	15
390			min	-620.653	3	.599	15	-26.797	3	-.04	2	-.034	3	-.004	4
391		6	max	1743.552	2	2.039	4	61.029	2	.019	3	.094	2	-.001	15
392			min	-620.784	3	.479	15	-26.797	3	-.04	2	-.042	3	-.005	4
393		7	max	1743.378	2	1.529	4	61.029	2	.019	3	.112	2	-.001	15
394			min	-620.915	3	.36	15	-26.797	3	-.04	2	-.05	3	-.005	4
395		8	max	1743.203	2	1.02	4	61.029	2	.019	3	.13	2	-.001	15
396			min	-621.045	3	.24	15	-26.797	3	-.04	2	-.058	3	-.006	4
397		9	max	1743.029	2	.51	4	61.029	2	.019	3	.148	2	-.001	15
398			min	-621.176	3	.12	15	-26.797	3	-.04	2	-.065	3	-.006	4
399		10	max	1742.854	2	0	1	61.029	2	.019	3	.166	2	-.001	15
400			min	-621.307	3	0	1	-26.797	3	-.04	2	-.073	3	-.006	4
401		11	max	1742.68	2	-.12	15	61.029	2	.019	3	.184	2	-.001	15
402			min	-621.438	3	-.51	6	-26.797	3	-.04	2	-.081	3	-.006	4
403		12	max	1742.506	2	-.24	15	61.029	2	.019	3	.202	2	-.001	15
404			min	-621.569	3	-1.02	6	-26.797	3	-.04	2	-.089	3	-.006	4
405		13	max	1742.331	2	-.36	15	61.029	2	.019	3	.219	2	-.001	15
406			min	-621.699	3	-1.529	6	-26.797	3	-.04	2	-.097	3	-.005	4
407		14	max	1742.157	2	-.479	15	61.029	2	.019	3	.237	2	-.001	15
408			min	-621.83	3	-2.039	6	-26.797	3	-.04	2	-.105	3	-.005	4
409		15	max	1741.982	2	-.599	15	61.029	2	.019	3	.255	2	0	15
410			min	-621.961	3	-2.549	6	-26.797	3	-.04	2	-.112	3	-.004	4
411		16	max	1741.808	2	-.719	15	61.029	2	.019	3	.273	2	0	15
412			min	-622.092	3	-3.059	6	-26.797	3	-.04	2	-.12	3	-.003	4
413		17	max	1741.634	2	-.839	15	61.029	2	.019	3	.291	2	0	15
414			min	-622.222	3	-3.569	6	-26.797	3	-.04	2	-.128	3	-.002	4
415		18	max	1741.459	2	-.959	15	61.029	2	.019	3	.309	2	0	15
416			min	-622.353	3	-4.078	6	-26.797	3	-.04	2	-.136	3	-.001	4
417		19	max	1741.285	2	-1.079	15	61.029	2	.019	3	.326	2	0	1
418			min	-622.484	3	-4.588	6	-26.797	3	-.04	2	-.144	3	0	1
419	M6	1	max	5002.399	2	4.588	4	0	1	.005	5	.01	4	0	1
420			min	-2141.411	3	1.079	15	-17.046	4	0	1	0	1	0	1
421		2	max	5002.224	2	4.078	4	0	1	.005	5	.005	4	0	15
422			min	-2141.542	3	.959	15	-16.67	4	0	1	0	1	-.001	4
423		3	max	5002.05	2	3.569	4	0	1	.005	5	0	4	0	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
424			min	-2141.672	3	.839	15	-16.294	4	0	1	0	1	-.002	4
425		4	max	5001.875	2	3.059	4	0	1	.005	5	0	1	0	15
426			min	-2141.803	3	.719	15	-15.918	4	0	1	-.004	4	-.003	4
427		5	max	5001.701	2	2.549	4	0	1	.005	5	0	1	0	15
428			min	-2141.934	3	.599	15	-15.542	4	0	1	-.009	4	-.004	4
429		6	max	5001.527	2	2.039	4	0	1	.005	5	0	1	-.001	15
430			min	-2142.065	3	.479	15	-15.166	4	0	1	-.013	4	-.005	4
431		7	max	5001.352	2	1.529	4	0	1	.005	5	0	1	-.001	15
432			min	-2142.196	3	.36	15	-14.79	4	0	1	-.018	4	-.005	4
433		8	max	5001.178	2	1.02	4	0	1	.005	5	0	1	-.001	15
434			min	-2142.326	3	.24	15	-14.414	4	0	1	-.022	4	-.006	4
435		9	max	5001.003	2	.51	4	0	1	.005	5	0	1	-.001	15
436			min	-2142.457	3	.12	15	-14.038	4	0	1	-.026	4	-.006	4
437		10	max	5000.829	2	0	1	0	1	.005	5	0	1	-.001	15
438			min	-2142.588	3	0	1	-13.662	4	0	1	-.03	4	-.006	4
439		11	max	5000.655	2	-.12	15	0	1	.005	5	0	1	-.001	15
440			min	-2142.719	3	-.51	6	-13.286	4	0	1	-.034	4	-.006	4
441		12	max	5000.48	2	-.24	15	0	1	.005	5	0	1	-.001	15
442			min	-2142.85	3	-1.02	6	-12.91	4	0	1	-.038	4	-.006	4
443		13	max	5000.306	2	-.36	15	0	1	.005	5	0	1	-.001	15
444			min	-2142.98	3	-1.529	6	-12.534	4	0	1	-.042	4	-.005	4
445		14	max	5000.132	2	-.479	15	0	1	.005	5	0	1	-.001	15
446			min	-2143.111	3	-2.039	6	-12.158	4	0	1	-.045	4	-.005	4
447		15	max	4999.957	2	-.599	15	0	1	.005	5	0	1	0	15
448			min	-2143.242	3	-2.549	6	-11.782	4	0	1	-.049	4	-.004	4
449		16	max	4999.783	2	-.719	15	0	1	.005	5	0	1	0	15
450			min	-2143.373	3	-3.059	6	-11.406	4	0	1	-.052	4	-.003	4
451		17	max	4999.608	2	-.839	15	0	1	.005	5	0	1	0	15
452			min	-2143.504	3	-3.569	6	-11.03	4	0	1	-.056	4	-.002	4
453		18	max	4999.434	2	-.959	15	0	1	.005	5	0	1	0	15
454			min	-2143.634	3	-4.078	6	-10.654	4	0	1	-.059	4	-.001	4
455		19	max	4999.26	2	-1.079	15	0	1	.005	5	0	1	0	1
456			min	-2143.765	3	-4.588	6	-10.278	4	0	1	-.062	4	0	1
457	M9	1	max	1744.424	2	4.588	6	26.797	3	.04	2	.01	5	0	1
458			min	-620.13	3	1.079	15	-61.029	2	-.019	3	-.005	2	0	1
459		2	max	1744.249	2	4.078	6	26.797	3	.04	2	.011	3	0	15
460			min	-620.261	3	.959	15	-61.029	2	-.019	3	-.023	2	-.001	6
461		3	max	1744.075	2	3.569	6	26.797	3	.04	2	.018	3	0	15
462			min	-620.391	3	.839	15	-61.029	2	-.019	3	-.041	2	-.002	6
463		4	max	1743.901	2	3.059	6	26.797	3	.04	2	.026	3	0	15
464			min	-620.522	3	.719	15	-61.029	2	-.019	3	-.059	2	-.003	6
465		5	max	1743.726	2	2.549	6	26.797	3	.04	2	.034	3	0	15
466			min	-620.653	3	.599	15	-61.029	2	-.019	3	-.077	2	-.004	6
467		6	max	1743.552	2	2.039	6	26.797	3	.04	2	.042	3	-.001	15
468			min	-620.784	3	.479	15	-61.029	2	-.019	3	-.094	2	-.005	6
469		7	max	1743.378	2	1.529	6	26.797	3	.04	2	.05	3	-.001	15
470			min	-620.915	3	.36	15	-61.029	2	-.019	3	-.112	2	-.005	6
471		8	max	1743.203	2	1.02	6	26.797	3	.04	2	.058	3	-.001	15
472			min	-621.045	3	.24	15	-61.029	2	-.019	3	-.13	2	-.006	6
473		9	max	1743.029	2	.51	6	26.797	3	.04	2	.065	3	-.001	15
474			min	-621.176	3	.12	15	-61.029	2	-.019	3	-.148	2	-.006	6
475		10	max	1742.854	2	0	1	26.797	3	.04	2	.073	3	-.001	15
476			min	-621.307	3	0	1	-61.029	2	-.019	3	-.166	2	-.006	6
477		11	max	1742.68	2	-.12	15	26.797	3	.04	2	.081	3	-.001	15
478			min	-621.438	3	-.51	4	-61.029	2	-.019	3	-.184	2	-.006	6
479		12	max	1742.506	2	-.24	15	26.797	3	.04	2	.089	3	-.001	15
480			min	-621.569	3	-1.02	4	-61.029	2	-.019	3	-.202	2	-.006	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
481		13	max	1742.331	2	-.36	15	26.797	3	.04	2	.097	3	-.001	15
482			min	-621.699	3	-1.529	4	-61.029	2	-.019	3	-.219	2	-.005	6
483		14	max	1742.157	2	-.479	15	26.797	3	.04	2	.105	3	-.001	15
484			min	-621.83	3	-2.039	4	-61.029	2	-.019	3	-.237	2	-.005	6
485		15	max	1741.982	2	-.599	15	26.797	3	.04	2	.112	3	0	15
486			min	-621.961	3	-2.549	4	-61.029	2	-.019	3	-.255	2	-.004	6
487		16	max	1741.808	2	-.719	15	26.797	3	.04	2	.12	3	0	15
488			min	-622.092	3	-3.059	4	-61.029	2	-.019	3	-.273	2	-.003	6
489		17	max	1741.634	2	-.839	15	26.797	3	.04	2	.128	3	0	15
490			min	-622.222	3	-3.569	4	-61.029	2	-.019	3	-.291	2	-.002	6
491		18	max	1741.459	2	-.959	15	26.797	3	.04	2	.136	3	0	15
492			min	-622.353	3	-4.078	4	-61.029	2	-.019	3	-.309	2	-.001	6
493		19	max	1741.285	2	-1.079	15	26.797	3	.04	2	.144	3	0	1
494			min	-622.484	3	-4.588	4	-61.029	2	-.019	3	-.326	2	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	-.022	15	.044	3	.024	1	9.867e-3	3	NC	3	NC	3
2			min	-.248	1	-.617	1	-.501	5	-2.529e-2	2	201.939	1	339.67	5
3		2	max	-.022	15	.018	3	.007	1	9.867e-3	3	8535.404	12	NC	3
4			min	-.248	1	-.522	1	-.479	4	-2.529e-2	2	235.704	1	361.084	5
5		3	max	-.022	15	-.006	12	0	12	9.353e-3	3	4262.662	12	NC	2
6			min	-.248	1	-.427	1	-.457	4	-2.345e-2	2	283.083	1	386.634	5
7		4	max	-.022	15	-.02	12	0	12	8.566e-3	3	2904.91	12	NC	1
8			min	-.248	1	-.335	1	-.43	4	-2.062e-2	2	351.099	1	421.657	5
9		5	max	-.022	15	-.021	15	0	3	7.778e-3	3	3063.975	15	NC	1
10			min	-.248	1	-.252	1	-.397	4	-1.78e-2	2	448.542	1	468.868	5
11		6	max	-.022	15	-.017	15	.001	3	7.851e-3	3	3373.487	15	NC	1
12			min	-.248	1	-.184	1	-.363	4	-1.691e-2	2	582.302	1	531.407	5
13		7	max	-.022	15	-.013	15	.002	3	8.519e-3	3	4694.141	10	NC	2
14			min	-.247	1	-.129	1	-.329	4	-1.736e-2	2	764.42	1	611.874	5
15		8	max	-.022	15	-.009	15	0	3	9.187e-3	3	NC	10	NC	2
16			min	-.247	1	-.083	1	-.296	4	-1.781e-2	2	1034.639	1	713.879	5
17		9	max	-.022	15	-.006	15	0	10	1.011e-2	3	NC	2	NC	2
18			min	-.246	1	-.064	3	-.268	4	-1.728e-2	2	1237.827	3	841.82	5
19		10	max	-.022	15	.005	2	0	2	1.149e-2	3	9533.652	11	NC	2
20			min	-.246	1	-.057	3	-.239	4	-1.502e-2	2	1326.937	3	1028.387	5
21		11	max	-.022	15	.034	2	.001	3	1.287e-2	3	NC	1	NC	2
22			min	-.245	1	-.046	3	-.211	4	-1.276e-2	2	1495.502	3	1311.862	5
23		12	max	-.022	15	.068	1	.006	3	1.06e-2	3	NC	9	NC	2
24			min	-.245	1	-.03	3	-.185	4	-9.408e-3	2	1772.914	2	1764.371	5
25		13	max	-.022	15	.095	1	.011	3	6.257e-3	3	NC	9	NC	2
26			min	-.244	1	-.004	3	-.16	4	-5.428e-3	2	1405.814	2	2639.481	5
27		14	max	-.022	15	.112	1	.011	3	2.123e-3	3	NC	3	NC	2
28			min	-.243	1	.01	15	-.138	4	-4.709e-3	4	1288.74	2	4391.03	5
29		15	max	-.022	15	.113	1	.007	3	7.232e-3	3	NC	4	NC	2
30			min	-.243	1	.013	15	-.124	5	-4.377e-3	2	1374.249	2	4817.569	1
31		16	max	-.022	15	.184	3	.01	1	1.234e-2	3	NC	4	NC	3
32			min	-.243	1	.016	15	-.116	5	-7.158e-3	2	954.169	3	4291.49	1
33		17	max	-.022	15	.277	3	.006	1	1.745e-2	3	NC	4	NC	3
34			min	-.244	1	.013	10	-.112	5	-9.938e-3	2	575.661	3	4848.294	1
35		18	max	-.022	15	.373	3	0	12	2.078e-2	3	NC	4	NC	2
36			min	-.244	1	-.003	10	-.111	4	-1.175e-2	2	406.953	3	8923.669	1
37		19	max	-.022	15	.47	3	-.003	12	2.078e-2	3	NC	1	NC	1
38			min	-.244	1	-.019	10	-.112	4	-1.175e-2	2	314.818	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
39	M4	1	max	-.016	15	.223	3	0	1	2.142e-4	4	NC	3	NC	1
40			min	-.513	1	-1.388	1	-.498	4	0	1	100.486	1	342.622	4
41		2	max	-.016	15	.145	3	0	1	2.142e-4	4	3991.795	15	NC	1
42			min	-.513	1	-1.166	1	-.479	4	0	1	120.539	1	359.897	4
43		3	max	-.016	15	.067	3	0	1	6.918e-7	5	4816.503	15	NC	1
44			min	-.513	1	-.943	1	-.458	4	-6.47e-7	14	150.686	1	380.975	4
45		4	max	-.016	15	-.006	12	0	1	0	1	6020.368	15	NC	1
46			min	-.513	1	-.729	1	-.431	4	-3.291e-4	4	198.467	1	413.241	4
47		5	max	-.016	15	-.016	15	0	1	0	1	7788.453	15	NC	1
48			min	-.513	1	-.538	1	-.398	4	-6.58e-4	4	276.784	1	459.462	4
49		6	max	-.016	15	-.012	15	0	1	0	1	NC	15	NC	1
50			min	-.512	1	-.385	1	-.363	4	-6.331e-4	4	404.318	1	522.731	4
51		7	max	-.016	15	-.009	15	0	1	0	1	NC	15	NC	1
52			min	-.511	1	-.269	1	-.328	4	-3.635e-4	4	386.537	3	604.873	4
53		8	max	-.016	15	-.006	15	0	1	0	1	NC	2	NC	1
54			min	-.509	1	-.175	1	-.296	4	-9.384e-5	4	381.906	3	707.292	4
55		9	max	-.016	15	-.003	15	0	1	2.224e-5	5	NC	5	NC	1
56			min	-.508	1	-.124	3	-.268	4	0	1	386.147	3	829.765	4
57		10	max	-.016	15	.003	10	0	1	0	1	NC	4	NC	1
58			min	-.507	1	-.115	3	-.239	4	-1.337e-4	4	396.375	3	1013.382	4
59		11	max	-.016	15	.071	1	0	1	0	1	NC	4	NC	1
60			min	-.506	1	-.099	3	-.21	4	-2.896e-4	4	416.89	3	1290.275	4
61		12	max	-.016	15	.144	1	0	1	0	1	NC	5	NC	1
62			min	-.504	1	-.073	3	-.185	4	-1.339e-3	4	453.704	3	1700.15	4
63		13	max	-.016	15	.202	1	0	1	0	1	NC	5	NC	1
64			min	-.503	1	-.024	3	-.161	4	-2.894e-3	4	427.825	2	2473.689	4
65		14	max	-.016	15	.229	1	0	1	0	1	NC	5	NC	1
66			min	-.501	1	.007	15	-.141	4	-4.39e-3	4	405.455	2	3918.492	4
67		15	max	-.016	15	.22	3	0	1	0	1	NC	3	NC	1
68			min	-.501	1	.007	15	-.128	4	-3.299e-3	4	439.767	2	6342.386	4
69		16	max	-.016	15	.416	3	0	1	0	1	NC	5	NC	1
70			min	-.502	1	.006	15	-.119	4	-2.208e-3	4	542.677	2	NC	1
71		17	max	-.016	15	.639	3	0	1	0	1	NC	5	NC	1
72			min	-.502	1	.005	15	-.114	4	-1.117e-3	4	321.705	3	NC	1
73		18	max	-.016	15	.873	3	0	1	0	1	NC	4	NC	1
74			min	-.502	1	-.049	2	-.11	4	-4.06e-4	4	206.13	3	NC	1
75		19	max	-.016	15	1.106	3	0	1	0	1	NC	1	NC	1
76			min	-.502	1	-.134	2	-.106	4	-4.06e-4	4	151.762	3	NC	1
77	M7	1	max	.006	5	.044	3	-.001	12	2.529e-2	2	NC	3	NC	3
78			min	-.248	1	-.617	1	-.511	4	-9.867e-3	3	201.939	1	326.687	4
79		2	max	.006	5	.018	3	0	12	2.529e-2	2	NC	5	NC	3
80			min	-.248	1	-.522	1	-.483	4	-9.867e-3	3	235.704	1	351.243	4
81		3	max	.006	5	.002	5	.007	1	2.345e-2	2	NC	5	NC	2
82			min	-.248	1	-.427	1	-.454	4	-9.353e-3	3	283.083	1	380.217	4
83		4	max	.006	5	.003	5	.013	1	2.062e-2	2	NC	5	NC	1
84			min	-.248	1	-.335	1	-.423	5	-8.566e-3	3	351.099	1	416.471	4
85		5	max	.006	5	.004	5	.014	1	1.78e-2	2	NC	5	NC	1
86			min	-.248	1	-.252	1	-.391	5	-7.778e-3	3	448.542	1	462.567	4
87		6	max	.006	5	.005	5	.011	1	1.691e-2	2	NC	5	NC	1
88			min	-.248	1	-.184	1	-.358	4	-7.851e-3	3	582.302	1	521.425	4
89		7	max	.006	5	.005	5	.005	1	1.736e-2	2	NC	4	NC	2
90			min	-.247	1	-.129	1	-.327	4	-8.519e-3	3	764.42	1	594.331	4
91		8	max	.006	5	.004	5	.001	2	1.781e-2	2	NC	4	NC	2
92			min	-.247	1	-.083	1	-.297	4	-9.187e-3	3	1034.639	1	685.934	4
93		9	max	.006	5	.003	5	0	3	1.728e-2	2	NC	2	NC	2
94			min	-.246	1	-.064	3	-.268	4	-1.011e-2	3	1237.827	3	804.424	4
95		10	max	.006	5	.005	2	0	3	1.502e-2	2	NC	4	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
96			min	-.246	1	-.057	3	-.239	4	-1.149e-2	3	1326.937	3	972.876	4
97		11	max	.006	5	.034	2	0	2	1.276e-2	2	NC	1	NC	2
98			min	-.245	1	-.046	3	-.21	4	-1.287e-2	3	1495.502	3	1226.549	4
99		12	max	.006	5	.068	1	.006	1	9.408e-3	2	NC	5	NC	2
100			min	-.245	1	-.03	3	-.183	4	-1.06e-2	3	1772.914	2	1640.221	4
101		13	max	.006	5	.095	1	.007	2	5.428e-3	2	NC	5	NC	2
102			min	-.244	1	-.004	3	-.158	4	-6.257e-3	3	1405.814	2	2371.824	4
103		14	max	.006	5	.112	1	.004	2	1.618e-3	1	NC	3	NC	2
104			min	-.243	1	-.003	5	-.139	4	-4.317e-3	5	1288.74	2	3542.604	4
105		15	max	.006	5	.113	1	0	10	4.377e-3	2	NC	5	NC	2
106			min	-.243	1	-.006	5	-.128	4	-7.232e-3	3	1374.249	2	4817.569	1
107		16	max	.006	5	.184	3	-.001	10	7.158e-3	2	NC	5	NC	3
108			min	-.243	1	-.01	5	-.121	4	-1.234e-2	3	954.169	3	4291.49	1
109		17	max	.006	5	.277	3	-.001	12	9.938e-3	2	NC	4	NC	3
110			min	-.244	1	-.015	5	-.115	4	-1.745e-2	3	575.661	3	4848.294	1
111		18	max	.006	5	.373	3	.006	1	1.175e-2	2	NC	4	NC	2
112			min	-.244	1	-.019	5	-.108	5	-2.078e-2	3	406.953	3	8923.669	1
113		19	max	.006	5	.47	3	.021	1	1.175e-2	2	NC	1	NC	1
114			min	-.244	1	-.024	5	-.104	5	-2.078e-2	3	314.818	3	NC	1
115	M10	1	max	.001	1	.34	3	.244	1	1.295e-2	3	NC	1	NC	1
116			min	-.111	4	-.018	5	-.006	5	-3.684e-3	2	NC	1	NC	1
117		2	max	0	1	.611	3	.292	1	1.498e-2	3	NC	4	NC	3
118			min	-.111	4	-.13	2	0	15	-4.535e-3	2	841.461	3	4706.382	1
119		3	max	0	1	.861	3	.366	1	1.702e-2	3	NC	5	NC	3
120			min	-.111	4	-.264	2	.005	15	-5.386e-3	2	437.321	3	1855.559	1
121		4	max	0	1	1.049	3	.443	1	1.906e-2	3	NC	5	NC	5
122			min	-.111	4	-.354	2	.008	15	-6.237e-3	2	321.345	3	1144.974	1
123		5	max	0	1	1.151	3	.504	1	2.11e-2	3	NC	5	NC	5
124			min	-.111	4	-.385	2	.011	15	-7.088e-3	2	280.906	3	875.817	1
125		6	max	0	1	1.162	3	.54	1	2.313e-2	3	NC	5	NC	5
126			min	-.111	4	-.355	2	.012	15	-7.939e-3	2	277.409	3	768.076	1
127		7	max	0	1	1.092	3	.55	1	2.517e-2	3	NC	5	NC	5
128			min	-.111	4	-.275	2	.012	15	-8.79e-3	2	303.105	3	744.29	1
129		8	max	0	1	.972	3	.537	1	2.721e-2	3	NC	4	NC	5
130			min	-.111	4	-.167	2	.012	15	-9.641e-3	2	360.459	3	776.29	1
131		9	max	0	1	.85	3	.515	1	2.925e-2	3	NC	4	NC	5
132			min	-.111	4	-.066	2	.013	15	-1.049e-2	2	446.516	3	840.867	1
133		10	max	0	1	.792	3	.502	1	3.128e-2	3	NC	4	NC	5
134			min	-.111	4	-.025	10	.016	15	-1.134e-2	2	504.228	3	883.317	1
135		11	max	0	10	.85	3	.515	1	2.925e-2	3	NC	4	NC	5
136			min	-.111	4	-.066	2	.019	15	-1.049e-2	2	446.516	3	840.867	1
137		12	max	0	10	.972	3	.537	1	2.721e-2	3	NC	4	NC	5
138			min	-.111	4	-.167	2	.023	15	-9.641e-3	2	360.459	3	776.29	1
139		13	max	0	10	1.092	3	.55	1	2.517e-2	3	NC	4	NC	5
140			min	-.111	4	-.275	2	.025	15	-8.79e-3	2	303.105	3	744.29	1
141		14	max	0	10	1.162	3	.54	1	2.313e-2	3	NC	5	NC	5
142			min	-.111	4	-.355	2	.025	15	-7.939e-3	2	277.409	3	768.076	1
143		15	max	0	10	1.151	3	.504	1	2.11e-2	3	NC	5	NC	5
144			min	-.111	4	-.385	2	.025	15	-7.088e-3	2	280.906	3	875.817	1
145		16	max	0	10	1.049	3	.443	1	1.906e-2	3	NC	5	NC	5
146			min	-.111	4	-.354	2	.023	15	-6.237e-3	2	321.345	3	1144.974	1
147		17	max	0	10	.861	3	.366	1	1.702e-2	3	NC	4	NC	3
148			min	-.111	4	-.264	2	.022	15	-5.386e-3	2	437.321	3	1855.559	1
149		18	max	0	10	.611	3	.292	1	1.498e-2	3	NC	4	NC	3
150			min	-.111	4	-.13	2	.021	15	-4.535e-3	2	841.461	3	4706.382	1
151		19	max	0	10	.34	3	.244	1	1.295e-2	3	NC	1	NC	1
152			min	-.111	4	.003	10	.022	15	-3.684e-3	2	4772.772	4	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
153	M11	1	max	.002	1	.047	1	.245	1	4.563e-3	1	NC	1	NC	1
154			min	-.2	4	-.04	3	-.006	5	-1.44e-4	5	NC	1	NC	1
155		2	max	.002	1	.139	3	.282	1	5.154e-3	1	NC	4	NC	3
156			min	-.2	4	-.106	2	.018	15	-7.502e-5	5	1269.619	3	5938.469	4
157		3	max	.002	1	.304	3	.351	1	5.745e-3	1	NC	5	NC	3
158			min	-.201	4	-.233	2	.027	15	-1.212e-5	15	661.957	3	2155.387	1
159		4	max	.002	1	.414	3	.425	1	6.335e-3	1	NC	5	NC	3
160			min	-.201	4	-.311	2	.026	15	3.363e-5	15	501.991	3	1262.943	1
161		5	max	.001	1	.446	3	.488	1	6.926e-3	1	NC	5	NC	3
162			min	-.201	4	-.328	2	.019	15	7.938e-5	15	468.765	3	936.521	1
163		6	max	.001	1	.396	3	.529	1	7.517e-3	1	NC	5	NC	5
164			min	-.201	4	-.283	2	.008	15	1.251e-4	15	522.415	3	803.272	1
165		7	max	0	1	.277	3	.543	1	8.108e-3	1	NC	5	NC	5
166			min	-.201	4	-.188	2	-.002	15	1.709e-4	15	717.755	3	764.485	1
167		8	max	0	1	.121	3	.535	1	8.699e-3	1	NC	4	NC	5
168			min	-.201	4	-.067	2	-.009	5	2.166e-4	15	1413.845	3	784.904	1
169		9	max	0	1	.049	1	.517	1	9.29e-3	1	NC	1	NC	5
170			min	-.201	4	-.024	3	-.003	5	2.624e-4	15	NC	1	839.301	1
171		10	max	0	1	.098	1	.505	1	9.881e-3	1	NC	4	NC	5
172			min	-.201	4	-.09	3	.016	15	3.081e-4	15	4485.386	1	876.517	1
173		11	max	0	3	.049	1	.517	1	9.29e-3	1	NC	1	9041.356	15
174			min	-.201	4	-.024	3	.035	15	3.222e-4	15	NC	1	839.301	1
175		12	max	0	3	.121	3	.535	1	8.699e-3	1	NC	4	7555.791	15
176			min	-.201	4	-.067	2	.042	15	3.362e-4	15	1413.845	3	784.904	1
177		13	max	0	3	.277	3	.543	1	8.108e-3	1	NC	5	9079.337	15
178			min	-.201	4	-.188	2	.038	15	3.503e-4	15	717.755	3	764.485	1
179		14	max	.001	3	.396	3	.529	1	7.517e-3	1	NC	5	NC	5
180			min	-.201	4	-.283	2	.028	15	3.643e-4	15	522.415	3	803.272	1
181		15	max	.001	3	.446	3	.488	1	6.926e-3	1	NC	15	NC	3
182			min	-.201	4	-.328	2	.015	15	3.784e-4	15	468.765	3	936.521	1
183		16	max	.002	3	.414	3	.425	1	6.335e-3	1	NC	15	NC	3
184			min	-.201	4	-.311	2	.004	15	3.925e-4	15	501.991	3	1262.943	1
185		17	max	.002	3	.304	3	.351	1	5.745e-3	1	NC	15	NC	3
186			min	-.201	4	-.233	2	-.003	5	4.065e-4	15	661.957	3	2155.387	1
187		18	max	.002	3	.139	3	.282	1	5.154e-3	1	NC	5	NC	3
188			min	-.201	4	-.106	2	.002	15	4.206e-4	15	1269.619	3	6131.015	1
189		19	max	.003	3	.047	1	.245	1	4.563e-3	1	NC	1	NC	1
190			min	-.201	4	-.04	3	.022	15	4.346e-4	15	NC	1	NC	1
191	M12	1	max	0	2	.004	5	.246	1	5.531e-3	1	NC	1	NC	1
192			min	-.278	4	-.066	3	-.006	5	-9.754e-5	5	NC	1	NC	1
193		2	max	0	2	.049	3	.277	1	6.177e-3	1	NC	5	NC	2
194			min	-.278	4	-.267	2	.019	15	-2.592e-5	15	995.518	2	5798.371	4
195		3	max	0	2	.138	3	.343	1	6.824e-3	1	NC	5	NC	3
196			min	-.278	4	-.464	2	.029	15	2.17e-5	15	535.303	2	2368.983	1
197		4	max	0	2	.187	3	.417	1	7.471e-3	1	NC	5	NC	3
198			min	-.278	4	-.593	2	.027	15	6.933e-5	15	411.104	2	1338.998	1
199		5	max	0	2	.19	3	.481	1	8.117e-3	1	NC	5	NC	12
200			min	-.278	4	-.635	2	.019	15	1.17e-4	15	382.351	2	972.953	1
201		6	max	0	2	.15	3	.523	1	8.764e-3	1	NC	5	NC	5
202			min	-.278	4	-.588	2	.007	15	1.646e-4	15	414.814	2	822.866	1
203		7	max	0	2	.077	3	.541	1	9.41e-3	1	NC	5	NC	5
204			min	-.278	4	-.469	2	-.005	5	2.122e-4	15	529.553	2	774.396	1
205		8	max	0	2	-.005	15	.536	1	1.006e-2	1	NC	5	NC	5
206			min	-.278	4	-.311	2	-.013	5	2.598e-4	15	837.22	2	787.417	1
207		9	max	0	2	-.004	15	.519	1	1.07e-2	1	NC	4	NC	5
208			min	-.278	4	-.179	1	-.006	5	3.075e-4	15	1815.004	2	835.375	1
209		10	max	0	1	-.004	15	.509	1	1.135e-2	1	NC	4	NC	5

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
210			min	-.278	4	-.126	3	.016	15	3.551e-4	15	3501.631	1	869.304	1
211		11	max	0	9	-.006	15	.519	1	1.07e-2	1	NC	4	8386.504	15
212			min	-.278	4	-.179	1	.037	15	3.67e-4	15	1815.004	2	835.375	1
213		12	max	0	9	-.008	12	.536	1	1.006e-2	1	NC	5	7122.527	12
214			min	-.278	4	-.311	2	.044	15	3.79e-4	15	837.22	2	787.417	1
215		13	max	0	9	.077	3	.541	1	9.41e-3	1	NC	5	8363.227	15
216			min	-.278	4	-.469	2	.04	15	3.91e-4	15	529.553	2	774.396	1
217		14	max	0	9	.15	3	.523	1	8.764e-3	1	NC	15	NC	5
218			min	-.278	4	-.588	2	.029	15	4.001e-4	12	414.814	2	822.866	1
219		15	max	0	9	.19	3	.481	1	8.117e-3	1	NC	15	NC	5
220			min	-.278	4	-.635	2	.015	15	3.98e-4	12	382.351	2	972.953	1
221		16	max	0	9	.187	3	.417	1	7.471e-3	1	NC	15	NC	3
222			min	-.278	4	-.593	2	.003	15	3.96e-4	12	411.104	2	1338.998	1
223		17	max	0	9	.138	3	.343	1	6.824e-3	1	NC	5	NC	3
224			min	-.278	4	-.464	2	-.005	5	3.939e-4	12	535.303	2	2368.983	1
225		18	max	0	9	.049	3	.277	1	6.177e-3	1	NC	5	NC	2
226			min	-.278	4	-.267	2	0	15	3.919e-4	12	995.518	2	7389.022	1
227		19	max	0	9	-.007	15	.246	1	5.531e-3	1	NC	1	NC	1
228			min	-.278	4	-.066	3	.022	15	3.898e-4	12	NC	1	NC	1
229	M13	1	max	0	12	.01	3	.248	1	1.28e-2	2	NC	1	NC	1
230			min	-.473	4	-.489	1	-.006	5	-3.425e-3	3	NC	1	NC	1
231		2	max	0	12	.133	3	.299	1	1.487e-2	2	NC	5	NC	3
232			min	-.473	4	-.774	1	.018	15	-4.201e-3	3	711.946	2	4466.169	1
233		3	max	0	12	.239	3	.375	1	1.695e-2	2	NC	5	NC	3
234			min	-.473	4	-1.054	2	.028	15	-4.977e-3	3	375.742	2	1790.181	1
235		4	max	0	12	.311	3	.453	1	1.902e-2	2	NC	5	NC	3
236			min	-.473	4	-1.268	2	.029	15	-5.753e-3	3	277.672	2	1112.804	1
237		5	max	0	12	.34	3	.515	1	2.109e-2	2	NC	15	NC	12
238			min	-.473	4	-1.389	2	.023	15	-6.529e-3	3	242.04	2	854.403	1
239		6	max	0	12	.328	3	.552	1	2.316e-2	2	NC	15	NC	5
240			min	-.473	4	-1.413	2	.014	15	-7.305e-3	3	236.122	2	750.62	1
241		7	max	0	12	.28	3	.561	1	2.523e-2	2	NC	15	NC	5
242			min	-.473	4	-1.353	2	.005	15	-8.081e-3	3	251.812	2	727.654	1
243		8	max	0	12	.212	3	.549	1	2.731e-2	2	NC	15	NC	5
244			min	-.472	4	-1.239	2	0	15	-8.857e-3	3	287.752	2	758.379	1
245		9	max	0	12	.148	3	.526	1	2.938e-2	2	NC	15	NC	5
246			min	-.472	4	-1.136	1	.002	15	-9.633e-3	3	338.008	2	820.254	1
247		10	max	0	1	.118	3	.513	1	3.145e-2	2	NC	15	NC	5
248			min	-.472	4	-1.089	1	.016	15	-1.041e-2	3	369.197	2	860.815	1
249		11	max	0	1	.148	3	.526	1	2.938e-2	2	NC	15	NC	15
250			min	-.472	4	-1.136	1	.031	15	-9.633e-3	3	338.008	2	820.254	1
251		12	max	0	1	.212	3	.549	1	2.731e-2	2	NC	15	9475.889	15
252			min	-.472	4	-1.239	2	.036	15	-8.857e-3	3	287.752	2	758.379	1
253		13	max	0	1	.28	3	.561	1	2.523e-2	2	NC	15	NC	15
254			min	-.472	4	-1.353	2	.032	15	-8.081e-3	3	251.812	2	727.654	1
255		14	max	0	1	.328	3	.552	1	2.316e-2	2	9564.644	15	NC	5
256			min	-.472	4	-1.413	2	.024	15	-7.305e-3	3	236.122	2	750.62	1
257		15	max	0	1	.34	3	.515	1	2.109e-2	2	9568.97	15	NC	5
258			min	-.472	4	-1.389	2	.013	15	-6.529e-3	3	242.04	2	854.403	1
259		16	max	0	1	.311	3	.453	1	1.902e-2	2	NC	15	NC	3
260			min	-.472	4	-1.268	2	.003	15	-5.753e-3	3	277.672	2	1112.804	1
261		17	max	.001	1	.239	3	.375	1	1.695e-2	2	NC	15	NC	3
262			min	-.472	4	-1.054	2	-.001	15	-4.977e-3	3	375.742	2	1790.181	1
263		18	max	.001	1	.133	3	.299	1	1.487e-2	2	NC	5	NC	3
264			min	-.472	4	-.774	1	.004	15	-4.201e-3	3	711.946	2	4466.169	1
265		19	max	.001	1	.01	3	.248	1	1.28e-2	2	NC	1	NC	1
266			min	-.472	4	-.489	1	.022	15	-3.425e-3	3	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	5	2.69e-3	2	NC	1	NC	1
270			min	0	1	-.001	1	0	1	-2.756e-3	5	NC	1	NC	1
271		3	max	0	3	0	15	.003	5	5.381e-3	2	NC	1	NC	1
272			min	0	1	-.004	1	0	1	-5.512e-3	5	NC	1	NC	1
273		4	max	0	3	0	15	.006	5	6.301e-3	2	NC	3	NC	1
274			min	0	1	-.01	1	-.001	1	-6.646e-3	5	6236.192	1	NC	1
275		5	max	0	3	-.002	15	.01	5	5.783e-3	2	NC	4	NC	1
276			min	0	1	-.017	1	-.002	1	-6.461e-3	5	3486.547	1	5875.39	5
277		6	max	0	3	-.003	15	.016	5	5.266e-3	2	NC	5	NC	1
278			min	0	1	-.027	1	-.003	1	-6.277e-3	5	2242.338	1	3867.732	5
279		7	max	0	3	-.004	15	.022	5	4.749e-3	2	NC	5	NC	1
280			min	0	1	-.039	1	-.004	1	-6.092e-3	5	1574.117	1	2761.128	5
281		8	max	0	3	-.005	15	.029	5	4.231e-3	2	NC	15	NC	1
282			min	0	1	-.052	1	-.005	1	-5.908e-3	5	1173.099	1	2085.096	5
283		9	max	0	3	-.006	15	.037	5	3.714e-3	2	9935.979	15	NC	1
284			min	0	1	-.066	1	-.005	1	-5.723e-3	5	913.12	1	1641.068	5
285		10	max	0	3	-.008	15	.045	5	3.197e-3	2	8028.817	15	NC	9
286			min	0	1	-.082	1	-.006	1	-5.539e-3	5	734.686	1	1333.261	5
287		11	max	0	3	-.009	15	.055	5	2.679e-3	2	6653.39	15	NC	9
288			min	0	1	-.1	1	-.007	1	-5.354e-3	5	606.769	1	1110.865	5
289		12	max	0	3	-.011	15	.064	5	2.162e-3	2	5628.187	15	NC	9
290			min	-.001	1	-.118	1	-.007	1	-5.17e-3	5	511.88	1	944.852	5
291		13	max	0	3	-.013	15	.074	5	1.645e-3	2	4843.048	15	NC	9
292			min	-.001	1	-.138	1	-.007	1	-4.986e-3	5	439.495	1	817.576	5
293		14	max	.001	3	-.014	15	.084	5	1.127e-3	2	4228.163	15	NC	9
294			min	-.001	1	-.158	1	-.007	1	-4.801e-3	5	382.99	1	717.836	5
295		15	max	.001	3	-.016	15	.095	5	6.101e-4	2	3737.467	15	NC	9
296			min	-.001	1	-.179	1	-.006	1	-4.673e-3	4	338.022	1	638.231	5
297		16	max	.001	3	-.018	15	.106	5	5.992e-4	3	3339.694	15	NC	9
298			min	-.001	1	-.201	1	-.005	1	-4.549e-3	4	301.656	1	573.728	5
299		17	max	.001	3	-.02	15	.117	4	8.791e-4	3	3012.889	15	NC	1
300			min	-.002	1	-.223	1	-.003	1	-4.425e-3	4	271.839	1	519.619	4
301		18	max	.001	3	-.022	15	.128	4	1.159e-3	3	2741.273	15	NC	1
302			min	-.002	1	-.245	1	-.006	3	-4.301e-3	4	247.103	1	474.595	4
303		19	max	.001	3	-.024	15	.139	4	1.439e-3	3	2513.288	15	NC	1
304			min	-.002	1	-.268	1	-.011	3	-4.177e-3	4	226.373	1	436.828	4
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	4	0	1	NC	1	NC	1
308			min	0	2	-.002	1	0	1	-2.925e-3	4	NC	1	NC	1
309		3	max	0	3	0	15	.003	4	0	1	NC	3	NC	1
310			min	0	2	-.008	1	0	1	-5.849e-3	4	7488.946	1	NC	1
311		4	max	0	3	0	15	.006	4	0	1	NC	4	NC	1
312			min	0	2	-.019	1	0	1	-7.041e-3	4	3178.543	1	9683.812	4
313		5	max	.001	3	-.001	15	.011	4	0	1	NC	5	NC	1
314			min	-.001	2	-.035	1	0	1	-6.826e-3	4	1748.738	1	5620.553	4
315		6	max	.001	3	-.002	15	.016	4	0	1	NC	5	NC	1
316			min	-.001	2	-.054	1	0	1	-6.61e-3	4	1114.602	1	3702.857	4
317		7	max	.001	3	-.002	15	.023	4	0	1	NC	5	NC	1
318			min	-.002	1	-.078	1	0	1	-6.395e-3	4	777.976	1	2645.75	4
319		8	max	.002	3	-.003	15	.03	4	0	1	NC	5	NC	1
320			min	-.002	1	-.105	1	0	1	-6.179e-3	4	577.49	1	1999.927	4
321		9	max	.002	3	-.004	15	.038	4	0	1	NC	15	NC	1
322			min	-.002	1	-.135	1	0	1	-5.964e-3	4	448.211	1	1575.735	4
323		10	max	.002	3	-.005	15	.047	4	0	1	NC	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
324			min	-.002	1	-.168	1	0	1	-5.748e-3	4	359.834	1	1281.689	4
325		11	max	.002	3	-.006	15	.057	4	0	1	9442.369	15	NC	1
326			min	-.003	1	-.204	1	0	1	-5.533e-3	4	296.673	1	1069.257	4
327		12	max	.003	3	-.008	15	.067	4	0	1	7965.915	15	NC	1
328			min	-.003	1	-.242	1	0	1	-5.317e-3	4	249.934	1	910.711	4
329		13	max	.003	3	-.009	15	.077	4	0	1	6839.577	15	NC	1
330			min	-.003	1	-.283	1	0	1	-5.102e-3	4	214.35	1	789.198	4
331		14	max	.003	3	-.01	15	.087	4	0	1	5960.328	15	NC	1
332			min	-.003	1	-.325	1	0	1	-4.886e-3	4	186.619	1	694.018	4
333		15	max	.003	3	-.012	15	.098	4	0	1	5260.578	15	NC	1
334			min	-.004	1	-.368	1	0	1	-4.671e-3	4	164.581	1	618.105	4
335		16	max	.004	3	-.013	15	.109	4	0	1	4694.67	15	NC	1
336			min	-.004	1	-.413	1	0	1	-4.456e-3	4	146.779	1	556.652	4
337		17	max	.004	3	-.014	15	.12	4	0	1	4230.674	15	NC	1
338			min	-.004	1	-.458	1	0	1	-4.24e-3	4	132.199	1	506.28	4
339		18	max	.004	3	-.016	15	.13	4	0	1	3845.728	15	NC	1
340			min	-.004	1	-.505	1	0	1	-4.025e-3	4	120.114	1	464.563	4
341		19	max	.004	3	-.017	15	.141	4	0	1	3523.133	15	NC	1
342			min	-.005	1	-.551	1	0	1	-3.809e-3	4	109.994	1	429.724	4
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	5	0	4	1.191e-3	3	NC	1	NC	1
346			min	0	1	-.001	1	0	3	-3.212e-3	4	NC	1	NC	1
347		3	max	0	3	0	5	.003	4	2.381e-3	3	NC	1	NC	1
348			min	0	1	-.004	1	0	3	-6.425e-3	4	NC	1	NC	1
349		4	max	0	3	0	5	.006	4	2.76e-3	3	NC	3	NC	1
350			min	0	1	-.01	1	-.001	3	-7.708e-3	4	6236.192	1	9604.637	4
351		5	max	0	3	0	5	.011	4	2.48e-3	3	NC	4	NC	1
352			min	0	1	-.017	1	-.002	3	-7.425e-3	4	3486.547	1	5583.105	4
353		6	max	0	3	0	5	.016	4	2.2e-3	3	NC	4	NC	1
354			min	0	1	-.027	1	-.003	3	-7.142e-3	4	2242.338	1	3682.775	4
355		7	max	0	3	.001	5	.023	4	1.92e-3	3	NC	4	NC	1
356			min	0	1	-.039	1	-.004	3	-6.859e-3	4	1574.117	1	2634.425	4
357		8	max	0	3	.001	5	.03	4	1.64e-3	3	NC	5	NC	1
358			min	0	1	-.052	1	-.005	3	-6.576e-3	4	1173.099	1	1993.602	4
359		9	max	0	3	.002	5	.039	4	1.361e-3	3	NC	5	NC	1
360			min	0	1	-.066	1	-.006	3	-6.293e-3	4	913.12	1	1572.53	4
361		10	max	0	3	.002	5	.047	4	1.081e-3	3	NC	5	NC	9
362			min	0	1	-.082	1	-.006	3	-6.01e-3	4	734.686	1	1280.572	4
363		11	max	0	3	.003	5	.057	4	8.006e-4	3	NC	5	NC	9
364			min	0	1	-.1	1	-.006	3	-5.727e-3	4	606.769	1	1069.62	4
365		12	max	0	3	.003	5	.066	4	5.207e-4	3	NC	5	NC	9
366			min	-.001	1	-.118	1	-.006	3	-5.444e-3	4	511.88	1	912.176	4
367		13	max	0	3	.004	5	.077	4	2.407e-4	3	NC	5	NC	9
368			min	-.001	1	-.138	1	-.006	3	-5.161e-3	4	439.495	1	791.522	4
369		14	max	.001	3	.004	5	.087	4	-2.512e-5	12	NC	5	NC	9
370			min	-.001	1	-.158	1	-.004	3	-4.878e-3	4	382.99	1	697.043	4
371		15	max	.001	3	.005	5	.097	4	8.963e-5	9	NC	5	NC	9
372			min	-.001	1	-.179	1	-.003	3	-4.6e-3	5	338.022	1	621.729	4
373		16	max	.001	3	.005	5	.108	4	2.87e-4	1	NC	5	NC	9
374			min	-.001	1	-.201	1	0	3	-4.379e-3	5	301.656	1	560.807	4
375		17	max	.001	3	.006	5	.119	4	7.701e-4	1	NC	5	NC	1
376			min	-.002	1	-.223	1	0	10	-4.159e-3	5	271.839	1	510.926	4
377		18	max	.001	3	.006	5	.129	4	1.253e-3	1	NC	7	NC	1
378			min	-.002	1	-.245	1	-.001	2	-3.939e-3	5	247.103	1	469.678	4
379		19	max	.001	3	.007	5	.139	4	1.736e-3	1	NC	15	NC	1
380			min	-.002	1	-.268	1	-.004	2	-3.719e-3	5	226.373	1	435.302	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
381	M3	1	max	.006	1	0	15	.004	5	2.505e-3	2	NC	1	NC	1
382			min	0	15	-.003	1	0	1	-1.86e-3	5	NC	1	NC	1
383		2	max	.005	1	-.002	15	.027	5	2.981e-3	2	NC	1	NC	4
384			min	0	15	-.022	1	-.022	2	-1.884e-3	5	NC	1	2887.089	2
385		3	max	.005	1	-.004	15	.05	5	3.457e-3	2	NC	1	NC	4
386			min	0	15	-.041	1	-.043	2	-1.907e-3	5	NC	1	1460.28	2
387		4	max	.004	1	-.006	15	.074	5	3.933e-3	2	NC	1	NC	4
388			min	0	15	-.06	1	-.063	2	-1.93e-3	5	NC	1	990.943	2
389		5	max	.004	1	-.007	15	.097	5	4.409e-3	2	NC	1	NC	4
390			min	0	15	-.078	1	-.082	2	-1.953e-3	5	NC	1	761.477	2
391		6	max	.004	3	-.009	15	.12	5	4.885e-3	2	NC	1	NC	4
392			min	0	10	-.097	1	-.098	2	-2.137e-3	3	NC	1	628.56	2
393		7	max	.004	3	-.011	15	.143	5	5.361e-3	2	NC	1	NC	4
394			min	0	10	-.116	1	-.113	2	-2.365e-3	3	NC	1	544.635	2
395		8	max	.004	3	-.012	15	.166	5	5.837e-3	2	NC	1	NC	4
396			min	0	10	-.134	1	-.126	2	-2.594e-3	3	NC	1	489.584	2
397		9	max	.004	3	-.014	15	.188	5	6.312e-3	2	NC	1	NC	4
398			min	0	10	-.153	1	-.136	2	-2.822e-3	3	NC	1	453.689	2
399		10	max	.004	3	-.016	15	.21	5	6.788e-3	2	NC	1	NC	4
400			min	-.001	2	-.171	1	-.142	2	-3.051e-3	3	NC	1	432.011	2
401		11	max	.005	3	-.017	15	.232	5	7.264e-3	2	NC	1	NC	4
402			min	-.002	2	-.19	1	-.145	2	-3.279e-3	3	NC	1	422.26	2
403		12	max	.005	3	-.019	15	.253	5	7.74e-3	2	NC	1	NC	4
404			min	-.002	2	-.208	1	-.144	2	-3.508e-3	3	NC	1	424.025	2
405		13	max	.005	3	-.02	15	.273	5	8.216e-3	2	NC	1	NC	4
406			min	-.003	2	-.226	1	-.138	2	-3.736e-3	3	NC	1	438.783	2
407		14	max	.005	3	-.022	15	.293	5	8.692e-3	2	NC	1	NC	4
408			min	-.003	2	-.244	1	-.128	2	-3.965e-3	3	NC	1	470.786	2
409		15	max	.006	3	-.023	15	.312	5	9.168e-3	2	NC	1	NC	4
410			min	-.004	2	-.262	1	-.112	2	-4.193e-3	3	NC	1	479.554	14
411		16	max	.006	3	-.025	15	.33	5	9.644e-3	2	NC	1	NC	4
412			min	-.005	2	-.28	1	-.091	2	-4.422e-3	3	NC	1	431.403	14
413		17	max	.006	3	-.026	15	.347	5	1.012e-2	2	NC	1	NC	4
414			min	-.005	2	-.297	1	-.064	2	-4.65e-3	3	NC	1	389.49	14
415		18	max	.006	3	-.028	15	.364	5	1.06e-2	2	NC	1	NC	4
416			min	-.006	2	-.315	1	-.031	2	-4.879e-3	3	NC	1	352.768	14
417		19	max	.006	3	-.029	15	.384	4	1.107e-2	2	NC	1	NC	1
418			min	-.006	2	-.333	1	0	3	-5.107e-3	3	NC	1	320.417	14
419	M6	1	max	.011	1	0	15	.004	4	0	1	NC	1	NC	1
420			min	0	15	-.006	1	0	1	-1.988e-3	4	NC	1	NC	1
421		2	max	.01	1	-.002	15	.029	4	0	1	NC	1	NC	1
422			min	0	15	-.045	1	0	1	-2.047e-3	4	NC	1	NC	1
423		3	max	.008	1	-.003	15	.053	4	0	1	NC	1	NC	1
424			min	0	15	-.083	1	0	1	-2.106e-3	4	NC	1	9167.504	4
425		4	max	.007	3	-.004	15	.078	4	0	1	NC	1	NC	1
426			min	0	15	-.122	1	0	1	-2.164e-3	4	NC	1	6073.58	4
427		5	max	.008	3	-.006	15	.102	4	0	1	NC	1	NC	1
428			min	0	15	-.161	1	0	1	-2.223e-3	4	NC	1	4572.036	4
429		6	max	.009	3	-.007	15	.127	4	0	1	NC	1	NC	1
430			min	0	10	-.2	1	0	1	-2.282e-3	4	NC	1	3707.611	4
431		7	max	.01	3	-.008	15	.151	4	0	1	NC	1	NC	1
432			min	-.002	10	-.239	1	0	1	-2.34e-3	4	NC	1	3163.721	4
433		8	max	.01	3	-.009	15	.174	4	0	1	NC	1	NC	1
434			min	-.003	2	-.277	1	0	1	-2.399e-3	4	NC	1	2806.504	4
435		9	max	.011	3	-.011	15	.198	4	0	1	NC	1	NC	1
436			min	-.005	2	-.316	1	0	1	-2.458e-3	4	NC	1	2571.1	4
437		10	max	.012	3	-.012	15	.22	4	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
438			min	-.007	2	-.354	1	0	1	-2.516e-3	4	NC	1	2424.126	4
439		11	max	.013	3	-.013	15	.242	4	0	1	NC	1	NC	1
440			min	-.008	2	-.392	1	0	1	-2.575e-3	4	NC	1	2349.278	4
441		12	max	.013	3	-.014	15	.263	4	0	1	NC	1	NC	1
442			min	-.01	2	-.43	1	0	1	-2.634e-3	4	NC	1	2341.871	4
443		13	max	.014	3	-.015	15	.284	4	0	1	NC	1	NC	1
444			min	-.012	2	-.468	1	0	1	-2.692e-3	4	NC	1	2408.255	4
445		14	max	.015	3	-.016	15	.303	4	0	1	NC	1	NC	1
446			min	-.013	2	-.506	1	0	1	-2.751e-3	4	NC	1	2570.24	4
447		15	max	.015	3	-.017	15	.321	4	0	1	NC	1	NC	1
448			min	-.015	2	-.544	1	0	1	-2.81e-3	4	NC	1	2879.727	4
449		16	max	.016	3	-.018	15	.339	4	0	1	NC	1	NC	1
450			min	-.017	2	-.582	1	0	1	-2.868e-3	4	NC	1	3465.109	4
451		17	max	.017	3	-.019	15	.355	4	0	1	NC	1	NC	1
452			min	-.018	2	-.62	1	0	1	-2.927e-3	4	NC	1	4719.022	4
453		18	max	.018	3	-.02	15	.37	4	0	1	NC	1	NC	1
454			min	-.02	2	-.657	1	0	1	-2.986e-3	4	NC	1	8615.081	4
455		19	max	.018	3	-.021	15	.384	4	0	1	NC	1	NC	1
456			min	-.022	2	-.695	1	0	1	-3.044e-3	4	NC	1	NC	1
457	M9	1	max	.006	1	0	5	.004	4	9.942e-4	3	NC	1	NC	1
458			min	0	5	-.003	1	0	3	-2.505e-3	2	NC	1	NC	1
459		2	max	.005	1	0	5	.031	4	1.223e-3	3	NC	1	NC	4
460			min	0	5	-.022	1	-.011	3	-2.981e-3	2	NC	1	2887.089	2
461		3	max	.005	1	0	5	.058	4	1.451e-3	3	NC	1	NC	15
462			min	0	5	-.041	1	-.02	3	-3.457e-3	2	NC	1	1460.28	2
463		4	max	.004	1	0	5	.085	4	1.68e-3	3	NC	1	8481.754	15
464			min	0	5	-.06	1	-.029	3	-3.933e-3	2	NC	1	990.943	2
465		5	max	.004	1	0	5	.111	4	1.908e-3	3	NC	1	6388.4	15
466			min	0	5	-.078	1	-.037	3	-4.409e-3	2	NC	1	761.477	2
467		6	max	.004	3	0	5	.137	4	2.137e-3	3	NC	1	5182.866	15
468			min	0	5	-.097	1	-.045	3	-4.885e-3	2	NC	1	628.56	2
469		7	max	.004	3	.001	5	.163	4	2.365e-3	3	NC	1	4424.128	15
470			min	0	5	-.116	1	-.052	3	-5.361e-3	2	NC	1	544.635	2
471		8	max	.004	3	.002	5	.188	4	2.594e-3	3	NC	1	3925.687	15
472			min	0	5	-.134	1	-.057	3	-5.837e-3	2	NC	1	489.584	2
473		9	max	.004	3	.002	5	.212	4	2.822e-3	3	NC	1	3597.172	15
474			min	0	10	-.153	1	-.062	3	-6.312e-3	2	NC	1	453.689	2
475		10	max	.004	3	.002	5	.235	4	3.051e-3	3	NC	1	3392.076	15
476			min	-.001	2	-.171	1	-.065	3	-6.788e-3	2	NC	1	432.011	2
477		11	max	.005	3	.003	5	.257	4	3.279e-3	3	NC	1	3287.699	15
478			min	-.002	2	-.19	1	-.066	3	-7.264e-3	2	NC	1	422.26	2
479		12	max	.005	3	.003	5	.277	4	3.508e-3	3	NC	1	3277.553	15
480			min	-.002	2	-.208	1	-.066	3	-7.74e-3	2	NC	1	424.025	2
481		13	max	.005	3	.004	5	.297	4	3.736e-3	3	NC	1	3370.561	15
482			min	-.003	2	-.226	1	-.063	3	-8.216e-3	2	NC	1	438.783	2
483		14	max	.005	3	.004	5	.315	4	3.965e-3	3	NC	1	3597.263	15
484			min	-.003	2	-.244	1	-.059	3	-8.692e-3	2	NC	1	470.786	2
485		15	max	.006	3	.005	5	.331	4	4.193e-3	3	NC	1	4030.286	15
486			min	-.004	2	-.262	1	-.052	3	-9.168e-3	2	NC	1	529.825	2
487		16	max	.006	3	.006	5	.346	4	4.422e-3	3	NC	1	4849.265	15
488			min	-.005	2	-.28	1	-.043	3	-9.644e-3	2	NC	1	639.872	2
489		17	max	.006	3	.006	5	.358	4	4.65e-3	3	NC	1	6603.517	15
490			min	-.005	2	-.297	1	-.031	3	-1.012e-2	2	NC	1	874.015	2
491		18	max	.006	3	.007	5	.369	4	4.879e-3	3	NC	1	NC	15
492			min	-.006	2	-.315	1	-.017	3	-1.06e-2	2	9077.607	5	1599.342	2
493		19	max	.006	3	.008	5	.378	5	5.107e-3	3	NC	1	NC	1
494			min	-.006	2	-.333	1	-.013	1	-1.107e-2	2	8235.848	5	NC	1