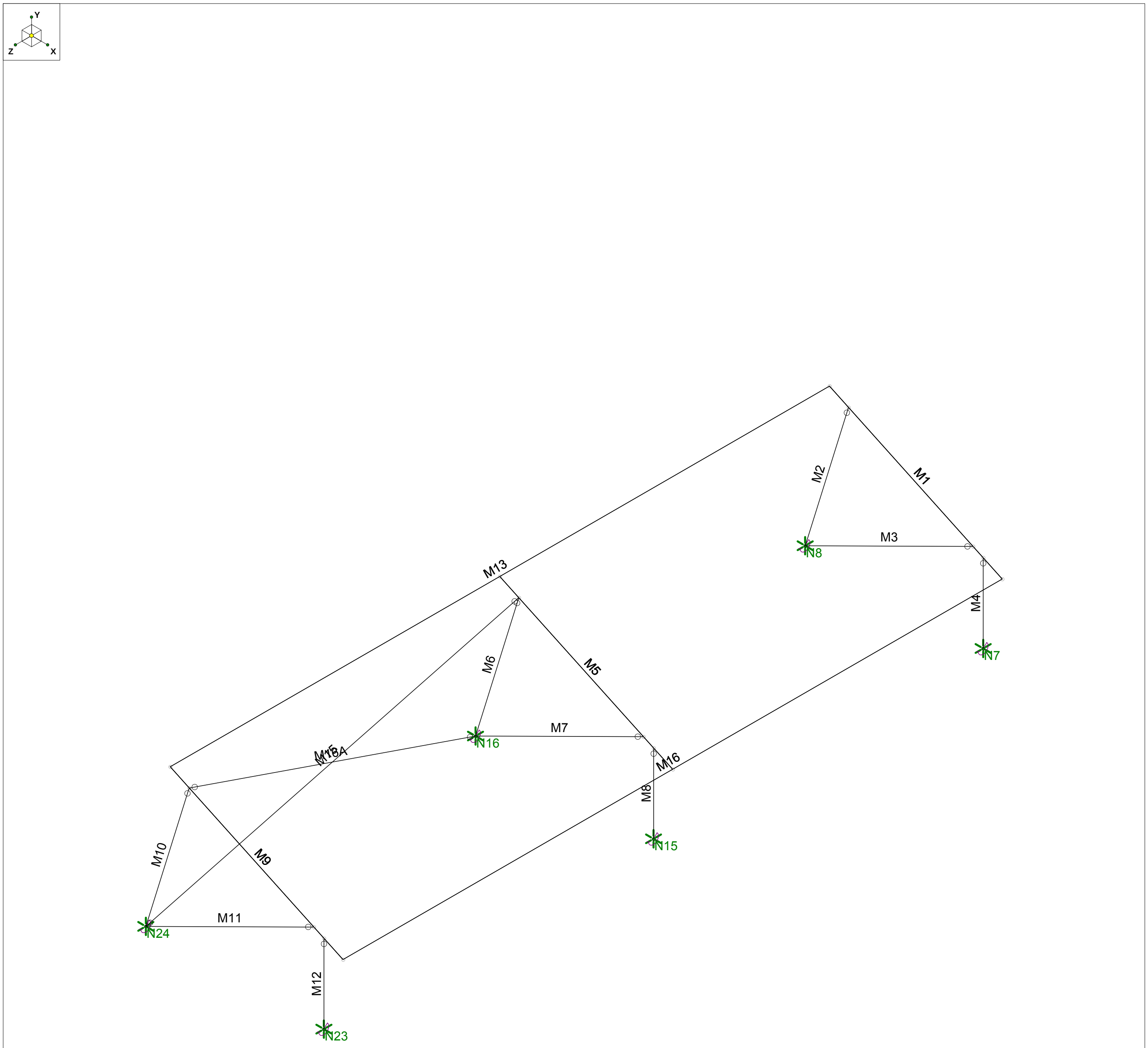


Schletter, Inc.		25° Tilt w/ Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

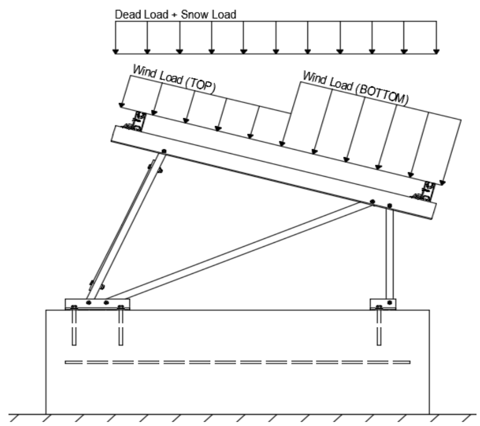
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 1
Module Tilt = 25°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 18.56 psf *(ASCE 7-05, Eq. 7-2)*
I_s = 1.00
C_s = 0.82
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 120 mph
Height ≤ 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 22.61 psf *Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.1	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.7	
$Cf-_{TOP}$	=	-2.2	*(Suction)*
$Cf-_{BOTTOM}$	=	-1	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W
1.2D + 1.6W + 0.5S
0.9D + 1.6W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 1.0W
1.0D + 0.75L + 0.75W + 0.75S
0.6D + 1.0W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

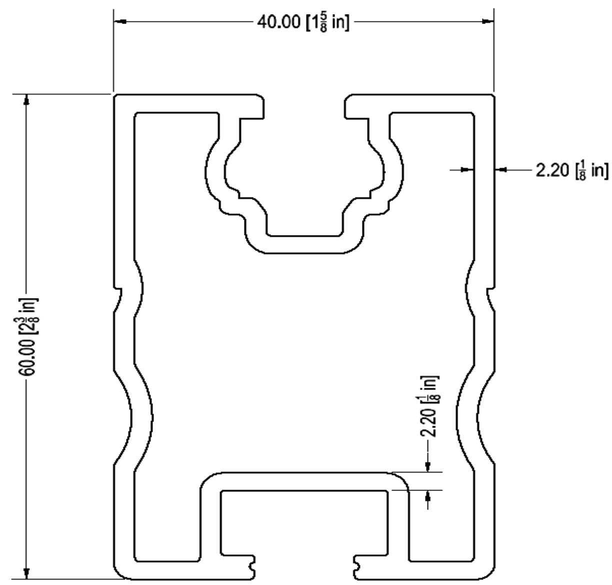
Purlins	Location	**Diagonal Struts**	Location	**Front Reactions**	Location
M13	Top	M3	Outer	N7	Outer
M16	Bottom	M7	Inner	N15	Inner
		M11	Outer	N23	Outer
Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer
Front Struts	Location	**Bracing**			
M4	Outer	M15			
M8	Inner	M16A			
M12	Outer				

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

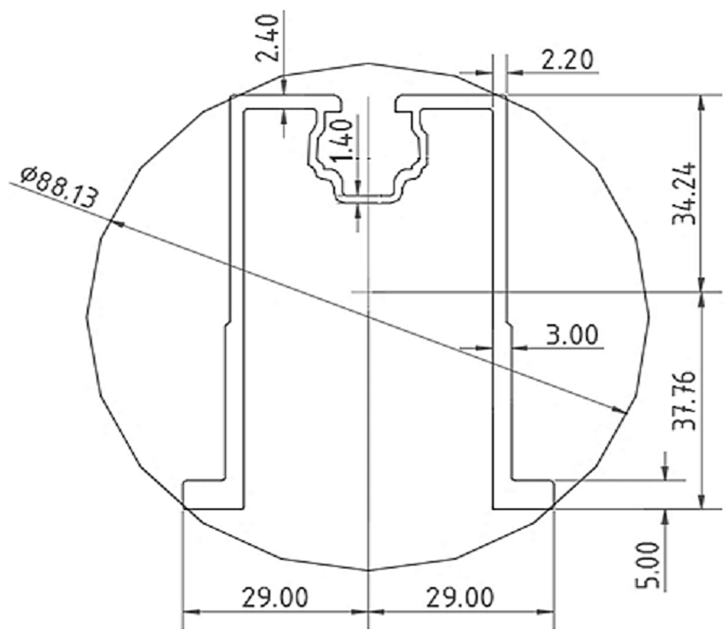
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	48	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.75	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	0.374	k-ft
M_z =	0.033	k-ft
$M_{y\ allowable}$ =	1.266	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	33%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

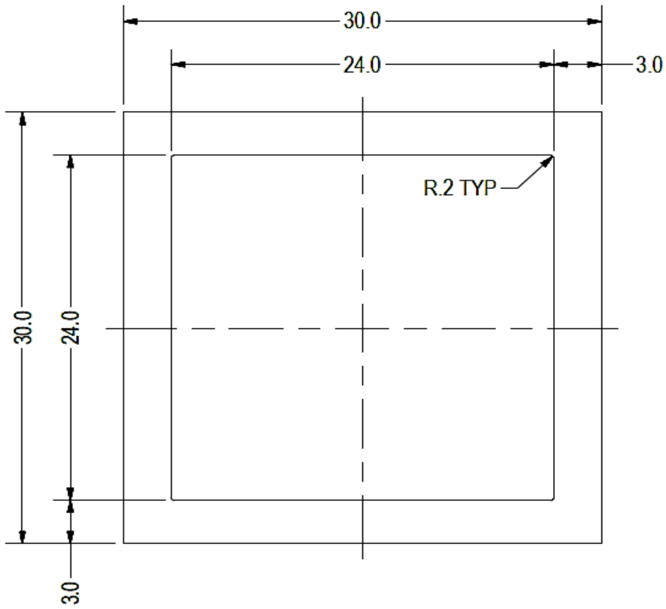
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.77	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	-0.459	k-ft
M_z =	-0.019	k-ft
P_n =	0.158	k
$M_{y\ allowable}$ =	1.461	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	36%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

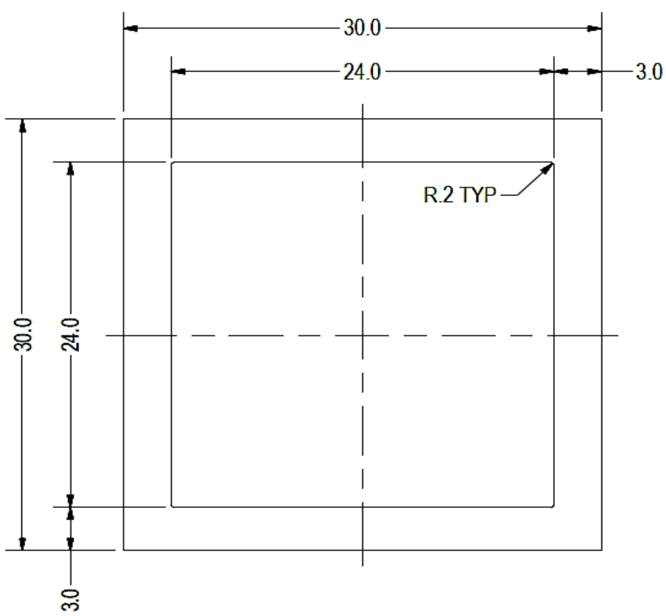
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.026	k-ft
P_n =	0.147	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	7%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

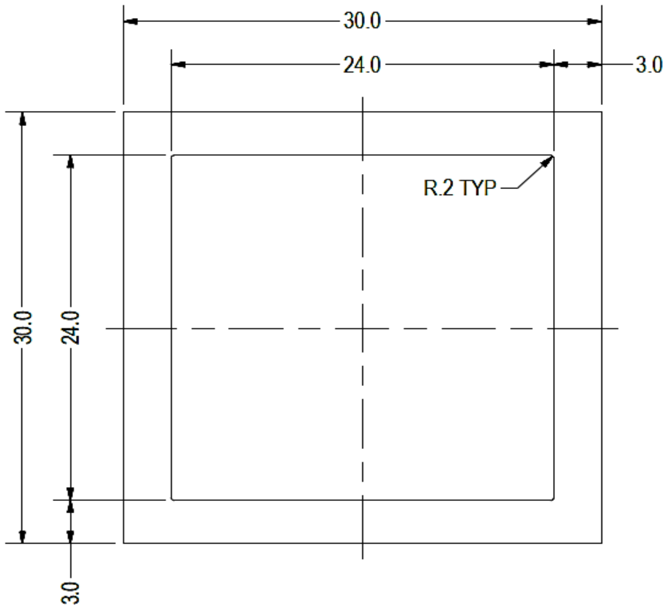
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.447	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	12%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

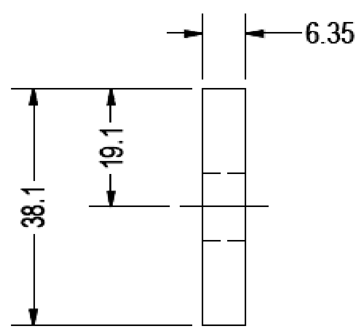
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	36.18	in
$\Phi F_{ty\ AXIAL}$ =	11.59	ksi
$\Phi F_{ty\ BENDING}$ =	30.23	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.674	k
$M_{y\ allowable}$ =	0.410	k-ft
$M_{z\ allowable}$ =	0.410	k-ft
$P_{n\ allowable}$ =	5.820	k
Utilization =	12%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.003	k-ft
P_n =	0.168	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	8%	



A cross brace kit is required every 24 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

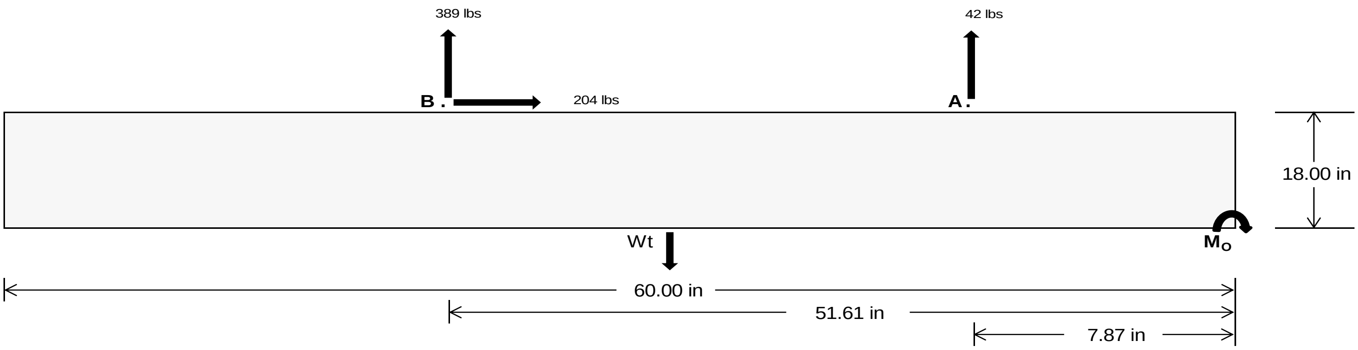
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	178.73	1620.25	k
Compressive Load =	1087.33	1074.38	k
Lateral Load =	21.57	848.24	k
Moment (Weak Axis) =	0.03	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC tables 1804.2 (2003, 2006) & 1806.2 (2009).



Concrete Properties
Weight of Concrete = 145 pcf
Compressive Strength = 2500 psi
Yield Strength = 60000 psi

Footing Reinforcement
Use fiber reinforcing with (1) #5 rebar.

Overturning Check
M_O = 24082.4 in-lbs
Resisting Force Required = 802.75 lbs
S.F. = 1.67
Weight Required = 1337.91 lbs
Minimum Width = 21 in in
Weight Provided = 1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.

Sliding
Force = 203.88 lbs
Friction = 0.4
Weight Required = 509.69 lbs
Resisting Weight = 1903.13 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion
Sliding Force = 203.88 lbs
Cohesion = 130 psf
Area = 8.75 ft^2
Resisting = 951.56 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key
Additional Force = 0 lbs
Lateral Bearing Pressure = 200 psf/ft
Required Depth = 0.00 ft
f'_c = 2500 psi
Length = 8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	21 in	22 in	23 in	24 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.75 ft) =	1903 lbs	1994 lbs	2084 lbs	2175 lbs

ASD LC	1.0D + 1.0S				1.0D + 1.0W				1.0D + 0.75L + 0.75W + 0.75S				0.6D + 1.0W			
Width	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in
F_A	353 lbs	353 lbs	353 lbs	353 lbs	428 lbs	428 lbs	428 lbs	428 lbs	556 lbs	556 lbs	556 lbs	556 lbs	-84 lbs	-84 lbs	-84 lbs	-84 lbs
F_B	246 lbs	246 lbs	246 lbs	246 lbs	464 lbs	464 lbs	464 lbs	464 lbs	511 lbs	511 lbs	511 lbs	511 lbs	-778 lbs	-778 lbs	-778 lbs	-778 lbs
F_V	28 lbs	28 lbs	28 lbs	28 lbs	362 lbs	362 lbs	362 lbs	362 lbs	291 lbs	291 lbs	291 lbs	291 lbs	-408 lbs	-408 lbs	-408 lbs	-408 lbs
P_{total}	2503 lbs	2594 lbs	2684 lbs	2775 lbs	2794 lbs	2885 lbs	2976 lbs	3066 lbs	2970 lbs	3061 lbs	3152 lbs	3242 lbs	279 lbs	334 lbs	388 lbs	443 lbs
M	250 lbs-ft	250 lbs-ft	250 lbs-ft	250 lbs-ft	497 lbs-ft	497 lbs-ft	497 lbs-ft	497 lbs-ft	541 lbs-ft	541 lbs-ft	541 lbs-ft	541 lbs-ft	634 lbs-ft	634 lbs-ft	634 lbs-ft	634 lbs-ft
e	0.10 ft	0.10 ft	0.09 ft	0.09 ft	0.18 ft	0.17 ft	0.17 ft	0.16 ft	0.18 ft	0.18 ft	0.17 ft	0.17 ft	2.27 ft	1.90 ft	1.63 ft	1.43 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	251.8 psf	250.2 psf	248.8 psf	247.5 psf	251.2 psf	249.7 psf	248.3 psf	247.0 psf	265.3 psf	263.1 psf	261.1 psf	259.3 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	320.3 psf	315.7 psf	311.4 psf	307.5 psf	387.5 psf	379.8 psf	372.7 psf	366.2 psf	413.7 psf	404.8 psf	396.6 psf	389.1 psf	463.0 psf	202.4 psf	155.9 psf	138.3 psf

Maximum Bearing Pressure = 463 psf
Allowable Bearing Pressure = 1500 psf

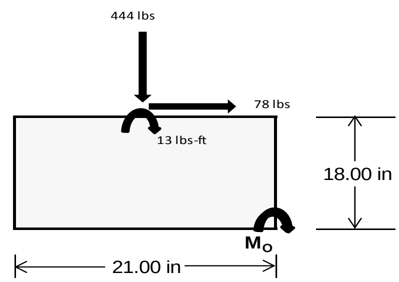
Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O =	258.7 ft-lbs
Resisting Force Required =	295.61 lbs
S.F. =	1.67
Weight Required =	492.68 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	21 in			21 in			21 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	113 lbs	61 lbs	54 lbs	219 lbs	444 lbs	174 lbs	76 lbs	-29 lbs	19 lbs
F_V	12 lbs	104 lbs	12 lbs	9 lbs	78 lbs	10 lbs	13 lbs	103 lbs	12 lbs
P_{total}	2469 lbs	2417 lbs	2410 lbs	2462 lbs	2687 lbs	2417 lbs	765 lbs	660 lbs	708 lbs
M	35 lbs-ft	173 lbs-ft	36 lbs-ft	25 lbs-ft	130 lbs-ft	27 lbs-ft	35 lbs-ft	172 lbs-ft	36 lbs-ft
e	0.01 ft	0.07 ft	0.01 ft	0.01 ft	0.05 ft	0.01 ft	0.05 ft	0.26 ft	0.05 ft
L/6	0.29 ft	1.61 ft	1.72 ft	1.73 ft	1.65 ft	1.73 ft	1.66 ft	1.23 ft	1.65 ft
f_{min}	268.5 sqft	208.3 sqft	261.5 sqft	271.4 sqft	256.2 sqft	265.6 sqft	73.8 sqft	7.9 sqft	67.0 sqft
f_{max}	295.7 psf	344.1 psf	289.4 psf	291.3 psf	357.9 psf	286.9 psf	101.1 psf	142.9 psf	94.9 psf

Maximum Bearing Pressure =	358 psf
Allowable Bearing Pressure =	1500 psf

Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 21in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

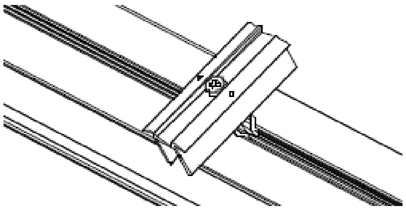
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

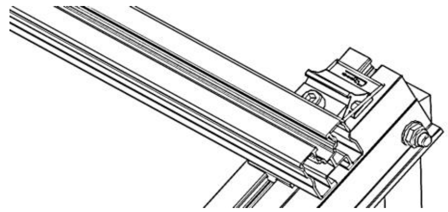
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

Fastening of Modules to Purlins			Fastening of Purlins to Girders	
Maximum Uplifting Force =	0.749 k		Maximum Uplifting Force =	1.070 k
Allowable Uplift =	1.214 k		Allowable Uplift =	1.116 k
Utilization =	62%		Utilization =	96%



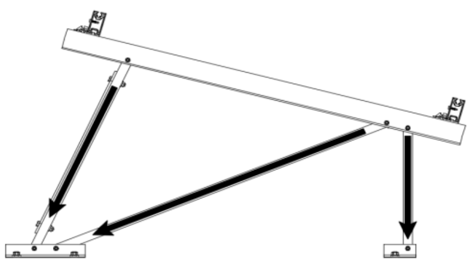


6.2 Bolted Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut			Rear Strut	
Maximum Axial Load =	0.836 k		Maximum Axial Load =	1.085 k
M8 Bolt Capacity =	5.692 k		M8 Bolt Capacity =	5.692 k
Strut Bearing Capacity =	7.952 k		Strut Bearing Capacity =	7.952 k
Utilization =	15%		Utilization =	19%

Diagonal Strut			Bracing	
Maximum Axial Load =	0.447 k		Maximum Axial Load =	0.168 k
M8 Bolt Shear Capacity =	5.692 k		M10 Bolt Capacity =	8.894 k
Strut Bearing Capacity =	7.952 k		Strut Bearing Capacity =	7.952 k
Utilization =	8%		Utilization =	2%



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

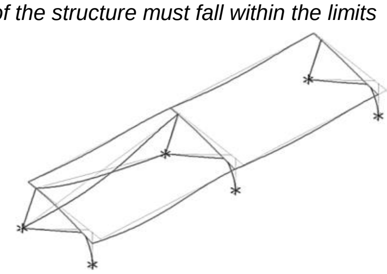
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	30.83 in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$
	0.617 in
Max Drift, Δ_{MAX} =	0.054 in

$0.054 \leq 0.617$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus**

Strong Axis:

3.4.14

L_b = 48.00 in

J = 0.255

124.989

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.7 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 48.00 in

J = 0.255

129.794

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.7

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 30
Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

$\varphi F_L St$= 29.7 ksi
Ix = 250988 mm^4
0.603 in^4
y = 30 mm
Sx = 0.511 in^3
$M_{max}St$ = 1.266 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 20
Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi
Iy = 120291 mm^4
0.289 in^4
x = 20 mm
Sy = 0.367 in^3
$M_{max}Wk$ = 0.871 k-ft

Compression

3.4.9

b/t = 7.4
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 23.9
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 28.47 ksi
A = 578.06 mm^2
0.90 in^2
P_{max} = 25.51 kips

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.33

21.3453

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.8 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.33

24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.8 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7

F_{UT}= (φbk2*√(BpE))/(5.1b/t)

F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

F_{ST}= φb[Bp-1.6Dp*b/t]

F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.2

N/A for Strong Direction

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.461 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

3.4.8

b/t = 24.46
S1 = 3.83
S2 = 10.30
φF_L= (φck2*√(BpE))/(5.1b/t)
φF_L= 10.4 ksi

3.4.9

b/t = 4.29
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 24.46
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.9.1

b/t = 24.46
t = 2.6
ds = 6.05
rs = 3.49
S = 21.70
ρst = 0.22
F_{UT}= 10.43
F_{ST}= 28.24
φF_L= Fut + (Fst - Fut)ρst < Fst
φF_L= 14.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 14.29 ksi
A = 576.21 mm^2
0.89 in^2
P_{max} = 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 31.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.2 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.423 k-ft

Compression

3.4.7

λ = 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83792

$\varphi F_L = \varphi cc(Bc - Dc^*\lambda)$

$\varphi F_L =$ 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 24.52 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.404 k-ft

Weak Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.85841

φF_L = $(\varphi ccFcy)/(\lambda^2)$

φF_L = 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = $\varphi yFcy$

φF_L = 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L = $\varphi yFcy$

φF_L = 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = $\varphi yFcy$

φF_L = 33.25 ksi

φF_L = 7.60 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 36.18 in
J = 0.16
94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.2 ksi
Ix = 39958.2 mm^4
0.096 in^4
y = 15 mm
Sx = 0.163 in^3
M_{max}St = 0.410 k-ft

Weak Axis:

3.4.14

L_b = 36.18 in
J = 0.16
94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi
Iy = 39958.2 mm^4
0.096 in^4
x = 15 mm
Sy = 0.163 in^3
M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.5514

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.7972

φF_L = (φccFcy)/(λ²)

φF_L = 11.5927 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L = φyFcy

φF_L = 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 11.59 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 5.82 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-51.748	-51.748	0	0
2	M16	Y	-51.748	-51.748	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-69.356	-69.356	0	0
2	M16	y	-107.187	-107.187	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	138.712	138.712	0	0
2	M16	y	63.051	63.051	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8														
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6														
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	183.185	2	262.493	2	.003	10	0	10	0	1	0	1
2		min	-219.144	3	-393.793	3	-2.264	4	0	3	0	1	0	1
3	N7	max	0	4	293.608	1	.018	10	0	10	0	1	0	1
4		min	-.119	2	-30.925	3	-16.231	4	-.026	4	0	1	0	1
5	N15	max	0	15	836.408	1	.134	9	0	9	0	1	0	1
6		min	-1.187	2	-137.482	3	-16.59	5	-.026	4	0	1	0	1
7	N16	max	590.067	2	826.449	2	0	11	0	9	0	1	0	1
8		min	-652.496	3	-1246.345	3	-137.575	4	0	3	0	1	0	1
9	N23	max	0	15	293.793	1	.703	1	.001	1	0	1	0	1
10		min	-.119	2	-30.383	3	-15.44	5	-.024	5	0	1	0	1
11	N24	max	183.185	2	264.873	2	76.277	3	0	4	0	1	0	1
12		min	-219.615	3	-392.905	3	-3.234	5	0	3	0	1	0	1
13	Totals:	max	955.012	2	2682.222	2	0	1						
14		min	-1091.44	3	-2231.834	3	-190.852	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	214.653	1	.641	6	1.002	4	0	10	0	10	0	1
2			min	-354.471	3	.149	15	-.087	3	0	4	0	4	0	1
3		2	max	214.769	1	.595	6	.897	4	0	10	0	5	0	15
4			min	-354.383	3	.139	15	-.087	3	0	4	0	3	0	6
5		3	max	214.886	1	.55	6	.791	4	0	10	0	4	0	15
6			min	-354.296	3	.128	15	-.087	3	0	4	0	3	0	6
7		4	max	215.002	1	.504	6	.686	4	0	10	0	4	0	15
8			min	-354.209	3	.117	15	-.087	3	0	4	0	3	0	6
9		5	max	215.119	1	.458	6	.58	4	0	10	0	4	0	15
10			min	-354.122	3	.106	15	-.087	3	0	4	0	3	0	6
11		6	max	215.235	1	.413	6	.475	4	0	10	0	4	0	15
12			min	-354.034	3	.096	15	-.087	3	0	4	0	3	0	6
13		7	max	215.351	1	.367	6	.369	4	0	10	0	4	0	15
14			min	-353.947	3	.085	15	-.087	3	0	4	0	3	0	6
15		8	max	215.468	1	.321	6	.264	4	0	10	0	4	0	15
16			min	-353.86	3	.074	15	-.087	3	0	4	0	3	0	6
17		9	max	215.584	1	.276	6	.158	4	0	10	0	4	0	15
18			min	-353.772	3	.064	15	-.087	3	0	4	0	3	0	6
19		10	max	215.701	1	.23	6	.121	1	0	10	0	4	0	15
20			min	-353.685	3	.053	15	-.087	3	0	4	0	3	0	6
21		11	max	215.817	1	.184	6	.121	1	0	10	0	4	0	15
22			min	-353.598	3	.042	15	-.087	3	0	4	0	3	0	6
23		12	max	215.933	1	.14	2	.121	1	0	10	0	4	0	15
24			min	-353.51	3	.031	15	-.192	5	0	4	0	3	0	6
25		13	max	216.05	1	.104	2	.121	1	0	10	0	4	0	15
26			min	-353.423	3	.018	12	-.297	5	0	4	0	3	0	6
27		14	max	216.166	1	.069	2	.121	1	0	10	0	4	0	15
28			min	-353.336	3	-.002	3	-.403	5	0	4	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	216.283	1	.033	2	.121	1	0	10	0	4	0	15
30			min	-353.249	3	-.029	3	-.508	5	0	4	0	3	0	6
31		16	max	216.399	1	-.002	2	.121	1	0	10	0	4	0	15
32			min	-353.161	3	-.056	3	-.614	5	0	4	0	3	0	6
33		17	max	216.515	1	-.022	15	.121	1	0	10	0	4	0	15
34			min	-353.074	3	-.09	4	-.719	5	0	4	0	3	0	6
35		18	max	216.632	1	-.033	15	.121	1	0	10	0	1	0	15
36			min	-352.987	3	-.135	4	-.825	5	0	4	0	3	0	6
37		19	max	216.748	1	-.044	15	.121	1	0	10	0	1	0	15
38			min	-352.899	3	-.181	4	-.93	5	0	4	0	3	0	6
39	M3	1	max	137.106	2	1.776	6	.003	10	0	5	0	4	0	6
40			min	-128.77	3	.417	15	-1.337	4	0	1	0	10	0	15
41		2	max	137.038	2	1.599	6	.003	10	0	5	0	1	0	2
42			min	-128.822	3	.375	15	-1.204	4	0	1	0	10	0	15
43		3	max	136.969	2	1.422	6	.003	10	0	5	0	1	0	2
44			min	-128.873	3	.333	15	-1.07	4	0	1	0	5	0	3
45		4	max	136.901	2	1.245	6	.003	10	0	5	0	1	0	15
46			min	-128.925	3	.292	15	-.937	4	0	1	0	5	0	4
47		5	max	136.832	2	1.068	6	.003	10	0	5	0	1	0	15
48			min	-128.976	3	.25	15	-.803	4	0	1	0	5	0	4
49		6	max	136.763	2	.89	6	.003	10	0	5	0	1	0	15
50			min	-129.028	3	.208	15	-.669	4	0	1	0	5	0	4
51		7	max	136.695	2	.713	6	.003	10	0	5	0	1	0	15
52			min	-129.079	3	.167	15	-.536	4	0	1	0	5	0	4
53		8	max	136.626	2	.536	6	.003	10	0	5	0	1	0	15
54			min	-129.131	3	.125	15	-.402	4	0	1	0	5	-.001	4
55		9	max	136.558	2	.359	6	.003	10	0	5	0	1	0	15
56			min	-129.182	3	.083	15	-.268	4	0	1	0	5	-.001	4
57		10	max	136.489	2	.182	6	.003	10	0	5	0	1	0	15
58			min	-129.233	3	.042	15	-.15	1	0	1	0	5	-.001	4
59		11	max	136.42	2	.029	2	.033	5	0	5	0	1	0	15
60			min	-129.285	3	-.021	3	-.15	1	0	1	0	5	-.001	4
61		12	max	136.352	2	-.042	15	.167	5	0	5	0	1	0	15
62			min	-129.336	3	-.173	4	-.15	1	0	1	0	5	-.001	4
63		13	max	136.283	2	-.083	15	.3	5	0	5	0	1	0	15
64			min	-129.388	3	-.35	4	-.15	1	0	1	0	5	-.001	4
65		14	max	136.215	2	-.125	15	.434	5	0	5	0	1	0	15
66			min	-129.439	3	-.527	4	-.15	1	0	1	0	5	-.001	4
67		15	max	136.146	2	-.167	15	.567	5	0	5	0	9	0	15
68			min	-129.491	3	-.704	4	-.15	1	0	1	0	5	0	4
69		16	max	136.077	2	-.208	15	.701	5	0	5	0	10	0	15
70			min	-129.542	3	-.882	4	-.15	1	0	1	0	4	0	4
71		17	max	136.009	2	-.25	15	.835	5	0	5	0	10	0	15
72			min	-129.594	3	-1.059	4	-.15	1	0	1	0	4	0	4
73		18	max	135.94	2	-.292	15	.968	5	0	5	0	10	0	15
74			min	-129.645	3	-1.236	4	-.15	1	0	1	0	4	0	4
75		19	max	135.872	2	-.333	15	1.102	5	0	5	0	5	0	1
76			min	-129.697	3	-1.413	4	-.15	1	0	1	0	1	0	1
77	M4	1	max	292.444	1	0	1	.018	10	0	1	0	5	0	1
78			min	-31.799	3	0	1	-15.414	4	0	1	0	2	0	1
79		2	max	292.508	1	0	1	.018	10	0	1	0	10	0	1
80			min	-31.75	3	0	1	-15.47	4	0	1	-.001	4	0	1
81		3	max	292.573	1	0	1	.018	10	0	1	0	10	0	1
82			min	-31.702	3	0	1	-15.526	4	0	1	-.003	4	0	1
83		4	max	292.638	1	0	1	.018	10	0	1	0	10	0	1
84			min	-31.653	3	0	1	-15.583	4	0	1	-.004	4	0	1
85		5	max	292.703	1	0	1	.018	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	-31.605	3	0	1	-15.639	4	0	1	-.006	4	0	1
87		6	max	292.767	1	0	1	.018	10	0	1	0	10	0	1
88			min	-31.556	3	0	1	-15.695	4	0	1	-.007	4	0	1
89		7	max	292.832	1	0	1	.018	10	0	1	0	10	0	1
90			min	-31.508	3	0	1	-15.751	4	0	1	-.008	4	0	1
91		8	max	292.897	1	0	1	.018	10	0	1	0	10	0	1
92			min	-31.459	3	0	1	-15.807	4	0	1	-.01	4	0	1
93		9	max	292.961	1	0	1	.018	10	0	1	0	10	0	1
94			min	-31.411	3	0	1	-15.863	4	0	1	-.011	4	0	1
95		10	max	293.026	1	0	1	.018	10	0	1	0	10	0	1
96			min	-31.362	3	0	1	-15.919	4	0	1	-.013	4	0	1
97		11	max	293.091	1	0	1	.018	10	0	1	0	10	0	1
98			min	-31.314	3	0	1	-15.975	4	0	1	-.014	4	0	1
99		12	max	293.155	1	0	1	.018	10	0	1	0	10	0	1
100			min	-31.265	3	0	1	-16.031	4	0	1	-.015	4	0	1
101		13	max	293.22	1	0	1	.018	10	0	1	0	10	0	1
102			min	-31.217	3	0	1	-16.087	4	0	1	-.017	4	0	1
103		14	max	293.285	1	0	1	.018	10	0	1	0	10	0	1
104			min	-31.168	3	0	1	-16.143	4	0	1	-.018	4	0	1
105		15	max	293.35	1	0	1	.018	10	0	1	0	10	0	1
106			min	-31.12	3	0	1	-16.199	4	0	1	-.02	4	0	1
107		16	max	293.414	1	0	1	.018	10	0	1	0	10	0	1
108			min	-31.071	3	0	1	-16.255	4	0	1	-.021	4	0	1
109		17	max	293.479	1	0	1	.018	10	0	1	0	10	0	1
110			min	-31.023	3	0	1	-16.312	4	0	1	-.023	4	0	1
111		18	max	293.544	1	0	1	.018	10	0	1	0	10	0	1
112			min	-30.974	3	0	1	-16.368	4	0	1	-.024	4	0	1
113		19	max	293.608	1	0	1	.018	10	0	1	0	10	0	1
114			min	-30.925	3	0	1	-16.424	4	0	1	-.026	4	0	1
115	M6	1	max	672.025	1	.629	6	.963	4	0	3	0	3	0	1
116			min	-1085.172	3	.141	15	-.268	3	0	5	0	2	0	1
117		2	max	672.142	1	.583	6	.858	4	0	3	0	4	0	15
118			min	-1085.084	3	.131	15	-.268	3	0	5	0	2	0	6
119		3	max	672.258	1	.537	6	.752	4	0	3	0	4	0	15
120			min	-1084.997	3	.12	15	-.268	3	0	5	0	2	0	6
121		4	max	672.374	1	.492	6	.647	4	0	3	0	4	0	15
122			min	-1084.91	3	.109	15	-.268	3	0	5	0	2	0	6
123		5	max	672.491	1	.449	2	.541	4	0	3	0	4	0	15
124			min	-1084.822	3	.098	15	-.268	3	0	5	0	2	0	6
125		6	max	672.607	1	.413	2	.436	4	0	3	0	4	0	15
126			min	-1084.735	3	.088	15	-.268	3	0	5	0	2	0	6
127		7	max	672.724	1	.378	2	.33	4	0	3	0	4	0	15
128			min	-1084.648	3	.077	15	-.268	3	0	5	0	3	0	6
129		8	max	672.84	1	.342	2	.225	4	0	3	0	4	0	15
130			min	-1084.56	3	.066	15	-.268	3	0	5	0	3	0	6
131		9	max	672.957	1	.307	2	.119	4	0	3	0	4	0	15
132			min	-1084.473	3	.049	12	-.268	3	0	5	0	3	0	2
133		10	max	673.073	1	.271	2	.028	9	0	3	0	4	0	15
134			min	-1084.386	3	.031	12	-.268	3	0	5	0	3	0	2
135		11	max	673.189	1	.235	2	.028	9	0	3	0	4	0	15
136			min	-1084.299	3	.014	12	-.268	3	0	5	0	3	0	2
137		12	max	673.306	1	.2	2	.028	9	0	3	0	4	0	15
138			min	-1084.211	3	-.012	3	-.268	3	0	5	0	3	0	2
139		13	max	673.422	1	.164	2	.028	9	0	3	0	4	0	15
140			min	-1084.124	3	-.039	3	-.313	5	0	5	0	3	0	2
141		14	max	673.539	1	.129	2	.028	9	0	3	0	4	0	15
142			min	-1084.037	3	-.066	3	-.419	5	0	5	0	3	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	673.655	1	.093	2	.028	9	0	3	0	4	0	15
144			min	-1083.949	3	-.092	3	-.524	5	0	5	0	3	0	2
145		16	max	673.771	1	.057	2	.028	9	0	3	0	4	0	12
146			min	-1083.862	3	-.119	3	-.63	5	0	5	0	3	0	2
147		17	max	673.888	1	.022	2	.028	9	0	3	0	4	0	12
148			min	-1083.775	3	-.146	3	-.735	5	0	5	0	3	0	2
149		18	max	674.004	1	-.014	2	.028	9	0	3	0	4	0	12
150			min	-1083.687	3	-.172	3	-.841	5	0	5	0	3	0	2
151		19	max	674.121	1	-.049	2	.028	9	0	3	0	14	0	12
152			min	-1083.6	3	-.199	3	-.946	5	0	5	0	3	0	2
153	M7	1	max	447.125	2	1.791	4	.022	3	0	9	0	4	0	2
154			min	-354.844	3	.426	15	-1.353	4	0	3	0	3	0	12
155		2	max	447.057	2	1.614	4	.022	3	0	9	0	4	0	2
156			min	-354.895	3	.384	15	-1.219	4	0	3	0	3	0	3
157		3	max	446.988	2	1.437	4	.022	3	0	9	0	1	0	2
158			min	-354.947	3	.343	15	-1.085	4	0	3	0	3	0	3
159		4	max	446.919	2	1.259	4	.022	3	0	9	0	1	0	2
160			min	-354.998	3	.301	15	-.952	4	0	3	0	3	0	3
161		5	max	446.851	2	1.082	4	.022	3	0	9	0	1	0	15
162			min	-355.05	3	.259	15	-.818	4	0	3	0	5	0	3
163		6	max	446.782	2	.905	4	.022	3	0	9	0	1	0	15
164			min	-355.101	3	.218	15	-.685	4	0	3	0	5	0	6
165		7	max	446.714	2	.728	4	.022	3	0	9	0	1	0	15
166			min	-355.152	3	.176	15	-.551	4	0	3	0	5	0	6
167		8	max	446.645	2	.551	4	.022	3	0	9	0	1	0	15
168			min	-355.204	3	.134	15	-.417	4	0	3	0	5	0	6
169		9	max	446.576	2	.373	4	.022	3	0	9	0	1	0	15
170			min	-355.255	3	.093	15	-.284	4	0	3	0	5	-.001	6
171		10	max	446.508	2	.214	2	.022	3	0	9	0	1	0	15
172			min	-355.307	3	.026	12	-.15	4	0	3	0	5	-.001	6
173		11	max	446.439	2	.076	2	.022	3	0	9	0	1	0	15
174			min	-355.358	3	-.069	3	-.016	4	0	3	0	5	-.001	6
175		12	max	446.371	2	-.032	15	.118	5	0	9	0	1	0	15
176			min	-355.41	3	-.173	3	-.015	1	0	3	0	5	-.001	6
177		13	max	446.302	2	-.074	15	.252	5	0	9	0	1	0	15
178			min	-355.461	3	-.336	6	-.015	1	0	3	0	5	-.001	6
179		14	max	446.233	2	-.115	15	.386	5	0	9	0	1	0	15
180			min	-355.513	3	-.513	6	-.015	1	0	3	0	5	-.001	6
181		15	max	446.165	2	-.157	15	.519	5	0	9	0	1	0	15
182			min	-355.564	3	-.69	6	-.015	1	0	3	0	5	0	6
183		16	max	446.096	2	-.199	15	.653	5	0	9	0	1	0	15
184			min	-355.616	3	-.868	6	-.015	1	0	3	0	5	0	6
185		17	max	446.028	2	-.24	15	.787	5	0	9	0	1	0	15
186			min	-355.667	3	-1.045	6	-.015	1	0	3	0	5	0	6
187		18	max	445.959	2	-.282	15	.92	5	0	9	0	9	0	15
188			min	-355.718	3	-1.222	6	-.015	1	0	3	0	3	0	6
189		19	max	445.89	2	-.324	15	1.054	5	0	9	0	9	0	1
190			min	-355.77	3	-1.399	6	-.015	1	0	3	0	3	0	1
191	M8	1	max	835.244	1	0	1	.142	9	0	1	0	4	0	1
192			min	-138.356	3	0	1	-15.708	4	0	1	0	3	0	1
193		2	max	835.308	1	0	1	.142	9	0	1	0	9	0	1
194			min	-138.307	3	0	1	-15.764	4	0	1	-.001	4	0	1
195		3	max	835.373	1	0	1	.142	9	0	1	0	9	0	1
196			min	-138.259	3	0	1	-15.82	4	0	1	-.003	4	0	1
197		4	max	835.438	1	0	1	.142	9	0	1	0	9	0	1
198			min	-138.21	3	0	1	-15.876	4	0	1	-.004	4	0	1
199		5	max	835.503	1	0	1	.142	9	0	1	0	9	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	-138.162	3	0	1	-15.932	4	0	1	-.006	4	0	1
201		6	max	835.567	1	0	1	.142	9	0	1	0	9	0	1
202			min	-138.113	3	0	1	-15.988	4	0	1	-.007	4	0	1
203		7	max	835.632	1	0	1	.142	9	0	1	0	9	0	1
204			min	-138.065	3	0	1	-16.044	4	0	1	-.009	4	0	1
205		8	max	835.697	1	0	1	.142	9	0	1	0	9	0	1
206			min	-138.016	3	0	1	-16.1	4	0	1	-.01	4	0	1
207		9	max	835.761	1	0	1	.142	9	0	1	0	9	0	1
208			min	-137.967	3	0	1	-16.156	4	0	1	-.011	4	0	1
209		10	max	835.826	1	0	1	.142	9	0	1	0	9	0	1
210			min	-137.919	3	0	1	-16.213	4	0	1	-.013	4	0	1
211		11	max	835.891	1	0	1	.142	9	0	1	0	9	0	1
212			min	-137.87	3	0	1	-16.269	4	0	1	-.014	4	0	1
213		12	max	835.956	1	0	1	.142	9	0	1	0	9	0	1
214			min	-137.822	3	0	1	-16.325	4	0	1	-.016	4	0	1
215		13	max	836.02	1	0	1	.142	9	0	1	0	9	0	1
216			min	-137.773	3	0	1	-16.381	4	0	1	-.017	4	0	1
217		14	max	836.085	1	0	1	.142	9	0	1	0	9	0	1
218			min	-137.725	3	0	1	-16.437	4	0	1	-.019	4	0	1
219		15	max	836.15	1	0	1	.142	9	0	1	0	9	0	1
220			min	-137.676	3	0	1	-16.493	4	0	1	-.02	4	0	1
221		16	max	836.214	1	0	1	.142	9	0	1	0	9	0	1
222			min	-137.628	3	0	1	-16.549	4	0	1	-.022	4	0	1
223		17	max	836.279	1	0	1	.142	9	0	1	0	9	0	1
224			min	-137.579	3	0	1	-16.605	4	0	1	-.023	4	0	1
225		18	max	836.344	1	0	1	.142	9	0	1	0	9	0	1
226			min	-137.531	3	0	1	-16.661	4	0	1	-.025	4	0	1
227		19	max	836.408	1	0	1	.142	9	0	1	0	9	0	1
228			min	-137.482	3	0	1	-16.717	4	0	1	-.026	4	0	1
229	M10	1	max	216.114	1	.672	4	1.077	5	0	1	0	1	0	1
230			min	-296.423	3	.17	15	-.106	1	-.001	5	0	3	0	1
231		2	max	216.231	1	.626	4	.971	5	0	1	0	4	0	15
232			min	-296.336	3	.159	15	-.106	1	-.001	5	0	3	0	4
233		3	max	216.347	1	.581	4	.866	5	0	1	0	4	0	15
234			min	-296.249	3	.149	15	-.106	1	-.001	5	0	3	0	4
235		4	max	216.463	1	.535	4	.76	5	0	1	0	4	0	15
236			min	-296.161	3	.138	15	-.106	1	-.001	5	0	3	0	4
237		5	max	216.58	1	.489	4	.655	5	0	1	0	4	0	15
238			min	-296.074	3	.127	15	-.106	1	-.001	5	0	3	0	4
239		6	max	216.696	1	.444	4	.549	5	0	1	0	4	0	15
240			min	-295.987	3	.116	15	-.106	1	-.001	5	0	3	0	4
241		7	max	216.813	1	.398	4	.444	5	0	1	0	4	0	15
242			min	-295.899	3	.106	15	-.106	1	-.001	5	0	3	0	4
243		8	max	216.929	1	.352	4	.338	5	0	1	0	4	0	15
244			min	-295.812	3	.095	15	-.106	1	-.001	5	0	3	0	4
245		9	max	217.045	1	.307	4	.233	5	0	1	0	5	0	15
246			min	-295.725	3	.084	15	-.106	1	-.001	5	0	3	0	4
247		10	max	217.162	1	.261	4	.127	5	0	1	0	5	0	15
248			min	-295.638	3	.074	15	-.106	1	-.001	5	0	3	0	4
249		11	max	217.278	1	.215	4	.022	5	0	1	0	5	0	15
250			min	-295.55	3	.063	15	-.106	1	-.001	5	0	3	0	4
251		12	max	217.395	1	.17	4	0	10	0	1	0	5	0	15
252			min	-295.463	3	.047	12	-.106	1	-.001	5	0	3	0	4
253		13	max	217.511	1	.124	4	0	10	0	1	0	5	0	15
254			min	-295.376	3	.03	12	-.203	4	-.001	5	0	3	0	4
255		14	max	217.627	1	.078	4	0	10	0	1	0	5	0	15
256			min	-295.288	3	.012	12	-.308	4	-.001	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	217.744	1	.033	2	0	10	0	1	0	5	0	15
258			min	-295.201	3	-.01	3	-.414	4	-.001	5	0	3	0	4
259		16	max	217.86	1	.013	5	0	10	0	1	0	5	0	15
260			min	-295.114	3	-.036	3	-.519	4	-.001	5	0	3	0	4
261		17	max	217.977	1	-.002	15	0	10	0	1	0	5	0	15
262			min	-295.026	3	-.063	3	-.625	4	-.001	5	0	3	0	4
263		18	max	218.093	1	-.012	15	0	10	0	1	0	5	0	15
264			min	-294.939	3	-.105	6	-.73	4	-.001	5	0	3	0	4
265		19	max	218.21	1	-.023	15	0	10	0	1	0	5	0	15
266			min	-294.852	3	-.151	6	-.836	4	-.001	5	0	3	0	4
267	M11	1	max	136.694	2	1.77	6	.158	1	0	4	0	5	0	6
268			min	-129.514	3	.412	15	-1.26	5	0	10	0	1	0	15
269		2	max	136.626	2	1.593	6	.158	1	0	4	0	5	0	2
270			min	-129.566	3	.37	15	-1.126	5	0	10	0	1	0	12
271		3	max	136.557	2	1.416	6	.158	1	0	4	0	3	0	2
272			min	-129.617	3	.329	15	-.993	5	0	10	0	1	0	3
273		4	max	136.488	2	1.238	6	.158	1	0	4	0	3	0	15
274			min	-129.668	3	.287	15	-.859	5	0	10	0	1	0	4
275		5	max	136.42	2	1.061	6	.158	1	0	4	0	3	0	15
276			min	-129.72	3	.245	15	-.726	5	0	10	0	1	0	4
277		6	max	136.351	2	.884	6	.158	1	0	4	0	3	0	15
278			min	-129.771	3	.204	15	-.592	5	0	10	0	1	0	4
279		7	max	136.283	2	.707	6	.158	1	0	4	0	3	0	15
280			min	-129.823	3	.162	15	-.458	5	0	10	0	4	0	4
281		8	max	136.214	2	.53	6	.158	1	0	4	0	3	0	15
282			min	-129.874	3	.12	15	-.325	5	0	10	0	4	-.001	4
283		9	max	136.145	2	.352	6	.158	1	0	4	0	3	0	15
284			min	-129.926	3	.079	15	-.191	5	0	10	0	4	-.001	4
285		10	max	136.077	2	.175	6	.158	1	0	4	0	3	0	15
286			min	-129.977	3	.037	15	-.057	5	0	10	0	4	-.001	4
287		11	max	136.008	2	.028	2	.158	1	0	4	0	3	0	15
288			min	-130.029	3	-.031	3	-.042	3	0	10	0	4	-.001	4
289		12	max	135.94	2	-.046	15	.246	4	0	4	0	3	0	15
290			min	-130.08	3	-.18	4	-.042	3	0	10	0	4	-.001	4
291		13	max	135.871	2	-.088	15	.38	4	0	4	0	3	0	15
292			min	-130.132	3	-.357	4	-.042	3	0	10	0	4	-.001	4
293		14	max	135.802	2	-.13	15	.513	4	0	4	0	3	0	15
294			min	-130.183	3	-.534	4	-.042	3	0	10	0	4	-.001	4
295		15	max	135.734	2	-.171	15	.647	4	0	4	0	3	0	15
296			min	-130.234	3	-.711	4	-.042	3	0	10	0	5	0	4
297		16	max	135.665	2	-.213	15	.781	4	0	4	0	3	0	15
298			min	-130.286	3	-.888	4	-.042	3	0	10	0	5	0	4
299		17	max	135.597	2	-.255	15	.914	4	0	4	0	3	0	15
300			min	-130.337	3	-1.066	4	-.042	3	0	10	0	10	0	4
301		18	max	135.528	2	-.296	15	1.048	4	0	4	0	4	0	15
302			min	-130.389	3	-1.243	4	-.042	3	0	10	0	10	0	4
303		19	max	135.459	2	-.338	15	1.182	4	0	4	0	4	0	1
304			min	-130.44	3	-1.42	4	-.042	3	0	10	0	10	0	1
305	M12	1	max	292.629	1	0	1	.739	1	0	1	0	4	0	1
306			min	-31.257	3	0	1	-14.435	5	0	1	0	3	0	1
307		2	max	292.693	1	0	1	.739	1	0	1	0	1	0	1
308			min	-31.208	3	0	1	-14.491	5	0	1	-.001	5	0	1
309		3	max	292.758	1	0	1	.739	1	0	1	0	1	0	1
310			min	-31.16	3	0	1	-14.547	5	0	1	-.003	5	0	1
311		4	max	292.823	1	0	1	.739	1	0	1	0	1	0	1
312			min	-31.111	3	0	1	-14.603	5	0	1	-.004	5	0	1
313		5	max	292.887	1	0	1	.739	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	-31.063	3	0	1	-14.659	5	0	1	-.005	5	0	1
315		6	max	292.952	1	0	1	.739	1	0	1	0	1	0	1
316			min	-31.014	3	0	1	-14.715	5	0	1	-.006	5	0	1
317		7	max	293.017	1	0	1	.739	1	0	1	0	1	0	1
318			min	-30.966	3	0	1	-14.771	5	0	1	-.008	5	0	1
319		8	max	293.082	1	0	1	.739	1	0	1	0	1	0	1
320			min	-30.917	3	0	1	-14.827	5	0	1	-.009	5	0	1
321		9	max	293.146	1	0	1	.739	1	0	1	0	1	0	1
322			min	-30.869	3	0	1	-14.884	5	0	1	-.01	5	0	1
323		10	max	293.211	1	0	1	.739	1	0	1	0	1	0	1
324			min	-30.82	3	0	1	-14.94	5	0	1	-.012	5	0	1
325		11	max	293.276	1	0	1	.739	1	0	1	0	1	0	1
326			min	-30.772	3	0	1	-14.996	5	0	1	-.013	5	0	1
327		12	max	293.34	1	0	1	.739	1	0	1	0	1	0	1
328			min	-30.723	3	0	1	-15.052	5	0	1	-.014	5	0	1
329		13	max	293.405	1	0	1	.739	1	0	1	0	1	0	1
330			min	-30.675	3	0	1	-15.108	5	0	1	-.016	5	0	1
331		14	max	293.47	1	0	1	.739	1	0	1	0	1	0	1
332			min	-30.626	3	0	1	-15.164	5	0	1	-.017	5	0	1
333		15	max	293.535	1	0	1	.739	1	0	1	0	1	0	1
334			min	-30.578	3	0	1	-15.22	5	0	1	-.019	5	0	1
335		16	max	293.599	1	0	1	.739	1	0	1	.001	1	0	1
336			min	-30.529	3	0	1	-15.276	5	0	1	-.02	5	0	1
337		17	max	293.664	1	0	1	.739	1	0	1	.001	1	0	1
338			min	-30.48	3	0	1	-15.332	5	0	1	-.021	5	0	1
339		18	max	293.729	1	0	1	.739	1	0	1	.001	1	0	1
340			min	-30.432	3	0	1	-15.388	5	0	1	-.023	5	0	1
341		19	max	293.793	1	0	1	.739	1	0	1	.001	1	0	1
342			min	-30.383	3	0	1	-15.444	5	0	1	-.024	5	0	1
343	M1	1	max	71.379	1	334.434	3	.307	10	0	2	.034	1	0	2
344			min	4.988	10	-224.156	2	-17.087	1	0	3	0	10	0	3
345		2	max	71.497	1	334.245	3	.307	10	0	2	.03	1	.049	2
346			min	5.086	10	-224.409	2	-17.087	1	0	3	0	10	-.073	3
347		3	max	59.456	3	4.657	4	.308	10	0	5	.026	1	.097	2
348			min	-9.697	10	-19.328	2	-17.016	1	0	1	0	10	-.144	3
349		4	max	59.545	3	4.369	14	.308	10	0	5	.022	1	.101	2
350			min	-9.599	10	-19.582	2	-17.016	1	0	1	0	10	-.14	3
351		5	max	59.633	3	4.12	14	.308	10	0	5	.019	1	.105	2
352			min	-9.501	10	-19.835	2	-17.016	1	0	1	0	10	-.136	3
353		6	max	59.722	3	3.872	14	.308	10	0	5	.015	1	.11	2
354			min	-9.402	10	-20.088	2	-17.016	1	0	1	0	10	-.133	3
355		7	max	59.81	3	3.623	14	.308	10	0	5	.011	1	.114	2
356			min	-9.304	10	-20.341	2	-17.016	1	0	1	0	10	-.129	3
357		8	max	59.899	3	3.374	14	.308	10	0	5	.007	1	.118	2
358			min	-9.206	10	-20.594	2	-17.016	1	0	1	0	10	-.125	3
359		9	max	59.987	3	3.126	14	.308	10	0	5	.004	1	.123	2
360			min	-9.107	10	-20.847	2	-17.016	1	0	1	0	10	-.121	3
361		10	max	60.076	3	2.877	14	.308	10	0	5	.002	3	.127	2
362			min	-9.009	10	-21.1	2	-17.016	1	0	1	0	10	-.117	3
363		11	max	60.164	3	2.628	14	.308	10	0	5	0	3	.132	2
364			min	-8.911	10	-21.353	2	-17.016	1	0	1	-.004	1	-.113	3
365		12	max	60.253	3	2.38	14	.308	10	0	5	0	10	.137	2
366			min	-8.812	10	-21.606	2	-17.016	1	0	1	-.007	1	-.109	3
367		13	max	60.341	3	2.147	9	.308	10	0	5	0	10	.141	2
368			min	-8.714	10	-21.859	2	-17.016	1	0	1	-.011	1	-.105	3
369		14	max	60.43	3	1.936	9	.308	10	0	5	0	10	.146	2
370			min	-8.616	10	-22.112	2	-17.016	1	0	1	-.015	1	-.101	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	60.518	3	1.725	9	.308	10	0	5	0	10	.151	2
372			min	-8.517	10	-22.365	2	-17.016	1	0	1	-.018	1	-.097	3
373		16	max	84.119	2	83.212	2	.31	10	0	1	0	10	.155	2
374			min	-19.624	3	-121.287	3	-17.152	1	0	5	-.022	1	-.092	3
375		17	max	84.237	2	82.959	2	.31	10	0	1	0	10	.137	2
376			min	-19.535	3	-121.476	3	-17.152	1	0	5	-.026	1	-.065	3
377		18	max	-3.929	12	317.18	2	.328	10	0	5	0	10	.069	2
378			min	-71.482	1	-150.523	3	-25.509	4	0	2	-.03	1	-.033	3
379		19	max	-3.87	12	316.926	2	.328	10	0	5	0	10	0	2
380			min	-71.364	1	-150.713	3	-25.267	4	0	2	-.034	1	0	3
381	M5	1	max	175.572	1	1070.696	3	0	11	0	9	.029	4	0	3
382			min	-1.707	3	-710.122	2	-68.533	3	0	5	0	11	0	2
383		2	max	175.69	1	1070.506	3	0	11	0	9	.025	4	.154	2
384			min	-1.618	3	-710.375	2	-68.533	3	0	5	-.005	3	-.232	3
385		3	max	157.725	3	5.262	9	7.398	3	0	3	.021	4	.305	2
386			min	-25.011	10	-66.525	2	-16.376	4	0	4	-.019	3	-.459	3
387		4	max	157.814	3	5.051	9	7.398	3	0	3	.017	4	.319	2
388			min	-24.913	10	-66.778	2	-16.134	4	0	4	-.017	3	-.445	3
389		5	max	157.902	3	4.84	9	7.398	3	0	3	.014	4	.334	2
390			min	-24.815	10	-67.031	2	-15.892	4	0	4	-.016	3	-.432	3
391		6	max	157.991	3	4.629	9	7.398	3	0	3	.011	4	.349	2
392			min	-24.716	10	-67.284	2	-15.65	4	0	4	-.014	3	-.418	3
393		7	max	158.079	3	4.418	9	7.398	3	0	3	.007	4	.363	2
394			min	-24.618	10	-67.537	2	-15.408	4	0	4	-.013	3	-.404	3
395		8	max	158.168	3	4.207	9	7.398	3	0	3	.004	4	.378	2
396			min	-24.52	10	-67.79	2	-15.166	4	0	4	-.011	3	-.391	3
397		9	max	158.256	3	3.996	9	7.398	3	0	3	0	4	.393	2
398			min	-24.421	10	-68.043	2	-14.924	4	0	4	-.009	3	-.377	3
399		10	max	158.345	3	3.785	9	7.398	3	0	3	0	2	.407	2
400			min	-24.323	10	-68.296	2	-14.682	4	0	4	-.008	3	-.363	3
401		11	max	158.433	3	3.574	9	7.398	3	0	3	0	2	.422	2
402			min	-24.225	10	-68.549	2	-14.44	4	0	4	-.006	3	-.349	3
403		12	max	158.522	3	3.364	9	7.398	3	0	3	0	2	.437	2
404			min	-24.126	10	-68.802	2	-14.198	4	0	4	-.009	4	-.335	3
405		13	max	158.61	3	3.153	9	7.398	3	0	3	0	2	.452	2
406			min	-24.028	10	-69.055	2	-13.956	4	0	4	-.012	4	-.321	3
407		14	max	158.699	3	2.942	9	7.398	3	0	3	0	11	.467	2
408			min	-23.929	10	-69.309	2	-13.714	4	0	4	-.015	4	-.308	3
409		15	max	158.787	3	2.731	9	7.398	3	0	3	0	3	.482	2
410			min	-23.831	10	-69.562	2	-13.472	4	0	4	-.018	4	-.294	3
411		16	max	265.992	2	280.993	2	7.369	3	0	3	.001	3	.494	2
412			min	-62.415	3	-343.021	3	-12.183	4	0	4	-.021	4	-.277	3
413		17	max	266.11	2	280.74	2	7.369	3	0	3	.003	3	.433	2
414			min	-62.327	3	-343.211	3	-11.941	4	0	4	-.023	4	-.203	3
415		18	max	-2.825	12	1007.032	2	6.793	3	0	4	.004	3	.218	2
416			min	-175.727	1	-469.305	3	-27.096	5	0	9	-.029	4	-.101	3
417		19	max	-2.766	12	1006.779	2	6.793	3	0	4	.006	3	0	3
418			min	-175.609	1	-469.495	3	-26.854	5	0	9	-.035	4	0	2
419	M9	1	max	71.294	1	334.362	3	114.035	4	0	3	0	10	0	2
420			min	.636	15	-224.156	2	-.307	10	0	2	-.033	1	0	3
421		2	max	71.412	1	334.172	3	114.277	4	0	3	.024	5	.049	2
422			min	.672	15	-224.409	2	-.307	10	0	2	-.03	1	-.073	3
423		3	max	59.006	3	4.243	9	16.832	1	0	1	.046	5	.097	2
424			min	-9.367	10	-19.304	2	-21.117	5	0	10	-.026	1	-.144	3
425		4	max	59.095	3	4.032	9	16.832	1	0	1	.041	5	.101	2
426			min	-9.269	10	-19.557	2	-20.875	5	0	10	-.022	1	-.14	3
427		5	max	59.183	3	3.821	9	16.832	1	0	1	.037	5	.105	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-9.171	10	-19.81	2	-20.633	5	0	10	-.018	1	-.136	3
429		6	max	59.272	3	3.611	9	16.832	1	0	1	.033	5	.11	2
430			min	-9.072	10	-20.063	2	-20.391	5	0	10	-.015	1	-.133	3
431		7	max	59.36	3	3.4	9	16.832	1	0	1	.028	5	.114	2
432			min	-8.974	10	-20.317	2	-20.149	5	0	10	-.011	1	-.129	3
433		8	max	59.449	3	3.189	9	16.832	1	0	1	.024	5	.118	2
434			min	-8.876	10	-20.57	2	-19.907	5	0	10	-.007	1	-.125	3
435		9	max	59.537	3	2.978	9	16.832	1	0	1	.019	5	.123	2
436			min	-8.777	10	-20.823	2	-19.665	5	0	10	-.004	1	-.121	3
437		10	max	59.626	3	2.767	9	16.832	1	0	1	.015	4	.127	2
438			min	-8.679	10	-21.076	2	-19.423	5	0	10	0	1	-.117	3
439		11	max	59.715	3	2.556	9	16.832	1	0	1	.012	4	.132	2
440			min	-8.581	10	-21.329	2	-19.181	5	0	10	0	10	-.113	3
441		12	max	59.803	3	2.345	9	16.832	1	0	1	.009	3	.137	2
442			min	-8.482	10	-21.582	2	-18.939	5	0	10	0	10	-.109	3
443		13	max	59.892	3	2.134	9	16.832	1	0	1	.011	1	.141	2
444			min	-8.384	10	-21.835	2	-18.697	5	0	10	0	10	-.105	3
445		14	max	59.98	3	1.923	9	16.832	1	0	1	.015	1	.146	2
446			min	-8.286	10	-22.088	2	-18.455	5	0	10	-.001	5	-.101	3
447		15	max	60.069	3	1.712	9	16.832	1	0	1	.018	1	.151	2
448			min	-8.187	10	-22.341	2	-18.213	5	0	10	-.005	5	-.097	3
449		16	max	84.258	2	82.915	2	16.975	1	0	10	.022	1	.155	2
450			min	-20.53	3	-121.77	3	-16.827	5	0	4	-.008	5	-.092	3
451		17	max	84.376	2	82.662	2	16.975	1	0	10	.026	1	.137	2
452			min	-20.441	3	-121.96	3	-16.585	5	0	4	-.012	5	-.065	3
453		18	max	7.494	5	317.18	2	17.716	1	0	2	.03	1	.069	2
454			min	-71.39	1	-150.514	3	-30.771	5	0	3	-.018	5	-.033	3
455		19	max	7.549	5	316.927	2	17.716	1	0	2	.033	1	0	2
456			min	-71.272	1	-150.704	3	-30.529	5	0	3	-.025	5	0	3
457	M13	1	max	114.035	4	224.08	2	-.636	15	0	2	.033	1	0	2
458			min	-.307	10	-334.404	3	-71.29	1	0	3	0	10	0	3
459		2	max	109.669	4	159.773	2	.006	15	0	2	.013	3	.127	3
460			min	-.307	10	-237.768	3	-53.61	1	0	3	-.002	10	-.085	2
461		3	max	105.304	4	95.467	2	.883	5	0	2	.01	3	.211	3
462			min	-.307	10	-141.132	3	-35.93	1	0	3	-.014	1	-.142	2
463		4	max	100.939	4	31.16	2	1.876	5	0	2	.007	3	.253	3
464			min	-.307	10	-44.496	3	-18.249	1	0	3	-.026	1	-.17	2
465		5	max	96.574	4	52.139	3	2.87	5	0	2	.004	3	.251	3
466			min	-.307	10	-33.147	2	-5.148	3	0	3	-.03	1	-.17	2
467		6	max	92.209	4	148.775	3	17.111	1	0	2	.003	5	.206	3
468			min	-.307	10	-97.454	2	-4.214	3	0	3	-.027	1	-.141	2
469		7	max	87.844	4	245.411	3	34.792	1	0	2	.005	5	.119	3
470			min	-.307	10	-161.76	2	-3.279	3	0	3	-.015	1	-.083	2
471		8	max	83.478	4	342.047	3	52.472	1	0	2	.008	4	.005	1
472			min	-.307	10	-226.067	2	-2.345	3	0	3	0	3	-.012	3
473		9	max	79.113	4	438.682	3	70.152	1	0	2	.031	1	.118	2
474			min	-.307	10	-290.374	2	-1.411	3	0	3	-.001	3	-.185	3
475		10	max	74.748	4	-7.666	15	87.833	1	0	2	.067	1	.261	2
476			min	-.307	10	-535.318	3	.596	12	0	3	-.015	5	-.402	3
477		11	max	51.385	4	290.374	2	5.771	5	0	3	.031	1	.118	2
478			min	-.307	10	-438.682	3	-70.067	1	0	2	-.013	5	-.185	3
479		12	max	47.02	4	226.067	2	6.764	5	0	3	.006	2	.005	1
480			min	-.307	10	-342.047	3	-52.387	1	0	2	-.01	5	-.012	3
481		13	max	42.655	4	161.76	2	7.758	5	0	3	0	10	.119	3
482			min	-.307	10	-245.411	3	-34.707	1	0	2	-.015	1	-.083	2
483		14	max	38.289	4	97.454	2	8.751	5	0	3	-.002	10	.206	3
484			min	-.307	10	-148.775	3	-17.027	1	0	2	-.027	1	-.141	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	33.924	4	33.147	2	10.351	4	0	3	0	5	.251	3
486			min	-.307	10	-52.139	3	-2.793	2	0	2	-.03	1	-.17	2
487		16	max	29.559	4	44.496	3	18.334	1	0	3	.005	5	.253	3
488			min	-.307	10	-31.16	2	-.333	10	0	2	-.026	1	-.17	2
489		17	max	25.194	4	141.132	3	36.014	1	0	3	.01	5	.211	3
490			min	-.307	10	-95.467	2	1.441	10	0	2	-.014	1	-.142	2
491		18	max	20.829	4	237.768	3	53.695	1	0	3	.018	4	.127	3
492			min	-.307	10	-159.773	2	3.214	10	0	2	-.002	10	-.085	2
493		19	max	17.116	1	334.404	3	71.375	1	0	3	.034	1	0	2
494			min	-.307	10	-224.08	2	4.988	10	0	2	0	10	0	3
495	M16	1	max	30.519	5	317.019	2	7.549	5	0	3	.033	1	0	2
496			min	-17.686	1	-150.726	3	-71.276	1	0	2	-.025	5	0	3
497		2	max	26.154	5	225.811	2	8.542	5	0	3	.006	1	.057	3
498			min	-17.686	1	-107.894	3	-53.596	1	0	2	-.022	5	-.121	2
499		3	max	21.789	5	134.602	2	9.535	5	0	3	0	3	.096	3
500			min	-17.686	1	-65.061	3	-35.916	1	0	2	-.02	4	-.201	2
501		4	max	17.424	5	43.393	2	10.529	5	0	3	-.001	12	.115	3
502			min	-17.686	1	-22.229	3	-18.235	1	0	2	-.026	1	-.24	2
503		5	max	13.059	5	20.603	3	11.522	5	0	3	-.002	12	.116	3
504			min	-17.686	1	-47.815	2	-3.328	3	0	2	-.03	1	-.239	2
505		6	max	8.694	5	63.436	3	17.125	1	0	3	-.002	10	.097	3
506			min	-17.686	1	-139.024	2	-2.394	3	0	2	-.027	1	-.198	2
507		7	max	4.328	5	106.268	3	34.806	1	0	3	.003	5	.059	3
508			min	-17.686	1	-230.233	2	-1.459	3	0	2	-.015	1	-.116	2
509		8	max	2.238	3	149.101	3	52.486	1	0	3	.01	4	.007	2
510			min	-17.686	1	-321.442	2	-.525	3	0	2	-.006	3	0	15
511		9	max	2.238	3	191.933	3	70.166	1	0	3	.031	1	.17	2
512			min	-17.686	1	-412.65	2	.406	12	0	2	-.006	3	-.073	3
513		10	max	18.094	5	-7.591	15	87.847	1	0	14	.067	1	.374	2
514			min	-17.686	1	-503.859	2	-2.481	3	0	2	-.006	3	-.168	3
515		11	max	13.729	5	412.65	2	4.838	5	0	2	.031	1	.17	2
516			min	-17.655	1	-191.933	3	-70.074	1	0	3	-.01	5	-.073	3
517		12	max	9.364	5	321.442	2	5.832	5	0	2	.006	2	.007	2
518			min	-17.655	1	-149.101	3	-52.394	1	0	3	-.008	5	0	15
519		13	max	4.999	5	230.233	2	6.825	5	0	2	0	10	.059	3
520			min	-17.655	1	-106.268	3	-34.713	1	0	3	-.015	1	-.116	2
521		14	max	.634	5	139.024	2	7.818	5	0	2	0	12	.097	3
522			min	-17.655	1	-63.436	3	-17.033	1	0	3	-.027	1	-.198	2
523		15	max	.328	10	47.815	2	9.397	4	0	2	.002	5	.116	3
524			min	-17.655	1	-20.603	3	-2.786	2	0	3	-.03	1	-.239	2
525		16	max	.328	10	22.229	3	18.327	1	0	2	.006	5	.115	3
526			min	-17.655	1	-43.393	2	-.329	10	0	3	-.026	1	-.24	2
527		17	max	.328	10	65.061	3	36.008	1	0	2	.011	5	.096	3
528			min	-17.655	1	-134.602	2	1.444	10	0	3	-.014	1	-.201	2
529		18	max	.328	10	107.894	3	53.688	1	0	2	.018	4	.057	3
530			min	-20.923	4	-225.811	2	3.218	10	0	3	-.002	10	-.121	2
531		19	max	.328	10	150.726	3	71.368	1	0	2	.034	1	0	2
532			min	-25.288	4	-317.019	2	3.87	12	0	3	0	10	0	5
533	M15	1	max	0	1	.83	3	.133	3	0	1	0	1	0	1
534			min	-95.166	3	0	1	0	1	0	3	0	3	0	1
535		2	max	0	1	.737	3	.133	3	0	1	0	1	0	1
536			min	-95.231	3	0	1	0	1	0	3	0	3	0	3
537		3	max	0	1	.645	3	.133	3	0	1	0	1	0	1
538			min	-95.296	3	0	1	0	1	0	3	0	3	0	3
539		4	max	0	1	.553	3	.133	3	0	1	0	1	0	1
540			min	-95.362	3	0	1	0	1	0	3	0	3	0	3
541		5	max	0	1	.461	3	.133	3	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-95.427	3	0	1	0	1	0	3	0	3	0	3
543		6	max	0	1	.369	3	.133	3	0	1	0	1	0	1
544			min	-95.492	3	0	1	0	1	0	3	0	3	0	3
545		7	max	0	1	.277	3	.133	3	0	1	0	3	0	1
546			min	-95.557	3	0	1	0	1	0	3	0	1	0	3
547		8	max	0	1	.184	3	.133	3	0	1	0	3	0	1
548			min	-95.622	3	0	1	0	1	0	3	0	1	0	3
549		9	max	0	1	.092	3	.133	3	0	1	0	3	0	1
550			min	-95.688	3	0	1	0	1	0	3	0	1	-.001	3
551		10	max	0	1	0	1	.133	3	0	1	0	3	0	1
552			min	-95.753	3	0	1	0	1	0	3	0	1	-.001	3
553		11	max	0	1	0	1	.133	3	0	1	0	3	0	1
554			min	-95.818	3	-.092	3	0	1	0	3	0	1	-.001	3
555		12	max	0	1	0	1	.133	3	0	1	0	3	0	1
556			min	-95.883	3	-.184	3	0	1	0	3	0	1	0	3
557		13	max	0	1	0	1	.133	3	0	1	0	3	0	1
558			min	-95.948	3	-.277	3	0	1	0	3	0	1	0	3
559		14	max	0	1	0	1	.133	3	0	1	0	3	0	1
560			min	-96.014	3	-.369	3	0	1	0	3	0	1	0	3
561		15	max	0	1	0	1	.133	3	0	1	0	3	0	1
562			min	-96.079	3	-.461	3	0	1	0	3	0	1	0	3
563		16	max	0	1	0	1	.133	3	0	1	0	3	0	1
564			min	-96.144	3	-.553	3	0	1	0	3	0	1	0	3
565		17	max	0	1	0	1	.133	3	0	1	0	3	0	1
566			min	-96.209	3	-.645	3	0	1	0	3	0	1	0	3
567		18	max	0	1	0	1	.133	3	0	1	0	3	0	1
568			min	-96.274	3	-.737	3	0	1	0	3	0	1	0	3
569		19	max	0	1	0	1	.133	3	0	1	0	3	0	1
570			min	-96.339	3	-.83	3	0	1	0	3	0	1	0	1
571	M16A	1	max	0	2	2.082	4	.287	4	0	3	0	3	0	1
572			min	-168.315	4	0	2	-.054	3	0	1	0	4	0	1
573		2	max	0	2	1.85	4	.259	4	0	3	0	3	0	2
574			min	-168.308	4	0	2	-.054	3	0	1	0	4	0	4
575		3	max	0	2	1.619	4	.231	4	0	3	0	3	0	2
576			min	-168.3	4	0	2	-.054	3	0	1	0	4	-.001	4
577		4	max	0	2	1.388	4	.203	4	0	3	0	3	0	2
578			min	-168.292	4	0	2	-.054	3	0	1	0	1	-.001	4
579		5	max	0	2	1.156	4	.174	4	0	3	0	3	0	2
580			min	-168.285	4	0	2	-.054	3	0	1	0	1	-.002	4
581		6	max	0	2	.925	4	.146	4	0	3	0	3	0	2
582			min	-168.277	4	0	2	-.054	3	0	1	0	1	-.002	4
583		7	max	0	2	.694	4	.118	4	0	3	0	3	0	2
584			min	-168.27	4	0	2	-.054	3	0	1	0	1	-.002	4
585		8	max	0	2	.463	4	.09	4	0	3	0	5	0	2
586			min	-168.262	4	0	2	-.054	3	0	1	0	1	-.002	4
587		9	max	0	2	.231	4	.062	4	0	3	0	5	0	2
588			min	-168.255	4	0	2	-.054	3	0	1	0	1	-.003	4
589		10	max	0	2	0	1	.041	1	0	3	0	5	0	2
590			min	-168.247	4	0	1	-.054	3	0	1	0	1	-.003	4
591		11	max	0	2	0	2	.041	1	0	3	0	5	0	2
592			min	-168.24	4	-.231	4	-.054	3	0	1	0	1	-.003	4
593		12	max	0	2	0	2	.041	1	0	3	0	5	0	2
594			min	-168.232	4	-.463	4	-.054	3	0	1	0	1	-.002	4
595		13	max	0	2	0	2	.041	1	0	3	0	5	0	2
596			min	-168.225	4	-.694	4	-.055	5	0	1	0	3	-.002	4
597		14	max	0	2	0	2	.041	1	0	3	0	5	0	2
598			min	-168.217	4	-.925	4	-.083	5	0	1	0	3	-.002	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.047	1	0	2	.041	1	0	3	0	5	0	2
600			min	-168.209	4	-1.156	4	-.111	5	0	1	0	3	-.002	4
601		16	max	.134	1	0	2	.041	1	0	3	0	1	0	2
602			min	-168.202	4	-1.388	4	-.139	5	0	1	0	3	-.001	4
603		17	max	.221	1	0	2	.041	1	0	3	0	1	0	2
604			min	-168.194	4	-1.619	4	-.167	5	0	1	0	3	-.001	4
605		18	max	.308	1	0	2	.041	1	0	3	0	1	0	2
606			min	-168.237	5	-1.85	4	-.196	5	0	1	0	3	0	4
607		19	max	.395	1	0	2	.041	1	0	3	0	1	0	1
608			min	-168.301	5	-2.082	4	-.224	5	0	1	0	5	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	1	.008	2	.003	1	8.871e-4	5	NC	3	NC	1
2			min	-.003	3	-.008	3	-.009	5	-2.656e-4	1	4655.349	2	NC	1
3		2	max	.002	1	.007	2	.002	1	9.073e-4	5	NC	3	NC	1
4			min	-.003	3	-.007	3	-.009	5	-2.537e-4	1	5075.448	2	NC	1
5		3	max	.002	1	.007	2	.002	1	9.275e-4	5	NC	1	NC	1
6			min	-.003	3	-.007	3	-.009	5	-2.419e-4	1	5574.236	2	NC	1
7		4	max	.002	1	.006	2	.002	1	9.477e-4	5	NC	1	NC	1
8			min	-.003	3	-.007	3	-.008	5	-2.301e-4	1	6170.699	2	NC	1
9		5	max	.002	1	.005	2	.002	1	9.679e-4	5	NC	1	NC	1
10			min	-.002	3	-.006	3	-.008	5	-2.182e-4	1	6890.149	2	NC	1
11		6	max	.001	1	.005	2	.002	1	9.882e-4	5	NC	1	NC	1
12			min	-.002	3	-.006	3	-.008	5	-2.064e-4	1	7766.895	2	NC	1
13		7	max	.001	1	.004	2	.001	1	1.008e-3	5	NC	1	NC	1
14			min	-.002	3	-.006	3	-.007	5	-1.946e-4	1	8848.348	2	NC	1
15		8	max	.001	1	.004	2	.001	1	1.029e-3	5	NC	1	NC	1
16			min	-.002	3	-.005	3	-.007	5	-1.827e-4	1	NC	1	NC	1
17		9	max	.001	1	.003	2	.001	1	1.049e-3	5	NC	1	NC	1
18			min	-.002	3	-.005	3	-.007	5	-1.709e-4	1	NC	1	NC	1
19		10	max	0	1	.003	2	0	1	1.069e-3	5	NC	1	NC	1
20			min	-.002	3	-.005	3	-.006	5	-1.591e-4	1	NC	1	NC	1
21		11	max	0	1	.002	2	0	1	1.089e-3	5	NC	1	NC	1
22			min	-.001	3	-.004	3	-.006	5	-1.473e-4	1	NC	1	NC	1
23		12	max	0	1	.002	2	0	1	1.109e-3	5	NC	1	NC	1
24			min	-.001	3	-.004	3	-.005	5	-1.354e-4	1	NC	1	NC	1
25		13	max	0	1	.001	2	0	1	1.13e-3	5	NC	1	NC	1
26			min	-.001	3	-.003	3	-.004	5	-1.236e-4	1	NC	1	NC	1
27		14	max	0	1	.001	2	0	1	1.15e-3	5	NC	1	NC	1
28			min	0	3	-.003	3	-.004	5	-1.118e-4	1	NC	1	NC	1
29		15	max	0	1	0	2	0	1	1.17e-3	5	NC	1	NC	1
30			min	0	3	-.002	3	-.003	5	-9.993e-5	1	NC	1	NC	1
31		16	max	0	1	0	2	0	1	1.19e-3	5	NC	1	NC	1
32			min	0	3	-.002	3	-.002	5	-8.81e-5	1	NC	1	NC	1
33		17	max	0	1	0	2	0	1	1.21e-3	5	NC	1	NC	1
34			min	0	3	-.001	3	-.002	5	-7.628e-5	1	NC	1	NC	1
35		18	max	0	1	0	2	0	1	1.231e-3	5	NC	1	NC	1
36			min	0	3	0	3	0	5	-6.445e-5	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	1.251e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-5.262e-5	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	2.455e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-5.818e-4	5	NC	1	NC	1
41		2	max	0	3	0	2	.003	5	3.297e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	1	-5.851e-4	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	3	0	2	.006	5	4.138e-5	1	NC	1	NC	1
44			min	0	2	-.002	3	0	1	-5.884e-4	5	NC	1	NC	1
45		4	max	0	3	0	2	.009	5	4.979e-5	1	NC	1	NC	1
46			min	0	2	-.002	3	0	1	-5.918e-4	5	NC	1	NC	1
47		5	max	0	3	0	2	.012	4	5.821e-5	1	NC	1	NC	1
48			min	0	2	-.003	3	0	9	-5.951e-4	5	NC	1	NC	1
49		6	max	0	3	0	2	.015	4	6.662e-5	1	NC	1	NC	1
50			min	0	2	-.004	3	0	9	-5.984e-4	5	NC	1	NC	1
51		7	max	0	3	0	2	.018	4	7.504e-5	1	NC	1	NC	1
52			min	0	2	-.005	3	0	9	-6.017e-4	5	NC	1	NC	1
53		8	max	0	3	0	2	.021	4	8.345e-5	1	NC	1	NC	1
54			min	0	2	-.005	3	0	9	-6.05e-4	5	NC	1	NC	1
55		9	max	0	3	.001	2	.024	4	9.186e-5	1	NC	1	NC	1
56			min	0	2	-.006	3	0	10	-6.083e-4	5	NC	1	NC	1
57		10	max	0	3	.001	2	.026	4	1.003e-4	1	NC	1	NC	1
58			min	0	2	-.006	3	0	10	-6.116e-4	5	NC	1	NC	1
59		11	max	0	3	.002	2	.029	4	1.087e-4	1	NC	1	NC	1
60			min	0	2	-.007	3	0	10	-6.149e-4	5	NC	1	NC	1
61		12	max	0	3	.002	2	.032	4	1.171e-4	1	NC	1	NC	1
62			min	0	2	-.007	3	0	10	-6.182e-4	5	NC	1	NC	1
63		13	max	0	3	.003	2	.034	4	1.255e-4	1	NC	1	NC	1
64			min	-.001	2	-.007	3	0	10	-6.215e-4	5	NC	1	NC	1
65		14	max	.001	3	.004	2	.036	4	1.339e-4	1	NC	1	NC	1
66			min	-.001	2	-.007	3	0	10	-6.248e-4	5	NC	1	NC	1
67		15	max	.001	3	.005	2	.039	4	1.423e-4	1	NC	1	NC	1
68			min	-.001	2	-.007	3	0	10	-6.281e-4	5	NC	1	NC	1
69		16	max	.001	3	.005	2	.041	4	1.508e-4	1	NC	1	NC	1
70			min	-.001	2	-.008	3	0	10	-6.314e-4	5	8483.966	2	NC	1
71		17	max	.001	3	.006	2	.043	4	1.592e-4	1	NC	1	NC	1
72			min	-.001	2	-.008	3	0	10	-6.347e-4	5	7245.522	2	NC	1
73		18	max	.001	3	.007	2	.045	4	1.676e-4	1	NC	1	NC	1
74			min	-.001	2	-.008	3	0	10	-6.38e-4	5	6287.741	2	NC	1
75		19	max	.001	3	.008	2	.047	4	1.76e-4	1	NC	3	NC	1
76			min	-.002	2	-.007	3	0	10	-6.414e-4	5	5539.216	2	NC	1
77	M4	1	max	.001	1	.009	2	0	10	2.787e-3	5	NC	1	NC	1
78			min	0	3	-.008	3	-.05	4	-2.08e-4	1	NC	1	387.802	4
79		2	max	.001	1	.008	2	0	10	2.787e-3	5	NC	1	NC	1
80			min	0	3	-.007	3	-.046	4	-2.08e-4	1	NC	1	422.708	4
81		3	max	.001	1	.008	2	0	10	2.787e-3	5	NC	1	NC	1
82			min	0	3	-.007	3	-.042	4	-2.08e-4	1	NC	1	464.247	4
83		4	max	.001	1	.007	2	0	10	2.787e-3	5	NC	1	NC	1
84			min	0	3	-.006	3	-.038	4	-2.08e-4	1	NC	1	514.166	4
85		5	max	.001	1	.007	2	0	10	2.787e-3	5	NC	1	NC	1
86			min	0	3	-.006	3	-.034	4	-2.08e-4	1	NC	1	574.845	4
87		6	max	.001	1	.006	2	0	10	2.787e-3	5	NC	1	NC	1
88			min	0	3	-.005	3	-.03	4	-2.08e-4	1	NC	1	649.592	4
89		7	max	0	1	.006	2	0	10	2.787e-3	5	NC	1	NC	1
90			min	0	3	-.005	3	-.026	4	-2.08e-4	1	NC	1	743.12	4
91		8	max	0	1	.005	2	0	10	2.787e-3	5	NC	1	NC	1
92			min	0	3	-.005	3	-.022	4	-2.08e-4	1	NC	1	862.329	4
93		9	max	0	1	.005	2	0	10	2.787e-3	5	NC	1	NC	1
94			min	0	3	-.004	3	-.019	4	-2.08e-4	1	NC	1	1017.655	4
95		10	max	0	1	.004	2	0	10	2.787e-3	5	NC	1	NC	1
96			min	0	3	-.004	3	-.016	4	-2.08e-4	1	NC	1	1225.5	4
97		11	max	0	1	.004	2	0	10	2.787e-3	5	NC	1	NC	1
98			min	0	3	-.003	3	-.013	4	-2.08e-4	1	NC	1	1512.879	4
99		12	max	0	1	.003	2	0	10	2.787e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	3	-.003	3	-.01	4	-2.08e-4	1	NC	1	1926.909	4
101		13	max	0	1	.003	2	0	10	2.787e-3	5	NC	1	NC	1
102			min	0	3	-.003	3	-.008	4	-2.08e-4	1	NC	1	2555.967	4
103		14	max	0	1	.002	2	0	10	2.787e-3	5	NC	1	NC	1
104			min	0	3	-.002	3	-.005	4	-2.08e-4	1	NC	1	3582.334	4
105		15	max	0	1	.002	2	0	10	2.787e-3	5	NC	1	NC	1
106			min	0	3	-.002	3	-.004	4	-2.08e-4	1	NC	1	5434.223	4
107		16	max	0	1	.001	2	0	10	2.787e-3	5	NC	1	NC	1
108			min	0	3	-.001	3	-.002	4	-2.08e-4	1	NC	1	9328.88	4
109		17	max	0	1	0	2	0	10	2.787e-3	5	NC	1	NC	1
110			min	0	3	0	3	0	4	-2.08e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	10	2.787e-3	5	NC	1	NC	1
112			min	0	3	0	3	0	4	-2.08e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	2.787e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-2.08e-4	1	NC	1	NC	1
115	M6	1	max	.006	1	.025	2	0	9	9.422e-4	4	NC	3	NC	1
116			min	-.01	3	-.022	3	-.009	5	-8.435e-8	2	1444.667	2	6672.031	3
117		2	max	.006	1	.024	2	0	9	9.623e-4	4	NC	3	NC	1
118			min	-.009	3	-.021	3	-.009	5	-7.968e-8	2	1545.704	2	7106.457	3
119		3	max	.005	1	.022	2	0	9	9.824e-4	4	NC	3	NC	1
120			min	-.009	3	-.02	3	-.009	5	-1.558e-6	1	1661.476	2	7619.929	3
121		4	max	.005	1	.02	2	0	9	1.003e-3	4	NC	3	NC	1
122			min	-.008	3	-.019	3	-.008	5	-3.148e-6	1	1794.947	2	8229.708	3
123		5	max	.005	1	.019	2	0	9	1.023e-3	4	NC	3	NC	1
124			min	-.008	3	-.018	3	-.008	5	-4.739e-6	1	1949.94	2	8958.642	3
125		6	max	.004	1	.017	2	0	9	1.043e-3	4	NC	3	NC	1
126			min	-.007	3	-.017	3	-.008	5	-6.329e-6	1	2131.462	2	9837.443	3
127		7	max	.004	1	.015	2	0	9	1.063e-3	4	NC	3	NC	1
128			min	-.006	3	-.015	3	-.008	5	-7.919e-6	1	2346.197	2	NC	1
129		8	max	.004	1	.014	2	0	9	1.083e-3	4	NC	3	NC	1
130			min	-.006	3	-.014	3	-.007	5	-9.509e-6	1	2603.269	2	NC	1
131		9	max	.003	1	.012	2	0	9	1.103e-3	4	NC	3	NC	1
132			min	-.005	3	-.013	3	-.007	5	-1.11e-5	1	2915.458	2	NC	1
133		10	max	.003	1	.011	2	0	9	1.123e-3	4	NC	3	NC	1
134			min	-.005	3	-.012	3	-.006	5	-1.269e-5	1	3301.231	2	NC	1
135		11	max	.003	1	.01	2	0	9	1.144e-3	4	NC	3	NC	1
136			min	-.004	3	-.01	3	-.006	5	-1.428e-5	1	3788.293	2	NC	1
137		12	max	.002	1	.008	2	0	9	1.164e-3	4	NC	3	NC	1
138			min	-.004	3	-.009	3	-.005	5	-1.587e-5	1	4420.185	2	NC	1
139		13	max	.002	1	.007	2	0	9	1.184e-3	4	NC	3	NC	1
140			min	-.003	3	-.008	3	-.004	5	-1.746e-5	1	5269.474	2	NC	1
141		14	max	.002	1	.006	2	0	9	1.204e-3	4	NC	1	NC	1
142			min	-.003	3	-.007	3	-.004	5	-1.905e-5	1	6466.773	2	NC	1
143		15	max	.001	1	.004	2	0	9	1.224e-3	4	NC	1	NC	1
144			min	-.002	3	-.005	3	-.003	5	-2.064e-5	1	8273.291	2	NC	1
145		16	max	.001	1	.003	2	0	1	1.244e-3	4	NC	1	NC	1
146			min	-.002	3	-.004	3	-.002	5	-2.223e-5	1	NC	1	NC	1
147		17	max	0	1	.002	2	0	1	1.264e-3	4	NC	1	NC	1
148			min	-.001	3	-.003	3	-.002	5	-2.382e-5	1	NC	1	NC	1
149		18	max	0	1	.001	2	0	1	1.284e-3	4	NC	1	NC	1
150			min	0	3	-.001	3	0	5	-2.541e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.305e-3	4	NC	1	NC	1
152			min	0	1	0	1	0	1	-2.7e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	1.254e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-6.067e-4	4	NC	1	NC	1
155		2	max	0	3	.001	2	.003	4	1.165e-5	1	NC	1	NC	1
156			min	0	2	-.002	3	0	1	-5.994e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	3	.002	2	.006	4	1.076e-5	1	NC	1	NC	1
158			min	0	2	-.003	3	0	1	-5.921e-4	4	NC	1	NC	1
159		4	max	0	3	.004	2	.009	4	9.867e-6	1	NC	1	NC	1
160			min	0	2	-.005	3	0	1	-5.848e-4	4	NC	1	NC	1
161		5	max	0	3	.005	2	.013	4	8.974e-6	1	NC	1	NC	1
162			min	-.001	2	-.007	3	0	1	-5.774e-4	4	9855.249	2	NC	1
163		6	max	.001	3	.006	2	.016	4	1.877e-5	3	NC	1	NC	1
164			min	-.001	2	-.008	3	0	1	-5.701e-4	4	7897.557	2	NC	1
165		7	max	.001	3	.007	2	.019	4	4.102e-5	3	NC	1	NC	1
166			min	-.002	2	-.01	3	0	1	-5.628e-4	4	6554.328	2	NC	1
167		8	max	.002	3	.008	2	.022	4	6.328e-5	3	NC	3	NC	1
168			min	-.002	2	-.011	3	0	1	-5.555e-4	4	5566.534	2	NC	1
169		9	max	.002	3	.01	2	.025	4	8.553e-5	3	NC	3	NC	1
170			min	-.002	2	-.013	3	0	1	-5.481e-4	4	4805.233	2	NC	1
171		10	max	.002	3	.011	2	.027	4	1.078e-4	3	NC	3	NC	1
172			min	-.003	2	-.014	3	0	1	-5.408e-4	4	4198.977	2	NC	1
173		11	max	.002	3	.012	2	.03	4	1.3e-4	3	NC	3	NC	1
174			min	-.003	2	-.015	3	0	1	-5.335e-4	4	3704.824	2	NC	1
175		12	max	.002	3	.014	2	.033	4	1.523e-4	3	NC	3	NC	1
176			min	-.003	2	-.016	3	0	1	-5.262e-4	4	3295.22	2	NC	1
177		13	max	.003	3	.016	2	.035	4	1.745e-4	3	NC	3	NC	1
178			min	-.003	2	-.018	3	0	9	-5.188e-4	4	2951.498	2	NC	1
179		14	max	.003	3	.017	2	.038	4	1.968e-4	3	NC	3	NC	1
180			min	-.004	2	-.018	3	0	9	-5.115e-4	4	2660.423	2	NC	1
181		15	max	.003	3	.019	2	.04	4	2.19e-4	3	NC	3	NC	1
182			min	-.004	2	-.019	3	0	9	-5.042e-4	4	2412.252	2	NC	1
183		16	max	.003	3	.021	2	.042	4	2.413e-4	3	NC	3	NC	1
184			min	-.004	2	-.02	3	0	9	-4.969e-4	4	2199.589	2	NC	1
185		17	max	.004	3	.023	2	.044	4	2.635e-4	3	NC	3	NC	1
186			min	-.005	2	-.021	3	0	9	-4.895e-4	4	2016.682	2	NC	1
187		18	max	.004	3	.025	2	.046	4	2.858e-4	3	NC	3	NC	1
188			min	-.005	2	-.022	3	0	9	-4.822e-4	4	1858.98	2	NC	1
189		19	max	.004	3	.027	2	.049	4	3.08e-4	3	NC	3	NC	1
190			min	-.005	2	-.023	3	0	9	-4.749e-4	4	1722.83	2	NC	1
191	M8	1	max	.004	1	.028	2	0	9	2.632e-3	4	NC	1	NC	1
192			min	0	3	-.023	3	-.051	4	-2.3e-4	3	NC	1	380.747	4
193		2	max	.004	1	.027	2	0	9	2.632e-3	4	NC	1	NC	1
194			min	0	3	-.021	3	-.047	4	-2.3e-4	3	NC	1	415.018	4
195		3	max	.004	1	.025	2	0	9	2.632e-3	4	NC	1	NC	1
196			min	0	3	-.02	3	-.042	4	-2.3e-4	3	NC	1	455.803	4
197		4	max	.003	1	.024	2	0	9	2.632e-3	4	NC	1	NC	1
198			min	0	3	-.019	3	-.038	4	-2.3e-4	3	NC	1	504.816	4
199		5	max	.003	1	.022	2	0	9	2.632e-3	4	NC	1	NC	1
200			min	0	3	-.018	3	-.034	4	-2.3e-4	3	NC	1	564.394	4
201		6	max	.003	1	.021	2	0	9	2.632e-3	4	NC	1	NC	1
202			min	0	3	-.016	3	-.03	4	-2.3e-4	3	NC	1	637.786	4
203		7	max	.003	1	.019	2	0	9	2.632e-3	4	NC	1	NC	1
204			min	0	3	-.015	3	-.026	4	-2.3e-4	3	NC	1	729.619	4
205		8	max	.002	1	.017	2	0	9	2.632e-3	4	NC	1	NC	1
206			min	0	3	-.014	3	-.023	4	-2.3e-4	3	NC	1	846.668	4
207		9	max	.002	1	.016	2	0	9	2.632e-3	4	NC	1	NC	1
208			min	0	3	-.013	3	-.019	4	-2.3e-4	3	NC	1	999.179	4
209		10	max	.002	1	.014	2	0	9	2.632e-3	4	NC	1	NC	1
210			min	0	3	-.011	3	-.016	4	-2.3e-4	3	NC	1	1203.26	4
211		11	max	.002	1	.013	2	0	9	2.632e-3	4	NC	1	NC	1
212			min	0	3	-.01	3	-.013	4	-2.3e-4	3	NC	1	1485.434	4
213		12	max	.002	1	.011	2	0	9	2.632e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	3	-.009	3	-.01	4	-2.3e-4	3	NC	1	1891.969	4
215		13	max	.001	1	.009	2	0	9	2.632e-3	4	NC	1	NC	1
216			min	0	3	-.008	3	-.008	4	-2.3e-4	3	NC	1	2509.64	4
217		14	max	.001	1	.008	2	0	9	2.632e-3	4	NC	1	NC	1
218			min	0	3	-.006	3	-.005	4	-2.3e-4	3	NC	1	3517.434	4
219		15	max	0	1	.006	2	0	9	2.632e-3	4	NC	1	NC	1
220			min	0	3	-.005	3	-.004	4	-2.3e-4	3	NC	1	5335.82	4
221		16	max	0	1	.005	2	0	9	2.632e-3	4	NC	1	NC	1
222			min	0	3	-.004	3	-.002	4	-2.3e-4	3	NC	1	9160.033	4
223		17	max	0	1	.003	2	0	9	2.632e-3	4	NC	1	NC	1
224			min	0	3	-.003	3	0	4	-2.3e-4	3	NC	1	NC	1
225		18	max	0	1	.002	2	0	9	2.632e-3	4	NC	1	NC	1
226			min	0	3	-.001	3	0	4	-2.3e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	2.632e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-2.3e-4	3	NC	1	NC	1
229	M10	1	max	.002	1	.008	2	0	3	2.659e-4	1	NC	3	NC	1
230			min	-.003	3	-.007	3	-.004	4	-4.992e-4	3	4660.915	2	NC	1
231		2	max	.002	1	.007	2	0	3	2.53e-4	1	NC	3	NC	1
232			min	-.003	3	-.007	3	-.004	4	-4.831e-4	3	5081.671	2	NC	1
233		3	max	.002	1	.007	2	0	3	2.56e-4	4	NC	1	NC	1
234			min	-.002	3	-.007	3	-.004	4	-4.669e-4	3	5581.27	2	NC	1
235		4	max	.002	1	.006	2	0	3	3.04e-4	4	NC	1	NC	1
236			min	-.002	3	-.007	3	-.005	4	-4.508e-4	3	6178.742	2	NC	1
237		5	max	.002	1	.005	2	0	3	3.52e-4	4	NC	1	NC	1
238			min	-.002	3	-.006	3	-.005	4	-4.346e-4	3	6899.459	2	NC	1
239		6	max	.001	1	.005	2	0	3	4.e-4	4	NC	1	NC	1
240			min	-.002	3	-.006	3	-.005	4	-4.185e-4	3	7777.818	2	NC	1
241		7	max	.001	1	.004	2	0	3	4.48e-4	4	NC	1	NC	1
242			min	-.002	3	-.006	3	-.005	4	-4.023e-4	3	8861.354	2	NC	1
243		8	max	.001	1	.004	2	0	3	4.96e-4	4	NC	1	NC	1
244			min	-.002	3	-.005	3	-.004	4	-3.862e-4	3	NC	1	NC	1
245		9	max	.001	1	.003	2	0	3	5.439e-4	4	NC	1	NC	1
246			min	-.001	3	-.005	3	-.004	4	-3.7e-4	3	NC	1	NC	1
247		10	max	0	1	.003	2	0	3	5.919e-4	4	NC	1	NC	1
248			min	-.001	3	-.005	3	-.004	4	-3.539e-4	3	NC	1	NC	1
249		11	max	0	1	.002	2	0	3	6.399e-4	4	NC	1	NC	1
250			min	-.001	3	-.004	3	-.004	4	-3.377e-4	3	NC	1	NC	1
251		12	max	0	1	.002	2	0	3	6.879e-4	4	NC	1	NC	1
252			min	-.001	3	-.004	3	-.004	4	-3.216e-4	3	NC	1	NC	1
253		13	max	0	1	.001	2	0	3	7.359e-4	4	NC	1	NC	1
254			min	0	3	-.003	3	-.003	4	-3.054e-4	3	NC	1	NC	1
255		14	max	0	1	.001	2	0	3	7.839e-4	4	NC	1	NC	1
256			min	0	3	-.003	3	-.003	4	-2.893e-4	3	NC	1	NC	1
257		15	max	0	1	0	2	0	3	8.319e-4	4	NC	1	NC	1
258			min	0	3	-.002	3	-.002	4	-2.731e-4	3	NC	1	NC	1
259		16	max	0	1	0	2	0	3	8.799e-4	4	NC	1	NC	1
260			min	0	3	-.002	3	-.002	4	-2.57e-4	3	NC	1	NC	1
261		17	max	0	1	0	2	0	3	9.279e-4	4	NC	1	NC	1
262			min	0	3	-.001	3	-.001	4	-2.408e-4	3	NC	1	NC	1
263		18	max	0	1	0	2	0	3	9.759e-4	4	NC	1	NC	1
264			min	0	3	0	3	0	4	-2.247e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.024e-3	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-2.085e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	9.718e-5	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-4.766e-4	4	NC	1	NC	1
269		2	max	0	3	0	2	.002	4	7.524e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-5.186e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	3	0	2	.005	4	5.33e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-5.605e-4	4	NC	1	NC	1
273		4	max	0	3	0	2	.008	4	3.136e-5	3	NC	1	NC	1
274			min	0	2	-.002	3	-.001	3	-6.025e-4	4	NC	1	NC	1
275		5	max	0	3	0	2	.01	4	9.419e-6	3	NC	1	NC	1
276			min	0	2	-.003	3	-.002	3	-6.444e-4	4	NC	1	NC	1
277		6	max	0	3	0	2	.013	4	1.159e-6	10	NC	1	NC	1
278			min	0	2	-.004	3	-.002	3	-6.864e-4	4	NC	1	NC	1
279		7	max	0	3	0	2	.015	5	1.322e-6	10	NC	1	NC	1
280			min	0	2	-.005	3	-.002	3	-7.283e-4	4	NC	1	NC	1
281		8	max	0	3	0	2	.018	5	1.486e-6	10	NC	1	NC	1
282			min	0	2	-.005	3	-.002	3	-7.703e-4	4	NC	1	NC	1
283		9	max	0	3	.001	2	.02	5	1.649e-6	10	NC	1	NC	1
284			min	0	2	-.006	3	-.003	3	-8.122e-4	4	NC	1	NC	1
285		10	max	0	3	.001	2	.023	5	1.812e-6	10	NC	1	NC	1
286			min	0	2	-.006	3	-.003	3	-8.542e-4	4	NC	1	NC	1
287		11	max	0	3	.002	2	.025	5	1.975e-6	10	NC	1	NC	1
288			min	0	2	-.007	3	-.003	3	-8.961e-4	4	NC	1	NC	1
289		12	max	0	3	.002	2	.027	5	2.138e-6	10	NC	1	NC	1
290			min	0	2	-.007	3	-.003	3	-9.381e-4	4	NC	1	NC	1
291		13	max	0	3	.003	2	.03	5	2.301e-6	10	NC	1	NC	1
292			min	-.001	2	-.007	3	-.003	3	-9.8e-4	4	NC	1	NC	1
293		14	max	.001	3	.004	2	.032	5	2.464e-6	10	NC	1	NC	1
294			min	-.001	2	-.007	3	-.003	3	-1.022e-3	4	NC	1	NC	1
295		15	max	.001	3	.005	2	.034	5	2.627e-6	10	NC	1	NC	1
296			min	-.001	2	-.008	3	-.003	3	-1.064e-3	4	NC	1	NC	1
297		16	max	.001	3	.005	2	.036	5	2.79e-6	10	NC	1	NC	1
298			min	-.001	2	-.008	3	-.003	3	-1.106e-3	4	8494.918	2	NC	1
299		17	max	.001	3	.006	2	.038	5	2.953e-6	10	NC	1	NC	1
300			min	-.001	2	-.008	3	-.003	3	-1.148e-3	4	7253.969	2	NC	1
301		18	max	.001	3	.007	2	.041	5	3.116e-6	10	NC	1	NC	1
302			min	-.001	2	-.008	3	-.003	1	-1.19e-3	4	6294.446	2	NC	1
303		19	max	.001	3	.008	2	.043	5	3.279e-6	10	NC	3	NC	1
304			min	-.002	2	-.008	3	-.003	1	-1.232e-3	4	5544.686	2	NC	1
305	M12	1	max	.001	1	.009	2	.002	1	3.286e-3	4	NC	1	NC	2
306			min	0	3	-.008	3	-.047	5	-3.893e-6	10	NC	1	413.537	5
307		2	max	.001	1	.008	2	.002	1	3.286e-3	4	NC	1	NC	2
308			min	0	3	-.007	3	-.043	5	-3.893e-6	10	NC	1	450.749	5
309		3	max	.001	1	.008	2	.002	1	3.286e-3	4	NC	1	NC	2
310			min	0	3	-.007	3	-.039	5	-3.893e-6	10	NC	1	495.031	5
311		4	max	.001	1	.007	2	.002	1	3.286e-3	4	NC	1	NC	1
312			min	0	3	-.006	3	-.035	5	-3.893e-6	10	NC	1	548.246	5
313		5	max	.001	1	.007	2	.002	1	3.286e-3	4	NC	1	NC	1
314			min	0	3	-.006	3	-.032	5	-3.893e-6	10	NC	1	612.929	5
315		6	max	.001	1	.006	2	.001	1	3.286e-3	4	NC	1	NC	1
316			min	0	3	-.005	3	-.028	5	-3.893e-6	10	NC	1	692.609	5
317		7	max	0	1	.006	2	.001	1	3.286e-3	4	NC	1	NC	1
318			min	0	3	-.005	3	-.024	5	-3.893e-6	10	NC	1	792.306	5
319		8	max	0	1	.005	2	.001	1	3.286e-3	4	NC	1	NC	1
320			min	0	3	-.005	3	-.021	5	-3.893e-6	10	NC	1	919.377	5
321		9	max	0	1	.005	2	0	1	3.286e-3	4	NC	1	NC	1
322			min	0	3	-.004	3	-.018	5	-3.893e-6	10	NC	1	1084.942	5
323		10	max	0	1	.004	2	0	1	3.286e-3	4	NC	1	NC	1
324			min	0	3	-.004	3	-.015	5	-3.893e-6	10	NC	1	1306.485	5
325		11	max	0	1	.004	2	0	1	3.286e-3	4	NC	1	NC	1
326			min	0	3	-.003	3	-.012	5	-3.893e-6	10	NC	1	1612.798	5
327		12	max	0	1	.003	2	0	1	3.286e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	3	-.003	3	-.009	5	-3.893e-6	10	NC	1	2054.099	5
329		13	max	0	1	.003	2	0	1	3.286e-3	4	NC	1	NC	1
330			min	0	3	-.003	3	-.007	5	-3.893e-6	10	NC	1	2724.577	5
331		14	max	0	1	.002	2	0	1	3.286e-3	4	NC	1	NC	1
332			min	0	3	-.002	3	-.005	5	-3.893e-6	10	NC	1	3818.504	5
333		15	max	0	1	.002	2	0	1	3.286e-3	4	NC	1	NC	1
334			min	0	3	-.002	3	-.003	5	-3.893e-6	10	NC	1	5792.257	5
335		16	max	0	1	.001	2	0	1	3.286e-3	4	NC	1	NC	1
336			min	0	3	-.001	3	-.002	5	-3.893e-6	10	NC	1	9943.114	5
337		17	max	0	1	0	2	0	1	3.286e-3	4	NC	1	NC	1
338			min	0	3	0	3	0	5	-3.893e-6	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	3.286e-3	4	NC	1	NC	1
340			min	0	3	0	3	0	5	-3.893e-6	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	3.286e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	-3.893e-6	10	NC	1	NC	1
343	M1	1	max	.007	3	.023	3	.005	5	5.883e-3	2	NC	1	NC	1
344			min	-.007	2	-.019	2	0	9	-8.395e-3	3	NC	1	NC	1
345		2	max	.007	3	.013	3	.007	5	2.902e-3	2	NC	4	NC	1
346			min	-.007	2	-.011	2	-.002	1	-4.13e-3	3	4989.118	3	NC	1
347		3	max	.007	3	.004	3	.009	5	2.537e-4	5	NC	4	NC	1
348			min	-.007	2	-.003	2	-.003	1	-1.297e-4	1	2587.642	3	NC	1
349		4	max	.007	3	.004	2	.012	5	2.517e-4	5	NC	4	NC	1
350			min	-.007	2	-.003	3	-.003	1	-1.069e-4	1	1848.542	3	7417.417	5
351		5	max	.007	3	.01	2	.014	5	2.498e-4	5	NC	4	NC	1
352			min	-.007	2	-.01	3	-.003	1	-8.402e-5	1	1497.036	3	5269.665	5
353		6	max	.007	3	.015	2	.017	5	2.479e-4	5	NC	4	NC	1
354			min	-.007	2	-.015	3	-.003	1	-6.117e-5	1	1301.725	3	4025.864	5
355		7	max	.007	3	.019	2	.02	5	2.46e-4	5	NC	4	NC	1
356			min	-.007	2	-.018	3	-.003	1	-4.078e-5	9	1162.135	2	3226.272	5
357		8	max	.007	3	.022	2	.023	5	2.44e-4	5	NC	4	NC	1
358			min	-.007	2	-.021	3	-.002	1	-2.373e-5	9	1073.688	2	2675.768	5
359		9	max	.007	3	.024	2	.026	5	2.421e-4	5	NC	4	NC	1
360			min	-.007	2	-.022	3	-.001	1	-6.673e-6	9	1021.425	2	2277.937	5
361		10	max	.007	3	.025	2	.029	5	2.457e-4	4	NC	4	NC	1
362			min	-.007	2	-.023	3	0	9	-3.424e-7	10	997.438	2	1964.244	4
363		11	max	.007	3	.025	2	.032	4	2.494e-4	4	NC	4	NC	1
364			min	-.007	2	-.022	3	0	9	-7.919e-7	10	998.891	2	1725.338	4
365		12	max	.007	3	.023	2	.036	4	2.53e-4	4	NC	4	NC	1
366			min	-.007	2	-.02	3	0	10	-1.241e-6	10	1026.961	2	1540.137	4
367		13	max	.007	3	.02	2	.039	4	2.567e-4	4	NC	4	NC	1
368			min	-.007	2	-.017	3	0	10	-1.691e-6	10	1087.471	2	1394.179	4
369		14	max	.007	3	.016	2	.042	4	2.604e-4	4	NC	4	NC	1
370			min	-.007	2	-.014	3	0	10	-2.14e-6	10	1193.831	2	1277.768	4
371		15	max	.007	3	.011	2	.045	4	2.64e-4	4	NC	4	NC	1
372			min	-.007	2	-.009	3	0	10	-2.589e-6	10	1375.447	2	1184.21	4
373		16	max	.007	3	.004	2	.047	4	4.335e-4	4	NC	4	NC	1
374			min	-.007	2	-.003	3	0	10	-2.922e-6	10	1704.146	2	1108.776	4
375		17	max	.007	3	.003	3	.05	4	4.55e-3	4	NC	4	NC	1
376			min	-.007	2	-.005	2	0	10	-4.764e-7	10	2408.917	2	1048.14	4
377		18	max	.007	3	.01	3	.052	4	4.065e-3	2	NC	4	NC	1
378			min	-.007	2	-.014	2	0	10	-2.051e-3	3	4664.739	2	999.673	4
379		19	max	.007	3	.018	3	.054	4	8.193e-3	2	NC	1	NC	1
380			min	-.007	2	-.025	2	0	9	-4.198e-3	3	NC	1	962.655	4
381	M5	1	max	.021	3	.071	3	.005	5	1.43e-5	4	NC	1	NC	1
382			min	-.024	2	-.061	2	0	9	0	1	NC	1	NC	1
383		2	max	.021	3	.04	3	.007	5	1.26e-4	5	NC	4	NC	1
384			min	-.024	2	-.034	2	0	9	-1.548e-5	9	1590.687	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.021	3	.012	3	.009	5	2.359e-4	5	NC	5	NC	1
386			min	-.024	2	-.009	2	0	9	-3.075e-5	9	825.454	3	NC	1
387		4	max	.021	3	.013	2	.012	5	2.44e-4	5	NC	5	NC	1
388			min	-.024	2	-.011	3	0	9	-2.919e-5	9	590.424	3	NC	1
389		5	max	.021	3	.033	2	.015	5	2.522e-4	5	NC	5	NC	1
390			min	-.024	2	-.031	3	0	9	-2.763e-5	9	478.783	3	NC	1
391		6	max	.021	3	.049	2	.018	5	2.603e-4	5	NC	5	NC	1
392			min	-.024	2	-.046	3	0	9	-2.607e-5	9	409.202	2	9671.707	3
393		7	max	.021	3	.062	2	.021	5	2.684e-4	5	NC	5	NC	1
394			min	-.024	2	-.058	3	0	9	-2.451e-5	9	364.731	2	9192.856	3
395		8	max	.021	3	.071	2	.024	5	2.765e-4	5	NC	5	NC	1
396			min	-.024	2	-.066	3	0	9	-2.295e-5	9	336.873	2	9089.49	3
397		9	max	.02	3	.077	2	.027	5	2.846e-4	5	NC	5	NC	1
398			min	-.024	2	-.07	3	0	9	-2.139e-5	9	320.399	2	9290.789	3
399		10	max	.02	3	.08	2	.031	5	2.928e-4	5	NC	5	NC	1
400			min	-.024	2	-.071	3	0	9	-1.983e-5	9	312.817	2	9788.856	3
401		11	max	.02	3	.079	2	.034	4	3.009e-4	5	NC	5	NC	1
402			min	-.024	2	-.068	3	0	9	-1.827e-5	9	313.234	2	NC	1
403		12	max	.02	3	.074	2	.037	4	3.09e-4	5	NC	5	NC	1
404			min	-.024	2	-.063	3	0	9	-1.671e-5	9	322.014	2	NC	1
405		13	max	.02	3	.065	2	.041	4	3.171e-4	5	NC	5	NC	1
406			min	-.024	2	-.054	3	0	9	-1.515e-5	9	340.985	2	NC	1
407		14	max	.02	3	.051	2	.043	4	3.252e-4	5	NC	5	NC	1
408			min	-.024	2	-.042	3	0	9	-1.359e-5	9	374.355	2	NC	1
409		15	max	.02	3	.034	2	.046	4	3.333e-4	5	NC	5	NC	1
410			min	-.024	2	-.027	3	0	9	-1.203e-5	9	431.362	2	NC	1
411		16	max	.02	3	.012	2	.049	4	5.054e-4	4	NC	5	NC	1
412			min	-.024	2	-.01	3	0	9	-1.147e-5	9	534.574	2	NC	1
413		17	max	.02	3	.01	3	.051	4	4.563e-3	4	NC	5	NC	1
414			min	-.024	2	-.015	2	0	9	-3.474e-5	9	756.081	2	NC	1
415		18	max	.02	3	.032	3	.052	4	2.343e-3	4	NC	4	NC	1
416			min	-.024	2	-.046	2	0	9	-1.777e-5	9	1464.635	2	NC	1
417		19	max	.02	3	.054	3	.054	4	5.178e-6	5	NC	1	NC	1
418			min	-.024	2	-.079	2	0	9	-9.993e-7	3	NC	1	NC	1
419	M9	1	max	.007	3	.022	3	.005	5	8.408e-3	3	NC	1	NC	1
420			min	-.007	2	-.019	2	0	9	-5.883e-3	2	NC	1	NC	1
421		2	max	.007	3	.012	3	.004	4	4.153e-3	3	NC	4	NC	1
422			min	-.007	2	-.011	2	0	10	-2.902e-3	2	4991.483	3	NC	1
423		3	max	.007	3	.004	3	.004	4	7.712e-5	1	NC	4	NC	1
424			min	-.007	2	-.003	2	0	3	-3.426e-5	5	2588.894	3	NC	1
425		4	max	.007	3	.004	2	.005	4	5.661e-5	1	NC	4	NC	1
426			min	-.007	2	-.004	3	-.001	3	-3.519e-5	5	1849.419	3	NC	1
427		5	max	.007	3	.01	2	.006	4	3.611e-5	1	NC	4	NC	1
428			min	-.007	2	-.01	3	-.002	3	-3.887e-5	3	1497.7	3	NC	1
429		6	max	.007	3	.015	2	.008	4	1.96e-5	11	NC	4	NC	1
430			min	-.007	2	-.015	3	-.003	3	-4.643e-5	3	1302.25	3	8991.841	3
431		7	max	.007	3	.019	2	.011	4	9.311e-6	11	NC	4	NC	1
432			min	-.007	2	-.019	3	-.004	3	-5.4e-5	3	1162.419	2	7683.694	4
433		8	max	.007	3	.022	2	.013	4	-4.183e-7	10	NC	4	NC	1
434			min	-.007	2	-.021	3	-.004	3	-6.156e-5	3	1073.961	2	5342.677	4
435		9	max	.007	3	.024	2	.016	4	0	10	NC	4	NC	1
436			min	-.007	2	-.023	3	-.004	3	-6.912e-5	3	1021.694	2	3976.303	4
437		10	max	.007	3	.025	2	.02	5	4.645e-7	10	NC	4	NC	1
438			min	-.007	2	-.023	3	-.004	3	-7.668e-5	3	997.71	2	3106.022	4
439		11	max	.007	3	.025	2	.023	5	9.059e-7	10	NC	4	NC	1
440			min	-.007	2	-.022	3	-.004	3	-8.693e-5	1	999.171	2	2516.094	4
441		12	max	.007	3	.023	2	.027	5	1.347e-6	10	NC	4	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.007	2	-.02	3	-.004	3	-1.074e-4	1	1027.257	2	2093.578	5
443		13	max	.007	3	.02	2	.031	5	1.789e-6	10	NC	4	NC	1
444			min	-.007	2	-.017	3	-.004	3	-1.279e-4	1	1087.791	2	1779.18	5
445		14	max	.007	3	.016	2	.035	5	2.23e-6	10	NC	4	NC	1
446			min	-.007	2	-.014	3	-.003	3	-1.484e-4	1	1194.188	2	1544.649	5
447		15	max	.007	3	.011	2	.039	5	2.671e-6	10	NC	4	NC	1
448			min	-.007	2	-.009	3	-.003	1	-1.69e-4	1	1375.861	2	1365.479	5
449		16	max	.007	3	.004	2	.043	5	1.31e-4	5	NC	4	NC	1
450			min	-.007	2	-.003	3	-.003	1	-1.846e-4	1	1704.653	2	1226.098	5
451		17	max	.007	3	.003	3	.047	5	4.529e-3	4	NC	4	NC	1
452			min	-.007	2	-.005	2	-.002	1	-8.531e-5	1	2409.583	2	1116.097	5
453		18	max	.007	3	.01	3	.05	5	2.232e-3	5	NC	4	NC	1
454			min	-.007	2	-.014	2	-.002	1	-4.066e-3	2	4665.987	2	1024.431	4
455		19	max	.007	3	.018	3	.054	4	4.196e-3	3	NC	1	NC	1
456			min	-.007	2	-.025	2	0	9	-8.193e-3	2	NC	1	949.296	4
457	M13	1	max	0	9	.022	3	.007	3	3.642e-3	3	NC	1	NC	1
458			min	-.005	5	-.019	2	-.007	2	-3.186e-3	2	NC	1	NC	1
459		2	max	0	9	.065	3	.005	3	4.514e-3	3	NC	4	NC	1
460			min	-.005	5	-.05	2	-.006	2	-3.957e-3	2	2213.773	3	NC	1
461		3	max	0	9	.102	3	.007	9	5.385e-3	3	NC	4	NC	2
462			min	-.005	5	-.075	2	-.006	2	-4.728e-3	2	1202.761	3	9658.379	1
463		4	max	0	9	.127	3	.01	9	6.257e-3	3	NC	5	NC	2
464			min	-.005	5	-.093	2	-.006	10	-5.498e-3	2	917.402	3	7010.336	1
465		5	max	0	9	.138	3	.011	9	7.128e-3	3	NC	5	NC	2
466			min	-.005	5	-.102	2	-.007	2	-6.269e-3	2	830.899	3	6641.359	1
467		6	max	0	9	.135	3	.01	3	8.e-3	3	NC	5	NC	2
468			min	-.005	5	-.101	2	-.01	2	-7.04e-3	2	852.62	3	8182.083	1
469		7	max	0	9	.121	3	.013	3	8.871e-3	3	NC	5	NC	1
470			min	-.005	5	-.093	2	-.014	2	-7.811e-3	2	976.49	3	NC	1
471		8	max	0	9	.1	3	.016	3	9.743e-3	3	NC	4	NC	1
472			min	-.005	5	-.08	2	-.019	2	-8.582e-3	2	1237.27	3	8508.055	2
473		9	max	0	9	.08	3	.018	3	1.061e-2	3	NC	4	NC	1
474			min	-.005	5	-.067	2	-.022	2	-9.353e-3	2	1662.76	3	6403.388	2
475		10	max	0	9	.071	3	.021	3	1.149e-2	3	NC	4	NC	4
476			min	-.005	5	-.061	2	-.024	2	-1.012e-2	2	1981.253	3	5779.607	2
477		11	max	0	9	.08	3	.022	3	1.062e-2	3	NC	4	NC	1
478			min	-.005	5	-.067	2	-.022	2	-9.353e-3	2	1662.759	3	6231.56	3
479		12	max	0	9	.1	3	.023	3	9.747e-3	3	NC	4	NC	1
480			min	-.005	5	-.079	2	-.019	2	-8.582e-3	2	1237.268	3	6085.072	3
481		13	max	0	9	.121	3	.022	3	8.877e-3	3	NC	5	NC	1
482			min	-.005	5	-.093	2	-.014	2	-7.811e-3	2	976.489	3	6401.482	3
483		14	max	0	9	.135	3	.02	3	8.007e-3	3	NC	5	NC	2
484			min	-.005	5	-.101	2	-.01	2	-7.04e-3	2	852.619	3	7243.845	3
485		15	max	0	9	.138	3	.018	3	7.138e-3	3	NC	5	NC	2
486			min	-.005	5	-.102	2	-.007	2	-6.269e-3	2	830.898	3	6644.864	1
487		16	max	0	9	.127	3	.015	3	6.268e-3	3	NC	5	NC	2
488			min	-.005	5	-.093	2	-.006	10	-5.499e-3	2	917.402	3	7020.631	1
489		17	max	0	9	.102	3	.012	3	5.398e-3	3	NC	4	NC	2
490			min	-.005	5	-.075	2	-.006	2	-4.728e-3	2	1202.76	3	9683.613	1
491		18	max	0	9	.066	3	.009	3	4.529e-3	3	NC	4	NC	1
492			min	-.005	5	-.05	2	-.006	2	-3.957e-3	2	2213.772	3	NC	1
493		19	max	0	9	.023	3	.007	3	3.659e-3	3	NC	1	NC	1
494			min	-.005	5	-.019	2	-.007	2	-3.186e-3	2	NC	1	NC	1
495	M16	1	max	0	9	.018	3	.007	3	3.925e-3	2	NC	1	NC	1
496			min	-.054	4	-.025	2	-.007	2	-2.834e-3	3	NC	1	NC	1
497		2	max	0	9	.04	3	.009	3	4.879e-3	2	NC	4	NC	1
498			min	-.054	4	-.067	2	-.006	2	-3.483e-3	3	2267.806	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	0	9	.058	3	.012	3	5.832e-3	2	NC	4	NC	2
500			min	-.054	4	-.103	2	-.006	2	-4.132e-3	3	1229.138	2	9715.647	1
501		4	max	0	9	.071	3	.015	3	6.786e-3	2	NC	5	NC	2
502			min	-.054	4	-.128	2	-.006	2	-4.782e-3	3	933.542	2	7054.954	1
503		5	max	0	9	.078	3	.017	3	7.74e-3	2	NC	5	NC	2
504			min	-.054	4	-.139	2	-.007	2	-5.431e-3	3	839.818	2	6693.594	1
505		6	max	0	9	.079	3	.019	3	8.693e-3	2	NC	5	NC	2
506			min	-.054	4	-.137	2	-.01	2	-6.08e-3	3	852.67	2	7920.583	3
507		7	max	0	9	.074	3	.02	3	9.647e-3	2	NC	5	NC	1
508			min	-.054	4	-.125	2	-.014	2	-6.729e-3	3	960.113	2	7103.756	3
509		8	max	0	9	.066	3	.021	3	1.06e-2	2	NC	4	NC	1
510			min	-.054	4	-.106	2	-.019	2	-7.379e-3	3	1183.663	2	6752.375	3
511		9	max	0	9	.058	3	.021	3	1.155e-2	2	NC	4	NC	1
512			min	-.054	4	-.088	2	-.022	2	-8.028e-3	3	1528.794	2	6397.83	2
513		10	max	0	9	.054	3	.02	3	1.251e-2	2	NC	4	NC	4
514			min	-.054	4	-.079	2	-.024	2	-8.677e-3	3	1771.634	2	5775.178	2
515		11	max	0	9	.058	3	.019	3	1.155e-2	2	NC	4	NC	1
516			min	-.054	4	-.088	2	-.022	2	-8.026e-3	3	1528.794	2	6397.842	2
517		12	max	0	9	.066	3	.018	3	1.06e-2	2	NC	4	NC	1
518			min	-.054	4	-.106	2	-.019	2	-7.375e-3	3	1183.663	2	8497.787	2
519		13	max	0	9	.074	3	.016	3	9.647e-3	2	NC	5	NC	1
520			min	-.054	4	-.125	2	-.014	2	-6.724e-3	3	960.113	2	NC	1
521		14	max	0	9	.079	3	.015	3	8.694e-3	2	NC	5	NC	2
522			min	-.054	4	-.137	2	-.01	2	-6.073e-3	3	852.67	2	8286.843	1
523		15	max	0	9	.078	3	.013	3	7.74e-3	2	NC	5	NC	2
524			min	-.054	4	-.139	2	-.007	2	-5.422e-3	3	839.818	2	6706.622	1
525		16	max	0	9	.071	3	.011	3	6.787e-3	2	NC	5	NC	2
526			min	-.054	4	-.128	2	-.006	2	-4.772e-3	3	933.542	2	7075.469	1
527		17	max	0	9	.058	3	.009	3	5.833e-3	2	NC	4	NC	2
528			min	-.054	4	-.103	2	-.006	2	-4.121e-3	3	1229.138	2	9756.992	1
529		18	max	0	9	.039	3	.008	3	4.88e-3	2	NC	4	NC	1
530			min	-.054	4	-.067	2	-.007	2	-3.47e-3	3	2267.806	2	NC	1
531		19	max	0	9	.018	3	.007	3	3.926e-3	2	NC	1	NC	1
532			min	-.054	4	-.025	2	-.007	2	-2.819e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	3.736e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-5.519e-4	5	NC	1	NC	1
535		2	max	0	3	0	5	.004	4	7.767e-4	3	NC	1	NC	1
536			min	0	4	-.002	1	0	3	-5.632e-4	5	NC	1	NC	1
537		3	max	0	3	.001	5	.008	4	1.18e-3	3	NC	1	NC	1
538			min	0	4	-.004	1	-.003	3	-8.422e-4	2	NC	1	7565.469	4
539		4	max	0	3	.002	5	.012	4	1.583e-3	3	NC	1	NC	9
540			min	-.001	4	-.005	1	-.006	3	-1.241e-3	2	NC	1	4886.659	4
541		5	max	0	3	.002	5	.017	4	1.986e-3	3	NC	3	NC	9
542			min	-.002	4	-.007	1	-.011	3	-1.64e-3	2	8385.627	2	3665.369	4
543		6	max	0	3	.003	5	.02	4	2.389e-3	3	NC	4	9519.266	9
544			min	-.002	4	-.008	1	-.015	3	-2.038e-3	2	7057.392	2	2718.926	3
545		7	max	0	3	.003	5	.023	4	2.792e-3	3	NC	5	7506.764	9
546			min	-.003	4	-.009	1	-.02	3	-2.437e-3	2	6258.633	2	2125.686	3
547		8	max	0	3	.003	5	.025	4	3.195e-3	3	NC	5	6231.141	9
548			min	-.003	4	-.01	1	-.025	3	-2.836e-3	2	5779.258	2	1752.791	3
549		9	max	0	3	.004	5	.025	4	3.598e-3	3	NC	5	5392.025	9
550			min	-.003	4	-.01	1	-.029	3	-3.235e-3	2	5521.23	2	1508.781	3
551		10	max	0	3	.004	5	.026	2	4.001e-3	3	NC	5	4837.144	9
552			min	-.004	4	-.01	1	-.032	3	-3.633e-3	2	5439.602	2	1347.733	3
553		11	max	0	3	.004	5	.027	2	4.404e-3	3	NC	5	4739.699	15
554			min	-.004	4	-.01	1	-.035	3	-4.032e-3	2	5521.23	2	1245.538	3
555		12	max	0	3	.005	5	.028	1	4.808e-3	3	NC	5	5466.422	15

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.005	4	-.01	1	-.035	3	-4.431e-3	2	5779.258	2	1190.233	3
557		13	max	.001	3	.005	5	.027	1	5.211e-3	3	NC	5	6768.67	15
558			min	-.005	4	-.009	1	-.035	3	-4.83e-3	2	6258.633	2	1178.341	3
559		14	max	.001	3	.005	5	.025	1	5.614e-3	3	NC	4	9235.718	15
560			min	-.006	4	-.008	9	-.032	3	-5.228e-3	2	7057.392	2	1214.993	3
561		15	max	.001	3	.005	5	.021	1	6.017e-3	3	NC	3	NC	7
562			min	-.006	4	-.007	9	-.026	3	-5.627e-3	2	8385.627	2	1319.057	3
563		16	max	.001	3	.005	5	.015	1	6.42e-3	3	NC	1	NC	5
564			min	-.006	4	-.006	9	-.018	3	-6.026e-3	2	NC	1	1541.785	3
565		17	max	.001	3	.005	5	.007	1	6.823e-3	3	NC	1	NC	4
566			min	-.007	4	-.004	9	-.007	3	-6.425e-3	2	NC	1	2043.98	3
567		18	max	.001	3	.005	5	.007	3	7.226e-3	3	NC	1	NC	4
568			min	-.007	4	-.003	9	-.01	2	-6.823e-3	2	NC	1	3639.102	3
569		19	max	.002	3	.005	5	.025	3	7.629e-3	3	NC	1	NC	1
570			min	-.008	4	-.001	9	-.025	2	-7.222e-3	2	NC	1	NC	1
571	M16A	1	max	0	2	.001	2	.008	3	2.2e-3	3	NC	1	NC	1
572			min	-.003	4	-.003	4	-.008	2	-2.232e-3	2	NC	1	NC	1
573		2	max	0	2	0	10	.001	3	2.114e-3	3	NC	1	NC	1
574			min	-.003	4	-.007	4	-.003	2	-2.13e-3	2	NC	1	NC	1
575		3	max	0	2	-.002	12	.003	1	2.028e-3	3	NC	1	NC	4
576			min	-.002	4	-.01	4	-.004	5	-2.028e-3	2	8324.286	4	5738.962	3
577		4	max	0	2	-.003	12	.006	1	1.943e-3	3	NC	1	NC	4
578			min	-.002	4	-.013	4	-.008	5	-1.926e-3	2	5710.947	4	4366.168	3
579		5	max	0	2	-.004	12	.008	1	1.857e-3	3	NC	3	NC	9
580			min	-.002	4	-.016	4	-.012	5	-1.823e-3	2	4456.31	4	3772.071	3
581		6	max	0	2	-.005	12	.009	1	1.771e-3	3	NC	12	NC	9
582			min	-.002	4	-.018	4	-.016	5	-1.721e-3	2	3750.456	4	3513.716	3
583		7	max	0	2	-.005	12	.01	1	1.685e-3	3	NC	12	NC	9
584			min	-.002	4	-.02	4	-.019	5	-1.619e-3	2	3325.977	4	3272.793	5
585		8	max	0	2	-.005	12	.01	1	1.6e-3	3	NC	12	NC	9
586			min	-.002	4	-.022	4	-.023	5	-1.517e-3	2	3071.227	4	2779.888	5
587		9	max	0	2	-.006	12	.009	1	1.514e-3	3	NC	12	NC	9
588			min	-.001	4	-.022	4	-.025	5	-1.415e-3	2	2934.105	4	2496.397	5
589		10	max	0	2	-.006	12	.008	1	1.428e-3	3	NC	12	NC	9
590			min	-.001	4	-.022	4	-.026	5	-1.312e-3	2	2890.726	4	2351.529	5
591		11	max	0	2	-.006	12	.007	1	1.342e-3	3	NC	12	NC	9
592			min	-.001	4	-.022	4	-.027	5	-1.21e-3	2	2934.105	4	2314.678	5
593		12	max	0	2	-.005	12	.006	1	1.257e-3	3	NC	12	NC	9
594			min	-.001	4	-.021	4	-.026	5	-1.108e-3	2	3071.227	4	2379.455	5
595		13	max	0	2	-.005	12	.005	1	1.171e-3	3	NC	12	NC	2
596			min	0	4	-.019	4	-.024	5	-1.006e-3	2	3325.977	4	2561.086	5
597		14	max	0	2	-.004	12	.003	1	1.085e-3	3	NC	12	NC	1
598			min	0	4	-.017	4	-.021	5	-9.033e-4	2	3750.456	4	2905.214	5
599		15	max	0	2	-.004	12	.002	1	9.995e-4	3	NC	3	NC	1
600			min	0	4	-.014	4	-.017	5	-8.011e-4	2	4456.31	4	3518.372	5
601		16	max	0	2	-.003	12	.001	9	9.137e-4	3	NC	1	NC	1
602			min	0	4	-.011	4	-.013	5	-6.989e-4	2	5710.947	4	4665.902	5
603		17	max	0	2	-.002	12	0	9	8.28e-4	3	NC	1	NC	1
604			min	0	4	-.008	4	-.009	5	-5.966e-4	2	8324.286	4	7171.744	5
605		18	max	0	2	-.001	12	0	3	8.422e-4	4	NC	1	NC	1
606			min	0	4	-.004	4	-.004	5	-4.944e-4	2	NC	1	NC	1
607		19	max	0	1	0	1	0	1	9.028e-4	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-3.921e-4	2	NC	1	NC	1

SIMPSON Strong-Tie®

Anchor Designer™
Software
Version 2.4.5673.0

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

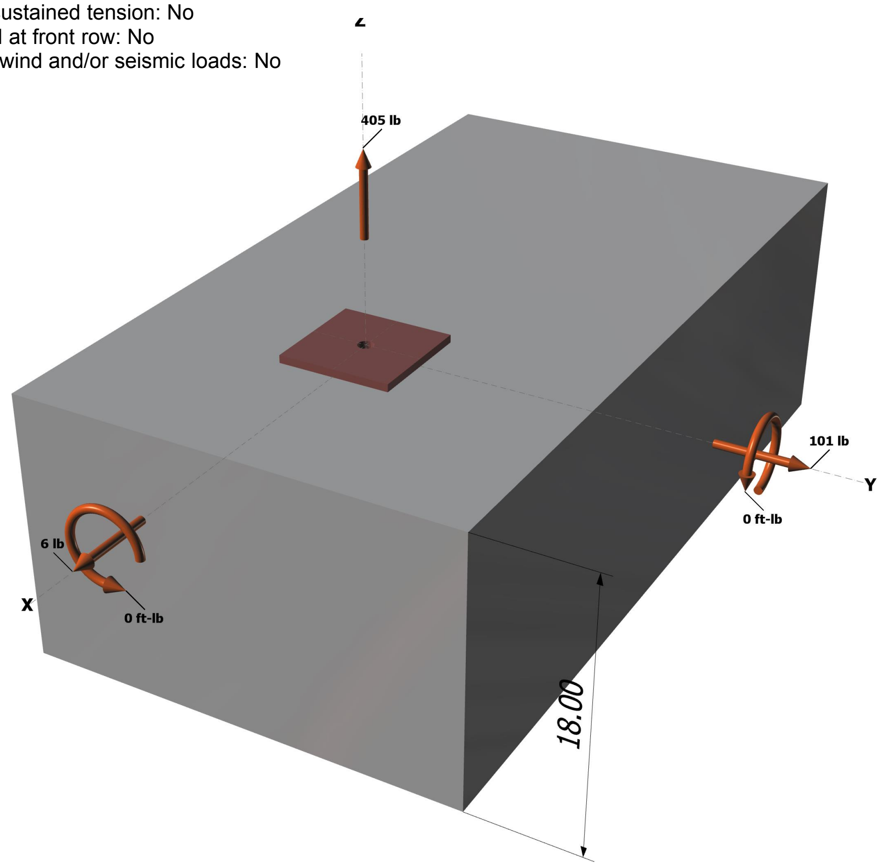
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'$_c$ (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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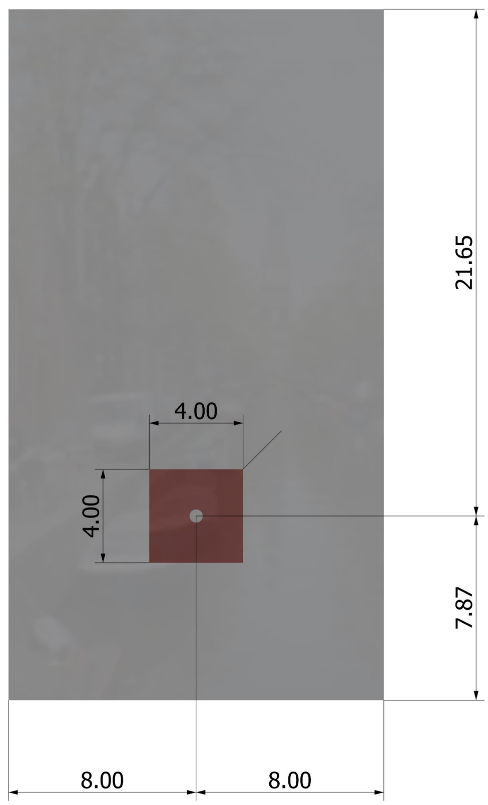


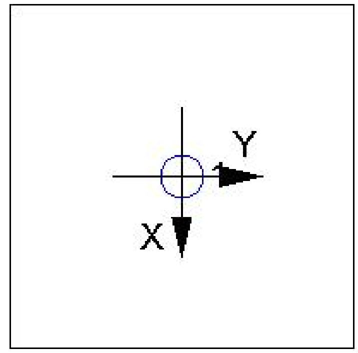
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\,\mathrm{min}|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\,\mathrm{min}|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

SIMPSON Strong-Tie®

Anchor Designer™
Software
Version 2.4.5673.0

Company:	Schletter, Inc.	Date:	12/10/2015
Engineer:	HCV	Page:	1/5
Project:	Standard PVMini - Worst Case		
Address:			
Phone:			
E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

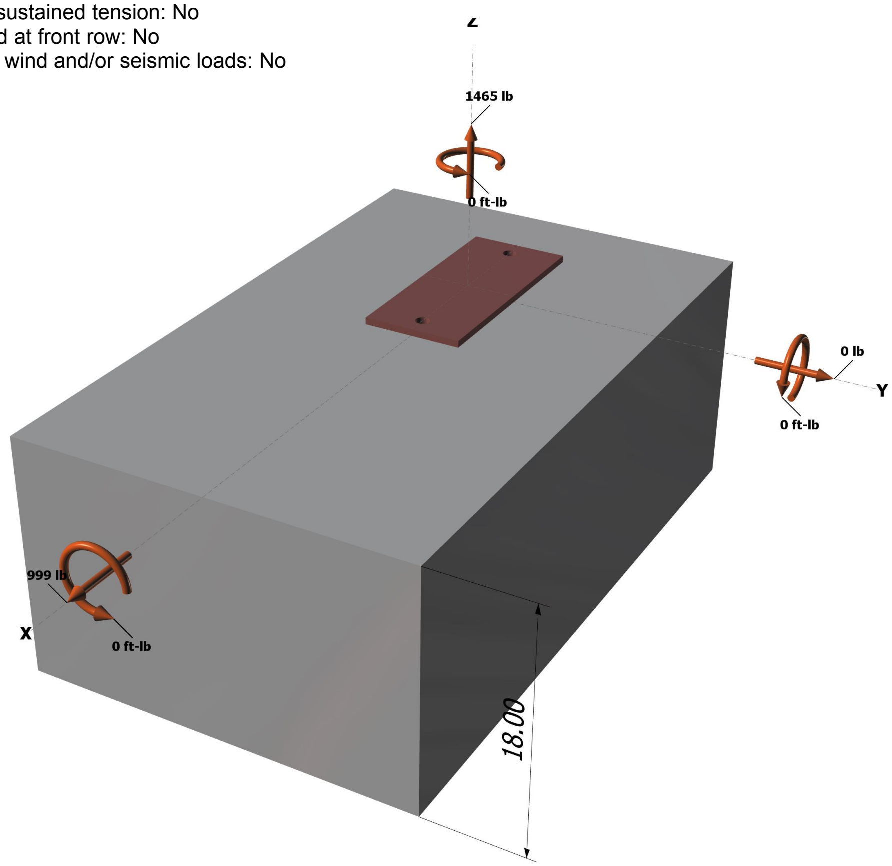
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



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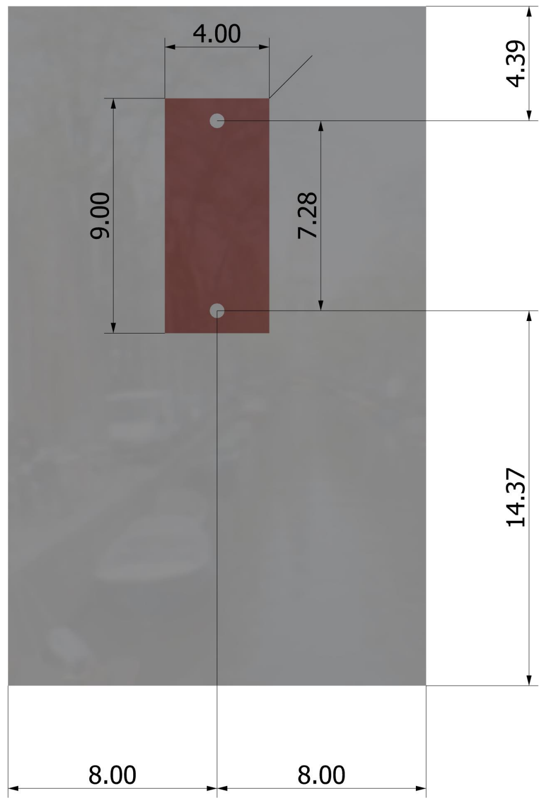


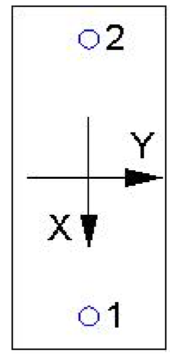
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\, (A_{Nc} / A_{Nco})\, \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\, (A_{Na} / A_{Na0})\, \Psi_{ed,Na} \Psi_{g,Na} \Psi_{ec,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.