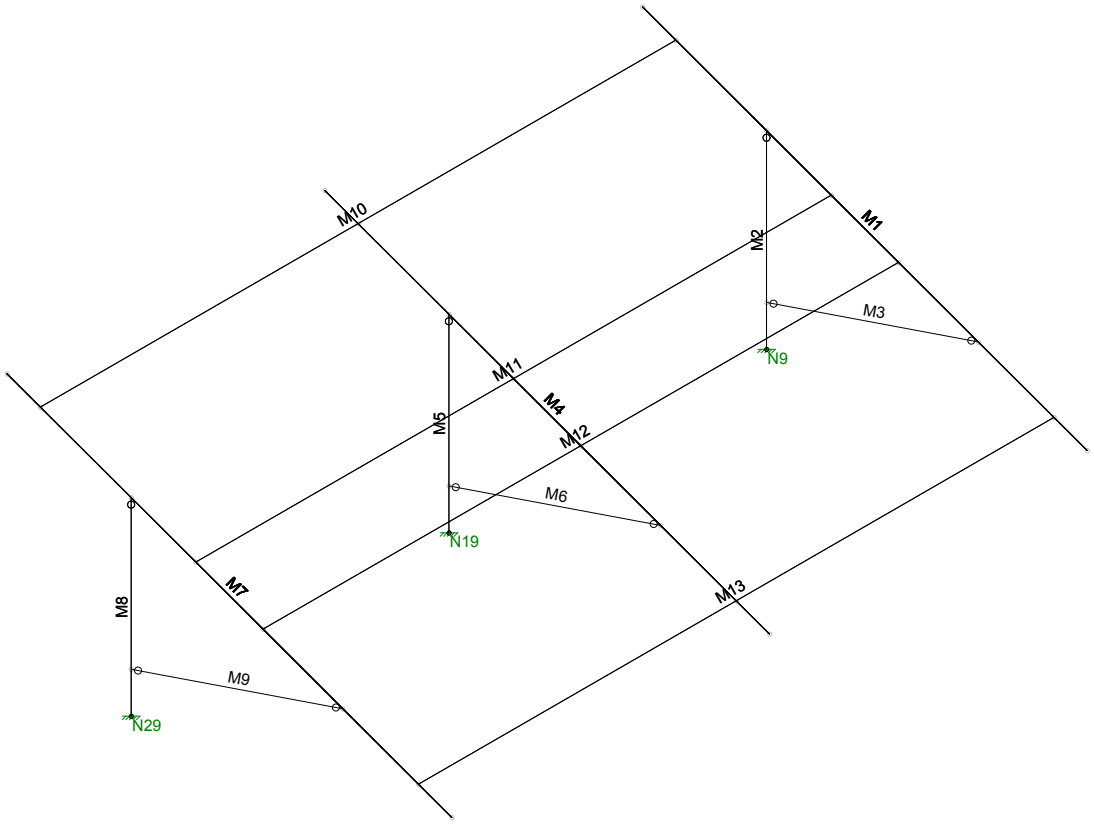


Schletter, Inc.		20° Tilt w/ Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

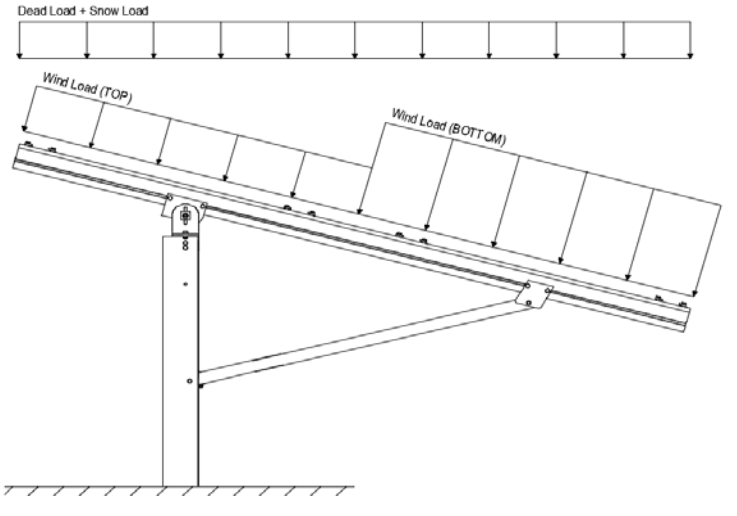
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row =	2
Module Tilt =	20°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	20.62	psf	*(ASCE 7-10, Eq. 7.4-1)*
I_s =	1.00		
C_s =	0.91		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	160	mph	Exposure Category = C
Height <	15	ft	Importance Category = II
Peak Velocity Pressure, q_z =	40.19	psf	*Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.05		*(Pressure)*
$Cf+_{BOTTOM}$ =	1.65		
$Cf-_{TOP}$ =	-2.12		*(Suction)*
$Cf-_{BOTTOM}$ =	-1		

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.07	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W	
1.2D + 1.0W + 0.5S	
0.9D + 1.0W [M]	
1.54D + 1.3E + 0.2S [R]	*(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)*
0.56D + 1.3E [R]	
1.54D + 1.25E + 0.2S [O]	
0.56D + 1.25E [O]	

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S	
1.0D + 0.6W	
1.0D + 0.75L + 0.45W + 0.75S	
0.6D + 0.6W [M]	*(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)*
1.238D + 0.875E [O]	
1.1785D + 0.65625E + 0.75S [O]	
0.362D + 0.875E [O]	

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

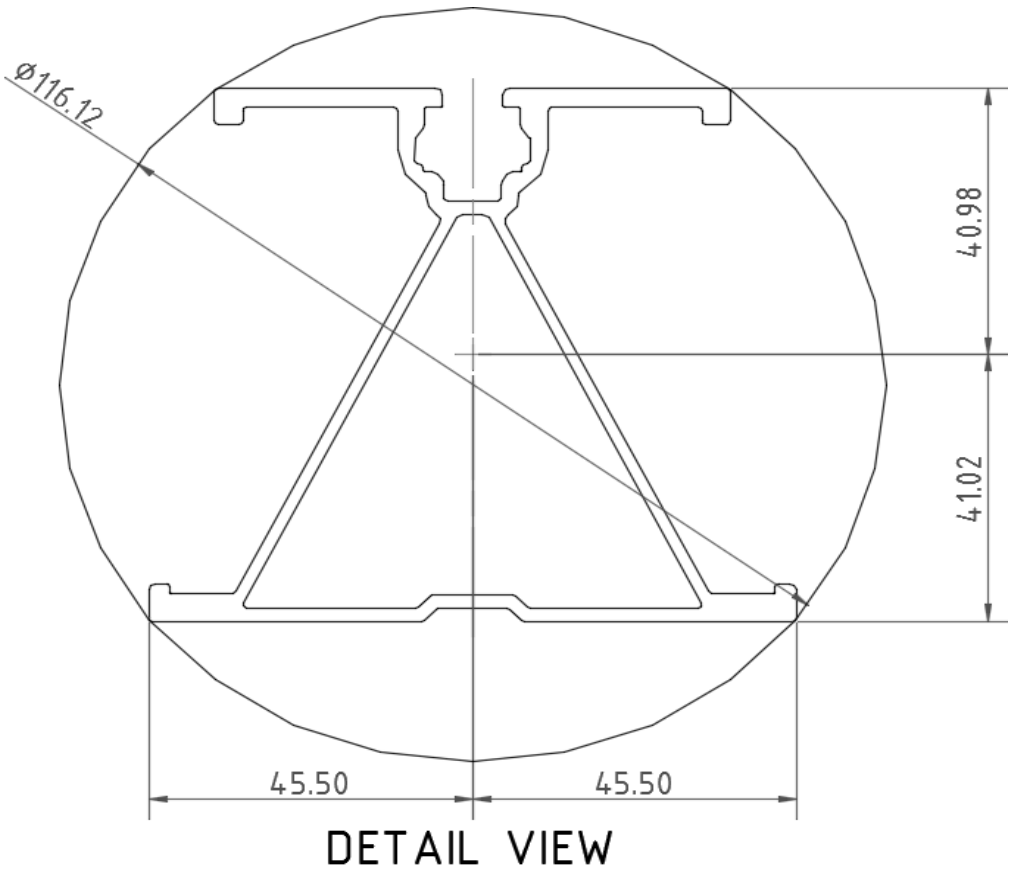
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

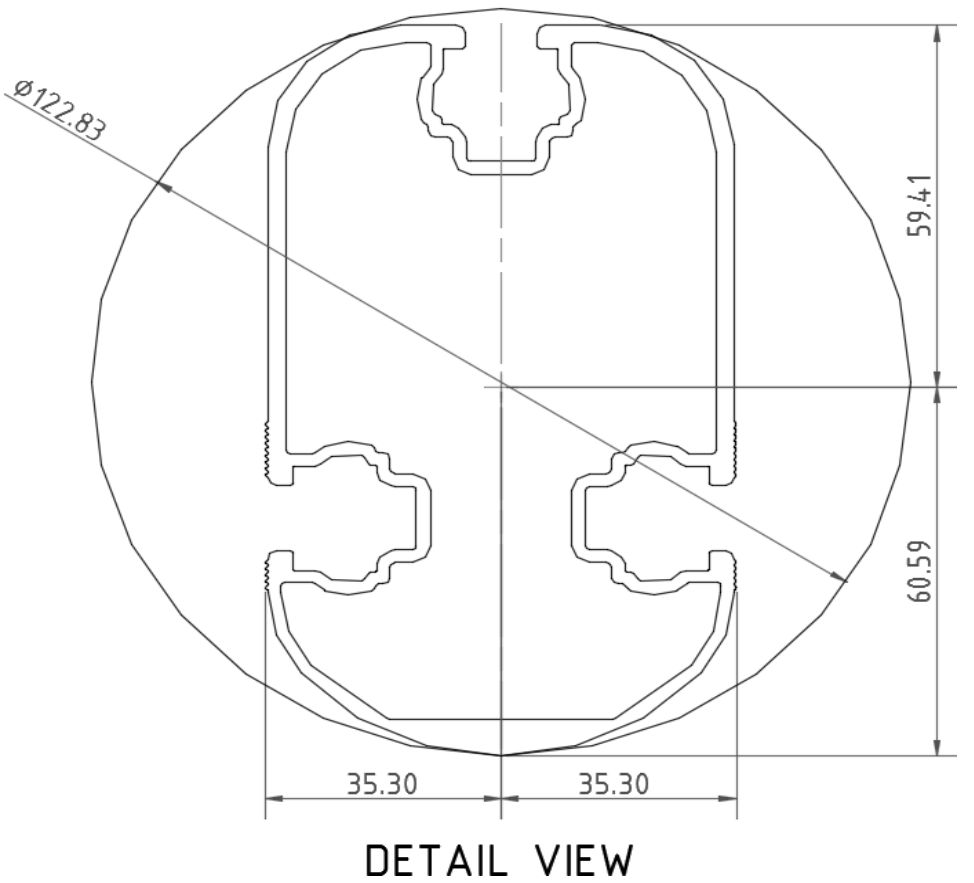
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	90	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.6	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.382	k-ft
M_z =	0.134	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	61%	



4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

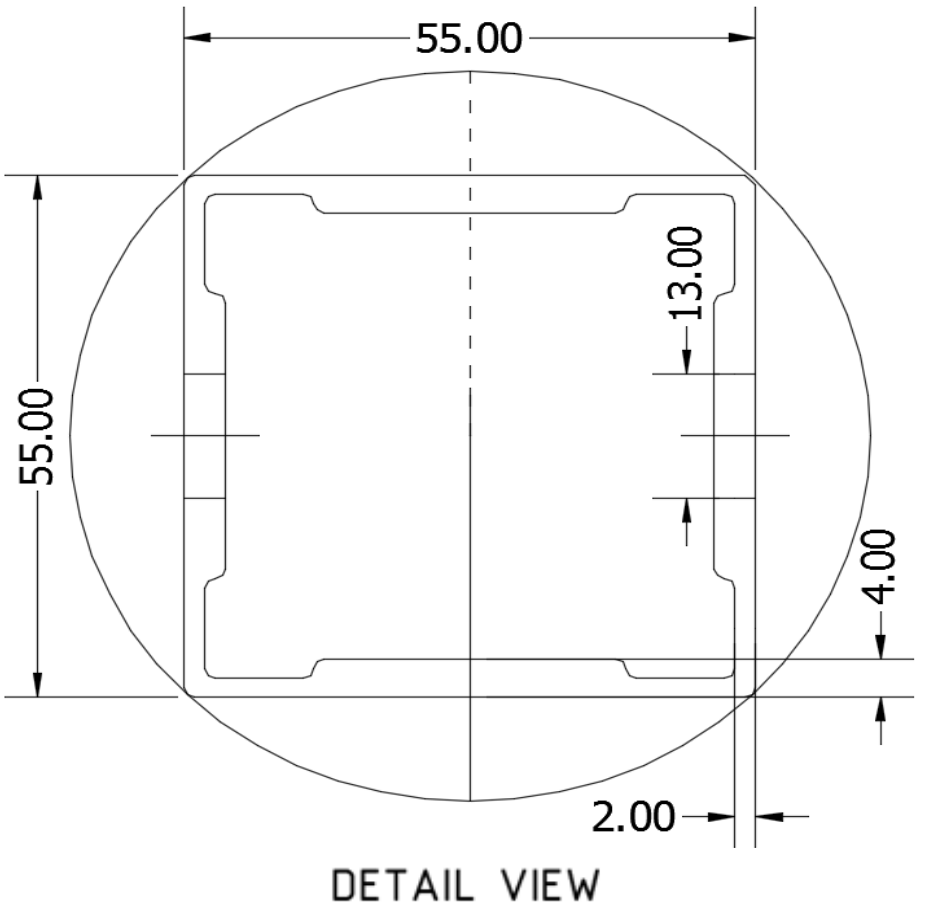
Girder Type =	**T5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	63.82	in
$\Phi F_{ty\ AXIAL}$ =	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	30.46	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	31.56	ksi
S_y =	1.98	in^3
S_x =	1.32	in^3
E =	10100	ksi
I_y =	4.74	in^4
I_x =	1.83	in^4
A =	1.93	in^2
g =	2.32	lbs/ft
M_y =	4.459	k-ft
M_z =	0.000	k-ft
P_n =	0.030	k
$M_{y\ allowable}$ =	5.026	k-ft
$M_{z\ allowable}$ =	3.472	k-ft
$P_{n\ allowable}$ =	59.439	k
Utilization =	89%	



4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.00	in
$\Phi F_{ty\ AXIAL}$ =	13.67	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.005	k-ft
M_z =	0.000	k-ft
P_n =	5.793	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.425	k
Utilization =	44%	

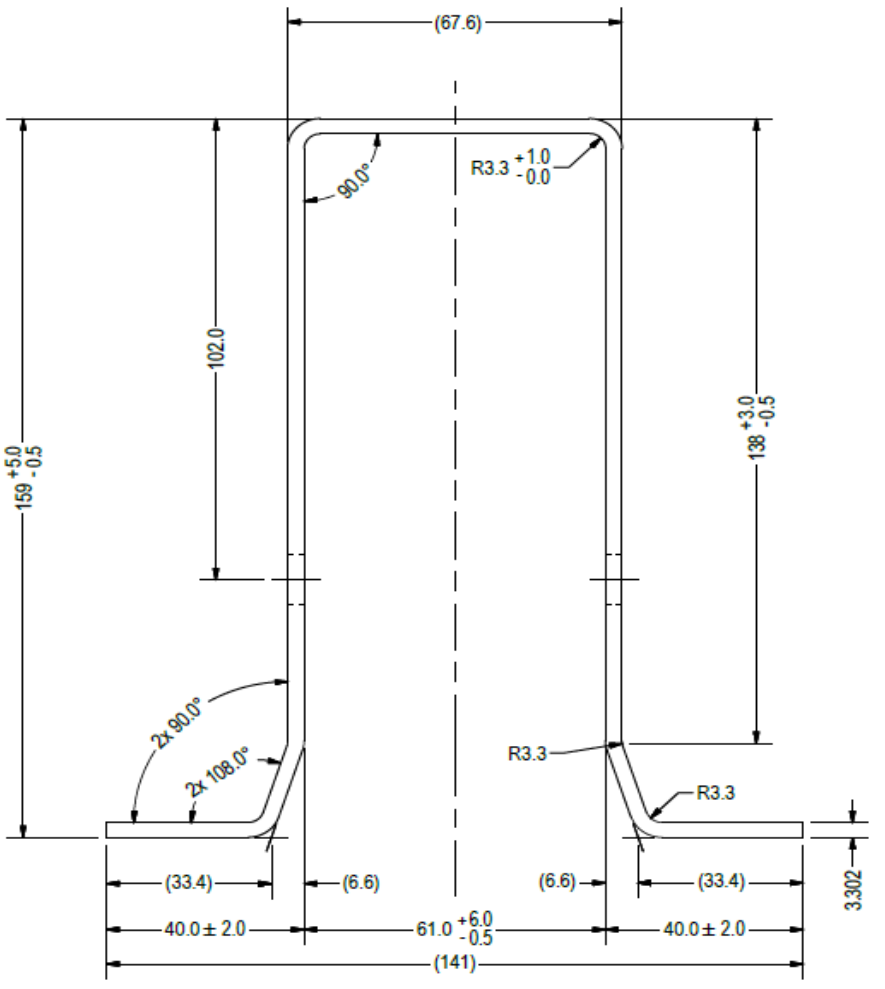


DETAIL VIEW

4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	65.62	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	11.262	k-ft
M_z =	0.000	k-ft
P_r =	6.342	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	46.025	k
Utilization =	73%	



DETAIL VIEW

5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	7.23	k
Maximum Lateral Load =	2.92	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

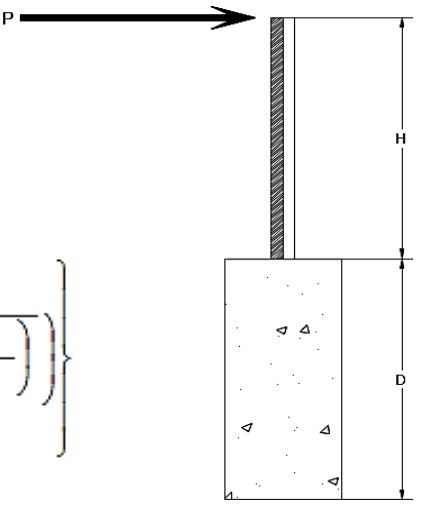
Lateral Force @ Top of Pole, P =	1.47	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1 + \sqrt{1 + \left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

Non-Constrained

Lateral Force @ Top of Pole, P =	1.47	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	7.95	
Required Footing Depth, D =	11.36	ft

2nd Trial @ D_2 =	7.30	ft
Lateral Soil Bearing @ D/3, S_1 =	0.49	ksf
Lateral Soil Bearing @ D, S_3 =	1.46	ksf
Constant 2.34P/(S_1B), A =	3.54	
Required Footing Depth, D =	6.28	ft

3rd Trial @ D_3 =	6.79	ft
Lateral Soil Bearing @ D/3, S_1 =	0.45	ksf
Lateral Soil Bearing @ D, S_3 =	1.36	ksf
Constant 2.34P/(S_1B), A =	3.80	
Required Footing Depth, D =	6.61	ft

4th Trial @ D_4 =	6.70	ft
Lateral Soil Bearing @ D/3, S_1 =	0.45	ksf
Lateral Soil Bearing @ D, S_3 =	1.34	ksf
Constant 2.34P/(S_1B), A =	3.86	
Required Footing Depth, D =	6.67	ft

5th Trial @ D_5 =	6.68	ft
Lateral Soil Bearing @ D/3, S_1 =	0.45	ksf
Lateral Soil Bearing @ D, S_3 =	1.34	ksf
Constant 2.34P/(S_1B), A =	3.86	
Required Footing Depth, D =	6.75	ft

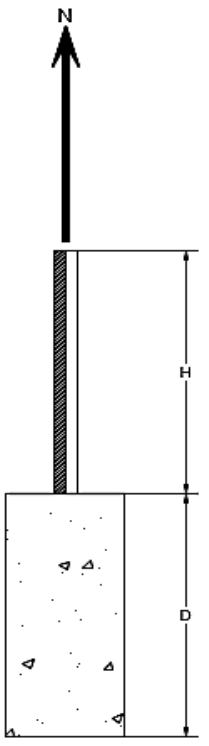
A 2ft diameter x 6.75ft deep footing unrestrained at ground level is required for the racking structure.

5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	3.32	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	2.18	k
Required Concrete Volume, V =	15.06	ft^3
Required Footing Depth, D =	5.00	ft

A 2ft diameter x 5ft deep footing unrestrained at ground level is required for the racking structure.



Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	7.18
2	0.4	0.2	118.10	7.08
3	0.6	0.2	118.10	6.97
4	0.8	0.2	118.10	6.87
5	1	0.2	118.10	6.77
6	1.2	0.2	118.10	6.66
7	1.4	0.2	118.10	6.56
8	1.6	0.2	118.10	6.45
9	1.8	0.2	118.10	6.35
10	2	0.2	118.10	6.25
11	2.2	0.2	118.10	6.14
12	2.4	0.2	118.10	6.04
13	2.6	0.2	118.10	5.94
14	2.8	0.2	118.10	5.83
15	3	0.2	118.10	5.73
16	3.2	0.2	118.10	5.62
17	3.4	0.2	118.10	5.52
18	3.6	0.2	118.10	5.42
19	3.8	0.2	118.10	5.31
20	4	0.2	118.10	5.21
21	4.2	0.2	118.10	5.11
22	4.4	0.2	118.10	5.00
23	4.6	0.2	118.10	4.90
24	4.8	0.2	118.10	4.80
25	0	0.0	0.00	4.80
26	0	0.0	0.00	4.80
27	0	0.0	0.00	4.80
28	0	0.0	0.00	4.80
29	0	0.0	0.00	4.80
30	0	0.0	0.00	4.80
31	0	0.0	0.00	4.80
32	0	0.0	0.00	4.80
33	0	0.0	0.00	4.80
34	0	0.0	0.00	4.80
Max	4.8	Sum	1.13	

5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	6.75	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	4.03	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	23.56	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

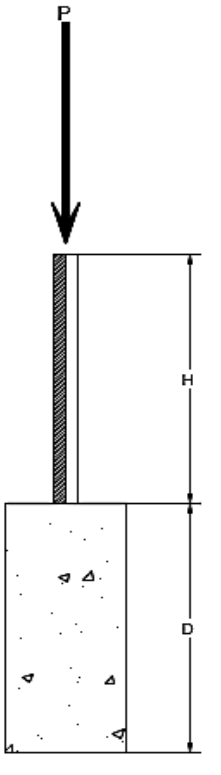
Weight of Concrete

Footing Volume	21.21	ft^3
Weight	3.07	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	3.53	k
1/3 Increase for Wind =	1.33	
Total Resistance =	11.00	k
Applied Force =	7.10	k
Utilization =	65%	

A 2ft diameter footing passes at a depth of 6.75ft.



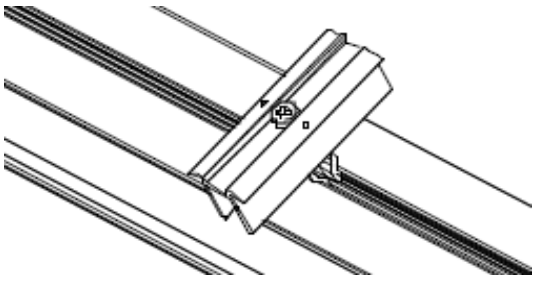
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

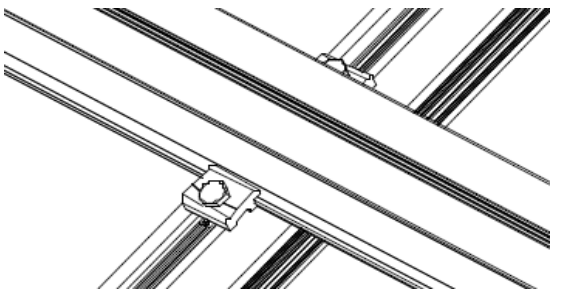
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.803 k
Allowable Uplift	=	1.214 k
Utilization	=	66%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	2.150 k
Allowable Uplift	=	2.180 k
Utilization	=	99%

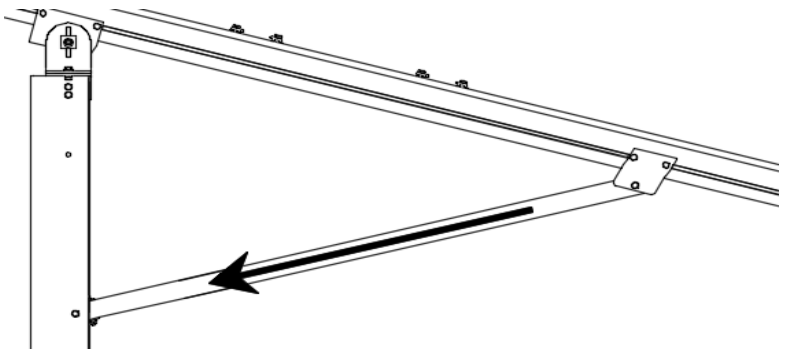


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load	=	5.793 k
M10 Bolt Shear Capacity	=	8.894 k
Utilization	=	65%

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

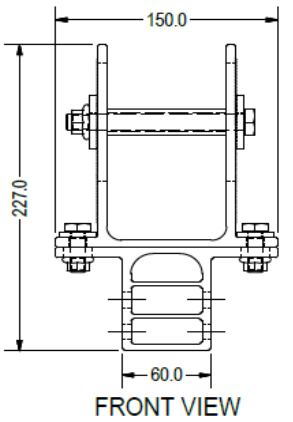


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

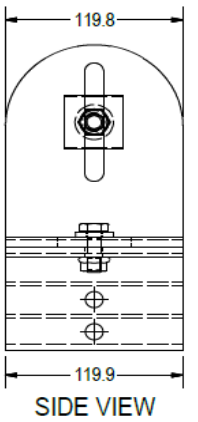
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

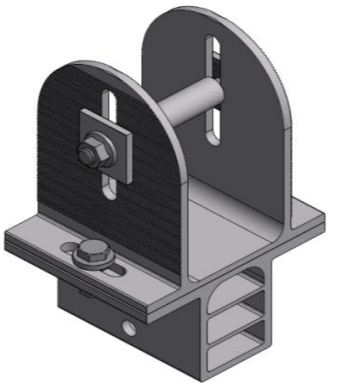
Maximum Tensile Load	=	4.548 k
Allowable Load	=	5.649 k
Utilization	=	81%



FRONT VIEW



SIDE VIEW



7. SEISMIC DESIGN

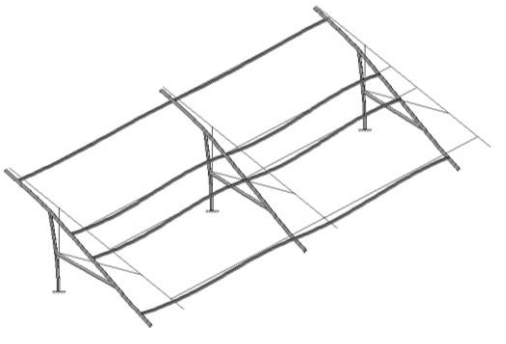
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	53.92 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.078 in
Max Drift, Δ_{MAX}	=	0.338 in

0.338 ≤ 1.078, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 90 in

J = 0.432

248.982

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.2 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 90

J = 0.432

158.338

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.3

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 63.8189 in
J = 1.98
82.1278

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.5 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 63.8189
J = 1.98
89.1294

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.3

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = φb[Bt-Dt*√(Rb/t)]

φF_L = 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L St$ = 30.5 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 5.001 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L Wk$ = 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φc[Bt-Dt*√(Rb/t)]

φF_L = 30.80 ksi

φF_L = 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 61 in

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St$ = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 61

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk$ = 1.460 k-ft

Compression

3.4.7

λ = 1.41113

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

S1* = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

S2* = 1.23671

φcc = 0.77756

φF_L = (φccFcy)/(λ²)

φF_L = 13.6667 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 13.67 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 14.07 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	65.62	in	
Pr =	6.34	k	(LRFD Factored Load)
Mr (Strong) =	11.26	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	94.42		
4.71√(E/Fy) =	103.55	=> kL/r	≤ 4.71√(E/Fy)
Fcr =	27.44	ksi	
Fe =	32.10	ksi	
Pn =	61.196	k	

Torsional/Flexural Torsional Buckling:

Fcr =	20.6391	ksi
Fey =	81.8881	ksi
Fez =	26.2099	ksi
Pn =	46.0252	k

Bending (Strong Axis):

Yielding:

Mn =	21.95	k-ft

Flange Local Buckling:

Mn =	19.207	k-ft

Pr/Pc =	0.1531	<	0.2	
Utilization =	0.73	<	1.0	OK

Bending (Weak Axis):

Yielding:

Mn =	14.65	k-ft

Flange Local Buckling:

Mn =	14.39	k-ft

Pr/Pc =	0.153	<	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 73%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-8.366	-8.366	0	0
2	M11	Y	-8.366	-8.366	0	0
3	M12	Y	-8.366	-8.366	0	0
4	M13	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-4.45	-4.45	0	0
2	M11	Y	-4.45	-4.45	0	0
3	M12	Y	-4.45	-4.45	0	0
4	M13	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-54.031	-54.031	0	0
2	M11	Y	-54.031	-54.031	0	0
3	M12	Y	-54.031	-54.031	0	0
4	M13	Y	-54.031	-54.031	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-117.695	-117.695	0	0
2	M11	y	-117.695	-117.695	0	0
3	M12	y	-184.95	-184.95	0	0
4	M13	y	-184.95	-184.95	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	237.633	237.633	0	0
2	M11	y	237.633	237.633	0	0
3	M12	y	112.091	112.091	0	0
4	M13	y	112.091	112.091	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Z	6.693	6.693	0	0
2	M11	Z	6.693	6.693	0	0
3	M12	Z	6.693	6.693	0	0
4	M13	Z	6.693	6.693	0	0
5	M10	Z	0	0	0	0
6	M11	Z	0	0	0	0
7	M12	Z	0	0	0	0
8	M13	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	461.108	2	2363.778	2	174.898	2	.185	1	.005	5	5.58	1
2		min	-719.442	3	-1900.52	3	-264.533	5	-.958	5	-.005	2	.29	12
3	N19	max	2183.105	2	6374.818	2	0	2	0	9	.005	4	10.164	1
4		min	-2149.495	3	-5557.181	3	-282.983	5	-1	4	0	12	.262	15
5	N29	max	461.108	2	2363.778	2	201.097	3	.209	3	.005	4	5.58	1
6		min	-719.442	3	-1900.52	3	-296.621	4	-1.002	4	-.002	3	-.212	5
7	Totals:	max	3105.321	2	11102.373	2	0	12						
8		min	-3588.38	3	-9358.222	3	-823.041	4						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.006	2	0	4	0	1	0	1	0	1
2			min	0	1	-.002	3	0	1	0	1	0	1	0	1
3		2	max	-.179	15	-.49	15	0	3	0	1	0	3	0	6
4			min	-.76	6	-2.085	6	-1.499	5	0	1	0	5	0	15
5		3	max	-1.828	12	333.483	3	15.518	3	.072	3	.194	1	.322	2
6			min	-155.213	1	-728.501	2	-125.16	1	-.204	2	-.005	3	-.147	3
7		4	max	-2.124	12	332.264	3	15.518	3	.072	3	.116	1	.775	2
8			min	-155.805	1	-730.127	2	-125.16	1	-.204	2	.003	12	-.353	3
9		5	max	-2.42	12	331.044	3	15.518	3	.072	3	.05	4	1.229	2
10			min	-156.397	1	-731.753	2	-125.16	1	-.204	2	.002	10	-.559	3
11		6	max	643.406	3	625.187	2	34.243	3	-.005	15	.087	2	1.185	2
12			min	-1793.152	2	-190.735	3	-161.658	1	-.023	2	-.036	3	-.573	3
13		7	max	642.962	3	623.561	2	34.243	3	-.005	15	.003	10	.797	2
14			min	-1793.744	2	-191.955	3	-161.658	1	-.023	2	-.042	4	-.454	3
15		8	max	642.518	3	621.935	2	34.243	3	-.005	15	.006	3	.411	2
16			min	-1794.336	2	-193.174	3	-161.658	1	-.023	2	-.121	1	-.335	3
17		9	max	641.957	3	93.918	3	43.464	3	.011	5	.077	1	.184	2
18			min	-1887.332	2	-46.238	2	-180.366	1	-.161	2	.007	12	-.282	3
19		10	max	641.514	3	92.699	3	43.464	3	.011	5	.039	3	.213	2
20			min	-1887.924	2	-47.864	2	-180.366	1	-.161	2	-.037	2	-.34	3
21		11	max	641.07	3	91.479	3	43.464	3	.011	5	.066	3	.244	2
22			min	-1888.516	2	-49.49	2	-180.366	1	-.161	2	-.147	1	-.397	3
23		12	max	636.255	3	802.447	3	53.208	2	.249	3	.103	1	.464	2
24			min	-1976.645	2	-503.173	2	-174.613	3	-.233	2	.006	15	-.737	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
25		13	max	635.811	3	801.228	3	53.208	2	.249	3	.117	1	.776	2
26			min	-1977.237	2	-504.8	2	-174.613	3	-.233	2	-.098	3	-1.235	3
27		14	max	156.901	1	473.67	2	57.613	5	.15	1	.001	3	1.077	2
28			min	1.886	12	-742.513	3	-108.023	1	-.318	3	-.15	4	-1.711	3
29		15	max	156.309	1	472.044	2	56.113	5	.15	1	.006	3	.783	2
30			min	1.59	12	-743.732	3	-108.023	1	-.318	3	-.126	4	-1.25	3
31		16	max	155.718	1	470.418	2	54.613	5	.15	1	.011	3	.491	2
32			min	1.195	3	-744.952	3	-108.023	1	-.318	3	-.138	1	-.788	3
33		17	max	155.126	1	468.792	2	53.114	5	.15	1	.016	3	.199	2
34			min	.751	3	-746.171	3	-108.023	1	-.318	3	-.205	1	-.325	3
35		18	max	.76	6	2.087	6	1.5	4	0	1	0	12	0	6
36			min	.179	15	.49	15	0	12	0	1	0	4	0	15
37		19	max	0	1	0	2	0	1	0	1	0	1	0	1
38			min	0	1	-.003	3	0	5	0	1	0	1	0	1
39	M4	1	max	0	1	.013	2	0	4	0	1	0	1	0	1
40			min	0	1	-.004	3	0	1	0	1	0	1	0	1
41		2	max	-.179	15	-.49	15	0	1	0	1	0	1	0	4
42			min	-.76	6	-2.085	4	-1.499	5	0	1	0	5	0	15
43		3	max	10.473	10	931.196	3	0	1	.015	4	.165	4	.704	2
44			min	-197.402	1	-1871.426	2	-79.503	5	0	1	0	1	-.352	3
45		4	max	9.98	10	929.977	3	0	1	.015	4	.115	4	1.866	2
46			min	-197.994	1	-1873.052	2	-81.003	5	0	1	0	1	-.929	3
47		5	max	9.487	10	928.757	3	0	1	.015	4	.064	4	3.029	2
48			min	-198.585	1	-1874.678	2	-82.503	5	0	1	0	1	-1.506	3
49		6	max	2056.42	3	1756.689	2	0	1	0	1	0	1	2.86	2
50			min	-4600.002	2	-739.098	3	-81.683	4	-.01	4	-.007	5	-1.471	3
51		7	max	2055.976	3	1755.063	2	0	1	0	1	0	1	1.771	2
52			min	-4600.594	2	-740.317	3	-83.183	4	-.01	4	-.058	4	-1.011	3
53		8	max	2055.532	3	1753.437	2	0	1	0	1	0	1	.682	2
54			min	-4601.186	2	-741.537	3	-84.683	4	-.01	4	-.11	4	-.552	3
55		9	max	2027.83	3	277.449	3	0	1	.009	4	.101	4	.059	1
56			min	-4616.329	2	-259.61	2	-178.313	4	0	1	0	1	-.314	3
57		10	max	2027.386	3	276.229	3	0	1	.009	4	0	1	.213	1
58			min	-4616.921	2	-261.236	2	-179.812	4	0	1	-.01	4	-.486	3
59		11	max	2026.942	3	275.01	3	0	1	.009	4	0	1	.368	1
60			min	-4617.513	2	-262.862	2	-181.312	4	0	1	-.122	4	-.657	3
61		12	max	2007.747	3	2322.712	3	0	1	.087	4	.036	5	1.062	2
62			min	-4642.392	2	-1696.328	2	-183.547	5	0	1	0	1	-1.637	3
63		13	max	2007.303	3	2321.492	3	0	1	.087	4	0	1	2.116	2
64			min	-4642.983	2	-1697.954	2	-185.047	5	0	1	-.078	4	-3.078	3
65		14	max	199.352	1	1390.502	2	51.509	5	0	1	0	1	3.128	2
66			min	-9.062	10	-1986.326	3	0	1	-.059	4	-.138	5	-4.459	3
67		15	max	198.76	1	1388.876	2	50.009	5	0	1	0	1	2.265	2
68			min	-9.555	10	-1987.545	3	0	1	-.059	4	-.106	5	-3.226	3
69		16	max	198.168	1	1387.25	2	48.509	5	0	1	0	1	1.404	2
70			min	-10.048	10	-1988.765	3	0	1	-.059	4	-.076	4	-1.992	3
71		17	max	197.576	1	1385.624	2	47.01	5	0	1	0	1	.543	2
72			min	-10.542	10	-1989.984	3	0	1	-.059	4	-.046	4	-.757	3
73		18	max	.76	6	2.087	6	1.5	5	0	1	0	1	0	6
74			min	.179	15	.491	15	0	1	0	1	0	5	0	15
75		19	max	0	1	.003	2	0	1	0	1	0	1	0	1
76			min	0	1	-.008	3	0	4	0	1	0	1	0	1
77	M7	1	max	0	1	.006	2	.001	4	0	1	0	1	0	1
78			min	0	1	-.002	3	0	3	0	1	0	1	0	1
79		2	max	-.179	15	-.491	15	0	1	0	1	0	1	0	4
80			min	-.76	6	-2.086	4	-1.499	5	0	1	0	5	0	15
81		3	max	19.462	5	333.483	3	125.16	1	.204	2	.084	5	.322	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
82			min	-155.213	1	-728.501	2	-36.453	5	-.072	3	-.194	1	-.147	3
83		4	max	19.185	5	332.264	3	125.16	1	.204	2	.061	5	.775	2
84			min	-155.805	1	-730.127	2	-37.952	5	-.072	3	-.116	1	-.353	3
85		5	max	18.909	5	331.044	3	125.16	1	.204	2	.037	5	1.229	2
86			min	-156.397	1	-731.753	2	-39.452	5	-.072	3	-.038	1	-.559	3
87		6	max	643.406	3	625.187	2	161.658	1	.023	2	.036	3	1.185	2
88			min	-1793.152	2	-190.735	3	-36.956	5	-.007	5	-.087	2	-.573	3
89		7	max	642.962	3	623.561	2	161.658	1	.023	2	.02	1	.797	2
90			min	-1793.744	2	-191.955	3	-38.456	5	-.007	5	-.034	5	-.454	3
91		8	max	642.518	3	621.935	2	161.658	1	.023	2	.121	1	.411	2
92			min	-1794.336	2	-193.174	3	-39.955	5	-.007	5	-.059	5	-.335	3
93		9	max	641.957	3	93.918	3	180.366	1	.161	2	.042	5	.184	2
94			min	-1887.332	2	-46.238	2	-70.742	5	.011	15	-.077	1	-.282	3
95		10	max	641.514	3	92.699	3	180.366	1	.161	2	.037	2	.213	2
96			min	-1887.924	2	-47.864	2	-72.242	5	.011	15	-.039	3	-.34	3
97		11	max	641.07	3	91.479	3	180.366	1	.161	2	.147	1	.244	2
98			min	-1888.516	2	-49.49	2	-73.742	5	.011	15	-.066	3	-.397	3
99		12	max	636.255	3	802.447	3	174.613	3	.233	2	0	15	.464	2
100			min	-1976.645	2	-503.173	2	-159.373	5	-.249	3	-.103	1	-.737	3
101		13	max	635.811	3	801.228	3	174.613	3	.233	2	.098	3	.776	2
102			min	-1977.237	2	-504.8	2	-160.872	5	-.249	3	-.117	1	-1.235	3
103		14	max	156.901	1	473.67	2	108.023	1	.318	3	.004	1	1.077	2
104			min	1.886	12	-742.513	3	-8.026	3	-.15	1	-.149	5	-1.711	3
105		15	max	156.309	1	472.044	2	108.023	1	.318	3	.071	1	.783	2
106			min	1.59	12	-743.732	3	-8.026	3	-.15	1	-.108	5	-1.25	3
107		16	max	155.718	1	470.418	2	108.023	1	.318	3	.138	1	.491	2
108			min	1.195	3	-744.952	3	-8.026	3	-.15	1	-.067	5	-.788	3
109		17	max	155.126	1	468.792	2	108.023	1	.318	3	.205	1	.199	2
110			min	.751	3	-746.171	3	-8.026	3	-.15	1	-.028	5	-.325	3
111		18	max	.76	6	2.087	4	1.5	5	0	1	0	1	0	4
112			min	.179	15	.491	15	0	1	0	1	0	5	0	15
113		19	max	0	1	0	2	0	12	0	1	0	1	0	1
114			min	0	1	-.003	3	0	1	0	1	0	1	0	1
115	M10	1	max	108.019	1	465.49	2	.134	3	.009	1	.248	1	.15	1
116			min	-8.026	3	-748.568	3	-154.211	1	-.024	3	-.02	3	-.318	3
117		2	max	108.019	1	336.981	2	1.661	3	.009	1	.132	1	.225	3
118			min	-8.026	3	-554.736	3	-126.196	1	-.024	3	-.019	3	-.185	2
119		3	max	108.019	1	208.472	2	3.189	3	.009	1	.059	2	.606	3
120			min	-8.026	3	-360.905	3	-98.18	1	-.024	3	-.017	3	-.412	2
121		4	max	108.019	1	80.13	1	4.716	3	.009	1	.014	10	.826	3
122			min	-8.026	3	-167.074	3	-70.165	1	-.024	3	-.032	1	-.533	2
123		5	max	108.019	1	26.757	3	6.243	3	.009	1	-.004	15	.885	3
124			min	-8.026	3	-48.547	2	-42.15	1	-.024	3	-.079	1	-.546	2
125		6	max	108.019	1	220.588	3	7.771	3	.009	1	-.002	12	.782	3
126			min	-8.026	3	-177.056	2	-28.742	2	-.024	3	-.102	1	-.452	2
127		7	max	108.019	1	414.42	3	18.515	9	.009	1	.004	3	.517	3
128			min	-8.026	3	-305.565	2	-17.666	2	-.024	3	-.102	1	-.251	1
129		8	max	108.019	1	608.251	3	41.897	1	.009	1	.012	3	.091	3
130			min	-8.026	3	-434.075	2	-11.439	10	-.024	3	-.084	2	-.011	5
131		9	max	108.019	1	802.082	3	69.912	1	.009	1	.022	3	.473	2
132			min	-8.605	5	-562.584	2	-8.625	10	-.024	3	-.085	2	-.497	3
133		10	max	108.019	1	223.65	14	97.927	1	0	15	.062	9	.995	2
134			min	-8.026	3	-995.913	3	-57.928	14	-.024	3	-.076	2	-1.246	3
135		11	max	108.019	1	562.584	2	8.625	10	.024	3	.022	3	.473	2
136			min	-8.026	3	-802.082	3	-69.912	1	-.009	1	-.085	2	-.497	3
137		12	max	108.019	1	434.075	2	11.439	10	.024	3	.012	3	.091	3
138			min	-8.026	3	-608.251	3	-41.897	1	-.009	1	-.084	2	.009	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
139		13	max	108.019	1	305.565	2	17.666	2	.024	3	.004	3	.517	3
140			min	-8.026	3	-414.42	3	-18.515	9	-.009	1	-.102	1	-.251	1
141		14	max	108.019	1	177.056	2	28.742	2	.024	3	-.002	12	.782	3
142			min	-8.026	3	-220.588	3	-7.771	3	-.009	1	-.102	1	-.452	2
143		15	max	108.019	1	48.547	2	42.15	1	.024	3	-.002	15	.885	3
144			min	-15.908	5	-26.757	3	-6.243	3	-.009	1	-.079	1	-.546	2
145		16	max	108.019	1	167.074	3	70.165	1	.024	3	.014	10	.826	3
146			min	-24.462	5	-80.13	1	-4.716	3	-.009	1	-.032	1	-.533	2
147		17	max	108.019	1	360.905	3	98.18	1	.024	3	.059	2	.606	3
148			min	-33.017	5	-208.472	2	-3.189	3	-.009	1	-.017	3	-.412	2
149		18	max	108.019	1	554.736	3	126.196	1	.024	3	.132	1	.225	3
150			min	-41.571	5	-336.981	2	-1.661	3	-.009	1	-.019	3	-.185	2
151		19	max	108.019	1	748.568	3	154.211	1	.024	3	.248	1	.15	1
152			min	-50.125	5	-465.49	2	-.134	3	-.009	1	-.02	3	-.318	3
153	M11	1	max	201.831	1	448.981	2	28.618	5	.002	3	.282	1	.096	1
154			min	-217.906	3	-714.125	3	-161.041	1	-.01	2	-.128	5	-.315	3
155		2	max	201.831	1	320.472	2	30.193	5	.002	3	.16	1	.199	3
156			min	-217.906	3	-520.294	3	-133.025	1	-.01	2	-.103	5	-.248	2
157		3	max	201.831	1	192.993	1	31.768	5	.002	3	.072	2	.552	3
158			min	-217.906	3	-326.463	3	-105.01	1	-.01	2	-.077	5	-.462	2
159		4	max	201.831	1	66.981	1	33.344	5	.002	3	.021	2	.744	3
160			min	-217.906	3	-132.632	3	-76.995	1	-.01	2	-.057	4	-.568	2
161		5	max	201.831	1	61.2	3	34.919	5	.002	3	0	12	.773	3
162			min	-217.906	3	-65.056	2	-48.979	1	-.01	2	-.068	1	-.568	2
163		6	max	201.831	1	255.031	3	36.494	5	.002	3	.008	5	.642	3
164			min	-217.906	3	-193.565	2	-32.656	2	-.01	2	-.097	1	-.46	2
165		7	max	201.831	1	448.862	3	42.851	4	.002	3	.039	5	.348	3
166			min	-217.906	3	-322.075	2	-21.581	2	-.01	2	-.103	1	-.245	2
167		8	max	201.831	1	642.693	3	50.264	4	.002	3	.071	5	.077	2
168			min	-217.906	3	-450.584	2	-12.92	10	-.01	2	-.088	2	-.107	3
169		9	max	201.831	1	836.524	3	63.082	1	.002	3	.106	4	.506	2
170			min	-217.906	3	-579.093	2	-10.107	10	-.01	2	-.092	2	-.723	3
171		10	max	201.831	1	1030.356	3	30.801	5	0	15	.157	4	1.042	2
172			min	-217.906	3	23.908	15	-91.098	1	-.01	2	-.087	2	-1.501	3
173		11	max	201.831	1	579.093	2	32.376	5	.01	2	.015	3	.506	2
174			min	-217.906	3	-836.524	3	-63.082	1	-.002	3	-.105	5	-.723	3
175		12	max	201.831	1	450.584	2	33.952	5	.01	2	.009	3	.077	2
176			min	-217.906	3	-642.693	3	-35.067	1	-.002	3	-.088	4	-.107	3
177		13	max	201.831	1	322.075	2	35.527	5	.01	2	.004	3	.348	3
178			min	-217.906	3	-448.862	3	-14.583	9	-.002	3	-.103	1	-.245	2
179		14	max	201.831	1	193.565	2	38.346	4	.01	2	.001	3	.642	3
180			min	-217.906	3	-255.031	3	-3.187	3	-.002	3	-.097	1	-.46	2
181		15	max	201.831	1	65.056	2	48.979	1	.01	2	.014	5	.773	3
182			min	-217.906	3	-61.2	3	-1.66	3	-.002	3	-.068	1	-.568	2
183		16	max	201.831	1	132.632	3	76.995	1	.01	2	.047	5	.744	3
184			min	-217.906	3	-66.981	1	-.133	3	-.002	3	-.021	9	-.568	2
185		17	max	201.831	1	326.463	3	105.01	1	.01	2	.087	4	.552	3
186			min	-217.906	3	-192.993	1	1.141	12	-.002	3	-.001	3	-.462	2
187		18	max	201.831	1	520.294	3	133.025	1	.01	2	.16	1	.199	3
188			min	-217.906	3	-320.472	2	2.159	12	-.002	3	0	3	-.248	2
189		19	max	201.831	1	714.125	3	161.041	1	.01	2	.282	1	.096	1
190			min	-217.906	3	-448.981	2	3.177	12	-.002	3	.003	12	-.315	3
191	M12	1	max	29.196	5	663.226	2	29.966	5	.003	3	.302	1	.139	2
192			min	-18.527	9	-289.544	3	-165.148	1	-.009	2	-.132	5	.016	15
193		2	max	20.642	5	478.671	2	31.541	5	.003	3	.176	1	.261	3
194			min	-18.527	9	-200.331	3	-137.133	1	-.009	2	-.106	5	-.337	2
195		3	max	12.087	5	294.116	2	33.116	5	.003	3	.086	2	.39	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
196			min	-18.527	9	-111.118	3	-109.117	1	-.009	2	-.079	5	-.659	2
197		4	max	9.813	2	109.561	2	34.692	5	.003	3	.032	2	.446	3
198			min	-18.527	9	-21.906	3	-81.102	1	-.009	2	-.057	4	-.827	2
199		5	max	9.813	2	67.307	3	36.267	5	.003	3	.001	10	.427	3
200			min	-18.527	9	-74.994	2	-53.087	1	-.009	2	-.062	1	-.842	2
201		6	max	9.813	2	156.52	3	37.843	5	.003	3	.009	5	.334	3
202			min	-21.139	14	-259.549	2	-37.053	2	-.009	2	-.094	1	-.702	2
203		7	max	9.813	2	245.733	3	43.728	4	.003	3	.041	5	.166	3
204			min	-28.087	4	-444.104	2	-25.978	2	-.009	2	-.103	1	-.409	2
205		8	max	9.813	2	334.946	3	51.14	4	.003	3	.075	5	.038	2
206			min	-36.642	4	-628.66	2	-15.233	10	-.009	2	-.092	2	-.076	3
207		9	max	9.813	2	424.159	3	59.835	14	.003	3	.11	5	.639	2
208			min	-45.196	4	-813.215	2	-12.42	10	-.009	2	-.1	2	-.392	3
209		10	max	9.813	2	997.77	2	74.701	14	0	15	.162	4	1.393	2
210			min	-53.75	4	-220.049	14	-86.99	1	-.009	2	-.098	2	-.783	3
211		11	max	35.679	5	813.215	2	34	5	.009	2	.022	3	.639	2
212			min	-18.527	9	-424.159	3	-58.975	1	-.003	3	-.111	4	-.392	3
213		12	max	27.124	5	628.66	2	35.575	5	.009	2	.013	3	.038	2
214			min	-18.527	9	-334.946	3	-31.248	9	-.003	3	-.092	4	-.076	3
215		13	max	18.57	5	444.104	2	37.151	5	.009	2	.005	3	.166	3
216			min	-18.527	9	-245.733	3	-13.035	9	-.003	3	-.103	1	-.409	2
217		14	max	10.016	5	259.549	2	40.49	4	.009	2	-.002	12	.334	3
218			min	-18.527	9	-156.52	3	-7.523	3	-.003	3	-.094	1	-.702	2
219		15	max	9.813	2	74.994	2	53.087	1	.009	2	.014	5	.427	3
220			min	-18.527	9	-67.307	3	-5.996	3	-.003	3	-.062	1	-.842	2
221		16	max	9.813	2	21.906	3	81.102	1	.009	2	.048	5	.446	3
222			min	-18.527	9	-109.561	2	-4.469	3	-.003	3	-.018	9	-.827	2
223		17	max	9.813	2	111.118	3	109.117	1	.009	2	.092	4	.39	3
224			min	-22.152	14	-294.116	2	-2.941	3	-.003	3	-.015	3	-.659	2
225		18	max	9.813	2	200.331	3	137.133	1	.009	2	.176	1	.261	3
226			min	-30.126	4	-478.671	2	-1.414	3	-.003	3	-.017	3	-.337	2
227		19	max	9.813	2	289.544	3	165.148	1	.009	2	.302	1	.139	2
228			min	-38.68	4	-663.226	2	.113	3	-.003	3	-.018	3	-.019	5
229	M13	1	max	33.399	5	725.652	2	20.015	5	.012	3	.244	1	.204	2
230			min	-125.087	1	-335.975	3	-153.707	1	-.027	2	-.099	5	-.072	3
231		2	max	24.844	5	541.097	2	21.591	5	.012	3	.128	1	.171	3
232			min	-125.087	1	-246.762	3	-125.692	1	-.027	2	-.082	5	-.324	2
233		3	max	16.29	5	356.542	2	23.166	5	.012	3	.056	2	.34	3
234			min	-125.087	1	-157.549	3	-97.676	1	-.027	2	-.063	5	-.698	2
235		4	max	15.518	3	171.987	2	24.741	5	.012	3	.012	10	.434	3
236			min	-125.087	1	-68.336	3	-69.661	1	-.027	2	-.054	4	-.918	2
237		5	max	15.518	3	20.877	3	26.317	5	.012	3	-.004	12	.453	3
238			min	-125.087	1	-12.568	2	-41.645	1	-.027	2	-.081	1	-.985	2
239		6	max	15.518	3	110.09	3	28.137	4	.012	3	0	5	.399	3
240			min	-125.087	1	-197.123	2	-28.406	2	-.027	2	-.104	1	-.897	2
241		7	max	15.518	3	199.303	3	35.549	4	.012	3	.024	5	.27	3
242			min	-125.087	1	-381.678	2	-17.33	2	-.027	2	-.104	1	-.656	2
243		8	max	15.518	3	288.515	3	44.314	14	.012	3	.05	5	.067	3
244			min	-125.087	1	-566.233	2	-11.289	10	-.027	2	-.085	2	-.261	2
245		9	max	15.518	3	377.728	3	70.416	1	.012	3	.079	4	.287	2
246			min	-125.087	1	-750.789	2	-8.476	10	-.027	2	-.086	2	-.211	3
247		10	max	15.518	3	935.344	2	74.047	14	.027	2	.124	4	.99	2
248			min	-125.087	1	-202.172	14	-98.431	1	-.012	3	-.077	2	-.563	3
249		11	max	24.396	5	750.789	2	23.057	5	.027	2	.021	3	.287	2
250			min	-125.087	1	-377.728	3	-70.416	1	-.012	3	-.086	2	-.211	3
251		12	max	15.841	5	566.233	2	24.632	5	.027	2	.012	3	.067	3
252			min	-125.087	1	-288.515	3	-42.401	1	-.012	3	-.085	2	-.261	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
253		13	max	15.518	3	381.678	2	26.207	5	.027	2	.005	3	.27	3
254			min	-125.087	1	-199.303	3	-18.789	9	-.012	3	-.104	1	-.656	2
255		14	max	15.518	3	197.123	2	28.406	2	.027	2	0	12	.399	3
256			min	-125.087	1	-110.09	3	-6.39	3	-.012	3	-.104	1	-.897	2
257		15	max	15.518	3	12.568	2	41.645	1	.027	2	.013	5	.453	3
258			min	-125.087	1	-20.877	3	-4.863	3	-.012	3	-.081	1	-.985	2
259		16	max	15.518	3	68.336	3	69.661	1	.027	2	.038	5	.434	3
260			min	-125.087	1	-171.987	2	-3.335	3	-.012	3	-.035	1	-.918	2
261		17	max	15.518	3	157.549	3	97.676	1	.027	2	.066	4	.34	3
262			min	-125.087	1	-356.542	2	-1.808	3	-.012	3	-.011	3	-.698	2
263		18	max	15.518	3	246.762	3	125.692	1	.027	2	.128	1	.171	3
264			min	-125.087	1	-541.097	2	-.281	3	-.012	3	-.012	3	-.324	2
265		19	max	15.518	3	335.975	3	153.707	1	.027	2	.244	1	.204	2
266			min	-125.087	1	-725.652	2	1.234	12	-.012	3	-.012	3	-.072	3
267	M2	1	max	2363.778	2	719.294	3	175.074	2	.005	5	.958	5	5.58	1
268			min	-1900.52	3	-458.4	2	-264.589	5	-.005	2	-.185	1	.29	12
269		2	max	2361.517	2	719.294	3	175.074	2	.005	5	.893	5	5.607	1
270			min	-1902.216	3	-458.4	2	-262.63	5	-.005	2	-.144	1	.182	12
271		3	max	2359.256	2	719.294	3	175.074	2	.005	5	.828	5	5.634	1
272			min	-1903.911	3	-458.4	2	-260.671	5	-.005	2	-.102	1	.075	12
273		4	max	2356.996	2	719.294	3	175.074	2	.005	5	.763	5	5.661	1
274			min	-1905.607	3	-458.4	2	-258.711	5	-.005	2	-.061	1	-.081	3
275		5	max	1665.808	2	1619.285	1	132.15	2	.002	2	.702	5	5.628	1
276			min	-1643.838	3	-66.849	3	-248.368	5	0	3	-.06	1	-.232	3
277		6	max	1663.547	2	1619.285	1	132.15	2	.002	2	.64	4	5.226	1
278			min	-1645.534	3	-66.849	3	-246.409	5	0	3	-.028	1	-.216	3
279		7	max	1661.287	2	1619.285	1	132.15	2	.002	2	.583	4	4.824	1
280			min	-1647.229	3	-66.849	3	-244.45	5	0	3	-.059	3	-.199	3
281		8	max	1659.026	2	1619.285	1	132.15	2	.002	2	.526	4	4.422	1
282			min	-1648.924	3	-66.849	3	-242.491	5	0	3	-.104	3	-.183	3
283		9	max	1656.765	2	1619.285	1	132.15	2	.002	2	.47	4	4.02	1
284			min	-1650.62	3	-66.849	3	-240.532	5	0	3	-.149	3	-.166	3
285		10	max	1654.505	2	1619.285	1	132.15	2	.002	2	.414	4	3.618	1
286			min	-1652.315	3	-66.849	3	-238.572	5	0	3	-.195	3	-.149	3
287		11	max	1652.244	2	1619.285	1	132.15	2	.002	2	.359	4	3.216	1
288			min	-1654.011	3	-66.849	3	-236.613	5	0	3	-.24	3	-.133	3
289		12	max	1649.984	2	1619.285	1	132.15	2	.002	2	.304	4	2.814	1
290			min	-1655.706	3	-66.849	3	-234.654	5	0	3	-.285	3	-.116	3
291		13	max	1647.723	2	1619.285	1	132.15	2	.002	2	.25	4	2.412	1
292			min	-1657.402	3	-66.849	3	-232.695	5	0	3	-.331	3	-.1	3
293		14	max	1645.462	2	1619.285	1	132.15	2	.002	2	.243	2	2.01	1
294			min	-1659.097	3	-66.849	3	-230.736	5	0	3	-.376	3	-.083	3
295		15	max	1643.202	2	1619.285	1	132.15	2	.002	2	.276	2	1.608	1
296			min	-1660.793	3	-66.849	3	-228.777	5	0	3	-.422	3	-.066	3
297		16	max	1640.941	2	1619.285	1	132.15	2	.002	2	.308	2	1.206	1
298			min	-1662.488	3	-66.849	3	-226.817	5	0	3	-.467	3	-.05	3
299		17	max	1638.681	2	1619.285	1	132.15	2	.002	2	.341	2	.804	1
300			min	-1664.184	3	-66.849	3	-224.858	5	0	3	-.512	3	-.033	3
301		18	max	1636.42	2	1619.285	1	132.15	2	.002	2	.374	2	.402	1
302			min	-1665.879	3	-66.849	3	-222.899	5	0	3	-.558	3	-.017	3
303		19	max	1634.159	2	1619.285	1	132.15	2	.002	2	.407	2	0	1
304			min	-1667.574	3	-66.849	3	-220.94	5	0	3	-.603	3	0	1
305	M5	1	max	6374.818	2	2148.96	3	0	1	.005	4	1	4	10.164	1
306			min	-5557.181	3	-2169.165	2	-283.098	5	0	1	0	1	.262	15
307		2	max	6372.558	2	2148.96	3	0	1	.005	4	.931	4	10.491	1
308			min	-5558.877	3	-2169.165	2	-281.138	5	0	1	0	1	.143	12
309		3	max	6370.297	2	2148.96	3	0	1	.005	4	.861	4	10.852	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
310			min	-5560.572	3	-2169.165	2	-279.179	5	0	1	0	1	-.336	3
311		4	max	6368.036	2	2148.96	3	0	1	.005	4	.792	4	11.39	2
312			min	-5562.268	3	-2169.165	2	-277.22	5	0	1	0	1	-.869	3
313		5	max	4572.052	2	3376.432	2	0	1	0	1	.729	4	11.735	2
314			min	-4706.111	3	-378.213	3	-268.247	4	0	4	0	1	-1.315	3
315		6	max	4569.792	2	3376.432	2	0	1	0	1	.663	4	10.897	2
316			min	-4707.806	3	-378.213	3	-266.288	4	0	4	0	1	-1.221	3
317		7	max	4567.531	2	3376.432	2	0	1	0	1	.597	4	10.059	2
318			min	-4709.502	3	-378.213	3	-264.329	4	0	4	0	1	-1.127	3
319		8	max	4565.27	2	3376.432	2	0	1	0	1	.531	4	9.22	2
320			min	-4711.197	3	-378.213	3	-262.369	4	0	4	0	1	-1.033	3
321		9	max	4563.01	2	3376.432	2	0	1	0	1	.467	4	8.382	2
322			min	-4712.893	3	-378.213	3	-260.41	4	0	4	0	1	-.939	3
323		10	max	4560.749	2	3376.432	2	0	1	0	1	.402	4	7.544	2
324			min	-4714.588	3	-378.213	3	-258.451	4	0	4	0	1	-.845	3
325		11	max	4558.489	2	3376.432	2	0	1	0	1	.338	4	6.706	2
326			min	-4716.284	3	-378.213	3	-256.492	4	0	4	0	1	-.751	3
327		12	max	4556.228	2	3376.432	2	0	1	0	1	.275	4	5.868	2
328			min	-4717.979	3	-378.213	3	-254.533	4	0	4	0	1	-.657	3
329		13	max	4553.968	2	3376.432	2	0	1	0	1	.212	4	5.029	2
330			min	-4719.674	3	-378.213	3	-252.574	4	0	4	0	1	-.563	3
331		14	max	4551.707	2	3376.432	2	0	1	0	1	.149	4	4.191	2
332			min	-4721.37	3	-378.213	3	-250.614	4	0	4	0	1	-.469	3
333		15	max	4549.446	2	3376.432	2	0	1	0	1	.087	4	3.353	2
334			min	-4723.065	3	-378.213	3	-248.655	4	0	4	0	1	-.376	3
335		16	max	4547.186	2	3376.432	2	0	1	0	1	.026	4	2.515	2
336			min	-4724.761	3	-378.213	3	-246.696	4	0	4	0	1	-.282	3
337		17	max	4544.925	2	3376.432	2	0	1	0	1	0	1	1.676	2
338			min	-4726.456	3	-378.213	3	-244.737	4	0	4	-.035	4	-.188	3
339		18	max	4542.665	2	3376.432	2	0	1	0	1	0	1	.838	2
340			min	-4728.152	3	-378.213	3	-242.778	4	0	4	-.096	4	-.094	3
341		19	max	4540.404	2	3376.432	2	0	1	0	1	0	1	0	1
342			min	-4729.847	3	-378.213	3	-240.818	4	0	4	-.156	4	0	1
343	M8	1	max	2363.778	2	719.294	3	200.929	3	.005	4	1.002	4	5.58	1
344			min	-1900.52	3	-458.4	2	-296.838	4	-.002	3	-.209	3	-.212	5
345		2	max	2361.517	2	719.294	3	200.929	3	.005	4	.929	4	5.607	1
346			min	-1902.216	3	-458.4	2	-294.879	4	-.002	3	-.159	3	-.186	5
347		3	max	2359.256	2	719.294	3	200.929	3	.005	4	.856	4	5.634	1
348			min	-1903.911	3	-458.4	2	-292.92	4	-.002	3	-.109	3	-.161	5
349		4	max	2356.996	2	719.294	3	200.929	3	.005	4	.783	4	5.661	1
350			min	-1905.607	3	-458.4	2	-290.96	4	-.002	3	-.06	3	-.136	5
351		5	max	1665.808	2	1619.285	1	182.785	3	0	3	.721	4	5.628	1
352			min	-1643.838	3	-66.849	3	-275.426	4	-.002	2	-.032	3	-.232	3
353		6	max	1663.547	2	1619.285	1	182.785	3	0	3	.652	4	5.226	1
354			min	-1645.534	3	-66.849	3	-273.467	4	-.002	2	.008	12	-.216	3
355		7	max	1661.287	2	1619.285	1	182.785	3	0	3	.585	4	4.824	1
356			min	-1647.229	3	-66.849	3	-271.508	4	-.002	2	-.013	2	-.199	3
357		8	max	1659.026	2	1619.285	1	182.785	3	0	3	.518	4	4.422	1
358			min	-1648.924	3	-66.849	3	-269.549	4	-.002	2	-.046	2	-.183	3
359		9	max	1656.765	2	1619.285	1	182.785	3	0	3	.455	5	4.02	1
360			min	-1650.62	3	-66.849	3	-267.59	4	-.002	2	-.079	2	-.166	3
361		10	max	1654.505	2	1619.285	1	182.785	3	0	3	.393	5	3.618	1
362			min	-1652.315	3	-66.849	3	-265.63	4	-.002	2	-.111	2	-.149	3
363		11	max	1652.244	2	1619.285	1	182.785	3	0	3	.332	5	3.216	1
364			min	-1654.011	3	-66.849	3	-263.671	4	-.002	2	-.144	2	-.133	3
365		12	max	1649.984	2	1619.285	1	182.785	3	0	3	.285	3	2.814	1
366			min	-1655.706	3	-66.849	3	-261.712	4	-.002	2	-.177	2	-.116	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
367		13	max	1647.723	2	1619.285	1	182.785	3	0	3	.331	3	2.412	1
368			min	-1657.402	3	-66.849	3	-259.753	4	-.002	2	-.21	2	-.1	3
369		14	max	1645.462	2	1619.285	1	182.785	3	0	3	.376	3	2.01	1
370			min	-1659.097	3	-66.849	3	-257.794	4	-.002	2	-.243	2	-.083	3
371		15	max	1643.202	2	1619.285	1	182.785	3	0	3	.422	3	1.608	1
372			min	-1660.793	3	-66.849	3	-255.835	4	-.002	2	-.276	2	-.066	3
373		16	max	1640.941	2	1619.285	1	182.785	3	0	3	.467	3	1.206	1
374			min	-1662.488	3	-66.849	3	-253.875	4	-.002	2	-.308	2	-.05	3
375		17	max	1638.681	2	1619.285	1	182.785	3	0	3	.512	3	.804	1
376			min	-1664.184	3	-66.849	3	-251.916	4	-.002	2	-.341	2	-.033	3
377		18	max	1636.42	2	1619.285	1	182.785	3	0	3	.558	3	.402	1
378			min	-1665.879	3	-66.849	3	-249.957	4	-.002	2	-.374	2	-.017	3
379		19	max	1634.159	2	1619.285	1	182.785	3	0	3	.603	3	0	1
380			min	-1667.574	3	-66.849	3	-247.998	4	-.002	2	-.407	2	0	1
381	M3	1	max	2175.476	2	4.757	4	42.296	2	.022	3	.009	2	0	1
382			min	-829.378	3	1.118	15	-18.715	3	-.046	2	-.004	3	0	1
383		2	max	2175.337	2	4.229	4	42.296	2	.022	3	.021	2	0	15
384			min	-829.482	3	.994	15	-18.715	3	-.046	2	-.01	3	-.001	4
385		3	max	2175.198	2	3.7	4	42.296	2	.022	3	.034	2	0	15
386			min	-829.587	3	.87	15	-18.715	3	-.046	2	-.015	3	-.002	4
387		4	max	2175.058	2	3.171	4	42.296	2	.022	3	.046	2	0	15
388			min	-829.691	3	.745	15	-18.715	3	-.046	2	-.021	3	-.003	4
389		5	max	2174.919	2	2.643	4	42.296	2	.022	3	.058	2	-.001	15
390			min	-829.796	3	.621	15	-18.715	3	-.046	2	-.026	3	-.004	4
391		6	max	2174.779	2	2.114	4	42.296	2	.022	3	.071	2	-.001	15
392			min	-829.901	3	.497	15	-18.715	3	-.046	2	-.032	3	-.005	4
393		7	max	2174.64	2	1.586	4	42.296	2	.022	3	.083	2	-.001	15
394			min	-830.005	3	.373	15	-18.715	3	-.046	2	-.037	3	-.006	4
395		8	max	2174.501	2	1.057	4	42.296	2	.022	3	.096	2	-.001	15
396			min	-830.11	3	.248	15	-18.715	3	-.046	2	-.043	3	-.006	4
397		9	max	2174.361	2	.529	4	42.296	2	.022	3	.108	2	-.001	15
398			min	-830.214	3	.124	15	-18.715	3	-.046	2	-.048	3	-.006	4
399		10	max	2174.222	2	0	1	42.296	2	.022	3	.12	2	-.001	15
400			min	-830.319	3	0	1	-18.715	3	-.046	2	-.054	3	-.006	4
401		11	max	2174.082	2	-.124	15	42.296	2	.022	3	.133	2	-.001	15
402			min	-830.423	3	-.529	6	-18.715	3	-.046	2	-.059	3	-.006	4
403		12	max	2173.943	2	-.248	15	42.296	2	.022	3	.145	2	-.001	15
404			min	-830.528	3	-1.057	6	-18.715	3	-.046	2	-.064	3	-.006	4
405		13	max	2173.803	2	-.373	15	42.296	2	.022	3	.158	2	-.001	15
406			min	-830.632	3	-1.586	6	-18.715	3	-.046	2	-.07	3	-.006	4
407		14	max	2173.664	2	-.497	15	42.296	2	.022	3	.17	2	-.001	15
408			min	-830.737	3	-2.114	6	-18.715	3	-.046	2	-.075	3	-.005	4
409		15	max	2173.525	2	-.621	15	42.296	2	.022	3	.182	2	-.001	15
410			min	-830.842	3	-2.643	6	-18.715	3	-.046	2	-.081	3	-.004	4
411		16	max	2173.385	2	-.745	15	42.296	2	.022	3	.195	2	0	15
412			min	-830.946	3	-3.171	6	-18.715	3	-.046	2	-.086	3	-.003	4
413		17	max	2173.246	2	-.87	15	42.296	2	.022	3	.207	2	0	15
414			min	-831.051	3	-3.7	6	-18.715	3	-.046	2	-.092	3	-.002	4
415		18	max	2173.106	2	-.994	15	42.296	2	.022	3	.22	2	0	15
416			min	-831.155	3	-4.229	6	-18.715	3	-.046	2	-.097	3	-.001	4
417		19	max	2172.967	2	-1.118	15	42.296	2	.022	3	.232	2	0	1
418			min	-831.26	3	-4.757	6	-18.715	3	-.046	2	-.103	3	0	1
419	M6	1	max	5793.115	2	4.757	4	0	1	.006	4	.004	4	0	1
420			min	-2673.107	3	1.118	15	-9.911	4	0	1	0	1	0	1
421		2	max	5792.976	2	4.229	4	0	1	.006	4	0	4	0	15
422			min	-2673.212	3	.994	15	-9.534	4	0	1	0	1	-.001	4
423		3	max	5792.836	2	3.7	4	0	1	.006	4	0	1	0	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
424			min	-2673.316	3	.87	15	-9.157	4	0	1	-.002	4	-.002	4
425		4	max	5792.697	2	3.171	4	0	1	.006	4	0	1	0	15
426			min	-2673.421	3	.745	15	-8.78	4	0	1	-.005	4	-.003	4
427		5	max	5792.557	2	2.643	4	0	1	.006	4	0	1	-.001	15
428			min	-2673.525	3	.621	15	-8.403	4	0	1	-.007	4	-.004	4
429		6	max	5792.418	2	2.114	4	0	1	.006	4	0	1	-.001	15
430			min	-2673.63	3	.497	15	-8.027	4	0	1	-.01	4	-.005	4
431		7	max	5792.278	2	1.586	4	0	1	.006	4	0	1	-.001	15
432			min	-2673.735	3	.373	15	-7.65	4	0	1	-.012	4	-.006	4
433		8	max	5792.139	2	1.057	4	0	1	.006	4	0	1	-.001	15
434			min	-2673.839	3	.248	15	-7.273	4	0	1	-.014	4	-.006	4
435		9	max	5792	2	.529	4	0	1	.006	4	0	1	-.001	15
436			min	-2673.944	3	.124	15	-6.896	4	0	1	-.016	4	-.006	4
437		10	max	5791.86	2	0	1	0	1	.006	4	0	1	-.001	15
438			min	-2674.048	3	0	1	-6.519	4	0	1	-.018	4	-.006	4
439		11	max	5791.721	2	-.124	15	0	1	.006	4	0	1	-.001	15
440			min	-2674.153	3	-.529	6	-6.142	4	0	1	-.02	4	-.006	4
441		12	max	5791.581	2	-.248	15	0	1	.006	4	0	1	-.001	15
442			min	-2674.257	3	-1.057	6	-5.765	4	0	1	-.022	4	-.006	4
443		13	max	5791.442	2	-.373	15	0	1	.006	4	0	1	-.001	15
444			min	-2674.362	3	-1.586	6	-5.389	4	0	1	-.023	4	-.006	4
445		14	max	5791.303	2	-.497	15	0	1	.006	4	0	1	-.001	15
446			min	-2674.466	3	-2.114	6	-5.012	4	0	1	-.025	4	-.005	4
447		15	max	5791.163	2	-.621	15	0	1	.006	4	0	1	-.001	15
448			min	-2674.571	3	-2.643	6	-4.635	4	0	1	-.026	4	-.004	4
449		16	max	5791.024	2	-.745	15	0	1	.006	4	0	1	0	15
450			min	-2674.676	3	-3.171	6	-4.258	4	0	1	-.028	4	-.003	4
451		17	max	5790.884	2	-.87	15	0	1	.006	4	0	1	0	15
452			min	-2674.78	3	-3.7	6	-3.881	4	0	1	-.029	4	-.002	4
453		18	max	5790.745	2	-.994	15	0	1	.006	4	0	1	0	15
454			min	-2674.885	3	-4.229	6	-3.504	4	0	1	-.03	4	-.001	4
455		19	max	5790.606	2	-1.118	15	0	1	.006	4	0	1	0	1
456			min	-2674.989	3	-4.757	6	-3.128	4	0	1	-.031	4	0	1
457	M9	1	max	2175.476	2	4.757	4	18.715	3	.046	2	.004	3	0	1
458			min	-829.378	3	1.118	15	-42.296	2	-.022	3	-.009	2	0	1
459		2	max	2175.337	2	4.229	4	18.715	3	.046	2	.01	3	0	15
460			min	-829.482	3	.994	15	-42.296	2	-.022	3	-.021	2	-.001	4
461		3	max	2175.198	2	3.7	4	18.715	3	.046	2	.015	3	0	15
462			min	-829.587	3	.87	15	-42.296	2	-.022	3	-.034	2	-.002	4
463		4	max	2175.058	2	3.171	4	18.715	3	.046	2	.021	3	0	15
464			min	-829.691	3	.745	15	-42.296	2	-.022	3	-.046	2	-.003	4
465		5	max	2174.919	2	2.643	4	18.715	3	.046	2	.026	3	-.001	15
466			min	-829.796	3	.621	15	-42.296	2	-.022	3	-.058	2	-.004	4
467		6	max	2174.779	2	2.114	4	18.715	3	.046	2	.032	3	-.001	15
468			min	-829.901	3	.497	15	-42.296	2	-.022	3	-.071	2	-.005	4
469		7	max	2174.64	2	1.586	4	18.715	3	.046	2	.037	3	-.001	15
470			min	-830.005	3	.373	15	-42.296	2	-.022	3	-.083	2	-.006	4
471		8	max	2174.501	2	1.057	4	18.715	3	.046	2	.043	3	-.001	15
472			min	-830.11	3	.248	15	-42.296	2	-.022	3	-.096	2	-.006	4
473		9	max	2174.361	2	.529	4	18.715	3	.046	2	.048	3	-.001	15
474			min	-830.214	3	.124	15	-42.296	2	-.022	3	-.108	2	-.006	4
475		10	max	2174.222	2	0	1	18.715	3	.046	2	.054	3	-.001	15
476			min	-830.319	3	0	1	-42.296	2	-.022	3	-.12	2	-.006	4
477		11	max	2174.082	2	-.124	15	18.715	3	.046	2	.059	3	-.001	15
478			min	-830.423	3	-.529	6	-42.296	2	-.022	3	-.133	2	-.006	4
479		12	max	2173.943	2	-.248	15	18.715	3	.046	2	.064	3	-.001	15
480			min	-830.528	3	-1.057	6	-42.296	2	-.022	3	-.145	2	-.006	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
481		13	max	2173.803	2	-.373	15	18.715	3	.046	2	.07	3	-.001	15
482			min	-830.632	3	-1.586	6	-42.296	2	-.022	3	-.158	2	-.006	4
483		14	max	2173.664	2	-.497	15	18.715	3	.046	2	.075	3	-.001	15
484			min	-830.737	3	-2.114	6	-42.296	2	-.022	3	-.17	2	-.005	4
485		15	max	2173.525	2	-.621	15	18.715	3	.046	2	.081	3	-.001	15
486			min	-830.842	3	-2.643	6	-42.296	2	-.022	3	-.182	2	-.004	4
487		16	max	2173.385	2	-.745	15	18.715	3	.046	2	.086	3	0	15
488			min	-830.946	3	-3.171	6	-42.296	2	-.022	3	-.195	2	-.003	4
489		17	max	2173.246	2	-.87	15	18.715	3	.046	2	.092	3	0	15
490			min	-831.051	3	-3.7	6	-42.296	2	-.022	3	-.207	2	-.002	4
491		18	max	2173.106	2	-.994	15	18.715	3	.046	2	.097	3	0	15
492			min	-831.155	3	-4.229	6	-42.296	2	-.022	3	-.22	2	-.001	4
493		19	max	2172.967	2	-1.118	15	18.715	3	.046	2	.103	3	0	1
494			min	-831.26	3	-4.757	6	-42.296	2	-.022	3	-.232	2	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	.005	3	.191	3	.018	1	9.152e-3	3	NC	3	NC	3
2			min	-.239	1	-.755	2	-.346	5	-2.188e-2	2	168.48	2	458.789	5
3		2	max	.005	3	.148	3	.005	1	9.152e-3	3	5272.4	12	NC	3
4			min	-.239	1	-.644	2	-.33	4	-2.188e-2	2	195.887	2	485.133	5
5		3	max	.005	3	.106	3	0	3	8.59e-3	3	2837.201	15	NC	1
6			min	-.239	1	-.532	2	-.315	4	-2.029e-2	2	233.988	2	516.452	5
7		4	max	.005	3	.065	3	0	3	7.726e-3	3	3102.523	15	NC	1
8			min	-.238	1	-.425	2	-.296	4	-1.783e-2	2	286.894	1	559.895	5
9		5	max	.005	3	.028	3	.001	3	6.863e-3	3	3409.411	15	NC	1
10			min	-.238	1	-.329	2	-.273	4	-1.538e-2	2	355.091	1	618.579	5
11		6	max	.005	3	0	3	.002	3	6.578e-3	3	3757.122	15	NC	1
12			min	-.238	1	-.252	1	-.248	4	-1.422e-2	2	443.234	1	695.96	5
13		7	max	.004	3	-.012	12	.001	3	6.693e-3	3	4151.695	15	NC	1
14			min	-.237	1	-.191	1	-.224	4	-1.395e-2	2	554.879	1	794.728	5
15		8	max	.004	3	-.011	15	0	3	6.808e-3	3	4611.164	15	NC	2
16			min	-.237	1	-.14	1	-.201	4	-1.367e-2	2	595.522	3	917.744	5
17		9	max	.004	3	-.008	15	0	10	7.169e-3	3	5163.747	15	NC	2
18			min	-.236	1	-.093	1	-.18	4	-1.28e-2	2	571.935	3	1067.628	5
19		10	max	.004	3	-.005	15	0	2	7.966e-3	3	5849.744	15	NC	2
20			min	-.236	1	-.049	1	-.159	4	-1.086e-2	2	558.901	3	1283.248	5
21		11	max	.004	3	-.002	15	0	3	8.763e-3	3	6720.439	15	NC	2
22			min	-.235	1	-.049	3	-.138	4	-8.919e-3	2	557.131	3	1604.383	5
23		12	max	.003	3	.031	2	.004	3	7.138e-3	3	NC	2	NC	1
24			min	-.234	1	-.045	3	-.119	4	-6.423e-3	2	567.849	3	2104.033	5
25		13	max	.003	3	.062	1	.008	3	4.143e-3	3	NC	1	NC	1
26			min	-.233	1	-.03	3	-.099	4	-3.612e-3	2	605.102	3	3055.164	5
27		14	max	.003	3	.083	1	.008	3	1.3e-3	3	NC	9	NC	2
28			min	-.233	1	.001	12	-.081	4	-3.02e-3	4	705.998	3	4913.083	5
29		15	max	.003	3	.09	1	.006	3	5.131e-3	3	NC	4	NC	2
30			min	-.233	1	.009	15	-.07	5	-2.741e-3	4	992.417	3	6875.205	1
31		16	max	.003	3	.128	3	.007	1	8.962e-3	3	NC	4	NC	3
32			min	-.233	1	.011	15	-.063	5	-4.498e-3	2	2128.553	3	6036.679	1
33		17	max	.003	3	.211	3	.004	1	1.279e-2	3	NC	4	NC	3
34			min	-.233	1	.013	15	-.059	5	-6.299e-3	1	4580.068	2	6710.813	1
35		18	max	.003	3	.299	3	0	12	1.529e-2	3	NC	1	NC	1
36			min	-.233	1	.016	15	-.057	4	-7.474e-3	1	1249.661	3	NC	1
37		19	max	.003	3	.386	3	-.001	12	1.529e-2	3	NC	1	NC	1
38			min	-.233	1	.018	15	-.057	4	-7.474e-3	1	689.599	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
39	M4	1	max	.041	3	.501	3	0	1	2.892e-4	4	NC	3	NC	1
40			min	-.481	2	-1.623	2	-.342	4	0	1	84.586	2	464.358	4
41		2	max	.041	3	.397	3	0	1	2.892e-4	4	4742.333	15	NC	1
42			min	-.481	2	-1.38	2	-.33	4	0	1	99.904	2	484.745	4
43		3	max	.041	3	.294	3	0	1	1.744e-4	5	5673.985	15	NC	1
44			min	-.481	2	-1.136	2	-.316	4	0	1	122.069	2	509.824	4
45		4	max	.041	3	.195	3	0	1	0	1	7007.706	15	NC	1
46			min	-.481	2	-.902	2	-.297	4	-1.741e-6	4	155.194	2	549.758	4
47		5	max	.041	3	.109	3	0	1	0	1	8915.709	15	NC	1
48			min	-.481	2	-.693	2	-.274	4	-1.778e-4	4	204.599	2	607.637	4
49		6	max	.04	3	.044	3	0	1	0	1	NC	15	NC	1
50			min	-.48	2	-.528	2	-.249	4	-1.809e-4	4	273.769	2	686.747	4
51		7	max	.039	3	0	3	0	1	0	1	NC	15	NC	1
52			min	-.478	2	-.403	2	-.223	4	-6.441e-5	4	267.667	3	788.744	4
53		8	max	.039	3	-.007	15	0	1	5.23e-5	5	NC	5	NC	1
54			min	-.476	2	-.303	2	-.2	4	0	1	252.573	3	913.263	4
55		9	max	.038	3	-.005	15	0	1	8.948e-5	4	NC	5	NC	1
56			min	-.475	2	-.211	2	-.18	4	0	1	242.255	3	1056.663	4
57		10	max	.037	3	-.003	15	0	1	0	1	NC	4	NC	1
58			min	-.473	2	-.119	2	-.159	4	-1.316e-5	4	234.41	3	1271.538	4
59		11	max	.036	3	0	15	0	1	0	1	NC	2	NC	1
60			min	-.471	2	-.083	3	-.138	4	-1.158e-4	4	229.673	3	1589.302	4
61		12	max	.036	3	.055	1	0	1	0	1	NC	5	NC	1
62			min	-.469	2	-.086	3	-.119	4	-8.254e-4	4	228.392	3	2041.666	4
63		13	max	.035	3	.125	2	0	1	0	1	NC	5	NC	1
64			min	-.468	2	-.067	3	-.1	4	-1.878e-3	4	235.936	3	2895.137	4
65		14	max	.034	3	.166	2	0	1	0	1	NC	5	NC	1
66			min	-.466	2	-.006	3	-.083	4	-2.892e-3	4	264.55	3	4505.397	4
67		15	max	.034	3	.164	2	0	1	0	1	NC	5	NC	1
68			min	-.466	2	.004	15	-.072	4	-2.183e-3	4	348.137	3	7267.867	4
69		16	max	.034	3	.282	3	0	1	0	1	NC	5	NC	1
70			min	-.466	2	.003	15	-.064	4	-1.473e-3	4	612.848	3	NC	1
71		17	max	.034	3	.476	3	0	1	0	1	NC	5	NC	1
72			min	-.466	2	.002	15	-.06	4	-7.63e-4	4	1137.635	2	NC	1
73		18	max	.034	3	.68	3	0	1	0	1	NC	4	NC	1
74			min	-.466	2	0	15	-.056	4	-3.002e-4	4	749.065	3	NC	1
75		19	max	.034	3	.883	3	0	1	0	1	NC	1	NC	1
76			min	-.466	2	-.041	1	-.053	4	-3.002e-4	4	350.825	3	NC	1
77	M7	1	max	.006	5	.191	3	.001	3	2.188e-2	2	NC	3	NC	3
78			min	-.239	1	-.755	2	-.352	4	-9.152e-3	3	168.48	2	444.479	4
79		2	max	.006	5	.148	3	0	3	2.188e-2	2	NC	5	NC	3
80			min	-.239	1	-.644	2	-.333	4	-9.152e-3	3	195.887	2	474.555	4
81		3	max	.006	5	.106	3	.006	1	2.029e-2	2	NC	5	NC	1
82			min	-.239	1	-.532	2	-.313	4	-8.59e-3	3	233.988	2	509.828	4
83		4	max	.006	5	.065	3	.01	1	1.783e-2	2	NC	5	NC	1
84			min	-.238	1	-.425	2	-.292	5	-7.726e-3	3	286.894	1	554.711	4
85		5	max	.006	5	.028	3	.01	1	1.538e-2	2	NC	5	NC	1
86			min	-.238	1	-.329	2	-.269	5	-6.863e-3	3	355.091	1	612.319	4
87		6	max	.006	5	.006	5	.008	1	1.422e-2	2	NC	5	NC	1
88			min	-.238	1	-.252	1	-.246	5	-6.578e-3	3	443.234	1	686.045	4
89		7	max	.006	5	.005	5	.004	2	1.395e-2	2	NC	4	NC	1
90			min	-.237	1	-.191	1	-.223	4	-6.693e-3	3	554.879	1	777.186	4
91		8	max	.006	5	.005	5	0	2	1.367e-2	2	NC	4	NC	2
92			min	-.237	1	-.14	1	-.201	4	-6.808e-3	3	595.522	3	889.991	4
93		9	max	.006	5	.004	5	0	3	1.28e-2	2	NC	4	NC	2
94			min	-.236	1	-.093	1	-.18	4	-7.169e-3	3	571.935	3	1031.43	4
95		10	max	.006	5	.003	5	0	3	1.086e-2	2	NC	4	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
96			min	-.236	1	-.049	1	-.159	4	-7.966e-3	3	558.901	3	1230.587	4
97		11	max	.006	5	.002	5	0	2	8.919e-3	2	NC	4	NC	2
98			min	-.235	1	-.049	3	-.138	4	-8.763e-3	3	557.131	3	1525.933	4
99		12	max	.006	5	.031	2	.004	1	6.423e-3	2	NC	2	NC	1
100			min	-.234	1	-.045	3	-.117	4	-7.138e-3	3	567.849	3	1996.958	4
101		13	max	.006	5	.062	1	.005	2	3.612e-3	2	NC	1	NC	1
102			min	-.233	1	-.03	3	-.097	4	-4.143e-3	3	605.102	3	2840.202	4
103		14	max	.006	5	.083	1	.003	2	9.031e-4	2	NC	5	NC	2
104			min	-.233	1	-.002	5	-.081	4	-2.827e-3	5	705.998	3	4262.636	4
105		15	max	.006	5	.09	1	0	10	2.701e-3	2	NC	5	NC	2
106			min	-.233	1	-.005	5	-.072	4	-5.131e-3	3	992.417	3	6229.033	4
107		16	max	.006	5	.128	3	-.002	10	4.498e-3	2	NC	5	NC	3
108			min	-.233	1	-.009	5	-.065	4	-8.962e-3	3	2128.553	3	6036.679	1
109		17	max	.006	5	.211	3	0	12	6.299e-3	1	NC	4	NC	3
110			min	-.233	1	-.013	5	-.06	4	-1.279e-2	3	4580.068	2	6710.813	1
111		18	max	.006	5	.299	3	.005	1	7.474e-3	1	NC	1	NC	1
112			min	-.233	1	-.017	5	-.056	5	-1.529e-2	3	1249.661	3	NC	1
113		19	max	.006	5	.386	3	.015	1	7.474e-3	1	NC	1	NC	1
114			min	-.233	1	-.021	5	-.052	5	-1.529e-2	3	689.599	3	NC	1
115	M10	1	max	0	1	.268	3	.233	1	1.17e-2	3	NC	1	NC	1
116			min	-.057	4	-.015	5	-.006	5	-1.958e-3	2	NC	1	NC	1
117		2	max	0	1	.424	3	.259	1	1.343e-2	3	NC	4	NC	3
118			min	-.057	4	-.015	2	-.002	3	-2.616e-3	2	1153.438	3	6868.768	1
119		3	max	0	1	.569	3	.3	1	1.516e-2	3	NC	4	NC	3
120			min	-.057	4	-.08	2	-.003	3	-3.275e-3	2	599.075	3	2678.745	1
121		4	max	0	1	.68	3	.346	1	1.689e-2	3	NC	5	NC	3
122			min	-.057	4	-.124	2	-.007	3	-3.933e-3	2	436.682	3	1598.32	1
123		5	max	0	1	.747	3	.388	1	1.862e-2	3	NC	5	NC	3
124			min	-.057	4	-.138	2	-.011	3	-4.591e-3	2	375.672	3	1163.495	1
125		6	max	0	1	.766	3	.421	1	2.035e-2	3	NC	4	NC	3
126			min	-.057	4	-.123	2	-.017	3	-5.249e-3	2	361.398	3	956.032	1
127		7	max	0	1	.743	3	.444	1	2.209e-2	3	NC	4	NC	5
128			min	-.057	4	-.084	2	-.023	3	-5.908e-3	2	379.224	3	854.145	1
129		8	max	0	1	.692	3	.455	1	2.382e-2	3	NC	4	NC	5
130			min	-.057	4	-.032	1	-.028	3	-6.566e-3	2	425.045	3	810.551	1
131		9	max	0	1	.636	3	.461	2	2.555e-2	3	NC	4	NC	5
132			min	-.057	4	-.001	5	-.032	3	-7.224e-3	2	489.076	3	771.818	2
133		10	max	0	1	.609	3	.466	2	2.728e-2	3	NC	4	NC	5
134			min	-.057	4	.001	15	-.034	3	-7.882e-3	2	528.315	3	757.236	2
135		11	max	0	3	.636	3	.461	2	2.555e-2	3	NC	4	NC	5
136			min	-.057	4	.002	15	-.032	3	-7.224e-3	2	489.076	3	771.818	2
137		12	max	0	3	.692	3	.455	1	2.382e-2	3	NC	4	NC	5
138			min	-.057	4	-.032	1	-.028	3	-6.566e-3	2	425.045	3	810.551	1
139		13	max	0	3	.743	3	.444	1	2.209e-2	3	NC	4	NC	5
140			min	-.057	4	-.084	2	-.023	3	-5.908e-3	2	379.224	3	854.145	1
141		14	max	0	3	.766	3	.421	1	2.035e-2	3	NC	4	NC	3
142			min	-.057	4	-.123	2	-.017	3	-5.249e-3	2	361.398	3	956.032	1
143		15	max	0	3	.747	3	.388	1	1.862e-2	3	NC	4	NC	3
144			min	-.057	4	-.138	2	-.011	3	-4.591e-3	2	375.672	3	1163.495	1
145		16	max	0	3	.68	3	.346	1	1.689e-2	3	NC	4	NC	3
146			min	-.057	4	-.124	2	-.007	3	-3.933e-3	2	436.682	3	1598.32	1
147		17	max	0	3	.569	3	.3	1	1.516e-2	3	NC	4	NC	3
148			min	-.057	4	-.08	2	-.003	3	-3.275e-3	2	599.075	3	2678.745	1
149		18	max	0	3	.424	3	.259	1	1.343e-2	3	NC	6	NC	3
150			min	-.057	4	-.015	2	-.002	3	-2.616e-3	2	1153.438	3	6868.768	1
151		19	max	0	3	.268	3	.233	1	1.17e-2	3	NC	1	NC	1
152			min	-.057	4	.015	15	-.003	3	-1.958e-3	2	4805.218	4	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
153	M11	1	max	.001	1	.007	2	.235	1	5.157e-3	1	NC	1	NC	1
154			min	-.13	4	-.048	3	-.006	5	-1.441e-4	5	NC	1	NC	1
155		2	max	.001	1	.046	3	.255	1	5.815e-3	1	NC	4	NC	2
156			min	-.131	4	-.073	2	-.007	3	-8.255e-5	5	1919.963	3	8563.729	4
157		3	max	.001	1	.129	3	.292	1	6.473e-3	1	NC	4	NC	3
158			min	-.131	4	-.141	2	-.011	3	-2.11e-5	15	1015.491	3	3113.862	1
159		4	max	0	1	.183	3	.337	1	7.156e-3	2	NC	5	NC	3
160			min	-.131	4	-.183	2	-.016	3	1.975e-5	15	779.005	3	1755.273	1
161		5	max	0	1	.196	3	.38	1	7.861e-3	2	NC	5	NC	3
162			min	-.131	4	-.195	2	-.02	3	5.103e-5	12	735.774	3	1234.638	1
163		6	max	0	1	.168	3	.416	1	8.567e-3	2	NC	5	NC	5
164			min	-.131	4	-.176	2	-.024	3	-5.472e-5	3	832.014	3	990.509	1
165		7	max	0	1	.105	3	.442	1	9.273e-3	2	NC	5	NC	5
166			min	-.131	4	-.132	2	-.028	3	-1.727e-4	3	1173.16	3	869.06	1
167		8	max	0	1	.024	3	.456	1	9.978e-3	2	NC	4	NC	5
168			min	-.131	4	-.075	2	-.032	3	-2.906e-4	3	2179.008	2	813.242	1
169		9	max	0	1	0	15	.465	2	1.068e-2	2	NC	3	NC	5
170			min	-.131	4	-.051	3	-.035	3	-4.086e-4	3	5917.9	2	764.572	2
171		10	max	0	1	.003	1	.47	2	1.139e-2	2	NC	1	NC	5
172			min	-.131	4	-.085	3	-.036	3	-5.265e-4	3	4885.079	3	748.629	2
173		11	max	0	3	0	15	.465	2	1.068e-2	2	NC	3	NC	15
174			min	-.131	4	-.051	3	-.035	3	-4.086e-4	3	5917.9	2	764.572	2
175		12	max	0	3	.024	3	.456	1	9.978e-3	2	NC	4	NC	12
176			min	-.131	4	-.075	2	-.032	3	-2.906e-4	3	2179.008	2	813.242	1
177		13	max	0	3	.105	3	.442	1	9.273e-3	2	NC	5	NC	12
178			min	-.131	4	-.132	2	-.028	3	-1.727e-4	3	1173.16	3	869.06	1
179		14	max	0	3	.168	3	.416	1	8.567e-3	2	NC	5	NC	5
180			min	-.131	4	-.176	2	-.024	3	-5.472e-5	3	832.014	3	990.509	1
181		15	max	0	3	.196	3	.38	1	7.861e-3	2	NC	5	NC	3
182			min	-.131	4	-.195	2	-.02	3	5.103e-5	12	735.774	3	1234.638	1
183		16	max	.001	3	.183	3	.337	1	7.156e-3	2	NC	5	NC	3
184			min	-.131	4	-.183	2	-.016	3	1.217e-4	12	779.005	3	1755.273	1
185		17	max	.001	3	.129	3	.292	1	6.473e-3	1	NC	5	NC	3
186			min	-.131	4	-.141	2	-.011	3	1.923e-4	12	1015.491	3	3113.862	1
187		18	max	.001	3	.046	3	.255	1	5.815e-3	1	NC	4	NC	2
188			min	-.131	4	-.073	2	-.007	3	2.629e-4	12	1919.963	3	9016.87	1
189		19	max	.002	3	.007	2	.235	1	5.157e-3	1	NC	1	NC	1
190			min	-.131	4	-.048	3	-.003	3	3.336e-4	12	NC	1	NC	1
191	M12	1	max	0	2	.004	5	.236	1	6.22e-3	1	NC	1	NC	1
192			min	-.187	4	-.11	1	-.006	5	-1.184e-3	3	NC	1	NC	1
193		2	max	0	2	.025	3	.253	1	6.88e-3	1	NC	4	NC	1
194			min	-.187	4	-.24	2	-.004	3	-1.384e-3	3	1345.713	2	8666.831	4
195		3	max	0	2	.076	3	.289	1	7.539e-3	1	NC	5	NC	3
196			min	-.187	4	-.356	2	-.006	3	-1.584e-3	3	721.031	2	3423.283	1
197		4	max	0	2	.106	3	.334	1	8.199e-3	1	NC	5	NC	3
198			min	-.187	4	-.437	2	-.01	3	-1.784e-3	3	545.606	2	1854.039	1
199		5	max	0	2	.111	3	.378	1	8.885e-3	2	NC	5	NC	3
200			min	-.187	4	-.472	2	-.015	3	-1.984e-3	3	492.763	2	1275.069	1
201		6	max	0	2	.094	3	.415	1	9.576e-3	2	NC	5	NC	3
202			min	-.187	4	-.462	2	-.021	3	-2.184e-3	3	507.063	2	1007.611	1
203		7	max	0	2	.058	3	.442	1	1.027e-2	2	NC	5	NC	5
204			min	-.187	4	-.413	2	-.027	3	-2.384e-3	3	586.923	2	874.235	1
205		8	max	0	2	.013	3	.458	1	1.096e-2	2	NC	5	NC	4
206			min	-.187	4	-.343	2	-.032	3	-2.584e-3	3	760.968	2	811.141	1
207		9	max	0	2	-.005	15	.47	2	1.165e-2	2	NC	3	NC	5
208			min	-.187	4	-.276	2	-.036	3	-2.784e-3	3	1063.911	2	757.339	2
209		10	max	0	1	-.006	15	.475	2	1.234e-2	2	NC	3	NC	5

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
210			min	-.187	4	-.244	2	-.038	3	-2.984e-3	3	1306.896	2	739.912	2
211		11	max	0	9	-.007	15	.47	2	1.165e-2	2	NC	3	NC	15
212			min	-.187	4	-.276	2	-.036	3	-2.784e-3	3	1063.911	2	757.339	2
213		12	max	0	9	.013	3	.458	1	1.096e-2	2	NC	5	NC	12
214			min	-.187	4	-.343	2	-.032	3	-2.584e-3	3	760.968	2	811.141	1
215		13	max	0	9	.058	3	.442	1	1.027e-2	2	NC	5	NC	12
216			min	-.187	4	-.413	2	-.027	3	-2.384e-3	3	586.923	2	874.235	1
217		14	max	0	9	.094	3	.415	1	9.576e-3	2	NC	5	NC	3
218			min	-.187	4	-.462	2	-.021	3	-2.184e-3	3	507.063	2	1007.611	1
219		15	max	0	9	.111	3	.378	1	8.885e-3	2	NC	5	NC	3
220			min	-.187	4	-.472	2	-.015	3	-1.984e-3	3	492.763	2	1275.069	1
221		16	max	0	9	.106	3	.334	1	8.199e-3	1	NC	5	NC	3
222			min	-.187	4	-.437	2	-.01	3	-1.784e-3	3	545.606	2	1854.039	1
223		17	max	0	9	.076	3	.289	1	7.539e-3	1	NC	5	NC	3
224			min	-.187	4	-.356	2	-.006	3	-1.584e-3	3	721.031	2	3423.283	1
225		18	max	0	9	.025	3	.253	1	6.88e-3	1	NC	5	NC	1
226			min	-.187	4	-.24	2	-.004	3	-1.384e-3	3	1345.713	2	NC	1
227		19	max	0	9	-.009	15	.236	1	6.22e-3	1	NC	1	NC	1
228			min	-.187	4	-.11	1	-.004	3	-1.184e-3	3	NC	1	NC	1
229	M13	1	max	0	3	.134	3	.239	1	1.495e-2	2	NC	1	NC	1
230			min	-.326	4	-.605	2	-.006	5	-5.757e-3	3	NC	1	NC	1
231		2	max	0	3	.225	3	.267	1	1.691e-2	2	NC	5	NC	3
232			min	-.326	4	-.824	2	-.006	3	-6.659e-3	3	821.768	2	6351.518	1
233		3	max	0	3	.306	3	.31	1	1.888e-2	2	NC	5	NC	3
234			min	-.326	4	-1.026	2	-.009	3	-7.56e-3	3	427.63	2	2533.838	1
235		4	max	0	3	.37	3	.356	1	2.084e-2	2	NC	5	NC	3
236			min	-.326	4	-1.19	2	-.013	3	-8.462e-3	3	307.67	2	1528.131	1
237		5	max	0	3	.41	3	.399	1	2.281e-2	2	NC	5	NC	3
238			min	-.326	4	-1.304	2	-.019	3	-9.363e-3	3	257.415	2	1118.87	1
239		6	max	0	3	.425	3	.434	1	2.477e-2	2	NC	15	NC	5
240			min	-.326	4	-1.365	2	-.024	3	-1.027e-2	3	236.869	2	922.32	1
241		7	max	0	3	.419	3	.457	1	2.673e-2	2	NC	15	NC	5
242			min	-.326	4	-1.377	2	-.03	3	-1.117e-2	3	233.215	2	825.343	1
243		8	max	0	3	.398	3	.468	1	2.87e-2	2	NC	15	NC	5
244			min	-.326	4	-1.353	2	-.035	3	-1.207e-2	3	240.555	2	783.615	1
245		9	max	0	3	.374	3	.476	2	3.066e-2	2	NC	15	NC	5
246			min	-.326	4	-1.316	2	-.039	3	-1.297e-2	3	253.155	2	743.471	2
247		10	max	0	1	.361	3	.481	2	3.263e-2	2	NC	15	NC	5
248			min	-.326	4	-1.295	2	-.041	3	-1.387e-2	3	260.744	2	729.728	2
249		11	max	0	1	.374	3	.476	2	3.066e-2	2	NC	15	NC	5
250			min	-.326	4	-1.316	2	-.039	3	-1.297e-2	3	253.155	2	743.471	2
251		12	max	0	1	.398	3	.468	1	2.87e-2	2	NC	15	NC	12
252			min	-.326	4	-1.353	2	-.035	3	-1.207e-2	3	240.555	2	783.615	1
253		13	max	0	1	.419	3	.457	1	2.673e-2	2	NC	15	NC	5
254			min	-.326	4	-1.377	2	-.03	3	-1.117e-2	3	233.215	2	825.343	1
255		14	max	0	1	.425	3	.434	1	2.477e-2	2	NC	15	NC	5
256			min	-.326	4	-1.365	2	-.024	3	-1.027e-2	3	236.869	2	922.32	1
257		15	max	0	1	.41	3	.399	1	2.281e-2	2	NC	15	NC	3
258			min	-.326	4	-1.304	2	-.019	3	-9.363e-3	3	257.415	2	1118.87	1
259		16	max	0	1	.37	3	.356	1	2.084e-2	2	NC	5	NC	3
260			min	-.326	4	-1.19	2	-.013	3	-8.462e-3	3	307.67	2	1528.131	1
261		17	max	0	1	.306	3	.31	1	1.888e-2	2	NC	5	NC	3
262			min	-.326	4	-1.026	2	-.009	3	-7.56e-3	3	427.63	2	2533.838	1
263		18	max	0	1	.225	3	.267	1	1.691e-2	2	NC	5	NC	3
264			min	-.326	4	-.824	2	-.006	3	-6.659e-3	3	821.768	2	6351.518	1
265		19	max	0	1	.134	3	.239	1	1.495e-2	2	NC	1	NC	1
266			min	-.326	4	-.605	2	-.005	3	-5.757e-3	3	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	5	1.222e-3	2	NC	1	NC	1
270			min	0	2	0	1	0	1	-1.146e-3	5	NC	1	NC	1
271		3	max	0	3	0	12	.002	5	2.444e-3	2	NC	1	NC	1
272			min	0	2	-.004	1	0	1	-2.292e-3	5	NC	1	NC	1
273		4	max	0	3	0	12	.004	5	3.666e-3	2	NC	3	NC	1
274			min	0	2	-.008	1	0	1	-3.438e-3	5	6359.871	1	NC	1
275		5	max	0	3	0	12	.006	5	4.661e-3	2	NC	3	NC	1
276			min	0	2	-.015	1	0	1	-4.406e-3	5	3560.193	1	8846.13	5
277		6	max	0	3	0	12	.009	5	4.266e-3	2	NC	3	NC	1
278			min	0	2	-.024	1	-.001	1	-4.286e-3	5	2258.397	1	5827.179	5
279		7	max	0	3	0	12	.013	5	3.871e-3	2	NC	3	NC	1
280			min	0	2	-.034	1	-.002	1	-4.166e-3	5	1568.899	1	4160.735	5
281		8	max	0	3	0	12	.017	5	3.476e-3	2	NC	3	NC	1
282			min	0	2	-.046	1	-.002	1	-4.047e-3	5	1159.969	1	3142.149	5
283		9	max	0	3	0	12	.022	5	3.081e-3	2	NC	3	NC	1
284			min	0	2	-.06	1	-.003	1	-3.927e-3	5	897.161	1	2472.453	5
285		10	max	0	3	0	12	.027	5	2.686e-3	2	NC	3	NC	1
286			min	0	2	-.075	1	-.003	1	-3.807e-3	5	718.264	1	2008.314	5
287		11	max	0	3	0	3	.032	5	2.291e-3	2	NC	3	NC	1
288			min	0	2	-.091	1	-.003	1	-3.687e-3	5	590.845	1	1672.949	5
289		12	max	0	3	0	3	.038	5	1.896e-3	2	NC	3	NC	1
290			min	0	2	-.108	1	-.003	1	-3.567e-3	5	496.786	1	1422.484	5
291		13	max	0	3	0	3	.044	5	1.501e-3	2	NC	3	NC	1
292			min	-.001	2	-.126	1	-.003	1	-3.447e-3	5	425.361	1	1230.448	5
293		14	max	.001	3	0	3	.05	5	1.106e-3	2	NC	3	NC	1
294			min	-.001	2	-.145	1	-.003	1	-3.328e-3	5	369.813	1	1079.919	5
295		15	max	.001	3	0	3	.056	5	7.107e-4	2	NC	3	NC	1
296			min	-.001	2	-.165	1	-.003	1	-3.208e-3	5	325.755	1	959.758	5
297		16	max	.001	3	.001	3	.062	4	3.157e-4	2	NC	3	NC	1
298			min	-.001	2	-.185	1	-.002	1	-3.123e-3	4	290.23	1	861.733	4
299		17	max	.001	3	.002	3	.069	4	3.558e-4	3	NC	3	NC	1
300			min	-.001	2	-.205	1	-.003	3	-3.044e-3	4	261.173	1	780.314	4
301		18	max	.001	3	.002	3	.075	4	5.581e-4	3	NC	3	NC	1
302			min	-.001	2	-.226	1	-.006	3	-2.965e-3	4	237.122	1	712.651	4
303		19	max	.001	3	.002	3	.082	4	7.603e-4	3	NC	3	NC	1
304			min	-.001	2	-.247	1	-.008	3	-2.886e-3	4	217.009	1	655.885	4
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	4	0	1	NC	1	NC	1
308			min	0	2	-.002	1	0	1	-1.197e-3	4	NC	1	NC	1
309		3	max	0	3	0	15	.002	4	0	1	NC	3	NC	1
310			min	0	2	-.007	1	0	1	-2.394e-3	4	8056.862	1	NC	1
311		4	max	0	3	0	15	.004	4	0	1	NC	3	NC	1
312			min	0	2	-.015	1	0	1	-3.59e-3	4	3487.766	1	NC	1
313		5	max	.001	3	0	12	.006	4	0	1	NC	3	NC	1
314			min	-.001	2	-.028	1	0	1	-4.6e-3	4	1920.839	1	8485.655	4
315		6	max	.001	3	0	12	.01	4	0	1	NC	3	NC	1
316			min	-.001	2	-.045	1	0	1	-4.467e-3	4	1200.008	1	5592.927	4
317		7	max	.001	3	0	3	.013	4	0	1	NC	3	NC	1
318			min	-.002	2	-.065	1	0	1	-4.333e-3	4	825.249	1	3995.715	4
319		8	max	.002	3	.002	3	.018	4	0	1	NC	3	NC	1
320			min	-.002	2	-.089	2	0	1	-4.199e-3	4	605.198	2	3019.398	4
321		9	max	.002	3	.004	3	.023	4	0	1	NC	3	NC	1
322			min	-.002	2	-.116	2	0	1	-4.066e-3	4	463.728	2	2377.529	4
323		10	max	.002	3	.006	3	.028	4	0	1	NC	12	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
324			min	-.002	2	-.145	2	0	1	-3.932e-3	4	368.62	2	1932.72	4
325		11	max	.002	3	.009	3	.033	4	0	1	NC	12	NC	1
326			min	-.002	2	-.178	2	0	1	-3.798e-3	4	301.533	2	1611.372	4
327		12	max	.003	3	.011	3	.039	4	0	1	NC	15	NC	1
328			min	-.003	2	-.212	2	0	1	-3.664e-3	4	252.393	2	1371.43	4
329		13	max	.003	3	.014	3	.045	4	0	1	8939.168	15	NC	1
330			min	-.003	2	-.249	2	0	1	-3.531e-3	4	215.314	2	1187.516	4
331		14	max	.003	3	.017	3	.051	4	0	1	7769.011	15	NC	1
332			min	-.003	2	-.287	2	0	1	-3.397e-3	4	186.63	2	1043.414	4
333		15	max	.003	3	.021	3	.058	4	0	1	6841.388	15	NC	1
334			min	-.003	2	-.327	2	0	1	-3.263e-3	4	163.98	2	928.448	4
335		16	max	.003	3	.024	3	.064	4	0	1	6093.753	15	NC	1
336			min	-.003	2	-.368	2	0	1	-3.13e-3	4	145.787	2	835.334	4
337		17	max	.004	3	.028	3	.071	4	0	1	5482.496	15	NC	1
338			min	-.004	2	-.409	2	0	1	-2.996e-3	4	130.956	2	758.955	4
339		18	max	.004	3	.031	3	.077	4	0	1	4976.722	15	NC	1
340			min	-.004	2	-.452	2	0	1	-2.862e-3	4	118.717	2	695.644	4
341		19	max	.004	3	.035	3	.083	4	0	1	4553.885	15	NC	1
342			min	-.004	2	-.494	2	0	1	-2.728e-3	4	108.508	2	642.705	4
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	5	0	4	5.44e-4	3	NC	1	NC	1
346			min	0	2	0	1	0	3	-1.325e-3	4	NC	1	NC	1
347		3	max	0	3	0	5	.002	4	1.088e-3	3	NC	1	NC	1
348			min	0	2	-.004	1	0	3	-2.65e-3	4	NC	1	NC	1
349		4	max	0	3	0	5	.004	4	1.632e-3	3	NC	3	NC	1
350			min	0	2	-.008	1	0	3	-3.976e-3	4	6359.871	1	NC	1
351		5	max	0	3	0	5	.006	4	2.071e-3	3	NC	3	NC	1
352			min	0	2	-.015	1	-.001	3	-5.089e-3	4	3560.193	1	8506.574	4
353		6	max	0	3	0	5	.01	4	1.869e-3	3	NC	3	NC	1
354			min	0	2	-.024	1	-.001	3	-4.905e-3	4	2258.397	1	5614.798	4
355		7	max	0	3	.001	5	.013	4	1.667e-3	3	NC	3	NC	1
356			min	0	2	-.034	1	-.002	3	-4.721e-3	4	1568.899	1	4016.042	4
357		8	max	0	3	.001	5	.018	4	1.464e-3	3	NC	3	NC	1
358			min	0	2	-.046	1	-.002	3	-4.537e-3	4	1159.969	1	3038.004	4
359		9	max	0	3	.002	5	.022	4	1.262e-3	3	NC	3	NC	1
360			min	0	2	-.06	1	-.002	3	-4.354e-3	4	897.161	1	2394.674	4
361		10	max	0	3	.002	5	.028	4	1.06e-3	3	NC	3	NC	1
362			min	0	2	-.075	1	-.003	3	-4.17e-3	4	718.264	1	1948.698	4
363		11	max	0	3	.002	5	.033	4	8.576e-4	3	NC	3	NC	1
364			min	0	2	-.091	1	-.003	3	-3.986e-3	4	590.845	1	1626.441	4
365		12	max	0	3	.003	5	.039	4	6.553e-4	3	NC	3	NC	1
366			min	0	2	-.108	1	-.002	3	-3.802e-3	4	496.786	1	1385.805	4
367		13	max	0	3	.003	5	.045	4	4.531e-4	3	NC	3	NC	1
368			min	-.001	2	-.126	1	-.002	3	-3.619e-3	4	425.361	1	1201.369	4
369		14	max	.001	3	.004	5	.051	4	2.509e-4	3	NC	3	NC	1
370			min	-.001	2	-.145	1	-.001	3	-3.435e-3	4	369.813	1	1056.889	4
371		15	max	.001	3	.004	5	.057	4	4.862e-5	3	NC	3	NC	1
372			min	-.001	2	-.165	1	0	12	-3.251e-3	4	325.755	1	941.665	4
373		16	max	.001	3	.005	5	.063	4	6.929e-5	9	NC	3	NC	1
374			min	-.001	2	-.185	1	0	10	-3.076e-3	5	290.23	1	848.398	4
375		17	max	.001	3	.005	5	.069	4	2.843e-4	1	NC	3	NC	1
376			min	-.001	2	-.205	1	0	10	-2.934e-3	5	261.173	1	771.962	4
377		18	max	.001	3	.006	5	.076	4	6.407e-4	1	NC	3	NC	1
378			min	-.001	2	-.226	1	-.001	2	-2.792e-3	5	237.122	1	708.678	4
379		19	max	.001	3	.006	5	.082	4	9.972e-4	1	NC	3	NC	1
380			min	-.001	2	-.247	1	-.003	2	-2.65e-3	5	217.009	1	655.848	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
381	M3	1	max	.013	1	0	3	.006	5	1.413e-3	2	NC	1	NC	1
382			min	0	12	-.005	1	0	1	-5.55e-4	3	NC	1	NC	1
383		2	max	.013	1	0	3	.021	5	1.959e-3	2	NC	1	NC	4
384			min	0	12	-.026	1	-.017	2	-8.112e-4	3	NC	1	3902.288	2
385		3	max	.012	1	0	3	.037	5	2.505e-3	2	NC	1	NC	4
386			min	0	12	-.048	1	-.032	2	-1.067e-3	3	NC	1	1979.354	2
387		4	max	.011	1	.001	3	.053	5	3.051e-3	2	NC	1	NC	4
388			min	.001	15	-.069	1	-.046	2	-1.323e-3	3	NC	1	1346.651	2
389		5	max	.011	1	.002	3	.069	5	3.597e-3	2	NC	1	NC	4
390			min	.001	15	-.09	1	-.06	2	-1.58e-3	3	NC	1	1037.259	2
391		6	max	.01	1	.002	3	.085	5	4.143e-3	2	NC	1	NC	4
392			min	.001	15	-.111	1	-.072	2	-1.836e-3	3	NC	1	858.058	2
393		7	max	.009	1	.003	3	.1	5	4.689e-3	2	NC	1	NC	4
394			min	.001	15	-.133	1	-.083	2	-2.092e-3	3	NC	1	744.975	2
395		8	max	.009	1	.003	3	.115	5	5.235e-3	2	NC	1	NC	4
396			min	0	15	-.154	1	-.092	2	-2.348e-3	3	NC	1	670.91	2
397		9	max	.008	1	.004	3	.13	5	5.781e-3	2	NC	1	NC	4
398			min	0	15	-.175	1	-.099	2	-2.604e-3	3	NC	1	622.784	2
399		10	max	.008	1	.005	3	.145	5	6.327e-3	2	NC	1	NC	4
400			min	0	15	-.195	1	-.103	2	-2.86e-3	3	NC	1	593.97	2
401		11	max	.007	1	.006	3	.16	5	6.872e-3	2	NC	1	NC	4
402			min	0	15	-.216	1	-.105	2	-3.117e-3	3	NC	1	581.425	2
403		12	max	.006	1	.007	3	.174	5	7.418e-3	2	NC	1	NC	4
404			min	0	15	-.237	1	-.104	2	-3.373e-3	3	9320.926	3	584.664	2
405		13	max	.006	1	.008	3	.187	5	7.964e-3	2	NC	1	NC	4
406			min	0	15	-.257	1	-.099	2	-3.629e-3	3	8078.857	3	605.797	2
407		14	max	.005	1	.009	3	.201	5	8.51e-3	2	NC	1	NC	4
408			min	0	15	-.278	1	-.092	2	-3.885e-3	3	7072.245	3	650.774	2
409		15	max	.005	3	.01	3	.214	5	9.056e-3	2	NC	1	NC	4
410			min	0	10	-.298	1	-.08	2	-4.141e-3	3	6248.836	3	711.619	14
411		16	max	.005	3	.011	3	.226	5	9.602e-3	2	NC	1	NC	4
412			min	0	10	-.318	1	-.065	2	-4.398e-3	3	5569.942	3	639.688	14
413		17	max	.005	3	.013	3	.238	5	1.015e-2	2	NC	1	NC	4
414			min	0	10	-.338	1	-.045	2	-4.654e-3	3	5006.469	3	577.019	14
415		18	max	.006	3	.014	3	.25	5	1.069e-2	2	NC	1	NC	4
416			min	0	10	-.359	1	-.021	2	-4.91e-3	3	4536.259	3	522.072	14
417		19	max	.006	3	.015	3	.263	4	1.124e-2	2	NC	1	NC	1
418			min	0	10	-.379	1	-.002	3	-5.166e-3	3	4142.268	3	473.637	14
419	M6	1	max	.024	1	0	3	.006	4	0	1	NC	1	NC	1
420			min	0	15	-.009	1	0	1	-5.753e-4	4	NC	1	NC	1
421		2	max	.023	1	.005	3	.022	4	0	1	NC	1	NC	1
422			min	0	15	-.053	2	0	1	-6.509e-4	4	NC	1	NC	1
423		3	max	.021	1	.009	3	.039	4	0	1	NC	1	NC	1
424			min	0	15	-.096	2	0	1	-7.266e-4	4	7306.038	3	NC	1
425		4	max	.019	1	.014	3	.055	4	0	1	NC	1	NC	1
426			min	0	15	-.14	2	0	1	-8.023e-4	4	4855.803	3	9711.308	4
427		5	max	.018	1	.018	3	.072	4	0	1	NC	1	NC	1
428			min	0	15	-.184	2	0	1	-8.779e-4	4	3627.046	3	7391.805	4
429		6	max	.016	1	.023	3	.088	4	0	1	NC	1	NC	1
430			min	0	15	-.227	2	0	1	-9.536e-4	4	2887.277	3	6056.596	4
431		7	max	.014	1	.027	3	.104	4	0	1	NC	1	NC	1
432			min	0	15	-.271	2	0	1	-1.029e-3	4	2392.335	3	5218.833	4
433		8	max	.013	1	.032	3	.12	4	0	1	NC	1	NC	1
434			min	0	15	-.314	2	0	1	-1.105e-3	4	2037.573	3	4672.796	4
435		9	max	.011	1	.036	3	.135	4	0	1	NC	1	NC	1
436			min	0	15	-.357	2	0	1	-1.181e-3	4	1770.664	3	4319.162	4
437		10	max	.01	1	.041	3	.15	4	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
438			min	0	15	-.4	2	0	1	-1.256e-3	4	1562.528	3	4107.424	4
439		11	max	.01	3	.046	3	.165	4	0	1	NC	1	NC	1
440			min	0	15	-.443	2	0	1	-1.332e-3	4	1395.71	3	4013.953	4
441		12	max	.011	3	.051	3	.179	4	0	1	NC	1	NC	1
442			min	0	10	-.486	2	0	1	-1.408e-3	4	1259.093	3	4033.991	4
443		13	max	.012	3	.056	3	.193	4	0	1	NC	1	NC	1
444			min	0	10	-.529	2	0	1	-1.483e-3	4	1145.258	3	4181.544	4
445		14	max	.013	3	.061	3	.206	4	0	1	NC	1	NC	1
446			min	-.002	10	-.571	2	0	1	-1.559e-3	4	1049.062	3	4497.936	4
447		15	max	.014	3	.066	3	.219	4	0	1	NC	1	NC	1
448			min	-.004	2	-.614	2	0	1	-1.635e-3	4	966.825	3	5078.693	4
449		16	max	.015	3	.071	3	.231	4	0	1	NC	1	NC	1
450			min	-.006	2	-.657	2	0	1	-1.71e-3	4	895.842	3	6158.081	4
451		17	max	.016	3	.076	3	.243	4	0	1	NC	1	NC	1
452			min	-.008	2	-.699	2	0	1	-1.786e-3	4	834.082	3	8450.547	4
453		18	max	.017	3	.082	3	.253	4	0	1	NC	1	NC	1
454			min	-.01	2	-.741	2	0	1	-1.862e-3	4	779.985	3	NC	1
455		19	max	.018	3	.087	3	.264	4	0	1	NC	1	NC	1
456			min	-.012	2	-.784	2	0	1	-1.937e-3	4	732.336	3	NC	1
457	M9	1	max	.013	1	0	5	.006	4	5.55e-4	3	NC	1	NC	1
458			min	0	5	-.005	1	-.001	3	-1.413e-3	2	NC	1	NC	1
459		2	max	.013	1	0	3	.024	4	8.112e-4	3	NC	1	NC	4
460			min	0	5	-.026	1	-.008	3	-1.959e-3	2	NC	1	3902.288	2
461		3	max	.012	1	0	3	.042	4	1.067e-3	3	NC	1	NC	5
462			min	0	5	-.048	1	-.015	3	-2.505e-3	2	NC	1	1979.354	2
463		4	max	.011	1	.001	3	.06	4	1.323e-3	3	NC	1	NC	15
464			min	0	5	-.069	1	-.022	3	-3.051e-3	2	NC	1	1346.651	2
465		5	max	.011	1	.002	3	.078	4	1.58e-3	3	NC	1	9693.138	15
466			min	0	5	-.09	1	-.028	3	-3.597e-3	2	NC	1	1037.259	2
467		6	max	.01	1	.002	3	.095	4	1.836e-3	3	NC	1	7944.115	15
468			min	0	5	-.111	1	-.033	3	-4.143e-3	2	NC	1	858.058	2
469		7	max	.009	1	.003	3	.112	4	2.092e-3	3	NC	1	6845.782	15
470			min	0	5	-.133	1	-.038	3	-4.689e-3	2	NC	1	744.975	2
471		8	max	.009	1	.003	3	.129	4	2.348e-3	3	NC	1	6129.122	15
472			min	0	5	-.154	1	-.042	3	-5.235e-3	2	NC	1	670.91	2
473		9	max	.008	1	.004	3	.145	4	2.604e-3	3	NC	1	5664.206	15
474			min	0	5	-.175	1	-.045	3	-5.781e-3	2	NC	1	622.784	2
475		10	max	.008	1	.005	3	.161	4	2.86e-3	3	NC	1	5384.923	15
476			min	0	5	-.195	1	-.047	3	-6.327e-3	2	NC	1	593.97	2
477		11	max	.007	1	.006	3	.175	4	3.117e-3	3	NC	1	5260.29	15
478			min	0	5	-.216	1	-.048	3	-6.872e-3	2	NC	1	581.425	2
479		12	max	.006	1	.007	3	.189	4	3.373e-3	3	NC	1	5283.975	15
480			min	0	5	-.237	1	-.048	3	-7.418e-3	2	9320.926	3	584.664	2
481		13	max	.006	1	.008	3	.202	4	3.629e-3	3	NC	1	5474.129	15
482			min	0	5	-.257	1	-.046	3	-7.964e-3	2	8078.857	3	605.797	2
483		14	max	.005	1	.009	3	.214	4	3.885e-3	3	NC	1	5884.518	15
484			min	0	5	-.278	1	-.042	3	-8.51e-3	2	7072.245	3	650.774	2
485		15	max	.005	3	.01	3	.226	4	4.141e-3	3	NC	1	6639.535	15
486			min	0	5	-.298	1	-.037	3	-9.056e-3	2	6248.836	3	733.221	2
487		16	max	.005	3	.011	3	.236	4	4.398e-3	3	NC	1	8044.326	15
488			min	0	5	-.318	1	-.031	3	-9.602e-3	2	5569.942	3	886.47	2
489		17	max	.005	3	.013	3	.245	4	4.654e-3	3	NC	1	NC	15
490			min	0	5	-.338	1	-.022	3	-1.015e-2	2	5006.469	3	1212.081	2
491		18	max	.006	3	.014	3	.253	4	4.91e-3	3	NC	1	NC	5
492			min	0	5	-.359	1	-.011	3	-1.069e-2	2	4536.259	3	2220.094	2
493		19	max	.006	3	.015	3	.26	5	5.166e-3	3	NC	1	NC	1
494			min	0	10	-.379	1	-.01	1	-1.124e-2	2	4142.268	3	NC	1