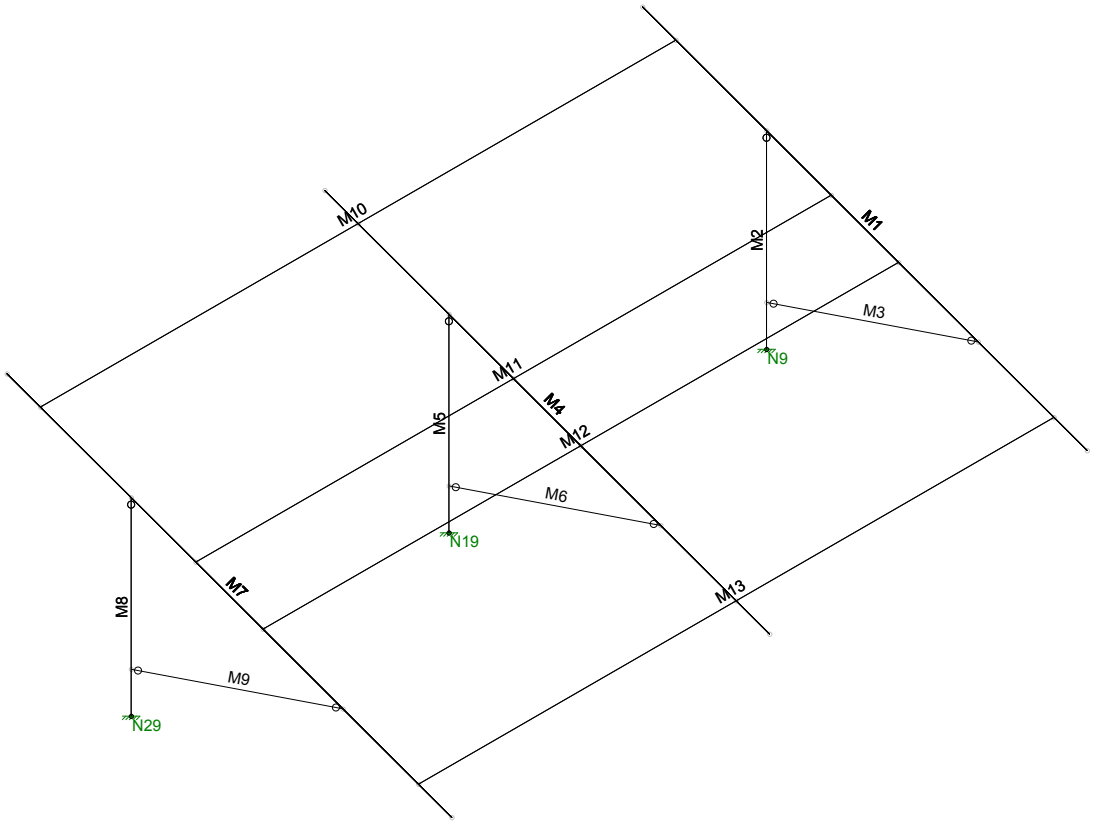


Schletter, Inc.		20° Tilt w/o Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

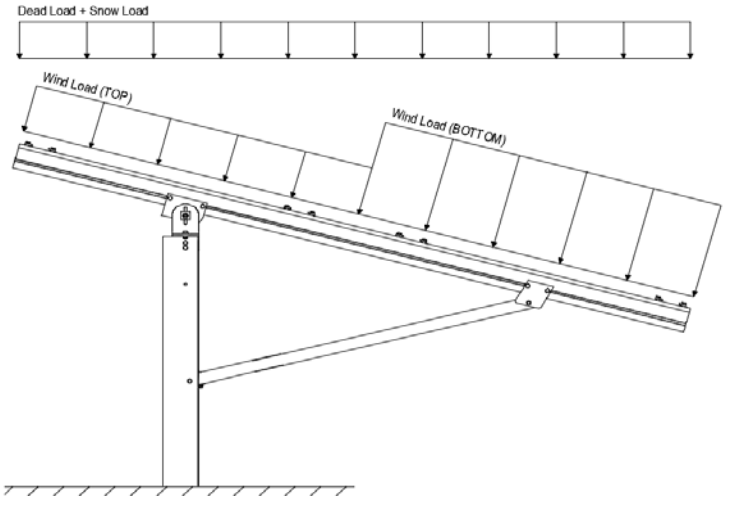
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row =	2
Module Tilt =	20°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	20.62	psf	*(ASCE 7-10, Eq. 7.4-1)*
I_s =	1.00		
C_s =	0.91		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	130	mph	Exposure Category = C
Height <	15	ft	Importance Category = II

Peak Velocity Pressure, q_z =	26.53	psf	*Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.05	*(Pressure)*	*Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.*
$Cf+_{BOTTOM}$ =	1.65		
$Cf-_{TOP}$ =	-2.12	*(Suction)*	
$Cf-_{BOTTOM}$ =	-1		

2.4 Seismic Loads - N/A

S_S =	0.00	R =	1.25
S_{DS} =	0.00	C_S =	0
S_1 =	0.00	ρ =	1.3
S_{D1} =	0.00	Ω =	1.25
T_a =	0.00	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W	
1.2D + 1.0W + 0.5S	
0.9D + 1.0W [M]	
1.54D + 1.3E + 0.2S [R]	*(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)*
0.56D + 1.3E [R]	
1.54D + 1.25E + 0.2S [O]	
0.56D + 1.25E [O]	

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S	
1.0D + 0.6W	
1.0D + 0.75L + 0.45W + 0.75S	
0.6D + 0.6W [M]	*(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)*
1.238D + 0.875E [O]	
1.1785D + 0.65625E + 0.75S [O]	
0.362D + 0.875E [O]	

[M] *Uses the minimum allowable module dead load.*

[R] *Include redundancy factor of 1.3.*

[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

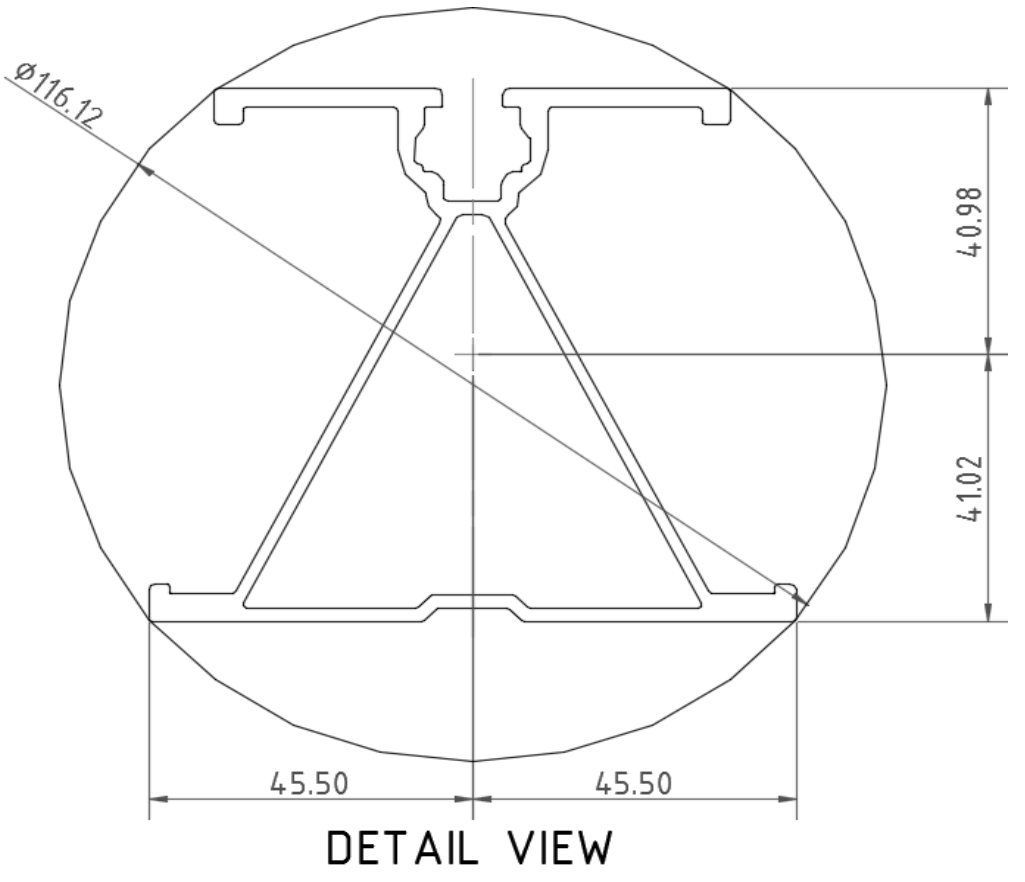
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

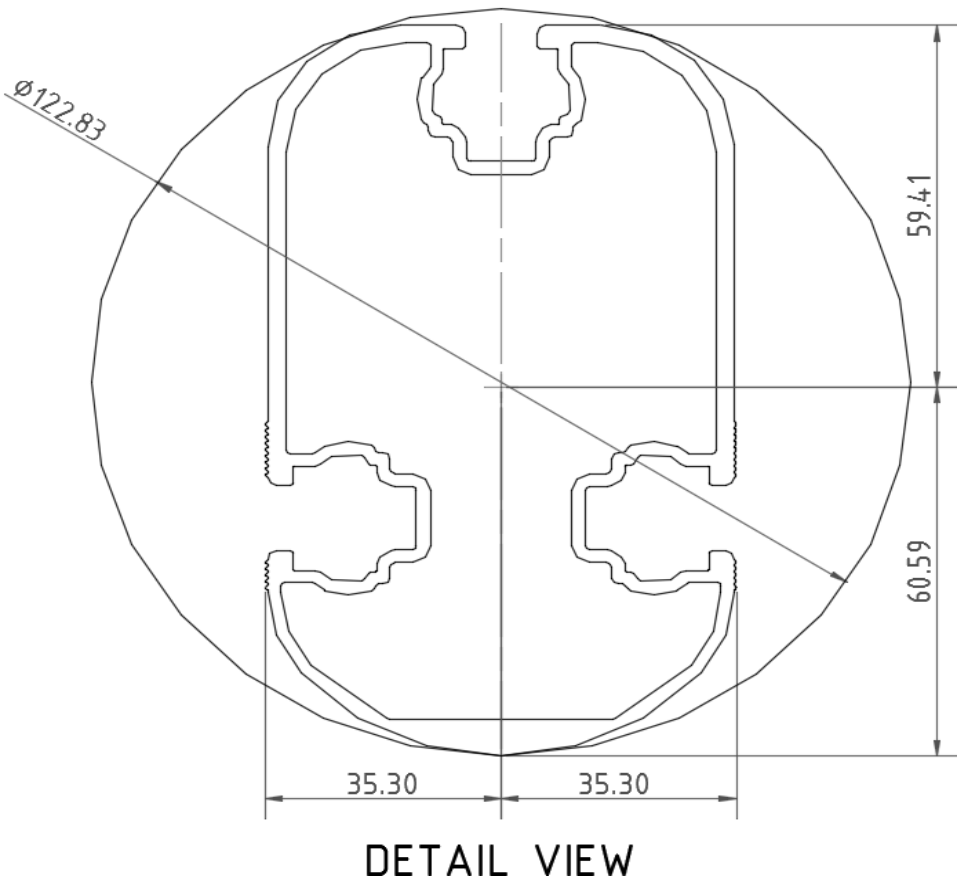
Purlin Type	=	**S1.5**	
Aluminum Type	=	6105-T5	
F_{ty}	=	35	ksi
L_b	=	132	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$	=	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$	=	23.08	ksi
S_y	=	1.33	in^3
S_x	=	0.6	in^3
E	=	10100	ksi
I_y	=	2.16	in^4
I_x	=	1.07	in^4
A	=	1.25	in^2
g	=	1.50	lbs/ft
M_y	=	2.132	k-ft
M_z	=	0.226	k-ft
$M_{y\ allowable}$	=	2.779	k-ft
$M_{z\ allowable}$	=	1.154	k-ft
Utilization	=	96%	



4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

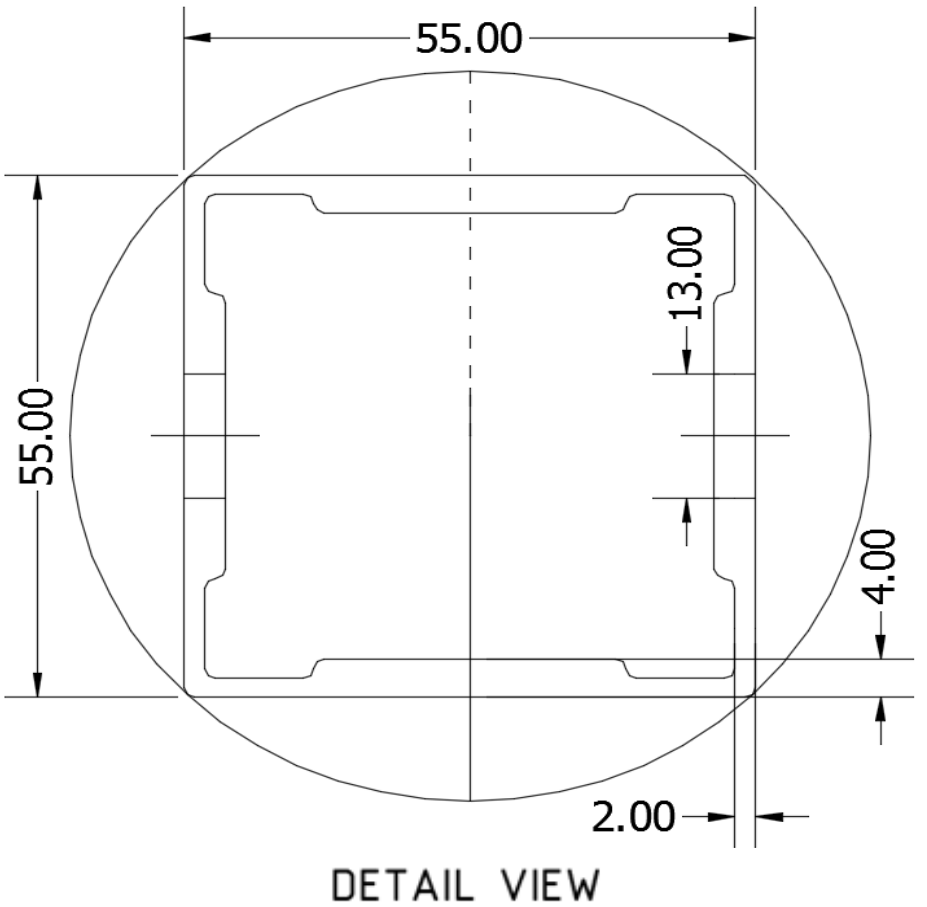
Girder Type	=	**T5**	
Aluminum Type	=	6105-T5	
F_{ty}	=	35	ksi
L_b	=	63.82	in
$\Phi F_{ty\ AXIAL}$	=	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$	=	30.46	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$	=	31.56	ksi
S_y	=	1.98	in^3
S_x	=	1.32	in^3
E	=	10100	ksi
I_y	=	4.74	in^4
I_x	=	1.83	in^4
A	=	1.93	in^2
g	=	2.32	lbs/ft
M_y	=	4.346	k-ft
M_z	=	0.000	k-ft
P_n	=	0.030	k
$M_{y\ allowable}$	=	5.026	k-ft
$M_{z\ allowable}$	=	3.472	k-ft
$P_{n\ allowable}$	=	59.439	k
Utilization	=	87%	



4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.00	in
$\Phi F_{ty\ AXIAL}$ =	13.67	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.005	k-ft
M_z =	0.000	k-ft
P_n =	6.250	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.425	k
Utilization =	47%	

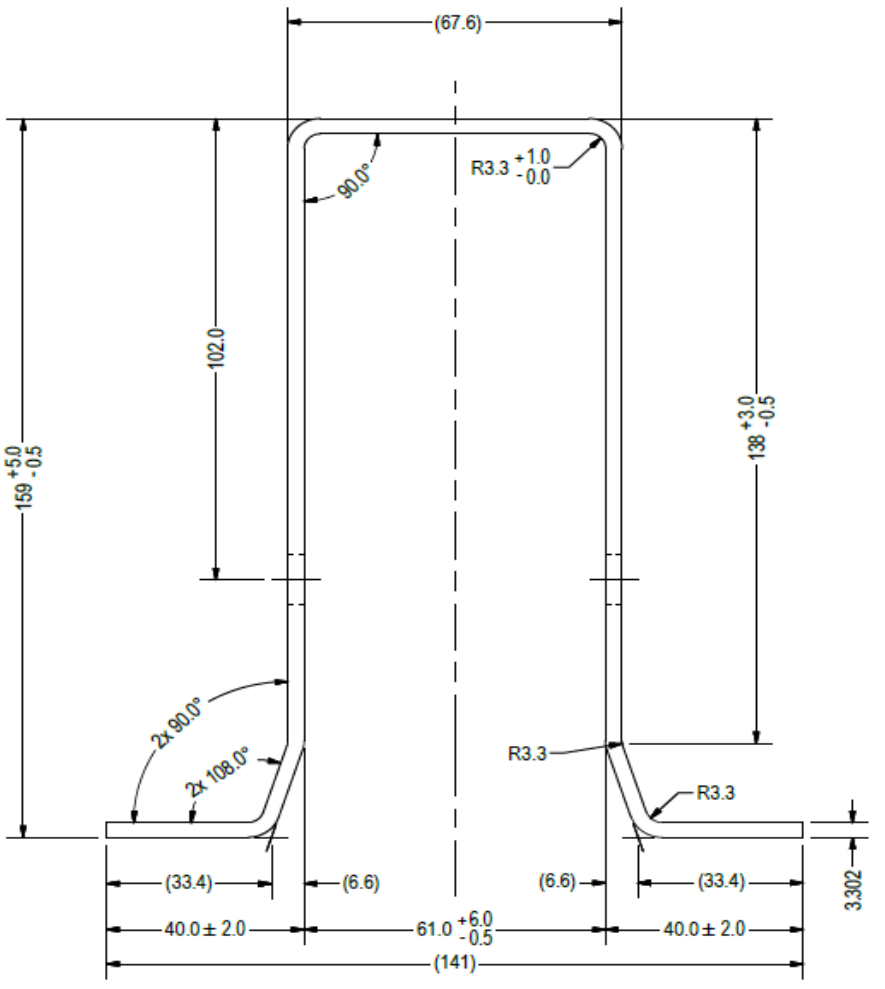


DETAIL VIEW

4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	65.62	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	15.386	k-ft
M_z =	0.000	k-ft
P_r =	7.502	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	46.025	k
Utilization =	98%	



DETAIL VIEW

5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	6.90	k
Maximum Lateral Load =	2.68	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

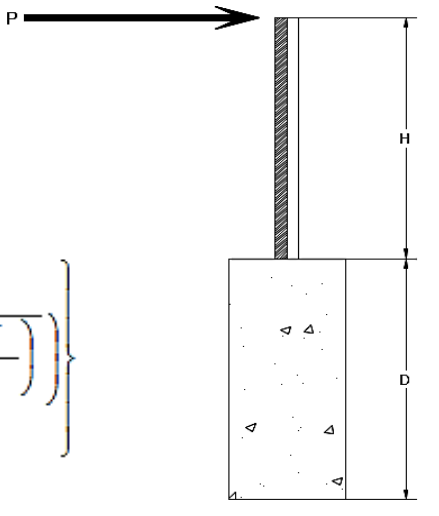
Lateral Force @ Top of Pole, P =	2.01	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1 + \sqrt{1 + \left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

Non-Constrained

Lateral Force @ Top of Pole, P =	2.01	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	10.84	
Required Footing Depth, D =	14.49	ft

2nd Trial @ D_2 =	8.87	ft
Lateral Soil Bearing @ D/3, S_1 =	0.59	ksf
Lateral Soil Bearing @ D, S_3 =	1.77	ksf
Constant 2.34P/(S_1B), A =	3.97	
Required Footing Depth, D =	6.81	ft

3rd Trial @ D_3 =	7.84	ft
Lateral Soil Bearing @ D/3, S_1 =	0.52	ksf
Lateral Soil Bearing @ D, S_3 =	1.57	ksf
Constant 2.34P/(S_1B), A =	4.49	
Required Footing Depth, D =	7.44	ft

4th Trial @ D_4 =	7.64	ft
Lateral Soil Bearing @ D/3, S_1 =	0.51	ksf
Lateral Soil Bearing @ D, S_3 =	1.53	ksf
Constant 2.34P/(S_1B), A =	4.61	
Required Footing Depth, D =	7.58	ft

5th Trial @ D_5 =	7.61	ft
Lateral Soil Bearing @ D/3, S_1 =	0.51	ksf
Lateral Soil Bearing @ D, S_3 =	1.52	ksf
Constant 2.34P/(S_1B), A =	4.63	
Required Footing Depth, D =	7.75	ft

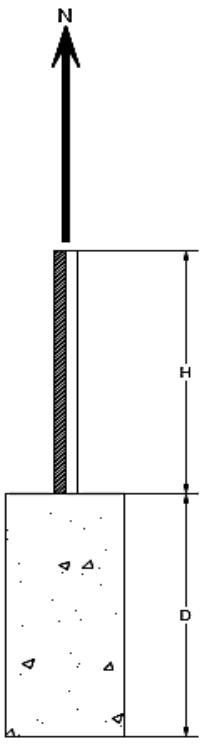
A 2ft diameter x 7.75ft deep footing unrestrained at ground level is required for the racking structure.

5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	3.16	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	2.07	k
Required Concrete Volume, V =	14.31	ft^3
Required Footing Depth, D =	4.75	ft

A 2ft diameter x 4.75ft deep footing unrestrained at ground level is required for the racking structure.



Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	6.84
2	0.4	0.2	118.10	6.73
3	0.6	0.2	118.10	6.63
4	0.8	0.2	118.10	6.52
5	1	0.2	118.10	6.42
6	1.2	0.2	118.10	6.32
7	1.4	0.2	118.10	6.21
8	1.6	0.2	118.10	6.11
9	1.8	0.2	118.10	6.01
10	2	0.2	118.10	5.90
11	2.2	0.2	118.10	5.80
12	2.4	0.2	118.10	5.69
13	2.6	0.2	118.10	5.59
14	2.8	0.2	118.10	5.49
15	3	0.2	118.10	5.38
16	3.2	0.2	118.10	5.28
17	3.4	0.2	118.10	5.18
18	3.6	0.2	118.10	5.07
19	3.8	0.2	118.10	4.97
20	4	0.2	118.10	4.86
21	4.2	0.2	118.10	4.76
22	4.4	0.2	118.10	4.66
23	4.6	0.2	118.10	4.55
24	0	0.0	0.00	4.55
25	0	0.0	0.00	4.55
26	0	0.0	0.00	4.55
27	0	0.0	0.00	4.55
28	0	0.0	0.00	4.55
29	0	0.0	0.00	4.55
30	0	0.0	0.00	4.55
31	0	0.0	0.00	4.55
32	0	0.0	0.00	4.55
33	0	0.0	0.00	4.55
34	0	0.0	0.00	4.55
Max	4.6	Sum	1.09	

5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	7.75	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	4.84	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	29.85	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

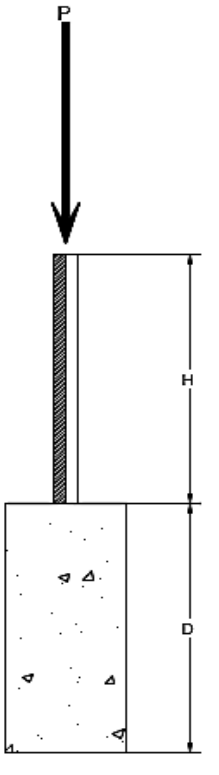
Weight of Concrete

Footing Volume	24.35	ft^3
Weight	3.53	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	4.48	k
1/3 Increase for Wind =	1.33	
Total Resistance =	12.25	k
Applied Force =	8.37	k
Utilization =	68%	

A 2ft diameter footing passes at a depth of 7.75ft.



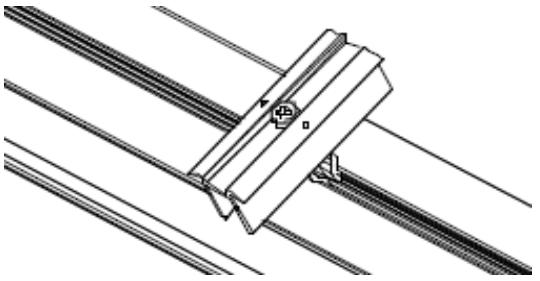
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

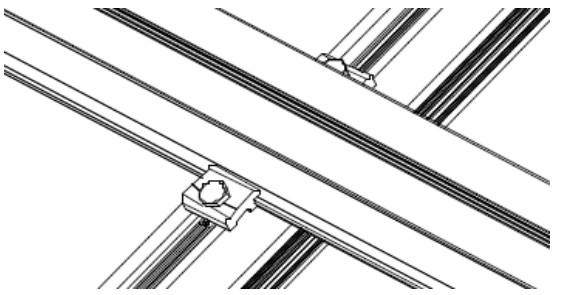
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.525 k
Allowable Uplift	=	1.214 k
Utilization	=	43%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	2.044 k
Allowable Uplift	=	2.180 k
Utilization	=	94%

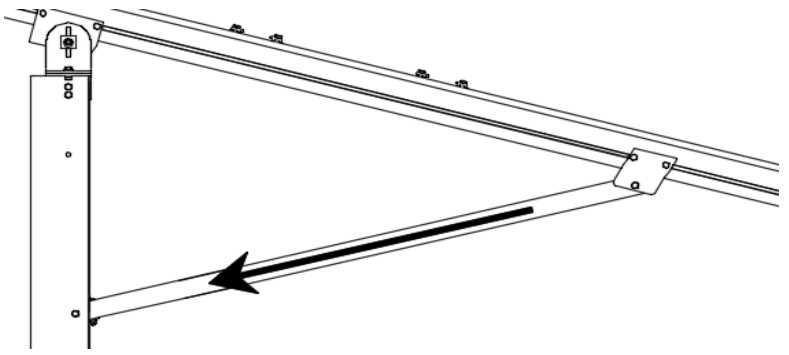


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load	=	6.250 k
M10 Bolt Shear Capacity	=	8.894 k
Utilization	=	70%

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

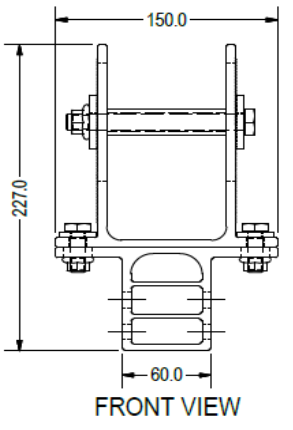


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

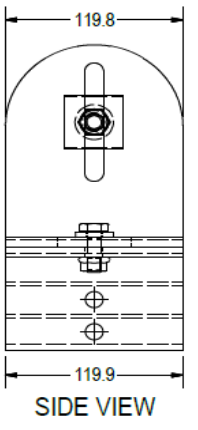
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

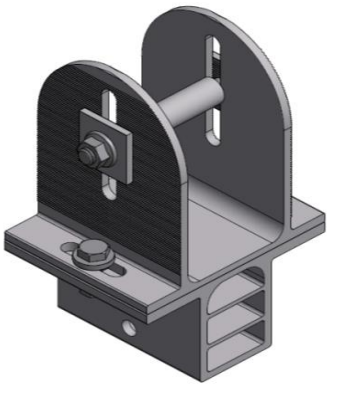
Maximum Tensile Load	=	4.361 k
Allowable Load	=	5.649 k
Utilization	=	77%



FRONT VIEW



SIDE VIEW



7. SEISMIC DESIGN

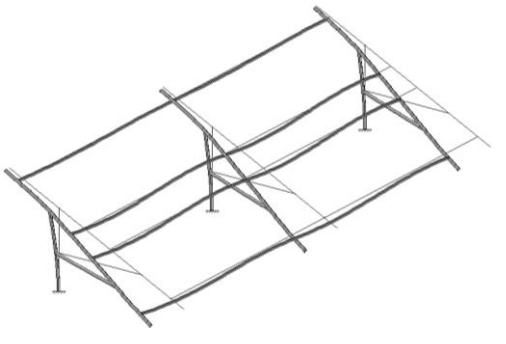
7.1 Seismic Drift - N/A

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	65.92 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.318 in
Max Drift, Δ_{MAX}	=	0 in

N/A

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 132 in

J = 0.432

365.174

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 27.1 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 132

J = 0.432

232.229

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.4

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 63.8189 in
J = 1.98
82.1278

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.5 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 63.8189
J = 1.98
89.1294

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.3

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = φb[Bt-Dt*√(Rb/t)]

φF_L = 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L St$ = 30.5 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 5.001 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L Wk$ = 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φc[Bt-Dt*√(Rb/t)]

φF_L = 30.80 ksi

φF_L = 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 61 in

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St$ = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 61

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk$ = 1.460 k-ft

Compression

3.4.7

λ = 1.41113

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

S1* = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

S2* = 1.23671

φcc = 0.77756

φF_L = (φccFcy)/(λ²)

φF_L = 13.6667 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 13.67 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 14.07 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	65.62	in	
Pr =	7.50	k	(LRFD Factored Load)
Mr (Strong) =	15.39	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	94.42		
4.71√(E/Fy) =	103.55	=> kL/r	≤ 4.71√(E/Fy)
Fcr =	27.44	ksi	
Fe =	32.10	ksi	
Pn =	61.196	k	

Torsional/Flexural Torsional Buckling:

Fcr =	20.6391	ksi
Fey =	81.8881	ksi
Fez =	26.2099	ksi
Pn =	46.0252	k

Bending (Strong Axis):

Yielding:

Mn =	21.95	k-ft		
Flange Local Buckling:				
Mn =	19.207	k-ft		
Pr/Pc =	0.1811	<	0.2	
Utilization =	0.98	<	1.0	OK

Bending (Weak Axis):

Yielding:

Mn =	14.65	k-ft		
Flange Local Buckling:				
Mn =	14.39	k-ft		
Pr/Pc =	0.181	<	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 98%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL								

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-8.366	-8.366	0	0
2	M11	Y	-8.366	-8.366	0	0
3	M12	Y	-8.366	-8.366	0	0
4	M13	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-4.45	-4.45	0	0
2	M11	Y	-4.45	-4.45	0	0
3	M12	Y	-4.45	-4.45	0	0
4	M13	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-54.031	-54.031	0	0
2	M11	Y	-54.031	-54.031	0	0
3	M12	Y	-54.031	-54.031	0	0
4	M13	Y	-54.031	-54.031	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-77.697	-77.697	0	0
2	M11	y	-77.697	-77.697	0	0
3	M12	y	-122.096	-122.096	0	0
4	M13	y	-122.096	-122.096	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	156.875	156.875	0	0
2	M11	y	156.875	156.875	0	0
3	M12	y	73.997	73.997	0	0
4	M13	y	73.997	73.997	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5																
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1																
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1														
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3														
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3														
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25														
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25														

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
8																										
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																		
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6																
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45																
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6														
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875														
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656														
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875														

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	497.201	2	2742.761	1	369.83	1	.39	1	.004	3	6.521	1
2		min	-709.316	3	-1794.884	3	-332.692	3	-.331	3	-.008	2	.204	15
3	N19	max	2012.26	2	7533.692	1	0	2	0	2	0	1	14.612	1
4		min	-2055.735	3	-5305.16	3	0	3	0	3	0	3	.405	15
5	N29	max	497.201	2	2742.761	1	332.692	3	.331	3	.008	2	6.521	1
6		min	-709.316	3	-1794.884	3	-369.83	1	-.39	1	-.004	3	.204	15
7	Totals:	max	3006.662	2	13019.215	1	0	2						
8		min	-3474.366	3	-8894.929	3	0	3						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.006	1	0	3	0	1	0	1	0	1
2			min	0	1	-.001	3	-.001	1	0	1	0	1	0	1
3		2	max	-.179	15	-.49	15	0	3	0	1	0	12	0	4
4			min	-.76	4	-2.085	4	-.001	1	0	1	0	1	0	15
5		3	max	-5.966	12	300.158	3	16.453	3	.081	3	.3	1	.316	2
6			min	-197.872	1	-720.89	2	-203.122	1	-.275	2	.008	12	-.13	3
7		4	max	-6.262	12	298.938	3	16.453	3	.081	3	.174	1	.764	2
8			min	-198.464	1	-722.516	2	-203.122	1	-.275	2	.006	15	-.316	3
9		5	max	-6.558	12	297.719	3	16.453	3	.081	3	.048	1	1.213	2
10			min	-199.056	1	-724.143	2	-203.122	1	-.275	2	-.014	10	-.501	3
11		6	max	592.174	3	641.149	2	48.269	3	.037	1	.154	1	1.161	2
12			min	-1849.949	1	-188.495	3	-274.024	1	-.058	3	-.059	3	-.508	3
13		7	max	591.73	3	639.523	2	48.269	3	.037	1	.02	2	.764	2
14			min	-1850.541	1	-189.715	3	-274.024	1	-.058	3	-.029	3	-.391	3
15		8	max	591.286	3	637.897	2	48.269	3	.037	1	.001	3	.379	1
16			min	-1851.133	1	-190.934	3	-274.024	1	-.058	3	-.187	1	-.272	3
17		9	max	583.375	3	84.195	3	51.596	3	-.004	15	.092	1	.166	1
18			min	-2056.808	1	-72.078	1	-274.997	1	-.266	2	0	10	-.218	3
19		10	max	582.931	3	82.976	3	51.596	3	-.004	15	.067	3	.211	1
20			min	-2057.4	1	-73.704	1	-274.997	1	-.266	2	-.079	1	-.27	3
21		11	max	582.487	3	81.756	3	51.596	3	-.004	15	.099	3	.257	1
22			min	-2057.992	1	-75.33	1	-274.997	1	-.266	2	-.25	1	-.321	3
23		12	max	571.312	3	782.361	3	168.37	2	.468	3	.157	1	.546	1
24			min	-2258.488	1	-663.195	1	-297.689	3	-.524	1	.005	15	-.65	3
25		13	max	570.868	3	781.141	3	168.37	2	.468	3	.236	1	.958	1
26			min	-2259.08	1	-664.821	1	-297.689	3	-.524	1	-.165	3	-1.135	3
27		14	max	200.07	1	596.842	1	3.586	3	.35	1	0	10	1.354	1
28			min	5.883	12	-696.192	3	-171.37	1	-.48	3	-.006	1	-1.599	3
29		15	max	199.478	1	595.216	1	3.586	3	.35	1	0	3	.984	1
30			min	5.587	12	-697.412	3	-171.37	1	-.48	3	-.112	1	-1.167	3
31		16	max	198.886	1	593.59	1	3.586	3	.35	1	.003	3	.615	1
32			min	5.291	12	-698.631	3	-171.37	1	-.48	3	-.218	1	-.734	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
33		17	max	198.295	1	591.964	1	3.586	3	.35	1	.005	3	.247	1
34			min	4.995	12	-699.851	3	-171.37	1	-.48	3	-.325	1	-.3	3
35		18	max	.76	4	2.087	4	0	1	0	1	0	15	0	4
36			min	.179	15	.491	15	0	5	0	1	0	1	0	15
37		19	max	0	1	0	1	0	1	0	1	0	1	0	1
38			min	0	1	-.003	3	0	5	0	1	0	1	0	1
39	M4	1	max	0	1	.016	1	0	1	0	1	0	1	0	1
40			min	0	1	-.004	3	0	1	0	1	0	1	0	1
41		2	max	-.179	15	-.49	15	0	1	0	1	0	1	0	4
42			min	-.76	4	-2.083	4	0	1	0	1	0	1	0	15
43		3	max	-13.443	15	909.115	3	0	1	0	1	0	1	.783	2
44			min	-347.413	1	-2050.991	2	0	1	0	1	0	1	-.348	3
45		4	max	-13.622	15	907.895	3	0	1	0	1	0	1	2.057	2
46			min	-348.005	1	-2052.617	2	0	1	0	1	0	1	-.912	3
47		5	max	-13.8	15	906.676	3	0	1	0	1	0	1	3.331	2
48			min	-348.597	1	-2054.243	2	0	1	0	1	0	1	-1.475	3
49		6	max	1950.168	3	1866.856	2	0	1	0	1	0	1	3.167	2
50			min	-5065.264	1	-675.293	3	0	1	0	1	0	1	-1.458	3
51		7	max	1949.724	3	1865.23	2	0	1	0	1	0	1	2.009	2
52			min	-5065.856	1	-676.513	3	0	1	0	1	0	1	-1.038	3
53		8	max	1949.28	3	1863.604	2	0	1	0	1	0	1	.855	1
54			min	-5066.448	1	-677.732	3	0	1	0	1	0	1	-.618	3
55		9	max	1923.449	3	276.703	3	0	1	0	1	0	1	.199	1
56			min	-5396.478	1	-283.402	1	0	1	0	1	0	1	-.407	3
57		10	max	1923.005	3	275.483	3	0	1	0	1	0	1	.375	1
58			min	-5397.07	1	-285.028	1	0	1	0	1	0	1	-.578	3
59		11	max	1922.562	3	274.264	3	0	1	0	1	0	1	.553	1
60			min	-5397.662	1	-286.655	1	0	1	0	1	0	1	-.749	3
61		12	max	1903.259	3	2195.072	3	0	1	0	1	0	1	1.404	1
62			min	-5738.052	1	-2032.498	1	0	1	0	1	0	1	-1.679	3
63		13	max	1902.816	3	2193.852	3	0	1	0	1	0	1	2.666	1
64			min	-5738.644	1	-2034.124	1	0	1	0	1	0	1	-3.041	3
65		14	max	348.343	1	1719.547	1	0	1	0	1	0	1	3.878	1
66			min	13.901	15	-1930.592	3	0	1	0	1	0	1	-4.346	3
67		15	max	347.751	1	1717.921	1	0	1	0	1	0	1	2.811	1
68			min	13.723	15	-1931.812	3	0	1	0	1	0	1	-3.147	3
69		16	max	347.159	1	1716.295	1	0	1	0	1	0	1	1.745	1
70			min	13.544	15	-1933.031	3	0	1	0	1	0	1	-1.948	3
71		17	max	346.568	1	1714.669	1	0	1	0	1	0	1	.681	1
72			min	13.366	15	-1934.251	3	0	1	0	1	0	1	-.748	3
73		18	max	.76	4	2.088	4	0	1	0	1	0	1	0	4
74			min	.179	15	.491	15	0	1	0	1	0	1	0	15
75		19	max	0	1	.004	1	0	1	0	1	0	1	0	1
76			min	0	1	-.008	3	0	1	0	1	0	1	0	1
77	M7	1	max	0	1	.006	1	.001	1	0	1	0	1	0	1
78			min	0	1	-.001	3	0	3	0	1	0	1	0	1
79		2	max	-.179	15	-.49	15	.001	1	0	1	0	1	0	4
80			min	-.76	4	-2.085	4	0	3	0	1	0	12	0	15
81		3	max	-5.966	12	300.158	3	203.122	1	.275	2	-.008	12	.316	2
82			min	-197.872	1	-720.89	2	-16.453	3	-.081	3	-.3	1	-.13	3
83		4	max	-6.262	12	298.938	3	203.122	1	.275	2	-.006	15	.764	2
84			min	-198.464	1	-722.516	2	-16.453	3	-.081	3	-.174	1	-.316	3
85		5	max	-6.558	12	297.719	3	203.122	1	.275	2	.014	10	1.213	2
86			min	-199.056	1	-724.143	2	-16.453	3	-.081	3	-.048	1	-.501	3
87		6	max	592.174	3	641.149	2	274.024	1	.058	3	.059	3	1.161	2
88			min	-1849.949	1	-188.495	3	-48.269	3	-.037	1	-.154	1	-.508	3
89		7	max	591.73	3	639.523	2	274.024	1	.058	3	.029	3	.764	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
90			min	-1850.541	1	-189.715	3	-48.269	3	-.037	1	-.02	2	-.391	3
91		8	max	591.286	3	637.897	2	274.024	1	.058	3	.187	1	.379	1
92			min	-1851.133	1	-190.934	3	-48.269	3	-.037	1	-.001	3	-.272	3
93		9	max	583.375	3	84.195	3	274.997	1	.266	2	0	10	.166	1
94			min	-2056.808	1	-72.078	1	-51.596	3	.004	15	-.092	1	-.218	3
95		10	max	582.931	3	82.976	3	274.997	1	.266	2	.079	1	.211	1
96			min	-2057.4	1	-73.704	1	-51.596	3	.004	15	-.067	3	-.27	3
97		11	max	582.487	3	81.756	3	274.997	1	.266	2	.25	1	.257	1
98			min	-2057.992	1	-75.33	1	-51.596	3	.004	15	-.099	3	-.321	3
99		12	max	571.312	3	782.361	3	297.689	3	.524	1	-.005	15	.546	1
100			min	-2258.488	1	-663.195	1	-168.37	2	-.468	3	-.157	1	-.65	3
101		13	max	570.868	3	781.141	3	297.689	3	.524	1	.165	3	.958	1
102			min	-2259.08	1	-664.821	1	-168.37	2	-.468	3	-.236	1	-1.135	3
103		14	max	200.07	1	596.842	1	171.37	1	.48	3	.006	1	1.354	1
104			min	5.883	12	-696.192	3	-3.586	3	-.35	1	0	10	-1.599	3
105		15	max	199.478	1	595.216	1	171.37	1	.48	3	.112	1	.984	1
106			min	5.587	12	-697.412	3	-3.586	3	-.35	1	0	3	-1.167	3
107		16	max	198.886	1	593.59	1	171.37	1	.48	3	.218	1	.615	1
108			min	5.291	12	-698.631	3	-3.586	3	-.35	1	-.003	3	-.734	3
109		17	max	198.295	1	591.964	1	171.37	1	.48	3	.325	1	.247	1
110			min	4.995	12	-699.851	3	-3.586	3	-.35	1	-.005	3	-.3	3
111		18	max	.76	4	2.087	4	0	5	0	1	0	1	0	4
112			min	.179	15	.491	15	0	1	0	1	0	15	0	15
113		19	max	0	1	0	1	0	5	0	1	0	1	0	1
114			min	0	1	-.003	3	0	1	0	1	0	1	0	1
115	M10	1	max	171.327	1	588.483	1	-4.403	12	.007	1	.394	1	.35	1
116			min	-3.582	3	-702.212	3	-197.586	1	-.017	3	-.007	3	-.48	3
117		2	max	171.327	1	428.11	1	-2.91	12	.007	1	.178	1	.265	3
118			min	-3.582	3	-516.63	3	-156.497	1	-.017	3	-.013	3	-.271	1
119		3	max	171.327	1	267.737	1	-1.417	12	.007	1	.035	2	.783	3
120			min	-3.582	3	-331.049	3	-115.407	1	-.017	3	-.016	3	-.696	1
121		4	max	171.327	1	107.363	1	.524	3	.007	1	.002	10	1.074	3
122			min	-3.582	3	-145.467	3	-74.318	1	-.017	3	-.104	1	-.926	1
123		5	max	171.327	1	40.115	3	2.764	3	.007	1	-.006	15	1.139	3
124			min	-3.582	3	-53.01	1	-33.229	1	-.017	3	-.17	1	-.959	1
125		6	max	171.327	1	225.696	3	9.394	9	.007	1	-.007	15	.976	3
126			min	-3.582	3	-213.383	1	-7.169	2	-.017	3	-.186	1	-.796	1
127		7	max	171.327	1	411.278	3	48.949	1	.007	1	-.002	12	.587	3
128			min	-3.582	3	-373.756	1	-2.014	10	-.017	3	-.151	1	-.437	1
129		8	max	171.327	1	596.859	3	90.039	1	.007	1	.007	3	.118	1
130			min	-3.582	3	-534.129	1	2.112	10	-.017	3	-.066	1	-.029	3
131		9	max	171.327	1	782.441	3	131.128	1	.007	1	.069	1	.868	1
132			min	-3.582	3	-694.503	1	5.01	15	-.017	3	-.023	10	-.872	3
133		10	max	171.327	1	968.022	3	172.217	1	.017	3	.255	1	1.815	1
134			min	-3.582	3	-854.876	1	6.504	15	0	15	-.013	10	-1.942	3
135		11	max	171.327	1	694.503	1	-5.01	15	.017	3	.069	1	.868	1
136			min	-3.582	3	-782.441	3	-131.128	1	-.007	1	-.023	10	-.872	3
137		12	max	171.327	1	534.129	1	-2.112	10	.017	3	.007	3	.118	1
138			min	-3.582	3	-596.859	3	-90.039	1	-.007	1	-.066	1	-.029	3
139		13	max	171.327	1	373.756	1	2.014	10	.017	3	-.002	12	.587	3
140			min	-3.582	3	-411.278	3	-48.949	1	-.007	1	-.151	1	-.437	1
141		14	max	171.327	1	213.383	1	7.169	2	.017	3	-.007	15	.976	3
142			min	-3.582	3	-225.696	3	-9.394	9	-.007	1	-.186	1	-.796	1
143		15	max	171.327	1	53.01	1	33.229	1	.017	3	-.006	15	1.139	3
144			min	-3.582	3	-40.115	3	-2.764	3	-.007	1	-.17	1	-.959	1
145		16	max	171.327	1	145.467	3	74.318	1	.017	3	.002	10	1.074	3
146			min	-3.582	3	-107.363	1	-.524	3	-.007	1	-.104	1	-.926	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
147		17	max	171.327	1	331.049	3	115.407	1	.017	3	.035	2	.783	3
148			min	-3.582	3	-267.737	1	1.417	12	-.007	1	-.016	3	-.696	1
149		18	max	171.327	1	516.63	3	156.497	1	.017	3	.178	1	.265	3
150			min	-3.582	3	-428.11	1	2.91	12	-.007	1	-.013	3	-.271	1
151		19	max	171.327	1	702.212	3	197.586	1	.017	3	.394	1	.35	1
152			min	-3.582	3	-588.483	1	4.403	12	-.007	1	-.007	3	-.48	3
153	M11	1	max	400.763	1	582.927	1	-7.087	15	0	3	.419	1	.305	1
154			min	-349.037	3	-703.393	3	-201.025	1	-.009	1	.014	15	-.575	3
155		2	max	400.763	1	422.554	1	-5.593	15	0	3	.198	1	.171	3
156			min	-349.037	3	-517.811	3	-159.936	1	-.009	1	.006	15	-.309	1
157		3	max	400.763	1	262.181	1	-4.1	15	0	3	.036	2	.691	3
158			min	-349.037	3	-332.23	3	-118.846	1	-.009	1	0	15	-.728	1
159		4	max	400.763	1	101.807	1	-2.606	15	0	3	0	3	.983	3
160			min	-349.037	3	-146.648	3	-77.757	1	-.009	1	-.092	1	-.95	1
161		5	max	400.763	1	38.933	3	-1.112	15	0	3	-.003	12	1.049	3
162			min	-349.037	3	-58.566	1	-36.668	1	-.009	1	-.162	1	-.976	1
163		6	max	400.763	1	224.515	3	6.732	9	0	3	-.003	12	.888	3
164			min	-349.037	3	-218.939	1	-7.44	2	-.009	1	-.182	1	-.807	1
165		7	max	400.763	1	410.096	3	45.51	1	0	3	-.002	12	.5	3
166			min	-349.037	3	-379.312	1	-1.599	10	-.009	1	-.151	1	-.441	1
167		8	max	400.763	1	595.678	3	86.6	1	0	3	.002	3	.12	1
168			min	-349.037	3	-539.685	1	2.527	10	-.009	1	-.071	1	-.114	3
169		9	max	400.763	1	781.259	3	127.689	1	0	3	.06	1	.878	1
170			min	-349.037	3	-700.059	1	4.753	12	-.009	1	-.022	10	-.956	3
171		10	max	400.763	1	966.841	3	168.778	1	.009	1	.242	1	1.832	1
172			min	-349.037	3	-860.432	1	6.246	12	0	15	-.012	10	-2.024	3
173		11	max	400.763	1	700.059	1	-4.753	12	.009	1	.06	1	.878	1
174			min	-349.037	3	-781.259	3	-127.689	1	0	3	-.022	10	-.956	3
175		12	max	400.763	1	539.685	1	-2.527	10	.009	1	.002	3	.12	1
176			min	-349.037	3	-595.678	3	-86.6	1	0	3	-.071	1	-.114	3
177		13	max	400.763	1	379.312	1	1.599	10	.009	1	-.002	12	.5	3
178			min	-349.037	3	-410.096	3	-45.51	1	0	3	-.151	1	-.441	1
179		14	max	400.763	1	218.939	1	7.44	2	.009	1	-.003	12	.888	3
180			min	-349.037	3	-224.515	3	-6.732	9	0	3	-.182	1	-.807	1
181		15	max	400.763	1	58.566	1	36.668	1	.009	1	-.003	12	1.049	3
182			min	-349.037	3	-38.933	3	1.112	15	0	3	-.162	1	-.976	1
183		16	max	400.763	1	146.648	3	77.757	1	.009	1	0	3	.983	3
184			min	-349.037	3	-101.807	1	2.606	15	0	3	-.092	1	-.95	1
185		17	max	400.763	1	332.23	3	118.846	1	.009	1	.036	2	.691	3
186			min	-349.037	3	-262.181	1	4.1	15	0	3	0	15	-.728	1
187		18	max	400.763	1	517.811	3	159.936	1	.009	1	.198	1	.171	3
188			min	-349.037	3	-422.554	1	5.593	15	0	3	.006	15	-.309	1
189		19	max	400.763	1	703.393	3	201.025	1	.009	1	.419	1	.305	1
190			min	-349.037	3	-582.927	1	7.087	15	0	3	.014	15	-.575	3
191	M12	1	max	43.812	2	700.013	2	-5.19	12	.002	3	.448	1	.298	2
192			min	-17.425	9	-277.272	3	-205.086	1	-.01	1	.003	3	.005	15
193		2	max	43.812	2	506.154	2	-3.696	12	.002	3	.223	1	.336	3
194			min	-17.425	9	-192.986	3	-163.996	1	-.01	1	-.005	3	-.453	1
195		3	max	43.812	2	312.295	2	-2.203	12	.002	3	.054	2	.521	3
196			min	-17.425	9	-108.7	3	-122.907	1	-.01	1	-.01	3	-.939	2
197		4	max	43.812	2	118.435	2	-.71	12	.002	3	.007	10	.602	3
198			min	-17.425	9	-24.414	3	-81.818	1	-.01	1	-.078	1	-1.203	2
199		5	max	43.812	2	59.873	3	1.494	3	.002	3	-.006	15	.58	3
200			min	-17.425	9	-76.819	1	-40.729	1	-.01	1	-.152	1	-1.229	2
201		6	max	43.812	2	144.159	3	4.947	9	.002	3	-.006	12	.456	3
202			min	-17.425	9	-269.283	2	-11.162	2	-.01	1	-.177	1	-1.018	2
203		7	max	43.812	2	228.445	3	41.45	1	.002	3	-.002	12	.228	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
204			min	-17.425	9	-463.142	2	-3.458	10	-.01	1	-.152	1	-.571	2
205		8	max	43.812	2	312.731	3	82.539	1	.002	3	.006	3	.114	2
206			min	-17.425	9	-657.002	2	.668	10	-.01	1	-.076	1	-.103	3
207		9	max	43.812	2	397.017	3	123.628	1	.002	3	.052	9	1.035	2
208			min	-17.425	9	-850.861	2	4.762	15	-.01	1	-.028	2	-.536	3
209		10	max	43.812	2	481.304	3	164.717	1	.002	3	.226	1	2.194	2
210			min	-17.425	9	-1044.72	2	6.256	15	-.01	1	-.019	10	-1.073	3
211		11	max	43.812	2	850.861	2	-4.762	15	.01	1	.052	9	1.035	2
212			min	-17.425	9	-397.017	3	-123.628	1	-.002	3	-.028	2	-.536	3
213		12	max	43.812	2	657.002	2	-.668	10	.01	1	.006	3	.114	2
214			min	-17.425	9	-312.731	3	-82.539	1	-.002	3	-.076	1	-.103	3
215		13	max	43.812	2	463.142	2	3.458	10	.01	1	-.002	12	.228	3
216			min	-17.425	9	-228.445	3	-41.45	1	-.002	3	-.152	1	-.571	2
217		14	max	43.812	2	269.283	2	11.162	2	.01	1	-.006	12	.456	3
218			min	-17.425	9	-144.159	3	-4.947	9	-.002	3	-.177	1	-1.018	2
219		15	max	43.812	2	76.819	1	40.729	1	.01	1	-.006	15	.58	3
220			min	-17.425	9	-59.873	3	-1.494	3	-.002	3	-.152	1	-1.229	2
221		16	max	43.812	2	24.414	3	81.818	1	.01	1	.007	10	.602	3
222			min	-17.425	9	-118.435	2	.71	12	-.002	3	-.078	1	-1.203	2
223		17	max	43.812	2	108.7	3	122.907	1	.01	1	.054	2	.521	3
224			min	-17.425	9	-312.295	2	2.203	12	-.002	3	-.01	3	-.939	2
225		18	max	43.812	2	192.986	3	163.996	1	.01	1	.223	1	.336	3
226			min	-17.425	9	-506.154	2	3.696	12	-.002	3	-.005	3	-.453	1
227		19	max	43.812	2	277.272	3	205.086	1	.01	1	.448	1	.298	2
228			min	-17.425	9	-700.013	2	5.19	12	-.002	3	.003	3	.005	15
229	M13	1	max	16.452	3	717.941	2	-5.372	12	.009	3	.382	1	.275	2
230			min	-202.962	1	-302.668	3	-196.109	1	-.024	1	.005	12	-.081	3
231		2	max	16.452	3	524.082	2	-3.879	12	.009	3	.168	1	.238	3
232			min	-202.962	1	-218.381	3	-155.02	1	-.024	1	-.002	3	-.484	2
233		3	max	16.452	3	330.222	2	-2.386	12	.009	3	.028	2	.453	3
234			min	-202.962	1	-134.095	3	-113.93	1	-.024	1	-.009	9	-1.007	2
235		4	max	16.452	3	136.363	2	-.892	12	.009	3	0	10	.566	3
236			min	-202.962	1	-49.809	3	-72.841	1	-.024	1	-.111	1	-1.292	2
237		5	max	16.452	3	34.477	3	1.143	3	.009	3	-.006	15	.575	3
238			min	-202.962	1	-57.496	2	-31.752	1	-.024	1	-.175	1	-1.34	2
239		6	max	16.452	3	118.763	3	10.098	9	.009	3	-.005	12	.481	3
240			min	-202.962	1	-251.356	2	-5.945	2	-.024	1	-.189	1	-1.151	2
241		7	max	16.452	3	203.05	3	50.426	1	.009	3	-.002	12	.285	3
242			min	-202.962	1	-445.215	2	-1.424	10	-.024	1	-.152	1	-.725	2
243		8	max	16.452	3	287.336	3	91.516	1	.009	3	.006	3	-.002	15
244			min	-202.962	1	-639.074	2	2.701	10	-.024	1	-.065	1	-.08	1
245		9	max	16.452	3	371.622	3	132.605	1	.009	3	.072	1	.837	2
246			min	-202.962	1	-832.933	2	5.05	15	-.024	1	-.022	10	-.418	3
247		10	max	16.452	3	455.908	3	173.694	1	.009	3	.259	1	1.973	2
248			min	-202.962	1	-1026.793	2	-6.543	15	-.024	1	-.011	10	-.923	3
249		11	max	16.452	3	832.933	2	-5.05	15	.024	1	.072	1	.837	2
250			min	-202.962	1	-371.622	3	-132.605	1	-.009	3	-.022	10	-.418	3
251		12	max	16.452	3	639.074	2	-2.701	10	.024	1	.006	3	-.002	15
252			min	-202.962	1	-287.336	3	-91.516	1	-.009	3	-.065	1	-.08	1
253		13	max	16.452	3	445.215	2	1.424	10	.024	1	-.002	12	.285	3
254			min	-202.962	1	-203.05	3	-50.426	1	-.009	3	-.152	1	-.725	2
255		14	max	16.452	3	251.356	2	5.945	2	.024	1	-.005	12	.481	3
256			min	-202.962	1	-118.763	3	-10.098	9	-.009	3	-.189	1	-1.151	2
257		15	max	16.452	3	57.496	2	31.752	1	.024	1	-.006	15	.575	3
258			min	-202.962	1	-34.477	3	-1.143	3	-.009	3	-.175	1	-1.34	2
259		16	max	16.452	3	49.809	3	72.841	1	.024	1	0	10	.566	3
260			min	-202.962	1	-136.363	2	.892	12	-.009	3	-.111	1	-1.292	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
261		17	max	16.452	3	134.095	3	113.93	1	.024	1	.028	2	.453	3
262			min	-202.962	1	-330.222	2	2.386	12	-.009	3	-.009	9	-1.007	2
263		18	max	16.452	3	218.381	3	155.02	1	.024	1	.168	1	.238	3
264			min	-202.962	1	-524.082	2	3.879	12	-.009	3	-.002	3	-.484	2
265		19	max	16.452	3	302.668	3	196.109	1	.024	1	.382	1	.275	2
266			min	-202.962	1	-717.941	2	5.372	12	-.009	3	.005	12	-.081	3
267	M2	1	max	2742.761	1	709.119	3	370.281	1	.004	3	.331	3	6.521	1
268			min	-1794.884	3	-494.411	2	-332.445	3	-.008	2	-.39	1	.204	15
269		2	max	2740.501	1	709.119	3	370.281	1	.004	3	.249	3	6.55	1
270			min	-1796.58	3	-494.411	2	-332.445	3	-.008	2	-.298	1	.202	15
271		3	max	2738.24	1	709.119	3	370.281	1	.004	3	.166	3	6.578	1
272			min	-1798.275	3	-494.411	2	-332.445	3	-.008	2	-.206	1	.17	12
273		4	max	2735.98	1	709.119	3	370.281	1	.004	3	.084	3	6.607	1
274			min	-1799.971	3	-494.411	2	-332.445	3	-.008	2	-.114	1	.064	12
275		5	max	2069.823	1	1889.031	1	297.049	1	.003	1	.039	3	6.566	1
276			min	-1556.716	3	-22.948	3	-301.562	3	-.001	3	-.103	1	-.08	3
277		6	max	2067.563	1	1889.031	1	297.049	1	.003	1	0	10	6.097	1
278			min	-1558.412	3	-22.948	3	-301.562	3	-.001	3	-.035	3	-.074	3
279		7	max	2065.302	1	1889.031	1	297.049	1	.003	1	.056	2	5.628	1
280			min	-1560.107	3	-22.948	3	-301.562	3	-.001	3	-.11	3	-.068	3
281		8	max	2063.041	1	1889.031	1	297.049	1	.003	1	.121	2	5.159	1
282			min	-1561.803	3	-22.948	3	-301.562	3	-.001	3	-.185	3	-.063	3
283		9	max	2060.781	1	1889.031	1	297.049	1	.003	1	.192	1	4.69	1
284			min	-1563.498	3	-22.948	3	-301.562	3	-.001	3	-.26	3	-.057	3
285		10	max	2058.52	1	1889.031	1	297.049	1	.003	1	.266	1	4.221	1
286			min	-1565.193	3	-22.948	3	-301.562	3	-.001	3	-.335	3	-.051	3
287		11	max	2056.26	1	1889.031	1	297.049	1	.003	1	.339	1	3.752	1
288			min	-1566.889	3	-22.948	3	-301.562	3	-.001	3	-.41	3	-.046	3
289		12	max	2053.999	1	1889.031	1	297.049	1	.003	1	.413	1	3.283	1
290			min	-1568.584	3	-22.948	3	-301.562	3	-.001	3	-.485	3	-.04	3
291		13	max	2051.738	1	1889.031	1	297.049	1	.003	1	.487	1	2.814	1
292			min	-1570.28	3	-22.948	3	-301.562	3	-.001	3	-.559	3	-.034	3
293		14	max	2049.478	1	1889.031	1	297.049	1	.003	1	.561	1	2.345	1
294			min	-1571.975	3	-22.948	3	-301.562	3	-.001	3	-.634	3	-.028	3
295		15	max	2047.217	1	1889.031	1	297.049	1	.003	1	.634	1	1.876	1
296			min	-1573.671	3	-22.948	3	-301.562	3	-.001	3	-.709	3	-.023	3
297		16	max	2044.957	1	1889.031	1	297.049	1	.003	1	.708	1	1.407	1
298			min	-1575.366	3	-22.948	3	-301.562	3	-.001	3	-.784	3	-.017	3
299		17	max	2042.696	1	1889.031	1	297.049	1	.003	1	.782	1	.938	1
300			min	-1577.062	3	-22.948	3	-301.562	3	-.001	3	-.859	3	-.011	3
301		18	max	2040.435	1	1889.031	1	297.049	1	.003	1	.856	1	.469	1
302			min	-1578.757	3	-22.948	3	-301.562	3	-.001	3	-.934	3	-.006	3
303		19	max	2038.175	1	1889.031	1	297.049	1	.003	1	.929	1	0	1
304			min	-1580.452	3	-22.948	3	-301.562	3	-.001	3	-1.009	3	0	1
305	M5	1	max	7533.692	1	2055.171	3	0	1	0	1	0	1	14.612	1
306			min	-5305.16	3	-1993.534	2	0	1	0	1	0	1	.405	15
307		2	max	7531.431	1	2055.171	3	0	1	0	1	0	1	14.92	1
308			min	-5306.856	3	-1993.534	2	0	1	0	1	0	1	.191	12
309		3	max	7529.171	1	2055.171	3	0	1	0	1	0	1	15.228	1
310			min	-5308.551	3	-1993.534	2	0	1	0	1	0	1	-.256	3
311		4	max	7526.91	1	2055.171	3	0	1	0	1	0	1	15.536	1
312			min	-5310.247	3	-1993.534	2	0	1	0	1	0	1	-.766	3
313		5	max	5701.45	1	4500.913	1	0	1	0	1	0	1	15.643	1
314			min	-4498.481	3	-343.048	3	0	1	0	1	0	1	-1.192	3
315		6	max	5699.189	1	4500.913	1	0	1	0	1	0	1	14.526	1
316			min	-4500.177	3	-343.048	3	0	1	0	1	0	1	-1.107	3
317		7	max	5696.929	1	4500.913	1	0	1	0	1	0	1	13.409	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
318			min	-4501.872	3	-343.048	3	0	1	0	1	0	1	-1.022	3
319		8	max	5694.668	1	4500.913	1	0	1	0	1	0	1	12.291	1
320			min	-4503.568	3	-343.048	3	0	1	0	1	0	1	-.937	3
321		9	max	5692.408	1	4500.913	1	0	1	0	1	0	1	11.174	1
322			min	-4505.263	3	-343.048	3	0	1	0	1	0	1	-.852	3
323		10	max	5690.147	1	4500.913	1	0	1	0	1	0	1	10.057	1
324			min	-4506.959	3	-343.048	3	0	1	0	1	0	1	-.766	3
325		11	max	5687.886	1	4500.913	1	0	1	0	1	0	1	8.939	1
326			min	-4508.654	3	-343.048	3	0	1	0	1	0	1	-.681	3
327		12	max	5685.626	1	4500.913	1	0	1	0	1	0	1	7.822	1
328			min	-4510.349	3	-343.048	3	0	1	0	1	0	1	-.596	3
329		13	max	5683.365	1	4500.913	1	0	1	0	1	0	1	6.704	1
330			min	-4512.045	3	-343.048	3	0	1	0	1	0	1	-.511	3
331		14	max	5681.105	1	4500.913	1	0	1	0	1	0	1	5.587	1
332			min	-4513.74	3	-343.048	3	0	1	0	1	0	1	-.426	3
333		15	max	5678.844	1	4500.913	1	0	1	0	1	0	1	4.47	1
334			min	-4515.436	3	-343.048	3	0	1	0	1	0	1	-.341	3
335		16	max	5676.583	1	4500.913	1	0	1	0	1	0	1	3.352	1
336			min	-4517.131	3	-343.048	3	0	1	0	1	0	1	-.255	3
337		17	max	5674.323	1	4500.913	1	0	1	0	1	0	1	2.235	1
338			min	-4518.827	3	-343.048	3	0	1	0	1	0	1	-.17	3
339		18	max	5672.062	1	4500.913	1	0	1	0	1	0	1	1.117	1
340			min	-4520.522	3	-343.048	3	0	1	0	1	0	1	-.085	3
341		19	max	5669.802	1	4500.913	1	0	1	0	1	0	1	0	1
342			min	-4522.218	3	-343.048	3	0	1	0	1	0	1	0	1
343	M8	1	max	2742.761	1	709.119	3	332.445	3	.008	2	.39	1	6.521	1
344			min	-1794.884	3	-494.411	2	-370.281	1	-.004	3	-.331	3	.204	15
345		2	max	2740.501	1	709.119	3	332.445	3	.008	2	.298	1	6.55	1
346			min	-1796.58	3	-494.411	2	-370.281	1	-.004	3	-.249	3	.202	15
347		3	max	2738.24	1	709.119	3	332.445	3	.008	2	.206	1	6.578	1
348			min	-1798.275	3	-494.411	2	-370.281	1	-.004	3	-.166	3	.17	12
349		4	max	2735.98	1	709.119	3	332.445	3	.008	2	.114	1	6.607	1
350			min	-1799.971	3	-494.411	2	-370.281	1	-.004	3	-.084	3	.064	12
351		5	max	2069.823	1	1889.031	1	301.562	3	.001	3	.103	1	6.566	1
352			min	-1556.716	3	-22.948	3	-297.049	1	-.003	1	-.039	3	-.08	3
353		6	max	2067.563	1	1889.031	1	301.562	3	.001	3	.035	3	6.097	1
354			min	-1558.412	3	-22.948	3	-297.049	1	-.003	1	0	10	-.074	3
355		7	max	2065.302	1	1889.031	1	301.562	3	.001	3	.11	3	5.628	1
356			min	-1560.107	3	-22.948	3	-297.049	1	-.003	1	-.056	2	-.068	3
357		8	max	2063.041	1	1889.031	1	301.562	3	.001	3	.185	3	5.159	1
358			min	-1561.803	3	-22.948	3	-297.049	1	-.003	1	-.121	2	-.063	3
359		9	max	2060.781	1	1889.031	1	301.562	3	.001	3	.26	3	4.69	1
360			min	-1563.498	3	-22.948	3	-297.049	1	-.003	1	-.192	1	-.057	3
361		10	max	2058.52	1	1889.031	1	301.562	3	.001	3	.335	3	4.221	1
362			min	-1565.193	3	-22.948	3	-297.049	1	-.003	1	-.266	1	-.051	3
363		11	max	2056.26	1	1889.031	1	301.562	3	.001	3	.41	3	3.752	1
364			min	-1566.889	3	-22.948	3	-297.049	1	-.003	1	-.339	1	-.046	3
365		12	max	2053.999	1	1889.031	1	301.562	3	.001	3	.485	3	3.283	1
366			min	-1568.584	3	-22.948	3	-297.049	1	-.003	1	-.413	1	-.04	3
367		13	max	2051.738	1	1889.031	1	301.562	3	.001	3	.559	3	2.814	1
368			min	-1570.28	3	-22.948	3	-297.049	1	-.003	1	-.487	1	-.034	3
369		14	max	2049.478	1	1889.031	1	301.562	3	.001	3	.634	3	2.345	1
370			min	-1571.975	3	-22.948	3	-297.049	1	-.003	1	-.561	1	-.028	3
371		15	max	2047.217	1	1889.031	1	301.562	3	.001	3	.709	3	1.876	1
372			min	-1573.671	3	-22.948	3	-297.049	1	-.003	1	-.634	1	-.023	3
373		16	max	2044.957	1	1889.031	1	301.562	3	.001	3	.784	3	1.407	1
374			min	-1575.366	3	-22.948	3	-297.049	1	-.003	1	-.708	1	-.017	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
375		17	max	2042.696	1	1889.031	1	301.562	3	.001	3	.859	3	.938	1
376			min	-1577.062	3	-22.948	3	-297.049	1	-.003	1	-.782	1	-.011	3
377		18	max	2040.435	1	1889.031	1	301.562	3	.001	3	.934	3	.469	1
378			min	-1578.757	3	-22.948	3	-297.049	1	-.003	1	-.856	1	-.006	3
379		19	max	2038.175	1	1889.031	1	301.562	3	.001	3	1.009	3	0	1
380			min	-1580.452	3	-22.948	3	-297.049	1	-.003	1	-.929	1	0	1
381	M3	1	max	2189.212	2	4.757	4	71.711	1	.037	3	.015	2	0	1
382			min	-772.039	3	1.118	15	-31.814	3	-.079	2	-.007	3	0	1
383		2	max	2189.073	2	4.229	4	71.711	1	.037	3	.036	2	0	15
384			min	-772.144	3	.994	15	-31.814	3	-.079	2	-.016	3	-.001	4
385		3	max	2188.934	2	3.7	4	71.711	1	.037	3	.057	2	0	15
386			min	-772.248	3	.87	15	-31.814	3	-.079	2	-.026	3	-.002	4
387		4	max	2188.794	2	3.171	4	71.711	1	.037	3	.078	2	0	15
388			min	-772.353	3	.745	15	-31.814	3	-.079	2	-.035	3	-.003	4
389		5	max	2188.655	2	2.643	4	71.711	1	.037	3	.099	2	-.001	15
390			min	-772.457	3	.621	15	-31.814	3	-.079	2	-.044	3	-.004	4
391		6	max	2188.515	2	2.114	4	71.711	1	.037	3	.12	1	-.001	15
392			min	-772.562	3	.497	15	-31.814	3	-.079	2	-.054	3	-.005	4
393		7	max	2188.376	2	1.586	4	71.711	1	.037	3	.141	1	-.001	15
394			min	-772.667	3	.373	15	-31.814	3	-.079	2	-.063	3	-.006	4
395		8	max	2188.237	2	1.057	4	71.711	1	.037	3	.162	1	-.001	15
396			min	-772.771	3	.248	15	-31.814	3	-.079	2	-.072	3	-.006	4
397		9	max	2188.097	2	.529	4	71.711	1	.037	3	.183	1	-.001	15
398			min	-772.876	3	.124	15	-31.814	3	-.079	2	-.082	3	-.006	4
399		10	max	2187.958	2	0	1	71.711	1	.037	3	.204	1	-.001	15
400			min	-772.98	3	0	1	-31.814	3	-.079	2	-.091	3	-.006	4
401		11	max	2187.818	2	-.124	15	71.711	1	.037	3	.225	1	-.001	15
402			min	-773.085	3	-.529	4	-31.814	3	-.079	2	-.1	3	-.006	4
403		12	max	2187.679	2	-.248	15	71.711	1	.037	3	.246	1	-.001	15
404			min	-773.189	3	-1.057	4	-31.814	3	-.079	2	-.11	3	-.006	4
405		13	max	2187.54	2	-.373	15	71.711	1	.037	3	.267	1	-.001	15
406			min	-773.294	3	-1.586	4	-31.814	3	-.079	2	-.119	3	-.006	4
407		14	max	2187.4	2	-.497	15	71.711	1	.037	3	.288	1	-.001	15
408			min	-773.398	3	-2.114	4	-31.814	3	-.079	2	-.128	3	-.005	4
409		15	max	2187.261	2	-.621	15	71.711	1	.037	3	.309	1	-.001	15
410			min	-773.503	3	-2.643	4	-31.814	3	-.079	2	-.138	3	-.004	4
411		16	max	2187.121	2	-.745	15	71.711	1	.037	3	.33	1	0	15
412			min	-773.608	3	-3.171	4	-31.814	3	-.079	2	-.147	3	-.003	4
413		17	max	2186.982	2	-.87	15	71.711	1	.037	3	.351	1	0	15
414			min	-773.712	3	-3.7	4	-31.814	3	-.079	2	-.156	3	-.002	4
415		18	max	2186.843	2	-.994	15	71.711	1	.037	3	.372	1	0	15
416			min	-773.817	3	-4.229	4	-31.814	3	-.079	2	-.166	3	-.001	4
417		19	max	2186.703	2	-1.118	15	71.711	1	.037	3	.393	1	0	1
418			min	-773.921	3	-4.757	4	-31.814	3	-.079	2	-.175	3	0	1
419	M6	1	max	6250.353	2	4.757	4	0	1	0	1	0	1	0	1
420			min	-2536.157	3	1.118	15	0	1	0	1	0	1	0	1
421		2	max	6250.213	2	4.229	4	0	1	0	1	0	1	0	15
422			min	-2536.261	3	.994	15	0	1	0	1	0	1	-.001	4
423		3	max	6250.074	2	3.7	4	0	1	0	1	0	1	0	15
424			min	-2536.366	3	.87	15	0	1	0	1	0	1	-.002	4
425		4	max	6249.934	2	3.171	4	0	1	0	1	0	1	0	15
426			min	-2536.47	3	.745	15	0	1	0	1	0	1	-.003	4
427		5	max	6249.795	2	2.643	4	0	1	0	1	0	1	-.001	15
428			min	-2536.575	3	.621	15	0	1	0	1	0	1	-.004	4
429		6	max	6249.656	2	2.114	4	0	1	0	1	0	1	-.001	15
430			min	-2536.679	3	.497	15	0	1	0	1	0	1	-.005	4
431		7	max	6249.516	2	1.586	4	0	1	0	1	0	1	-.001	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
432			min	-2536.784	3	.373	15	0	1	0	1	0	1	-.006	4
433		8	max	6249.377	2	1.057	4	0	1	0	1	0	1	-.001	15
434			min	-2536.889	3	.248	15	0	1	0	1	0	1	-.006	4
435		9	max	6249.237	2	.529	4	0	1	0	1	0	1	-.001	15
436			min	-2536.993	3	.124	15	0	1	0	1	0	1	-.006	4
437		10	max	6249.098	2	0	1	0	1	0	1	0	1	-.001	15
438			min	-2537.098	3	0	1	0	1	0	1	0	1	-.006	4
439		11	max	6248.958	2	-.124	15	0	1	0	1	0	1	-.001	15
440			min	-2537.202	3	-.529	4	0	1	0	1	0	1	-.006	4
441		12	max	6248.819	2	-.248	15	0	1	0	1	0	1	-.001	15
442			min	-2537.307	3	-1.057	4	0	1	0	1	0	1	-.006	4
443		13	max	6248.68	2	-.373	15	0	1	0	1	0	1	-.001	15
444			min	-2537.411	3	-1.586	4	0	1	0	1	0	1	-.006	4
445		14	max	6248.54	2	-.497	15	0	1	0	1	0	1	-.001	15
446			min	-2537.516	3	-2.114	4	0	1	0	1	0	1	-.005	4
447		15	max	6248.401	2	-.621	15	0	1	0	1	0	1	-.001	15
448			min	-2537.62	3	-2.643	4	0	1	0	1	0	1	-.004	4
449		16	max	6248.261	2	-.745	15	0	1	0	1	0	1	0	15
450			min	-2537.725	3	-3.171	4	0	1	0	1	0	1	-.003	4
451		17	max	6248.122	2	-.87	15	0	1	0	1	0	1	0	15
452			min	-2537.83	3	-3.7	4	0	1	0	1	0	1	-.002	4
453		18	max	6247.983	2	-.994	15	0	1	0	1	0	1	0	15
454			min	-2537.934	3	-4.229	4	0	1	0	1	0	1	-.001	4
455		19	max	6247.843	2	-1.118	15	0	1	0	1	0	1	0	1
456			min	-2538.039	3	-4.757	4	0	1	0	1	0	1	0	1
457	M9	1	max	2189.212	2	4.757	4	31.814	3	.079	2	.007	3	0	1
458			min	-772.039	3	1.118	15	-71.711	1	-.037	3	-.015	2	0	1
459		2	max	2189.073	2	4.229	4	31.814	3	.079	2	.016	3	0	15
460			min	-772.144	3	.994	15	-71.711	1	-.037	3	-.036	2	-.001	4
461		3	max	2188.934	2	3.7	4	31.814	3	.079	2	.026	3	0	15
462			min	-772.248	3	.87	15	-71.711	1	-.037	3	-.057	2	-.002	4
463		4	max	2188.794	2	3.171	4	31.814	3	.079	2	.035	3	0	15
464			min	-772.353	3	.745	15	-71.711	1	-.037	3	-.078	2	-.003	4
465		5	max	2188.655	2	2.643	4	31.814	3	.079	2	.044	3	-.001	15
466			min	-772.457	3	.621	15	-71.711	1	-.037	3	-.099	2	-.004	4
467		6	max	2188.515	2	2.114	4	31.814	3	.079	2	.054	3	-.001	15
468			min	-772.562	3	.497	15	-71.711	1	-.037	3	-.12	1	-.005	4
469		7	max	2188.376	2	1.586	4	31.814	3	.079	2	.063	3	-.001	15
470			min	-772.667	3	.373	15	-71.711	1	-.037	3	-.141	1	-.006	4
471		8	max	2188.237	2	1.057	4	31.814	3	.079	2	.072	3	-.001	15
472			min	-772.771	3	.248	15	-71.711	1	-.037	3	-.162	1	-.006	4
473		9	max	2188.097	2	.529	4	31.814	3	.079	2	.082	3	-.001	15
474			min	-772.876	3	.124	15	-71.711	1	-.037	3	-.183	1	-.006	4
475		10	max	2187.958	2	0	1	31.814	3	.079	2	.091	3	-.001	15
476			min	-772.98	3	0	1	-71.711	1	-.037	3	-.204	1	-.006	4
477		11	max	2187.818	2	-.124	15	31.814	3	.079	2	.1	3	-.001	15
478			min	-773.085	3	-.529	4	-71.711	1	-.037	3	-.225	1	-.006	4
479		12	max	2187.679	2	-.248	15	31.814	3	.079	2	.11	3	-.001	15
480			min	-773.189	3	-1.057	4	-71.711	1	-.037	3	-.246	1	-.006	4
481		13	max	2187.54	2	-.373	15	31.814	3	.079	2	.119	3	-.001	15
482			min	-773.294	3	-1.586	4	-71.711	1	-.037	3	-.267	1	-.006	4
483		14	max	2187.4	2	-.497	15	31.814	3	.079	2	.128	3	-.001	15
484			min	-773.398	3	-2.114	4	-71.711	1	-.037	3	-.288	1	-.005	4
485		15	max	2187.261	2	-.621	15	31.814	3	.079	2	.138	3	-.001	15
486			min	-773.503	3	-2.643	4	-71.711	1	-.037	3	-.309	1	-.004	4
487		16	max	2187.121	2	-.745	15	31.814	3	.079	2	.147	3	0	15
488			min	-773.608	3	-3.171	4	-71.711	1	-.037	3	-.33	1	-.003	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
489		17	max	2186.982	2	-.87	15	31.814	3	.079	2	.156	3	0	15
490			min	-773.712	3	-3.7	4	-71.711	1	-.037	3	-.351	1	-.002	4
491		18	max	2186.843	2	-.994	15	31.814	3	.079	2	.166	3	0	15
492			min	-773.817	3	-4.229	4	-71.711	1	-.037	3	-.372	1	-.001	4
493		19	max	2186.703	2	-1.118	15	31.814	3	.079	2	.175	3	0	1
494			min	-773.921	3	-4.757	4	-71.711	1	-.037	3	-.393	1	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	-.002	3	.155	3	.029	1	1.406e-2	3	NC	3	NC	3
2			min	-.279	1	-.829	1	0	3	-3.459e-2	2	153.555	1	2549.405	1
3		2	max	-.002	3	.119	3	.009	1	1.406e-2	3	6279.032	12	NC	3
4			min	-.279	1	-.712	1	0	3	-3.459e-2	2	177.2	1	4132.494	1
5		3	max	-.002	3	.083	3	0	12	1.343e-2	3	7027.948	15	NC	2
6			min	-.278	1	-.596	1	-.008	1	-3.243e-2	2	209.489	1	8855.98	1
7		4	max	-.002	3	.048	3	0	3	1.246e-2	3	8366.557	15	NC	1
8			min	-.278	1	-.483	1	-.016	1	-2.912e-2	2	254.206	1	NC	1
9		5	max	-.002	3	.018	3	0	3	1.149e-2	3	NC	15	NC	1
10			min	-.278	1	-.381	1	-.017	1	-2.582e-2	2	315.391	1	NC	1
11		6	max	-.002	3	-.004	12	.002	3	1.15e-2	3	NC	15	NC	1
12			min	-.278	1	-.295	1	-.014	1	-2.47e-2	2	394.936	1	NC	1
13		7	max	-.002	3	-.007	15	.002	3	1.22e-2	3	NC	15	NC	2
14			min	-.277	1	-.226	1	-.007	1	-2.509e-2	2	496.675	1	8409.464	1
15		8	max	-.002	3	-.005	15	0	3	1.289e-2	3	NC	5	NC	2
16			min	-.276	1	-.167	1	-.002	2	-2.547e-2	2	635.858	1	6001.738	1
17		9	max	-.002	12	-.003	15	0	15	1.38e-2	3	NC	5	NC	2
18			min	-.276	1	-.113	1	0	3	-2.474e-2	1	693.327	3	5806.196	1
19		10	max	-.002	12	-.002	15	0	1	1.508e-2	3	NC	5	NC	2
20			min	-.275	1	-.061	1	0	3	-2.211e-2	1	679.749	3	5622.182	1
21		11	max	-.003	12	0	15	.002	3	1.637e-2	3	NC	5	NC	2
22			min	-.274	1	-.042	3	-.002	1	-1.947e-2	1	679.293	3	6160.122	1
23		12	max	-.003	12	.034	1	.008	3	1.323e-2	3	NC	1	NC	2
24			min	-.273	1	-.038	3	-.009	1	-1.449e-2	1	693.758	3	9635.944	1
25		13	max	-.003	12	.072	1	.015	3	7.589e-3	3	NC	4	NC	1
26			min	-.272	1	-.025	3	-.013	1	-8.179e-3	1	743.385	3	9201.207	3
27		14	max	-.003	12	.097	1	.016	3	2.2e-3	3	NC	4	NC	2
28			min	-.272	1	.002	12	-.009	2	-2.099e-3	1	883.75	3	8454.679	1
29		15	max	-.003	12	.104	1	.011	3	7.976e-3	3	NC	4	NC	2
30			min	-.272	1	.003	15	-.003	2	-6.314e-3	1	1321.682	3	5251.629	1
31		16	max	-.003	12	.12	3	.008	1	1.375e-2	3	NC	4	NC	2
32			min	-.272	1	.003	15	0	10	-1.053e-2	1	2542.116	1	4300.142	1
33		17	max	-.003	12	.197	3	.006	1	1.953e-2	3	NC	4	NC	2
34			min	-.272	1	.003	15	0	15	-1.474e-2	1	3226.404	3	4624.636	1
35		18	max	-.003	12	.277	3	0	15	2.33e-2	3	NC	4	NC	2
36			min	-.272	1	.002	15	-.007	1	-1.749e-2	1	1098.439	3	8396.532	1
37		19	max	-.003	12	.358	3	0	15	2.33e-2	3	NC	1	NC	1
38			min	-.272	1	.002	15	-.023	1	-1.749e-2	1	662.351	3	NC	1
39	M4	1	max	.036	3	.499	3	0	1	0	1	NC	3	NC	1
40			min	-.656	1	-2.026	1	0	1	0	1	66.188	1	NC	1
41		2	max	.036	3	.394	3	0	1	0	1	3027.717	15	NC	1
42			min	-.656	1	-1.736	1	0	1	0	1	77.234	1	NC	1
43		3	max	.036	3	.29	3	0	1	0	1	3613.326	15	NC	1
44			min	-.655	1	-1.446	1	0	1	0	1	92.748	1	NC	1
45		4	max	.036	3	.19	3	0	1	0	1	4446.609	15	NC	1
46			min	-.655	1	-1.166	1	0	1	0	1	115.081	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
47		5	max	.036	3	.102	3	0	1	0	1	5629.689	15	NC	1
48			min	-.655	1	-.912	1	0	1	0	1	147.046	1	NC	1
49		6	max	.036	3	.036	3	0	1	0	1	7244.325	15	NC	1
50			min	-.654	1	-.704	1	0	1	0	1	190.473	1	NC	1
51		7	max	.035	3	-.007	12	0	1	0	1	9449.934	15	NC	1
52			min	-.652	1	-.54	1	0	1	0	1	248.577	1	NC	1
53		8	max	.034	3	-.011	15	0	1	0	1	NC	15	NC	1
54			min	-.65	1	-.402	1	0	1	0	1	248.217	3	NC	1
55		9	max	.033	3	-.007	15	0	1	0	1	NC	5	NC	1
56			min	-.648	1	-.276	1	0	1	0	1	237.996	3	NC	1
57		10	max	.033	3	-.004	15	0	1	0	1	NC	5	NC	1
58			min	-.646	1	-.152	1	0	1	0	1	230.7	3	NC	1
59		11	max	.032	3	0	15	0	1	0	1	NC	4	NC	1
60			min	-.644	1	-.092	3	0	1	0	1	226.868	3	NC	1
61		12	max	.031	3	.079	1	0	1	0	1	NC	5	NC	1
62			min	-.642	1	-.092	3	0	1	0	1	226.873	3	NC	1
63		13	max	.031	3	.171	1	0	1	0	1	NC	5	NC	1
64			min	-.64	1	-.069	3	0	1	0	1	235.928	3	NC	1
65		14	max	.03	3	.227	1	0	1	0	1	NC	5	NC	1
66			min	-.638	1	-.005	3	0	1	0	1	266.33	3	NC	1
67		15	max	.03	3	.231	1	0	1	0	1	NC	5	NC	1
68			min	-.638	1	.006	15	0	1	0	1	352.984	3	NC	1
69		16	max	.03	3	.286	3	0	1	0	1	NC	5	NC	1
70			min	-.638	1	.005	15	0	1	0	1	630.429	3	NC	1
71		17	max	.03	3	.48	3	0	1	0	1	NC	5	NC	1
72			min	-.638	1	.004	15	0	1	0	1	982.059	1	NC	1
73		18	max	.03	3	.684	3	0	1	0	1	NC	4	NC	1
74			min	-.638	1	.002	15	0	1	0	1	723.273	3	NC	1
75		19	max	.03	3	.887	3	0	1	0	1	NC	1	NC	1
76			min	-.638	1	-.008	9	0	1	0	1	344.945	3	NC	1
77	M7	1	max	-.002	3	.155	3	0	3	3.459e-2	2	NC	3	NC	3
78			min	-.279	1	-.829	1	-.029	1	-1.406e-2	3	153.555	1	2549.405	1
79		2	max	-.002	3	.119	3	0	3	3.459e-2	2	6279.032	12	NC	3
80			min	-.279	1	-.712	1	-.009	1	-1.406e-2	3	177.2	1	4132.494	1
81		3	max	-.002	3	.083	3	.008	1	3.243e-2	2	7027.948	15	NC	2
82			min	-.278	1	-.596	1	0	12	-1.343e-2	3	209.489	1	8855.98	1
83		4	max	-.002	3	.048	3	.016	1	2.912e-2	2	8366.557	15	NC	1
84			min	-.278	1	-.483	1	0	3	-1.246e-2	3	254.206	1	NC	1
85		5	max	-.002	3	.018	3	.017	1	2.582e-2	2	NC	15	NC	1
86			min	-.278	1	-.381	1	0	3	-1.149e-2	3	315.391	1	NC	1
87		6	max	-.002	3	-.004	12	.014	1	2.47e-2	2	NC	15	NC	1
88			min	-.278	1	-.295	1	-.002	3	-1.15e-2	3	394.936	1	NC	1
89		7	max	-.002	3	-.007	15	.007	1	2.509e-2	2	NC	15	NC	2
90			min	-.277	1	-.226	1	-.002	3	-1.22e-2	3	496.675	1	8409.464	1
91		8	max	-.002	3	-.005	15	.002	2	2.547e-2	2	NC	5	NC	2
92			min	-.276	1	-.167	1	0	3	-1.289e-2	3	635.858	1	6001.738	1
93		9	max	-.002	12	-.003	15	0	3	2.474e-2	1	NC	5	NC	2
94			min	-.276	1	-.113	1	0	15	-1.38e-2	3	693.327	3	5806.196	1
95		10	max	-.002	12	-.002	15	0	3	2.211e-2	1	NC	5	NC	2
96			min	-.275	1	-.061	1	0	1	-1.508e-2	3	679.749	3	5622.182	1
97		11	max	-.003	12	0	15	.002	1	1.947e-2	1	NC	5	NC	2
98			min	-.274	1	-.042	3	-.002	3	-1.637e-2	3	679.293	3	6160.122	1
99		12	max	-.003	12	.034	1	.009	1	1.449e-2	1	NC	1	NC	2
100			min	-.273	1	-.038	3	-.008	3	-1.323e-2	3	693.758	3	9635.944	1
101		13	max	-.003	12	.072	1	.013	1	8.179e-3	1	NC	4	NC	1
102			min	-.272	1	-.025	3	-.015	3	-7.589e-3	3	743.385	3	9201.207	3
103		14	max	-.003	12	.097	1	.009	2	2.099e-3	1	NC	4	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
104			min	-.272	1	.002	12	-.016	3	-2.2e-3	3	883.75	3	8454.679	1
105		15	max	-.003	12	.104	1	.003	2	6.314e-3	1	NC	4	NC	2
106			min	-.272	1	.003	15	-.011	3	-7.976e-3	3	1321.682	3	5251.629	1
107		16	max	-.003	12	.12	3	0	10	1.053e-2	1	NC	4	NC	2
108			min	-.272	1	.003	15	-.008	1	-1.375e-2	3	2542.116	1	4300.142	1
109		17	max	-.003	12	.197	3	0	15	1.474e-2	1	NC	4	NC	2
110			min	-.272	1	.003	15	-.006	1	-1.953e-2	3	3226.404	3	4624.636	1
111		18	max	-.003	12	.277	3	.007	1	1.749e-2	1	NC	4	NC	2
112			min	-.272	1	.002	15	0	15	-2.33e-2	3	1098.439	3	8396.532	1
113		19	max	-.003	12	.358	3	.023	1	1.749e-2	1	NC	1	NC	1
114			min	-.272	1	.002	15	0	15	-2.33e-2	3	662.351	3	NC	1
115	M10	1	max	.002	1	.249	3	.272	1	1.079e-2	3	NC	1	NC	1
116			min	0	3	.003	15	.003	12	-2.493e-3	1	NC	1	NC	1
117		2	max	.002	1	.603	3	.341	1	1.262e-2	3	NC	5	NC	3
118			min	0	3	-.194	1	.007	12	-3.23e-3	1	746.06	3	3808.118	1
119		3	max	.001	1	.928	3	.454	1	1.446e-2	3	NC	5	NC	3
120			min	0	3	-.428	1	.01	12	-3.968e-3	1	389.07	3	1450.755	1
121		4	max	.001	1	1.162	3	.57	1	1.629e-2	3	NC	5	NC	3
122			min	0	3	-.581	1	.01	12	-4.705e-3	1	289.271	3	884.815	1
123		5	max	0	1	1.271	3	.663	1	1.813e-2	3	NC	15	NC	3
124			min	0	3	-.626	1	.008	12	-5.443e-3	1	258.41	3	675.384	1
125		6	max	0	1	1.247	3	.716	1	1.996e-2	3	NC	5	NC	3
126			min	0	3	-.559	1	.003	3	-6.18e-3	1	264.558	3	594.751	1
127		7	max	0	1	1.11	3	.726	1	2.179e-2	3	NC	5	NC	3
128			min	0	3	-.4	1	-.007	3	-6.918e-3	1	306.739	3	581.935	1
129		8	max	0	1	.905	3	.7	1	2.363e-2	3	NC	5	NC	3
130			min	0	3	-.191	1	-.018	3	-7.656e-3	1	402.372	3	616.126	1
131		9	max	0	1	.707	3	.66	1	2.546e-2	3	NC	4	NC	5
132			min	0	3	-.004	9	-.026	3	-8.393e-3	1	577.371	3	679.378	1
133		10	max	0	1	.613	3	.638	1	2.73e-2	3	NC	1	NC	5
134			min	0	1	.002	15	-.03	3	-9.131e-3	1	725.28	3	720.974	1
135		11	max	0	3	.707	3	.66	1	2.546e-2	3	NC	4	NC	5
136			min	0	1	-.004	9	-.026	3	-8.393e-3	1	577.371	3	679.378	1
137		12	max	0	3	.905	3	.7	1	2.363e-2	3	NC	5	NC	3
138			min	0	1	-.191	1	-.018	3	-7.656e-3	1	402.372	3	616.126	1
139		13	max	0	3	1.11	3	.726	1	2.179e-2	3	NC	5	NC	3
140			min	0	1	-.4	1	-.007	3	-6.918e-3	1	306.739	3	581.935	1
141		14	max	0	3	1.247	3	.716	1	1.996e-2	3	NC	5	NC	3
142			min	0	1	-.559	1	.003	3	-6.18e-3	1	264.558	3	594.751	1
143		15	max	0	3	1.271	3	.663	1	1.813e-2	3	NC	15	NC	3
144			min	0	1	-.626	1	.008	12	-5.443e-3	1	258.41	3	675.384	1
145		16	max	0	3	1.162	3	.57	1	1.629e-2	3	NC	5	NC	3
146			min	-.001	1	-.581	1	.01	12	-4.705e-3	1	289.271	3	884.815	1
147		17	max	0	3	.928	3	.454	1	1.446e-2	3	NC	5	NC	3
148			min	-.001	1	-.428	1	.01	12	-3.968e-3	1	389.07	3	1450.755	1
149		18	max	0	3	.603	3	.341	1	1.262e-2	3	NC	5	NC	3
150			min	-.002	1	-.194	1	.007	12	-3.23e-3	1	746.06	3	3808.118	1
151		19	max	0	3	.249	3	.272	1	1.079e-2	3	NC	1	NC	1
152			min	-.002	1	.003	15	.003	12	-2.493e-3	1	NC	1	NC	1
153	M11	1	max	.004	1	.006	2	.274	1	6.172e-3	1	NC	1	NC	1
154			min	-.004	3	-.041	3	.003	12	1.868e-4	15	NC	1	NC	1
155		2	max	.004	1	.224	3	.333	1	7.161e-3	1	NC	5	NC	3
156			min	-.003	3	-.271	1	-.005	3	2.102e-4	15	955.824	1	4450.277	1
157		3	max	.003	1	.47	3	.441	1	8.15e-3	1	NC	5	NC	3
158			min	-.003	3	-.512	1	-.009	3	2.335e-4	15	509.954	1	1581.834	1
159		4	max	.003	1	.637	3	.556	1	9.139e-3	1	NC	5	NC	3
160			min	-.002	3	-.67	1	-.011	3	1.968e-4	12	389.191	3	935.71	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
161		5	max	.002	1	.69	3	.65	1	1.013e-2	1	NC	15	NC	3
162			min	-.002	3	-.716	1	-.014	3	1.568e-4	12	361.134	3	701.315	1
163		6	max	.002	1	.621	3	.707	1	1.112e-2	1	NC	5	NC	3
164			min	-.002	3	-.649	1	-.017	3	1.169e-4	12	399.024	3	609.517	1
165		7	max	.001	1	.448	3	.721	1	1.211e-2	1	NC	5	NC	3
166			min	-.001	3	-.488	1	-.021	3	7.701e-5	12	535.464	1	589.907	1
167		8	max	0	1	.219	3	.701	1	1.309e-2	1	NC	5	NC	5
168			min	0	3	-.276	1	-.026	3	2.159e-5	3	937.39	1	618.415	1
169		9	max	0	1	.005	3	.664	1	1.408e-2	1	NC	4	NC	5
170			min	0	3	-.081	1	-.03	3	-4.635e-5	3	3054.2	1	676.109	1
171		10	max	0	1	.008	1	.643	1	1.507e-2	1	NC	1	NC	5
172			min	0	1	-.093	3	-.032	3	-1.143e-4	3	5057.317	3	714.605	1
173		11	max	0	3	.005	3	.664	1	1.408e-2	1	NC	4	NC	5
174			min	0	1	-.081	1	-.03	3	-4.635e-5	3	3054.2	1	676.109	1
175		12	max	0	3	.219	3	.701	1	1.309e-2	1	NC	5	NC	5
176			min	0	1	-.276	1	-.026	3	2.159e-5	3	937.39	1	618.415	1
177		13	max	.001	3	.448	3	.721	1	1.211e-2	1	NC	5	NC	3
178			min	-.001	1	-.488	1	-.021	3	7.701e-5	12	535.464	1	589.907	1
179		14	max	.002	3	.621	3	.707	1	1.112e-2	1	NC	5	NC	3
180			min	-.002	1	-.649	1	-.017	3	1.169e-4	12	399.024	3	609.517	1
181		15	max	.002	3	.69	3	.65	1	1.013e-2	1	NC	15	NC	3
182			min	-.002	1	-.716	1	-.014	3	1.568e-4	12	361.134	3	701.315	1
183		16	max	.002	3	.637	3	.556	1	9.139e-3	1	NC	5	NC	3
184			min	-.003	1	-.67	1	-.011	3	1.968e-4	12	389.191	3	935.71	1
185		17	max	.003	3	.47	3	.441	1	8.15e-3	1	NC	5	NC	3
186			min	-.003	1	-.512	1	-.009	3	2.335e-4	15	509.954	1	1581.834	1
187		18	max	.003	3	.224	3	.333	1	7.161e-3	1	NC	5	NC	3
188			min	-.004	1	-.271	1	-.005	3	2.102e-4	15	955.824	1	4450.277	1
189		19	max	.004	3	.006	2	.274	1	6.172e-3	1	NC	1	NC	1
190			min	-.004	1	-.041	3	.003	12	1.868e-4	15	NC	1	NC	1
191	M12	1	max	0	2	-.004	15	.276	1	7.239e-3	1	NC	1	NC	1
192			min	0	9	-.132	1	.002	12	-8.655e-4	3	NC	1	NC	1
193		2	max	0	2	.15	3	.323	1	8.321e-3	1	NC	5	NC	2
194			min	0	9	-.508	1	.004	12	-1.107e-3	3	697.247	2	5566.282	1
195		3	max	0	2	.298	3	.425	1	9.402e-3	1	NC	5	NC	3
196			min	0	9	-.833	1	.005	12	-1.348e-3	3	373.13	2	1772.578	1
197		4	max	0	2	.384	3	.539	1	1.048e-2	1	NC	15	NC	3
198			min	0	9	-1.05	1	.005	12	-1.589e-3	3	284.667	2	1004.72	1
199		5	max	0	2	.4	3	.635	1	1.157e-2	1	NC	15	NC	3
200			min	0	9	-1.129	1	0	3	-1.831e-3	3	262.155	2	735.169	1
201		6	max	0	2	.349	3	.696	1	1.265e-2	1	NC	15	NC	3
202			min	0	9	-1.068	1	-.006	3	-2.072e-3	3	279.858	2	628.39	1
203		7	max	0	2	.244	3	.716	1	1.373e-2	1	NC	5	NC	3
204			min	0	9	-.891	1	-.014	3	-2.314e-3	3	346.796	2	600.075	1
205		8	max	0	2	.114	3	.701	1	1.481e-2	1	NC	5	NC	3
206			min	0	9	-.65	1	-.023	3	-2.555e-3	3	509.209	1	621.678	1
207		9	max	0	2	-.003	12	.668	1	1.589e-2	1	NC	5	NC	5
208			min	0	9	-.425	1	-.031	3	-2.796e-3	3	899.999	1	672.944	1
209		10	max	0	1	-.008	15	.649	1	1.697e-2	1	NC	3	NC	5
210			min	0	1	-.322	1	-.034	3	-3.038e-3	3	1390.85	1	707.962	1
211		11	max	0	9	-.003	12	.668	1	1.589e-2	1	NC	5	NC	5
212			min	0	2	-.425	1	-.031	3	-2.796e-3	3	899.999	1	672.944	1
213		12	max	0	9	.114	3	.701	1	1.481e-2	1	NC	5	NC	3
214			min	0	2	-.65	1	-.023	3	-2.555e-3	3	509.209	1	621.678	1
215		13	max	0	9	.244	3	.716	1	1.373e-2	1	NC	5	NC	3
216			min	0	2	-.891	1	-.014	3	-2.314e-3	3	346.796	2	600.075	1
217		14	max	0	9	.349	3	.696	1	1.265e-2	1	NC	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
218			min	0	2	-1.068	1	-.006	3	-2.072e-3	3	279.858	2	628.39	1
219		15	max	0	9	.4	3	.635	1	1.157e-2	1	NC	15	NC	3
220			min	0	2	-1.129	1	0	3	-1.831e-3	3	262.155	2	735.169	1
221		16	max	0	9	.384	3	.539	1	1.048e-2	1	NC	15	NC	3
222			min	0	2	-1.05	1	.005	12	-1.589e-3	3	284.667	2	1004.72	1
223		17	max	0	9	.298	3	.425	1	9.402e-3	1	NC	5	NC	3
224			min	0	2	-.833	1	.005	12	-1.348e-3	3	373.13	2	1772.578	1
225		18	max	0	9	.15	3	.323	1	8.321e-3	1	NC	5	NC	2
226			min	0	2	-.508	1	.004	12	-1.107e-3	3	697.247	2	5566.282	1
227		19	max	0	9	-.004	15	.276	1	7.239e-3	1	NC	1	NC	1
228			min	0	2	-.132	1	.002	12	-8.655e-4	3	NC	1	NC	1
229	M13	1	max	0	3	.106	3	.279	1	1.564e-2	1	NC	1	NC	1
230			min	-.002	1	-.672	1	.002	3	-4.859e-3	3	NC	1	NC	1
231		2	max	0	3	.31	3	.355	1	1.822e-2	1	NC	5	NC	3
232			min	-.002	1	-1.173	1	.002	3	-5.875e-3	3	520.838	2	3464.737	1
233		3	max	0	3	.487	3	.472	1	2.081e-2	1	NC	15	NC	3
234			min	-.002	1	-1.622	1	.003	3	-6.891e-3	3	275.384	2	1365.778	1
235		4	max	0	3	.611	3	.591	1	2.339e-2	1	9143.836	15	NC	3
236			min	-.001	1	-1.957	1	.001	3	-7.907e-3	3	204.102	2	845.742	1
237		5	max	0	3	.67	3	.684	1	2.598e-2	1	7944.391	15	NC	3
238			min	-.001	1	-2.146	1	-.003	3	-8.924e-3	3	178.68	2	650.926	1
239		6	max	0	3	.661	3	.737	1	2.856e-2	1	7712.106	15	NC	3
240			min	0	1	-2.182	1	-.009	3	-9.94e-3	3	174.778	1	575.985	1
241		7	max	0	3	.595	3	.746	1	3.114e-2	1	8165.538	15	NC	3
242			min	0	1	-2.087	1	-.017	3	-1.096e-2	3	186.495	1	565.075	1
243		8	max	0	3	.498	3	.719	1	3.373e-2	1	9237.471	15	NC	5
244			min	0	1	-1.91	1	-.026	3	-1.197e-2	3	213.259	1	598.876	1
245		9	max	0	3	.403	3	.678	1	3.631e-2	1	NC	15	NC	5
246			min	0	1	-1.725	1	-.033	3	-1.299e-2	3	250.691	1	660.168	1
247		10	max	0	1	.358	3	.656	1	3.889e-2	1	NC	15	NC	5
248			min	0	1	-1.636	1	-.036	3	-1.4e-2	3	273.912	1	700.199	1
249		11	max	0	1	.403	3	.678	1	3.631e-2	1	NC	15	NC	5
250			min	0	3	-1.725	1	-.033	3	-1.299e-2	3	250.691	1	660.168	1
251		12	max	0	1	.498	3	.719	1	3.373e-2	1	9237.471	15	NC	5
252			min	0	3	-1.91	1	-.026	3	-1.197e-2	3	213.259	1	598.876	1
253		13	max	0	1	.595	3	.746	1	3.114e-2	1	8165.538	15	NC	3
254			min	0	3	-2.087	1	-.017	3	-1.096e-2	3	186.495	1	565.075	1
255		14	max	0	1	.661	3	.737	1	2.856e-2	1	7712.106	15	NC	3
256			min	0	3	-2.182	1	-.009	3	-9.94e-3	3	174.778	1	575.985	1
257		15	max	.001	1	.67	3	.684	1	2.598e-2	1	7944.391	15	NC	3
258			min	0	3	-2.146	1	-.003	3	-8.924e-3	3	178.68	2	650.926	1
259		16	max	.001	1	.611	3	.591	1	2.339e-2	1	9143.836	15	NC	3
260			min	0	3	-1.957	1	.001	3	-7.907e-3	3	204.102	2	845.742	1
261		17	max	.002	1	.487	3	.472	1	2.081e-2	1	NC	15	NC	3
262			min	0	3	-1.622	1	.003	3	-6.891e-3	3	275.384	2	1365.778	1
263		18	max	.002	1	.31	3	.355	1	1.822e-2	1	NC	5	NC	3
264			min	0	3	-1.173	1	.002	3	-5.875e-3	3	520.838	2	3464.737	1
265		19	max	.002	1	.106	3	.279	1	1.564e-2	1	NC	1	NC	1
266			min	0	3	-.672	1	.002	3	-4.859e-3	3	NC	1	NC	1
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	3	2.078e-3	2	NC	1	NC	1
270			min	0	1	-.001	1	0	1	-9.32e-4	3	NC	1	NC	1
271		3	max	0	3	0	15	0	3	4.157e-3	2	NC	1	NC	1
272			min	0	1	-.004	1	0	1	-1.864e-3	3	NC	1	NC	1
273		4	max	0	3	0	15	.001	3	6.235e-3	2	NC	3	NC	1
274			min	0	1	-.01	1	-.001	1	-2.796e-3	3	5442.739	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
275		5	max	0	3	0	15	.002	3	7.928e-3	2	NC	3	NC	1
276			min	0	1	-.018	1	-.002	1	-3.549e-3	3	3047.598	1	NC	1
277		6	max	0	3	0	15	.002	3	7.256e-3	2	NC	3	NC	1
278			min	0	1	-.028	1	-.003	1	-3.205e-3	3	1933.72	1	NC	1
279		7	max	0	3	-.001	15	.003	3	6.585e-3	2	NC	3	NC	2
280			min	0	1	-.04	1	-.004	1	-2.862e-3	3	1343.574	1	8731.125	1
281		8	max	0	3	-.001	12	.003	3	5.914e-3	2	NC	3	NC	2
282			min	0	1	-.054	1	-.004	1	-2.519e-3	3	993.494	1	7310.334	1
283		9	max	0	3	-.002	12	.004	3	5.243e-3	2	NC	3	NC	2
284			min	0	1	-.07	1	-.005	1	-2.176e-3	3	768.473	1	6362.733	1
285		10	max	0	3	-.002	12	.004	3	4.572e-3	2	NC	3	NC	2
286			min	0	1	-.087	1	-.006	1	-1.833e-3	3	615.279	1	5730.808	1
287		11	max	0	3	-.002	12	.004	3	3.901e-3	2	NC	3	NC	2
288			min	-.001	1	-.106	1	-.006	1	-1.489e-3	3	506.157	1	5330.129	1
289		12	max	0	3	-.002	12	.003	3	3.229e-3	2	NC	3	NC	2
290			min	-.001	1	-.126	1	-.006	1	-1.146e-3	3	425.598	1	5119.861	1
291		13	max	0	3	-.002	12	.002	3	2.558e-3	2	NC	3	NC	2
292			min	-.001	1	-.147	1	-.005	1	-8.031e-4	3	364.421	1	5089.575	1
293		14	max	0	3	-.003	12	0	3	1.887e-3	2	NC	3	NC	2
294			min	-.001	1	-.169	1	-.005	1	-4.599e-4	3	316.841	1	5265.917	1
295		15	max	.001	3	-.003	12	0	15	1.216e-3	2	NC	3	NC	2
296			min	-.001	1	-.192	1	-.003	1	-1.167e-4	3	279.101	1	5733.908	1
297		16	max	.001	3	-.003	12	0	10	5.447e-4	2	NC	3	NC	2
298			min	-.002	1	-.216	1	-.004	3	-1.23e-4	9	248.669	1	6717.819	1
299		17	max	.001	3	-.003	12	.003	2	5.697e-4	3	NC	3	NC	2
300			min	-.002	1	-.24	1	-.007	3	-5.788e-4	1	223.777	1	7655.727	3
301		18	max	.001	3	-.003	12	.006	2	9.129e-4	3	NC	3	NC	1
302			min	-.002	1	-.264	1	-.011	3	-1.278e-3	1	203.173	1	4891.173	3
303		19	max	.001	3	-.003	12	.009	2	1.256e-3	3	NC	3	NC	1
304			min	-.002	1	-.288	1	-.016	3	-1.978e-3	1	185.942	1	3412.25	3
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	1	0	1	NC	1	NC	1
308			min	0	1	-.002	1	0	1	0	1	NC	1	NC	1
309		3	max	0	3	0	15	0	1	0	1	NC	3	NC	1
310			min	0	1	-.01	1	0	1	0	1	5555.907	1	NC	1
311		4	max	0	3	0	15	0	1	0	1	NC	3	NC	1
312			min	-.001	1	-.022	1	0	1	0	1	2427.294	1	NC	1
313		5	max	0	3	0	12	0	1	0	1	NC	3	NC	1
314			min	-.001	1	-.04	1	0	1	0	1	1345.617	1	NC	1
315		6	max	.001	3	0	12	0	1	0	1	NC	3	NC	1
316			min	-.002	1	-.063	1	0	1	0	1	845.794	1	NC	1
317		7	max	.001	3	0	3	0	1	0	1	NC	3	NC	1
318			min	-.002	1	-.092	1	0	1	0	1	583.992	1	NC	1
319		8	max	.002	3	.002	3	0	1	0	1	NC	3	NC	1
320			min	-.002	1	-.125	1	0	1	0	1	429.911	1	NC	1
321		9	max	.002	3	.003	3	0	1	0	1	NC	3	NC	1
322			min	-.002	1	-.162	1	0	1	0	1	331.441	1	NC	1
323		10	max	.002	3	.005	3	0	1	0	1	NC	3	NC	1
324			min	-.003	1	-.203	1	0	1	0	1	264.695	1	NC	1
325		11	max	.002	3	.007	3	0	1	0	1	NC	12	NC	1
326			min	-.003	1	-.247	1	0	1	0	1	217.315	1	NC	1
327		12	max	.002	3	.01	3	0	1	0	1	NC	12	NC	1
328			min	-.003	1	-.294	1	0	1	0	1	182.433	1	NC	1
329		13	max	.003	3	.012	3	0	1	0	1	8271.995	12	NC	1
330			min	-.003	1	-.344	1	0	1	0	1	156.004	1	NC	1
331		14	max	.003	3	.015	3	0	1	0	1	6701.409	12	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
332			min	-.004	1	-.396	1	0	1	0	1	135.487	1	NC	1
333		15	max	.003	3	.018	3	0	1	0	1	5584.441	12	NC	1
334			min	-.004	1	-.45	1	0	1	0	1	119.24	1	NC	1
335		16	max	.003	3	.021	3	0	1	0	1	4759.147	12	NC	1
336			min	-.004	1	-.505	1	0	1	0	1	106.157	1	NC	1
337		17	max	.003	3	.024	3	0	1	0	1	4130.78	12	NC	1
338			min	-.005	1	-.562	1	0	1	0	1	95.469	1	NC	1
339		18	max	.004	3	.027	3	0	1	0	1	3640.968	12	NC	1
340			min	-.005	1	-.619	1	0	1	0	1	86.631	1	NC	1
341		19	max	.004	3	.03	3	0	1	0	1	3251.804	12	NC	1
342			min	-.005	1	-.677	1	0	1	0	1	79.247	1	NC	1
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	15	0	1	9.32e-4	3	NC	1	NC	1
346			min	0	1	-.001	1	0	3	-2.078e-3	2	NC	1	NC	1
347		3	max	0	3	0	15	0	1	1.864e-3	3	NC	1	NC	1
348			min	0	1	-.004	1	0	3	-4.157e-3	2	NC	1	NC	1
349		4	max	0	3	0	15	.001	1	2.796e-3	3	NC	3	NC	1
350			min	0	1	-.01	1	-.001	3	-6.235e-3	2	5442.739	1	NC	1
351		5	max	0	3	0	15	.002	1	3.549e-3	3	NC	3	NC	1
352			min	0	1	-.018	1	-.002	3	-7.928e-3	2	3047.598	1	NC	1
353		6	max	0	3	0	15	.003	1	3.205e-3	3	NC	3	NC	1
354			min	0	1	-.028	1	-.002	3	-7.256e-3	2	1933.72	1	NC	1
355		7	max	0	3	-.001	15	.004	1	2.862e-3	3	NC	3	NC	2
356			min	0	1	-.04	1	-.003	3	-6.585e-3	2	1343.574	1	8731.125	1
357		8	max	0	3	-.001	12	.004	1	2.519e-3	3	NC	3	NC	2
358			min	0	1	-.054	1	-.003	3	-5.914e-3	2	993.494	1	7310.334	1
359		9	max	0	3	-.002	12	.005	1	2.176e-3	3	NC	3	NC	2
360			min	0	1	-.07	1	-.004	3	-5.243e-3	2	768.473	1	6362.733	1
361		10	max	0	3	-.002	12	.006	1	1.833e-3	3	NC	3	NC	2
362			min	0	1	-.087	1	-.004	3	-4.572e-3	2	615.279	1	5730.808	1
363		11	max	0	3	-.002	12	.006	1	1.489e-3	3	NC	3	NC	2
364			min	-.001	1	-.106	1	-.004	3	-3.901e-3	2	506.157	1	5330.129	1
365		12	max	0	3	-.002	12	.006	1	1.146e-3	3	NC	3	NC	2
366			min	-.001	1	-.126	1	-.003	3	-3.229e-3	2	425.598	1	5119.861	1
367		13	max	0	3	-.002	12	.005	1	8.031e-4	3	NC	3	NC	2
368			min	-.001	1	-.147	1	-.002	3	-2.558e-3	2	364.421	1	5089.575	1
369		14	max	0	3	-.003	12	.005	1	4.599e-4	3	NC	3	NC	2
370			min	-.001	1	-.169	1	0	3	-1.887e-3	2	316.841	1	5265.917	1
371		15	max	.001	3	-.003	12	.003	1	1.167e-4	3	NC	3	NC	2
372			min	-.001	1	-.192	1	0	15	-1.216e-3	2	279.101	1	5733.908	1
373		16	max	.001	3	-.003	12	.004	3	1.23e-4	9	NC	3	NC	2
374			min	-.002	1	-.216	1	0	10	-5.447e-4	2	248.669	1	6717.819	1
375		17	max	.001	3	-.003	12	.007	3	5.788e-4	1	NC	3	NC	2
376			min	-.002	1	-.24	1	-.003	2	-5.697e-4	3	223.777	1	7655.727	3
377		18	max	.001	3	-.003	12	.011	3	1.278e-3	1	NC	3	NC	1
378			min	-.002	1	-.264	1	-.006	2	-9.129e-4	3	203.173	1	4891.173	3
379		19	max	.001	3	-.003	12	.016	3	1.978e-3	1	NC	3	NC	1
380			min	-.002	1	-.288	1	-.009	2	-1.256e-3	3	185.942	1	3412.25	3
381	M3	1	max	.015	1	0	12	.002	3	2.402e-3	2	NC	1	NC	1
382			min	0	15	-.006	1	-.002	1	-9.735e-4	3	NC	1	NC	1
383		2	max	.015	1	0	3	.014	3	3.338e-3	2	NC	1	NC	4
384			min	0	15	-.031	1	-.028	1	-1.41e-3	3	NC	1	2304.445	1
385		3	max	.014	1	0	3	.025	3	4.274e-3	2	NC	1	NC	5
386			min	0	15	-.055	1	-.054	2	-1.847e-3	3	NC	1	1168.817	1
387		4	max	.013	1	0	3	.037	3	5.21e-3	2	NC	1	NC	5
388			min	0	15	-.08	1	-.079	2	-2.283e-3	3	NC	1	795.163	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
389		5	max	.012	1	0	3	.047	3	6.146e-3	2	NC	1	NC	5
390			min	0	15	-.105	1	-.102	2	-2.72e-3	3	NC	1	612.447	1
391		6	max	.012	1	0	3	.057	3	7.082e-3	2	NC	1	NC	5
392			min	0	15	-.13	1	-.123	2	-3.156e-3	3	NC	1	506.616	1
393		7	max	.011	1	0	3	.065	3	8.018e-3	2	NC	1	NC	5
394			min	0	15	-.154	1	-.141	2	-3.593e-3	3	NC	1	439.832	1
395		8	max	.01	1	0	3	.072	3	8.955e-3	2	NC	1	NC	5
396			min	0	15	-.179	1	-.156	2	-4.03e-3	3	NC	1	396.09	1
397		9	max	.01	1	0	3	.077	3	9.891e-3	2	NC	1	NC	5
398			min	0	15	-.203	1	-.168	2	-4.466e-3	3	NC	1	367.665	1
399		10	max	.009	1	0	3	.081	3	1.083e-2	2	NC	1	NC	5
400			min	0	15	-.227	1	-.176	2	-4.903e-3	3	NC	1	350.643	1
401		11	max	.008	1	0	3	.082	3	1.176e-2	2	NC	1	NC	15
402			min	0	15	-.252	1	-.179	2	-5.339e-3	3	NC	1	343.228	1
403		12	max	.008	1	0	3	.081	3	1.27e-2	2	NC	1	NC	15
404			min	0	15	-.276	1	-.177	2	-5.776e-3	3	NC	1	345.131	1
405		13	max	.007	1	0	3	.078	3	1.364e-2	2	NC	1	NC	5
406			min	0	15	-.3	1	-.17	2	-6.212e-3	3	NC	1	357.596	1
407		14	max	.006	1	.002	3	.073	3	1.457e-2	2	NC	1	NC	5
408			min	0	15	-.324	1	-.157	2	-6.649e-3	3	NC	1	384.136	1
409		15	max	.005	1	.002	3	.064	3	1.551e-2	2	NC	1	NC	5
410			min	0	15	-.347	1	-.138	2	-7.086e-3	3	NC	1	432.793	1
411		16	max	.005	3	.003	3	.053	3	1.644e-2	2	NC	1	NC	5
412			min	0	10	-.371	1	-.112	2	-7.522e-3	3	NC	1	523.239	1
413		17	max	.005	3	.004	3	.038	3	1.738e-2	2	NC	1	NC	5
414			min	0	10	-.395	1	-.079	2	-7.959e-3	3	NC	1	715.417	1
415		18	max	.006	3	.004	3	.02	3	1.832e-2	2	NC	1	NC	5
416			min	0	10	-.418	1	-.038	2	-8.395e-3	3	NC	1	1310.359	1
417		19	max	.006	3	.005	3	.016	1	1.925e-2	2	NC	1	NC	1
418			min	-.001	10	-.442	1	-.002	3	-8.832e-3	3	NC	1	NC	1
419	M6	1	max	.035	1	0	3	0	1	0	1	NC	1	NC	1
420			min	0	15	-.013	1	0	1	0	1	NC	1	NC	1
421		2	max	.033	1	.004	3	0	1	0	1	NC	1	NC	1
422			min	0	15	-.071	1	0	1	0	1	NC	1	NC	1
423		3	max	.031	1	.008	3	0	1	0	1	NC	1	NC	1
424			min	0	15	-.13	1	0	1	0	1	8148.915	3	NC	1
425		4	max	.029	1	.012	3	0	1	0	1	NC	1	NC	1
426			min	0	15	-.188	1	0	1	0	1	5414.093	3	NC	1
427		5	max	.026	1	.016	3	0	1	0	1	NC	1	NC	1
428			min	0	15	-.246	1	0	1	0	1	4042.172	3	NC	1
429		6	max	.024	1	.02	3	0	1	0	1	NC	1	NC	1
430			min	0	15	-.304	1	0	1	0	1	3215.913	3	NC	1
431		7	max	.022	1	.024	3	0	1	0	1	NC	1	NC	1
432			min	0	15	-.362	1	0	1	0	1	2662.906	3	NC	1
433		8	max	.02	1	.028	3	0	1	0	1	NC	1	NC	1
434			min	0	15	-.42	1	0	1	0	1	2266.396	3	NC	1
435		9	max	.018	1	.033	3	0	1	0	1	NC	1	NC	1
436			min	0	15	-.478	1	0	1	0	1	1967.999	3	NC	1
437		10	max	.016	1	.037	3	0	1	0	1	NC	1	NC	1
438			min	0	15	-.535	1	0	1	0	1	1735.267	3	NC	1
439		11	max	.014	1	.041	3	0	1	0	1	NC	1	NC	1
440			min	0	15	-.593	1	0	1	0	1	1548.72	3	NC	1
441		12	max	.012	1	.046	3	0	1	0	1	NC	1	NC	1
442			min	0	15	-.65	1	0	1	0	1	1395.952	3	NC	1
443		13	max	.012	3	.05	3	0	1	0	1	NC	1	NC	1
444			min	0	15	-.708	1	0	1	0	1	1268.678	3	NC	1
445		14	max	.013	3	.055	3	0	1	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
446			min	0	10	-.765	1	0	1	0	1	1161.157	3	NC	1
447		15	max	.013	3	.06	3	0	1	0	1	NC	1	NC	1
448			min	-.002	10	-.822	1	0	1	0	1	1069.276	3	NC	1
449		16	max	.014	3	.064	3	0	1	0	1	NC	1	NC	1
450			min	-.003	10	-.879	1	0	1	0	1	990.013	3	NC	1
451		17	max	.015	3	.069	3	0	1	0	1	NC	1	NC	1
452			min	-.005	2	-.936	1	0	1	0	1	921.095	3	NC	1
453		18	max	.016	3	.074	3	0	1	0	1	NC	1	NC	1
454			min	-.007	2	-.993	1	0	1	0	1	860.779	3	NC	1
455		19	max	.017	3	.079	3	0	1	0	1	NC	1	NC	1
456			min	-.009	2	-1.05	1	0	1	0	1	807.705	3	NC	1
457	M9	1	max	.015	1	0	12	.002	1	9.735e-4	3	NC	1	NC	1
458			min	0	15	-.006	1	-.002	3	-2.402e-3	2	NC	1	NC	1
459		2	max	.015	1	0	3	.028	1	1.41e-3	3	NC	1	NC	4
460			min	0	15	-.031	1	-.014	3	-3.338e-3	2	NC	1	2304.445	1
461		3	max	.014	1	0	3	.054	2	1.847e-3	3	NC	1	NC	5
462			min	0	15	-.055	1	-.025	3	-4.274e-3	2	NC	1	1168.817	1
463		4	max	.013	1	0	3	.079	2	2.283e-3	3	NC	1	NC	5
464			min	0	15	-.08	1	-.037	3	-5.21e-3	2	NC	1	795.163	1
465		5	max	.012	1	0	3	.102	2	2.72e-3	3	NC	1	NC	5
466			min	0	15	-.105	1	-.047	3	-6.146e-3	2	NC	1	612.447	1
467		6	max	.012	1	0	3	.123	2	3.156e-3	3	NC	1	NC	5
468			min	0	15	-.13	1	-.057	3	-7.082e-3	2	NC	1	506.616	1
469		7	max	.011	1	0	3	.141	2	3.593e-3	3	NC	1	NC	5
470			min	0	15	-.154	1	-.065	3	-8.018e-3	2	NC	1	439.832	1
471		8	max	.01	1	0	3	.156	2	4.03e-3	3	NC	1	NC	5
472			min	0	15	-.179	1	-.072	3	-8.955e-3	2	NC	1	396.09	1
473		9	max	.01	1	0	3	.168	2	4.466e-3	3	NC	1	NC	5
474			min	0	15	-.203	1	-.077	3	-9.891e-3	2	NC	1	367.665	1
475		10	max	.009	1	0	3	.176	2	4.903e-3	3	NC	1	NC	5
476			min	0	15	-.227	1	-.081	3	-1.083e-2	2	NC	1	350.643	1
477		11	max	.008	1	0	3	.179	2	5.339e-3	3	NC	1	NC	15
478			min	0	15	-.252	1	-.082	3	-1.176e-2	2	NC	1	343.228	1
479		12	max	.008	1	0	3	.177	2	5.776e-3	3	NC	1	NC	15
480			min	0	15	-.276	1	-.081	3	-1.27e-2	2	NC	1	345.131	1
481		13	max	.007	1	0	3	.17	2	6.212e-3	3	NC	1	NC	5
482			min	0	15	-.3	1	-.078	3	-1.364e-2	2	NC	1	357.596	1
483		14	max	.006	1	.002	3	.157	2	6.649e-3	3	NC	1	NC	5
484			min	0	15	-.324	1	-.073	3	-1.457e-2	2	NC	1	384.136	1
485		15	max	.005	1	.002	3	.138	2	7.086e-3	3	NC	1	NC	5
486			min	0	15	-.347	1	-.064	3	-1.551e-2	2	NC	1	432.793	1
487		16	max	.005	3	.003	3	.112	2	7.522e-3	3	NC	1	NC	5
488			min	0	10	-.371	1	-.053	3	-1.644e-2	2	NC	1	523.239	1
489		17	max	.005	3	.004	3	.079	2	7.959e-3	3	NC	1	NC	5
490			min	0	10	-.395	1	-.038	3	-1.738e-2	2	NC	1	715.417	1
491		18	max	.006	3	.004	3	.038	2	8.395e-3	3	NC	1	NC	5
492			min	0	10	-.418	1	-.02	3	-1.832e-2	2	NC	1	1310.359	1
493		19	max	.006	3	.005	3	.002	3	8.832e-3	3	NC	1	NC	1
494			min	-.001	10	-.442	1	-.016	1	-1.925e-2	2	NC	1	NC	1