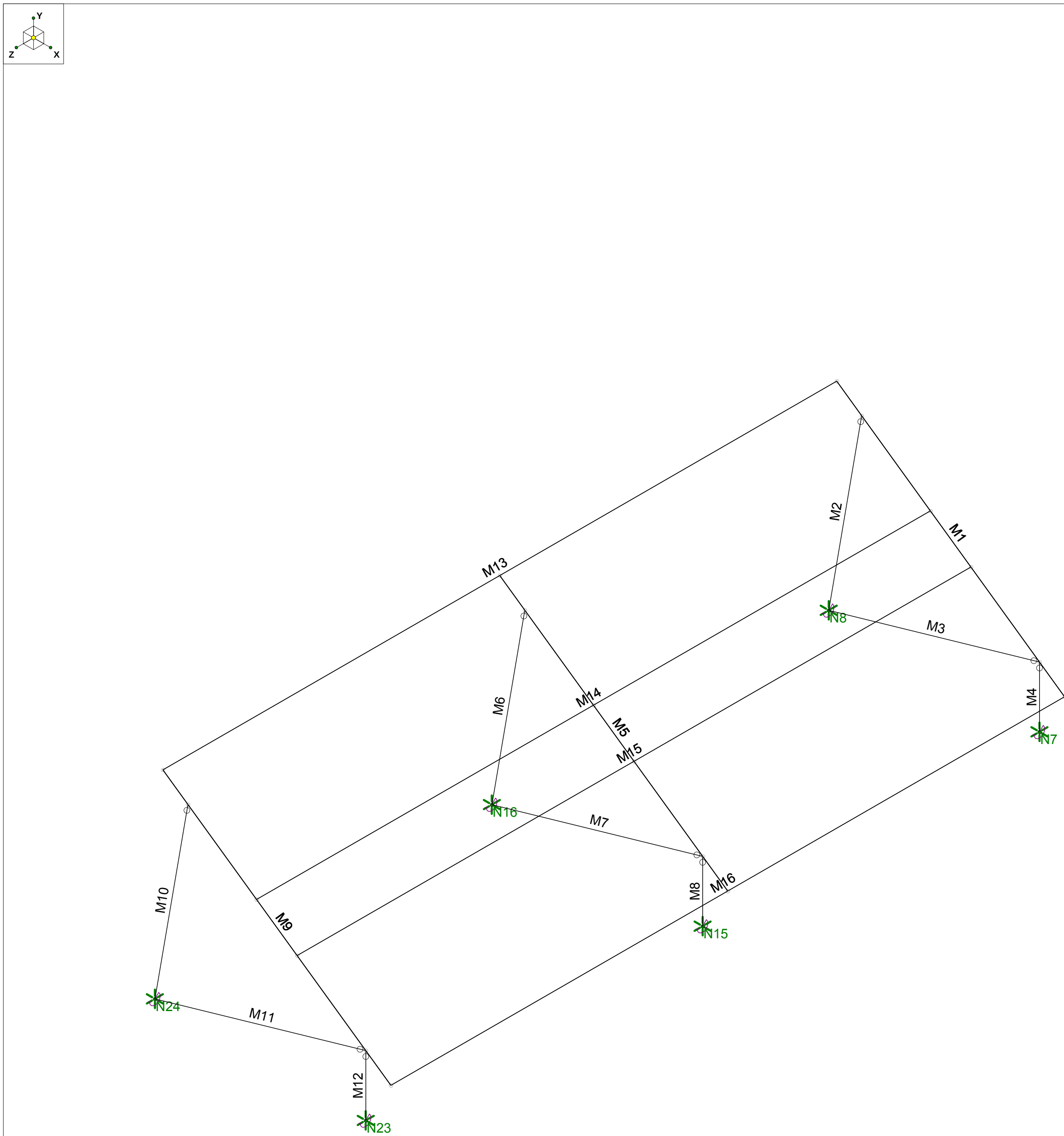


Schletter, Inc.	Standard PVMax Racking System	35° Tilt w/ Seismic Design
HCV	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

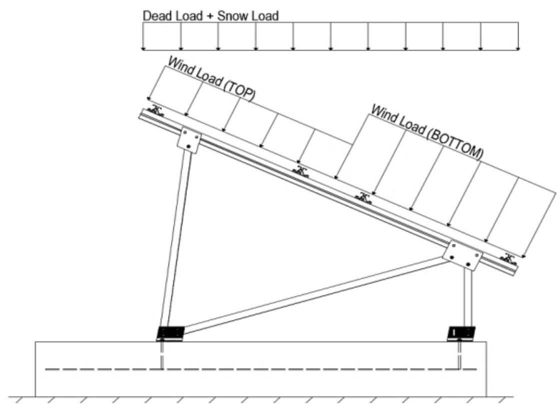
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 2
Module Tilt = 35°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 14.43 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.64
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 130 mph
Height < 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 26.53 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.200	*(Pressure)*
$Cf+_{BOTTOM}$	=	2.000	
$Cf-_{TOP, OUTER PURLIN}$	=	-2.700	
$Cf-_{TOP, INNER PURLIN}$	=	-2.100	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.200	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.06	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	Diagonal Struts	Location	Front Reactions	Location
M13	Top	M3	Outer	N7	Outer
M14	Mid-Top	M7	Inner	N15	Inner
M15	Mid-Bottom	M11	Outer	N23	Outer
M16	Bottom				

Girders	Location	Rear Struts	Location	Rear Reactions	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

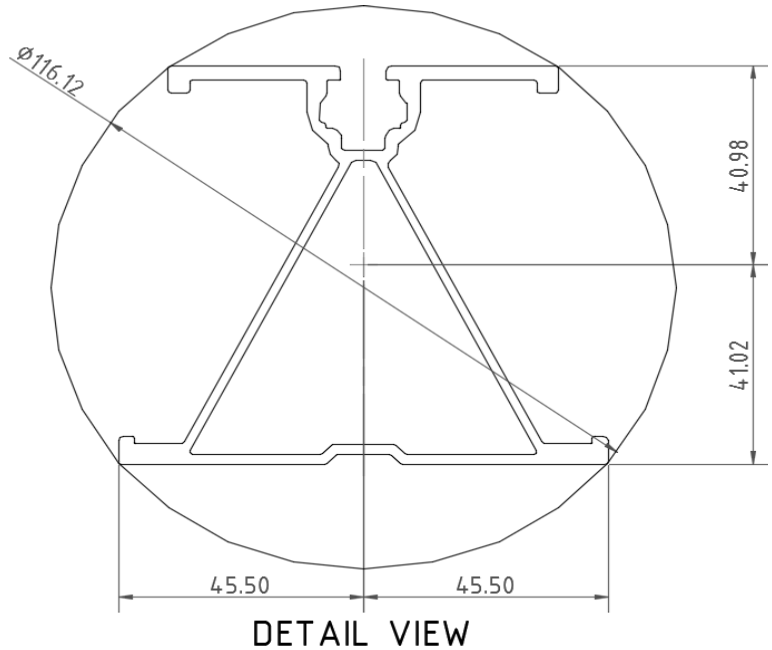
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

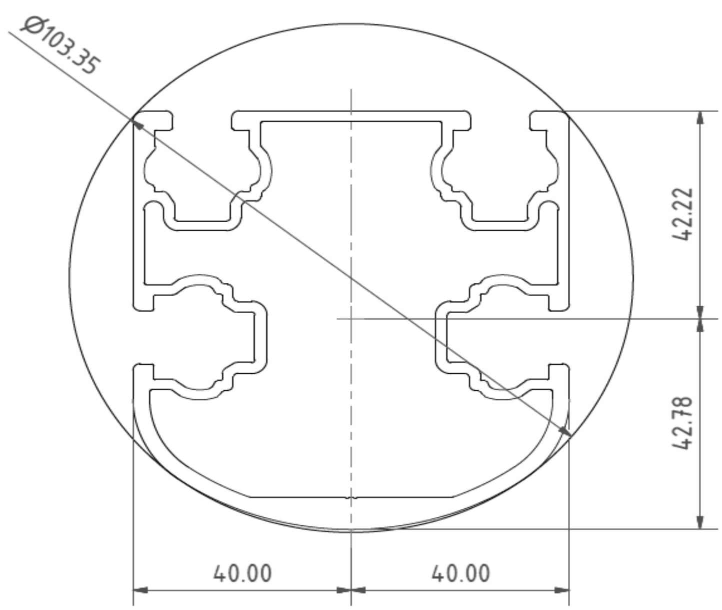
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	114	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.972	k-ft
M_z =	0.136	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	83%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

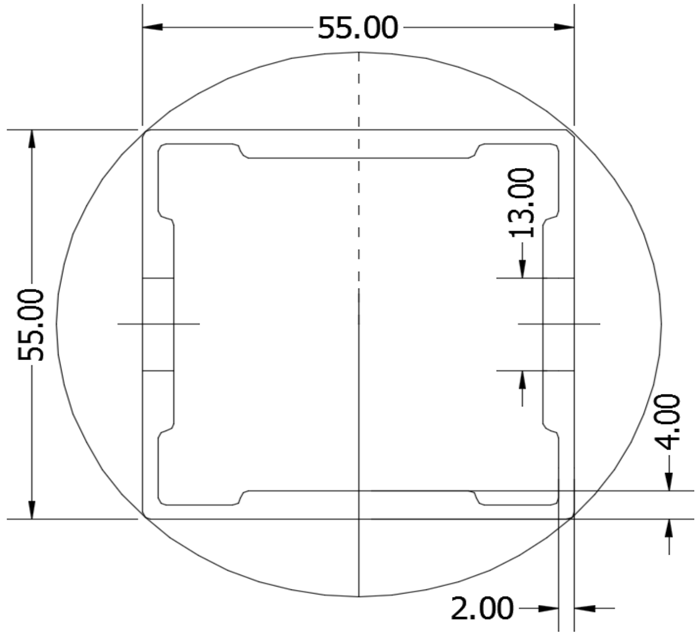
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	88.90	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.35	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-2.895	k-ft
M_z =	0.000	k-ft
P_n =	-0.974	k
$M_{y\ allowable}$ =	3.464	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	85%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

Strut Type =	<u>55x55</u>	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	<u>24.80</u>	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.523	k-ft
P_n =	0.541	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	<u>39%</u>	

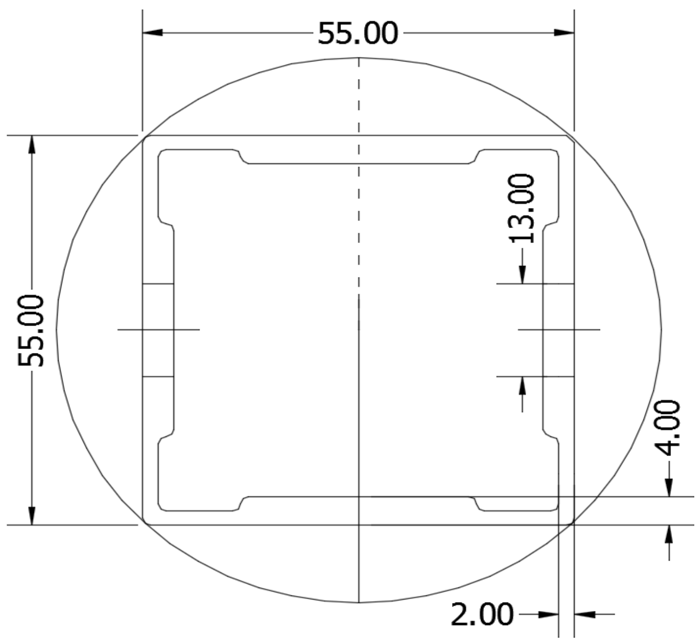


DETAIL VIEW

4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Strut Type =	<u>55x55</u>	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	<u>86.60</u>	in
$\Phi F_{ty\ AXIAL}$ =	7.50	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.009	k-ft
M_z =	0.000	k-ft
P_n =	2.859	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	7.371	k
Utilization =	<u>39%</u>	

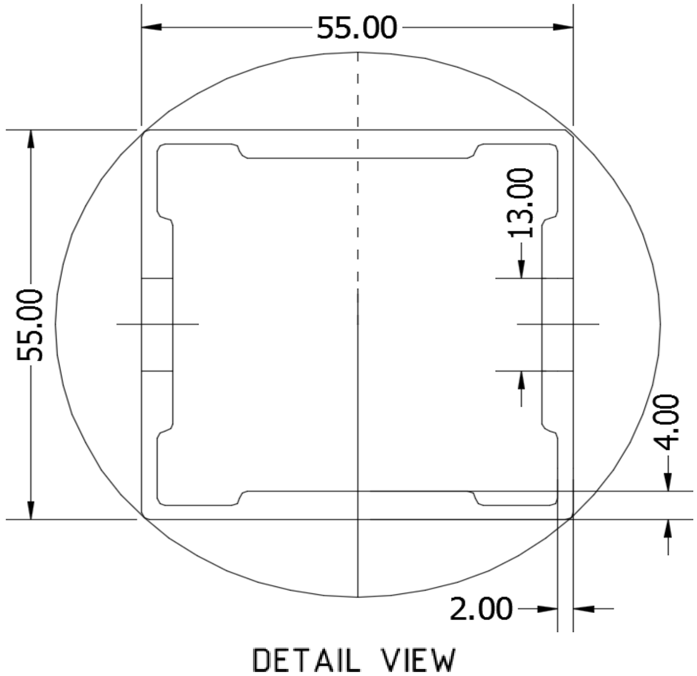


DETAIL VIEW

4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	55x55	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	78.03	in
$\Phi F_{ty\ AXIAL}$ =	8.94	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.009	k-ft
M_z =	0.000	k-ft
P_n =	3.105	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	8.786	k
Utilization =	36%	



5. FOUNDATION DESIGN CALCULATIONS

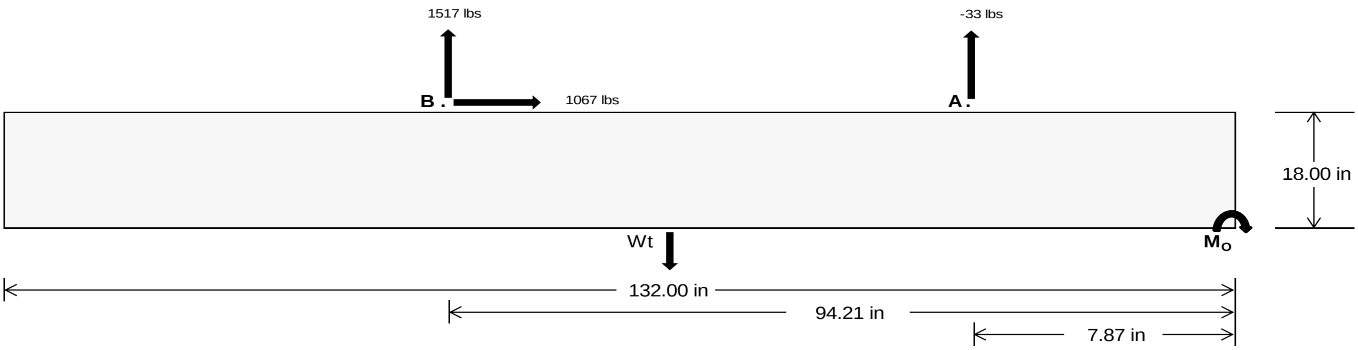
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	68.29	6591.43	k
Compressive Load =	2851.99	5008.16	k
Lateral Load =	374.39	4625.59	k
Moment (Weak Axis) =	0.71	0.21	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties		Footing Reinforcement	
Weight of Concrete =	145 pcf	*Use fiber reinforcing with (2) #5 rebar.*	
Compressive Strength =	2500 psi		
Yield Strength =	60000 psi		

Overturning Check

M_O =	161879.6 in-lbs
Resisting Force Required =	2452.72 lbs
S.F. =	1.67
Weight Required =	4087.87 lbs
Minimum Width =	32 in in
Weight Provided =	6380.00 lbs

A minimum 132in long x 32in wide x 18in tall ballast foundation is required to resist overturning.

Sliding

Force =	1066.93 lbs
Friction =	0.4
Weight Required =	2667.33 lbs
Resisting Weight =	6380.00 lbs
Additional Weight Required =	0 lbs

Use a 132in long x 32in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion

Sliding Force =	1066.93 lbs
Cohesion =	130 psf
Area =	29.33 ft^2
Resisting =	3190.00 lbs
Additional Weight Required =	0 lbs

Use a 132in long x 32in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	32 in	33 in	34 in	35 in
P_{ftg} = (145 pcf)(11 ft)(1.5 ft)(2.67 ft) =	6380 lbs	6579 lbs	6779 lbs	6978 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	32 in	33 in	34 in	35 in	32 in	33 in	34 in	35 in	32 in	33 in	34 in	35 in	32 in	33 in	34 in	35 in
F_A	1022 lbs	1022 lbs	1022 lbs	1022 lbs	1045 lbs	1045 lbs	1045 lbs	1045 lbs	1424 lbs	1424 lbs	1424 lbs	1424 lbs	66 lbs	66 lbs	66 lbs	66 lbs
F_B	916 lbs	916 lbs	916 lbs	916 lbs	2167 lbs	2167 lbs	2167 lbs	2167 lbs	2200 lbs	2200 lbs	2200 lbs	2200 lbs	-3034 lbs	-3034 lbs	-3034 lbs	-3034 lbs
F_V	162 lbs	162 lbs	162 lbs	162 lbs	1945 lbs	1945 lbs	1945 lbs	1945 lbs	1562 lbs	1562 lbs	1562 lbs	1562 lbs	-2134 lbs	-2134 lbs	-2134 lbs	-2134 lbs
P_{total}	8318 lbs	8518 lbs	8717 lbs	8916 lbs	9592 lbs	9792 lbs	9991 lbs	10190 lbs	10004 lbs	10203 lbs	10403 lbs	10602 lbs	860 lbs	980 lbs	1099 lbs	1219 lbs
M	3039 lbs-ft	3039 lbs-ft	3039 lbs-ft	3039 lbs-ft	2888 lbs-ft	2888 lbs-ft	2888 lbs-ft	2888 lbs-ft	4071 lbs-ft	4071 lbs-ft	4071 lbs-ft	4071 lbs-ft	4254 lbs-ft	4254 lbs-ft	4254 lbs-ft	4254 lbs-ft
e	0.37 ft	0.36 ft	0.35 ft	0.34 ft	0.30 ft	0.29 ft	0.29 ft	0.28 ft	0.41 ft	0.40 ft	0.39 ft	0.38 ft	4.95 ft	4.34 ft	3.87 ft	3.49 ft
L/6	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft
f_{min}	227.1 psf	226.8 psf	226.5 psf	226.3 psf	273.3 psf	271.6 psf	270.0 psf	268.5 psf	265.3 psf	263.9 psf	262.5 psf	261.2 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	340.1 psf	336.4 psf	332.9 psf	329.6 psf	380.7 psf	375.8 psf	371.1 psf	366.7 psf	416.7 psf	410.7 psf	405.0 psf	399.7 psf	388.6 psf	205.2 psf	158.7 psf	138.6 psf

Maximum Bearing Pressure = 417 psf
Allowable Bearing Pressure = 1500 psf

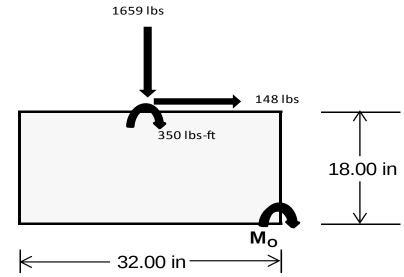
Use a 132in long x 32in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 1640.2 ft-lbs
Resisting Force Required = 1230.15 lbs
S.F. = 1.67
Weight Required = 2050.25 lbs
Minimum Width = 32 in in
Weight Provided = 6380.00 lbs

A minimum 132in long x 32in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	32 in			32 in			32 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	303 lbs	592 lbs	187 lbs	669 lbs	1659 lbs	581 lbs	129 lbs	173 lbs	14 lbs
F_V	204 lbs	200 lbs	208 lbs	149 lbs	148 lbs	161 lbs	205 lbs	201 lbs	206 lbs
P_{total}	8201 lbs	8491 lbs	8085 lbs	8188 lbs	9178 lbs	8100 lbs	2439 lbs	2483 lbs	2324 lbs
M	769 lbs-ft	758 lbs-ft	783 lbs-ft	570 lbs-ft	572 lbs-ft	609 lbs-ft	770 lbs-ft	757 lbs-ft	775 lbs-ft
e	0.09 ft	0.09 ft	0.10 ft	0.07 ft	0.06 ft	0.08 ft	0.32 ft	0.30 ft	0.33 ft
L/6	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft	0.44 ft
f_{min}	220.6 psf	231.3 psf	215.5 psf	235.4 psf	269.0 psf	229.4 psf	24.1 psf	26.6 psf	19.8 psf
f_{max}	338.5 psf	347.6 psf	335.7 psf	322.9 psf	356.7 psf	322.9 psf	142.2 psf	142.7 psf	138.6 psf

Maximum Bearing Pressure = 357 psf
Allowable Bearing Pressure = 1500 psf

Use a 132in long x 32in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 132in long x 32in wide x 18in tall ballast foundation and fiber reinforcing with (2) #5 rebar.

5.3 Foundation Anchors

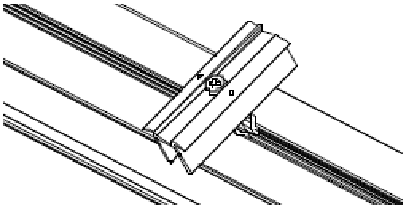
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

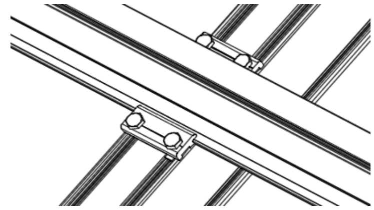
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.673	k
Allowable Uplift =	1.214	k
Utilization =	55%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	2.287	k
Allowable Uplift =	4.357	k
Utilization =	52%	



6.2 Strut Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	2.194	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	30%	

Rear Strut		
Maximum Axial Load =	4.346	k
M12 Bolt Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	59%	

Diagonal Strut		
Maximum Axial Load =	2.909	k
M12 Bolt Shear Capacity =	12.808	k
Strut Bearing Capacity =	7.421	k
Utilization =	39%	

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

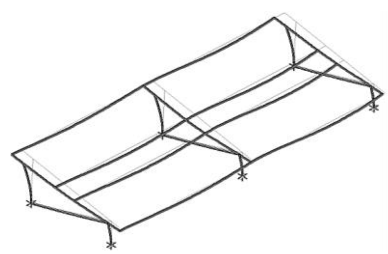
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	53.78	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	1.076	in
Max Drift, Δ_{MAX} =	0.649	in

$0.649 \le 1.076$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:
3.4.14
L_b = 114 in
J = 0.432
315.377

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 27.5 ksi

3.4.16
b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

3.4.16.1 Not Used
Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0
φF_L= 1.17φyFcy
φF_L= 38.9 ksi

3.4.18
h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 40.985
Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2
φF_L= φb[Bbr-mDbr*h/t]
φF_L= 43.2 ksi

$\varphi F_L St$= 25.1 ksi
Ix = 897074 mm^4
2.155 in^4
y = 41.015 mm
Sx = 1.335 in^3
$M_{max}St$ = 2.788 k-ft

Weak Axis:
3.4.14
L_b = 114
J = 0.432
200.561

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 28.8

3.4.16
b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 23.1 ksi

3.4.16.1
N/A for Weak Direction

3.4.18
h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 45.5
Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

$\varphi F_L Wk$= 23.1 ksi
Iy = 446476 mm^4
1.073 in^4
x = 45.5 mm
Sy = 0.599 in^3
$M_{max}Wk$ = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:

3.4.14

L_b = 88.9 in
J = 1.08
152.913

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.4 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

Weak Axis:

3.4.14

L_b = 88.9
J = 1.08
161.829

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.2

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Used

Rb/t = 18.1

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

$\varphi F_L = \varphi b[Bt-Dt*\sqrt{(Rb/t)}]$

$\varphi F_L =$ 31.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 35.2

m = 0.68

$C_0 =$ 41.067

Cc = 43.717

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 73.8

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

3.4.18

h/t = 16.2

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

$C_0 =$ 40

Cc = 40

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L St =$	29.4	ksi	$\varphi F_L Wk =$	33.3	ksi
Ix =	984962	mm^4	Iy =	923544	mm^4
	2.366	in^4		2.219	in^4
y =	43.717	mm	x =	40	mm
Sx =	1.375	in^3	Sy =	1.409	in^3
$M_{max}St =$	3.363	k-ft	$M_{max}Wk =$	3.904	k-ft

Compression

3.4.9

b/t = 16.2

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 31.6 ksi

b/t = 7.4

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi c[Bt-Dt*\sqrt{(Rb/t)}]$

$\varphi F_L =$ 31.09 ksi

$\varphi F_L =$ 31.09 ksi

A = 1215.13 mm^2

1.88 in^2

$P_{max} =$ 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:
3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

Weak Axis:
3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.87952

φF_L= φcc(Bc-Dc*λ)

φF_L= 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 86.60 in

J = 0.942

135.148

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6 ksi

Weak Axis:

3.4.14

L_b = 86.6

J = 0.942

135.148

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

$\varphi F_L = 1.17\varphi yFcy$

$\varphi F_L =$ 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L St =$ 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St =$ 1.460 k-ft

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$

$\varphi F_L =$ 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L Wk =$ 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk =$ 1.460 k-ft

Compression

3.4.7

λ = 2.00335

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.86047

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

$\varphi F_L =$ 7.50396 ksi

3.4.9

b/t = 24.5
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

b/t = 24.5
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 7.50 ksi
A = 663.99 mm^2
1.03 in^2
P_{max} = 7.72 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = <u>**55x55**</u>

<u>Strong Axis:</u>

3.4.14

L_b = 78.03 in
J = 0.942
121.773

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.8 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

<u>Weak Axis:</u>

3.4.14

L_b = 78.03
J = 0.942
121.773

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.8

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.80509

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83271

φF_L= (φccFcy)/(λ²)

φF_L= 8.94465 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 8.94 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 9.21 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M14	Y	-8.366	-8.366	0	0
3	M15	Y	-8.366	-8.366	0	0
4	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M14	Y	-4.45	-4.45	0	0
3	M15	Y	-4.45	-4.45	0	0
4	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-32.97	-32.97	0	0
2	M14	Y	-32.97	-32.97	0	0
3	M15	Y	-32.97	-32.97	0	0
4	M16	Y	-32.97	-32.97	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-88.797	-88.797	0	0
2	M14	y	-88.797	-88.797	0	0
3	M15	y	-147.995	-147.995	0	0
4	M16	y	-147.995	-147.995	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	199.793	199.793	0	0
2	M14	y	155.395	155.395	0	0
3	M15	y	88.797	88.797	0	0
4	M16	y	88.797	88.797	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M14	Z	6.693	6.693	0	0
3	M15	Z	6.693	6.693	0	0
4	M16	Z	6.693	6.693	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	937.365	2	1189.692	2	.568	1	.002	1	0	1	0	1
2		min	-1124.19	3	-1560.862	3	-23.839	5	-.162	4	0	1	0	1
3	N7	max	.034	3	887.292	1	-.756	12	-.001	12	0	1	0	1
4		min	-.192	2	-52.528	5	-287.989	4	-.543	4	0	1	0	1
5	N15	max	.226	3	2193.841	1	0	1	0	1	0	1	0	1
6		min	-1.968	2	90.932	15	-274.05	4	-.523	4	0	1	0	1
7	N16	max	3288.719	2	3852.427	2	0	11	0	1	0	1	0	1
8		min	-3558.146	3	-5070.334	3	-23.884	5	-.164	4	0	1	0	1
9	N23	max	.036	14	887.292	1	10.731	1	.02	1	0	1	0	1
10		min	-.192	2	66.208	12	-279.522	5	-.529	4	0	1	0	1
11	N24	max	937.365	2	1189.692	2	-.046	12	0	12	0	1	0	1
12		min	-1124.19	3	-1560.862	3	-24.486	5	-.164	4	0	1	0	1
13	Totals:	max	5161.096	2	9672.25	2	0	1						
14		min	-5806.233	3	-7773.578	3	-908.79	4						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	97.327	1	393.491	2	-10.32	12	.001	3	.233	1	0	4
2			min	7.242	12	-696.355	3	-168.538	1	-.013	2	.017	12	0	3
3		2	max	97.327	1	275.265	2	-8.158	12	.001	3	.125	4	.626	3
4			min	7.242	12	-490.096	3	-129.429	1	-.013	2	.008	12	-.353	2
5		3	max	97.327	1	157.04	2	-5.995	12	.001	3	.068	5	1.035	3
6			min	7.242	12	-283.837	3	-90.32	1	-.013	2	-.041	1	-.581	2
7		4	max	97.327	1	38.815	2	-3.832	12	.001	3	.035	5	1.225	3
8			min	7.242	12	-77.578	3	-51.21	1	-.013	2	-.115	1	-.684	2
9		5	max	97.327	1	128.682	3	-1.201	10	.001	3	.005	5	1.198	3
10			min	7.242	12	-79.41	2	-29.914	4	-.013	2	-.149	1	-.663	2
11		6	max	97.327	1	334.941	3	27.008	1	.001	3	-.009	12	.954	3
12			min	2.264	15	-197.636	2	-23.019	5	-.013	2	-.141	1	-.517	2
13		7	max	97.327	1	541.2	3	66.117	1	.001	3	-.007	12	.491	3
14			min	-7.146	5	-315.861	2	-19.673	5	-.013	2	-.092	1	-.246	2
15		8	max	97.327	1	747.459	3	105.226	1	.001	3	.002	2	.15	2
16			min	-17.982	5	-434.086	2	-16.326	5	-.013	2	-.064	4	-.189	3
17		9	max	97.327	1	953.718	3	144.336	1	.001	3	.13	1	.671	2
18			min	-28.817	5	-552.312	2	-12.98	5	-.013	2	-.078	5	-1.087	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	97.327	1	670.537	2	-9.146	12	.013	2	.303	1	1.316	2
20			min	7.242	12	-1159.977	3	-183.445	1	-.001	3	.012	12	-2.202	3
21		11	max	97.327	1	552.312	2	-6.983	12	.013	2	.133	4	.671	2
22			min	7.242	12	-953.718	3	-144.336	1	-.001	3	.003	12	-1.087	3
23		12	max	97.327	1	434.086	2	-4.82	12	.013	2	.062	4	.15	2
24			min	7.242	12	-747.459	3	-105.226	1	-.001	3	-.005	3	-.189	3
25		13	max	97.327	1	315.861	2	-2.657	12	.013	2	.028	5	.491	3
26			min	7.242	12	-541.2	3	-66.117	1	-.001	3	-.092	1	-.246	2
27		14	max	97.327	1	197.636	2	-.494	12	.013	2	-.002	15	.954	3
28			min	7.242	12	-334.941	3	-34.524	4	-.001	3	-.141	1	-.517	2
29		15	max	97.327	1	79.41	2	12.101	1	.013	2	-.008	12	1.198	3
30			min	1.256	15	-128.682	3	-24.189	5	-.001	3	-.149	1	-.663	2
31		16	max	97.327	1	77.578	3	51.21	1	.013	2	-.005	12	1.225	3
32			min	-8.689	5	-38.815	2	-20.842	5	-.001	3	-.115	1	-.684	2
33		17	max	97.327	1	283.837	3	90.32	1	.013	2	0	3	1.035	3
34			min	-19.524	5	-157.04	2	-17.496	5	-.001	3	-.086	4	-.581	2
35		18	max	97.327	1	490.096	3	129.429	1	.013	2	.075	1	.626	3
36			min	-30.36	5	-275.265	2	-14.149	5	-.001	3	-.091	5	-.353	2
37		19	max	97.327	1	696.355	3	168.538	1	.013	2	.233	1	0	2
38			min	-41.195	5	-393.491	2	-10.803	5	-.001	3	-.104	5	0	3
39	M14	1	max	52.77	4	423.948	2	-10.61	12	.009	3	.278	4	0	4
40			min	3.13	12	-557.707	3	-173.992	1	-.01	2	.019	12	0	3
41		2	max	46.561	1	305.722	2	-8.447	12	.009	3	.182	4	.505	3
42			min	3.13	12	-398.313	3	-134.883	1	-.01	2	.009	12	-.385	2
43		3	max	46.561	1	187.497	2	-6.284	12	.009	3	.102	5	.841	3
44			min	3.13	12	-238.918	3	-95.774	1	-.01	2	-.018	1	-.645	2
45		4	max	46.561	1	69.272	2	-4.121	12	.009	3	.054	5	1.009	3
46			min	3.13	12	-79.524	3	-58.423	4	-.01	2	-.098	1	-.781	2
47		5	max	46.561	1	79.871	3	-1.958	12	.009	3	.01	5	1.009	3
48			min	-2.323	5	-48.953	2	-45.228	4	-.01	2	-.137	1	-.792	2
49		6	max	46.561	1	239.266	3	21.554	1	.009	3	-.008	12	.84	3
50			min	-13.159	5	-167.179	2	-36.757	5	-.01	2	-.135	1	-.678	2
51		7	max	46.561	1	398.66	3	60.663	1	.009	3	-.007	12	.504	3
52			min	-23.994	5	-285.404	2	-33.411	5	-.01	2	-.092	1	-.439	2
53		8	max	46.561	1	558.055	3	99.772	1	.009	3	0	10	-.001	15
54			min	-34.83	5	-403.629	2	-30.064	5	-.01	2	-.105	4	-.075	2
55		9	max	46.561	1	717.449	3	138.881	1	.009	3	.119	1	.413	2
56			min	-45.665	5	-521.855	2	-26.718	5	-.01	2	-.131	5	-.674	3
57		10	max	76	4	640.08	2	-8.856	12	.01	2	.286	1	1.027	2
58			min	3.13	12	-876.844	3	-177.99	1	-.009	3	.011	12	-1.516	3
59		11	max	65.164	4	521.855	2	-6.693	12	.01	2	.182	4	.413	2
60			min	3.13	12	-717.449	3	-138.881	1	-.009	3	.003	12	-.674	3
61		12	max	54.329	4	403.629	2	-4.531	12	.01	2	.099	5	-.001	15
62			min	3.13	12	-558.055	3	-99.772	1	-.009	3	-.007	1	-.075	2
63		13	max	46.561	1	285.404	2	-2.368	12	.01	2	.052	5	.504	3
64			min	3.13	12	-398.66	3	-60.663	1	-.009	3	-.092	1	-.439	2
65		14	max	46.561	1	167.179	2	-.15	3	.01	2	.007	5	.84	3
66			min	3.13	12	-239.266	3	-46.151	4	-.009	3	-.135	1	-.678	2
67		15	max	46.561	1	48.953	2	17.556	1	.01	2	-.007	12	1.009	3
68			min	3.13	12	-79.871	3	-36.992	5	-.009	3	-.137	1	-.792	2
69		16	max	46.561	1	79.524	3	56.665	1	.01	2	-.004	12	1.009	3
70			min	-.95	5	-69.272	2	-33.645	5	-.009	3	-.098	1	-.781	2
71		17	max	46.561	1	238.918	3	95.774	1	.01	2	.003	3	.841	3
72			min	-11.786	5	-187.497	2	-30.299	5	-.009	3	-.11	4	-.645	2
73		18	max	46.561	1	398.313	3	134.883	1	.01	2	.104	1	.505	3
74			min	-22.621	5	-305.722	2	-26.952	5	-.009	3	-.135	5	-.385	2
75		19	max	46.561	1	557.707	3	173.992	1	.01	2	.267	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-33.457	5	-423.948	2	-23.606	5	-.009	3	-.162	5	0	3
77	M15	1	max	82.104	5	634.862	2	-10.531	12	.011	2	.328	4	0	2
78			min	-48.705	1	-320.61	3	-173.979	1	-.008	3	.019	12	0	3
79		2	max	71.269	5	454.15	2	-8.368	12	.011	2	.221	4	.291	3
80			min	-48.705	1	-231.513	3	-134.869	1	-.008	3	.009	12	-.575	2
81		3	max	60.433	5	273.438	2	-6.205	12	.011	2	.13	5	.489	3
82			min	-48.705	1	-142.417	3	-95.76	1	-.008	3	-.018	1	-.959	2
83		4	max	49.598	5	92.726	2	-4.042	12	.011	2	.071	5	.592	3
84			min	-48.705	1	-53.32	3	-68.726	4	-.008	3	-.098	1	-1.152	2
85		5	max	38.762	5	35.777	3	-1.879	12	.011	2	.016	5	.601	3
86			min	-48.705	1	-87.987	2	-55.531	4	-.008	3	-.138	1	-1.155	2
87		6	max	27.927	5	124.873	3	21.567	1	.011	2	-.008	12	.517	3
88			min	-48.705	1	-268.699	2	-47.014	5	-.008	3	-.135	1	-.966	2
89		7	max	17.091	5	213.97	3	60.677	1	.011	2	-.007	12	.338	3
90			min	-48.705	1	-449.411	2	-43.668	5	-.008	3	-.107	4	-.587	2
91		8	max	6.256	5	303.067	3	99.786	1	.011	2	0	10	.065	3
92			min	-48.705	1	-630.123	2	-40.321	5	-.008	3	-.131	4	-.024	1
93		9	max	-2.948	15	392.163	3	138.895	1	.011	2	.119	1	.743	2
94			min	-48.705	1	-810.835	2	-36.975	5	-.008	3	-.168	5	-.302	3
95		10	max	-3.731	12	991.547	2	-8.936	12	.008	3	.328	4	1.694	2
96			min	-48.705	1	-481.26	3	-178.004	1	-.011	2	.011	12	-.763	3
97		11	max	-2.771	15	810.835	2	-6.773	12	.008	3	.22	4	.743	2
98			min	-48.705	1	-392.163	3	-138.895	1	-.011	2	.003	12	-.302	3
99		12	max	-3.731	12	630.123	2	-4.61	12	.008	3	.126	5	.065	3
100			min	-48.705	1	-303.067	3	-99.786	1	-.011	2	-.007	1	-.024	1
101		13	max	-3.731	12	449.411	2	-2.447	12	.008	3	.067	5	.338	3
102			min	-48.705	1	-213.97	3	-69.68	4	-.011	2	-.092	1	-.587	2
103		14	max	-3.731	12	268.699	2	-.281	3	.008	3	.012	5	.517	3
104			min	-49.881	4	-124.873	3	-56.485	4	-.011	2	-.135	1	-.966	2
105		15	max	-3.731	12	87.987	2	17.542	1	.008	3	-.007	12	.601	3
106			min	-60.716	4	-35.777	3	-47.255	5	-.011	2	-.138	1	-1.155	2
107		16	max	-3.731	12	53.32	3	56.651	1	.008	3	-.004	12	.592	3
108			min	-71.552	4	-92.726	2	-43.908	5	-.011	2	-.113	4	-1.152	2
109		17	max	-3.731	12	142.417	3	95.76	1	.008	3	.002	3	.489	3
110			min	-82.387	4	-273.438	2	-40.562	5	-.011	2	-.138	4	-.959	2
111		18	max	-3.731	12	231.513	3	134.869	1	.008	3	.104	1	.291	3
112			min	-93.223	4	-454.15	2	-37.215	5	-.011	2	-.173	5	-.575	2
113		19	max	-3.731	12	320.61	3	173.979	1	.008	3	.267	1	0	2
114			min	-104.058	4	-634.862	2	-33.869	5	-.011	2	-.211	5	0	5
115	M16	1	max	80.14	5	605.619	2	-10.057	12	.009	2	.262	4	0	2
116			min	-105.348	1	-295.48	3	-168.826	1	-.012	3	.016	12	0	3
117		2	max	69.305	5	424.907	2	-7.894	12	.009	2	.169	4	.265	3
118			min	-105.348	1	-206.384	3	-129.717	1	-.012	3	.007	12	-.544	2
119		3	max	58.469	5	244.195	2	-5.731	12	.009	2	.099	5	.436	3
120			min	-105.348	1	-117.287	3	-90.608	1	-.012	3	-.04	1	-.897	2
121		4	max	47.634	5	63.483	2	-3.568	12	.009	2	.054	5	.512	3
122			min	-105.348	1	-28.19	3	-54.461	4	-.012	3	-.115	1	-1.059	2
123		5	max	36.798	5	60.906	3	-1.376	10	.009	2	.013	5	.495	3
124			min	-105.348	1	-117.229	2	-41.266	4	-.012	3	-.148	1	-1.031	2
125		6	max	25.963	5	150.003	3	26.72	1	.009	2	-.008	12	.384	3
126			min	-105.348	1	-297.941	2	-34.218	5	-.012	3	-.141	1	-.812	2
127		7	max	15.127	5	239.1	3	65.829	1	.009	2	-.006	12	.179	3
128			min	-105.348	1	-478.653	2	-30.871	5	-.012	3	-.092	1	-.402	2
129		8	max	4.292	5	328.196	3	104.938	1	.009	2	.001	2	.199	2
130			min	-105.348	1	-659.365	2	-27.525	5	-.012	3	-.092	4	-.121	3
131		9	max	-4.204	15	417.293	3	144.048	1	.009	2	.129	1	.99	2
132			min	-105.348	1	-840.077	2	-24.179	5	-.012	3	-.117	5	-.514	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-7.351	12	1020.789	2	-9.41	12	.012	3	.302	1	1.972	2
134			min	-105.348	1	-506.39	3	-183.157	1	-.009	2	.013	12	-1.002	3
135		11	max	-7.351	12	840.077	2	-7.247	12	.012	3	.173	4	.99	2
136			min	-105.348	1	-417.293	3	-144.048	1	-.009	2	.004	12	-.514	3
137		12	max	-7.351	12	659.365	2	-5.084	12	.012	3	.09	4	.199	2
138			min	-105.348	1	-328.196	3	-104.938	1	-.009	2	-.004	3	-.121	3
139		13	max	-7.351	12	478.653	2	-2.921	12	.012	3	.043	5	.179	3
140			min	-105.348	1	-239.1	3	-65.829	1	-.009	2	-.092	1	-.402	2
141		14	max	-7.351	12	297.941	2	-.758	12	.012	3	0	15	.384	3
142			min	-105.348	1	-150.003	3	-45.772	4	-.009	2	-.141	1	-.812	2
143		15	max	-7.351	12	117.229	2	12.389	1	.012	3	-.008	12	.495	3
144			min	-105.348	1	-60.906	3	-35.365	5	-.009	2	-.148	1	-1.031	2
145		16	max	-7.351	12	28.19	3	51.498	1	.012	3	-.005	12	.512	3
146			min	-105.348	1	-63.483	2	-32.018	5	-.009	2	-.115	1	-1.059	2
147		17	max	-7.351	12	117.287	3	90.608	1	.012	3	0	3	.436	3
148			min	-105.348	1	-244.195	2	-28.672	5	-.009	2	-.117	4	-.897	2
149		18	max	-7.351	12	206.384	3	129.717	1	.012	3	.077	1	.265	3
150			min	-115.108	4	-424.907	2	-25.326	5	-.009	2	-.134	5	-.544	2
151		19	max	-7.351	12	295.48	3	168.826	1	.012	3	.234	1	0	2
152			min	-125.944	4	-605.619	2	-21.979	5	-.009	2	-.159	5	0	5
153	M2	1	max	968.978	2	2.041	4	.33	1	0	3	0	3	0	1
154			min	-1337.133	3	.49	15	-22.944	4	0	4	0	2	0	1
155		2	max	969.498	2	1.922	4	.33	1	0	3	0	1	0	15
156			min	-1336.743	3	.462	15	-23.402	4	0	4	-.008	4	0	4
157		3	max	970.019	2	1.803	4	.33	1	0	3	0	1	0	15
158			min	-1336.352	3	.434	15	-23.86	4	0	4	-.017	4	-.001	4
159		4	max	970.54	2	1.684	4	.33	1	0	3	0	1	0	15
160			min	-1335.962	3	.406	15	-24.319	4	0	4	-.025	4	-.002	4
161		5	max	971.06	2	1.565	4	.33	1	0	3	0	1	0	15
162			min	-1335.571	3	.378	15	-24.777	4	0	4	-.034	4	-.003	4
163		6	max	971.581	2	1.446	4	.33	1	0	3	0	1	0	15
164			min	-1335.181	3	.35	15	-25.235	4	0	4	-.043	4	-.003	4
165		7	max	972.102	2	1.328	4	.33	1	0	3	0	1	0	15
166			min	-1334.79	3	.322	15	-25.694	4	0	4	-.052	4	-.004	4
167		8	max	972.622	2	1.209	4	.33	1	0	3	0	1	0	15
168			min	-1334.4	3	.294	15	-26.152	4	0	4	-.061	4	-.004	4
169		9	max	973.143	2	1.09	4	.33	1	0	3	0	1	-.001	15
170			min	-1334.009	3	.254	12	-26.61	4	0	4	-.071	4	-.004	4
171		10	max	973.664	2	.971	4	.33	1	0	3	.001	1	-.001	15
172			min	-1333.619	3	.208	12	-27.069	4	0	4	-.08	4	-.005	4
173		11	max	974.185	2	.852	4	.33	1	0	3	.001	1	-.001	15
174			min	-1333.228	3	.162	12	-27.527	4	0	4	-.09	4	-.005	4
175		12	max	974.705	2	.75	2	.33	1	0	3	.001	1	-.001	15
176			min	-1332.838	3	.115	12	-27.985	4	0	4	-.1	4	-.005	4
177		13	max	975.226	2	.657	2	.33	1	0	3	.001	1	-.001	15
178			min	-1332.447	3	.069	12	-28.444	4	0	4	-.11	4	-.006	4
179		14	max	975.747	2	.564	2	.33	1	0	3	.002	1	-.001	15
180			min	-1332.057	3	.007	3	-28.902	4	0	4	-.12	4	-.006	4
181		15	max	976.267	2	.472	2	.33	1	0	3	.002	1	-.001	15
182			min	-1331.666	3	-.063	3	-29.36	4	0	4	-.131	4	-.006	4
183		16	max	976.788	2	.379	2	.33	1	0	3	.002	1	-.001	12
184			min	-1331.276	3	-.132	3	-29.819	4	0	4	-.141	4	-.006	4
185		17	max	977.309	2	.287	2	.33	1	0	3	.002	1	-.001	12
186			min	-1330.885	3	-.201	3	-30.277	4	0	4	-.152	4	-.006	4
187		18	max	977.829	2	.194	2	.33	1	0	3	.002	1	-.001	12
188			min	-1330.495	3	-.271	3	-30.736	4	0	4	-.163	4	-.006	4
189		19	max	978.35	2	.101	2	.33	1	0	3	.002	1	-.001	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-1330.104	3	-.34	3	-31.194	4	0	4	-.174	4	-.006	4
191	M3	1	max	798.798	2	7.681	4	6.726	4	0	12	0	1	.006	4
192			min	-925.452	3	1.814	15	.021	12	0	4	-.032	4	.001	12
193		2	max	798.627	2	6.92	4	7.261	4	0	12	0	1	.004	2
194			min	-925.58	3	1.635	15	.021	12	0	4	-.029	4	0	3
195		3	max	798.457	2	6.159	4	7.796	4	0	12	0	1	.001	2
196			min	-925.708	3	1.457	15	.021	12	0	4	-.026	4	-.001	3
197		4	max	798.287	2	5.398	4	8.33	4	0	12	0	1	0	15
198			min	-925.836	3	1.278	15	.021	12	0	4	-.022	4	-.003	3
199		5	max	798.116	2	4.637	4	8.865	4	0	12	0	1	0	15
200			min	-925.963	3	1.099	15	.021	12	0	4	-.019	5	-.004	6
201		6	max	797.946	2	3.876	4	9.4	4	0	12	.001	1	-.001	15
202			min	-926.091	3	.92	15	.021	12	0	4	-.015	5	-.006	6
203		7	max	797.776	2	3.115	4	9.934	4	0	12	.001	1	-.002	15
204			min	-926.219	3	.741	15	.021	12	0	4	-.011	5	-.007	6
205		8	max	797.605	2	2.354	4	10.469	4	0	12	.001	1	-.002	15
206			min	-926.347	3	.562	15	.021	12	0	4	-.007	5	-.008	6
207		9	max	797.435	2	1.593	4	11.004	4	0	12	.001	1	-.002	15
208			min	-926.474	3	.383	15	.021	12	0	4	-.003	5	-.009	6
209		10	max	797.264	2	.832	4	11.538	4	0	12	.003	4	-.002	15
210			min	-926.602	3	.178	12	.021	12	0	4	0	12	-.01	6
211		11	max	797.094	2	.209	2	12.073	4	0	12	.007	4	-.002	15
212			min	-926.73	3	-.201	3	.021	12	0	4	0	12	-.01	6
213		12	max	796.924	2	-.153	15	12.608	4	0	12	.013	4	-.002	15
214			min	-926.858	3	-.69	6	.021	12	0	4	0	12	-.01	6
215		13	max	796.753	2	-.332	15	13.142	4	0	12	.018	4	-.002	15
216			min	-926.985	3	-1.451	6	.021	12	0	4	0	12	-.009	6
217		14	max	796.583	2	-.511	15	13.677	4	0	12	.024	4	-.002	15
218			min	-927.113	3	-2.212	6	.021	12	0	4	0	12	-.009	6
219		15	max	796.413	2	-.69	15	14.212	4	0	12	.029	4	-.002	15
220			min	-927.241	3	-2.973	6	.021	12	0	4	0	12	-.007	6
221		16	max	796.242	2	-.869	15	14.747	4	0	12	.035	4	-.001	15
222			min	-927.369	3	-3.734	6	.021	12	0	4	0	12	-.006	6
223		17	max	796.072	2	-1.048	15	15.281	4	0	12	.042	4	-.001	15
224			min	-927.497	3	-4.495	6	.021	12	0	4	0	12	-.004	6
225		18	max	795.902	2	-1.227	15	15.816	4	0	12	.048	4	0	15
226			min	-927.624	3	-5.256	6	.021	12	0	4	0	12	-.002	6
227		19	max	795.731	2	-1.406	15	16.351	4	0	12	.055	4	0	1
228			min	-927.752	3	-6.017	6	.021	12	0	4	0	12	0	1
229	M4	1	max	884.225	1	0	1	-.758	12	0	1	.052	4	0	1
230			min	-53.959	5	0	1	-286.362	4	0	1	0	12	0	1
231		2	max	884.396	1	0	1	-.758	12	0	1	.019	4	0	1
232			min	-53.879	5	0	1	-286.51	4	0	1	0	12	0	1
233		3	max	884.566	1	0	1	-.758	12	0	1	0	3	0	1
234			min	-53.8	5	0	1	-286.657	4	0	1	-.014	4	0	1
235		4	max	884.736	1	0	1	-.758	12	0	1	0	12	0	1
236			min	-53.72	5	0	1	-286.805	4	0	1	-.047	4	0	1
237		5	max	884.907	1	0	1	-.758	12	0	1	0	12	0	1
238			min	-53.641	5	0	1	-286.952	4	0	1	-.08	4	0	1
239		6	max	885.077	1	0	1	-.758	12	0	1	0	12	0	1
240			min	-53.561	5	0	1	-287.1	4	0	1	-.113	4	0	1
241		7	max	885.247	1	0	1	-.758	12	0	1	0	12	0	1
242			min	-53.482	5	0	1	-287.248	4	0	1	-.146	4	0	1
243		8	max	885.418	1	0	1	-.758	12	0	1	0	12	0	1
244			min	-53.402	5	0	1	-287.395	4	0	1	-.179	4	0	1
245		9	max	885.588	1	0	1	-.758	12	0	1	0	12	0	1
246			min	-53.323	5	0	1	-287.543	4	0	1	-.212	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	885.758	1	0	1	-.758	12	0	1	0	12	0	1
248			min	-53.243	5	0	1	-287.691	4	0	1	-.245	4	0	1
249		11	max	885.929	1	0	1	-.758	12	0	1	0	12	0	1
250			min	-53.164	5	0	1	-287.838	4	0	1	-.278	4	0	1
251		12	max	886.099	1	0	1	-.758	12	0	1	0	12	0	1
252			min	-53.084	5	0	1	-287.986	4	0	1	-.311	4	0	1
253		13	max	886.27	1	0	1	-.758	12	0	1	0	12	0	1
254			min	-53.005	5	0	1	-288.134	4	0	1	-.344	4	0	1
255		14	max	886.44	1	0	1	-.758	12	0	1	0	12	0	1
256			min	-52.925	5	0	1	-288.281	4	0	1	-.377	4	0	1
257		15	max	886.61	1	0	1	-.758	12	0	1	-.001	12	0	1
258			min	-52.846	5	0	1	-288.429	4	0	1	-.41	4	0	1
259		16	max	886.781	1	0	1	-.758	12	0	1	-.001	12	0	1
260			min	-52.766	5	0	1	-288.576	4	0	1	-.443	4	0	1
261		17	max	886.951	1	0	1	-.758	12	0	1	-.001	12	0	1
262			min	-52.687	5	0	1	-288.724	4	0	1	-.476	4	0	1
263		18	max	887.121	1	0	1	-.758	12	0	1	-.001	12	0	1
264			min	-52.607	5	0	1	-288.872	4	0	1	-.51	4	0	1
265		19	max	887.292	1	0	1	-.758	12	0	1	-.001	12	0	1
266			min	-52.528	5	0	1	-289.019	4	0	1	-.543	4	0	1
267	M6	1	max	3095.19	2	2.248	2	0	1	0	1	0	4	0	1
268			min	-4346.398	3	.27	12	-23.195	4	0	4	0	1	0	1
269		2	max	3095.711	2	2.156	2	0	1	0	1	0	1	0	12
270			min	-4346.008	3	.224	12	-23.653	4	0	4	-.008	4	0	2
271		3	max	3096.231	2	2.063	2	0	1	0	1	0	1	0	12
272			min	-4345.617	3	.177	12	-24.112	4	0	4	-.017	4	-.002	2
273		4	max	3096.752	2	1.97	2	0	1	0	1	0	1	0	12
274			min	-4345.227	3	.11	3	-24.57	4	0	4	-.026	4	-.002	2
275		5	max	3097.273	2	1.878	2	0	1	0	1	0	1	0	12
276			min	-4344.836	3	.04	3	-25.028	4	0	4	-.034	4	-.003	2
277		6	max	3097.793	2	1.785	2	0	1	0	1	0	1	0	3
278			min	-4344.446	3	-.029	3	-25.487	4	0	4	-.043	4	-.004	2
279		7	max	3098.314	2	1.693	2	0	1	0	1	0	1	0	3
280			min	-4344.055	3	-.099	3	-25.945	4	0	4	-.053	4	-.004	2
281		8	max	3098.835	2	1.6	2	0	1	0	1	0	1	0	3
282			min	-4343.665	3	-.168	3	-26.403	4	0	4	-.062	4	-.005	2
283		9	max	3099.356	2	1.507	2	0	1	0	1	0	1	0	3
284			min	-4343.274	3	-.238	3	-26.862	4	0	4	-.071	4	-.005	2
285		10	max	3099.876	2	1.415	2	0	1	0	1	0	1	0	3
286			min	-4342.884	3	-.307	3	-27.32	4	0	4	-.081	4	-.006	2
287		11	max	3100.397	2	1.322	2	0	1	0	1	0	1	0	3
288			min	-4342.493	3	-.377	3	-27.778	4	0	4	-.091	4	-.006	2
289		12	max	3100.918	2	1.229	2	0	1	0	1	0	1	0	3
290			min	-4342.102	3	-.446	3	-28.237	4	0	4	-.101	4	-.007	2
291		13	max	3101.438	2	1.137	2	0	1	0	1	0	1	0	3
292			min	-4341.712	3	-.516	3	-28.695	4	0	4	-.111	4	-.007	2
293		14	max	3101.959	2	1.044	2	0	1	0	1	0	1	0	3
294			min	-4341.321	3	-.585	3	-29.154	4	0	4	-.121	4	-.008	2
295		15	max	3102.48	2	.952	2	0	1	0	1	0	1	0	3
296			min	-4340.931	3	-.654	3	-29.612	4	0	4	-.132	4	-.008	2
297		16	max	3103	2	.859	2	0	1	0	1	0	1	.001	3
298			min	-4340.54	3	-.724	3	-30.07	4	0	4	-.142	4	-.008	2
299		17	max	3103.521	2	.766	2	0	1	0	1	0	1	.001	3
300			min	-4340.15	3	-.793	3	-30.529	4	0	4	-.153	4	-.009	2
301		18	max	3104.042	2	.674	2	0	1	0	1	0	1	.002	3
302			min	-4339.759	3	-.863	3	-30.987	4	0	4	-.164	4	-.009	2
303		19	max	3104.562	2	.581	2	0	1	0	1	0	1	.002	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-4339.369	3	-.932	3	-31.445	4	0	4	-.175	4	-.009	2
305	M7	1	max	2858.789	2	7.689	6	6.334	4	0	1	0	1	.009	2
306			min	-2906.469	3	1.806	15	0	1	0	4	-.032	4	-.002	3
307		2	max	2858.618	2	6.928	6	6.869	4	0	1	0	1	.006	2
308			min	-2906.597	3	1.627	15	0	1	0	4	-.029	4	-.003	3
309		3	max	2858.448	2	6.167	6	7.404	4	0	1	0	1	.004	2
310			min	-2906.725	3	1.448	15	0	1	0	4	-.026	4	-.005	3
311		4	max	2858.278	2	5.406	6	7.938	4	0	1	0	1	.002	2
312			min	-2906.852	3	1.269	15	0	1	0	4	-.023	4	-.006	3
313		5	max	2858.107	2	4.645	6	8.473	4	0	1	0	1	0	2
314			min	-2906.98	3	1.09	15	0	1	0	4	-.02	4	-.007	3
315		6	max	2857.937	2	3.884	6	9.008	4	0	1	0	1	-.001	15
316			min	-2907.108	3	.911	15	0	1	0	4	-.016	4	-.007	3
317		7	max	2857.767	2	3.123	6	9.542	4	0	1	0	1	-.002	15
318			min	-2907.236	3	.732	15	0	1	0	4	-.012	4	-.008	3
319		8	max	2857.596	2	2.399	2	10.077	4	0	1	0	1	-.002	15
320			min	-2907.363	3	.467	12	0	1	0	4	-.008	4	-.008	4
321		9	max	2857.426	2	1.806	2	10.612	4	0	1	0	1	-.002	15
322			min	-2907.491	3	.171	12	0	1	0	4	-.004	5	-.009	4
323		10	max	2857.256	2	1.213	2	11.147	4	0	1	0	4	-.002	15
324			min	-2907.619	3	-.263	3	0	1	0	4	0	1	-.01	4
325		11	max	2857.085	2	.62	2	11.681	4	0	1	.006	4	-.002	15
326			min	-2907.747	3	-.708	3	0	1	0	4	0	1	-.01	4
327		12	max	2856.915	2	.027	2	12.216	4	0	1	.01	4	-.002	15
328			min	-2907.874	3	-1.153	3	0	1	0	4	0	1	-.01	4
329		13	max	2856.745	2	-.341	15	12.751	4	0	1	.016	4	-.002	15
330			min	-2908.002	3	-1.597	3	0	1	0	4	0	1	-.009	4
331		14	max	2856.574	2	-.52	15	13.285	4	0	1	.021	4	-.002	15
332			min	-2908.13	3	-2.204	4	0	1	0	4	0	1	-.009	4
333		15	max	2856.404	2	-.699	15	13.82	4	0	1	.027	4	-.002	15
334			min	-2908.258	3	-2.965	4	0	1	0	4	0	1	-.007	4
335		16	max	2856.234	2	-.878	15	14.355	4	0	1	.033	4	-.001	15
336			min	-2908.385	3	-3.726	4	0	1	0	4	0	1	-.006	4
337		17	max	2856.063	2	-1.056	15	14.889	4	0	1	.039	4	-.001	15
338			min	-2908.513	3	-4.487	4	0	1	0	4	0	1	-.004	4
339		18	max	2855.893	2	-1.235	15	15.424	4	0	1	.045	4	0	15
340			min	-2908.641	3	-5.248	4	0	1	0	4	0	1	-.002	4
341		19	max	2855.723	2	-1.414	15	15.959	4	0	1	.051	4	0	1
342			min	-2908.769	3	-6.009	4	0	1	0	4	0	1	0	1
343	M8	1	max	2190.775	1	0	1	0	1	0	1	.049	4	0	1
344			min	90.007	15	0	1	-275.493	4	0	1	0	1	0	1
345		2	max	2190.946	1	0	1	0	1	0	1	.017	4	0	1
346			min	90.059	15	0	1	-275.64	4	0	1	0	1	0	1
347		3	max	2191.116	1	0	1	0	1	0	1	0	1	0	1
348			min	90.11	15	0	1	-275.788	4	0	1	-.014	4	0	1
349		4	max	2191.286	1	0	1	0	1	0	1	0	1	0	1
350			min	90.161	15	0	1	-275.936	4	0	1	-.046	4	0	1
351		5	max	2191.457	1	0	1	0	1	0	1	0	1	0	1
352			min	90.213	15	0	1	-276.083	4	0	1	-.078	4	0	1
353		6	max	2191.627	1	0	1	0	1	0	1	0	1	0	1
354			min	90.264	15	0	1	-276.231	4	0	1	-.109	4	0	1
355		7	max	2191.797	1	0	1	0	1	0	1	0	1	0	1
356			min	90.315	15	0	1	-276.379	4	0	1	-.141	4	0	1
357		8	max	2191.968	1	0	1	0	1	0	1	0	1	0	1
358			min	90.367	15	0	1	-276.526	4	0	1	-.173	4	0	1
359		9	max	2192.138	1	0	1	0	1	0	1	0	1	0	1
360			min	90.418	15	0	1	-276.674	4	0	1	-.205	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	2192.308	1	0	1	0	1	0	1	0	1	0	1
362			min	90.47	15	0	1	-276.821	4	0	1	-.237	4	0	1
363		11	max	2192.479	1	0	1	0	1	0	1	0	1	0	1
364			min	90.521	15	0	1	-276.969	4	0	1	-.268	4	0	1
365		12	max	2192.649	1	0	1	0	1	0	1	0	1	0	1
366			min	90.572	15	0	1	-277.117	4	0	1	-.3	4	0	1
367		13	max	2192.819	1	0	1	0	1	0	1	0	1	0	1
368			min	90.624	15	0	1	-277.264	4	0	1	-.332	4	0	1
369		14	max	2192.99	1	0	1	0	1	0	1	0	1	0	1
370			min	90.675	15	0	1	-277.412	4	0	1	-.364	4	0	1
371		15	max	2193.16	1	0	1	0	1	0	1	0	1	0	1
372			min	90.727	15	0	1	-277.56	4	0	1	-.396	4	0	1
373		16	max	2193.33	1	0	1	0	1	0	1	0	1	0	1
374			min	90.778	15	0	1	-277.707	4	0	1	-.428	4	0	1
375		17	max	2193.501	1	0	1	0	1	0	1	0	1	0	1
376			min	90.829	15	0	1	-277.855	4	0	1	-.459	4	0	1
377		18	max	2193.671	1	0	1	0	1	0	1	0	1	0	1
378			min	90.881	15	0	1	-278.002	4	0	1	-.491	4	0	1
379		19	max	2193.841	1	0	1	0	1	0	1	0	1	0	1
380			min	90.932	15	0	1	-278.15	4	0	1	-.523	4	0	1
381	M10	1	max	968.978	2	1.995	6	-.022	12	0	1	0	2	0	1
382			min	-1337.133	3	.459	15	-23.168	4	0	5	0	3	0	1
383		2	max	969.498	2	1.877	6	-.022	12	0	1	0	10	0	15
384			min	-1336.743	3	.431	15	-23.626	4	0	5	-.008	4	0	6
385		3	max	970.019	2	1.758	6	-.022	12	0	1	0	10	0	15
386			min	-1336.352	3	.403	15	-24.085	4	0	5	-.017	4	-.001	6
387		4	max	970.54	2	1.639	6	-.022	12	0	1	0	12	0	15
388			min	-1335.962	3	.375	15	-24.543	4	0	5	-.026	4	-.002	6
389		5	max	971.06	2	1.52	6	-.022	12	0	1	0	12	0	15
390			min	-1335.571	3	.348	15	-25.001	4	0	5	-.034	4	-.003	6
391		6	max	971.581	2	1.401	6	-.022	12	0	1	0	12	0	15
392			min	-1335.181	3	.32	15	-25.46	4	0	5	-.043	4	-.003	6
393		7	max	972.102	2	1.282	6	-.022	12	0	1	0	12	0	15
394			min	-1334.79	3	.292	15	-25.918	4	0	5	-.052	4	-.004	6
395		8	max	972.622	2	1.163	6	-.022	12	0	1	0	12	0	15
396			min	-1334.4	3	.264	15	-26.377	4	0	5	-.062	4	-.004	6
397		9	max	973.143	2	1.045	6	-.022	12	0	1	0	12	0	15
398			min	-1334.009	3	.236	15	-26.835	4	0	5	-.071	4	-.004	6
399		10	max	973.664	2	.935	2	-.022	12	0	1	0	12	-.001	15
400			min	-1333.619	3	.208	15	-27.293	4	0	5	-.081	4	-.005	6
401		11	max	974.185	2	.842	2	-.022	12	0	1	0	12	-.001	15
402			min	-1333.228	3	.162	12	-27.752	4	0	5	-.091	4	-.005	6
403		12	max	974.705	2	.75	2	-.022	12	0	1	0	12	-.001	15
404			min	-1332.838	3	.115	12	-28.21	4	0	5	-.101	4	-.005	6
405		13	max	975.226	2	.657	2	-.022	12	0	1	0	12	-.001	15
406			min	-1332.447	3	.069	12	-28.668	4	0	5	-.111	4	-.005	6
407		14	max	975.747	2	.564	2	-.022	12	0	1	0	12	-.001	15
408			min	-1332.057	3	.007	3	-29.127	4	0	5	-.121	4	-.006	6
409		15	max	976.267	2	.472	2	-.022	12	0	1	0	12	-.001	15
410			min	-1331.666	3	-.063	3	-29.585	4	0	5	-.132	4	-.006	6
411		16	max	976.788	2	.379	2	-.022	12	0	1	0	12	-.001	15
412			min	-1331.276	3	-.132	3	-30.043	4	0	5	-.142	4	-.006	6
413		17	max	977.309	2	.287	2	-.022	12	0	1	0	12	-.001	15
414			min	-1330.885	3	-.201	3	-30.502	4	0	5	-.153	4	-.006	6
415		18	max	977.829	2	.194	2	-.022	12	0	1	0	12	-.001	15
416			min	-1330.495	3	-.271	3	-30.96	4	0	5	-.164	4	-.006	6
417		19	max	978.35	2	.101	2	-.022	12	0	1	0	12	-.001	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-1330.104	3	-.34	3	-31.418	4	0	5	-.175	4	-.006	2
419	M11	1	max	798.798	2	7.642	6	6.522	4	0	1	0	12	.006	2
420			min	-925.452	3	1.788	15	-.3	1	0	4	-.032	4	.001	15
421		2	max	798.627	2	6.881	6	7.057	4	0	1	0	12	.004	2
422			min	-925.58	3	1.609	15	-.3	1	0	4	-.029	4	0	3
423		3	max	798.457	2	6.12	6	7.591	4	0	1	0	12	.001	2
424			min	-925.708	3	1.43	15	-.3	1	0	4	-.026	4	-.001	3
425		4	max	798.287	2	5.359	6	8.126	4	0	1	0	12	0	2
426			min	-925.836	3	1.251	15	-.3	1	0	4	-.023	4	-.003	3
427		5	max	798.116	2	4.598	6	8.661	4	0	1	0	12	-.001	15
428			min	-925.963	3	1.073	15	-.3	1	0	4	-.019	4	-.004	4
429		6	max	797.946	2	3.837	6	9.195	4	0	1	0	12	-.001	15
430			min	-926.091	3	.894	15	-.3	1	0	4	-.016	4	-.006	4
431		7	max	797.776	2	3.076	6	9.73	4	0	1	0	12	-.002	15
432			min	-926.219	3	.715	15	-.3	1	0	4	-.012	4	-.007	4
433		8	max	797.605	2	2.316	6	10.265	4	0	1	0	12	-.002	15
434			min	-926.347	3	.536	15	-.3	1	0	4	-.007	4	-.009	4
435		9	max	797.435	2	1.555	6	10.8	4	0	1	0	12	-.002	15
436			min	-926.474	3	.357	15	-.3	1	0	4	-.003	4	-.009	4
437		10	max	797.264	2	.801	2	11.334	4	0	1	.002	5	-.002	15
438			min	-926.602	3	.178	15	-.3	1	0	4	-.002	1	-.01	4
439		11	max	797.094	2	.209	2	11.869	4	0	1	.007	5	-.002	15
440			min	-926.73	3	-.201	3	-.3	1	0	4	-.002	1	-.01	4
441		12	max	796.924	2	-.18	15	12.404	4	0	1	.012	5	-.002	15
442			min	-926.858	3	-.729	4	-.3	1	0	4	-.002	1	-.01	4
443		13	max	796.753	2	-.358	15	12.938	4	0	1	.017	5	-.002	15
444			min	-926.985	3	-1.49	4	-.3	1	0	4	-.002	1	-.009	4
445		14	max	796.583	2	-.537	15	13.473	4	0	1	.022	5	-.002	15
446			min	-927.113	3	-2.251	4	-.3	1	0	4	-.002	1	-.009	4
447		15	max	796.413	2	-.716	15	14.008	4	0	1	.028	5	-.002	15
448			min	-927.241	3	-3.012	4	-.3	1	0	4	-.002	1	-.008	4
449		16	max	796.242	2	-.895	15	14.542	4	0	1	.034	5	-.001	15
450			min	-927.369	3	-3.773	4	-.3	1	0	4	-.002	1	-.006	4
451		17	max	796.072	2	-1.074	15	15.077	4	0	1	.04	5	-.001	15
452			min	-927.497	3	-4.534	4	-.3	1	0	4	-.002	1	-.004	4
453		18	max	795.902	2	-1.253	15	15.612	4	0	1	.046	5	0	15
454			min	-927.624	3	-5.295	4	-.3	1	0	4	-.003	1	-.002	4
455		19	max	795.731	2	-1.432	15	16.146	4	0	1	.053	5	0	1
456			min	-927.752	3	-6.056	4	-.3	1	0	4	-.003	1	0	1
457	M12	1	max	884.225	1	0	1	10.989	1	0	1	.05	5	0	1
458			min	64.675	12	0	1	-278.865	4	0	1	-.002	1	0	1
459		2	max	884.396	1	0	1	10.989	1	0	1	.018	5	0	1
460			min	64.76	12	0	1	-279.013	4	0	1	-.001	1	0	1
461		3	max	884.566	1	0	1	10.989	1	0	1	0	1	0	1
462			min	64.845	12	0	1	-279.161	4	0	1	-.014	4	0	1
463		4	max	884.736	1	0	1	10.989	1	0	1	.001	1	0	1
464			min	64.931	12	0	1	-279.308	4	0	1	-.046	4	0	1
465		5	max	884.907	1	0	1	10.989	1	0	1	.003	1	0	1
466			min	65.016	12	0	1	-279.456	4	0	1	-.078	4	0	1
467		6	max	885.077	1	0	1	10.989	1	0	1	.004	1	0	1
468			min	65.101	12	0	1	-279.604	4	0	1	-.11	4	0	1
469		7	max	885.247	1	0	1	10.989	1	0	1	.005	1	0	1
470			min	65.186	12	0	1	-279.751	4	0	1	-.142	4	0	1
471		8	max	885.418	1	0	1	10.989	1	0	1	.006	1	0	1
472			min	65.271	12	0	1	-279.899	4	0	1	-.174	4	0	1
473		9	max	885.588	1	0	1	10.989	1	0	1	.008	1	0	1
474			min	65.356	12	0	1	-280.046	4	0	1	-.206	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	885.758	1	0	1	10.989	1	0	1	.009	1	0	1
476			min	65.442	12	0	1	-280.194	4	0	1	-.239	4	0	1
477		11	max	885.929	1	0	1	10.989	1	0	1	.01	1	0	1
478			min	65.527	12	0	1	-280.342	4	0	1	-.271	4	0	1
479		12	max	886.099	1	0	1	10.989	1	0	1	.011	1	0	1
480			min	65.612	12	0	1	-280.489	4	0	1	-.303	4	0	1
481		13	max	886.27	1	0	1	10.989	1	0	1	.013	1	0	1
482			min	65.697	12	0	1	-280.637	4	0	1	-.335	4	0	1
483		14	max	886.44	1	0	1	10.989	1	0	1	.014	1	0	1
484			min	65.782	12	0	1	-280.785	4	0	1	-.367	4	0	1
485		15	max	886.61	1	0	1	10.989	1	0	1	.015	1	0	1
486			min	65.867	12	0	1	-280.932	4	0	1	-.4	4	0	1
487		16	max	886.781	1	0	1	10.989	1	0	1	.016	1	0	1
488			min	65.953	12	0	1	-281.08	4	0	1	-.432	4	0	1
489		17	max	886.951	1	0	1	10.989	1	0	1	.018	1	0	1
490			min	66.038	12	0	1	-281.227	4	0	1	-.464	4	0	1
491		18	max	887.121	1	0	1	10.989	1	0	1	.019	1	0	1
492			min	66.123	12	0	1	-281.375	4	0	1	-.497	4	0	1
493		19	max	887.292	1	0	1	10.989	1	0	1	.02	1	0	1
494			min	66.208	12	0	1	-281.523	4	0	1	-.529	4	0	1
495	M1	1	max	168.545	1	696.309	3	41.161	5	0	2	.233	1	.001	3
496			min	-10.803	5	-392.868	2	-97.213	1	0	3	-.104	5	-.013	2
497		2	max	169.366	1	695.429	3	42.403	5	0	2	.181	1	.194	2
498			min	-10.42	5	-394.041	2	-97.213	1	0	3	-.082	5	-.366	3
499		3	max	580.731	3	480.484	2	21.24	5	0	3	.13	1	.392	2
500			min	-332.1	2	-521.599	3	-97.039	1	0	2	-.06	5	-.718	3
501		4	max	581.347	3	479.311	2	22.481	5	0	3	.079	1	.139	2
502			min	-331.278	2	-522.479	3	-97.039	1	0	2	-.048	5	-.442	3
503		5	max	581.963	3	478.137	2	23.722	5	0	3	.028	1	-.003	15
504			min	-330.457	2	-523.359	3	-97.039	1	0	2	-.036	5	-.166	3
505		6	max	582.579	3	476.964	2	24.964	5	0	3	-.002	12	.11	3
506			min	-329.635	2	-524.239	3	-97.039	1	0	2	-.03	4	-.366	2
507		7	max	583.195	3	475.79	2	26.205	5	0	3	-.005	12	.387	3
508			min	-328.814	2	-525.119	3	-97.039	1	0	2	-.075	1	-.617	2
509		8	max	583.812	3	474.617	2	27.447	5	0	3	.004	5	.664	3
510			min	-327.992	2	-525.999	3	-97.039	1	0	2	-.126	1	-.868	2
511		9	max	600.499	3	52.739	2	62.023	5	0	9	.075	1	.773	3
512			min	-251.85	2	.355	15	-143.64	1	0	3	-.132	5	-.995	2
513		10	max	601.116	3	51.565	2	63.265	5	0	9	0	10	.755	3
514			min	-251.028	2	0	5	-143.64	1	0	3	-.1	4	-1.023	2
515		11	max	601.732	3	50.392	2	64.506	5	0	9	-.006	12	.738	3
516			min	-250.207	2	-1.456	4	-143.64	1	0	3	-.085	4	-1.05	2
517		12	max	618.289	3	356.83	3	156.605	5	0	2	.125	1	.644	3
518			min	-174.02	2	-584.101	2	-94.976	1	0	3	-.223	5	-.932	2
519		13	max	618.906	3	355.95	3	157.847	5	0	2	.074	1	.456	3
520			min	-173.198	2	-585.274	2	-94.976	1	0	3	-.14	5	-.623	2
521		14	max	619.522	3	355.07	3	159.088	5	0	2	.024	1	.268	3
522			min	-172.377	2	-586.447	2	-94.976	1	0	3	-.056	5	-.314	2
523		15	max	620.138	3	354.19	3	160.33	5	0	2	.028	5	.081	3
524			min	-171.555	2	-587.621	2	-94.976	1	0	3	-.026	1	-.023	1
525		16	max	620.754	3	353.31	3	161.571	5	0	2	.113	5	.306	2
526			min	-170.733	2	-588.794	2	-94.976	1	0	3	-.076	1	-.105	3
527		17	max	621.37	3	352.43	3	162.813	5	0	2	.199	5	.617	2
528			min	-169.912	2	-589.967	2	-94.976	1	0	3	-.126	1	-.292	3
529		18	max	21.595	5	607.317	2	-7.352	12	0	5	.212	5	.311	2
530			min	-169.642	1	-294.692	3	-127.292	4	0	2	-.178	1	-.144	3
531		19	max	21.979	5	606.144	2	-7.352	12	0	5	.159	5	.012	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-168.82	1	-295.572	3	-126.051	4	0	2	-.234	1	-.009	2
533	M5	1	max	366.876	1	2319.798	3	96.07	5	0	1	0	1	.027	2
534			min	18.293	12	-1337.496	2	0	1	0	4	-.234	4	-.003	3
535		2	max	367.698	1	2318.918	3	97.311	5	0	1	0	1	.733	2
536			min	18.704	12	-1338.67	2	0	1	0	4	-.183	4	-1.227	3
537		3	max	1857.103	3	1435.599	2	78.572	4	0	4	0	1	1.406	2
538			min	-1138.628	2	-1658.951	3	0	1	0	1	-.132	4	-2.402	3
539		4	max	1857.72	3	1434.426	2	79.813	4	0	4	0	1	.649	2
540			min	-1137.806	2	-1659.831	3	0	1	0	1	-.09	4	-1.527	3
541		5	max	1858.336	3	1433.253	2	81.054	4	0	4	0	1	.006	9
542			min	-1136.985	2	-1660.711	3	0	1	0	1	-.047	4	-.651	3
543		6	max	1858.952	3	1432.079	2	82.296	4	0	4	0	1	.226	3
544			min	-1136.163	2	-1661.591	3	0	1	0	1	-.004	5	-.864	2
545		7	max	1859.568	3	1430.906	2	83.537	4	0	4	.039	4	1.103	3
546			min	-1135.342	2	-1662.471	3	0	1	0	1	0	1	-1.619	2
547		8	max	1860.184	3	1429.732	2	84.779	4	0	4	.084	4	1.98	3
548			min	-1134.52	2	-1663.351	3	0	1	0	1	0	1	-2.374	2
549		9	max	1887.057	3	176.9	2	207.306	4	0	1	0	1	2.273	3
550			min	-975.61	2	.354	15	0	1	0	1	-.201	4	-2.71	2
551		10	max	1887.673	3	175.727	2	208.547	4	0	1	0	1	2.208	3
552			min	-974.788	2	0	15	0	1	0	1	-.091	4	-2.803	2
553		11	max	1888.289	3	174.554	2	209.789	4	0	1	.019	4	2.144	3
554			min	-973.966	2	-1.324	6	0	1	0	1	0	1	-2.895	2
555		12	max	1915.422	3	1121.251	3	232.729	4	0	1	0	1	1.886	3
556			min	-815.145	2	-1788.803	2	0	1	0	4	-.33	4	-2.596	2
557		13	max	1916.038	3	1120.371	3	233.97	4	0	1	0	1	1.295	3
558			min	-814.323	2	-1789.976	2	0	1	0	4	-.207	4	-1.652	2
559		14	max	1916.654	3	1119.491	3	235.212	4	0	1	0	1	.704	3
560			min	-813.502	2	-1791.149	2	0	1	0	4	-.083	4	-.707	2
561		15	max	1917.27	3	1118.611	3	236.453	4	0	1	.041	4	.238	2
562			min	-812.68	2	-1792.323	2	0	1	0	4	0	1	-.003	13
563		16	max	1917.887	3	1117.731	3	237.695	4	0	1	.166	4	1.184	2
564			min	-811.859	2	-1793.496	2	0	1	0	4	0	1	-.476	3
565		17	max	1918.503	3	1116.851	3	238.936	4	0	1	.292	4	2.131	2
566			min	-811.037	2	-1794.67	2	0	1	0	4	0	1	-1.066	3
567		18	max	-19.229	12	2045.567	2	0	1	0	4	.346	4	1.098	2
568			min	-367.147	1	-1012.41	3	-17.806	5	0	1	0	1	-.558	3
569		19	max	-18.818	12	2044.394	2	0	1	0	4	.338	4	.018	2
570			min	-366.325	1	-1013.29	3	-16.564	5	0	1	0	1	-.023	3
571	M9	1	max	168.545	1	696.309	3	97.213	1	0	3	-.017	12	.001	3
572			min	10.32	12	-392.868	2	7.242	12	0	4	-.233	1	-.013	2
573		2	max	169.366	1	695.429	3	97.213	1	0	3	-.014	12	.194	2
574			min	10.73	12	-394.041	2	7.242	12	0	4	-.181	1	-.366	3
575		3	max	580.731	3	480.484	2	97.039	1	0	2	-.01	12	.392	2
576			min	-332.1	2	-521.599	3	7.221	12	0	3	-.13	1	-.718	3
577		4	max	581.347	3	479.311	2	97.039	1	0	2	-.006	12	.139	2
578			min	-331.278	2	-522.479	3	7.221	12	0	3	-.083	4	-.442	3
579		5	max	581.963	3	478.137	2	97.039	1	0	2	-.002	12	-.003	15
580			min	-330.457	2	-523.359	3	7.221	12	0	3	-.049	4	-.166	3
581		6	max	582.579	3	476.964	2	97.039	1	0	2	.024	1	.11	3
582			min	-329.635	2	-524.239	3	7.221	12	0	3	-.019	5	-.366	2
583		7	max	583.195	3	475.79	2	97.039	1	0	2	.075	1	.387	3
584			min	-328.814	2	-525.119	3	7.221	12	0	3	.002	15	-.617	2
585		8	max	583.812	3	474.617	2	97.039	1	0	2	.126	1	.664	3
586			min	-327.992	2	-525.999	3	7.221	12	0	3	.009	12	-.868	2
587		9	max	600.499	3	52.739	2	143.64	1	0	3	-.005	12	.773	3
588			min	-251.85	2	.363	15	10.343	12	0	9	-.165	4	-.995	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	601.116	3	51.565	2	143.64	1	0	3	0	1	.755	3
590			min	-251.028	2	.009	15	10.343	12	0	9	-.099	4	-1.023	2
591		11	max	601.732	3	50.392	2	143.64	1	0	3	.077	1	.738	3
592			min	-250.207	2	-1.406	6	10.343	12	0	9	-.052	5	-1.05	2
593		12	max	618.289	3	356.83	3	199.106	4	0	3	-.009	12	.644	3
594			min	-174.02	2	-584.101	2	6.619	12	0	2	-.278	4	-.932	2
595		13	max	618.906	3	355.95	3	200.347	4	0	3	-.005	12	.456	3
596			min	-173.198	2	-585.274	2	6.619	12	0	2	-.173	4	-.623	2
597		14	max	619.522	3	355.07	3	201.589	4	0	3	-.002	12	.268	3
598			min	-172.377	2	-586.447	2	6.619	12	0	2	-.067	4	-.314	2
599		15	max	620.138	3	354.19	3	202.83	4	0	3	.04	4	.081	3
600			min	-171.555	2	-587.621	2	6.619	12	0	2	.002	12	-.023	1
601		16	max	620.754	3	353.31	3	204.072	4	0	3	.147	4	.306	2
602			min	-170.733	2	-588.794	2	6.619	12	0	2	.005	12	-.105	3
603		17	max	621.37	3	352.43	3	205.313	4	0	3	.255	4	.617	2
604			min	-169.912	2	-589.967	2	6.619	12	0	2	.009	12	-.292	3
605		18	max	-10.468	12	607.317	2	105.458	1	0	2	.291	4	.311	2
606			min	-169.642	1	-294.692	3	-81.623	5	0	3	.012	12	-.144	3
607		19	max	-10.057	12	606.144	2	105.458	1	0	2	.262	4	.012	3
608			min	-168.82	1	-295.572	3	-80.382	5	0	3	.016	12	-.009	2

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.103	2	.01	3	8.738e-3	2	NC	1	NC	1
2			min	-.675	4	-.02	3	-.006	2	-2.205e-3	3	NC	1	NC	1
3		2	max	0	1	.262	3	.033	1	9.986e-3	2	NC	5	NC	2
4			min	-.675	4	-.042	1	-.021	5	-2.341e-3	3	806.878	3	6945.989	1
5		3	max	0	1	.491	3	.08	1	1.123e-2	2	NC	5	NC	3
6			min	-.675	4	-.148	2	-.025	5	-2.476e-3	3	445.851	3	2863.19	1
7		4	max	0	1	.63	3	.12	1	1.248e-2	2	NC	5	NC	3
8			min	-.675	4	-.208	2	-.017	5	-2.612e-3	3	350.598	3	1902.921	1
9		5	max	0	1	.662	3	.14	1	1.373e-2	2	NC	5	NC	3
10			min	-.675	4	-.208	2	-.003	5	-2.748e-3	3	334.059	3	1627.324	1
11		6	max	0	1	.59	3	.135	1	1.498e-2	2	NC	5	NC	5
12			min	-.675	4	-.151	2	.008	15	-2.884e-3	3	373.554	3	1694.29	1
13		7	max	0	1	.435	3	.105	1	1.623e-2	2	NC	5	NC	10
14			min	-.675	4	-.059	1	.006	10	-3.019e-3	3	500.579	3	2179.722	1
15		8	max	0	1	.238	3	.059	1	1.747e-2	2	NC	4	NC	2
16			min	-.675	4	.001	15	-.002	10	-3.155e-3	3	881.138	3	3868.887	1
17		9	max	0	1	.183	2	.032	3	1.872e-2	2	NC	4	NC	1
18			min	-.675	4	.004	15	-.012	2	-3.291e-3	3	2837.996	3	8662.213	4
19		10	max	0	1	.231	2	.031	3	1.997e-2	2	NC	3	NC	1
20			min	-.675	4	-.021	3	-.022	2	-3.426e-3	3	1773.83	2	NC	1
21		11	max	0	12	.183	2	.032	3	1.872e-2	2	NC	4	NC	1
22			min	-.675	4	.004	15	-.017	5	-3.291e-3	3	2837.996	3	NC	1
23		12	max	0	12	.238	3	.059	1	1.747e-2	2	NC	4	NC	2
24			min	-.675	4	.001	15	-.016	5	-3.155e-3	3	881.138	3	3868.887	1
25		13	max	0	12	.435	3	.105	1	1.623e-2	2	NC	5	NC	5
26			min	-.675	4	-.059	1	-.005	5	-3.019e-3	3	500.579	3	2179.722	1
27		14	max	0	12	.59	3	.135	1	1.498e-2	2	NC	5	NC	5
28			min	-.675	4	-.151	2	.008	15	-2.884e-3	3	373.554	3	1694.29	1
29		15	max	0	12	.662	3	.14	1	1.373e-2	2	NC	5	NC	3
30			min	-.675	4	-.208	2	.014	10	-2.748e-3	3	334.059	3	1627.324	1
31		16	max	0	12	.63	3	.12	1	1.248e-2	2	NC	5	NC	3
32			min	-.675	4	-.208	2	.012	10	-2.612e-3	3	350.598	3	1902.921	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	12	.491	3	.08	1	1.123e-2	2	NC	5	NC	3
34			min	-.675	4	-.148	2	.007	10	-2.476e-3	3	445.851	3	2863.19	1
35		18	max	0	12	.262	3	.037	4	9.986e-3	2	NC	5	NC	2
36			min	-.675	4	-.042	1	0	10	-2.341e-3	3	806.878	3	6167.37	4
37		19	max	0	12	.103	2	.01	3	8.738e-3	2	NC	1	NC	1
38			min	-.675	4	-.02	3	-.006	2	-2.205e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.237	3	.009	3	5.032e-3	2	NC	1	NC	1
40			min	-.499	4	-.337	2	-.005	2	-4.044e-3	3	NC	1	NC	1
41		2	max	0	1	.529	3	.022	1	6.003e-3	2	NC	5	NC	1
42			min	-.499	4	-.592	2	-.031	5	-4.905e-3	3	780.561	3	6925.137	5
43		3	max	0	1	.778	3	.064	1	6.973e-3	2	NC	5	NC	3
44			min	-.499	4	-.814	2	-.037	5	-5.766e-3	3	421.579	3	3604.694	1
45		4	max	0	1	.954	3	.102	1	7.944e-3	2	NC	15	NC	3
46			min	-.499	4	-.98	2	-.025	5	-6.627e-3	3	318.24	3	2238.243	1
47		5	max	0	1	1.041	3	.124	1	8.914e-3	2	NC	15	NC	3
48			min	-.499	4	-1.078	2	-.003	5	-7.489e-3	3	283.55	3	1844.1	1
49		6	max	0	1	1.041	3	.122	1	9.885e-3	2	NC	15	NC	3
50			min	-.499	4	-1.107	2	.011	10	-8.35e-3	3	283.656	3	1874.885	1
51		7	max	0	1	.968	3	.096	1	1.086e-2	2	NC	15	NC	3
52			min	-.499	4	-1.077	2	.006	10	-9.211e-3	3	307.815	2	2371.289	1
53		8	max	0	1	.851	3	.063	4	1.183e-2	2	NC	15	NC	2
54			min	-.499	4	-1.009	2	-.002	10	-1.007e-2	3	338.895	2	3704.284	4
55		9	max	0	1	.736	3	.041	4	1.28e-2	2	NC	5	NC	1
56			min	-.499	4	-.936	2	-.01	2	-1.093e-2	3	380.554	2	5709.176	4
57		10	max	0	1	.681	3	.027	3	1.377e-2	2	NC	5	NC	1
58			min	-.499	4	-.9	2	-.02	2	-1.179e-2	3	405.01	2	NC	1
59		11	max	0	12	.736	3	.028	3	1.28e-2	2	NC	5	NC	1
60			min	-.499	4	-.936	2	-.031	5	-1.093e-2	3	380.554	2	7379.471	5
61		12	max	0	12	.851	3	.055	1	1.183e-2	2	NC	15	NC	2
62			min	-.499	4	-1.009	2	-.035	5	-1.007e-2	3	338.895	2	4147.357	1
63		13	max	0	12	.968	3	.096	1	1.086e-2	2	NC	15	NC	3
64			min	-.499	4	-1.077	2	-.021	5	-9.211e-3	3	307.815	2	2371.289	1
65		14	max	0	12	1.041	3	.122	1	9.885e-3	2	NC	15	NC	3
66			min	-.499	4	-1.107	2	0	15	-8.35e-3	3	283.656	3	1874.885	1
67		15	max	0	12	1.041	3	.124	1	8.914e-3	2	NC	15	NC	3
68			min	-.499	4	-1.078	2	.012	10	-7.489e-3	3	283.55	3	1844.1	1
69		16	max	0	12	.954	3	.102	1	7.944e-3	2	NC	15	NC	3
70			min	-.499	4	-.98	2	.01	10	-6.627e-3	3	318.24	3	2238.243	1
71		17	max	0	12	.778	3	.067	4	6.973e-3	2	NC	5	NC	3
72			min	-.499	4	-.814	2	.005	10	-5.766e-3	3	421.579	3	3434.967	4
73		18	max	0	12	.529	3	.043	4	6.003e-3	2	NC	5	NC	1
74			min	-.499	4	-.592	2	0	10	-4.905e-3	3	780.561	3	5318.618	4
75		19	max	0	12	.237	3	.009	3	5.032e-3	2	NC	1	NC	1
76			min	-.499	4	-.337	2	-.005	2	-4.044e-3	3	NC	1	NC	1
77	M15	1	max	0	12	.241	3	.008	3	3.586e-3	3	NC	1	NC	1
78			min	-.404	4	-.336	2	-.005	2	-5.295e-3	2	NC	1	NC	1
79		2	max	0	12	.438	3	.022	1	4.356e-3	3	NC	5	NC	1
80			min	-.404	4	-.676	2	-.041	5	-6.323e-3	2	668.953	2	5379.527	5
81		3	max	0	12	.609	3	.064	1	5.125e-3	3	NC	5	NC	3
82			min	-.404	4	-.968	2	-.049	5	-7.35e-3	2	360.617	2	3593.212	1
83		4	max	0	12	.738	3	.102	1	5.895e-3	3	NC	15	NC	3
84			min	-.404	4	-1.176	2	-.035	5	-8.377e-3	2	271.33	2	2232.296	1
85		5	max	0	12	.816	3	.124	1	6.665e-3	3	NC	15	NC	3
86			min	-.404	4	-1.283	2	-.007	5	-9.405e-3	2	240.53	2	1839.297	1
87		6	max	0	12	.841	3	.122	1	7.435e-3	3	NC	15	NC	3
88			min	-.404	4	-1.29	2	.011	10	-1.043e-2	2	238.784	2	1869.364	1
89		7	max	0	12	.821	3	.097	1	8.205e-3	3	NC	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.404	4	-1.213	2	.006	10	-1.146e-2	2	259.757	2	2361.884	1
91		8	max	0	12	.771	3	.074	4	8.975e-3	3	NC	15	NC	2
92			min	-.404	4	-1.086	2	-.001	10	-1.249e-2	2	303.948	2	3168.108	4
93		9	max	0	12	.717	3	.05	4	9.744e-3	3	NC	5	NC	1
94			min	-.404	4	-.958	2	-.009	2	-1.351e-2	2	366.341	2	4704.148	4
95		10	max	0	1	.69	3	.025	3	1.051e-2	3	NC	5	NC	1
96			min	-.404	4	-.897	2	-.019	2	-1.454e-2	2	405.9	2	NC	1
97		11	max	0	1	.717	3	.026	3	9.744e-3	3	NC	5	NC	1
98			min	-.404	4	-.958	2	-.039	5	-1.351e-2	2	366.341	2	5788.884	5
99		12	max	0	1	.771	3	.056	1	8.975e-3	3	NC	15	NC	2
100			min	-.404	4	-1.086	2	-.045	5	-1.249e-2	2	303.948	2	4117.653	1
101		13	max	0	1	.821	3	.097	1	8.205e-3	3	NC	15	NC	3
102			min	-.404	4	-1.213	2	-.029	5	-1.146e-2	2	259.757	2	2361.884	1
103		14	max	0	1	.841	3	.122	1	7.435e-3	3	NC	15	NC	3
104			min	-.404	4	-1.29	2	0	15	-1.043e-2	2	238.784	2	1869.364	1
105		15	max	0	1	.816	3	.124	1	6.665e-3	3	NC	15	NC	3
106			min	-.404	4	-1.283	2	.013	10	-9.405e-3	2	240.53	2	1839.297	1
107		16	max	0	1	.738	3	.102	1	5.895e-3	3	NC	15	NC	3
108			min	-.404	4	-1.176	2	.01	10	-8.377e-3	2	271.33	2	2232.296	1
109		17	max	0	1	.609	3	.079	4	5.125e-3	3	NC	5	NC	3
110			min	-.404	4	-.968	2	.005	10	-7.35e-3	2	360.617	2	2900.517	4
111		18	max	0	1	.438	3	.052	4	4.356e-3	3	NC	5	NC	1
112			min	-.404	4	-.676	2	0	10	-6.323e-3	2	668.953	2	4347.743	4
113		19	max	0	1	.241	3	.008	3	3.586e-3	3	NC	1	NC	1
114			min	-.404	4	-.336	2	-.005	2	-5.295e-3	2	NC	1	NC	1
115	M16	1	max	0	12	.09	2	.007	3	6.298e-3	3	NC	1	NC	1
116			min	-.133	4	-.077	3	-.004	2	-7.082e-3	2	NC	1	NC	1
117		2	max	0	12	.025	3	.033	1	7.373e-3	3	NC	5	NC	2
118			min	-.133	4	-.14	2	-.032	5	-7.941e-3	2	988.41	2	6770.41	5
119		3	max	0	12	.104	3	.08	1	8.449e-3	3	NC	5	NC	3
120			min	-.133	4	-.324	2	-.04	5	-8.8e-3	2	549.842	2	2869.787	1
121		4	max	0	12	.146	3	.12	1	9.524e-3	3	NC	5	NC	3
122			min	-.133	4	-.431	2	-.03	5	-9.658e-3	2	437.83	2	1902.744	1
123		5	max	0	12	.142	3	.141	1	1.06e-2	3	NC	5	NC	3
124			min	-.133	4	-.444	2	-.01	5	-1.052e-2	2	426.51	2	1623.572	1
125		6	max	0	12	.096	3	.135	1	1.167e-2	3	NC	5	NC	3
126			min	-.133	4	-.368	2	.008	15	-1.138e-2	2	497.124	2	1685.511	1
127		7	max	0	12	.017	3	.106	1	1.275e-2	3	NC	5	NC	3
128			min	-.133	4	-.222	2	.008	10	-1.223e-2	2	730.015	2	2157.274	1
129		8	max	0	12	.013	9	.06	1	1.382e-2	3	NC	3	NC	2
130			min	-.133	4	-.078	3	0	10	-1.309e-2	2	1729.045	2	3777.084	1
131		9	max	0	12	.12	2	.036	4	1.49e-2	3	NC	4	NC	1
132			min	-.133	4	-.161	3	-.007	2	-1.395e-2	2	2716.942	3	6527.6	4
133		10	max	0	1	.192	2	.022	3	1.598e-2	3	NC	4	NC	1
134			min	-.133	4	-.198	3	-.017	2	-1.481e-2	2	1884.946	3	NC	1
135		11	max	0	1	.12	2	.023	3	1.49e-2	3	NC	4	NC	1
136			min	-.133	4	-.161	3	-.025	5	-1.395e-2	2	2716.942	3	8946.983	5
137		12	max	0	1	.013	9	.06	1	1.382e-2	3	NC	3	NC	2
138			min	-.133	4	-.078	3	-.026	5	-1.309e-2	2	1729.045	2	3777.084	1
139		13	max	0	1	.017	3	.106	1	1.275e-2	3	NC	5	NC	3
140			min	-.133	4	-.222	2	-.011	5	-1.223e-2	2	730.015	2	2157.274	1
141		14	max	0	1	.096	3	.135	1	1.167e-2	3	NC	5	NC	3
142			min	-.133	4	-.368	2	.008	15	-1.138e-2	2	497.124	2	1685.511	1
143		15	max	0	1	.142	3	.141	1	1.06e-2	3	NC	5	NC	3
144			min	-.133	4	-.444	2	.016	10	-1.052e-2	2	426.51	2	1623.572	1
145		16	max	0	1	.146	3	.12	1	9.524e-3	3	NC	5	NC	3
146			min	-.133	4	-.431	2	.013	10	-9.658e-3	2	437.83	2	1902.744	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.104	3	.08	1	8.449e-3	3	NC	5	NC	3
148			min	-.133	4	-.324	2	.008	10	-8.8e-3	2	549.842	2	2869.787	1
149		18	max	0	1	.025	3	.048	4	7.373e-3	3	NC	5	NC	2
150			min	-.132	4	-.14	2	.002	10	-7.941e-3	2	988.41	2	4743.96	4
151		19	max	0	1	.09	2	.007	3	6.298e-3	3	NC	1	NC	1
152			min	-.132	4	-.077	3	-.004	2	-7.082e-3	2	NC	1	NC	1
153	M2	1	max	.007	2	.01	2	.008	1	1.587e-3	5	NC	1	NC	1
154			min	-.01	3	-.015	3	-.632	4	-2.168e-4	1	8020.918	2	121.872	4
155		2	max	.007	2	.008	2	.007	1	1.659e-3	5	NC	1	NC	1
156			min	-.009	3	-.015	3	-.581	4	-2.053e-4	1	9361.221	2	132.499	4
157		3	max	.006	2	.007	2	.006	1	1.732e-3	5	NC	1	NC	1
158			min	-.009	3	-.014	3	-.531	4	-1.938e-4	1	NC	1	145.084	4
159		4	max	.006	2	.006	2	.006	1	1.805e-3	5	NC	1	NC	1
160			min	-.008	3	-.014	3	-.481	4	-1.823e-4	1	NC	1	160.13	4
161		5	max	.006	2	.004	2	.005	1	1.877e-3	5	NC	1	NC	1
162			min	-.008	3	-.013	3	-.432	4	-1.708e-4	1	NC	1	178.318	4
163		6	max	.005	2	.003	2	.005	1	1.95e-3	5	NC	1	NC	1
164			min	-.007	3	-.013	3	-.384	4	-1.593e-4	1	NC	1	200.588	4
165		7	max	.005	2	.002	2	.004	1	2.022e-3	5	NC	1	NC	1
166			min	-.007	3	-.012	3	-.337	4	-1.478e-4	1	NC	1	228.268	4
167		8	max	.004	2	.001	2	.003	1	2.095e-3	5	NC	1	NC	1
168			min	-.006	3	-.012	3	-.292	4	-1.363e-4	1	NC	1	263.281	4
169		9	max	.004	2	0	2	.003	1	2.167e-3	5	NC	1	NC	1
170			min	-.005	3	-.011	3	-.25	4	-1.248e-4	1	NC	1	308.504	4
171		10	max	.004	2	0	2	.002	1	2.24e-3	5	NC	1	NC	1
172			min	-.005	3	-.01	3	-.209	4	-1.133e-4	1	NC	1	368.398	4
173		11	max	.003	2	-.001	15	.002	1	2.313e-3	5	NC	1	NC	1
174			min	-.004	3	-.009	3	-.171	4	-1.018e-4	1	NC	1	450.19	4
175		12	max	.003	2	-.001	15	.002	1	2.387e-3	4	NC	1	NC	1
176			min	-.004	3	-.008	3	-.136	4	-9.032e-5	1	NC	1	566.241	4
177		13	max	.002	2	-.001	15	.001	1	2.463e-3	4	NC	1	NC	1
178			min	-.003	3	-.007	3	-.104	4	-7.881e-5	1	NC	1	739.17	4
179		14	max	.002	2	-.001	15	0	1	2.54e-3	4	NC	1	NC	1
180			min	-.003	3	-.006	3	-.076	4	-6.731e-5	1	NC	1	1014.164	4
181		15	max	.002	2	0	15	0	1	2.616e-3	4	NC	1	NC	1
182			min	-.002	3	-.005	3	-.052	4	-5.581e-5	1	NC	1	1492.899	4
183		16	max	.001	2	0	15	0	1	2.693e-3	4	NC	1	NC	1
184			min	-.002	3	-.004	3	-.031	4	-4.431e-5	1	NC	1	2447.049	4
185		17	max	0	2	0	15	0	1	2.769e-3	4	NC	1	NC	1
186			min	-.001	3	-.003	3	-.016	4	-3.28e-5	1	NC	1	4832.465	4
187		18	max	0	2	0	15	0	1	2.846e-3	4	NC	1	NC	1
188			min	0	3	-.001	6	-.005	4	-2.13e-5	1	NC	1	NC	1
189		19	max	0	1	0	1	0	1	2.922e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	-9.8e-6	1	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	1.945e-6	1	NC	1	NC	1
192			min	0	1	0	1	0	1	-7.532e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.014	4	2.125e-5	1	NC	1	NC	1
194			min	0	2	-.002	6	0	1	-1.395e-4	5	NC	1	6554.25	4
195		3	max	0	3	0	15	.026	4	4.836e-4	4	NC	1	NC	1
196			min	0	2	-.004	6	0	1	2.791e-6	12	NC	1	3436.138	4
197		4	max	.001	3	-.001	15	.037	4	1.102e-3	4	NC	1	NC	1
198			min	-.001	2	-.006	6	0	1	4.091e-6	12	NC	1	2398.689	4
199		5	max	.002	3	-.002	15	.048	4	1.72e-3	4	NC	1	NC	1
200			min	-.002	2	-.008	6	0	3	5.391e-6	12	NC	1	1880.296	4
201		6	max	.002	3	-.002	15	.057	4	2.339e-3	4	NC	1	NC	1
202			min	-.002	2	-.01	6	0	3	6.691e-6	12	9361.227	6	1568.399	4
203		7	max	.003	3	-.002	15	.066	4	2.957e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.002	2	-.011	6	0	12	7.991e-6	12	8088.277	6	1358.61	4
205		8	max	.003	3	-.003	15	.074	4	3.576e-3	4	NC	2	NC	1
206			min	-.003	2	-.012	6	0	12	9.29e-6	12	7304.614	6	1206.027	4
207		9	max	.004	3	-.003	15	.083	4	4.194e-3	4	NC	5	NC	1
208			min	-.003	2	-.013	6	0	12	1.059e-5	12	6846.655	6	1088.085	4
209		10	max	.004	3	-.003	15	.091	4	4.813e-3	4	NC	5	NC	1
210			min	-.003	2	-.014	6	0	12	1.189e-5	12	6635.563	6	992.188	4
211		11	max	.004	3	-.003	15	.099	4	5.431e-3	4	NC	5	NC	1
212			min	-.004	2	-.014	6	0	12	1.319e-5	12	6640.497	6	910.784	4
213		12	max	.005	3	-.003	15	.107	4	6.049e-3	4	NC	5	NC	1
214			min	-.004	2	-.013	6	0	12	1.449e-5	12	6866.787	6	839.133	4
215		13	max	.005	3	-.003	15	.116	4	6.668e-3	4	NC	2	NC	1
216			min	-.005	2	-.012	6	0	12	1.579e-5	12	7359.508	6	774.205	4
217		14	max	.006	3	-.002	15	.126	4	7.286e-3	4	NC	1	NC	1
218			min	-.005	2	-.011	6	0	12	1.709e-5	12	8226.36	6	714.074	4
219		15	max	.006	3	-.002	15	.137	4	7.905e-3	4	NC	1	NC	1
220			min	-.005	2	-.009	6	0	12	1.839e-5	12	9704.169	6	657.571	4
221		16	max	.007	3	-.001	15	.149	4	8.523e-3	4	NC	1	NC	1
222			min	-.006	2	-.007	6	0	12	1.969e-5	12	NC	1	604.048	4
223		17	max	.007	3	0	15	.162	4	9.142e-3	4	NC	1	NC	1
224			min	-.006	2	-.006	3	0	12	2.099e-5	12	NC	1	553.211	4
225		18	max	.008	3	0	15	.178	4	9.76e-3	4	NC	1	NC	1
226			min	-.007	2	-.004	3	0	12	2.229e-5	12	NC	1	504.998	4
227		19	max	.008	3	0	5	.196	4	1.038e-2	4	NC	1	NC	1
228			min	-.007	2	-.003	3	0	12	2.359e-5	12	NC	1	459.472	4
229	M4	1	max	.002	1	.007	2	0	12	7.548e-4	4	NC	1	NC	3
230			min	0	5	-.008	3	-.196	4	8.854e-6	12	NC	1	126.865	4
231		2	max	.002	1	.006	2	0	12	7.548e-4	4	NC	1	NC	3
232			min	0	5	-.008	3	-.18	4	8.854e-6	12	NC	1	137.673	4
233		3	max	.002	1	.006	2	0	12	7.548e-4	4	NC	1	NC	3
234			min	0	5	-.007	3	-.165	4	8.854e-6	12	NC	1	150.554	4
235		4	max	.002	1	.006	2	0	12	7.548e-4	4	NC	1	NC	2
236			min	0	5	-.007	3	-.149	4	8.854e-6	12	NC	1	166.041	4
237		5	max	.002	1	.005	2	0	12	7.548e-4	4	NC	1	NC	2
238			min	0	5	-.007	3	-.134	4	8.854e-6	12	NC	1	184.863	4
239		6	max	.002	1	.005	2	0	12	7.548e-4	4	NC	1	NC	2
240			min	0	5	-.006	3	-.119	4	8.854e-6	12	NC	1	208.028	4
241		7	max	.001	1	.004	2	0	12	7.548e-4	4	NC	1	NC	2
242			min	0	5	-.006	3	-.105	4	8.854e-6	12	NC	1	236.968	4
243		8	max	.001	1	.004	2	0	12	7.548e-4	4	NC	1	NC	2
244			min	0	5	-.005	3	-.091	4	8.854e-6	12	NC	1	273.772	4
245		9	max	.001	1	.004	2	0	12	7.548e-4	4	NC	1	NC	2
246			min	0	5	-.005	3	-.077	4	8.854e-6	12	NC	1	321.581	4
247		10	max	.001	1	.003	2	0	12	7.548e-4	4	NC	1	NC	1
248			min	0	5	-.004	3	-.064	4	8.854e-6	12	NC	1	385.309	4
249		11	max	0	1	.003	2	0	12	7.548e-4	4	NC	1	NC	1
250			min	0	5	-.004	3	-.052	4	8.854e-6	12	NC	1	472.987	4
251		12	max	0	1	.003	2	0	12	7.548e-4	4	NC	1	NC	1
252			min	0	5	-.003	3	-.041	4	8.854e-6	12	NC	1	598.506	4
253		13	max	0	1	.002	2	0	12	7.548e-4	4	NC	1	NC	1
254			min	0	5	-.003	3	-.031	4	8.854e-6	12	NC	1	787.637	4
255		14	max	0	1	.002	2	0	12	7.548e-4	4	NC	1	NC	1
256			min	0	5	-.002	3	-.023	4	8.854e-6	12	NC	1	1092.782	4
257		15	max	0	1	.001	2	0	12	7.548e-4	4	NC	1	NC	1
258			min	0	5	-.002	3	-.015	4	8.854e-6	12	NC	1	1634.672	4
259		16	max	0	1	.001	2	0	12	7.548e-4	4	NC	1	NC	1
260			min	0	5	-.001	3	-.009	4	8.854e-6	12	NC	1	2746.802	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	7.548e-4	4	NC	1	NC	1
262			min	0	5	0	3	-.004	4	8.854e-6	12	NC	1	5664.406	4
263		18	max	0	1	0	2	0	12	7.548e-4	4	NC	1	NC	1
264			min	0	5	0	3	-.001	4	8.854e-6	12	NC	1	NC	1
265		19	max	0	1	0	1	0	1	7.548e-4	4	NC	1	NC	1
266			min	0	1	0	1	0	1	8.854e-6	12	NC	1	NC	1
267	M6	1	max	.023	2	.035	2	0	1	1.682e-3	4	NC	4	NC	1
268			min	-.032	3	-.049	3	-.638	4	0	1	1579.564	3	120.715	4
269		2	max	.022	2	.032	2	0	1	1.753e-3	4	NC	4	NC	1
270			min	-.03	3	-.046	3	-.587	4	0	1	1672.377	3	131.243	4
271		3	max	.02	2	.029	2	0	1	1.823e-3	4	NC	4	NC	1
272			min	-.029	3	-.043	3	-.536	4	0	1	1776.91	3	143.71	4
273		4	max	.019	2	.026	2	0	1	1.893e-3	4	NC	4	NC	1
274			min	-.027	3	-.041	3	-.485	4	0	1	1895.646	3	158.616	4
275		5	max	.018	2	.023	2	0	1	1.964e-3	4	NC	4	NC	1
276			min	-.025	3	-.038	3	-.436	4	0	1	2031.782	3	176.635	4
277		6	max	.017	2	.02	2	0	1	2.034e-3	4	NC	4	NC	1
278			min	-.023	3	-.035	3	-.388	4	0	1	2189.496	3	198.698	4
279		7	max	.015	2	.017	2	0	1	2.104e-3	4	NC	1	NC	1
280			min	-.021	3	-.032	3	-.341	4	0	1	2374.361	3	226.121	4
281		8	max	.014	2	.015	2	0	1	2.175e-3	4	NC	1	NC	1
282			min	-.02	3	-.03	3	-.295	4	0	1	2593.981	3	260.811	4
283		9	max	.013	2	.012	2	0	1	2.245e-3	4	NC	1	NC	1
284			min	-.018	3	-.027	3	-.252	4	0	1	2859.007	3	305.616	4
285		10	max	.011	2	.01	2	0	1	2.315e-3	4	NC	1	NC	1
286			min	-.016	3	-.024	3	-.211	4	0	1	3184.832	3	364.957	4
287		11	max	.01	2	.008	2	0	1	2.386e-3	4	NC	1	NC	1
288			min	-.014	3	-.021	3	-.173	4	0	1	3594.559	3	445.996	4
289		12	max	.009	2	.006	2	0	1	2.456e-3	4	NC	1	NC	1
290			min	-.013	3	-.019	3	-.137	4	0	1	4124.509	3	560.98	4
291		13	max	.008	2	.004	2	0	1	2.526e-3	4	NC	1	NC	1
292			min	-.011	3	-.016	3	-.105	4	0	1	4835.248	3	732.322	4
293		14	max	.006	2	.003	2	0	1	2.596e-3	4	NC	1	NC	1
294			min	-.009	3	-.013	3	-.077	4	0	1	5835.835	3	1004.798	4
295		15	max	.005	2	.002	2	0	1	2.667e-3	4	NC	1	NC	1
296			min	-.007	3	-.01	3	-.052	4	0	1	7344.457	3	1479.161	4
297		16	max	.004	2	0	2	0	1	2.737e-3	4	NC	1	NC	1
298			min	-.005	3	-.008	3	-.032	4	0	1	9870.32	3	2424.624	4
299		17	max	.003	2	0	2	0	1	2.807e-3	4	NC	1	NC	1
300			min	-.004	3	-.005	3	-.016	4	0	1	NC	1	4788.413	4
301		18	max	.001	2	0	2	0	1	2.878e-3	4	NC	1	NC	1
302			min	-.002	3	-.003	3	-.005	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	2.948e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-7.599e-4	4	NC	1	NC	1
307		2	max	.001	3	0	2	.014	4	0	1	NC	1	NC	1
308			min	-.001	2	-.003	3	0	1	-1.583e-4	4	NC	1	6497.018	4
309		3	max	.003	3	0	2	.026	4	4.433e-4	4	NC	1	NC	1
310			min	-.003	2	-.006	3	0	1	0	1	NC	1	3407.294	4
311		4	max	.004	3	-.001	15	.038	4	1.045e-3	4	NC	1	NC	1
312			min	-.004	2	-.008	3	0	1	0	1	NC	1	2379.973	4
313		5	max	.006	3	-.002	15	.048	4	1.646e-3	4	NC	1	NC	1
314			min	-.005	2	-.01	3	0	1	0	1	NC	1	1867.274	4
315		6	max	.007	3	-.002	15	.058	4	2.248e-3	4	NC	1	NC	1
316			min	-.007	2	-.012	3	0	1	0	1	8781.016	3	1559.413	4
317		7	max	.008	3	-.003	15	.066	4	2.85e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.008	2	-.014	3	0	1	0	1	7848.687	3	1352.921	4
319		8	max	.01	3	-.003	15	.075	4	3.451e-3	4	NC	1	NC	1
320			min	-.01	2	-.015	3	0	1	0	1	7297.906	3	1203.284	4
321		9	max	.011	3	-.003	15	.083	4	4.053e-3	4	NC	1	NC	1
322			min	-.011	2	-.016	3	0	1	0	1	6876.675	4	1088.108	4
323		10	max	.013	3	-.003	15	.09	4	4.654e-3	4	NC	1	NC	1
324			min	-.012	2	-.017	3	0	1	0	1	6663.086	4	994.867	4
325		11	max	.014	3	-.003	15	.098	4	5.256e-3	4	NC	1	NC	1
326			min	-.014	2	-.017	3	0	1	0	1	6666.708	4	916.019	4
327		12	max	.015	3	-.003	15	.106	4	5.858e-3	4	NC	1	NC	1
328			min	-.015	2	-.017	3	0	1	0	1	6892.721	4	846.794	4
329		13	max	.017	3	-.003	15	.115	4	6.459e-3	4	NC	1	NC	1
330			min	-.016	2	-.016	3	0	1	0	1	7386.246	4	784.107	4
331		14	max	.018	3	-.003	15	.124	4	7.061e-3	4	NC	1	NC	1
332			min	-.018	2	-.015	3	0	1	0	1	8255.259	4	725.971	4
333		15	max	.02	3	-.002	15	.134	4	7.662e-3	4	NC	1	NC	1
334			min	-.019	2	-.014	3	0	1	0	1	9737.306	4	671.152	4
335		16	max	.021	3	-.002	15	.145	4	8.264e-3	4	NC	1	NC	1
336			min	-.021	2	-.013	3	0	1	0	1	NC	1	618.951	4
337		17	max	.022	3	0	2	.158	4	8.865e-3	4	NC	1	NC	1
338			min	-.022	2	-.011	3	0	1	0	1	NC	1	569.045	4
339		18	max	.024	3	0	2	.172	4	9.467e-3	4	NC	1	NC	1
340			min	-.023	2	-.01	3	0	1	0	1	NC	1	521.364	4
341		19	max	.025	3	.002	2	.189	4	1.007e-2	4	NC	1	NC	1
342			min	-.025	2	-.008	3	0	1	0	1	NC	1	475.991	4
343	M8	1	max	.005	1	.024	2	0	1	5.955e-4	4	NC	1	NC	1
344			min	0	15	-.026	3	-.189	4	0	1	NC	1	131.426	4
345		2	max	.005	1	.023	2	0	1	5.955e-4	4	NC	1	NC	1
346			min	0	15	-.025	3	-.174	4	0	1	NC	1	142.637	4
347		3	max	.005	1	.022	2	0	1	5.955e-4	4	NC	1	NC	1
348			min	0	15	-.023	3	-.159	4	0	1	NC	1	155.996	4
349		4	max	.004	1	.02	2	0	1	5.955e-4	4	NC	1	NC	1
350			min	0	15	-.022	3	-.144	4	0	1	NC	1	172.058	4
351		5	max	.004	1	.019	2	0	1	5.955e-4	4	NC	1	NC	1
352			min	0	15	-.02	3	-.129	4	0	1	NC	1	191.578	4
353		6	max	.004	1	.018	2	0	1	5.955e-4	4	NC	1	NC	1
354			min	0	15	-.019	3	-.115	4	0	1	NC	1	215.601	4
355		7	max	.003	1	.016	2	0	1	5.955e-4	4	NC	1	NC	1
356			min	0	15	-.018	3	-.101	4	0	1	NC	1	245.613	4
357		8	max	.003	1	.015	2	0	1	5.955e-4	4	NC	1	NC	1
358			min	0	15	-.016	3	-.087	4	0	1	NC	1	283.778	4
359		9	max	.003	1	.014	2	0	1	5.955e-4	4	NC	1	NC	1
360			min	0	15	-.015	3	-.074	4	0	1	NC	1	333.358	4
361		10	max	.003	1	.012	2	0	1	5.955e-4	4	NC	1	NC	1
362			min	0	15	-.013	3	-.062	4	0	1	NC	1	399.444	4
363		11	max	.002	1	.011	2	0	1	5.955e-4	4	NC	1	NC	1
364			min	0	15	-.012	3	-.051	4	0	1	NC	1	490.369	4
365		12	max	.002	1	.009	2	0	1	5.955e-4	4	NC	1	NC	1
366			min	0	15	-.01	3	-.04	4	0	1	NC	1	620.537	4
367		13	max	.002	1	.008	2	0	1	5.955e-4	4	NC	1	NC	1
368			min	0	15	-.009	3	-.03	4	0	1	NC	1	816.675	4
369		14	max	.001	1	.007	2	0	1	5.955e-4	4	NC	1	NC	1
370			min	0	15	-.007	3	-.022	4	0	1	NC	1	1133.134	4
371		15	max	.001	1	.005	2	0	1	5.955e-4	4	NC	1	NC	1
372			min	0	15	-.006	3	-.015	4	0	1	NC	1	1695.128	4
373		16	max	0	1	.004	2	0	1	5.955e-4	4	NC	1	NC	1
374			min	0	15	-.004	3	-.009	4	0	1	NC	1	2848.558	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	1	.003	2	0	1	5.955e-4	4	NC	1	NC	1
376			min	0	15	-.003	3	-.004	4	0	1	NC	1	5874.649	4
377		18	max	0	1	.001	2	0	1	5.955e-4	4	NC	1	NC	1
378			min	0	15	-.001	3	-.001	4	0	1	NC	1	NC	1
379		19	max	0	1	0	1	0	1	5.955e-4	4	NC	1	NC	1
380			min	0	1	0	1	0	1	0	1	NC	1	NC	1
381	M10	1	max	.007	2	.01	2	0	12	1.694e-3	4	NC	1	NC	1
382			min	-.01	3	-.015	3	-.637	4	1.708e-5	12	8020.918	2	120.883	4
383		2	max	.007	2	.008	2	0	12	1.762e-3	4	NC	1	NC	1
384			min	-.009	3	-.015	3	-.586	4	1.618e-5	12	9361.221	2	131.427	4
385		3	max	.006	2	.007	2	0	12	1.831e-3	4	NC	1	NC	1
386			min	-.009	3	-.014	3	-.535	4	1.528e-5	12	NC	1	143.913	4
387		4	max	.006	2	.006	2	0	12	1.899e-3	4	NC	1	NC	1
388			min	-.008	3	-.014	3	-.485	4	1.438e-5	12	NC	1	158.841	4
389		5	max	.006	2	.004	2	0	12	1.968e-3	4	NC	1	NC	1
390			min	-.008	3	-.013	3	-.435	4	1.348e-5	12	NC	1	176.888	4
391		6	max	.005	2	.003	2	0	12	2.037e-3	4	NC	1	NC	1
392			min	-.007	3	-.013	3	-.387	4	1.258e-5	12	NC	1	198.986	4
393		7	max	.005	2	.002	2	0	12	2.105e-3	4	NC	1	NC	1
394			min	-.007	3	-.012	3	-.34	4	1.168e-5	12	NC	1	226.453	4
395		8	max	.004	2	.001	2	0	12	2.174e-3	4	NC	1	NC	1
396			min	-.006	3	-.012	3	-.295	4	1.078e-5	12	NC	1	261.199	4
397		9	max	.004	2	0	2	0	12	2.243e-3	4	NC	1	NC	1
398			min	-.005	3	-.011	3	-.252	4	9.885e-6	12	NC	1	306.08	4
399		10	max	.004	2	0	2	0	12	2.311e-3	4	NC	1	NC	1
400			min	-.005	3	-.01	3	-.211	4	8.985e-6	12	NC	1	365.524	4
401		11	max	.003	2	-.001	2	0	12	2.38e-3	4	NC	1	NC	1
402			min	-.004	3	-.009	3	-.172	4	8.086e-6	12	NC	1	446.708	4
403		12	max	.003	2	-.002	2	0	12	2.448e-3	4	NC	1	NC	1
404			min	-.004	3	-.008	3	-.137	4	7.186e-6	12	NC	1	561.907	4
405		13	max	.002	2	-.002	15	0	12	2.517e-3	4	NC	1	NC	1
406			min	-.003	3	-.007	3	-.105	4	6.287e-6	12	NC	1	733.586	4
407		14	max	.002	2	-.001	15	0	12	2.586e-3	4	NC	1	NC	1
408			min	-.003	3	-.006	3	-.076	4	5.387e-6	12	NC	1	1006.632	4
409		15	max	.002	2	-.001	15	0	12	2.654e-3	4	NC	1	NC	1
410			min	-.002	3	-.005	3	-.052	4	4.488e-6	12	NC	1	1482.072	4
411		16	max	.001	2	-.001	15	0	12	2.723e-3	4	NC	1	NC	1
412			min	-.002	3	-.004	4	-.032	4	3.588e-6	12	NC	1	2429.925	4
413		17	max	0	2	0	15	0	12	2.791e-3	4	NC	1	NC	1
414			min	-.001	3	-.003	4	-.016	4	2.688e-6	12	NC	1	4800.666	4
415		18	max	0	2	0	15	0	12	2.86e-3	4	NC	1	NC	1
416			min	0	3	-.002	4	-.005	4	1.789e-6	12	NC	1	NC	1
417		19	max	0	1	0	1	0	1	2.929e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	8.894e-7	12	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	-1.913e-7	12	NC	1	NC	1
420			min	0	1	0	1	0	1	-7.545e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.014	4	-1.491e-6	12	NC	1	NC	1
422			min	0	2	-.002	4	0	12	-1.493e-4	4	NC	1	6541.201	4
423		3	max	0	3	-.001	15	.026	4	4.597e-4	5	NC	1	NC	1
424			min	0	2	-.004	4	0	12	-4.056e-5	1	NC	1	3430.971	4
425		4	max	.001	3	-.002	15	.037	4	1.063e-3	5	NC	1	NC	1
426			min	-.001	2	-.006	4	0	10	-5.987e-5	1	NC	1	2396.62	4
427		5	max	.002	3	-.002	15	.048	4	1.667e-3	4	NC	1	NC	1
428			min	-.002	2	-.008	4	0	10	-7.918e-5	1	NC	1	1880.198	4
429		6	max	.002	3	-.003	15	.057	4	2.272e-3	4	NC	1	NC	1
430			min	-.002	2	-.01	4	0	1	-9.848e-5	1	9133.374	4	1569.877	4
431		7	max	.003	3	-.003	15	.066	4	2.877e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.002	2	-.012	4	0	1	-1.178e-4	1	7905.61	4	1361.506	4
433		8	max	.003	3	-.003	15	.074	4	3.482e-3	4	NC	2	NC	1
434			min	-.003	2	-.013	4	0	1	-1.371e-4	1	7150.362	4	1210.275	4
435		9	max	.004	3	-.003	15	.082	4	4.088e-3	4	NC	5	NC	1
436			min	-.003	2	-.014	4	0	1	-1.564e-4	1	6710.542	4	1093.649	4
437		10	max	.004	3	-.004	15	.09	4	4.693e-3	4	NC	5	NC	1
438			min	-.003	2	-.015	4	0	1	-1.757e-4	1	6510.605	4	999.032	4
439		11	max	.004	3	-.004	15	.098	4	5.298e-3	4	NC	5	NC	1
440			min	-.004	2	-.015	4	-.001	1	-1.95e-4	1	6521.368	4	918.849	4
441		12	max	.005	3	-.004	15	.106	4	5.903e-3	4	NC	5	NC	1
442			min	-.004	2	-.014	4	-.002	1	-2.143e-4	1	6748.802	4	848.328	4
443		13	max	.005	3	-.003	15	.115	4	6.509e-3	4	NC	2	NC	1
444			min	-.005	2	-.013	4	-.002	1	-2.336e-4	1	7237.774	4	784.397	4
445		14	max	.006	3	-.003	15	.124	4	7.114e-3	4	NC	1	NC	1
446			min	-.005	2	-.012	4	-.003	1	-2.529e-4	1	8094.697	4	725.092	4
447		15	max	.006	3	-.003	15	.134	4	7.719e-3	4	NC	1	NC	1
448			min	-.005	2	-.011	4	-.003	1	-2.723e-4	1	9553.116	4	669.21	4
449		16	max	.007	3	-.002	15	.146	4	8.324e-3	4	NC	1	NC	1
450			min	-.006	2	-.009	4	-.004	1	-2.916e-4	1	NC	1	616.079	4
451		17	max	.007	3	-.002	15	.159	4	8.93e-3	4	NC	1	NC	1
452			min	-.006	2	-.006	4	-.005	1	-3.109e-4	1	NC	1	565.399	4
453		18	max	.008	3	-.001	15	.174	4	9.535e-3	4	NC	1	NC	1
454			min	-.007	2	-.004	3	-.006	1	-3.302e-4	1	NC	1	517.115	4
455		19	max	.008	3	0	10	.191	4	1.014e-2	4	NC	1	NC	1
456			min	-.007	2	-.003	3	-.007	1	-3.495e-4	1	NC	1	471.312	4
457	M12	1	max	.002	1	.007	2	.007	1	6.913e-4	5	NC	1	NC	3
458			min	0	12	-.008	3	-.191	4	-1.246e-4	1	NC	1	130.134	4
459		2	max	.002	1	.006	2	.007	1	6.913e-4	5	NC	1	NC	3
460			min	0	12	-.008	3	-.176	4	-1.246e-4	1	NC	1	141.225	4
461		3	max	.002	1	.006	2	.006	1	6.913e-4	5	NC	1	NC	3
462			min	0	12	-.007	3	-.161	4	-1.246e-4	1	NC	1	154.442	4
463		4	max	.002	1	.006	2	.006	1	6.913e-4	5	NC	1	NC	2
464			min	0	12	-.007	3	-.146	4	-1.246e-4	1	NC	1	170.334	4
465		5	max	.002	1	.005	2	.005	1	6.913e-4	5	NC	1	NC	2
466			min	0	12	-.007	3	-.131	4	-1.246e-4	1	NC	1	189.647	4
467		6	max	.002	1	.005	2	.004	1	6.913e-4	5	NC	1	NC	2
468			min	0	12	-.006	3	-.116	4	-1.246e-4	1	NC	1	213.416	4
469		7	max	.001	1	.004	2	.004	1	6.913e-4	5	NC	1	NC	2
470			min	0	12	-.006	3	-.102	4	-1.246e-4	1	NC	1	243.111	4
471		8	max	.001	1	.004	2	.003	1	6.913e-4	5	NC	1	NC	2
472			min	0	12	-.005	3	-.088	4	-1.246e-4	1	NC	1	280.874	4
473		9	max	.001	1	.004	2	.003	1	6.913e-4	5	NC	1	NC	2
474			min	0	12	-.005	3	-.075	4	-1.246e-4	1	NC	1	329.931	4
475		10	max	.001	1	.003	2	.002	1	6.913e-4	5	NC	1	NC	1
476			min	0	12	-.004	3	-.063	4	-1.246e-4	1	NC	1	395.32	4
477		11	max	0	1	.003	2	.002	1	6.913e-4	5	NC	1	NC	1
478			min	0	12	-.004	3	-.051	4	-1.246e-4	1	NC	1	485.285	4
479		12	max	0	1	.003	2	.002	1	6.913e-4	5	NC	1	NC	1
480			min	0	12	-.003	3	-.04	4	-1.246e-4	1	NC	1	614.078	4
481		13	max	0	1	.002	2	.001	1	6.913e-4	5	NC	1	NC	1
482			min	0	12	-.003	3	-.031	4	-1.246e-4	1	NC	1	808.142	4
483		14	max	0	1	.002	2	0	1	6.913e-4	5	NC	1	NC	1
484			min	0	12	-.002	3	-.022	4	-1.246e-4	1	NC	1	1121.249	4
485		15	max	0	1	.001	2	0	1	6.913e-4	5	NC	1	NC	1
486			min	0	12	-.002	3	-.015	4	-1.246e-4	1	NC	1	1677.282	4
487		16	max	0	1	.001	2	0	1	6.913e-4	5	NC	1	NC	1
488			min	0	12	-.001	3	-.009	4	-1.246e-4	1	NC	1	2818.45	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	6.913e-4	5	NC	1	NC	1
490			min	0	12	0	3	-.004	4	-1.246e-4	1	NC	1	5812.273	4
491		18	max	0	1	0	2	0	1	6.913e-4	5	NC	1	NC	1
492			min	0	12	0	3	-.001	4	-1.246e-4	1	NC	1	NC	1
493		19	max	0	1	0	1	0	1	6.913e-4	5	NC	1	NC	1
494			min	0	1	0	1	0	1	-1.246e-4	1	NC	1	NC	1
495	M1	1	max	.01	3	.103	2	.675	4	1.158e-2	2	NC	1	NC	1
496			min	-.006	2	-.02	3	0	12	-2.315e-2	3	NC	1	NC	1
497		2	max	.01	3	.047	2	.654	4	6.708e-3	4	NC	4	NC	1
498			min	-.006	2	-.006	3	-.005	1	-1.145e-2	3	2078.781	2	NC	1
499		3	max	.01	3	.016	3	.631	4	1.136e-2	4	NC	5	NC	1
500			min	-.006	2	-.012	2	-.008	1	-1.489e-4	1	1003.694	2	6258.507	5
501		4	max	.01	3	.051	3	.608	4	9.827e-3	4	NC	5	NC	1
502			min	-.006	2	-.079	2	-.007	1	-4.499e-3	3	635.221	2	4536.844	5
503		5	max	.009	3	.096	3	.585	4	8.291e-3	4	NC	5	NC	1
504			min	-.005	2	-.148	2	-.005	1	-8.87e-3	3	459.45	2	3677.494	5
505		6	max	.009	3	.143	3	.56	4	1.148e-2	2	NC	15	NC	1
506			min	-.005	2	-.215	2	-.002	1	-1.324e-2	3	362.475	2	3158.455	5
507		7	max	.009	3	.188	3	.535	4	1.531e-2	2	NC	15	NC	1
508			min	-.005	2	-.275	2	0	12	-1.761e-2	3	305.158	2	2783.937	4
509		8	max	.009	3	.226	3	.51	4	1.914e-2	2	NC	15	NC	1
510			min	-.005	2	-.322	2	0	12	-2.199e-2	3	271.225	2	2502.787	4
511		9	max	.009	3	.25	3	.483	4	2.198e-2	2	9793.161	15	NC	1
512			min	-.005	2	-.352	2	0	1	-2.226e-2	3	253.549	2	2317.483	4
513		10	max	.008	3	.258	3	.454	4	2.417e-2	2	9585.066	15	NC	1
514			min	-.005	2	-.362	2	0	12	-1.982e-2	3	248.395	2	2255.599	4
515		11	max	.008	3	.252	3	.423	4	2.636e-2	2	9792.649	15	NC	1
516			min	-.005	2	-.352	2	0	12	-1.738e-2	3	254.553	2	2291.607	4
517		12	max	.008	3	.231	3	.39	4	2.565e-2	2	NC	15	NC	1
518			min	-.005	2	-.32	2	0	1	-1.474e-2	3	274.284	2	2433.178	4
519		13	max	.008	3	.196	3	.354	4	2.057e-2	2	NC	15	NC	1
520			min	-.005	2	-.27	2	0	1	-1.179e-2	3	312.607	2	2824.697	4
521		14	max	.008	3	.153	3	.314	4	1.55e-2	2	NC	15	NC	1
522			min	-.005	2	-.207	2	0	12	-8.852e-3	3	378.391	2	3649.194	4
523		15	max	.007	3	.104	3	.274	4	1.043e-2	2	NC	5	NC	1
524			min	-.005	2	-.138	2	0	12	-5.91e-3	3	492.214	2	5418.321	4
525		16	max	.007	3	.054	3	.234	4	8.25e-3	4	NC	5	NC	1
526			min	-.005	2	-.069	2	0	12	-2.968e-3	3	704.337	2	NC	1
527		17	max	.007	3	.006	3	.196	4	9.429e-3	4	NC	5	NC	1
528			min	-.004	2	-.007	2	0	12	-2.534e-5	3	1160.582	2	NC	1
529		18	max	.007	3	.045	2	.163	4	9.448e-3	2	NC	4	NC	1
530			min	-.004	2	-.037	3	0	12	-4.136e-3	3	2478.647	2	NC	1
531		19	max	.007	3	.09	2	.132	4	1.894e-2	2	NC	1	NC	1
532			min	-.004	2	-.077	3	0	1	-8.412e-3	3	NC	1	NC	1
533	M5	1	max	.031	3	.231	2	.675	4	0	1	NC	1	NC	1
534			min	-.022	2	-.021	3	0	1	-6.78e-6	4	NC	1	NC	1
535		2	max	.031	3	.104	2	.658	4	5.843e-3	4	NC	5	NC	1
536			min	-.022	2	.002	15	0	1	0	1	906.641	2	8613.069	4
537		3	max	.031	3	.051	3	.637	4	1.151e-2	4	NC	5	NC	1
538			min	-.022	2	-.039	2	0	1	0	1	428.27	2	5057.528	4
539		4	max	.03	3	.145	3	.614	4	9.379e-3	4	NC	15	NC	1
540			min	-.021	2	-.208	2	0	1	0	1	263.546	2	3931.205	4
541		5	max	.029	3	.268	3	.588	4	7.246e-3	4	8171.676	15	NC	1
542			min	-.021	2	-.389	2	0	1	0	1	186.301	2	3400.407	4
543		6	max	.029	3	.405	3	.562	4	5.113e-3	4	6289.659	15	NC	1
544			min	-.021	2	-.568	2	0	1	0	1	144.466	2	3078.23	4
545		7	max	.028	3	.537	3	.535	4	2.979e-3	4	5203.163	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.02	2	-.73	2	0	1	0	1	120.118	2	2818.307	4
547		8	max	.028	3	.647	3	.509	4	8.464e-4	4	4571.589	15	NC	1
548			min	-.02	2	-.86	2	0	1	0	1	105.882	2	2549.661	4
549		9	max	.027	3	.718	3	.484	4	0	1	4247.774	15	NC	1
550			min	-.019	2	-.942	2	0	1	-5.009e-6	5	98.551	2	2311.153	4
551		10	max	.026	3	.742	3	.454	4	0	1	4150.246	15	NC	1
552			min	-.019	2	-.97	2	0	1	-4.869e-6	5	96.417	2	2269.71	4
553		11	max	.026	3	.723	3	.423	4	0	1	4247.969	15	NC	1
554			min	-.019	2	-.942	2	0	1	-4.73e-6	5	98.961	2	2318.529	4
555		12	max	.025	3	.66	3	.392	4	6.631e-4	4	4572.046	15	NC	1
556			min	-.019	2	-.855	2	0	1	0	1	107.223	2	2388.984	4
557		13	max	.024	3	.56	3	.355	4	2.335e-3	4	5204.089	15	NC	1
558			min	-.018	2	-.717	2	0	1	0	1	123.593	2	2781.596	4
559		14	max	.024	3	.434	3	.313	4	4.008e-3	4	6291.458	15	NC	1
560			min	-.018	2	-.545	2	0	1	0	1	152.294	2	3824.965	4
561		15	max	.023	3	.293	3	.27	4	5.68e-3	4	8175.219	15	NC	1
562			min	-.018	2	-.359	2	0	1	0	1	203.354	2	6769.881	4
563		16	max	.022	3	.151	3	.228	4	7.353e-3	4	NC	15	NC	1
564			min	-.017	2	-.178	2	0	1	0	1	302.069	2	NC	1
565		17	max	.022	3	.018	3	.19	4	9.025e-3	4	NC	5	NC	1
566			min	-.017	2	-.021	2	0	1	0	1	523.232	2	NC	1
567		18	max	.022	3	.097	2	.158	4	4.582e-3	4	NC	5	NC	1
568			min	-.017	2	-.096	3	0	1	0	1	1164.122	2	NC	1
569		19	max	.022	3	.192	2	.133	4	0	1	NC	1	NC	1
570			min	-.017	2	-.198	3	0	1	-4.186e-6	4	NC	1	NC	1
571	M9	1	max	.01	3	.103	2	.675	4	2.315e-2	3	NC	1	NC	1
572			min	-.006	2	-.02	3	0	1	-1.158e-2	2	NC	1	NC	1
573		2	max	.01	3	.047	2	.657	4	1.145e-2	3	NC	4	NC	1
574			min	-.006	2	-.006	3	0	12	-5.677e-3	2	2078.781	2	8974.687	4
575		3	max	.01	3	.016	3	.637	4	1.149e-2	4	NC	5	NC	1
576			min	-.006	2	-.012	2	0	12	-1.746e-5	10	1003.694	2	5196.964	4
577		4	max	.01	3	.051	3	.613	4	9.06e-3	5	NC	5	NC	1
578			min	-.006	2	-.079	2	0	12	-3.824e-3	2	635.221	2	3980.974	4
579		5	max	.009	3	.096	3	.588	4	8.87e-3	3	NC	5	NC	1
580			min	-.005	2	-.148	2	0	12	-7.654e-3	2	459.45	2	3397.743	4
581		6	max	.009	3	.143	3	.562	4	1.324e-2	3	NC	15	NC	1
582			min	-.005	2	-.215	2	0	12	-1.148e-2	2	362.475	2	3045.973	4
583		7	max	.009	3	.188	3	.535	4	1.761e-2	3	NC	15	NC	1
584			min	-.005	2	-.275	2	0	1	-1.531e-2	2	305.158	2	2779.43	4
585		8	max	.009	3	.226	3	.509	4	2.199e-2	3	NC	15	NC	1
586			min	-.005	2	-.322	2	0	1	-1.914e-2	2	271.225	2	2528.303	4
587		9	max	.009	3	.25	3	.483	4	2.226e-2	3	9767.97	15	NC	1
588			min	-.005	2	-.352	2	0	12	-2.198e-2	2	253.549	2	2310.395	4
589		10	max	.008	3	.258	3	.454	4	1.982e-2	3	9560.483	15	NC	1
590			min	-.005	2	-.362	2	0	1	-2.417e-2	2	248.395	2	2256.949	4
591		11	max	.008	3	.252	3	.423	4	1.738e-2	3	9767.454	15	NC	1
592			min	-.005	2	-.352	2	0	1	-2.636e-2	2	254.553	2	2300.79	4
593		12	max	.008	3	.231	3	.391	4	1.474e-2	3	NC	15	NC	1
594			min	-.005	2	-.32	2	0	12	-2.565e-2	2	274.284	2	2409.972	4
595		13	max	.008	3	.196	3	.354	4	1.179e-2	3	NC	15	NC	1
596			min	-.005	2	-.27	2	0	12	-2.057e-2	2	312.607	2	2825.611	4
597		14	max	.008	3	.153	3	.313	4	8.852e-3	3	NC	15	NC	1
598			min	-.005	2	-.207	2	-.002	1	-1.55e-2	2	378.391	2	3791.793	5
599		15	max	.007	3	.104	3	.271	4	5.91e-3	3	NC	5	NC	1
600			min	-.005	2	-.138	2	-.005	1	-1.043e-2	2	492.214	2	6075.618	5
601		16	max	.007	3	.054	3	.23	4	7.294e-3	5	NC	5	NC	1
602			min	-.005	2	-.069	2	-.007	1	-5.357e-3	2	704.337	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.007	3	.006	3	.191	4	9.133e-3	4	NC	5	NC	1
604			min	-.004	2	-.007	2	-.007	1	-4.852e-4	1	1160.582	2	NC	1
605		18	max	.007	3	.045	2	.159	4	4.401e-3	5	NC	4	NC	1
606			min	-.004	2	-.037	3	-.005	1	-9.448e-3	2	2478.647	2	NC	1
607		19	max	.007	3	.09	2	.133	4	8.412e-3	3	NC	1	NC	1
608			min	-.004	2	-.077	3	0	12	-1.894e-2	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

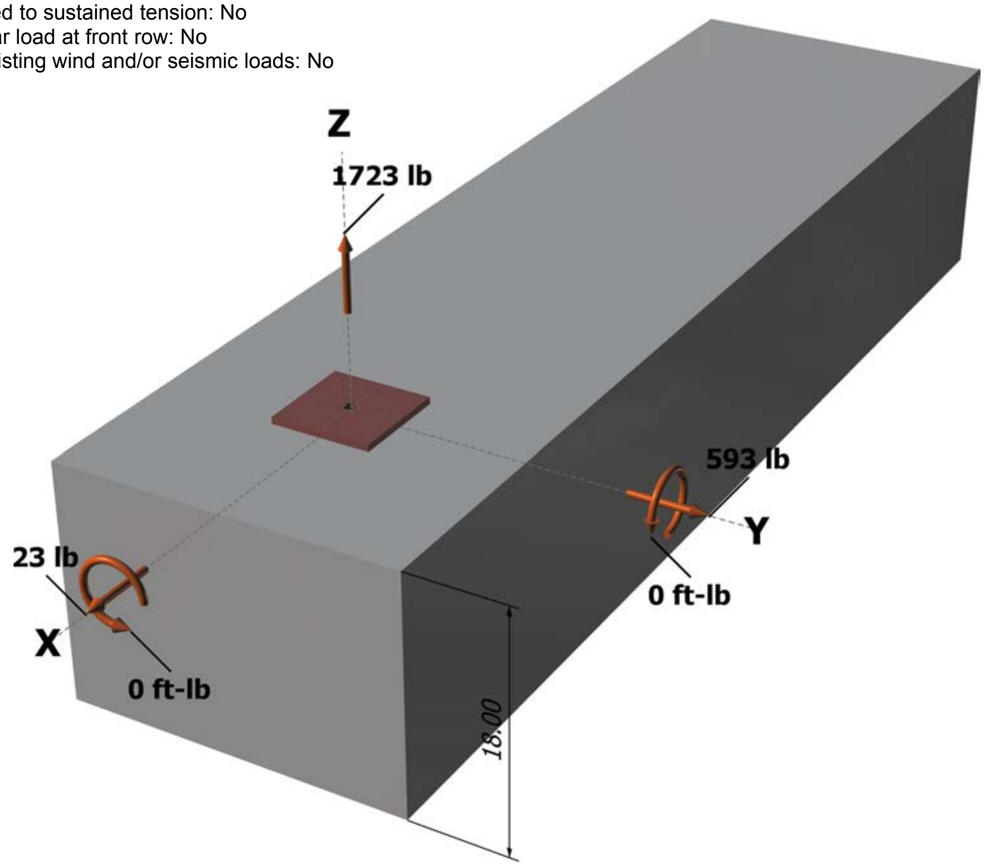
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'$_c$ (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>

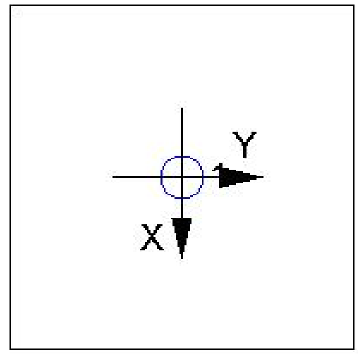
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1723.0	23.0	593.0	593.4
Sum	1723.0	23.0	593.0	593.4

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1723
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\,\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\,\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, øN_n (lb)	Ratio	Status
Steel	1723	6071	0.28	Pass
Concrete breakout	1723	5710	0.30	Pass
Adhesive	**1723**	**5365**	**0.32**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, øV_n (lb)	Ratio	Status
Steel	**593**	**3156**	**0.19**	**Pass (Governs)**
T Concrete breakout y+	593	3934	0.15	Pass
T Concrete breakout x+	23	3018	0.01	Pass
|| Concrete breakout y+	23	8508	0.00	Pass
|| Concrete breakout x+	593	6875	0.09	Pass
Concrete breakout, combined	-	-	0.15	Pass
Pryout	593	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.32	0.00	32.1 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

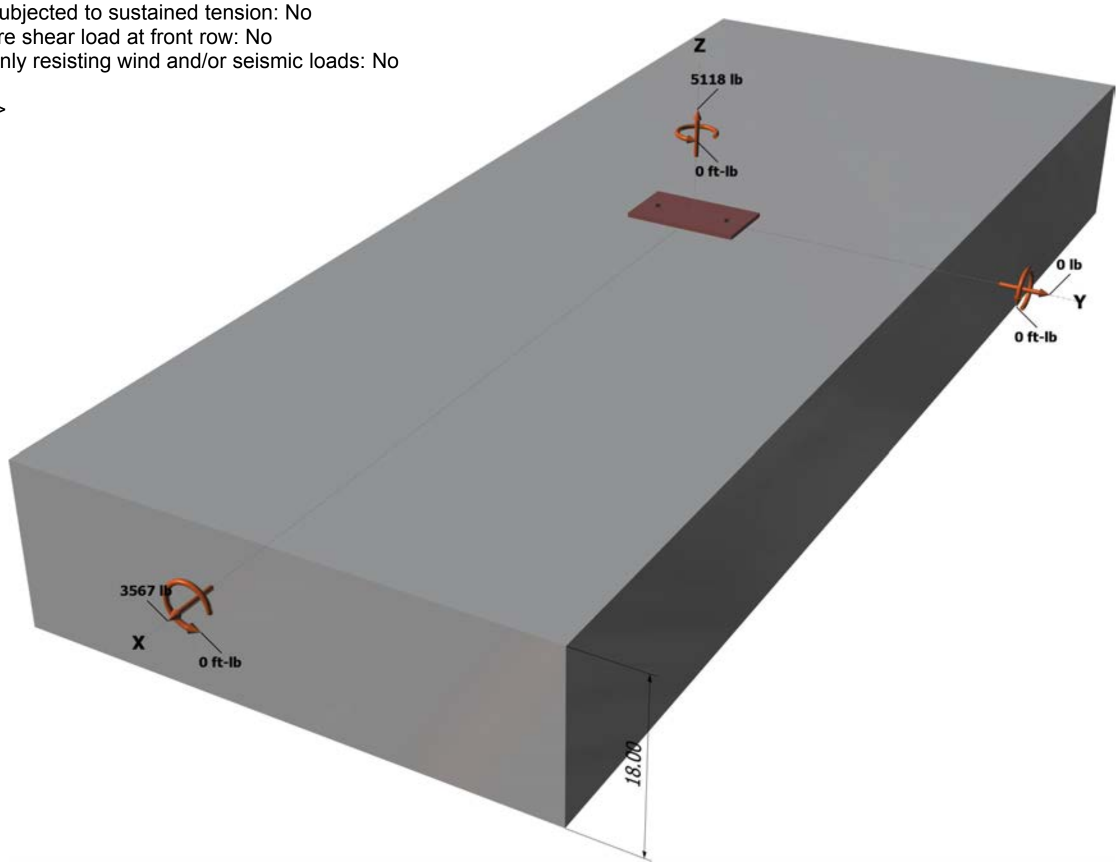
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

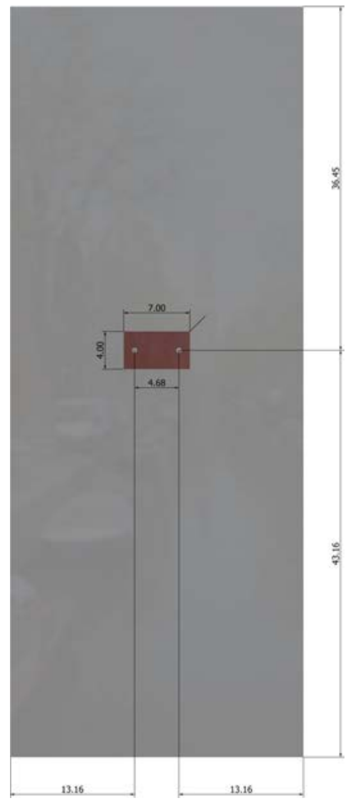
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'$_c$ (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



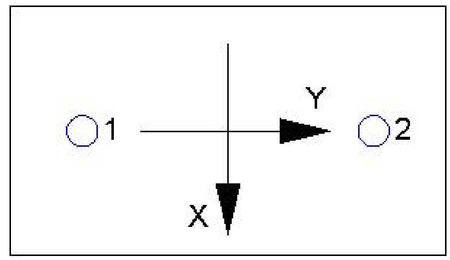
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2559.0	1783.5	0.0	1783.5
2	2559.0	1783.5	0.0	1783.5
Sum	5118.0	3567.0	0.0	3567.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 5118
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
408.24	324.00	1.000	1.000	1.00	1.000	12492	0.65	10231

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\,(A_{Vc}/A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
558.00	648.00	1.000	0.919	1.000	1.000	15593	0.70	8641

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	13.16	17908

$\phi V_{cbx} = \phi\,(2)(A_{Vc}/A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
710.64	779.34	1.000	1.000	1.000	17908	0.70	22862

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi \min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi \min|k_{cp}(A_{Na}/A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc}/A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
408.24	324.00	1.000	1.000	1.000	1.000	12492	15740	0.70

ϕV_{cpg} (lb)
20601

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	2559	6071	0.42	Pass
Concrete breakout	5118	10231	0.50	Pass
Adhesive	**5118**	**8093**	**0.63**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**1784**	**3156**	**0.57**	**Pass (Governs)**
T Concrete breakout x+	3567	8641	0.41	Pass
|| Concrete breakout y-	1784	22862	0.08	Pass
Pryout	3567	20601	0.17	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.63	0.57	119.8 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.