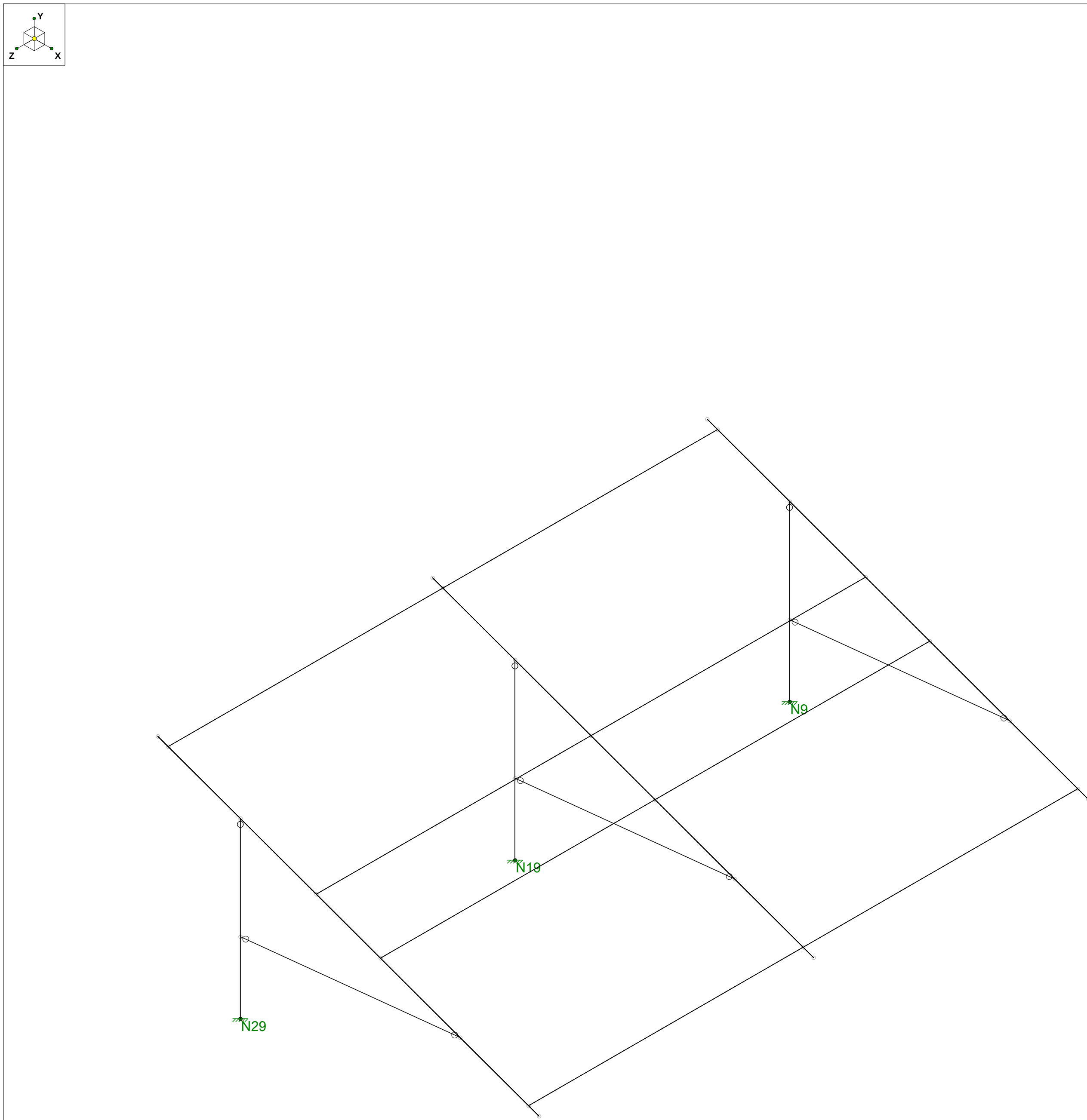


Schletter, Inc.	Standard FS Racking System	20° Tilt w/o Seismic Design
HCV	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

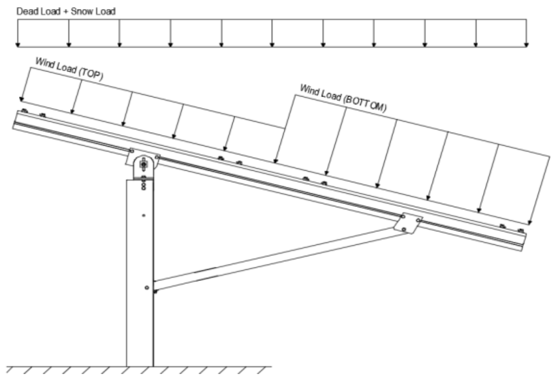
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	2000	mm	Height =	1900	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row = 2
Module Tilt = 20°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 20.62 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.91
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 150 mph
Height < 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 35.33 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$ = 1.05
$Cf+_{BOTTOM}$ = 1.65 *(Pressure)*
$Cf-_{TOP}$ = -2.12
$Cf-_{BOTTOM}$ = -1 *(Suction)*

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.

2.4 Seismic Loads - N/A

S_S =	0.00	R =	1.25
S_{DS} =	0.00	C_S =	0
S_1 =	0.00	ρ =	1.3
S_{D1} =	0.00	Ω =	1.25
T_a =	0.00	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W ^{M}
1.54D + 1.3E + 0.2S ^{R}
0.56D + 1.3E ^{R}
1.54D + 1.25E + 0.2S ^{O}
0.56D + 1.25E ^{O}

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W ^{M}
1.238D + 0.875E ^{O}
1.1785D + 0.65625E + 0.75S ^{O}
0.362D + 0.875E ^{O}

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

^{M} *Uses the minimum allowable module dead load.*
^{R} *Include redundancy factor of 1.3.*
^{O} *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

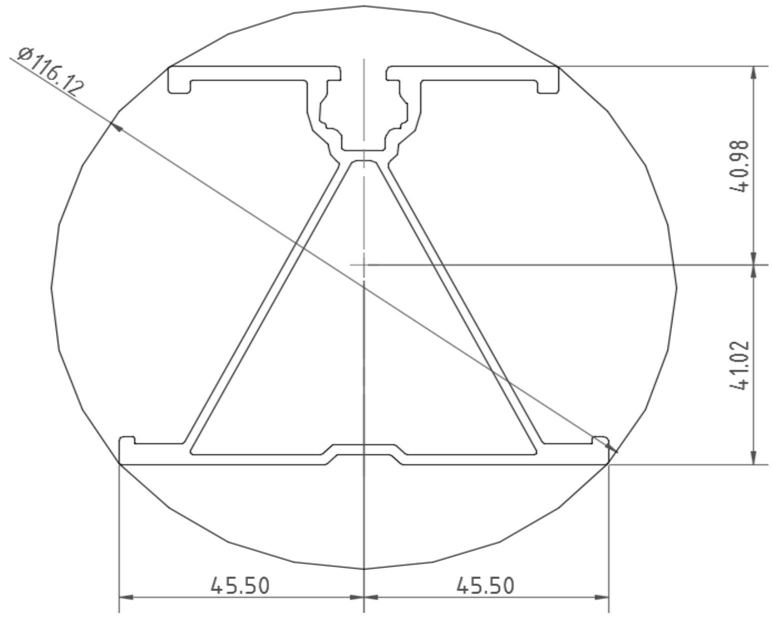
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	78	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.6	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	0.848	k-ft
M_z =	0.224	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	50%	

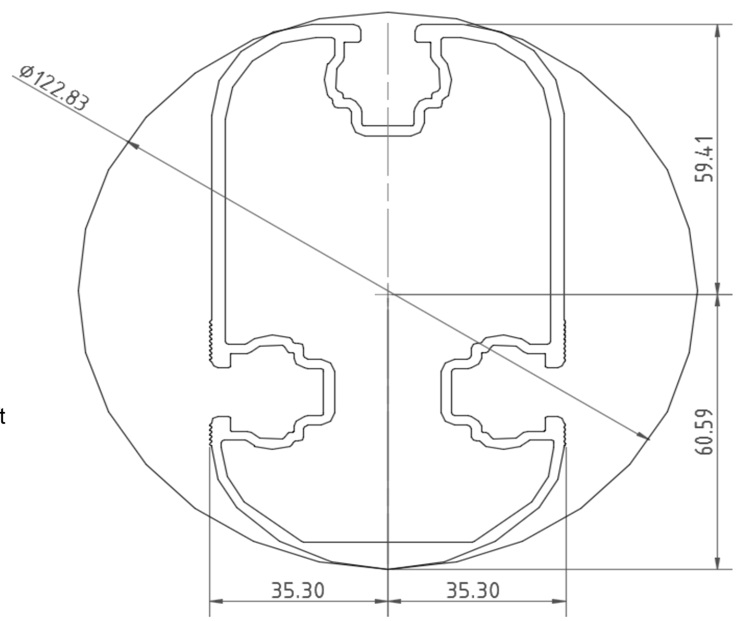


DETAIL VIEW

4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

Girder Type =	**T5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	81.77	in
$\Phi F_{ty\ AXIAL}$ =	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	30.06	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	31.56	ksi
S_y =	1.98	in^3
S_x =	1.32	in^3
E =	10100	ksi
I_y =	4.74	in^4
I_x =	1.83	in^4
A =	1.93	in^2
g =	2.32	lbs/ft
M_y =	3.842	k-ft
M_z =	0.000	k-ft
P_n =	3.113	k
$M_{y\ allowable}$ =	4.960	k-ft
$M_{z\ allowable}$ =	3.472	k-ft
$P_{n\ allowable}$ =	59.439	k
Utilization =	83%	

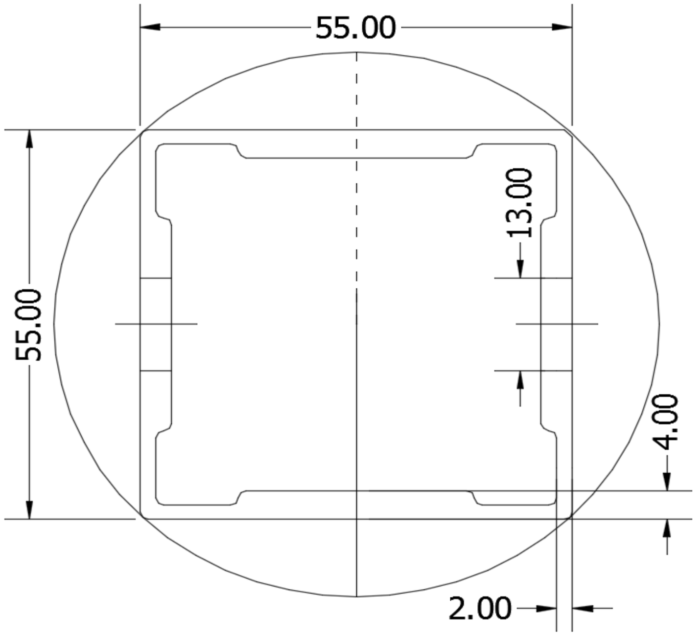


DETAIL VIEW

4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	74.80	in
$\Phi F_{ty\ AXIAL}$ =	9.61	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.008	k-ft
M_z =	0.000	k-ft
P_n =	7.247	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	9.441	k
Utilization =	77%	

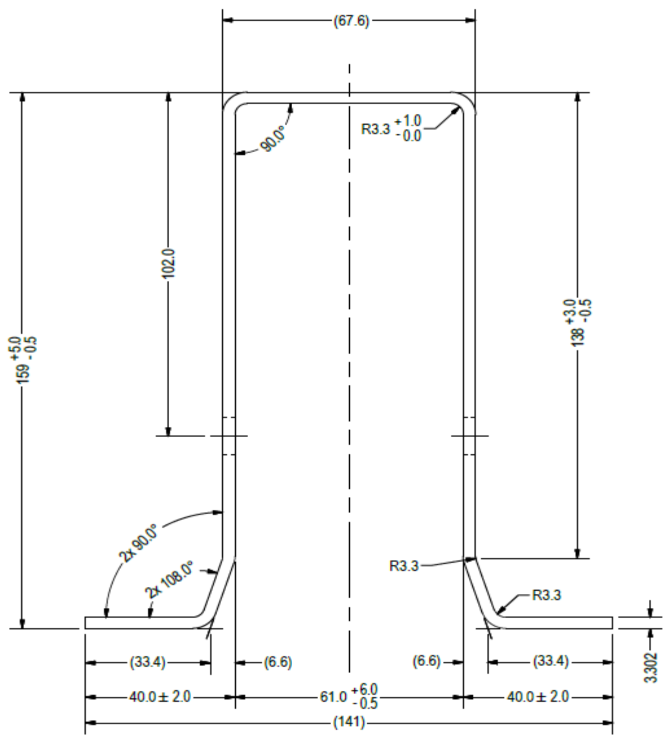


DETAIL VIEW

4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	72.67	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	15.219	k-ft
M_z =	0.000	k-ft
P_r =	5.567	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	38.013	k
Utilization =	96%	



DETAIL VIEW

5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	6.27	k
Maximum Lateral Load =	2.86	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

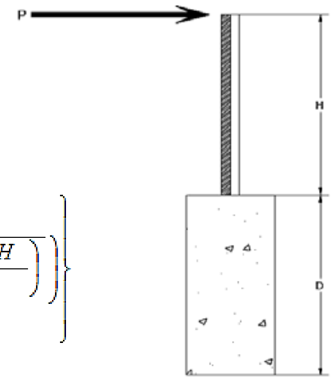
Lateral Force @ Top of Pole, P =	1.50	k
Height of Pole Above Grade, H =	5.06	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

$$S_3 = Min\left(D, 12'\right)$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\,{}^{P}\!/_{S_1 B}$$

$$D = \left\{0.5A\left(1+\sqrt{1+\left(\frac{4.36H}{A}\right)}\right)\right\}$$



Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

	Non-Constrained	
Lateral Force @ Top of Pole, P =	1.50	k
Height of Pole Above Grade, H =	5.06	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant $2.34P/(S_1B)$, A =	8.08	
Required Footing Depth, D =	11.84	ft
2nd Trial @ D_2 =	7.54	ft
Lateral Soil Bearing @ D/3, S_1 =	0.50	ksf
Lateral Soil Bearing @ D, S_3 =	1.51	ksf
Constant $2.34P/(S_1B)$, A =	3.48	
Required Footing Depth, D =	6.45	ft
3rd Trial @ D_3 =	7.00	ft
Lateral Soil Bearing @ D/3, S_1 =	0.47	ksf
Lateral Soil Bearing @ D, S_3 =	1.40	ksf
Constant $2.34P/(S_1B)$, A =	3.75	
Required Footing Depth, D =	6.79	ft

4th Trial @ D_4 =	6.90	ft
Lateral Soil Bearing @ D/3, S_1 =	0.46	ksf
Lateral Soil Bearing @ D, S_3 =	1.38	ksf
Constant $2.34P/(S_1B)$, A =	3.81	
Required Footing Depth, D =	6.86	ft
5th Trial @ D_5 =	6.88	ft
Lateral Soil Bearing @ D/3, S_1 =	0.46	ksf
Lateral Soil Bearing @ D, S_3 =	1.38	ksf
Constant $2.34P/(S_1B)$, A =	3.82	
Required Footing Depth, D =	7.00	ft

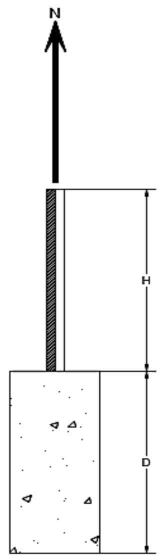
A 2ft diameter x 7ft deep footing unrestrained at ground level is required for the racking structure.

5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	2.88	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	1.88	k
Required Concrete Volume, V =	12.99	ft^3
Required Footing Depth, D =	4.25	ft

A 2ft diameter x 4.25ft deep footing unrestrained at ground level is required for the racking structure.



Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	6.21
2	0.4	0.2	118.10	6.11
3	0.6	0.2	118.10	6.00
4	0.8	0.2	118.10	5.90
5	1	0.2	118.10	5.79
6	1.2	0.2	118.10	5.69
7	1.4	0.2	118.10	5.59
8	1.6	0.2	118.10	5.48
9	1.8	0.2	118.10	5.38
10	2	0.2	118.10	5.28
11	2.2	0.2	118.10	5.17
12	2.4	0.2	118.10	5.07
13	2.6	0.2	118.10	4.96
14	2.8	0.2	118.10	4.86
15	3	0.2	118.10	4.76
16	3.2	0.2	118.10	4.65
17	3.4	0.2	118.10	4.55
18	3.6	0.2	118.10	4.45
19	3.8	0.2	118.10	4.34
20	4	0.2	118.10	4.24
21	4.2	0.2	118.10	4.13
22	0	0.0	0.00	4.13
23	0	0.0	0.00	4.13
24	0	0.0	0.00	4.13
25	0	0.0	0.00	4.13
26	0	0.0	0.00	4.13
27	0	0.0	0.00	4.13
28	0	0.0	0.00	4.13
29	0	0.0	0.00	4.13
30	0	0.0	0.00	4.13
31	0	0.0	0.00	4.13
32	0	0.0	0.00	4.13
33	0	0.0	0.00	4.13
34	0	0.0	0.00	4.13
Max	4.2	Sum	0.99	

5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	7.00	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	3.65	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	25.13	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

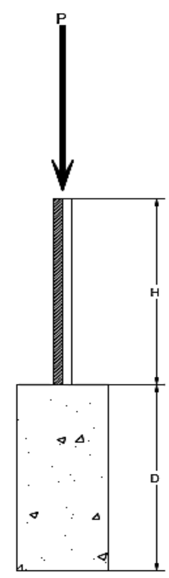
Weight of Concrete

Footing Volume	21.99	ft^3
Weight	3.19	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	3.77	k
1/3 Increase for Wind =	1.33	
Total Resistance =	11.31	k
Applied Force =	6.83	k
Utilization =	60%	

A 2ft diameter footing passes at a depth of 7ft.



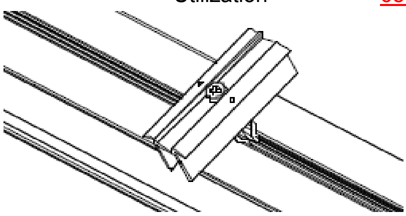
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

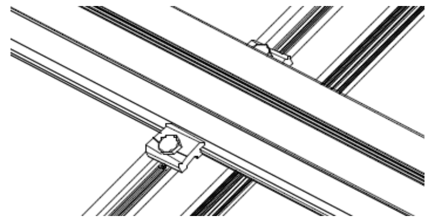
Fastening of Modules to Purlins

Maximum Uplifting Force =	0.829	k
Allowable Uplift =	1.214	k
Utilization =	68%	



Fastening of Purlins to Girders

Maximum Uplifting Force =	1.918	k
Allowable Uplift =	2.180	k
Utilization =	88%	

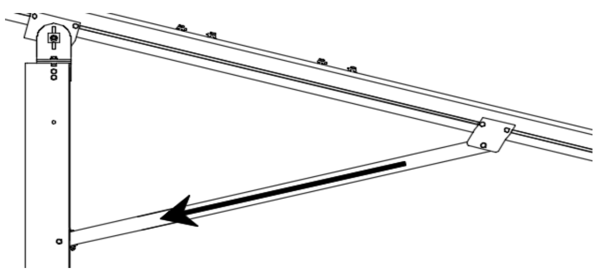


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load =	7.247	k
M10 Bolt Shear Capacity =	8.894	k
Utilization =	81%	

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

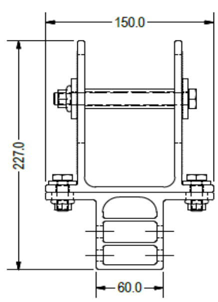


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

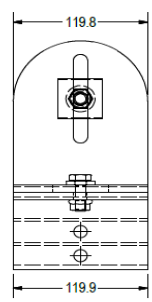
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

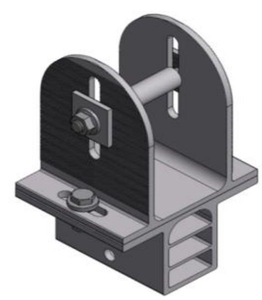
Maximum Tensile Load =	3.949	k
Allowable Load =	5.649	k
Utilization =	70%	



FRONT VIEW



SIDE VIEW



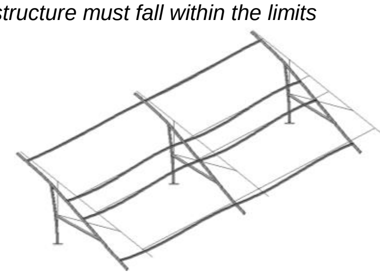
7. SEISMIC DESIGN

7.1 Seismic Drift - N/A

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	69.36	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	1.387	in
Max Drift, Δ_{MAX} =	0	in
N/A		

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 78 in

J = 0.432

215.785

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.6 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

$\varphi F_L St$= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in³

$M_{max}St$ = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 78

J = 0.432

137.226

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in³

$M_{max}Wk$ = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L= (φck2*√(BpE))/(1.6b/t)
φF_L= 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 81.7717 in
J = 1.98
105.231

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 30.1 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

Weak Axis:

3.4.14

L_b = 81.7717
J = 1.98
114.202

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.9

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φb[Bp-1.6Dp*b/t]
φF_L= 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$S2 = C_t$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.1 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in³

M_{max}St = 4.935 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in³

M_{max}Wk = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 30.80 ksi

φF_L= 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:		Weak Axis:	
3.4.14		**3.4.14**	
L_b =	74.8031 in	L_b =	74.8031
J =	0.942	J =	0.942
	116.737		116.737
$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$		$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$	
S1 =	0.51461	S1 =	0.51461
$S2 = \left(\frac{C_c}{1.6}\right)^2$		$S2 = \left(\frac{C_c}{1.6}\right)^2$	
S2 =	1701.56	S2 =	1701.56
φF_L=	φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]	φF_L=	φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L=	29.9 ksi	φF_L=	29.9
3.4.16		**3.4.16**	
b/t =	24.5	b/t =	24.5
$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$		$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$	
S1 =	12.2	S1 =	12.2
$S2 = \frac{k_1 Bp}{1.6Dp}$		$S2 = \frac{k_1 Bp}{1.6Dp}$	
S2 =	46.7	S2 =	46.7
φF_L=	φb[Bp-1.6Dp*b/t]	φF_L=	φb[Bp-1.6Dp*b/t]
φF_L=	28.2 ksi	φF_L=	28.2 ksi
3.4.16.1	Not Used	**3.4.16.1**	
Rb/t =	0.0	N/A for Weak Direction	
$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$			
S1 =	1.1		
$S2 = C_t$			
S2 =	141.0		
φF_L=	1.17φyFcy		
φF_L=	38.9 ksi		
3.4.18		**3.4.18**	
h/t =	24.5	h/t =	24.5
$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$		$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$	
S1 =	36.9	S1 =	36.9
m =	0.65	m =	0.65
C_0 =	27.5	C_0 =	27.5
Cc =	27.5	Cc =	27.5
$S2 = \frac{k_1 Bbr}{mDbr}$		$S2 = \frac{k_1 Bbr}{mDbr}$	
S2 =	77.3	S2 =	77.3
φF_L=	1.3φyFcy	φF_L=	1.3φyFcy
φF_L=	43.2 ksi	φF_L=	43.2 ksi
φF_LSt=	28.2 ksi	φF_LWk=	28.2 ksi
Ix =	279836 mm^4	Iy =	279836 mm^4
	0.672 in^4		0.672 in^4
y =	27.5 mm	x =	27.5 mm
Sx =	0.621 in^3	Sy =	0.621 in^3
M_{max}St =	1.460 k-ft	M_{max}Wk =	1.460 k-ft

<u>Compression</u>

3.4.7

λ = 1.73045

r = 0.81 in

$$S1^{*} = \frac{Bc - Fcy}{1.6Dc^{*}}$$

$S1^{*}$ = 0.33515

$$S2^{*} = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^{*}$ = 1.23671

φcc = 0.82226

φF_L= (φccFcy)/(λ²)

φF_L= 9.61085 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 9.61 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 9.89 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	72.67	in	
Pr =	5.57	k	(LRFD Factored Load)
Mr (Strong) =	15.22	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	104.56	
4.71√(E/Fy) =	103.55 =>	kL/r > 4.71√(E/Fy)
Fcr =	22.96 ksi	
Fe =	26.18 ksi	
Pn =	51.204 k	

Torsional/Flexural Torsional Buckling:

Fcr =	17.0464 ksi
Fey =	66.785 ksi
Fez =	21.7259 ksi
Pn =	38.0134 k

Bending (Strong Axis):

Yielding:			
Mn =	21.95 k-ft		
Flange Local Buckling:			
Mn =	19.207 k-ft		
Pr/Pc =	0.1627 <	0.2	
Utilization =	0.96 <	1.0	OK

Bending (Weak Axis):

Yielding:			
Mn =	14.65 k-ft		
Flange Local Buckling:			
Mn =	14.39 k-ft		
Pr/Pc =	0.163 <	0.2	
Utilization =	0.00 <	1.0	OK

Combined Forces

Utilization = 96%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL								

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-9.843	-9.843	0	0
2	M11	Y	-9.843	-9.843	0	0
3	M12	Y	-9.843	-9.843	0	0
4	M13	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-5.454	-5.454	0	0
2	M11	Y	-5.454	-5.454	0	0
3	M12	Y	-5.454	-5.454	0	0
4	M13	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-63.565	-63.565	0	0
2	M11	Y	-63.565	-63.565	0	0
3	M12	Y	-63.565	-63.565	0	0
4	M13	Y	-63.565	-63.565	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-121.698	-121.698	0	0
2	M11	y	-121.698	-121.698	0	0
3	M12	y	-191.24	-191.24	0	0
4	M13	y	-191.24	-191.24	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	245.714	245.714	0	0
2	M11	y	245.714	245.714	0	0
3	M12	y	115.903	115.903	0	0
4	M13	y	115.903	115.903	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65..	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	309.677	2	2339.592	2	114.037	1	.181	1	0	3	8.733	1
2		min	-603.035	3	-1745.182	3	-117.12	3	-.134	3	-.002	2	-1.033	3
3	N19	max	2163.455	2	5592.814	2	0	2	0	1	0	2	11.85	1
4		min	-2009.618	3	-4819.847	3	0	14	0	3	0	3	-.624	3
5	N29	max	309.677	2	2339.592	2	117.12	3	.134	3	.002	2	8.733	1
6		min	-603.035	3	-1745.182	3	-114.037	1	-.181	1	0	3	-1.033	3
7	Totals:	max	2782.809	2	10271.999	2	0	1						
8		min	-3215.688	3	-8310.212	3	0	3						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.004	2	0	3	0	1	0	1	0	1
2			min	0	1	0	3	0	1	0	1	0	1	0	1
3		2	max	11.54	3	329.088	3	24.901	3	.061	3	.25	1	.277	2
4			min	-184.566	1	-745.447	2	-122.512	1	-.185	2	-.041	3	-.121	3
5		3	max	11.07	3	327.798	3	24.901	3	.061	3	.17	1	.767	2
6			min	-185.192	1	-747.166	2	-122.512	1	-.185	2	-.025	3	-.337	3
7		4	max	10.601	3	326.509	3	24.901	3	.061	3	.089	1	1.258	2
8			min	-185.818	1	-748.885	2	-122.512	1	-.185	2	-.008	3	-.552	3
9		5	max	1248.826	3	676.353	2	35.738	3	.007	3	.119	1	1.487	2
10			min	-3086.122	2	-278.117	3	-144.911	1	-.058	2	-.042	3	-.655	3
11		6	max	1248.356	3	674.634	2	35.738	3	.007	3	.031	2	1.044	2
12			min	-3086.747	2	-279.407	3	-144.911	1	-.058	2	-.018	3	-.472	3
13		7	max	1247.887	3	672.914	2	35.738	3	.007	3	.005	3	.602	2
14			min	-3087.373	2	-280.696	3	-144.911	1	-.058	2	-.072	1	-.288	3
15		8	max	1247.418	3	671.195	2	35.738	3	.007	3	.029	3	.161	2
16			min	-3087.999	2	-281.985	3	-144.911	1	-.058	2	-.167	1	-.103	3
17		9	max	1263.041	3	23.09	1	58.154	3	-.002	15	.1	1	-.002	15
18			min	-3218.211	2	-3.448	3	-198.298	1	-.156	2	-.008	3	-.047	2
19		10	max	1262.572	3	21.371	1	58.154	3	-.002	15	.03	3	-.003	15
20			min	-3218.837	2	-4.738	3	-198.298	1	-.156	2	-.03	2	-.061	2
21		11	max	1262.102	3	19.652	1	58.154	3	-.002	15	.068	3	-.003	15
22			min	-3219.463	2	-6.027	3	-198.298	1	-.156	2	-.16	1	-.074	2
23		12	max	1272.353	3	626.809	3	-1.012	15	.16	3	.119	1	.08	1
24			min	-3342.954	2	-424.282	1	-77.911	3	-.181	2	.003	15	-.216	3
25		13	max	1271.883	3	625.519	3	-1.012	15	.16	3	.1	1	.359	1
26			min	-3343.579	2	-426.002	1	-77.911	3	-.181	2	-.033	3	-.627	3
27		14	max	1271.414	3	624.23	3	-1.012	15	.16	3	.081	1	.639	1
28			min	-3344.205	2	-427.721	1	-77.911	3	-.181	2	-.084	3	-1.037	3
29		15	max	1270.945	3	622.941	3	-1.012	15	.16	3	.067	2	.921	1
30			min	-3344.831	2	-429.44	1	-77.911	3	-.181	2	-.135	3	-1.446	3
31		16	max	185.761	1	424.25	1	28.89	3	.079	1	.013	3	.701	1
32			min	-12.696	3	-657.111	3	-119.483	1	-.217	3	-.102	1	-1.103	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
33		17	max	185.136	1	422.531	1	28.89	3	.079	1	.032	3	.423	1
34			min	-13.166	3	-658.4	3	-119.483	1	-.217	3	-.18	1	-.672	3
35		18	max	184.51	1	420.812	1	28.89	3	.079	1	.051	3	.146	1
36			min	-13.635	3	-659.689	3	-119.483	1	-.217	3	-.258	1	-.239	3
37		19	max	0	1	0	5	0	1	0	1	0	1	0	1
38			min	0	1	-.001	2	0	3	0	1	0	1	0	1
39	M4	1	max	0	1	.006	2	0	1	0	1	0	1	0	1
40			min	0	1	-.002	3	0	1	0	1	0	1	0	1
41		2	max	40.445	10	767.66	3	0	1	0	1	0	1	.464	2
42			min	-145.49	1	-1550.791	2	0	1	0	1	0	1	-.234	3
43		3	max	39.924	10	766.371	3	0	1	0	1	0	1	1.482	2
44			min	-146.116	1	-1552.51	2	0	1	0	1	0	1	-.738	3
45		4	max	39.402	10	765.082	3	0	1	0	1	0	1	2.501	2
46			min	-146.741	1	-1554.229	2	0	1	0	1	0	1	-1.24	3
47		5	max	3227.283	3	1601.243	2	0	1	0	1	0	1	2.942	2
48			min	-6569.913	2	-832.366	3	0	1	0	1	0	1	-1.448	3
49		6	max	3226.814	3	1599.524	2	0	1	0	1	0	1	1.891	2
50			min	-6570.539	2	-833.655	3	0	1	0	1	0	1	-.902	3
51		7	max	3226.345	3	1597.804	2	0	1	0	1	0	1	.842	2
52			min	-6571.164	2	-834.945	3	0	1	0	1	0	1	-.354	3
53		8	max	3225.875	3	1596.085	2	0	1	0	1	0	1	.194	3
54			min	-6571.79	2	-836.234	3	0	1	0	1	0	1	-.207	1
55		9	max	3165.375	3	32.405	3	0	1	0	1	0	1	.457	3
56			min	-6515.098	2	-159.981	2	0	1	0	1	0	1	-.685	2
57		10	max	3164.906	3	31.115	3	0	1	0	1	0	1	.436	3
58			min	-6515.724	2	-161.7	2	0	1	0	1	0	1	-.579	2
59		11	max	3164.437	3	29.826	3	0	1	0	1	0	1	.416	3
60			min	-6516.35	2	-163.419	2	0	1	0	1	0	1	-.473	2
61		12	max	3114.683	3	1866.631	3	0	1	0	1	0	1	.043	1
62			min	-6473.101	2	-1464.164	1	0	1	0	1	0	1	-.172	3
63		13	max	3114.214	3	1865.341	3	0	1	0	1	0	1	1.004	1
64			min	-6473.727	2	-1465.883	1	0	1	0	1	0	1	-1.396	3
65		14	max	3113.744	3	1864.052	3	0	1	0	1	0	1	1.967	1
66			min	-6474.353	2	-1467.602	1	0	1	0	1	0	1	-2.62	3
67		15	max	3113.275	3	1862.762	3	0	1	0	1	0	1	2.93	1
68			min	-6474.979	2	-1469.321	1	0	1	0	1	0	1	-3.842	3
69		16	max	146.854	1	1362.889	1	0	1	0	1	0	1	2.231	1
70			min	-39.224	10	-1792.578	3	0	1	0	1	0	1	-2.918	3
71		17	max	146.229	1	1361.17	1	0	1	0	1	0	1	1.337	1
72			min	-39.746	10	-1793.867	3	0	1	0	1	0	1	-1.742	3
73		18	max	145.603	1	1359.451	1	0	1	0	1	0	1	.444	1
74			min	-40.267	10	-1795.157	3	0	1	0	1	0	1	-.564	3
75		19	max	0	1	0	5	0	1	0	1	0	1	0	1
76			min	0	1	-.002	3	0	1	0	1	0	1	0	1
77	M7	1	max	0	1	.004	2	0	1	0	1	0	1	0	1
78			min	0	1	0	3	0	3	0	1	0	1	0	1
79		2	max	11.54	3	329.088	3	122.512	1	.185	2	.041	3	.277	2
80			min	-184.566	1	-745.447	2	-24.901	3	-.061	3	-.25	1	-.121	3
81		3	max	11.07	3	327.798	3	122.512	1	.185	2	.025	3	.767	2
82			min	-185.192	1	-747.166	2	-24.901	3	-.061	3	-.17	1	-.337	3
83		4	max	10.601	3	326.509	3	122.512	1	.185	2	.008	3	1.258	2
84			min	-185.818	1	-748.885	2	-24.901	3	-.061	3	-.089	1	-.552	3
85		5	max	1248.826	3	676.353	2	144.911	1	.058	2	.042	3	1.487	2
86			min	-3086.122	2	-278.117	3	-35.738	3	-.007	3	-.119	1	-.655	3
87		6	max	1248.356	3	674.634	2	144.911	1	.058	2	.018	3	1.044	2
88			min	-3086.747	2	-279.407	3	-35.738	3	-.007	3	-.031	2	-.472	3
89		7	max	1247.887	3	672.914	2	144.911	1	.058	2	.072	1	.602	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
90			min	-3087.373	2	-280.696	3	-35.738	3	-.007	3	-.005	3	-.288	3
91		8	max	1247.418	3	671.195	2	144.911	1	.058	2	.167	1	.161	2
92			min	-3087.999	2	-281.985	3	-35.738	3	-.007	3	-.029	3	-.103	3
93		9	max	1263.041	3	23.09	1	198.298	1	.156	2	.008	3	-.002	15
94			min	-3218.211	2	-3.448	3	-58.154	3	.002	15	-.1	1	-.047	2
95		10	max	1262.572	3	21.371	1	198.298	1	.156	2	.03	2	-.003	15
96			min	-3218.837	2	-4.738	3	-58.154	3	.002	15	-.03	3	-.061	2
97		11	max	1262.102	3	19.652	1	198.298	1	.156	2	.16	1	-.003	15
98			min	-3219.463	2	-6.027	3	-58.154	3	.002	15	-.068	3	-.074	2
99		12	max	1272.353	3	626.809	3	77.911	3	.181	2	-.003	15	.08	1
100			min	-3342.954	2	-424.282	1	1.012	15	-.16	3	-.119	1	-.216	3
101		13	max	1271.883	3	625.519	3	77.911	3	.181	2	.033	3	.359	1
102			min	-3343.579	2	-426.002	1	1.012	15	-.16	3	-.1	1	-.627	3
103		14	max	1271.414	3	624.23	3	77.911	3	.181	2	.084	3	.639	1
104			min	-3344.205	2	-427.721	1	1.012	15	-.16	3	-.081	1	-1.037	3
105		15	max	1270.945	3	622.941	3	77.911	3	.181	2	.135	3	.921	1
106			min	-3344.831	2	-429.44	1	1.012	15	-.16	3	-.067	2	-1.446	3
107		16	max	185.761	1	424.25	1	119.483	1	.217	3	.102	1	.701	1
108			min	-12.696	3	-657.111	3	-28.89	3	-.079	1	-.013	3	-1.103	3
109		17	max	185.136	1	422.531	1	119.483	1	.217	3	.18	1	.423	1
110			min	-13.166	3	-658.4	3	-28.89	3	-.079	1	-.032	3	-.672	3
111		18	max	184.51	1	420.812	1	119.483	1	.217	3	.258	1	.146	1
112			min	-13.635	3	-659.689	3	-28.89	3	-.079	1	-.051	3	-.239	3
113		19	max	0	1	0	5	0	3	0	1	0	1	0	1
114			min	0	1	-.001	2	0	1	0	1	0	1	0	1
115	M10	1	max	119.508	1	420.408	1	14.075	3	.005	1	.298	1	.079	1
116			min	-28.894	3	-660.98	3	-184.317	1	-.018	3	-.06	3	-.217	3
117		2	max	119.508	1	298.197	1	15.622	3	.005	1	.176	1	.198	3
118			min	-28.894	3	-487.77	3	-155.831	1	-.018	3	-.05	3	-.18	1
119		3	max	119.508	1	175.986	1	17.169	3	.005	1	.094	2	.488	3
120			min	-28.894	3	-314.56	3	-127.345	1	-.018	3	-.038	3	-.351	1
121		4	max	119.508	1	53.775	1	18.716	3	.005	1	.032	2	.652	3
122			min	-28.894	3	-141.351	3	-98.859	1	-.018	3	-.025	3	-.434	1
123		5	max	119.508	1	31.859	3	20.263	3	.005	1	-.003	15	.692	3
124			min	-28.894	3	-71.552	2	-70.373	1	-.018	3	-.069	1	-.429	1
125		6	max	119.508	1	205.069	3	21.81	3	.005	1	.004	3	.606	3
126			min	-28.894	3	-190.646	1	-57.308	2	-.018	3	-.11	1	-.335	1
127		7	max	119.508	1	378.279	3	23.357	3	.005	1	.021	3	.396	3
128			min	-28.894	3	-312.857	1	-46.094	2	-.018	3	-.13	1	-.154	1
129		8	max	119.508	1	551.489	3	26.543	9	.005	1	.038	3	.13	2
130			min	-28.894	3	-435.068	1	-34.88	2	-.018	3	-.133	2	.002	15
131		9	max	119.508	1	724.699	3	45.047	9	.005	1	.057	3	.482	2
132			min	-28.894	3	-557.278	1	-23.665	2	-.018	3	-.155	2	-.401	3
133		10	max	119.508	1	679.489	1	20.482	10	.005	1	.076	3	.921	1
134			min	-28.894	3	-897.908	3	-72.056	1	-.018	3	-.168	2	-.987	3
135		11	max	119.508	1	557.278	1	23.665	2	.018	3	.057	3	.482	2
136			min	-28.894	3	-724.699	3	-45.047	9	-.005	1	-.155	2	-.401	3
137		12	max	119.508	1	435.068	1	34.88	2	.018	3	.038	3	.13	2
138			min	-28.894	3	-551.489	3	-26.543	9	-.005	1	-.133	2	.002	15
139		13	max	119.508	1	312.857	1	46.094	2	.018	3	.021	3	.396	3
140			min	-28.894	3	-378.279	3	-23.357	3	-.005	1	-.13	1	-.154	1
141		14	max	119.508	1	190.646	1	57.308	2	.018	3	.004	3	.606	3
142			min	-28.894	3	-205.069	3	-21.81	3	-.005	1	-.11	1	-.335	1
143		15	max	119.508	1	71.552	2	70.373	1	.018	3	-.003	15	.692	3
144			min	-28.894	3	-31.859	3	-20.263	3	-.005	1	-.069	1	-.429	1
145		16	max	119.508	1	141.351	3	98.859	1	.018	3	.032	2	.652	3
146			min	-28.894	3	-53.775	1	-18.716	3	-.005	1	-.025	3	-.434	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
147		17	max	119.508	1	314.56	3	127.345	1	.018	3	.094	2	.488	3
148			min	-28.894	3	-175.986	1	-17.169	3	-.005	1	-.038	3	-.351	1
149		18	max	119.508	1	487.77	3	155.831	1	.018	3	.176	1	.198	3
150			min	-28.894	3	-298.197	1	-15.622	3	-.005	1	-.05	3	-.18	1
151		19	max	119.508	1	660.98	3	184.317	1	.018	3	.298	1	.079	1
152			min	-28.894	3	-420.408	1	-14.075	3	-.005	1	-.06	3	-.217	3
153	M11	1	max	168.57	1	442.688	1	10.579	3	.008	3	.355	1	.046	1
154			min	-135.768	3	-636.199	3	-197.678	1	-.018	2	-.045	3	-.185	3
155		2	max	168.57	1	320.477	1	12.126	3	.008	3	.223	1	.212	3
156			min	-135.768	3	-462.989	3	-169.193	1	-.018	2	-.036	3	-.241	2
157		3	max	168.57	1	198.266	1	13.673	3	.008	3	.121	2	.484	3
158			min	-135.768	3	-289.779	3	-140.707	1	-.018	2	-.027	3	-.421	2
159		4	max	168.57	1	76.056	1	15.22	3	.008	3	.053	2	.63	3
160			min	-135.768	3	-116.569	3	-112.221	1	-.018	2	-.017	3	-.516	1
161		5	max	168.57	1	56.641	3	16.766	3	.008	3	.003	10	.652	3
162			min	-135.768	3	-47.037	2	-83.735	1	-.018	2	-.051	1	-.527	1
163		6	max	168.57	1	229.85	3	18.313	3	.008	3	.008	3	.548	3
164			min	-135.768	3	-168.366	1	-67.355	2	-.018	2	-.101	1	-.449	1
165		7	max	168.57	1	403.06	3	19.86	3	.008	3	.021	3	.32	3
166			min	-135.768	3	-290.577	1	-56.141	2	-.018	2	-.131	1	-.285	2
167		8	max	168.57	1	576.27	3	21.407	3	.008	3	.036	3	0	15
168			min	-135.768	3	-412.787	1	-44.927	2	-.018	2	-.142	2	-.037	2
169		9	max	168.57	1	749.48	3	38.345	9	.008	3	.052	3	.313	1
170			min	-135.768	3	-534.998	1	-33.712	2	-.018	2	-.17	2	-.512	3
171		10	max	168.57	1	922.69	3	58.694	1	.018	2	.07	3	.743	1
172			min	-135.768	3	-657.209	1	-24.998	10	0	15	-.191	2	-1.116	3
173		11	max	168.57	1	534.998	1	33.712	2	.018	2	.052	3	.313	1
174			min	-135.768	3	-749.48	3	-38.345	9	-.008	3	-.17	2	-.512	3
175		12	max	168.57	1	412.787	1	44.927	2	.018	2	.036	3	0	15
176			min	-135.768	3	-576.27	3	-21.407	3	-.008	3	-.142	2	-.037	2
177		13	max	168.57	1	290.577	1	56.141	2	.018	2	.021	3	.32	3
178			min	-135.768	3	-403.06	3	-19.86	3	-.008	3	-.131	1	-.285	2
179		14	max	168.57	1	168.366	1	67.355	2	.018	2	.008	3	.548	3
180			min	-135.768	3	-229.85	3	-18.313	3	-.008	3	-.101	1	-.449	1
181		15	max	168.57	1	47.037	2	83.735	1	.018	2	.003	10	.652	3
182			min	-135.768	3	-56.641	3	-16.766	3	-.008	3	-.051	1	-.527	1
183		16	max	168.57	1	116.569	3	112.221	1	.018	2	.053	2	.63	3
184			min	-135.768	3	-76.056	1	-15.22	3	-.008	3	-.017	3	-.516	1
185		17	max	168.57	1	289.779	3	140.707	1	.018	2	.121	2	.484	3
186			min	-135.768	3	-198.266	1	-13.673	3	-.008	3	-.027	3	-.421	2
187		18	max	168.57	1	462.989	3	169.193	1	.018	2	.223	1	.212	3
188			min	-135.768	3	-320.477	1	-12.126	3	-.008	3	-.036	3	-.241	2
189		19	max	168.57	1	636.199	3	197.678	1	.018	2	.355	1	.046	1
190			min	-135.768	3	-442.688	1	-10.579	3	-.008	3	-.045	3	-.185	3
191	M12	1	max	22.64	3	643.97	2	16.117	3	.004	3	.38	1	.098	2
192			min	-51.652	1	-280.959	3	-203.598	1	-.013	2	-.068	3	.001	15
193		2	max	22.64	3	475.041	2	17.664	3	.004	3	.243	1	.207	3
194			min	-51.652	1	-201.502	3	-175.112	1	-.013	2	-.056	3	-.306	2
195		3	max	22.64	3	306.113	2	19.211	3	.004	3	.138	2	.324	3
196			min	-51.652	1	-122.045	3	-146.626	1	-.013	2	-.042	3	-.588	2
197		4	max	22.64	3	137.184	2	20.758	3	.004	3	.065	2	.383	3
198			min	-51.652	1	-42.587	3	-118.14	1	-.013	2	-.028	3	-.748	2
199		5	max	22.64	3	36.87	3	22.305	3	.004	3	.007	10	.385	3
200			min	-51.652	1	-31.744	2	-89.654	1	-.013	2	-.044	1	-.786	2
201		6	max	22.64	3	116.328	3	23.852	3	.004	3	.004	3	.33	3
202			min	-51.652	1	-200.673	2	-73.4	2	-.013	2	-.098	1	-.702	2
203		7	max	22.64	3	195.785	3	25.399	3	.004	3	.022	3	.217	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
204			min	-51.652	1	-369.602	2	-62.186	2	-.013	2	-.132	1	-.496	2
205		8	max	22.64	3	275.243	3	26.946	3	.004	3	.041	3	.047	3
206			min	-51.652	1	-538.53	2	-50.972	2	-.013	2	-.148	2	-.169	2
207		9	max	22.64	3	354.7	3	35.996	9	.004	3	.061	3	.281	2
208			min	-51.652	1	-707.459	2	-39.758	2	-.013	2	-.18	2	-.181	3
209		10	max	22.64	3	434.158	3	54.501	9	.004	3	.082	3	.853	2
210			min	-51.652	1	-876.387	2	-28.543	2	-.013	2	-.205	2	-.465	3
211		11	max	22.64	3	707.459	2	39.758	2	.013	2	.061	3	.281	2
212			min	-51.652	1	-354.7	3	-35.996	9	-.004	3	-.18	2	-.181	3
213		12	max	22.64	3	538.53	2	50.972	2	.013	2	.041	3	.047	3
214			min	-51.652	1	-275.243	3	-26.946	3	-.004	3	-.148	2	-.169	2
215		13	max	22.64	3	369.602	2	62.186	2	.013	2	.022	3	.217	3
216			min	-51.652	1	-195.785	3	-25.399	3	-.004	3	-.132	1	-.496	2
217		14	max	22.64	3	200.673	2	73.4	2	.013	2	.004	3	.33	3
218			min	-51.652	1	-116.328	3	-23.852	3	-.004	3	-.098	1	-.702	2
219		15	max	22.64	3	31.744	2	89.654	1	.013	2	.007	10	.385	3
220			min	-51.652	1	-36.87	3	-22.305	3	-.004	3	-.044	1	-.786	2
221		16	max	22.64	3	42.587	3	118.14	1	.013	2	.065	2	.383	3
222			min	-51.652	1	-137.184	2	-20.758	3	-.004	3	-.028	3	-.748	2
223		17	max	22.64	3	122.045	3	146.626	1	.013	2	.138	2	.324	3
224			min	-51.652	1	-306.113	2	-19.211	3	-.004	3	-.042	3	-.588	2
225		18	max	22.64	3	201.502	3	175.112	1	.013	2	.243	1	.207	3
226			min	-51.652	1	-475.041	2	-17.664	3	-.004	3	-.056	3	-.306	2
227		19	max	22.64	3	280.959	3	203.598	1	.013	2	.38	1	.098	2
228			min	-51.652	1	-643.97	2	-16.117	3	-.004	3	-.068	3	.001	15
229	M13	1	max	24.902	3	744.972	2	12.036	3	.011	3	.291	1	.185	2
230			min	-122.389	1	-330.405	3	-183.478	1	-.028	2	-.049	3	-.061	3
231		2	max	24.902	3	576.043	2	13.583	3	.011	3	.169	1	.148	3
232			min	-122.389	1	-250.947	3	-154.992	1	-.028	2	-.04	3	-.292	2
233		3	max	24.902	3	407.115	2	15.13	3	.011	3	.089	2	.301	3
234			min	-122.389	1	-171.49	3	-126.506	1	-.028	2	-.03	3	-.647	2
235		4	max	24.902	3	238.186	2	16.677	3	.011	3	.027	2	.396	3
236			min	-122.389	1	-92.032	3	-98.02	1	-.028	2	-.022	9	-.88	2
237		5	max	24.902	3	69.257	2	18.224	3	.011	3	-.003	15	.434	3
238			min	-122.389	1	-12.575	3	-69.535	1	-.028	2	-.074	1	-.991	2
239		6	max	24.902	3	66.882	3	19.771	3	.011	3	.008	3	.414	3
240			min	-122.389	1	-99.671	2	-56.969	2	-.028	2	-.114	1	-.98	2
241		7	max	24.902	3	146.34	3	21.318	3	.011	3	.023	3	.337	3
242			min	-122.389	1	-268.6	2	-45.755	2	-.028	2	-.134	1	-.847	2
243		8	max	24.902	3	225.797	3	27.089	9	.011	3	.039	3	.203	3
244			min	-122.389	1	-437.528	2	-34.541	2	-.028	2	-.137	2	-.592	2
245		9	max	24.902	3	305.255	3	45.594	9	.011	3	.056	3	.011	3
246			min	-122.389	1	-606.457	2	-23.326	2	-.028	2	-.158	2	-.228	1
247		10	max	24.902	3	775.386	2	20.384	10	.011	3	.074	3	.284	2
248			min	-122.389	1	-384.712	3	-72.895	1	-.028	2	-.171	2	-.238	3
249		11	max	24.902	3	606.457	2	23.326	2	.028	2	.056	3	.011	3
250			min	-122.389	1	-305.255	3	-45.594	9	-.011	3	-.158	2	-.228	1
251		12	max	24.902	3	437.528	2	34.541	2	.028	2	.039	3	.203	3
252			min	-122.389	1	-225.797	3	-27.089	9	-.011	3	-.137	2	-.592	2
253		13	max	24.902	3	268.6	2	45.755	2	.028	2	.023	3	.337	3
254			min	-122.389	1	-146.34	3	-21.318	3	-.011	3	-.134	1	-.847	2
255		14	max	24.902	3	99.671	2	56.969	2	.028	2	.008	3	.414	3
256			min	-122.389	1	-66.882	3	-19.771	3	-.011	3	-.114	1	-.98	2
257		15	max	24.902	3	12.575	3	69.535	1	.028	2	-.003	15	.434	3
258			min	-122.389	1	-69.257	2	-18.224	3	-.011	3	-.074	1	-.991	2
259		16	max	24.902	3	92.032	3	98.02	1	.028	2	.027	2	.396	3
260			min	-122.389	1	-238.186	2	-16.677	3	-.011	3	-.022	9	-.88	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
261		17	max	24.902	3	171.49	3	126.506	1	.028	2	.089	2	.301	3
262			min	-122.389	1	-407.115	2	-15.13	3	-.011	3	-.03	3	-.647	2
263		18	max	24.902	3	250.947	3	154.992	1	.028	2	.169	1	.148	3
264			min	-122.389	1	-576.043	2	-13.583	3	-.011	3	-.04	3	-.292	2
265		19	max	24.902	3	330.405	3	183.478	1	.028	2	.291	1	.185	2
266			min	-122.389	1	-744.972	2	-12.036	3	-.011	3	-.049	3	-.061	3
267	M2	1	max	2339.592	2	604.185	3	114.327	1	0	3	.134	3	8.733	1
268			min	-1745.182	3	-300.424	2	-117	3	-.002	2	-.181	1	-1.033	3
269		2	max	2337.035	2	604.185	3	114.327	1	0	3	.102	3	8.728	1
270			min	-1747.101	3	-300.424	2	-117	3	-.002	2	-.148	1	-1.202	3
271		3	max	2334.477	2	604.185	3	114.327	1	0	3	.069	3	8.723	1
272			min	-1749.019	3	-300.424	2	-117	3	-.002	2	-.116	1	-1.372	3
273		4	max	2331.92	2	604.185	3	114.327	1	0	3	.036	3	8.718	1
274			min	-1750.937	3	-300.424	2	-117	3	-.002	2	-.084	1	-1.542	3
275		5	max	2329.362	2	604.185	3	114.327	1	0	3	.003	3	8.712	1
276			min	-1752.855	3	-300.424	2	-117	3	-.002	2	-.052	1	-1.712	3
277		6	max	2326.805	2	604.185	3	114.327	1	0	3	0	10	8.707	1
278			min	-1754.773	3	-300.424	2	-117	3	-.002	2	-.03	3	-1.881	3
279		7	max	2324.248	2	604.185	3	114.327	1	0	3	.026	2	8.78	2
280			min	-1756.691	3	-300.424	2	-117	3	-.002	2	-.063	3	-2.051	3
281		8	max	2321.69	2	604.185	3	114.327	1	0	3	.058	2	8.864	2
282			min	-1758.609	3	-300.424	2	-117	3	-.002	2	-.096	3	-2.221	3
283		9	max	2029.919	1	2979.546	2	89.943	1	.002	2	.024	2	8.368	2
284			min	-1619.525	3	-764.817	3	-106.924	3	0	3	-.1	3	-2.148	3
285		10	max	2027.361	1	2979.546	2	89.943	1	.002	2	.048	2	7.532	2
286			min	-1621.443	3	-764.817	3	-106.924	3	0	3	-.13	3	-1.933	3
287		11	max	2024.804	1	2979.546	2	89.943	1	.002	2	.072	2	6.695	2
288			min	-1623.361	3	-764.817	3	-106.924	3	0	3	-.161	3	-1.718	3
289		12	max	2022.246	1	2979.546	2	89.943	1	.002	2	.096	2	5.858	2
290			min	-1625.279	3	-764.817	3	-106.924	3	0	3	-.191	3	-1.504	3
291		13	max	2019.689	1	2979.546	2	89.943	1	.002	2	.121	2	5.021	2
292			min	-1627.197	3	-764.817	3	-106.924	3	0	3	-.221	3	-1.289	3
293		14	max	2017.131	1	2979.546	2	89.943	1	.002	2	.145	2	4.184	2
294			min	-1629.115	3	-764.817	3	-106.924	3	0	3	-.251	3	-1.074	3
295		15	max	2014.574	1	2979.546	2	89.943	1	.002	2	.169	1	3.347	2
296			min	-1631.033	3	-764.817	3	-106.924	3	0	3	-.281	3	-.859	3
297		16	max	2012.016	1	2979.546	2	89.943	1	.002	2	.194	1	2.511	2
298			min	-1632.952	3	-764.817	3	-106.924	3	0	3	-.311	3	-.644	3
299		17	max	2009.459	1	2979.546	2	89.943	1	.002	2	.219	1	1.674	2
300			min	-1634.87	3	-764.817	3	-106.924	3	0	3	-.341	3	-.43	3
301		18	max	2006.901	1	2979.546	2	89.943	1	.002	2	.245	1	.837	2
302			min	-1636.788	3	-764.817	3	-106.924	3	0	3	-.371	3	-.215	3
303		19	max	2004.344	1	2979.546	2	89.943	1	.002	2	.27	1	0	1
304			min	-1638.706	3	-764.817	3	-106.924	3	0	3	-.401	3	0	1
305	M5	1	max	5592.814	2	2013.791	3	0	1	0	1	0	1	11.85	1
306			min	-4819.847	3	-2131.261	2	0	1	0	1	0	1	-.624	3
307		2	max	5590.257	2	2013.791	3	0	1	0	1	0	1	12.237	1
308			min	-4821.765	3	-2131.261	2	0	1	0	1	0	1	-1.19	3
309		3	max	5587.699	2	2013.791	3	0	1	0	1	0	1	12.624	1
310			min	-4823.683	3	-2131.261	2	0	1	0	1	0	1	-1.755	3
311		4	max	5585.142	2	2013.791	3	0	1	0	1	0	1	13.01	1
312			min	-4825.601	3	-2131.261	2	0	1	0	1	0	1	-2.321	3
313		5	max	5582.584	2	2013.791	3	0	1	0	1	0	1	13.397	1
314			min	-4827.52	3	-2131.261	2	0	1	0	1	0	1	-2.887	3
315		6	max	5580.027	2	2013.791	3	0	1	0	1	0	1	13.983	2
316			min	-4829.438	3	-2131.261	2	0	1	0	1	0	1	-3.452	3
317		7	max	5577.469	2	2013.791	3	0	1	0	1	0	1	14.581	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
318			min	-4831.356	3	-2131.261	2	0	1	0	1	0	1	-4.018	3
319		8	max	5574.912	2	2013.791	3	0	1	0	1	0	1	15.18	2
320			min	-4833.274	3	-2131.261	2	0	1	0	1	0	1	-4.583	3
321		9	max	4987.753	2	5158.646	2	0	1	0	1	0	1	14.489	2
322			min	-4445.103	3	-1605.305	3	0	1	0	1	0	1	-4.509	3
323		10	max	4985.196	2	5158.646	2	0	1	0	1	0	1	13.04	2
324			min	-4447.021	3	-1605.305	3	0	1	0	1	0	1	-4.058	3
325		11	max	4982.638	2	5158.646	2	0	1	0	1	0	1	11.591	2
326			min	-4448.939	3	-1605.305	3	0	1	0	1	0	1	-3.607	3
327		12	max	4980.081	2	5158.646	2	0	1	0	1	0	1	10.142	2
328			min	-4450.858	3	-1605.305	3	0	1	0	1	0	1	-3.156	3
329		13	max	4977.523	2	5158.646	2	0	1	0	1	0	1	8.693	2
330			min	-4452.776	3	-1605.305	3	0	1	0	1	0	1	-2.705	3
331		14	max	4974.966	2	5158.646	2	0	1	0	1	0	1	7.244	2
332			min	-4454.694	3	-1605.305	3	0	1	0	1	0	1	-2.254	3
333		15	max	4972.409	2	5158.646	2	0	1	0	1	0	1	5.795	2
334			min	-4456.612	3	-1605.305	3	0	1	0	1	0	1	-1.803	3
335		16	max	4969.851	2	5158.646	2	0	1	0	1	0	1	4.347	2
336			min	-4458.53	3	-1605.305	3	0	1	0	1	0	1	-1.353	3
337		17	max	4967.294	2	5158.646	2	0	1	0	1	0	1	2.898	2
338			min	-4460.448	3	-1605.305	3	0	1	0	1	0	1	-.902	3
339		18	max	4964.736	2	5158.646	2	0	1	0	1	0	1	1.449	2
340			min	-4462.366	3	-1605.305	3	0	1	0	1	0	1	-.451	3
341		19	max	4962.179	2	5158.646	2	0	1	0	1	0	1	0	1
342			min	-4464.284	3	-1605.305	3	0	1	0	1	0	1	0	1
343	M8	1	max	2339.592	2	604.185	3	117	3	.002	2	.181	1	8.733	1
344			min	-1745.182	3	-300.424	2	-114.327	1	0	3	-.134	3	-1.033	3
345		2	max	2337.035	2	604.185	3	117	3	.002	2	.148	1	8.728	1
346			min	-1747.101	3	-300.424	2	-114.327	1	0	3	-.102	3	-1.202	3
347		3	max	2334.477	2	604.185	3	117	3	.002	2	.116	1	8.723	1
348			min	-1749.019	3	-300.424	2	-114.327	1	0	3	-.069	3	-1.372	3
349		4	max	2331.92	2	604.185	3	117	3	.002	2	.084	1	8.718	1
350			min	-1750.937	3	-300.424	2	-114.327	1	0	3	-.036	3	-1.542	3
351		5	max	2329.362	2	604.185	3	117	3	.002	2	.052	1	8.712	1
352			min	-1752.855	3	-300.424	2	-114.327	1	0	3	-.003	3	-1.712	3
353		6	max	2326.805	2	604.185	3	117	3	.002	2	.03	3	8.707	1
354			min	-1754.773	3	-300.424	2	-114.327	1	0	3	0	10	-1.881	3
355		7	max	2324.248	2	604.185	3	117	3	.002	2	.063	3	8.78	2
356			min	-1756.691	3	-300.424	2	-114.327	1	0	3	-.026	2	-2.051	3
357		8	max	2321.69	2	604.185	3	117	3	.002	2	.096	3	8.864	2
358			min	-1758.609	3	-300.424	2	-114.327	1	0	3	-.058	2	-2.221	3
359		9	max	2029.919	1	2979.546	2	106.924	3	0	3	.1	3	8.368	2
360			min	-1619.525	3	-764.817	3	-89.943	1	-.002	2	-.024	2	-2.148	3
361		10	max	2027.361	1	2979.546	2	106.924	3	0	3	.13	3	7.532	2
362			min	-1621.443	3	-764.817	3	-89.943	1	-.002	2	-.048	2	-1.933	3
363		11	max	2024.804	1	2979.546	2	106.924	3	0	3	.161	3	6.695	2
364			min	-1623.361	3	-764.817	3	-89.943	1	-.002	2	-.072	2	-1.718	3
365		12	max	2022.246	1	2979.546	2	106.924	3	0	3	.191	3	5.858	2
366			min	-1625.279	3	-764.817	3	-89.943	1	-.002	2	-.096	2	-1.504	3
367		13	max	2019.689	1	2979.546	2	106.924	3	0	3	.221	3	5.021	2
368			min	-1627.197	3	-764.817	3	-89.943	1	-.002	2	-.121	2	-1.289	3
369		14	max	2017.131	1	2979.546	2	106.924	3	0	3	.251	3	4.184	2
370			min	-1629.115	3	-764.817	3	-89.943	1	-.002	2	-.145	2	-1.074	3
371		15	max	2014.574	1	2979.546	2	106.924	3	0	3	.281	3	3.347	2
372			min	-1631.033	3	-764.817	3	-89.943	1	-.002	2	-.169	1	-.859	3
373		16	max	2012.016	1	2979.546	2	106.924	3	0	3	.311	3	2.511	2
374			min	-1632.952	3	-764.817	3	-89.943	1	-.002	2	-.194	1	-.644	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
375		17	max	2009.459	1	2979.546	2	106.924	3	0	3	.341	3	1.674	2
376			min	-1634.87	3	-764.817	3	-89.943	1	-.002	2	-.219	1	-.43	3
377		18	max	2006.901	1	2979.546	2	106.924	3	0	3	.371	3	.837	2
378			min	-1636.788	3	-764.817	3	-89.943	1	-.002	2	-.245	1	-.215	3
379		19	max	2004.344	1	2979.546	2	106.924	3	0	3	.401	3	0	1
380			min	-1638.706	3	-764.817	3	-89.943	1	-.002	2	-.27	1	0	1
381	M3	1	max	3277.754	2	6.095	4	25.413	2	.026	3	.003	2	0	1
382			min	-1379.344	3	1.433	15	-10.765	3	-.06	2	-.001	3	0	1
383		2	max	3277.7	2	5.418	4	25.413	2	.026	3	.012	2	0	15
384			min	-1379.384	3	1.274	15	-10.765	3	-.06	2	-.005	3	-.002	4
385		3	max	3277.646	2	4.741	4	25.413	2	.026	3	.021	2	0	15
386			min	-1379.425	3	1.114	15	-10.765	3	-.06	2	-.009	3	-.004	4
387		4	max	3277.592	2	4.064	4	25.413	2	.026	3	.03	2	-.001	15
388			min	-1379.465	3	.955	15	-10.765	3	-.06	2	-.013	3	-.005	4
389		5	max	3277.538	2	3.386	4	25.413	2	.026	3	.039	2	-.002	15
390			min	-1379.505	3	.796	15	-10.765	3	-.06	2	-.017	3	-.007	4
391		6	max	3277.484	2	2.709	4	25.413	2	.026	3	.048	2	-.002	15
392			min	-1379.546	3	.637	15	-10.765	3	-.06	2	-.02	3	-.008	4
393		7	max	3277.43	2	2.032	4	25.413	2	.026	3	.057	2	-.002	15
394			min	-1379.586	3	.478	15	-10.765	3	-.06	2	-.024	3	-.009	4
395		8	max	3277.376	2	1.355	4	25.413	2	.026	3	.066	2	-.002	15
396			min	-1379.627	3	.318	15	-10.765	3	-.06	2	-.028	3	-.009	4
397		9	max	3277.322	2	.677	4	25.413	2	.026	3	.075	2	-.002	15
398			min	-1379.667	3	.159	15	-10.765	3	-.06	2	-.032	3	-.01	4
399		10	max	3277.268	2	0	1	25.413	2	.026	3	.085	2	-.002	15
400			min	-1379.708	3	0	1	-10.765	3	-.06	2	-.036	3	-.01	4
401		11	max	3277.214	2	-.159	15	25.413	2	.026	3	.094	2	-.002	15
402			min	-1379.748	3	-.677	4	-10.765	3	-.06	2	-.04	3	-.01	4
403		12	max	3277.16	2	-.318	15	25.413	2	.026	3	.103	2	-.002	15
404			min	-1379.789	3	-1.355	4	-10.765	3	-.06	2	-.043	3	-.009	4
405		13	max	3277.106	2	-.478	15	25.413	2	.026	3	.112	2	-.002	15
406			min	-1379.829	3	-2.032	4	-10.765	3	-.06	2	-.047	3	-.009	4
407		14	max	3277.052	2	-.637	15	25.413	2	.026	3	.121	2	-.002	15
408			min	-1379.87	3	-2.709	4	-10.765	3	-.06	2	-.051	3	-.008	4
409		15	max	3276.998	2	-.796	15	25.413	2	.026	3	.13	2	-.002	15
410			min	-1379.91	3	-3.386	4	-10.765	3	-.06	2	-.055	3	-.007	4
411		16	max	3276.944	2	-.955	15	25.413	2	.026	3	.139	2	-.001	15
412			min	-1379.951	3	-4.064	4	-10.765	3	-.06	2	-.059	3	-.005	4
413		17	max	3276.89	2	-1.114	15	25.413	2	.026	3	.148	2	0	15
414			min	-1379.991	3	-4.741	4	-10.765	3	-.06	2	-.063	3	-.004	4
415		18	max	3276.836	2	-1.274	15	25.413	2	.026	3	.157	2	0	15
416			min	-1380.032	3	-5.418	4	-10.765	3	-.06	2	-.067	3	-.002	4
417		19	max	3276.782	2	-1.433	15	25.413	2	.026	3	.166	2	0	1
418			min	-1380.072	3	-6.095	4	-10.765	3	-.06	2	-.07	3	0	1
419	M6	1	max	7246.822	2	6.095	4	0	1	0	1	0	1	0	1
420			min	-3657	3	1.433	15	0	1	0	1	0	1	0	1
421		2	max	7246.768	2	5.418	4	0	1	0	1	0	1	0	15
422			min	-3657.04	3	1.274	15	0	1	0	1	0	1	-.002	4
423		3	max	7246.714	2	4.741	4	0	1	0	1	0	1	0	15
424			min	-3657.081	3	1.114	15	0	1	0	1	0	1	-.004	4
425		4	max	7246.66	2	4.064	4	0	1	0	1	0	1	-.001	15
426			min	-3657.121	3	.955	15	0	1	0	1	0	1	-.005	4
427		5	max	7246.606	2	3.386	4	0	1	0	1	0	1	-.002	15
428			min	-3657.162	3	.796	15	0	1	0	1	0	1	-.007	4
429		6	max	7246.552	2	2.709	4	0	1	0	1	0	1	-.002	15
430			min	-3657.202	3	.637	15	0	1	0	1	0	1	-.008	4
431		7	max	7246.498	2	2.032	4	0	1	0	1	0	1	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
432			min	-3657.243	3	.478	15	0	1	0	1	0	1	-.009	4
433		8	max	7246.444	2	1.355	4	0	1	0	1	0	1	-.002	15
434			min	-3657.283	3	.318	15	0	1	0	1	0	1	-.009	4
435		9	max	7246.39	2	.677	4	0	1	0	1	0	1	-.002	15
436			min	-3657.324	3	.159	15	0	1	0	1	0	1	-.01	4
437		10	max	7246.336	2	0	1	0	1	0	1	0	1	-.002	15
438			min	-3657.364	3	0	1	0	1	0	1	0	1	-.01	4
439		11	max	7246.282	2	-.159	15	0	1	0	1	0	1	-.002	15
440			min	-3657.405	3	-.677	4	0	1	0	1	0	1	-.01	4
441		12	max	7246.228	2	-.318	15	0	1	0	1	0	1	-.002	15
442			min	-3657.445	3	-1.355	4	0	1	0	1	0	1	-.009	4
443		13	max	7246.174	2	-.478	15	0	1	0	1	0	1	-.002	15
444			min	-3657.486	3	-2.032	4	0	1	0	1	0	1	-.009	4
445		14	max	7246.12	2	-.637	15	0	1	0	1	0	1	-.002	15
446			min	-3657.526	3	-2.709	4	0	1	0	1	0	1	-.008	4
447		15	max	7246.066	2	-.796	15	0	1	0	1	0	1	-.002	15
448			min	-3657.567	3	-3.386	4	0	1	0	1	0	1	-.007	4
449		16	max	7246.012	2	-.955	15	0	1	0	1	0	1	-.001	15
450			min	-3657.607	3	-4.064	4	0	1	0	1	0	1	-.005	4
451		17	max	7245.958	2	-1.114	15	0	1	0	1	0	1	0	15
452			min	-3657.647	3	-4.741	4	0	1	0	1	0	1	-.004	4
453		18	max	7245.904	2	-1.274	15	0	1	0	1	0	1	0	15
454			min	-3657.688	3	-5.418	4	0	1	0	1	0	1	-.002	4
455		19	max	7245.85	2	-1.433	15	0	1	0	1	0	1	0	1
456			min	-3657.728	3	-6.095	4	0	1	0	1	0	1	0	1
457	M9	1	max	3277.754	2	6.095	4	10.765	3	.06	2	.001	3	0	1
458			min	-1379.344	3	1.433	15	-25.413	2	-.026	3	-.003	2	0	1
459		2	max	3277.7	2	5.418	4	10.765	3	.06	2	.005	3	0	15
460			min	-1379.384	3	1.274	15	-25.413	2	-.026	3	-.012	2	-.002	4
461		3	max	3277.646	2	4.741	4	10.765	3	.06	2	.009	3	0	15
462			min	-1379.425	3	1.114	15	-25.413	2	-.026	3	-.021	2	-.004	4
463		4	max	3277.592	2	4.064	4	10.765	3	.06	2	.013	3	-.001	15
464			min	-1379.465	3	.955	15	-25.413	2	-.026	3	-.03	2	-.005	4
465		5	max	3277.538	2	3.386	4	10.765	3	.06	2	.017	3	-.002	15
466			min	-1379.505	3	.796	15	-25.413	2	-.026	3	-.039	2	-.007	4
467		6	max	3277.484	2	2.709	4	10.765	3	.06	2	.02	3	-.002	15
468			min	-1379.546	3	.637	15	-25.413	2	-.026	3	-.048	2	-.008	4
469		7	max	3277.43	2	2.032	4	10.765	3	.06	2	.024	3	-.002	15
470			min	-1379.586	3	.478	15	-25.413	2	-.026	3	-.057	2	-.009	4
471		8	max	3277.376	2	1.355	4	10.765	3	.06	2	.028	3	-.002	15
472			min	-1379.627	3	.318	15	-25.413	2	-.026	3	-.066	2	-.009	4
473		9	max	3277.322	2	.677	4	10.765	3	.06	2	.032	3	-.002	15
474			min	-1379.667	3	.159	15	-25.413	2	-.026	3	-.075	2	-.01	4
475		10	max	3277.268	2	0	1	10.765	3	.06	2	.036	3	-.002	15
476			min	-1379.708	3	0	1	-25.413	2	-.026	3	-.085	2	-.01	4
477		11	max	3277.214	2	-.159	15	10.765	3	.06	2	.04	3	-.002	15
478			min	-1379.748	3	-.677	4	-25.413	2	-.026	3	-.094	2	-.01	4
479		12	max	3277.16	2	-.318	15	10.765	3	.06	2	.043	3	-.002	15
480			min	-1379.789	3	-1.355	4	-25.413	2	-.026	3	-.103	2	-.009	4
481		13	max	3277.106	2	-.478	15	10.765	3	.06	2	.047	3	-.002	15
482			min	-1379.829	3	-2.032	4	-25.413	2	-.026	3	-.112	2	-.009	4
483		14	max	3277.052	2	-.637	15	10.765	3	.06	2	.051	3	-.002	15
484			min	-1379.87	3	-2.709	4	-25.413	2	-.026	3	-.121	2	-.008	4
485		15	max	3276.998	2	-.796	15	10.765	3	.06	2	.055	3	-.002	15
486			min	-1379.91	3	-3.386	4	-25.413	2	-.026	3	-.13	2	-.007	4
487		16	max	3276.944	2	-.955	15	10.765	3	.06	2	.059	3	-.001	15
488			min	-1379.951	3	-4.064	4	-25.413	2	-.026	3	-.139	2	-.005	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
489		17	max	3276.89	2	-1.114	15	10.765	3	.06	2	.063	3	0	15
490			min	-1379.991	3	-4.741	4	-25.413	2	-.026	3	-.148	2	-.004	4
491		18	max	3276.836	2	-1.274	15	10.765	3	.06	2	.067	3	0	15
492			min	-1380.032	3	-5.418	4	-25.413	2	-.026	3	-.157	2	-.002	4
493		19	max	3276.782	2	-1.433	15	10.765	3	.06	2	.07	3	0	1
494			min	-1380.072	3	-6.095	4	-25.413	2	-.026	3	-.166	2	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	.109	3	.437	3	.01	1	1.021e-2	3	2866.78	15	NC	1
2			min	-.521	1	-1.551	2	-.002	3	-2.533e-2	2	71.805	2	NC	1
3		2	max	.109	3	.371	3	.001	3	9.815e-3	3	3128.903	15	NC	2
4			min	-.521	1	-1.364	2	-.007	1	-2.413e-2	2	79.299	2	8799.465	1
5		3	max	.109	3	.308	3	.003	3	9.032e-3	3	3437.919	15	NC	3
6			min	-.521	1	-1.182	2	-.016	1	-2.178e-2	2	88.319	2	6010.754	1
7		4	max	.109	3	.249	3	.004	3	8.25e-3	3	3793.032	15	NC	3
8			min	-.521	1	-1.011	2	-.017	1	-1.942e-2	2	98.83	2	5846.964	1
9		5	max	.109	3	.199	3	.004	3	7.661e-3	3	4184.962	15	NC	3
10			min	-.52	1	-.86	2	-.015	1	-1.752e-2	2	110.446	2	6707.611	1
11		6	max	.109	3	.16	3	.003	3	7.57e-3	3	NC	12	NC	2
12			min	-.519	1	-.733	2	-.01	1	-1.679e-2	2	122.645	2	9798.845	1
13		7	max	.108	3	.128	3	.002	3	7.48e-3	3	NC	3	NC	1
14			min	-.518	1	-.621	2	-.003	2	-1.605e-2	2	135.74	2	NC	1
15		8	max	.108	3	.1	3	0	1	7.389e-3	3	5792.628	12	NC	1
16			min	-.517	1	-.519	2	0	15	-1.531e-2	2	150.463	2	NC	1
17		9	max	.107	3	.074	3	0	15	7.511e-3	3	6236.257	15	NC	1
18			min	-.516	1	-.419	2	0	3	-1.393e-2	2	168.306	2	NC	1
19		10	max	.107	3	.047	3	.001	1	7.834e-3	3	7064.088	15	NC	1
20			min	-.515	1	-.318	2	-.001	3	-1.194e-2	2	191.199	2	NC	1
21		11	max	.106	3	.021	3	.001	1	8.156e-3	3	8165.402	15	NC	1
22			min	-.513	1	-.217	2	0	3	-9.956e-3	2	221.628	2	NC	1
23		12	max	.106	3	-.003	12	.003	3	7.335e-3	3	9705.385	15	NC	1
24			min	-.512	1	-.114	2	-.004	1	-7.816e-3	2	264.191	2	NC	1
25		13	max	.105	3	0	15	.007	3	5.3e-3	3	NC	15	NC	1
26			min	-.511	1	-.027	3	-.005	1	-5.51e-3	2	326.321	2	NC	1
27		14	max	.105	3	.088	1	.01	3	3.265e-3	3	NC	15	NC	1
28			min	-.51	1	-.041	3	-.004	2	-3.205e-3	2	420.023	2	NC	1
29		15	max	.104	3	.174	1	.009	3	1.23e-3	3	NC	5	NC	1
30			min	-.508	1	-.038	3	0	10	-9.001e-4	2	566.951	2	NC	1
31		16	max	.104	3	.247	2	.008	1	3.488e-3	3	NC	5	NC	1
32			min	-.508	1	-.013	3	0	15	-1.567e-3	1	805.344	2	NC	1
33		17	max	.104	3	.31	2	.011	1	6.25e-3	3	NC	5	NC	2
34			min	-.508	1	.008	15	0	15	-2.577e-3	1	1260.115	2	8343.427	1
35		18	max	.104	3	.368	2	.006	1	9.012e-3	3	NC	4	NC	1
36			min	-.508	1	.01	15	0	15	-3.586e-3	1	2532.96	3	NC	1
37		19	max	.104	3	.423	2	0	3	1.042e-2	3	NC	1	NC	1
38			min	-.508	1	.011	15	-.008	1	-4.102e-3	1	NC	1	NC	1
39	M4	1	max	.196	3	.81	3	0	1	0	1	2047.468	15	NC	1
40			min	-.822	2	-2.572	2	0	1	0	1	45.958	2	NC	1
41		2	max	.196	3	.694	3	0	1	0	1	2251.47	15	NC	1
42			min	-.822	2	-2.261	2	0	1	0	1	51.118	2	NC	1
43		3	max	.196	3	.581	3	0	1	0	1	2495.758	15	NC	1
44			min	-.822	2	-1.956	2	0	1	0	1	57.424	2	NC	1
45		4	max	.196	3	.479	3	0	1	0	1	2778.756	15	NC	1
46			min	-.822	2	-1.674	2	0	1	0	1	64.819	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
47		5	max	.195	3	.398	3	0	1	0	1	9246.805	12	NC	1
48			min	-.821	2	-1.432	2	0	1	0	1	72.886	2	NC	1
49		6	max	.194	3	.338	3	0	1	0	1	7137.526	12	NC	1
50			min	-.819	2	-1.236	2	0	1	0	1	81.061	2	NC	1
51		7	max	.193	3	.293	3	0	1	0	1	3766.808	15	NC	1
52			min	-.816	2	-1.07	2	0	1	0	1	89.612	2	NC	1
53		8	max	.191	3	.253	3	0	1	0	1	4178.181	15	NC	1
54			min	-.813	2	-.916	2	0	1	0	1	99.266	2	NC	1
55		9	max	.19	3	.21	3	0	1	0	1	4706.151	15	NC	1
56			min	-.811	2	-.758	2	0	1	0	1	111.582	2	NC	1
57		10	max	.189	3	.159	3	0	1	0	1	5434.041	15	NC	1
58			min	-.808	2	-.589	2	0	1	0	1	128.675	2	NC	1
59		11	max	.188	3	.102	3	0	1	0	1	6485.169	15	NC	1
60			min	-.806	2	-.412	2	0	1	0	1	153.427	2	NC	1
61		12	max	.186	3	.038	3	0	1	0	1	8120.764	15	NC	1
62			min	-.803	2	-.226	2	0	1	0	1	191.977	2	NC	1
63		13	max	.185	3	0	15	0	1	0	1	NC	15	NC	1
64			min	-.8	2	-.04	2	0	1	0	1	256.499	2	NC	1
65		14	max	.184	3	.135	1	0	1	0	1	NC	5	NC	1
66			min	-.798	2	-.065	3	0	1	0	1	327.744	3	NC	1
67		15	max	.183	3	.272	2	0	1	0	1	NC	5	NC	1
68			min	-.795	2	-.065	3	0	1	0	1	327.694	3	NC	1
69		16	max	.182	3	.369	2	0	1	0	1	NC	5	NC	1
70			min	-.795	2	-.006	3	0	1	0	1	378.896	3	NC	1
71		17	max	.182	3	.432	2	0	1	0	1	NC	4	NC	1
72			min	-.795	2	.01	15	0	1	0	1	524.788	3	NC	1
73		18	max	.182	3	.475	2	0	1	0	1	NC	4	NC	1
74			min	-.795	2	.011	15	0	1	0	1	1018.637	3	NC	1
75		19	max	.182	3	.512	2	0	1	0	1	NC	1	NC	1
76			min	-.795	2	.012	15	0	1	0	1	NC	1	NC	1
77	M7	1	max	.109	3	.437	3	.002	3	2.533e-2	2	2866.78	15	NC	1
78			min	-.521	1	-1.551	2	-.01	1	-1.021e-2	3	71.805	2	NC	1
79		2	max	.109	3	.371	3	.007	1	2.413e-2	2	3128.903	15	NC	2
80			min	-.521	1	-1.364	2	-.001	3	-9.815e-3	3	79.299	2	8799.465	1
81		3	max	.109	3	.308	3	.016	1	2.178e-2	2	3437.919	15	NC	3
82			min	-.521	1	-1.182	2	-.003	3	-9.032e-3	3	88.319	2	6010.754	1
83		4	max	.109	3	.249	3	.017	1	1.942e-2	2	3793.032	15	NC	3
84			min	-.521	1	-1.011	2	-.004	3	-8.25e-3	3	98.83	2	5846.964	1
85		5	max	.109	3	.199	3	.015	1	1.752e-2	2	4184.962	15	NC	3
86			min	-.52	1	-.86	2	-.004	3	-7.661e-3	3	110.446	2	6707.611	1
87		6	max	.109	3	.16	3	.01	1	1.679e-2	2	NC	12	NC	2
88			min	-.519	1	-.733	2	-.003	3	-7.57e-3	3	122.645	2	9798.845	1
89		7	max	.108	3	.128	3	.003	2	1.605e-2	2	NC	3	NC	1
90			min	-.518	1	-.621	2	-.002	3	-7.48e-3	3	135.74	2	NC	1
91		8	max	.108	3	.1	3	0	15	1.531e-2	2	5792.628	12	NC	1
92			min	-.517	1	-.519	2	0	1	-7.389e-3	3	150.463	2	NC	1
93		9	max	.107	3	.074	3	0	3	1.393e-2	2	6236.257	15	NC	1
94			min	-.516	1	-.419	2	0	15	-7.511e-3	3	168.306	2	NC	1
95		10	max	.107	3	.047	3	.001	3	1.194e-2	2	7064.088	15	NC	1
96			min	-.515	1	-.318	2	-.001	1	-7.834e-3	3	191.199	2	NC	1
97		11	max	.106	3	.021	3	0	3	9.956e-3	2	8165.402	15	NC	1
98			min	-.513	1	-.217	2	-.001	1	-8.156e-3	3	221.628	2	NC	1
99		12	max	.106	3	-.003	12	.004	1	7.816e-3	2	9705.385	15	NC	1
100			min	-.512	1	-.114	2	-.003	3	-7.335e-3	3	264.191	2	NC	1
101		13	max	.105	3	0	15	.005	1	5.51e-3	2	NC	15	NC	1
102			min	-.511	1	-.027	3	-.007	3	-5.3e-3	3	326.321	2	NC	1
103		14	max	.105	3	.088	1	.004	2	3.205e-3	2	NC	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
104			min	-.51	1	-.041	3	-.01	3	-3.265e-3	3	420.023	2	NC	1
105		15	max	.104	3	.174	1	0	10	9.001e-4	2	NC	5	NC	1
106			min	-.508	1	-.038	3	-.009	3	-1.23e-3	3	566.951	2	NC	1
107		16	max	.104	3	.247	2	0	15	1.567e-3	1	NC	5	NC	1
108			min	-.508	1	-.013	3	-.008	1	-3.488e-3	3	805.344	2	NC	1
109		17	max	.104	3	.31	2	0	15	2.577e-3	1	NC	5	NC	2
110			min	-.508	1	.008	15	-.011	1	-6.25e-3	3	1260.115	2	8343.427	1
111		18	max	.104	3	.368	2	0	15	3.586e-3	1	NC	4	NC	1
112			min	-.508	1	.01	15	-.006	1	-9.012e-3	3	2532.96	3	NC	1
113		19	max	.104	3	.423	2	.008	1	4.102e-3	1	NC	1	NC	1
114			min	-.508	1	.011	15	0	3	-1.042e-2	3	NC	1	NC	1
115	M10	1	max	0	1	.396	2	.508	1	7.084e-3	3	NC	1	NC	1
116			min	0	3	.011	15	-.104	3	1.944e-4	15	NC	1	NC	1
117		2	max	0	1	.365	2	.536	1	8.251e-3	3	NC	4	NC	3
118			min	0	3	.01	15	-.107	3	1.852e-4	15	1704.855	3	5605.404	1
119		3	max	0	1	.341	2	.579	1	9.418e-3	3	NC	4	NC	3
120			min	0	3	.009	15	-.114	3	1.759e-4	15	890.164	3	2215.588	1
121		4	max	0	1	.35	3	.628	1	1.059e-2	3	NC	4	NC	5
122			min	0	3	.009	15	-.123	3	1.667e-4	15	652.056	3	1308.34	1
123		5	max	0	1	.387	3	.676	1	1.175e-2	3	NC	4	NC	5
124			min	0	3	.009	15	-.135	3	1.574e-4	15	563.842	3	931.282	1
125		6	max	0	1	.396	3	.719	1	1.292e-2	3	NC	4	NC	5
126			min	0	3	.009	15	-.148	3	1.482e-4	15	545.643	3	742.307	1
127		7	max	0	1	.399	2	.752	1	1.409e-2	3	NC	2	NC	5
128			min	0	3	.01	15	-.161	3	1.389e-4	15	576.776	3	639.877	1
129		8	max	0	1	.441	2	.775	1	1.525e-2	3	NC	4	NC	5
130			min	0	3	.011	15	-.172	3	1.297e-4	15	652.459	3	584.763	1
131		9	max	0	1	.478	2	.788	2	1.642e-2	3	NC	4	NC	5
132			min	0	3	.012	15	-.179	3	1.204e-4	15	758.465	3	550.238	2
133		10	max	0	1	.494	2	.795	2	1.759e-2	3	NC	4	NC	5
134			min	0	1	.012	15	-.182	3	1.112e-4	15	824.117	3	537.108	2
135		11	max	0	3	.478	2	.788	2	1.642e-2	3	NC	4	NC	5
136			min	0	1	.012	15	-.179	3	1.204e-4	15	758.465	3	550.238	2
137		12	max	0	3	.441	2	.775	1	1.525e-2	3	NC	4	NC	5
138			min	0	1	.011	15	-.172	3	1.297e-4	15	652.459	3	584.763	1
139		13	max	0	3	.399	2	.752	1	1.409e-2	3	NC	2	NC	5
140			min	0	1	.01	15	-.161	3	1.389e-4	15	576.776	3	639.877	1
141		14	max	0	3	.396	3	.719	1	1.292e-2	3	NC	4	NC	5
142			min	0	1	.009	15	-.148	3	1.482e-4	15	545.643	3	742.307	1
143		15	max	0	3	.387	3	.676	1	1.175e-2	3	NC	4	NC	5
144			min	0	1	.009	15	-.135	3	1.574e-4	15	563.842	3	931.282	1
145		16	max	0	3	.35	3	.628	1	1.059e-2	3	NC	4	NC	5
146			min	0	1	.009	15	-.123	3	1.667e-4	15	652.056	3	1308.34	1
147		17	max	0	3	.341	2	.579	1	9.418e-3	3	NC	4	NC	3
148			min	0	1	.009	15	-.114	3	1.759e-4	15	890.164	3	2215.588	1
149		18	max	0	3	.365	2	.536	1	8.251e-3	3	NC	4	NC	3
150			min	0	1	.01	15	-.107	3	1.852e-4	15	1704.855	3	5605.404	1
151		19	max	0	3	.396	2	.508	1	7.084e-3	3	NC	1	NC	1
152			min	0	1	.011	15	-.104	3	1.944e-4	15	NC	1	NC	1
153	M11	1	max	.001	1	.008	3	.513	1	1.307e-2	2	NC	1	NC	1
154			min	0	3	-.164	2	-.106	3	-3.275e-3	3	NC	1	NC	1
155		2	max	0	1	.081	3	.533	1	1.423e-2	2	NC	4	NC	3
156			min	0	3	-.24	2	-.111	3	-3.81e-3	3	2058.987	2	7751.038	1
157		3	max	0	1	.145	3	.572	1	1.539e-2	2	NC	5	NC	3
158			min	0	3	-.306	2	-.12	3	-4.346e-3	3	1099.746	2	2647.78	1
159		4	max	0	1	.19	3	.62	1	1.655e-2	2	NC	5	NC	5
160			min	0	3	-.355	2	-.131	3	-4.881e-3	3	817.648	2	1457.052	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
161		5	max	0	1	.209	3	.67	1	1.771e-2	2	NC	5	NC	5
162			min	0	3	-.382	2	-.143	3	-5.416e-3	3	713.405	2	993.791	1
163		6	max	0	1	.202	3	.716	1	1.886e-2	2	NC	5	NC	5
164			min	0	3	-.389	2	-.155	3	-5.952e-3	3	692.969	2	769.384	1
165		7	max	0	1	.172	3	.753	1	2.002e-2	2	NC	5	NC	5
166			min	0	3	-.377	2	-.167	3	-6.487e-3	3	731.305	2	649.334	1
167		8	max	0	1	.13	3	.78	1	2.118e-2	2	NC	5	NC	5
168			min	0	3	-.354	2	-.177	3	-7.022e-3	3	821.072	2	584.332	1
169		9	max	0	1	.089	3	.796	2	2.234e-2	2	NC	5	NC	5
170			min	0	3	-.329	2	-.184	3	-7.557e-3	3	942.993	2	542.887	2
171		10	max	0	1	.07	3	.804	2	2.35e-2	2	NC	5	NC	5
172			min	0	1	-.317	2	-.187	3	-8.093e-3	3	1016.624	2	528.523	2
173		11	max	0	3	.089	3	.796	2	2.234e-2	2	NC	5	NC	5
174			min	0	1	-.329	2	-.184	3	-7.557e-3	3	942.993	2	542.887	2
175		12	max	0	3	.13	3	.78	1	2.118e-2	2	NC	5	NC	5
176			min	0	1	-.354	2	-.177	3	-7.022e-3	3	821.072	2	584.332	1
177		13	max	0	3	.172	3	.753	1	2.002e-2	2	NC	5	NC	5
178			min	0	1	-.377	2	-.167	3	-6.487e-3	3	731.305	2	649.334	1
179		14	max	0	3	.202	3	.716	1	1.886e-2	2	NC	5	NC	5
180			min	0	1	-.389	2	-.155	3	-5.952e-3	3	692.969	2	769.384	1
181		15	max	0	3	.209	3	.67	1	1.771e-2	2	NC	5	NC	5
182			min	0	1	-.382	2	-.143	3	-5.416e-3	3	713.405	2	993.791	1
183		16	max	0	3	.19	3	.62	1	1.655e-2	2	NC	5	NC	5
184			min	0	1	-.355	2	-.131	3	-4.881e-3	3	817.648	2	1457.052	1
185		17	max	0	3	.145	3	.572	1	1.539e-2	2	NC	5	NC	3
186			min	0	1	-.306	2	-.12	3	-4.346e-3	3	1099.746	2	2647.78	1
187		18	max	0	3	.081	3	.533	1	1.423e-2	2	NC	4	NC	3
188			min	0	1	-.24	2	-.111	3	-3.81e-3	3	2058.987	2	7751.038	1
189		19	max	0	3	.008	3	.513	1	1.307e-2	2	NC	1	NC	1
190			min	-.001	1	-.164	2	-.106	3	-3.275e-3	3	NC	1	NC	1
191	M12	1	max	0	3	.087	3	.516	1	1.276e-2	1	NC	1	NC	1
192			min	0	1	-.471	2	-.107	3	-3.353e-3	3	NC	1	NC	1
193		2	max	0	3	.149	3	.534	1	1.355e-2	1	NC	5	NC	2
194			min	0	1	-.599	2	-.11	3	-3.591e-3	3	1215.026	2	9135.459	1
195		3	max	0	3	.202	3	.571	1	1.434e-2	2	NC	5	NC	3
196			min	0	1	-.715	2	-.117	3	-3.83e-3	3	637.94	2	2861.915	1
197		4	max	0	3	.242	3	.619	1	1.516e-2	2	NC	5	NC	5
198			min	0	1	-.808	2	-.127	3	-4.068e-3	3	463.241	2	1519.949	1
199		5	max	0	3	.266	3	.67	1	1.597e-2	2	NC	5	NC	5
200			min	0	1	-.869	2	-.14	3	-4.306e-3	3	391.538	2	1016.269	1
201		6	max	0	3	.275	3	.717	1	1.679e-2	2	NC	5	NC	5
202			min	0	1	-.899	2	-.154	3	-4.544e-3	3	364.507	2	776.618	1
203		7	max	0	3	.27	3	.757	1	1.76e-2	2	NC	5	NC	5
204			min	0	1	-.9	2	-.168	3	-4.783e-3	3	363.748	2	649.43	1
205		8	max	0	3	.256	3	.785	1	1.842e-2	2	NC	5	NC	5
206			min	0	1	-.88	2	-.179	3	-5.021e-3	3	380.827	2	580.568	1
207		9	max	0	3	.241	3	.804	2	1.923e-2	2	NC	5	NC	5
208			min	0	1	-.855	2	-.188	3	-5.259e-3	3	406.412	2	536.385	2
209		10	max	0	1	.233	3	.812	2	2.005e-2	2	NC	5	NC	5
210			min	0	1	-.841	2	-.191	3	-5.497e-3	3	421.475	2	521.409	2
211		11	max	0	1	.241	3	.804	2	1.923e-2	2	NC	5	NC	5
212			min	0	3	-.855	2	-.188	3	-5.259e-3	3	406.412	2	536.385	2
213		12	max	0	1	.256	3	.785	1	1.842e-2	2	NC	5	NC	5
214			min	0	3	-.88	2	-.179	3	-5.021e-3	3	380.827	2	580.568	1
215		13	max	0	1	.27	3	.757	1	1.76e-2	2	NC	5	NC	5
216			min	0	3	-.9	2	-.168	3	-4.783e-3	3	363.748	2	649.43	1
217		14	max	0	1	.275	3	.717	1	1.679e-2	2	NC	5	NC	5

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
218			min	0	3	-.899	2	-.154	3	-4.544e-3	3	364.507	2	776.618	1
219		15	max	0	1	.266	3	.67	1	1.597e-2	2	NC	5	NC	5
220			min	0	3	-.869	2	-.14	3	-4.306e-3	3	391.538	2	1016.269	1
221		16	max	0	1	.242	3	.619	1	1.516e-2	2	NC	5	NC	5
222			min	0	3	-.808	2	-.127	3	-4.068e-3	3	463.241	2	1519.949	1
223		17	max	0	1	.202	3	.571	1	1.434e-2	2	NC	5	NC	3
224			min	0	3	-.715	2	-.117	3	-3.83e-3	3	637.94	2	2861.915	1
225		18	max	0	1	.149	3	.534	1	1.355e-2	1	NC	5	NC	2
226			min	0	3	-.599	2	-.11	3	-3.591e-3	3	1215.026	2	9135.459	1
227		19	max	0	1	.087	3	.516	1	1.276e-2	1	NC	1	NC	1
228			min	0	3	-.471	2	-.107	3	-3.353e-3	3	NC	1	NC	1
229	M13	1	max	0	3	.405	3	.521	1	2.367e-2	2	NC	1	NC	1
230			min	0	1	-1.46	2	-.109	3	-8.299e-3	3	NC	1	NC	1
231		2	max	0	3	.493	3	.552	1	2.542e-2	2	NC	5	NC	3
232			min	0	1	-1.679	2	-.115	3	-9.014e-3	3	709.685	2	5039.496	1
233		3	max	0	3	.575	3	.597	1	2.717e-2	2	NC	5	NC	3
234			min	0	1	-1.888	2	-.124	3	-9.73e-3	3	364.522	2	2049.826	1
235		4	max	0	3	.645	3	.648	1	2.893e-2	2	NC	15	NC	5
236			min	0	1	-2.069	2	-.135	3	-1.045e-2	3	255.851	2	1228.431	1
237		5	max	0	3	.699	3	.698	1	3.068e-2	2	NC	15	NC	5
238			min	0	1	-2.215	2	-.148	3	-1.116e-2	3	206.489	2	881.984	1
239		6	max	0	3	.735	3	.742	1	3.244e-2	2	9930.124	15	NC	5
240			min	0	1	-2.32	2	-.162	3	-1.188e-2	3	181.261	2	706.779	1
241		7	max	0	3	.754	3	.776	1	3.419e-2	2	9174.56	15	NC	5
242			min	0	1	-2.385	2	-.174	3	-1.259e-2	3	168.534	2	611.267	1
243		8	max	0	3	.759	3	.8	1	3.594e-2	2	8826.008	15	NC	5
244			min	0	1	-2.416	2	-.185	3	-1.331e-2	3	163.185	2	559.687	1
245		9	max	0	3	.757	3	.815	2	3.77e-2	2	8720.797	15	NC	5
246			min	0	1	-2.422	2	-.193	3	-1.402e-2	3	162.126	2	524.859	2
247		10	max	0	1	.753	3	.822	2	3.945e-2	2	8719.661	15	NC	5
248			min	0	1	-2.42	2	-.196	3	-1.474e-2	3	162.505	2	512.658	2
249		11	max	0	1	.757	3	.815	2	3.77e-2	2	8720.797	15	NC	5
250			min	0	3	-2.422	2	-.193	3	-1.402e-2	3	162.126	2	524.859	2
251		12	max	0	1	.759	3	.8	1	3.594e-2	2	8826.008	15	NC	5
252			min	0	3	-2.416	2	-.185	3	-1.331e-2	3	163.185	2	559.687	1
253		13	max	0	1	.754	3	.776	1	3.419e-2	2	9174.56	15	NC	5
254			min	0	3	-2.385	2	-.174	3	-1.259e-2	3	168.534	2	611.267	1
255		14	max	0	1	.735	3	.742	1	3.244e-2	2	9930.124	15	NC	5
256			min	0	3	-2.32	2	-.162	3	-1.188e-2	3	181.261	2	706.779	1
257		15	max	0	1	.699	3	.698	1	3.068e-2	2	NC	15	NC	5
258			min	0	3	-2.215	2	-.148	3	-1.116e-2	3	206.489	2	881.984	1
259		16	max	0	1	.645	3	.648	1	2.893e-2	2	NC	15	NC	5
260			min	0	3	-2.069	2	-.135	3	-1.045e-2	3	255.851	2	1228.431	1
261		17	max	0	1	.575	3	.597	1	2.717e-2	2	NC	5	NC	3
262			min	0	3	-1.888	2	-.124	3	-9.73e-3	3	364.522	2	2049.826	1
263		18	max	0	1	.493	3	.552	1	2.542e-2	2	NC	5	NC	3
264			min	0	3	-1.679	2	-.115	3	-9.014e-3	3	709.685	2	5039.496	1
265		19	max	0	1	.405	3	.521	1	2.367e-2	2	NC	1	NC	1
266			min	0	3	-1.46	2	-.109	3	-8.299e-3	3	NC	1	NC	1
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	3	0	3	5.021e-4	2	NC	1	NC	1
270			min	0	2	-.002	1	0	1	-2.147e-4	3	NC	1	NC	1
271		3	max	0	3	0	3	0	3	1.004e-3	2	NC	3	NC	1
272			min	0	2	-.008	1	0	1	-4.294e-4	3	8078.732	1	NC	1
273		4	max	0	3	.002	3	0	3	1.506e-3	2	NC	3	NC	1
274			min	0	2	-.017	1	0	1	-6.44e-4	3	3592.902	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
275		5	max	0	3	.004	3	0	3	2.009e-3	2	NC	3	NC	1
276			min	0	2	-.03	1	-.001	1	-8.587e-4	3	2021.869	1	NC	1
277		6	max	0	3	.007	3	.001	3	2.511e-3	2	NC	5	NC	1
278			min	0	2	-.047	1	-.002	1	-1.073e-3	3	1294.39	1	NC	1
279		7	max	0	3	.01	3	.001	3	3.013e-3	2	NC	5	NC	1
280			min	0	2	-.067	1	-.002	1	-1.288e-3	3	899.08	1	NC	1
281		8	max	0	3	.014	3	.002	3	3.515e-3	2	NC	5	NC	1
282			min	0	2	-.092	1	-.003	1	-1.503e-3	3	660.701	1	NC	1
283		9	max	0	3	.02	3	.002	3	3.426e-3	2	NC	5	NC	1
284			min	0	2	-.12	1	-.003	1	-1.442e-3	3	504.977	1	NC	1
285		10	max	0	3	.026	3	.002	3	2.99e-3	2	NC	15	NC	1
286			min	-.001	2	-.152	1	-.004	1	-1.22e-3	3	398.845	1	NC	1
287		11	max	0	3	.034	3	.002	3	2.553e-3	2	NC	15	NC	1
288			min	-.001	2	-.187	1	-.004	1	-9.975e-4	3	324.006	1	NC	1
289		12	max	0	3	.041	3	.001	3	2.117e-3	2	NC	15	NC	1
290			min	-.001	2	-.225	1	-.005	1	-7.752e-4	3	269.41	1	NC	1
291		13	max	.001	3	.05	3	0	3	1.681e-3	2	8576.748	15	NC	1
292			min	-.001	2	-.266	1	-.005	1	-5.529e-4	3	228.425	1	NC	1
293		14	max	.001	3	.059	3	0	3	1.245e-3	2	7404.757	15	NC	1
294			min	-.001	2	-.308	1	-.005	1	-3.306e-4	3	196.905	1	NC	1
295		15	max	.001	3	.069	3	0	15	8.083e-4	2	6483.016	15	NC	1
296			min	-.002	2	-.352	1	-.005	1	-1.083e-4	3	172.168	1	NC	1
297		16	max	.001	3	.079	3	0	15	3.721e-4	2	5745.502	15	NC	1
298			min	-.002	2	-.398	1	-.005	1	-6.202e-6	9	152.411	1	NC	1
299		17	max	.001	3	.089	3	0	15	3.363e-4	3	5146.761	15	NC	1
300			min	-.002	2	-.445	1	-.005	1	-2.355e-4	1	136.398	1	NC	1
301		18	max	.001	3	.1	3	0	15	5.586e-4	3	4654.529	15	NC	1
302			min	-.002	2	-.492	1	-.006	3	-6.495e-4	1	123.254	1	9909.307	3
303		19	max	.002	3	.11	3	0	15	7.809e-4	3	4245.541	15	NC	1
304			min	-.002	2	-.54	1	-.009	3	-1.063e-3	1	112.347	1	7069.034	3
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	12	0	1	0	1	NC	1	NC	1
308			min	0	2	-.002	1	0	1	0	1	NC	1	NC	1
309		3	max	0	3	0	3	0	1	0	1	NC	3	NC	1
310			min	0	2	-.01	1	0	1	0	1	6045.097	1	NC	1
311		4	max	0	3	.001	3	0	1	0	1	NC	3	NC	1
312			min	0	2	-.023	1	0	1	0	1	2625.839	1	NC	1
313		5	max	.001	3	.004	3	0	1	0	1	NC	3	NC	1
314			min	-.001	2	-.042	1	0	1	0	1	1452.749	1	NC	1
315		6	max	.001	3	.007	3	0	1	0	1	NC	5	NC	1
316			min	-.001	2	-.066	1	0	1	0	1	916.795	1	NC	1
317		7	max	.002	3	.012	3	0	1	0	1	NC	5	NC	1
318			min	-.002	2	-.097	1	0	1	0	1	628.593	1	NC	1
319		8	max	.002	3	.019	3	0	1	0	1	NC	5	NC	1
320			min	-.002	2	-.133	1	0	1	0	1	456.354	1	NC	1
321		9	max	.002	3	.027	3	0	1	0	1	NC	15	NC	1
322			min	-.002	2	-.176	1	0	1	0	1	344.449	1	NC	1
323		10	max	.002	3	.038	3	0	1	0	1	NC	15	NC	1
324			min	-.003	2	-.226	1	0	1	0	1	268.96	1	NC	1
325		11	max	.002	3	.051	3	0	1	0	1	8614.11	15	NC	1
326			min	-.003	2	-.28	1	0	1	0	1	216.4	1	NC	1
327		12	max	.003	3	.065	3	0	1	0	1	7137.955	15	NC	1
328			min	-.003	2	-.34	1	0	1	0	1	178.494	1	NC	1
329		13	max	.003	3	.081	3	0	1	0	1	6034.537	15	NC	1
330			min	-.003	2	-.404	1	0	1	0	1	150.323	1	NC	1
331		14	max	.003	3	.098	3	0	1	0	1	5189.148	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
332			min	-.004	2	-.471	1	0	1	0	1	128.848	1	NC	1
333		15	max	.003	3	.116	3	0	1	0	1	4527.852	15	NC	1
334			min	-.004	2	-.541	1	0	1	0	1	112.124	1	NC	1
335		16	max	.004	3	.134	3	0	1	0	1	4001.251	15	NC	1
336			min	-.004	2	-.614	2	0	1	0	1	98.813	2	NC	1
337		17	max	.004	3	.153	3	0	1	0	1	3575.557	15	NC	1
338			min	-.004	2	-.69	2	0	1	0	1	87.969	2	NC	1
339		18	max	.004	3	.173	3	0	1	0	1	3226.924	15	NC	1
340			min	-.005	2	-.767	2	0	1	0	1	79.141	2	NC	1
341		19	max	.004	3	.193	3	0	1	0	1	2938.256	15	NC	1
342			min	-.005	2	-.844	2	0	1	0	1	71.87	2	NC	1
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	3	0	1	2.147e-4	3	NC	1	NC	1
346			min	0	2	-.002	1	0	3	-5.021e-4	2	NC	1	NC	1
347		3	max	0	3	0	3	0	1	4.294e-4	3	NC	3	NC	1
348			min	0	2	-.008	1	0	3	-1.004e-3	2	8078.732	1	NC	1
349		4	max	0	3	.002	3	0	1	6.44e-4	3	NC	3	NC	1
350			min	0	2	-.017	1	0	3	-1.506e-3	2	3592.902	1	NC	1
351		5	max	0	3	.004	3	.001	1	8.587e-4	3	NC	3	NC	1
352			min	0	2	-.03	1	0	3	-2.009e-3	2	2021.869	1	NC	1
353		6	max	0	3	.007	3	.002	1	1.073e-3	3	NC	5	NC	1
354			min	0	2	-.047	1	-.001	3	-2.511e-3	2	1294.39	1	NC	1
355		7	max	0	3	.01	3	.002	1	1.288e-3	3	NC	5	NC	1
356			min	0	2	-.067	1	-.001	3	-3.013e-3	2	899.08	1	NC	1
357		8	max	0	3	.014	3	.003	1	1.503e-3	3	NC	5	NC	1
358			min	0	2	-.092	1	-.002	3	-3.515e-3	2	660.701	1	NC	1
359		9	max	0	3	.02	3	.003	1	1.442e-3	3	NC	5	NC	1
360			min	0	2	-.12	1	-.002	3	-3.426e-3	2	504.977	1	NC	1
361		10	max	0	3	.026	3	.004	1	1.22e-3	3	NC	15	NC	1
362			min	-.001	2	-.152	1	-.002	3	-2.99e-3	2	398.845	1	NC	1
363		11	max	0	3	.034	3	.004	1	9.975e-4	3	NC	15	NC	1
364			min	-.001	2	-.187	1	-.002	3	-2.553e-3	2	324.006	1	NC	1
365		12	max	0	3	.041	3	.005	1	7.752e-4	3	NC	15	NC	1
366			min	-.001	2	-.225	1	-.001	3	-2.117e-3	2	269.41	1	NC	1
367		13	max	.001	3	.05	3	.005	1	5.529e-4	3	8576.748	15	NC	1
368			min	-.001	2	-.266	1	0	3	-1.681e-3	2	228.425	1	NC	1
369		14	max	.001	3	.059	3	.005	1	3.306e-4	3	7404.757	15	NC	1
370			min	-.001	2	-.308	1	0	3	-1.245e-3	2	196.905	1	NC	1
371		15	max	.001	3	.069	3	.005	1	1.083e-4	3	6483.016	15	NC	1
372			min	-.002	2	-.352	1	0	15	-8.083e-4	2	172.168	1	NC	1
373		16	max	.001	3	.079	3	.005	1	6.202e-6	9	5745.502	15	NC	1
374			min	-.002	2	-.398	1	0	15	-3.721e-4	2	152.411	1	NC	1
375		17	max	.001	3	.089	3	.005	1	2.355e-4	1	5146.761	15	NC	1
376			min	-.002	2	-.445	1	0	15	-3.363e-4	3	136.398	1	NC	1
377		18	max	.001	3	.1	3	.006	3	6.495e-4	1	4654.529	15	NC	1
378			min	-.002	2	-.492	1	0	15	-5.586e-4	3	123.254	1	9909.307	3
379		19	max	.002	3	.11	3	.009	3	1.063e-3	1	4245.541	15	NC	1
380			min	-.002	2	-.54	1	0	15	-7.809e-4	3	112.347	1	7069.034	3
381	M3	1	max	.101	1	.002	3	.002	3	2.651e-4	2	NC	1	NC	1
382			min	-.016	3	-.011	1	-.003	1	-1.295e-4	3	NC	1	NC	1
383		2	max	.1	1	.014	3	.008	3	1.133e-3	2	NC	1	NC	3
384			min	-.016	3	-.069	2	-.018	2	-5.078e-4	3	6427.11	3	4625.227	2
385		3	max	.099	1	.026	3	.015	3	2.002e-3	2	NC	1	NC	4
386			min	-.015	3	-.128	2	-.034	2	-8.861e-4	3	3208.378	3	2339.705	2
387		4	max	.098	1	.039	3	.021	3	2.87e-3	2	NC	1	NC	4
388			min	-.014	3	-.186	2	-.049	2	-1.264e-3	3	2133.44	3	1587.892	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
389		5	max	.096	1	.051	3	.027	3	3.738e-3	2	NC	1	NC	5
390			min	-.014	3	-.244	2	-.062	2	-1.643e-3	3	1594.626	3	1220.316	2
391		6	max	.095	1	.063	3	.033	3	4.607e-3	2	NC	1	NC	5
392			min	-.013	3	-.302	2	-.075	2	-2.021e-3	3	1270.403	3	1007.399	2
393		7	max	.094	1	.076	3	.037	3	5.475e-3	2	NC	1	NC	5
394			min	-.013	3	-.36	2	-.086	2	-2.399e-3	3	1053.595	3	872.964	2
395		8	max	.093	1	.088	3	.041	3	6.343e-3	2	NC	5	NC	5
396			min	-.012	3	-.417	2	-.095	2	-2.778e-3	3	898.269	3	784.788	2
397		9	max	.092	1	.101	3	.044	3	7.212e-3	2	NC	5	NC	5
398			min	-.012	3	-.475	2	-.101	2	-3.156e-3	3	781.454	3	727.3	2
399		10	max	.09	1	.114	3	.046	3	8.08e-3	2	NC	5	NC	5
400			min	-.011	3	-.532	2	-.106	2	-3.534e-3	3	690.388	3	692.595	2
401		11	max	.089	1	.127	3	.047	3	8.948e-3	2	NC	5	NC	5
402			min	-.01	3	-.588	2	-.108	2	-3.913e-3	3	617.411	3	677.005	2
403		12	max	.088	1	.141	3	.046	3	9.817e-3	2	NC	5	NC	5
404			min	-.01	3	-.645	2	-.106	2	-4.291e-3	3	557.645	3	679.874	2
405		13	max	.087	1	.154	3	.044	3	1.068e-2	2	NC	1	NC	5
406			min	-.009	3	-.701	2	-.101	2	-4.669e-3	3	507.837	3	703.574	2
407		14	max	.086	1	.168	3	.041	3	1.155e-2	2	NC	1	NC	5
408			min	-.009	3	-.757	2	-.093	2	-5.048e-3	3	465.732	3	754.929	2
409		15	max	.084	1	.182	3	.036	3	1.242e-2	2	NC	1	NC	5
410			min	-.008	3	-.813	2	-.081	2	-5.426e-3	3	429.717	3	849.64	2
411		16	max	.083	1	.196	3	.029	3	1.329e-2	2	NC	1	NC	5
412			min	-.008	3	-.869	2	-.064	2	-5.804e-3	3	398.607	3	1026.159	2
413		17	max	.082	1	.21	3	.02	3	1.416e-2	2	NC	1	NC	4
414			min	-.007	3	-.925	2	-.043	2	-6.183e-3	3	371.513	3	1401.714	2
415		18	max	.081	1	.224	3	.009	3	1.503e-2	2	NC	1	NC	4
416			min	-.006	3	-.98	2	-.017	2	-6.561e-3	3	347.753	3	2565.068	2
417		19	max	.08	1	.239	3	.016	1	1.589e-2	2	NC	1	NC	1
418			min	-.006	3	-1.036	2	-.004	3	-6.939e-3	3	326.796	3	NC	1
419	M6	1	max	.147	1	.004	3	0	1	0	1	NC	1	NC	1
420			min	-.021	3	-.017	1	0	1	0	1	NC	1	NC	1
421		2	max	.144	1	.028	3	0	1	0	1	NC	1	NC	1
422			min	-.02	3	-.112	2	0	1	0	1	3179.86	3	NC	1
423		3	max	.142	1	.053	3	0	1	0	1	NC	1	NC	1
424			min	-.018	3	-.207	2	0	1	0	1	1588.662	3	NC	1
425		4	max	.139	1	.077	3	0	1	0	1	NC	1	NC	1
426			min	-.017	3	-.302	2	0	1	0	1	1057.763	3	NC	1
427		5	max	.137	1	.102	3	0	1	0	1	NC	1	NC	1
428			min	-.015	3	-.397	2	0	1	0	1	791.979	3	NC	1
429		6	max	.134	1	.126	3	0	1	0	1	NC	1	NC	1
430			min	-.014	3	-.492	2	0	1	0	1	632.274	3	NC	1
431		7	max	.132	1	.151	3	0	1	0	1	NC	1	NC	1
432			min	-.012	3	-.586	2	0	1	0	1	525.635	3	NC	1
433		8	max	.129	1	.176	3	0	1	0	1	NC	5	NC	1
434			min	-.011	3	-.681	2	0	1	0	1	449.343	3	NC	1
435		9	max	.126	1	.201	3	0	1	0	1	NC	5	NC	1
436			min	-.009	3	-.775	2	0	1	0	1	392.038	3	NC	1
437		10	max	.124	1	.226	3	0	1	0	1	NC	5	NC	1
438			min	-.008	3	-.869	2	0	1	0	1	347.408	3	NC	1
439		11	max	.121	1	.252	3	0	1	0	1	NC	5	NC	1
440			min	-.006	3	-.962	2	0	1	0	1	311.667	3	NC	1
441		12	max	.119	1	.278	3	0	1	0	1	NC	5	NC	1
442			min	-.005	3	-1.056	2	0	1	0	1	282.404	3	NC	1
443		13	max	.116	1	.303	3	0	1	0	1	NC	1	NC	1
444			min	-.003	3	-1.149	2	0	1	0	1	258.012	3	NC	1
445		14	max	.113	1	.329	3	0	1	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
446			min	-.002	3	-1.242	2	0	1	0	1	237.377	3	NC	1
447		15	max	.111	1	.356	3	0	1	0	1	NC	1	NC	1
448			min	0	3	-1.334	2	0	1	0	1	219.705	3	NC	1
449		16	max	.108	1	.382	3	0	1	0	1	NC	1	NC	1
450			min	.001	12	-1.427	2	0	1	0	1	204.413	3	NC	1
451		17	max	.106	1	.408	3	0	1	0	1	NC	1	NC	1
452			min	.002	12	-1.519	2	0	1	0	1	191.062	3	NC	1
453		18	max	.103	1	.435	3	0	1	0	1	NC	1	NC	1
454			min	.003	12	-1.611	2	0	1	0	1	179.317	3	NC	1
455		19	max	.101	1	.461	3	0	1	0	1	NC	1	NC	1
456			min	.003	15	-1.704	2	0	1	0	1	168.919	3	NC	1
457	M9	1	max	.101	1	.002	3	.003	1	1.295e-4	3	NC	1	NC	1
458			min	-.016	3	-.011	1	-.002	3	-2.651e-4	2	NC	1	NC	1
459		2	max	.1	1	.014	3	.018	2	5.078e-4	3	NC	1	NC	3
460			min	-.016	3	-.069	2	-.008	3	-1.133e-3	2	6427.11	3	4625.227	2
461		3	max	.099	1	.026	3	.034	2	8.861e-4	3	NC	1	NC	4
462			min	-.015	3	-.128	2	-.015	3	-2.002e-3	2	3208.378	3	2339.705	2
463		4	max	.098	1	.039	3	.049	2	1.264e-3	3	NC	1	NC	4
464			min	-.014	3	-.186	2	-.021	3	-2.87e-3	2	2133.44	3	1587.892	2
465		5	max	.096	1	.051	3	.062	2	1.643e-3	3	NC	1	NC	5
466			min	-.014	3	-.244	2	-.027	3	-3.738e-3	2	1594.626	3	1220.316	2
467		6	max	.095	1	.063	3	.075	2	2.021e-3	3	NC	1	NC	5
468			min	-.013	3	-.302	2	-.033	3	-4.607e-3	2	1270.403	3	1007.399	2
469		7	max	.094	1	.076	3	.086	2	2.399e-3	3	NC	1	NC	5
470			min	-.013	3	-.36	2	-.037	3	-5.475e-3	2	1053.595	3	872.964	2
471		8	max	.093	1	.088	3	.095	2	2.778e-3	3	NC	5	NC	5
472			min	-.012	3	-.417	2	-.041	3	-6.343e-3	2	898.269	3	784.788	2
473		9	max	.092	1	.101	3	.101	2	3.156e-3	3	NC	5	NC	5
474			min	-.012	3	-.475	2	-.044	3	-7.212e-3	2	781.454	3	727.3	2
475		10	max	.09	1	.114	3	.106	2	3.534e-3	3	NC	5	NC	5
476			min	-.011	3	-.532	2	-.046	3	-8.08e-3	2	690.388	3	692.595	2
477		11	max	.089	1	.127	3	.108	2	3.913e-3	3	NC	5	NC	5
478			min	-.01	3	-.588	2	-.047	3	-8.948e-3	2	617.411	3	677.005	2
479		12	max	.088	1	.141	3	.106	2	4.291e-3	3	NC	5	NC	5
480			min	-.01	3	-.645	2	-.046	3	-9.817e-3	2	557.645	3	679.874	2
481		13	max	.087	1	.154	3	.101	2	4.669e-3	3	NC	1	NC	5
482			min	-.009	3	-.701	2	-.044	3	-1.068e-2	2	507.837	3	703.574	2
483		14	max	.086	1	.168	3	.093	2	5.048e-3	3	NC	1	NC	5
484			min	-.009	3	-.757	2	-.041	3	-1.155e-2	2	465.732	3	754.929	2
485		15	max	.084	1	.182	3	.081	2	5.426e-3	3	NC	1	NC	5
486			min	-.008	3	-.813	2	-.036	3	-1.242e-2	2	429.717	3	849.64	2
487		16	max	.083	1	.196	3	.064	2	5.804e-3	3	NC	1	NC	5
488			min	-.008	3	-.869	2	-.029	3	-1.329e-2	2	398.607	3	1026.159	2
489		17	max	.082	1	.21	3	.043	2	6.183e-3	3	NC	1	NC	4
490			min	-.007	3	-.925	2	-.02	3	-1.416e-2	2	371.513	3	1401.714	2
491		18	max	.081	1	.224	3	.017	2	6.561e-3	3	NC	1	NC	4
492			min	-.006	3	-.98	2	-.009	3	-1.503e-2	2	347.753	3	2565.068	2
493		19	max	.08	1	.239	3	.004	3	6.939e-3	3	NC	1	NC	1
494			min	-.006	3	-1.036	2	-.016	1	-1.589e-2	2	326.796	3	NC	1