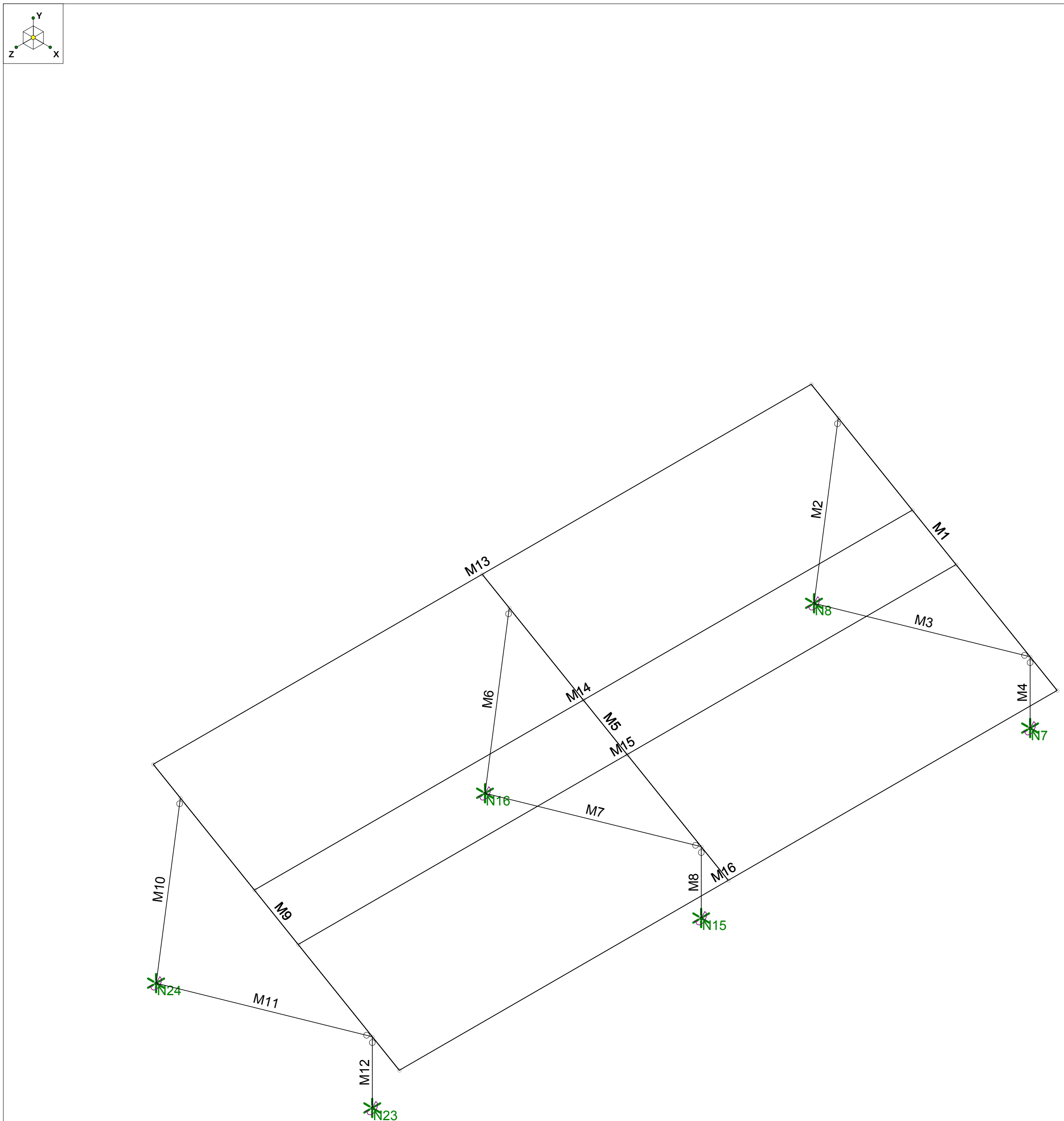


Schletter, Inc.	Standard PVMax Racking System	30° Tilt w/ Seismic Design
HCV	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

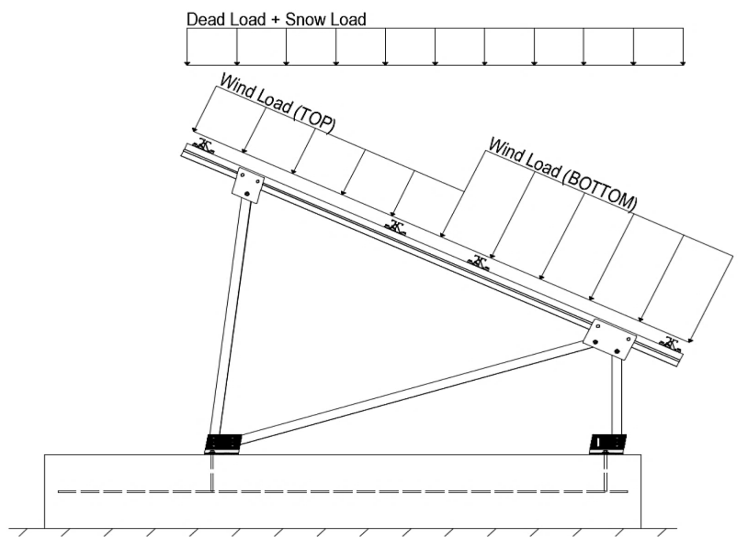
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 2
Module Tilt = 30°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads

Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 16.49 psf *(ASCE 7-05, Eq. 7-2)*
I_s = 1.00
C_s = 0.73
C_e = 0.90
C_t = 1.20

2.3 Wind Loads

Design Wind Speed, V = 110 mph Exposure Category = C
Height < 15 ft Importance Category = II

Peak Velocity Pressure, q_z = 19.00 psf *Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.150	(Pressure)
$Cf+_{BOTTOM}$	=	1.850	
$Cf-_{TOP, OUTER PURLIN}$	=	-2.600	
$Cf-_{TOP, INNER PURLIN}$	=	-2.000	(Suction)
$Cf-_{BOTTOM}$	=	-1.100	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.06	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W
1.2D + 1.6W + 0.5S
0.9D + 1.6W ^{M}
1.54D + 1.3E + 0.2S ^{R}
0.56D + 1.3E ^{R}
1.54D + 1.25E + 0.2S ^{O}
0.56D + 1.25E ^{O}

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 1.0W
1.0D + 0.75L + 0.75W + 0.75S
0.6D + 1.0W ^{M}
1.238D + 0.875E ^{O}
1.1785D + 0.65625E + 0.75S ^{O}
0.362D + 0.875E ^{O}

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

^{M} *Uses the minimum allowable module dead load.*
^{R} *Include redundancy factor of 1.3.*
^{O} *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	Diagonal Struts	Location	Front Reactions	Location
M13	Top	M3	Outer	N7	Outer
M14	Mid-Top	M7	Inner	N15	Inner
M15	Mid-Bottom	M11	Outer	N23	Outer
M16	Bottom				

Girders	Location	Rear Struts	Location	Rear Reactions	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

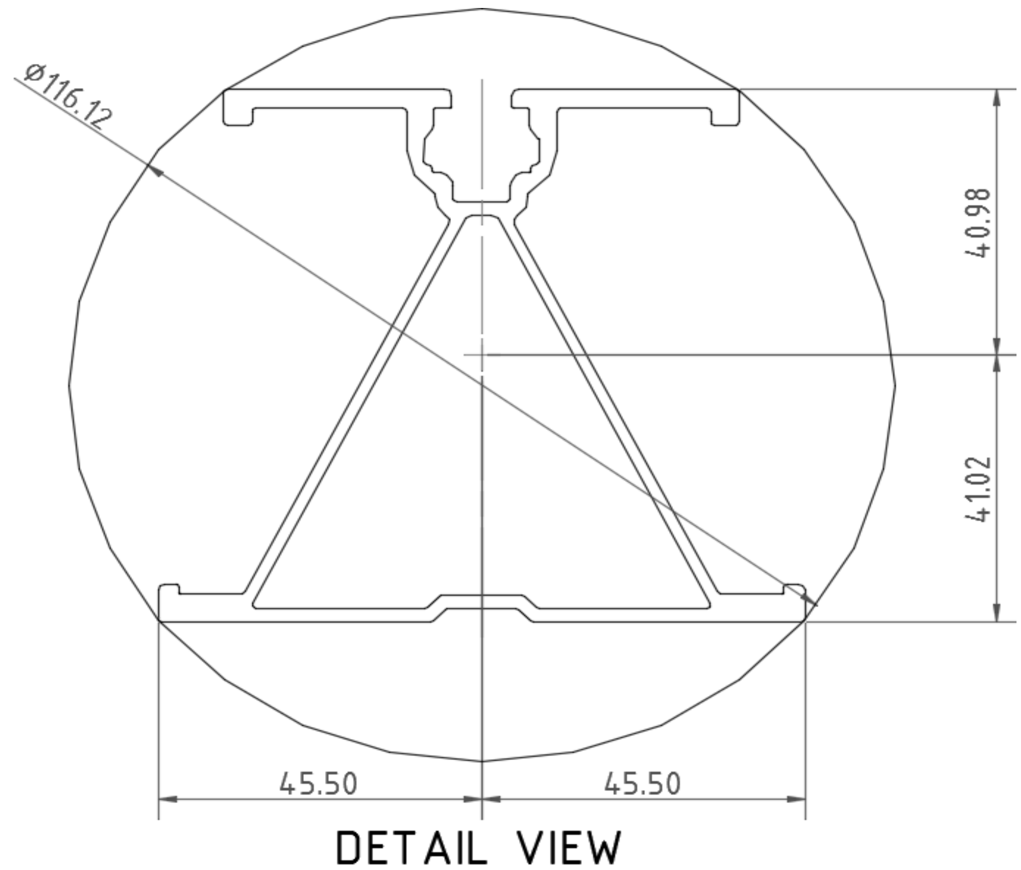
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

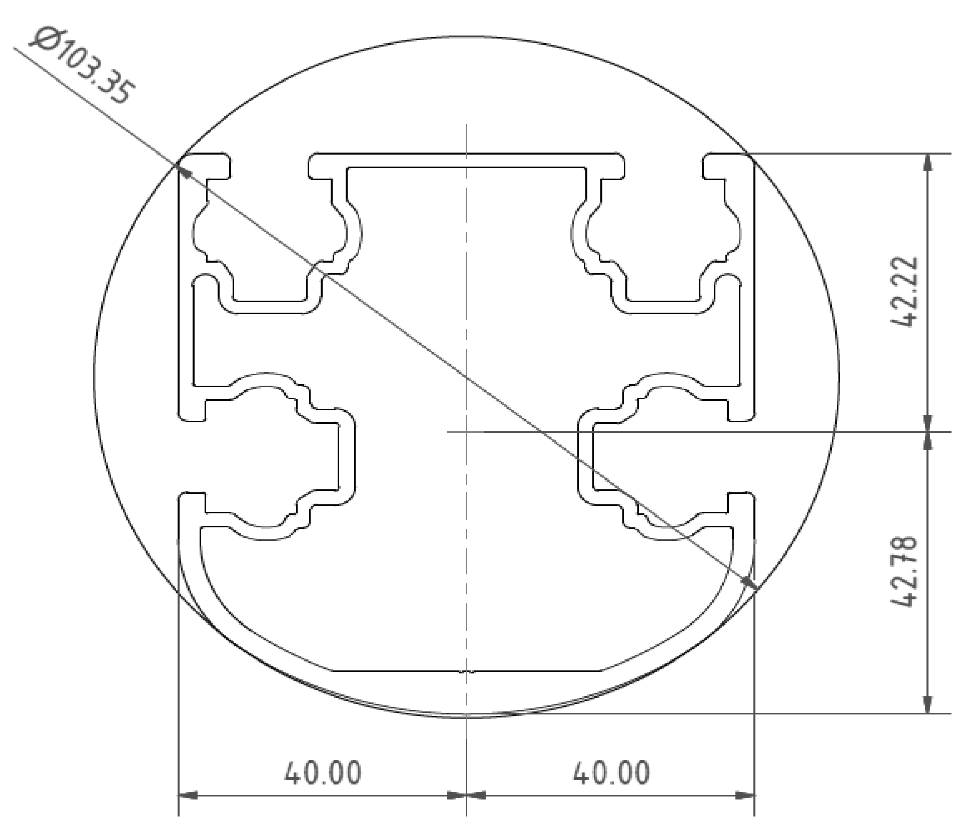
Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	114	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	-2.431	k-ft
M_z =	0.014	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	89%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

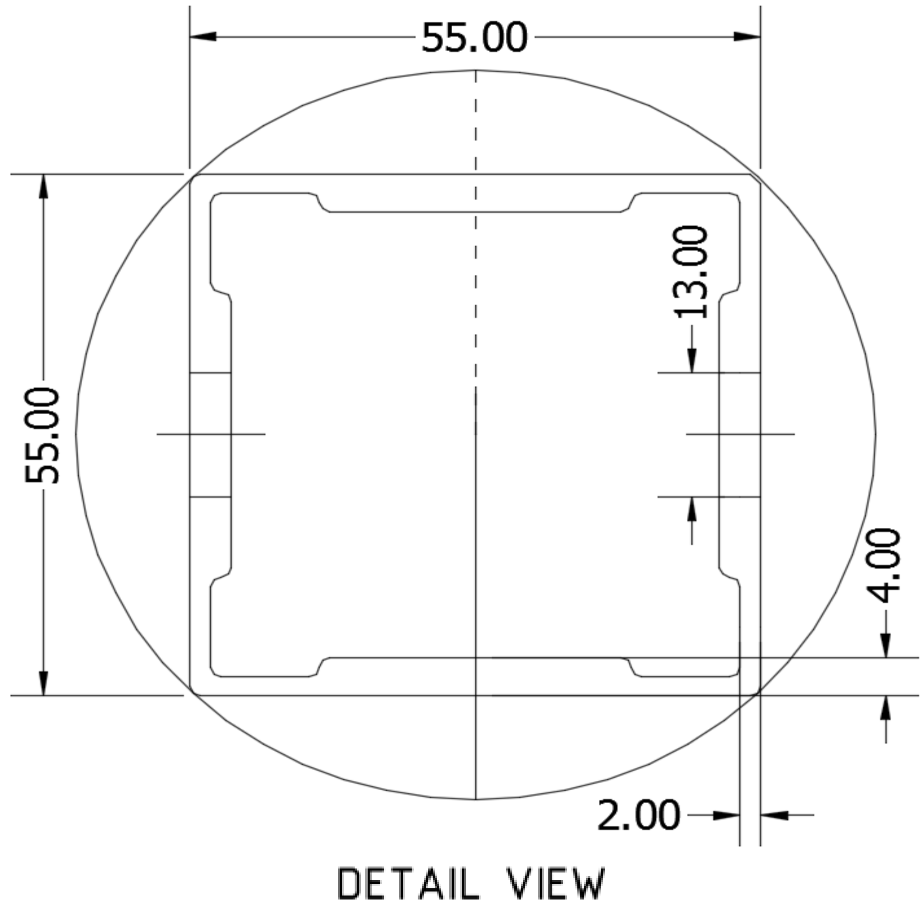
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	88.90	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.35	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-3.156	k-ft
M_z =	0.000	k-ft
P_n =	-0.938	k
$M_{y\ allowable}$ =	3.464	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	93%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

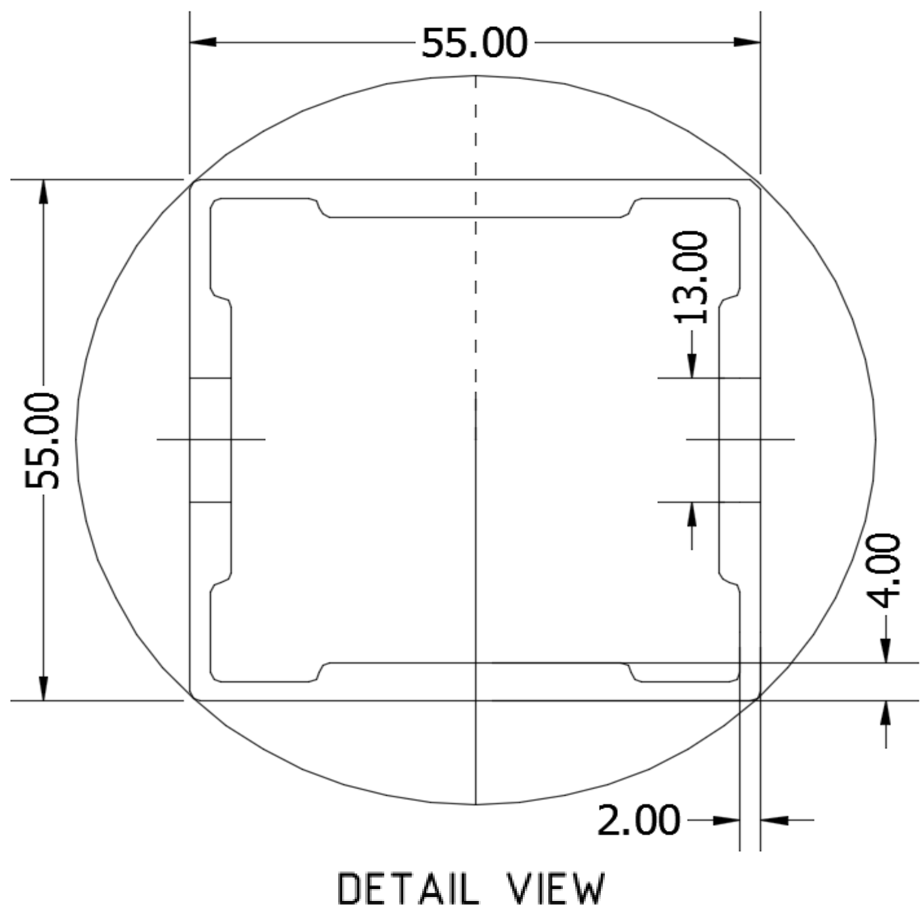
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	24.80	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.519	k-ft
P_n =	0.565	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	39%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

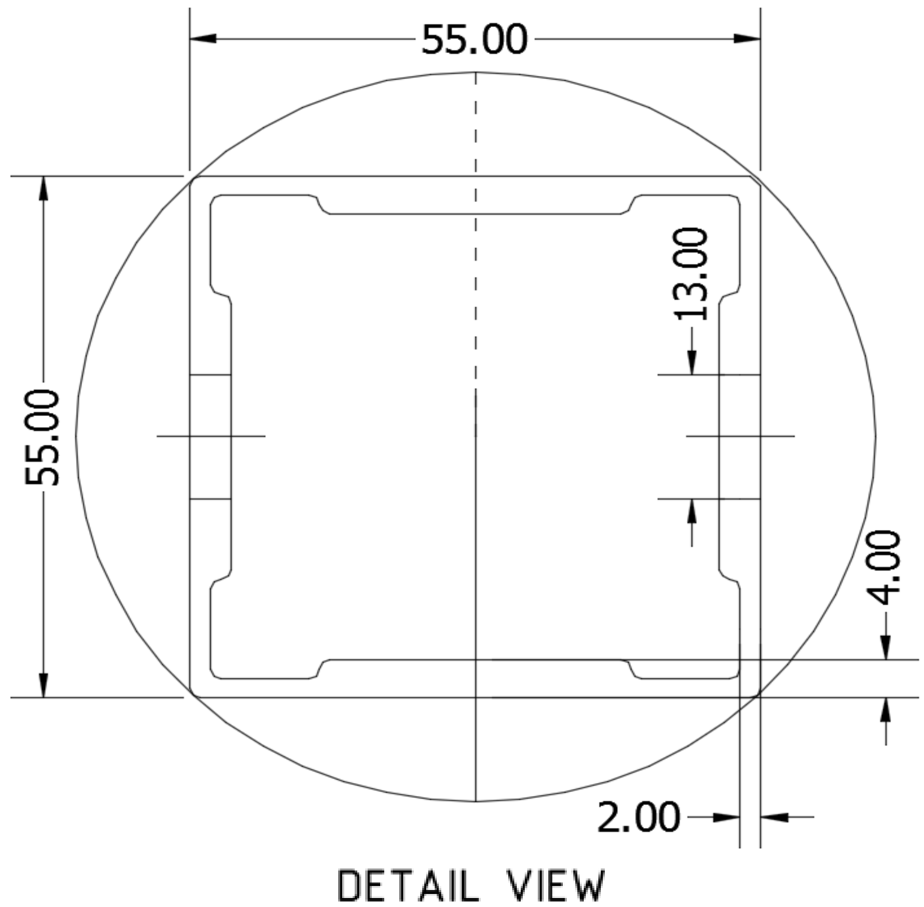
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	86.60	in
$\Phi F_{ty\ AXIAL}$ =	7.50	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.010	k-ft
M_z =	0.000	k-ft
P_n =	2.730	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	7.371	k
Utilization =	38%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	70.83	in
$\Phi F_{ty\ AXIAL}$ =	10.55	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.010	k-ft
M_z =	0.000	k-ft
P_n =	3.367	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	10.365	k
Utilization =	33%	



5. FOUNDATION DESIGN CALCULATIONS

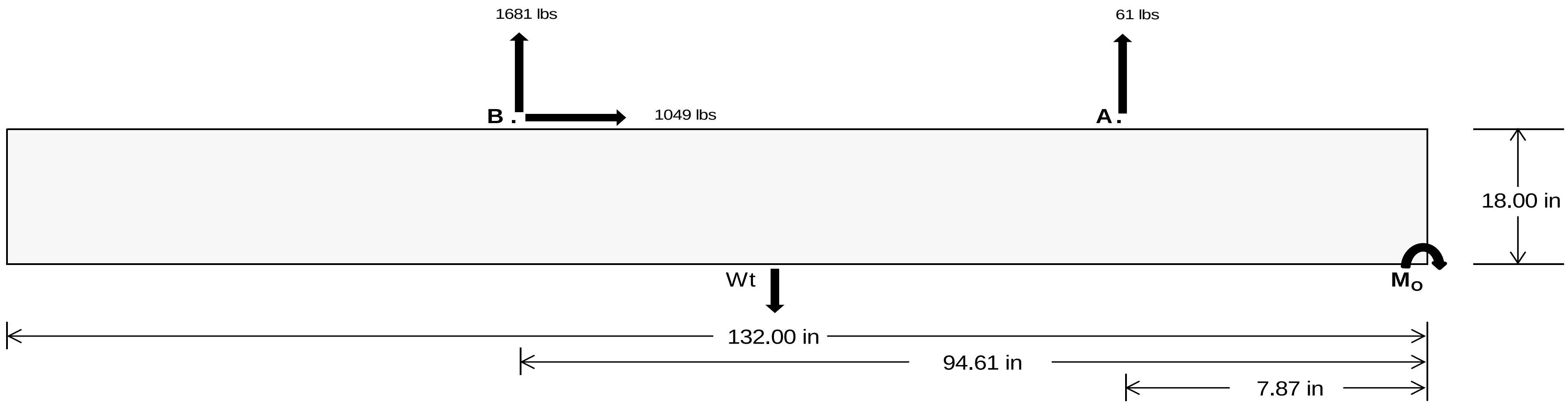
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	266.96	7001.35	k
Compressive Load =	3465.08	5319.24	k
Lateral Load =	361.75	4362.68	k
Moment (Weak Axis) =	0.70	0.25	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC tables 1804.2 (2003, 2006) & 1806.2 (2009).



Concrete Properties

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

Footing Reinforcement

Use fiber reinforcing with (3) #5 rebar.

Overturning Check

M_O =	178350.1 in-lbs
Resisting Force Required =	2702.27 lbs
S.F. =	1.67
Weight Required =	4503.79 lbs
Minimum Width =	36 in in
Weight Provided =	7177.50 lbs

A minimum 132in long x 36in wide x 18in tall ballast foundation is required to resist overturning.

Sliding

Force =	1048.52 lbs
Friction =	0.4
Weight Required =	2621.30 lbs
Resisting Weight =	7177.50 lbs
Additional Weight Required =	0 lbs

Use a 132in long x 36in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion

Sliding Force =	1048.52 lbs
Cohesion =	130 psf
Area =	33.00 ft^2
Resisting =	3588.75 lbs
Additional Weight Required =	0 lbs

Use a 132in long x 36in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	36 in	37 in	38 in	39 in
P_{ftg} = (145 pcf)(11 ft)(1.5 ft)(3 ft) =	7178 lbs	7377 lbs	7576 lbs	7776 lbs

ASD LC	1.0D + 1.0S				1.0D + 1.0W				1.0D + 0.75L + 0.75W + 0.75S				0.6D + 1.0W			
Width	36 in	37 in	38 in	39 in	36 in	37 in	38 in	39 in	36 in	37 in	38 in	39 in	36 in	37 in	38 in	39 in
F_A	1166 lbs	1166 lbs	1166 lbs	1166 lbs	1374 lbs	1374 lbs	1374 lbs	1374 lbs	1781 lbs	1781 lbs	1781 lbs	1781 lbs	-122 lbs	-122 lbs	-122 lbs	-122 lbs
F_B	1107 lbs	1107 lbs	1107 lbs	1107 lbs	2343 lbs	2343 lbs	2343 lbs	2343 lbs	2470 lbs	2470 lbs	2470 lbs	2470 lbs	-3361 lbs	-3361 lbs	-3361 lbs	-3361 lbs
F_V	173 lbs	173 lbs	173 lbs	173 lbs	1895 lbs	1895 lbs	1895 lbs	1895 lbs	1534 lbs	1534 lbs	1534 lbs	1534 lbs	-2097 lbs	-2097 lbs	-2097 lbs	-2097 lbs
P_{total}	9451 lbs	9650 lbs	9850 lbs	10049 lbs	10894 lbs	11094 lbs	11293 lbs	11493 lbs	11428 lbs	11628 lbs	11827 lbs	12026 lbs	823 lbs	943 lbs	1062 lbs	1182 lbs
M	3270 lbs-ft	3270 lbs-ft	3270 lbs-ft	3270 lbs-ft	3914 lbs-ft	3914 lbs-ft	3914 lbs-ft	3914 lbs-ft	5039 lbs-ft	5039 lbs-ft	5039 lbs-ft	5039 lbs-ft	4275 lbs-ft	4275 lbs-ft	4275 lbs-ft	4275 lbs-ft
e	0.35 ft	0.34 ft	0.33 ft	0.33 ft	0.36 ft	0.35 ft	0.35 ft	0.34 ft	0.44 ft	0.43 ft	0.43 ft	0.42 ft	5.19 ft	4.53 ft	4.02 ft	3.62 ft
L/6	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft	1.83 ft
f_{min}	232.3 psf	231.9 psf	231.6 psf	231.2 psf	265.4 psf	264.1 psf	262.9 psf	261.7 psf	263.0 psf	261.8 psf	260.6 psf	259.5 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	340.4 psf	337.1 psf	334.0 psf	331.0 psf	394.8 psf	390.0 psf	385.5 psf	381.2 psf	429.6 psf	423.9 psf	418.4 psf	413.3 psf	597.8 psf	211.2 psf	151.6 psf	128.8 psf

Maximum Bearing Pressure =	598 psf
Allowable Bearing Pressure =	1500 psf

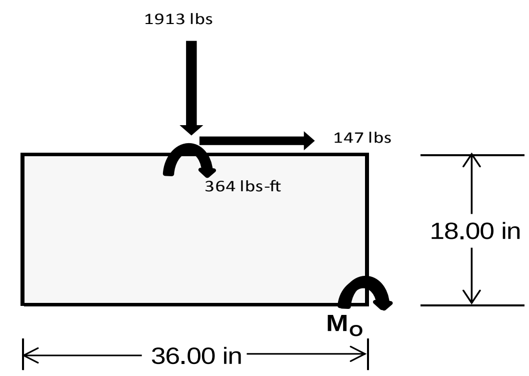
Use a 132in long x 36in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 2284.3 ft-lbs
Resisting Force Required = 1522.85 lbs
S.F. = 1.67
Weight Required = 2538.09 lbs
Minimum Width = 36 in in
Weight Provided = 7177.50 lbs

A minimum 132in long x 36in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	36 in			36 in			36 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	287 lbs	599 lbs	193 lbs	729 lbs	1913 lbs	657 lbs	117 lbs	175 lbs	24 lbs
F_V	203 lbs	200 lbs	207 lbs	150 lbs	147 lbs	161 lbs	204 lbs	200 lbs	206 lbs
P_{total}	9173 lbs	9485 lbs	9079 lbs	9187 lbs	10371 lbs	9116 lbs	2715 lbs	2773 lbs	2622 lbs
M	783 lbs-ft	774 lbs-ft	796 lbs-ft	583 lbs-ft	585 lbs-ft	620 lbs-ft	783 lbs-ft	773 lbs-ft	787 lbs-ft
e	0.09 ft	0.08 ft	0.09 ft	0.06 ft	0.06 ft	0.07 ft	0.29 ft	0.28 ft	0.30 ft
L/6	0.50 ft	0.50 ft	0.50 ft	0.50 ft	0.50 ft	0.50 ft	0.50 ft	0.50 ft	0.50 ft
f_{min}	230.5 psf	240.5 psf	226.9 psf	243.1 psf	278.8 psf	238.6 psf	34.8 psf	37.2 psf	31.7 psf
f_{max}	325.4 psf	334.3 psf	323.4 psf	313.8 psf	349.7 psf	313.8 psf	129.7 psf	130.9 psf	127.2 psf

Maximum Bearing Pressure = 350 psf
Allowable Bearing Pressure = 1500 psf

Use a 132in long x 36in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 132in long x 36in wide x 18in tall ballast foundation and fiber reinforcing with (3) #5 rebar.

5.3 Foundation Anchors

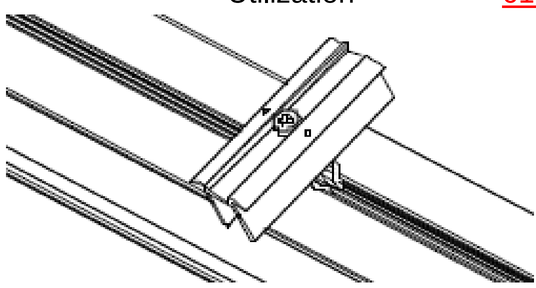
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

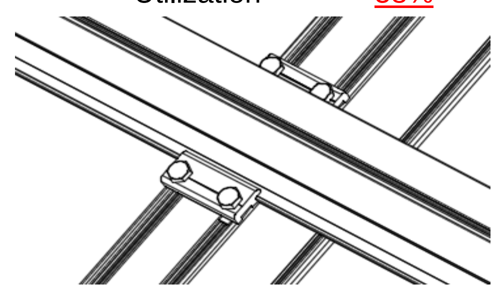
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

Fastening of Modules to Purlins	
Maximum Uplifting Force =	0.744 k
Allowable Uplift =	1.214 k
Utilization =	61%



Fastening of Purlins to Girders	
Maximum Uplifting Force =	2.527 k
Allowable Uplift =	4.357 k
Utilization =	58%



6.2 Strut Connections

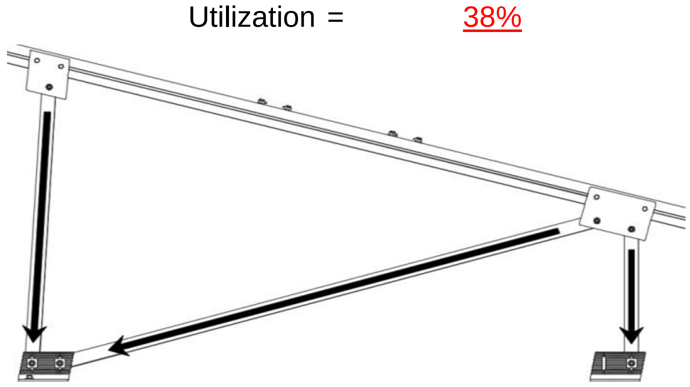
The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut	
Maximum Axial Load =	2.665 k
M12 Bolt Capacity =	12.808 k
Strut Bearing Capacity =	7.421 k
Utilization =	36%

Rear Strut	
Maximum Axial Load =	4.668 k
M12 Bolt Capacity =	12.808 k
Strut Bearing Capacity =	7.421 k
Utilization =	63%

Diagonal Strut	
Maximum Axial Load =	2.815 k
M12 Bolt Shear Capacity =	12.808 k
Strut Bearing Capacity =	7.421 k
Utilization =	38%

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)



Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

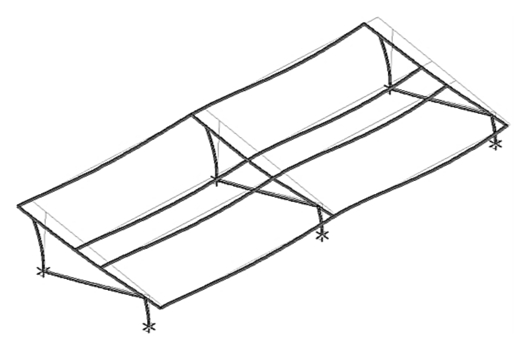
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	48.27 in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$ 0.965 in
Max Drift, Δ_{MAX} =	0.617 in

$0.617 \le 0.965$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 114 in

J = 0.432

315.377

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 27.5 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in³

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 114

J = 0.432

200.561

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.8

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in³

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
$\varphi F_L = (\varphi ck2*\sqrt{(BpE)})/(1.6b/t)$
$\varphi F_L =$ 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
$\varphi F_L = \varphi yFcy$
$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
$P_{max} =$ 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:

3.4.14

$L_b =$ 88.9 in
J = 1.08
152.913

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)}/2))}]$
$\varphi F_L =$ 29.4 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 31.6 ksi

Weak Axis:

3.4.14

$L_b =$ 88.9
J = 1.08
161.829

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)}/2))}]$
$\varphi F_L =$ 29.2

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
$\varphi F_L = \varphi yFcy$
$\varphi F_L =$ 33.3 ksi

3.4.16.1 Used

Rb/t = 18.1

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

$\varphi F_L = \varphi b[Bt-Dt^*\sqrt{(Rb/t)}]$

$\varphi F_L =$ 31.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 35.2

m = 0.68

C_0 = 41.067

Cc = 43.717

$$S2 = \frac{k_1Bbr}{mDbr}$$

S2 = 73.8

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L St =$ 29.4 ksi

Ix = 984962 mm^4

2.366 in^4

y = 43.717 mm

Sx = 1.375 in^3

$M_{max}St$ = 3.363 k-ft

3.4.18

h/t = 16.2

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40

Cc = 40

$$S2 = \frac{k_1Bbr}{mDbr}$$

S2 = 77.3

$\varphi F_L = 1.3\varphi yFcy$

$\varphi F_L =$ 43.2 ksi

$\varphi F_L Wk =$ 33.3 ksi

Iy = 923544 mm^4

2.219 in^4

x = 40 mm

Sy = 1.409 in^3

$M_{max}Wk$ = 3.904 k-ft

Compression

3.4.9

b/t = 16.2

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi c[Bp-1.6Dp^*b/t]$

$\varphi F_L =$ 31.6 ksi

b/t = 7.4

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi c[Bt-Dt^*\sqrt{(Rb/t)}]$

$\varphi F_L =$ 31.09 ksi

$\varphi F_L =$ 31.09 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.87952

φF_L= φcc(Bc-Dc*λ)

φF_L= 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 86.60 in

J = 0.942

135.148

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6 ksi

Weak Axis:

3.4.14

L_b = 86.6

J = 0.942

135.148

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.6

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in³

M_{max}St = 1.460 k-ft

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in³

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 2.00335

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.86047

φF_L= (φccFcy)/(λ²)

φF_L= 7.50396 ksi

3.4.9

b/t = 24.5
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

b/t = 24.5
S1 = 12.21
S2 = 32.70
$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
$\varphi F_L = \varphi yFcy$
$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 7.50 ksi
A = 663.99 mm^2
1.03 in^2
$P_{max} =$ 7.72 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

$L_b =$ 70.83 in
J = 0.942
110.537

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)/2}))}]$
$\varphi F_L =$ 30.0 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

Weak Axis:

3.4.14

$L_b =$ 70.83
J = 0.942
110.537

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
$\varphi F_L = \varphi b[Bc-1.6Dc*\sqrt{((LbSc)/(Cb*\sqrt{(IyJ)/2}))}]$
$\varphi F_L =$ 30.0

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
$\varphi F_L = \varphi b[Bp-1.6Dp*b/t]$
$\varphi F_L =$ 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$S2 = C_t$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.63853

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.80939

φF_L= (φccFcy)/(λ²)

φF_L= 10.5516 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 10.55 ksi

A = 663.99 mm^2

1.03 in^2

$P_{max} =$ 10.86 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M14	Y	-8.366	-8.366	0	0
3	M15	Y	-8.366	-8.366	0	0
4	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M14	Y	-4.45	-4.45	0	0
3	M15	Y	-4.45	-4.45	0	0
4	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-39.836	-39.836	0	0
2	M14	Y	-39.836	-39.836	0	0
3	M15	Y	-39.836	-39.836	0	0
4	M16	Y	-39.836	-39.836	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-60.928	-60.928	0	0
2	M14	y	-60.928	-60.928	0	0
3	M15	y	-98.014	-98.014	0	0
4	M16	y	-98.014	-98.014	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	137.749	137.749	0	0
2	M14	y	105.961	105.961	0	0
3	M15	y	58.278	58.278	0	0
4	M16	y	58.278	58.278	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M14	Z	6.693	6.693	0	0
3	M15	Z	6.693	6.693	0	0
4	M16	Z	6.693	6.693	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8														
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6														
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65..	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	872.538	2	1262.497	2	.6	1	.003	1	0	1	0	1
2		min	-1059.952	3	-1656.494	3	-32.177	5	-.191	4	0	1	0	1
3	N7	max	.032	9	1021.811	1	-.65	12	-.001	12	0	1	0	1
4		min	-.219	2	-39.478	5	-278.267	4	-.536	4	0	1	0	1
5	N15	max	.029	9	2665.445	1	0	9	0	9	0	1	0	1
6		min	-2.358	2	-205.357	3	-265.688	4	-.519	4	0	1	0	1
7	N16	max	3089.558	2	4091.721	2	0	2	0	2	0	1	0	1
8		min	-3355.908	3	-5385.65	3	-32.133	5	-.193	4	0	1	0	1
9	N23	max	.038	14	1021.811	1	10.342	1	.02	1	0	1	0	1
10		min	-.219	2	-32.033	3	-270.482	5	-.524	4	0	1	0	1
11	N24	max	872.538	2	1262.497	2	-.045	12	0	12	0	1	0	1
12		min	-1059.952	3	-1656.494	3	-32.803	5	-.192	4	0	1	0	1
13	Totals:	max	4831.837	2	10928.84	2	0	9						
14		min	-5476.043	3	-8968.061	3	-906.644	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	99.356	1	439.134	2	-9.141	12	0	3	.237	1	0	4
2			min	6.589	12	-768.958	3	-171.912	1	-.015	2	.016	12	0	3
3		2	max	99.356	1	307.199	2	-7.256	12	0	3	.116	4	.691	3
4			min	6.589	12	-541.214	3	-132.022	1	-.015	2	.007	12	-.394	2
5		3	max	99.356	1	175.263	2	-5.37	12	0	3	.063	5	1.143	3
6			min	6.589	12	-313.47	3	-92.132	1	-.015	2	-.042	1	-.649	2
7		4	max	99.356	1	43.328	2	-3.485	12	0	3	.033	5	1.353	3
8			min	6.589	12	-85.726	3	-52.242	1	-.015	2	-.118	1	-.764	2
9		5	max	99.356	1	142.018	3	-.942	10	0	3	.005	5	1.324	3
10			min	6.589	12	-88.608	2	-27.723	4	-.015	2	-.152	1	-.74	2
11		6	max	99.356	1	369.762	3	27.538	1	0	3	-.008	12	1.053	3
12			min	2.372	15	-220.543	2	-21.416	5	-.015	2	-.144	1	-.577	2
13		7	max	99.356	1	597.506	3	67.428	1	0	3	-.006	12	.543	3
14			min	-7.018	5	-352.478	2	-18.499	5	-.015	2	-.094	1	-.274	2
15		8	max	99.356	1	825.251	3	107.317	1	0	3	.002	2	.167	2
16			min	-17.853	5	-484.414	2	-15.582	5	-.015	2	-.059	4	-.208	3
17		9	max	99.356	1	1052.995	3	147.207	1	0	3	.133	1	.748	2
18			min	-28.689	5	-616.349	2	-12.665	5	-.015	2	-.073	5	-1.199	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	99.356	1	748.285	2	-7.828	12	.015	2	.309	1	1.468	2
20			min	6.589	12	-1280.739	3	-187.097	1	0	3	.01	12	-2.431	3
21		11	max	99.356	1	616.349	2	-5.943	12	.015	2	.133	1	.748	2
22			min	6.589	12	-1052.995	3	-147.207	1	0	3	.002	12	-1.199	3
23		12	max	99.356	1	484.414	2	-4.057	12	.015	2	.057	4	.167	2
24			min	6.589	12	-825.251	3	-107.317	1	0	3	-.005	3	-.208	3
25		13	max	99.356	1	352.478	2	-2.172	12	.015	2	.026	5	.543	3
26			min	6.589	12	-597.506	3	-67.428	1	0	3	-.094	1	-.274	2
27		14	max	99.356	1	220.543	2	-.286	12	.015	2	-.001	15	1.053	3
28			min	6.589	12	-369.762	3	-32.008	4	0	3	-.144	1	-.577	2
29		15	max	99.356	1	88.608	2	12.352	1	.015	2	-.007	12	1.324	3
30			min	-.234	15	-142.018	3	-22.439	5	0	3	-.152	1	-.74	2
31		16	max	99.356	1	85.726	3	52.242	1	.015	2	-.004	12	1.353	3
32			min	-10.946	5	-43.328	2	-19.522	5	0	3	-.118	1	-.764	2
33		17	max	99.356	1	313.47	3	92.132	1	.015	2	0	3	1.143	3
34			min	-21.781	5	-175.263	2	-16.605	5	0	3	-.079	4	-.649	2
35		18	max	99.356	1	541.214	3	132.022	1	.015	2	.077	1	.691	3
36			min	-32.617	5	-307.199	2	-13.687	5	0	3	-.085	5	-.394	2
37		19	max	99.356	1	768.958	3	171.912	1	.015	2	.237	1	0	2
38			min	-43.452	5	-439.134	2	-10.77	5	0	3	-.098	5	0	3
39	M14	1	max	53.412	4	472.423	2	-9.395	12	.01	3	.272	1	0	4
40			min	2.822	12	-608.247	3	-177.474	1	-.011	2	.018	12	0	3
41		2	max	47.562	1	340.488	2	-7.509	12	.01	3	.168	4	.55	3
42			min	2.822	12	-434.19	3	-137.584	1	-.011	2	.009	12	-.429	2
43		3	max	47.562	1	208.553	2	-5.624	12	.01	3	.094	5	.917	3
44			min	2.822	12	-260.132	3	-97.694	1	-.011	2	-.018	1	-.719	2
45		4	max	47.562	1	76.617	2	-3.738	12	.01	3	.051	5	1.099	3
46			min	2.822	12	-86.074	3	-57.804	1	-.011	2	-.1	1	-.869	2
47		5	max	47.562	1	87.984	3	-1.653	10	.01	3	.01	5	1.098	3
48			min	-1.072	5	-55.318	2	-41.872	4	-.011	2	-.14	1	-.881	2
49		6	max	47.562	1	262.041	3	21.976	1	.01	3	-.007	12	.914	3
50			min	-11.907	5	-187.254	2	-34.056	5	-.011	2	-.138	1	-.753	2
51		7	max	47.562	1	436.099	3	61.866	1	.01	3	-.006	12	.545	3
52			min	-22.743	5	-319.189	2	-31.138	5	-.011	2	-.094	1	-.485	2
53		8	max	47.562	1	610.157	3	101.756	1	.01	3	0	10	-.001	15
54			min	-33.578	5	-451.124	2	-28.221	5	-.011	2	-.097	4	-.079	2
55		9	max	47.562	1	784.215	3	141.646	1	.01	3	.121	1	.467	2
56			min	-44.414	5	-583.06	2	-25.304	5	-.011	2	-.121	5	-.743	3
57		10	max	73.127	4	714.995	2	-7.575	12	.011	2	.292	1	1.152	2
58			min	2.822	12	-958.272	3	-181.536	1	-.01	3	.009	12	-1.663	3
59		11	max	62.292	4	583.06	2	-5.689	12	.011	2	.169	4	.467	2
60			min	2.822	12	-784.215	3	-141.646	1	-.01	3	.002	12	-.743	3
61		12	max	51.456	4	451.124	2	-3.804	12	.011	2	.092	5	-.001	15
62			min	2.822	12	-610.157	3	-101.756	1	-.01	3	-.007	1	-.079	2
63		13	max	47.562	1	319.189	2	-1.918	12	.011	2	.048	5	.545	3
64			min	2.822	12	-436.099	3	-61.866	1	-.01	3	-.094	1	-.485	2
65		14	max	47.562	1	187.254	2	.047	3	.011	2	.007	5	.914	3
66			min	2.822	12	-262.041	3	-42.742	4	-.01	3	-.138	1	-.753	2
67		15	max	47.562	1	55.318	2	17.914	1	.011	2	-.006	12	1.098	3
68			min	2.822	12	-87.984	3	-34.264	5	-.01	3	-.14	1	-.881	2
69		16	max	47.562	1	86.074	3	57.804	1	.011	2	-.003	12	1.099	3
70			min	-3.169	5	-76.617	2	-31.346	5	-.01	3	-.1	1	-.869	2
71		17	max	47.562	1	260.132	3	97.694	1	.011	2	.003	3	.917	3
72			min	-14.005	5	-208.553	2	-28.429	5	-.01	3	-.102	4	-.719	2
73		18	max	47.562	1	434.19	3	137.584	1	.011	2	.106	1	.55	3
74			min	-24.84	5	-340.488	2	-25.512	5	-.01	3	-.125	5	-.429	2
75		19	max	47.562	1	608.247	3	177.474	1	.011	2	.272	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-35.676	5	-472.423	2	-22.595	5	-.01	3	-.15	5	0	3
77	M15	1	max	81.386	5	683.844	2	-9.316	12	.012	2	.306	4	0	2
78			min	-49.804	1	-336.686	3	-177.459	1	-.009	3	.017	12	0	3
79		2	max	70.55	5	489.275	2	-7.431	12	.012	2	.206	4	.306	3
80			min	-49.804	1	-243.159	3	-137.569	1	-.009	3	.008	12	-.619	2
81		3	max	59.715	5	294.705	2	-5.545	12	.012	2	.121	5	.513	3
82			min	-49.804	1	-149.633	3	-97.679	1	-.009	3	-.018	1	-1.033	2
83		4	max	48.879	5	100.136	2	-3.66	12	.012	2	.067	5	.622	3
84			min	-49.804	1	-56.107	3	-64.146	4	-.009	3	-.1	1	-1.241	2
85		5	max	38.044	5	37.42	3	-1.689	10	.012	2	.016	5	.632	3
86			min	-49.804	1	-94.434	2	-51.919	4	-.009	3	-.14	1	-1.244	2
87		6	max	27.208	5	130.946	3	21.991	1	.012	2	-.007	12	.543	3
88			min	-49.804	1	-289.003	2	-44.065	5	-.009	3	-.138	1	-1.042	2
89		7	max	16.373	5	224.473	3	61.88	1	.012	2	-.006	12	.355	3
90			min	-49.804	1	-483.573	2	-41.148	5	-.009	3	-.1	4	-.634	2
91		8	max	5.537	5	317.999	3	101.77	1	.012	2	0	10	.069	3
92			min	-49.804	1	-678.142	2	-38.231	5	-.009	3	-.123	4	-.03	1
93		9	max	-3.409	12	411.526	3	141.66	1	.012	2	.121	1	.797	2
94			min	-49.804	1	-872.712	2	-35.314	5	-.009	3	-.158	5	-.316	3
95		10	max	-3.409	12	1067.281	2	-7.653	12	.009	3	.306	4	1.821	2
96			min	-49.804	1	-505.052	3	-181.55	1	-.012	2	.009	12	-.8	3
97		11	max	-1.526	15	872.712	2	-5.768	12	.009	3	.205	4	.797	2
98			min	-49.804	1	-411.526	3	-141.66	1	-.012	2	.002	12	-.316	3
99		12	max	-3.409	12	678.142	2	-3.882	12	.009	3	.118	5	.069	3
100			min	-49.804	1	-317.999	3	-101.77	1	-.012	2	-.007	1	-.03	1
101		13	max	-3.409	12	483.573	2	-1.997	12	.009	3	.063	5	.355	3
102			min	-49.804	1	-224.473	3	-65.043	4	-.012	2	-.094	1	-.634	2
103		14	max	-3.409	12	289.003	2	-.078	3	.009	3	.012	5	.543	3
104			min	-49.804	1	-130.946	3	-52.816	4	-.012	2	-.138	1	-1.042	2
105		15	max	-3.409	12	94.434	2	17.899	1	.009	3	-.006	12	.632	3
106			min	-58.203	4	-37.42	3	-44.278	5	-.012	2	-.14	1	-1.244	2
107		16	max	-3.409	12	56.107	3	57.789	1	.009	3	-.003	12	.622	3
108			min	-69.039	4	-100.136	2	-41.361	5	-.012	2	-.106	4	-1.241	2
109		17	max	-3.409	12	149.633	3	97.679	1	.009	3	.003	3	.513	3
110			min	-79.874	4	-294.705	2	-38.443	5	-.012	2	-.129	4	-1.033	2
111		18	max	-3.409	12	243.159	3	137.569	1	.009	3	.106	1	.306	3
112			min	-90.71	4	-489.275	2	-35.526	5	-.012	2	-.163	5	-.619	2
113		19	max	-3.409	12	336.686	3	177.459	1	.009	3	.272	1	0	2
114			min	-101.545	4	-683.844	2	-32.609	5	-.012	2	-.199	5	0	5
115	M16	1	max	79.471	5	651.815	2	-8.878	12	.01	2	.242	4	0	2
116			min	-106.856	1	-310.003	3	-172.2	1	-.012	3	.015	12	0	3
117		2	max	68.636	5	457.245	2	-6.993	12	.01	2	.156	4	.278	3
118			min	-106.856	1	-216.477	3	-132.31	1	-.012	3	.006	12	-.585	2
119		3	max	57.8	5	262.675	2	-5.107	12	.01	2	.092	5	.457	3
120			min	-106.856	1	-122.95	3	-92.421	1	-.012	3	-.041	1	-.965	2
121		4	max	46.965	5	68.106	2	-3.222	12	.01	2	.051	5	.537	3
122			min	-106.856	1	-29.424	3	-52.531	1	-.012	3	-.117	1	-1.14	2
123		5	max	36.129	5	64.103	3	-1.112	10	.01	2	.013	5	.519	3
124			min	-106.856	1	-126.464	2	-38.138	4	-.012	3	-.151	1	-1.109	2
125		6	max	25.294	5	157.629	3	27.249	1	.01	2	-.007	12	.402	3
126			min	-106.856	1	-321.033	2	-31.692	5	-.012	3	-.144	1	-.873	2
127		7	max	14.458	5	251.156	3	67.139	1	.01	2	-.006	12	.186	3
128			min	-106.856	1	-515.603	2	-28.775	5	-.012	3	-.094	1	-.431	2
129		8	max	3.623	5	344.682	3	107.029	1	.01	2	.001	2	.216	2
130			min	-106.856	1	-710.172	2	-25.858	5	-.012	3	-.085	4	-.128	3
131		9	max	-4.694	15	438.209	3	146.919	1	.01	2	.132	1	1.068	2
132			min	-106.856	1	-904.742	2	-22.941	5	-.012	3	-.109	5	-.541	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-6.607	12	1099.311	2	-8.091	12	.012	3	.308	1	2.126	2
134			min	-106.856	1	-531.735	3	-186.809	1	-.01	2	.011	12	-1.053	3
135		11	max	-5.539	15	904.742	2	-6.206	12	.012	3	.16	4	1.068	2
136			min	-106.856	1	-438.209	3	-146.919	1	-.01	2	.003	12	-.541	3
137		12	max	-6.607	12	710.172	2	-4.32	12	.012	3	.083	4	.216	2
138			min	-106.856	1	-344.682	3	-107.029	1	-.01	2	-.003	3	-.128	3
139		13	max	-6.607	12	515.603	2	-2.435	12	.012	3	.04	5	.186	3
140			min	-106.856	1	-251.156	3	-67.139	1	-.01	2	-.094	1	-.431	2
141		14	max	-6.607	12	321.033	2	-.549	12	.012	3	.001	5	.402	3
142			min	-106.856	1	-157.629	3	-42.325	4	-.01	2	-.144	1	-.873	2
143		15	max	-6.607	12	126.464	2	12.641	1	.012	3	-.007	12	.519	3
144			min	-106.856	1	-64.103	3	-32.696	5	-.01	2	-.151	1	-1.109	2
145		16	max	-6.607	12	29.424	3	52.531	1	.012	3	-.005	12	.537	3
146			min	-106.856	1	-68.106	2	-29.779	5	-.01	2	-.117	1	-1.14	2
147		17	max	-6.607	12	122.95	3	92.421	1	.012	3	0	3	.457	3
148			min	-106.856	1	-262.675	2	-26.862	5	-.01	2	-.108	4	-.965	2
149		18	max	-6.607	12	216.477	3	132.31	1	.012	3	.078	1	.278	3
150			min	-110.391	4	-457.245	2	-23.944	5	-.01	2	-.124	5	-.585	2
151		19	max	-6.607	12	310.003	3	172.2	1	.012	3	.239	1	0	2
152			min	-121.226	4	-651.815	2	-21.027	5	-.01	2	-.148	5	0	5
153	M2	1	max	1050.384	2	1.959	4	.459	1	0	3	0	3	0	1
154			min	-1434.999	3	.474	15	-30.709	4	0	4	0	2	0	1
155		2	max	1050.86	2	1.873	4	.459	1	0	3	0	1	0	15
156			min	-1434.642	3	.454	15	-31.126	4	0	4	-.01	4	0	4
157		3	max	1051.335	2	1.788	4	.459	1	0	3	0	1	0	15
158			min	-1434.285	3	.433	15	-31.542	4	0	4	-.02	4	-.001	4
159		4	max	1051.811	2	1.702	4	.459	1	0	3	0	1	0	15
160			min	-1433.929	3	.413	15	-31.958	4	0	4	-.03	4	-.002	4
161		5	max	1052.287	2	1.617	4	.459	1	0	3	0	1	0	15
162			min	-1433.572	3	.393	15	-32.375	4	0	4	-.041	4	-.002	4
163		6	max	1052.763	2	1.531	4	.459	1	0	3	0	1	0	15
164			min	-1433.215	3	.373	15	-32.791	4	0	4	-.051	4	-.003	4
165		7	max	1053.238	2	1.445	4	.459	1	0	3	0	1	0	15
166			min	-1432.858	3	.35	12	-33.207	4	0	4	-.062	4	-.003	4
167		8	max	1053.714	2	1.36	4	.459	1	0	3	.001	1	0	15
168			min	-1432.501	3	.317	12	-33.624	4	0	4	-.073	4	-.004	4
169		9	max	1054.19	2	1.274	4	.459	1	0	3	.001	1	-.001	15
170			min	-1432.145	3	.283	12	-34.04	4	0	4	-.084	4	-.004	4
171		10	max	1054.666	2	1.189	4	.459	1	0	3	.001	1	-.001	15
172			min	-1431.788	3	.25	12	-34.457	4	0	4	-.095	4	-.005	4
173		11	max	1055.141	2	1.103	4	.459	1	0	3	.001	1	-.001	15
174			min	-1431.431	3	.217	12	-34.873	4	0	4	-.106	4	-.005	4
175		12	max	1055.617	2	1.018	4	.459	1	0	3	.002	1	-.001	15
176			min	-1431.074	3	.183	12	-35.289	4	0	4	-.118	4	-.005	4
177		13	max	1056.093	2	.941	2	.459	1	0	3	.002	1	-.001	12
178			min	-1430.717	3	.15	12	-35.706	4	0	4	-.129	4	-.006	4
179		14	max	1056.569	2	.874	2	.459	1	0	3	.002	1	-.001	12
180			min	-1430.361	3	.117	12	-36.122	4	0	4	-.141	4	-.006	4
181		15	max	1057.044	2	.807	2	.459	1	0	3	.002	1	-.001	12
182			min	-1430.004	3	.083	12	-36.538	4	0	4	-.152	4	-.006	4
183		16	max	1057.52	2	.741	2	.459	1	0	3	.002	1	-.001	12
184			min	-1429.647	3	.05	12	-36.955	4	0	4	-.164	4	-.006	4
185		17	max	1057.996	2	.674	2	.459	1	0	3	.002	1	-.001	12
186			min	-1429.29	3	.004	3	-37.371	4	0	4	-.176	4	-.007	4
187		18	max	1058.472	2	.607	2	.459	1	0	3	.003	1	-.001	12
188			min	-1428.933	3	-.046	3	-37.787	4	0	4	-.189	4	-.007	4
189		19	max	1058.947	2	.54	2	.459	1	0	3	.003	1	-.001	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-1428.576	3	-.096	3	-38.204	4	0	4	-.201	4	-.007	4
191	M3	1	max	755.98	2	7.802	4	5.226	4	0	12	0	1	.007	4
192			min	-894.538	3	1.844	15	.014	12	0	4	-.029	4	.001	12
193		2	max	755.81	2	7.037	4	5.763	4	0	12	0	1	.004	2
194			min	-894.665	3	1.664	15	.014	12	0	4	-.027	4	0	12
195		3	max	755.639	2	6.273	4	6.3	4	0	12	0	1	.002	2
196			min	-894.793	3	1.485	15	.014	12	0	4	-.024	4	-.001	3
197		4	max	755.469	2	5.508	4	6.837	4	0	12	0	1	0	2
198			min	-894.921	3	1.305	15	.014	12	0	4	-.021	4	-.002	3
199		5	max	755.299	2	4.744	4	7.374	4	0	12	0	1	0	15
200			min	-895.049	3	1.125	15	.014	12	0	4	-.018	4	-.004	3
201		6	max	755.128	2	3.979	4	7.911	4	0	12	0	1	-.001	15
202			min	-895.176	3	.946	15	.014	12	0	4	-.015	5	-.005	6
203		7	max	754.958	2	3.215	4	8.448	4	0	12	0	1	-.002	15
204			min	-895.304	3	.766	15	.014	12	0	4	-.012	5	-.007	6
205		8	max	754.787	2	2.451	4	8.985	4	0	12	.001	1	-.002	15
206			min	-895.432	3	.586	15	.014	12	0	4	-.008	5	-.008	6
207		9	max	754.617	2	1.686	4	9.522	4	0	12	.001	1	-.002	15
208			min	-895.56	3	.407	15	.014	12	0	4	-.005	5	-.009	6
209		10	max	754.447	2	.922	4	10.059	4	0	12	.001	1	-.002	15
210			min	-895.687	3	.194	12	.014	12	0	4	0	5	-.009	6
211		11	max	754.276	2	.289	2	10.596	4	0	12	.004	4	-.002	15
212			min	-895.815	3	-.172	3	.014	12	0	4	0	12	-.01	6
213		12	max	754.106	2	-.133	15	11.133	4	0	12	.009	4	-.002	15
214			min	-895.943	3	-.619	3	.014	12	0	4	0	12	-.01	6
215		13	max	753.936	2	-.312	15	11.67	4	0	12	.013	4	-.002	15
216			min	-896.071	3	-1.372	6	.014	12	0	4	0	12	-.009	6
217		14	max	753.765	2	-.492	15	12.207	4	0	12	.018	4	-.002	15
218			min	-896.199	3	-2.137	6	.014	12	0	4	0	12	-.008	6
219		15	max	753.595	2	-.672	15	12.744	4	0	12	.024	4	-.002	15
220			min	-896.326	3	-2.901	6	.014	12	0	4	0	12	-.007	6
221		16	max	753.425	2	-.851	15	13.28	4	0	12	.029	4	-.001	15
222			min	-896.454	3	-3.666	6	.014	12	0	4	0	12	-.006	6
223		17	max	753.254	2	-1.031	15	13.817	4	0	12	.035	4	-.001	15
224			min	-896.582	3	-4.43	6	.014	12	0	4	0	12	-.004	6
225		18	max	753.084	2	-1.211	15	14.354	4	0	12	.041	4	0	15
226			min	-896.71	3	-5.195	6	.014	12	0	4	0	12	-.002	6
227		19	max	752.914	2	-1.39	15	14.891	4	0	12	.047	4	0	1
228			min	-896.837	3	-5.959	6	.014	12	0	4	0	12	0	1
229	M4	1	max	1018.745	1	0	1	-.649	12	0	1	.039	4	0	1
230			min	-40.909	5	0	1	-276.753	4	0	1	0	12	0	1
231		2	max	1018.915	1	0	1	-.649	12	0	1	.007	4	0	1
232			min	-40.83	5	0	1	-276.9	4	0	1	0	12	0	1
233		3	max	1019.085	1	0	1	-.649	12	0	1	0	12	0	1
234			min	-40.75	5	0	1	-277.048	4	0	1	-.025	4	0	1
235		4	max	1019.256	1	0	1	-.649	12	0	1	0	12	0	1
236			min	-40.671	5	0	1	-277.196	4	0	1	-.057	4	0	1
237		5	max	1019.426	1	0	1	-.649	12	0	1	0	12	0	1
238			min	-40.591	5	0	1	-277.343	4	0	1	-.089	4	0	1
239		6	max	1019.597	1	0	1	-.649	12	0	1	0	12	0	1
240			min	-40.512	5	0	1	-277.491	4	0	1	-.12	4	0	1
241		7	max	1019.767	1	0	1	-.649	12	0	1	0	12	0	1
242			min	-40.432	5	0	1	-277.639	4	0	1	-.152	4	0	1
243		8	max	1019.937	1	0	1	-.649	12	0	1	0	12	0	1
244			min	-40.353	5	0	1	-277.786	4	0	1	-.184	4	0	1
245		9	max	1020.108	1	0	1	-.649	12	0	1	0	12	0	1
246			min	-40.273	5	0	1	-277.934	4	0	1	-.216	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	1020.278	1	0	1	-.649	12	0	1	0	12	0	1
248			min	-40.194	5	0	1	-278.082	4	0	1	-.248	4	0	1
249		11	max	1020.448	1	0	1	-.649	12	0	1	0	12	0	1
250			min	-40.114	5	0	1	-278.229	4	0	1	-.28	4	0	1
251		12	max	1020.619	1	0	1	-.649	12	0	1	0	12	0	1
252			min	-40.035	5	0	1	-278.377	4	0	1	-.312	4	0	1
253		13	max	1020.789	1	0	1	-.649	12	0	1	0	12	0	1
254			min	-39.955	5	0	1	-278.524	4	0	1	-.344	4	0	1
255		14	max	1020.959	1	0	1	-.649	12	0	1	0	12	0	1
256			min	-39.876	5	0	1	-278.672	4	0	1	-.376	4	0	1
257		15	max	1021.13	1	0	1	-.649	12	0	1	0	12	0	1
258			min	-39.796	5	0	1	-278.82	4	0	1	-.408	4	0	1
259		16	max	1021.3	1	0	1	-.649	12	0	1	-.001	12	0	1
260			min	-39.717	5	0	1	-278.967	4	0	1	-.44	4	0	1
261		17	max	1021.47	1	0	1	-.649	12	0	1	-.001	12	0	1
262			min	-39.637	5	0	1	-279.115	4	0	1	-.472	4	0	1
263		18	max	1021.641	1	0	1	-.649	12	0	1	-.001	12	0	1
264			min	-39.558	5	0	1	-279.263	4	0	1	-.504	4	0	1
265		19	max	1021.811	1	0	1	-.649	12	0	1	-.001	12	0	1
266			min	-39.478	5	0	1	-279.41	4	0	1	-.536	4	0	1
267	M6	1	max	3358.757	2	2.327	2	0	1	0	1	0	4	0	1
268			min	-4668.302	3	.094	3	-31.035	4	0	4	0	1	0	1
269		2	max	3359.233	2	2.26	2	0	1	0	1	0	1	0	3
270			min	-4667.946	3	.043	3	-31.451	4	0	4	-.01	4	0	2
271		3	max	3359.709	2	2.194	2	0	1	0	1	0	1	0	3
272			min	-4667.589	3	-.007	3	-31.867	4	0	4	-.02	4	-.001	2
273		4	max	3360.185	2	2.127	2	0	1	0	1	0	1	0	3
274			min	-4667.232	3	-.057	3	-32.284	4	0	4	-.031	4	-.002	2
275		5	max	3360.66	2	2.06	2	0	1	0	1	0	1	0	3
276			min	-4666.875	3	-.107	3	-32.7	4	0	4	-.041	4	-.003	2
277		6	max	3361.136	2	1.994	2	0	1	0	1	0	1	0	3
278			min	-4666.518	3	-.157	3	-33.116	4	0	4	-.052	4	-.003	2
279		7	max	3361.612	2	1.927	2	0	1	0	1	0	1	0	3
280			min	-4666.162	3	-.207	3	-33.533	4	0	4	-.063	4	-.004	2
281		8	max	3362.088	2	1.86	2	0	1	0	1	0	1	0	3
282			min	-4665.805	3	-.257	3	-33.949	4	0	4	-.074	4	-.005	2
283		9	max	3362.563	2	1.794	2	0	1	0	1	0	1	0	3
284			min	-4665.448	3	-.307	3	-34.365	4	0	4	-.085	4	-.005	2
285		10	max	3363.039	2	1.727	2	0	1	0	1	0	1	0	3
286			min	-4665.091	3	-.357	3	-34.782	4	0	4	-.096	4	-.006	2
287		11	max	3363.515	2	1.66	2	0	1	0	1	0	1	0	3
288			min	-4664.734	3	-.407	3	-35.198	4	0	4	-.107	4	-.006	2
289		12	max	3363.991	2	1.594	2	0	1	0	1	0	1	0	3
290			min	-4664.378	3	-.457	3	-35.615	4	0	4	-.119	4	-.007	2
291		13	max	3364.466	2	1.527	2	0	1	0	1	0	1	0	3
292			min	-4664.021	3	-.507	3	-36.031	4	0	4	-.13	4	-.007	2
293		14	max	3364.942	2	1.46	2	0	1	0	1	0	1	0	3
294			min	-4663.664	3	-.557	3	-36.447	4	0	4	-.142	4	-.008	2
295		15	max	3365.418	2	1.393	2	0	1	0	1	0	1	.001	3
296			min	-4663.307	3	-.607	3	-36.864	4	0	4	-.154	4	-.008	2
297		16	max	3365.894	2	1.327	2	0	1	0	1	0	1	.001	3
298			min	-4662.95	3	-.657	3	-37.28	4	0	4	-.166	4	-.009	2
299		17	max	3366.369	2	1.26	2	0	1	0	1	0	1	.002	3
300			min	-4662.593	3	-.707	3	-37.696	4	0	4	-.178	4	-.009	2
301		18	max	3366.845	2	1.193	2	0	1	0	1	0	1	.002	3
302			min	-4662.237	3	-.757	3	-38.113	4	0	4	-.19	4	-.01	2
303		19	max	3367.321	2	1.127	2	0	1	0	1	0	1	.002	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-4661.88	3	-.807	3	-38.529	4	0	4	-.203	4	-.01	2
305	M7	1	max	2729.549	2	7.809	6	4.932	4	0	1	0	1	.01	2
306			min	-2812.256	3	1.834	15	0	1	0	4	-.029	4	-.002	3
307		2	max	2729.378	2	7.045	6	5.469	4	0	1	0	1	.007	2
308			min	-2812.383	3	1.654	15	0	1	0	4	-.027	4	-.004	3
309		3	max	2729.208	2	6.28	6	6.006	4	0	1	0	1	.005	2
310			min	-2812.511	3	1.474	15	0	1	0	4	-.025	4	-.005	3
311		4	max	2729.037	2	5.516	6	6.543	4	0	1	0	1	.003	2
312			min	-2812.639	3	1.294	15	0	1	0	4	-.022	4	-.006	3
313		5	max	2728.867	2	4.751	6	7.079	4	0	1	0	1	0	2
314			min	-2812.767	3	1.115	15	0	1	0	4	-.019	4	-.007	3
315		6	max	2728.697	2	3.987	6	7.616	4	0	1	0	1	0	2
316			min	-2812.894	3	.935	15	0	1	0	4	-.016	4	-.008	3
317		7	max	2728.526	2	3.222	6	8.153	4	0	1	0	1	-.002	15
318			min	-2813.022	3	.743	12	0	1	0	4	-.013	4	-.008	3
319		8	max	2728.356	2	2.53	2	8.69	4	0	1	0	1	-.002	15
320			min	-2813.15	3	.445	12	0	1	0	4	-.009	4	-.008	3
321		9	max	2728.186	2	1.935	2	9.227	4	0	1	0	1	-.002	15
322			min	-2813.278	3	.147	12	0	1	0	4	-.006	4	-.009	4
323		10	max	2728.015	2	1.339	2	9.764	4	0	1	0	1	-.002	15
324			min	-2813.406	3	-.277	3	0	1	0	4	-.002	5	-.009	4
325		11	max	2727.845	2	.743	2	10.301	4	0	1	.003	4	-.002	15
326			min	-2813.533	3	-.723	3	0	1	0	4	0	1	-.01	4
327		12	max	2727.675	2	.148	2	10.838	4	0	1	.007	4	-.002	15
328			min	-2813.661	3	-1.17	3	0	1	0	4	0	1	-.01	4
329		13	max	2727.504	2	-.323	15	11.375	4	0	1	.012	4	-.002	15
330			min	-2813.789	3	-1.617	3	0	1	0	4	0	1	-.009	4
331		14	max	2727.334	2	-.502	15	11.912	4	0	1	.016	4	-.002	15
332			min	-2813.917	3	-2.129	4	0	1	0	4	0	1	-.008	4
333		15	max	2727.164	2	-.682	15	12.449	4	0	1	.022	4	-.002	15
334			min	-2814.044	3	-2.893	4	0	1	0	4	0	1	-.007	4
335		16	max	2726.993	2	-.862	15	12.986	4	0	1	.027	4	-.001	15
336			min	-2814.172	3	-3.658	4	0	1	0	4	0	1	-.006	4
337		17	max	2726.823	2	-1.042	15	13.523	4	0	1	.032	4	-.001	15
338			min	-2814.3	3	-4.422	4	0	1	0	4	0	1	-.004	4
339		18	max	2726.653	2	-1.221	15	14.06	4	0	1	.038	4	0	15
340			min	-2814.428	3	-5.186	4	0	1	0	4	0	1	-.002	4
341		19	max	2726.482	2	-1.401	15	14.597	4	0	1	.044	4	0	1
342			min	-2814.555	3	-5.951	4	0	1	0	4	0	1	0	1
343	M8	1	max	2662.379	1	0	1	0	1	0	1	.037	4	0	1
344			min	-207.656	3	0	1	-267.322	4	0	1	0	1	0	1
345		2	max	2662.549	1	0	1	0	1	0	1	.006	4	0	1
346			min	-207.529	3	0	1	-267.469	4	0	1	0	1	0	1
347		3	max	2662.719	1	0	1	0	1	0	1	0	1	0	1
348			min	-207.401	3	0	1	-267.617	4	0	1	-.025	4	0	1
349		4	max	2662.89	1	0	1	0	1	0	1	0	1	0	1
350			min	-207.273	3	0	1	-267.765	4	0	1	-.056	4	0	1
351		5	max	2663.06	1	0	1	0	1	0	1	0	1	0	1
352			min	-207.145	3	0	1	-267.912	4	0	1	-.086	4	0	1
353		6	max	2663.23	1	0	1	0	1	0	1	0	1	0	1
354			min	-207.017	3	0	1	-268.06	4	0	1	-.117	4	0	1
355		7	max	2663.401	1	0	1	0	1	0	1	0	1	0	1
356			min	-206.89	3	0	1	-268.207	4	0	1	-.148	4	0	1
357		8	max	2663.571	1	0	1	0	1	0	1	0	1	0	1
358			min	-206.762	3	0	1	-268.355	4	0	1	-.179	4	0	1
359		9	max	2663.741	1	0	1	0	1	0	1	0	1	0	1
360			min	-206.634	3	0	1	-268.503	4	0	1	-.209	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	2663.912	1	0	1	0	1	0	1	0	1	0	1
362			min	-206.506	3	0	1	-268.65	4	0	1	-.24	4	0	1
363		11	max	2664.082	1	0	1	0	1	0	1	0	1	0	1
364			min	-206.379	3	0	1	-268.798	4	0	1	-.271	4	0	1
365		12	max	2664.252	1	0	1	0	1	0	1	0	1	0	1
366			min	-206.251	3	0	1	-268.946	4	0	1	-.302	4	0	1
367		13	max	2664.423	1	0	1	0	1	0	1	0	1	0	1
368			min	-206.123	3	0	1	-269.093	4	0	1	-.333	4	0	1
369		14	max	2664.593	1	0	1	0	1	0	1	0	1	0	1
370			min	-205.995	3	0	1	-269.241	4	0	1	-.364	4	0	1
371		15	max	2664.764	1	0	1	0	1	0	1	0	1	0	1
372			min	-205.868	3	0	1	-269.389	4	0	1	-.395	4	0	1
373		16	max	2664.934	1	0	1	0	1	0	1	0	1	0	1
374			min	-205.74	3	0	1	-269.536	4	0	1	-.426	4	0	1
375		17	max	2665.104	1	0	1	0	1	0	1	0	1	0	1
376			min	-205.612	3	0	1	-269.684	4	0	1	-.457	4	0	1
377		18	max	2665.275	1	0	1	0	1	0	1	0	1	0	1
378			min	-205.484	3	0	1	-269.831	4	0	1	-.488	4	0	1
379		19	max	2665.445	1	0	1	0	1	0	1	0	1	0	1
380			min	-205.357	3	0	1	-269.979	4	0	1	-.519	4	0	1
381	M10	1	max	1050.384	2	1.901	6	-.027	12	0	1	0	2	0	1
382			min	-1434.999	3	.434	15	-30.993	4	0	5	0	3	0	1
383		2	max	1050.86	2	1.815	6	-.027	12	0	1	0	10	0	15
384			min	-1434.642	3	.414	15	-31.41	4	0	5	-.01	4	0	6
385		3	max	1051.335	2	1.73	6	-.027	12	0	1	0	10	0	15
386			min	-1434.285	3	.394	15	-31.826	4	0	5	-.02	4	-.001	6
387		4	max	1051.811	2	1.644	6	-.027	12	0	1	0	12	0	15
388			min	-1433.929	3	.374	15	-32.242	4	0	5	-.031	4	-.002	6
389		5	max	1052.287	2	1.559	6	-.027	12	0	1	0	12	0	15
390			min	-1433.572	3	.354	15	-32.659	4	0	5	-.041	4	-.002	6
391		6	max	1052.763	2	1.473	6	-.027	12	0	1	0	12	0	15
392			min	-1433.215	3	.334	15	-33.075	4	0	5	-.052	4	-.003	6
393		7	max	1053.238	2	1.387	6	-.027	12	0	1	0	12	0	15
394			min	-1432.858	3	.314	15	-33.491	4	0	5	-.063	4	-.003	6
395		8	max	1053.714	2	1.302	6	-.027	12	0	1	0	12	0	15
396			min	-1432.501	3	.294	15	-33.908	4	0	5	-.074	4	-.004	6
397		9	max	1054.19	2	1.216	6	-.027	12	0	1	0	12	0	15
398			min	-1432.145	3	.273	15	-34.324	4	0	5	-.085	4	-.004	6
399		10	max	1054.666	2	1.141	2	-.027	12	0	1	0	12	-.001	15
400			min	-1431.788	3	.25	12	-34.74	4	0	5	-.096	4	-.004	6
401		11	max	1055.141	2	1.074	2	-.027	12	0	1	0	12	-.001	15
402			min	-1431.431	3	.217	12	-35.157	4	0	5	-.107	4	-.005	6
403		12	max	1055.617	2	1.007	2	-.027	12	0	1	0	12	-.001	15
404			min	-1431.074	3	.183	12	-35.573	4	0	5	-.119	4	-.005	6
405		13	max	1056.093	2	.941	2	-.027	12	0	1	0	12	-.001	15
406			min	-1430.717	3	.15	12	-35.989	4	0	5	-.13	4	-.005	6
407		14	max	1056.569	2	.874	2	-.027	12	0	1	0	12	-.001	15
408			min	-1430.361	3	.117	12	-36.406	4	0	5	-.142	4	-.006	6
409		15	max	1057.044	2	.807	2	-.027	12	0	1	0	12	-.001	15
410			min	-1430.004	3	.083	12	-36.822	4	0	5	-.154	4	-.006	6
411		16	max	1057.52	2	.741	2	-.027	12	0	1	0	12	-.001	15
412			min	-1429.647	3	.05	12	-37.238	4	0	5	-.166	4	-.006	6
413		17	max	1057.996	2	.674	2	-.027	12	0	1	0	12	-.001	15
414			min	-1429.29	3	.004	3	-37.655	4	0	5	-.178	4	-.006	6
415		18	max	1058.472	2	.607	2	-.027	12	0	1	0	12	-.001	15
416			min	-1428.933	3	-.046	3	-38.071	4	0	5	-.19	4	-.006	2
417		19	max	1058.947	2	.54	2	-.027	12	0	1	0	12	-.001	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-1428.576	3	-.096	3	-38.488	4	0	5	-.202	4	-.007	2
419	M11	1	max	755.98	2	7.757	6	5.085	4	0	1	0	12	.007	2
420			min	-894.538	3	1.814	15	-.228	1	0	4	-.029	4	.001	12
421		2	max	755.81	2	6.992	6	5.622	4	0	1	0	12	.004	2
422			min	-894.665	3	1.634	15	-.228	1	0	4	-.027	4	0	12
423		3	max	755.639	2	6.228	6	6.159	4	0	1	0	12	.002	2
424			min	-894.793	3	1.454	15	-.228	1	0	4	-.025	4	-.001	3
425		4	max	755.469	2	5.463	6	6.696	4	0	1	0	12	0	2
426			min	-894.921	3	1.275	15	-.228	1	0	4	-.022	4	-.002	3
427		5	max	755.299	2	4.699	6	7.233	4	0	1	0	12	0	15
428			min	-895.049	3	1.095	15	-.228	1	0	4	-.019	4	-.004	4
429		6	max	755.128	2	3.934	6	7.77	4	0	1	0	12	-.001	15
430			min	-895.176	3	.915	15	-.228	1	0	4	-.016	4	-.006	4
431		7	max	754.958	2	3.17	6	8.307	4	0	1	0	12	-.002	15
432			min	-895.304	3	.736	15	-.228	1	0	4	-.012	4	-.007	4
433		8	max	754.787	2	2.406	6	8.844	4	0	1	0	12	-.002	15
434			min	-895.432	3	.556	15	-.228	1	0	4	-.009	4	-.008	4
435		9	max	754.617	2	1.641	6	9.381	4	0	1	0	12	-.002	15
436			min	-895.56	3	.376	15	-.228	1	0	4	-.005	4	-.009	4
437		10	max	754.447	2	.885	2	9.918	4	0	1	0	12	-.002	15
438			min	-895.687	3	.194	12	-.228	1	0	4	-.001	1	-.01	4
439		11	max	754.276	2	.289	2	10.455	4	0	1	.003	5	-.002	15
440			min	-895.815	3	-.172	3	-.228	1	0	4	-.001	1	-.01	4
441		12	max	754.106	2	-.163	15	10.992	4	0	1	.008	5	-.002	15
442			min	-895.943	3	-.653	4	-.228	1	0	4	-.001	1	-.01	4
443		13	max	753.936	2	-.343	15	11.529	4	0	1	.013	5	-.002	15
444			min	-896.071	3	-1.418	4	-.228	1	0	4	-.002	1	-.009	4
445		14	max	753.765	2	-.522	15	12.066	4	0	1	.017	5	-.002	15
446			min	-896.199	3	-2.182	4	-.228	1	0	4	-.002	1	-.009	4
447		15	max	753.595	2	-.702	15	12.603	4	0	1	.023	5	-.002	15
448			min	-896.326	3	-2.946	4	-.228	1	0	4	-.002	1	-.007	4
449		16	max	753.425	2	-.882	15	13.14	4	0	1	.028	5	-.001	15
450			min	-896.454	3	-3.711	4	-.228	1	0	4	-.002	1	-.006	4
451		17	max	753.254	2	-1.061	15	13.677	4	0	1	.033	5	-.001	15
452			min	-896.582	3	-4.475	4	-.228	1	0	4	-.002	1	-.004	4
453		18	max	753.084	2	-1.241	15	14.213	4	0	1	.039	4	0	15
454			min	-896.71	3	-5.24	4	-.228	1	0	4	-.002	1	-.002	4
455		19	max	752.914	2	-1.421	15	14.75	4	0	1	.045	4	0	1
456			min	-896.837	3	-6.004	4	-.228	1	0	4	-.002	1	0	1
457	M12	1	max	1018.745	1	0	1	10.645	1	0	1	.038	4	0	1
458			min	-34.333	3	0	1	-270.156	4	0	1	-.002	1	0	1
459		2	max	1018.915	1	0	1	10.645	1	0	1	.007	5	0	1
460			min	-34.205	3	0	1	-270.303	4	0	1	0	1	0	1
461		3	max	1019.085	1	0	1	10.645	1	0	1	0	1	0	1
462			min	-34.077	3	0	1	-270.451	4	0	1	-.024	4	0	1
463		4	max	1019.256	1	0	1	10.645	1	0	1	.002	1	0	1
464			min	-33.95	3	0	1	-270.599	4	0	1	-.056	4	0	1
465		5	max	1019.426	1	0	1	10.645	1	0	1	.003	1	0	1
466			min	-33.822	3	0	1	-270.746	4	0	1	-.087	4	0	1
467		6	max	1019.597	1	0	1	10.645	1	0	1	.004	1	0	1
468			min	-33.694	3	0	1	-270.894	4	0	1	-.118	4	0	1
469		7	max	1019.767	1	0	1	10.645	1	0	1	.006	1	0	1
470			min	-33.566	3	0	1	-271.041	4	0	1	-.149	4	0	1
471		8	max	1019.937	1	0	1	10.645	1	0	1	.007	1	0	1
472			min	-33.439	3	0	1	-271.189	4	0	1	-.18	4	0	1
473		9	max	1020.108	1	0	1	10.645	1	0	1	.008	1	0	1
474			min	-33.311	3	0	1	-271.337	4	0	1	-.211	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	1020.278	1	0	1	10.645	1	0	1	.009	1	0	1
476			min	-33.183	3	0	1	-271.484	4	0	1	-.242	4	0	1
477		11	max	1020.448	1	0	1	10.645	1	0	1	.01	1	0	1
478			min	-33.055	3	0	1	-271.632	4	0	1	-.273	4	0	1
479		12	max	1020.619	1	0	1	10.645	1	0	1	.012	1	0	1
480			min	-32.927	3	0	1	-271.78	4	0	1	-.305	4	0	1
481		13	max	1020.789	1	0	1	10.645	1	0	1	.013	1	0	1
482			min	-32.8	3	0	1	-271.927	4	0	1	-.336	4	0	1
483		14	max	1020.959	1	0	1	10.645	1	0	1	.014	1	0	1
484			min	-32.672	3	0	1	-272.075	4	0	1	-.367	4	0	1
485		15	max	1021.13	1	0	1	10.645	1	0	1	.015	1	0	1
486			min	-32.544	3	0	1	-272.223	4	0	1	-.398	4	0	1
487		16	max	1021.3	1	0	1	10.645	1	0	1	.017	1	0	1
488			min	-32.416	3	0	1	-272.37	4	0	1	-.43	4	0	1
489		17	max	1021.47	1	0	1	10.645	1	0	1	.018	1	0	1
490			min	-32.289	3	0	1	-272.518	4	0	1	-.461	4	0	1
491		18	max	1021.641	1	0	1	10.645	1	0	1	.019	1	0	1
492			min	-32.161	3	0	1	-272.665	4	0	1	-.492	4	0	1
493		19	max	1021.811	1	0	1	10.645	1	0	1	.02	1	0	1
494			min	-32.033	3	0	1	-272.813	4	0	1	-.524	4	0	1
495	M1	1	max	171.919	1	768.918	3	43.421	5	0	2	.237	1	0	3
496			min	-10.77	5	-438.476	2	-99.237	1	0	3	-.098	5	-.015	2
497		2	max	172.635	1	767.988	3	44.662	5	0	2	.185	1	.217	2
498			min	-10.436	5	-439.716	2	-99.237	1	0	3	-.075	5	-.405	3
499		3	max	553.386	3	529.401	2	15.889	5	0	3	.132	1	.438	2
500			min	-319.6	2	-566.838	3	-98.959	1	0	2	-.051	5	-.794	3
501		4	max	553.923	3	528.161	2	17.131	5	0	3	.08	1	.159	2
502			min	-318.883	2	-567.768	3	-98.959	1	0	2	-.042	5	-.494	3
503		5	max	554.46	3	526.92	2	18.372	5	0	3	.028	1	-.003	15
504			min	-318.167	2	-568.699	3	-98.959	1	0	2	-.033	5	-.194	3
505		6	max	554.998	3	525.68	2	19.614	5	0	3	-.002	12	.106	3
506			min	-317.451	2	-569.629	3	-98.959	1	0	2	-.029	4	-.397	2
507		7	max	555.535	3	524.439	2	20.855	5	0	3	-.005	12	.407	3
508			min	-316.735	2	-570.56	3	-98.959	1	0	2	-.076	1	-.674	2
509		8	max	556.072	3	523.199	2	22.096	5	0	3	0	15	.708	3
510			min	-316.018	2	-571.49	3	-98.959	1	0	2	-.129	1	-.951	2
511		9	max	570.797	3	52.947	2	58.904	5	0	9	.076	1	.826	3
512			min	-241.689	2	.375	15	-146.563	1	0	3	-.128	5	-1.089	2
513		10	max	571.334	3	51.706	2	60.145	5	0	9	0	10	.805	3
514			min	-240.972	2	0	5	-146.563	1	0	3	-.098	4	-1.117	2
515		11	max	571.871	3	50.466	2	61.386	5	0	9	-.005	12	.785	3
516			min	-240.256	2	-1.542	4	-146.563	1	0	3	-.083	4	-1.144	2
517		12	max	586.472	3	377.824	3	151.622	5	0	2	.127	1	.685	3
518			min	-165.884	2	-633.014	2	-96.801	1	0	3	-.212	5	-1.014	2
519		13	max	587.009	3	376.893	3	152.863	5	0	2	.076	1	.486	3
520			min	-165.168	2	-634.254	2	-96.801	1	0	3	-.132	5	-.68	2
521		14	max	587.546	3	375.963	3	154.105	5	0	2	.025	1	.287	3
522			min	-164.451	2	-635.495	2	-96.801	1	0	3	-.051	5	-.345	2
523		15	max	588.083	3	375.033	3	155.346	5	0	2	.031	5	.089	3
524			min	-163.735	2	-636.735	2	-96.801	1	0	3	-.026	1	-.03	1
525		16	max	588.621	3	374.102	3	156.588	5	0	2	.113	5	.327	2
526			min	-163.019	2	-637.976	2	-96.801	1	0	3	-.077	1	-.109	3
527		17	max	589.158	3	373.172	3	157.829	5	0	2	.196	5	.664	2
528			min	-162.303	2	-639.216	2	-96.801	1	0	3	-.128	1	-.306	3
529		18	max	20.692	5	653.617	2	-6.607	12	0	5	.199	5	.334	2
530			min	-172.911	1	-309.158	3	-122.56	4	0	2	-.182	1	-.151	3
531		19	max	21.027	5	652.377	2	-6.607	12	0	5	.148	5	.012	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-172.195	1	-310.089	3	-121.318	4	0	2	-.239	1	-.01	2
533	M5	1	max	374.181	1	2561.353	3	93.666	5	0	1	0	1	.029	2
534			min	15.658	12	-1492.776	2	0	1	0	4	-.217	4	-.002	3
535		2	max	374.897	1	2560.423	3	94.907	5	0	1	0	1	.817	2
536			min	16.016	12	-1494.016	2	0	1	0	4	-.167	4	-1.353	3
537		3	max	1771.97	3	1584.906	2	68.809	4	0	4	0	1	1.569	2
538			min	-1098.01	2	-1803.918	3	0	1	0	1	-.117	4	-2.651	3
539		4	max	1772.507	3	1583.665	2	70.051	4	0	4	0	1	.733	2
540			min	-1097.294	2	-1804.848	3	0	1	0	1	-.081	4	-1.699	3
541		5	max	1773.044	3	1582.425	2	71.292	4	0	4	0	1	.008	9
542			min	-1096.578	2	-1805.779	3	0	1	0	1	-.043	4	-.747	3
543		6	max	1773.582	3	1581.184	2	72.534	4	0	4	0	1	.206	3
544			min	-1095.862	2	-1806.709	3	0	1	0	1	-.006	5	-.937	2
545		7	max	1774.119	3	1579.944	2	73.775	4	0	4	.033	4	1.16	3
546			min	-1095.145	2	-1807.64	3	0	1	0	1	0	1	-1.771	2
547		8	max	1774.656	3	1578.703	2	75.016	4	0	4	.072	4	2.114	3
548			min	-1094.429	2	-1808.57	3	0	1	0	1	0	1	-2.605	2
549		9	max	1797.726	3	177.537	2	193.945	4	0	1	0	1	2.43	3
550			min	-939.202	2	.374	15	0	1	0	1	-.191	4	-2.97	2
551		10	max	1798.263	3	176.297	2	195.186	4	0	1	0	1	2.356	3
552			min	-938.485	2	0	15	0	1	0	1	-.089	4	-3.064	2
553		11	max	1798.8	3	175.056	2	196.428	4	0	1	.015	4	2.283	3
554			min	-937.769	2	-1.401	6	0	1	0	1	0	1	-3.156	2
555		12	max	1822.118	3	1187.088	3	221.781	4	0	1	0	1	2.006	3
556			min	-782.627	2	-1938.795	2	0	1	0	4	-.311	4	-2.828	2
557		13	max	1822.655	3	1186.158	3	223.022	4	0	1	0	1	1.38	3
558			min	-781.911	2	-1940.035	2	0	1	0	4	-.194	4	-1.805	2
559		14	max	1823.192	3	1185.228	3	224.264	4	0	1	0	1	.754	3
560			min	-781.195	2	-1941.276	2	0	1	0	4	-.076	4	-.78	2
561		15	max	1823.729	3	1184.297	3	225.505	4	0	1	.043	4	.244	2
562			min	-780.478	2	-1942.516	2	0	1	0	4	0	1	-.003	13
563		16	max	1824.266	3	1183.367	3	226.747	4	0	1	.162	4	1.27	2
564			min	-779.762	2	-1943.757	2	0	1	0	4	0	1	-.495	3
565		17	max	1824.803	3	1182.436	3	227.988	4	0	1	.282	4	2.295	2
566			min	-779.046	2	-1944.997	2	0	1	0	4	0	1	-1.12	3
567		18	max	-16.539	12	2202.903	2	0	1	0	4	.323	4	1.183	2
568			min	-374.346	1	-1063.01	3	-21.613	5	0	1	0	1	-.586	3
569		19	max	-16.181	12	2201.663	2	0	1	0	4	.312	4	.021	2
570			min	-373.63	1	-1063.94	3	-20.372	5	0	1	0	1	-.025	3
571	M9	1	max	171.919	1	768.918	3	99.237	1	0	3	-.016	12	0	3
572			min	9.14	12	-438.476	2	6.589	12	0	4	-.237	1	-.015	2
573		2	max	172.635	1	767.988	3	99.237	1	0	3	-.012	12	.217	2
574			min	9.499	12	-439.716	2	6.589	12	0	4	-.185	1	-.405	3
575		3	max	553.386	3	529.401	2	98.959	1	0	2	-.009	12	.438	2
576			min	-319.6	2	-566.838	3	6.561	12	0	3	-.132	1	-.794	3
577		4	max	553.923	3	528.161	2	98.959	1	0	2	-.005	12	.159	2
578			min	-318.883	2	-567.768	3	6.561	12	0	3	-.08	1	-.494	3
579		5	max	554.46	3	526.92	2	98.959	1	0	2	-.002	12	-.003	15
580			min	-318.167	2	-568.699	3	6.561	12	0	3	-.044	4	-.194	3
581		6	max	554.998	3	525.68	2	98.959	1	0	2	.024	1	.106	3
582			min	-317.451	2	-569.629	3	6.561	12	0	3	-.019	5	-.397	2
583		7	max	555.535	3	524.439	2	98.959	1	0	2	.076	1	.407	3
584			min	-316.735	2	-570.56	3	6.561	12	0	3	0	5	-.674	2
585		8	max	556.072	3	523.199	2	98.959	1	0	2	.129	1	.708	3
586			min	-316.018	2	-571.49	3	6.561	12	0	3	.008	12	-.951	2
587		9	max	570.797	3	52.947	2	146.563	1	0	3	-.005	12	.826	3
588			min	-241.689	2	.382	15	9.377	12	0	9	-.159	4	-1.089	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	571.334	3	51.706	2	146.563	1	0	3	0	1	.805	3
590			min	-240.972	2	.008	15	9.377	12	0	9	-.097	4	-1.117	2
591		11	max	571.871	3	50.466	2	146.563	1	0	3	.078	1	.785	3
592			min	-240.256	2	-1.491	6	9.377	12	0	9	-.053	5	-1.144	2
593		12	max	586.472	3	377.824	3	190.707	4	0	3	-.008	12	.685	3
594			min	-165.884	2	-633.014	2	5.974	12	0	2	-.263	4	-1.014	2
595		13	max	587.009	3	376.893	3	191.948	4	0	3	-.005	12	.486	3
596			min	-165.168	2	-634.254	2	5.974	12	0	2	-.162	4	-.68	2
597		14	max	587.546	3	375.963	3	193.19	4	0	3	-.002	12	.287	3
598			min	-164.451	2	-635.495	2	5.974	12	0	2	-.061	4	-.345	2
599		15	max	588.083	3	375.033	3	194.431	4	0	3	.042	4	.089	3
600			min	-163.735	2	-636.735	2	5.974	12	0	2	.002	12	-.03	1
601		16	max	588.621	3	374.102	3	195.672	4	0	3	.145	4	.327	2
602			min	-163.019	2	-637.976	2	5.974	12	0	2	.005	12	-.109	3
603		17	max	589.158	3	373.172	3	196.914	4	0	3	.248	4	.664	2
604			min	-162.303	2	-639.216	2	5.974	12	0	2	.008	12	-.306	3
605		18	max	-9.237	12	653.617	2	106.971	1	0	2	.271	4	.334	2
606			min	-172.911	1	-309.158	3	-80.916	5	0	3	.011	12	-.151	3
607		19	max	-8.879	12	652.377	2	106.971	1	0	2	.242	4	.012	3
608			min	-172.195	1	-310.089	3	-79.674	5	0	3	.015	12	-.01	2

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.113	2	.01	3	9.473e-3	2	NC	1	NC	1
2			min	-.641	4	-.021	3	-.005	2	-2.081e-3	3	NC	1	NC	1
3		2	max	0	1	.291	3	.034	1	1.082e-2	2	NC	5	NC	2
4			min	-.641	4	-.051	1	-.019	5	-2.164e-3	3	730.164	3	6809.588	1
5		3	max	0	1	.544	3	.082	1	1.217e-2	2	NC	5	NC	3
6			min	-.641	4	-.167	2	-.023	5	-2.247e-3	3	403.432	3	2806.772	1
7		4	max	0	1	.698	3	.123	1	1.352e-2	2	NC	5	NC	3
8			min	-.641	4	-.234	2	-.016	5	-2.33e-3	3	317.198	3	1865.304	1
9		5	max	0	1	.734	3	.143	1	1.487e-2	2	NC	5	NC	3
10			min	-.641	4	-.234	2	-.003	5	-2.413e-3	3	302.163	3	1595.019	1
11		6	max	0	1	.654	3	.138	1	1.622e-2	2	NC	5	NC	3
12			min	-.641	4	-.174	1	.007	15	-2.495e-3	3	337.74	3	1660.426	1
13		7	max	0	1	.483	3	.107	1	1.757e-2	2	NC	5	NC	5
14			min	-.641	4	-.071	1	.003	10	-2.578e-3	3	452.182	3	2135.562	1
15		8	max	0	1	.266	3	.061	1	1.892e-2	2	NC	4	NC	2
16			min	-.641	4	.001	15	-.004	10	-2.661e-3	3	794.05	3	3787.557	1
17		9	max	0	1	.202	2	.031	3	2.027e-2	2	NC	4	NC	1
18			min	-.641	4	.004	15	-.011	2	-2.744e-3	3	2527.422	3	8787.42	4
19		10	max	0	1	.257	2	.03	3	2.162e-2	2	NC	3	NC	1
20			min	-.641	4	-.02	3	-.021	2	-2.827e-3	3	1592.467	2	NC	1
21		11	max	0	12	.202	2	.031	3	2.027e-2	2	NC	4	NC	1
22			min	-.641	4	.004	15	-.016	5	-2.744e-3	3	2527.422	3	NC	1
23		12	max	0	12	.266	3	.061	1	1.892e-2	2	NC	4	NC	2
24			min	-.641	4	.001	15	-.015	5	-2.661e-3	3	794.05	3	3787.557	1
25		13	max	0	12	.483	3	.107	1	1.757e-2	2	NC	5	NC	4
26			min	-.641	4	-.071	1	-.005	5	-2.578e-3	3	452.182	3	2135.562	1
27		14	max	0	12	.654	3	.138	1	1.622e-2	2	NC	5	NC	3
28			min	-.641	4	-.174	1	.007	15	-2.495e-3	3	337.74	3	1660.426	1
29		15	max	0	12	.734	3	.143	1	1.487e-2	2	NC	5	NC	3
30			min	-.641	4	-.234	2	.011	10	-2.413e-3	3	302.163	3	1595.019	1
31		16	max	0	12	.698	3	.123	1	1.352e-2	2	NC	5	NC	3
32			min	-.641	4	-.234	2	.01	10	-2.33e-3	3	317.198	3	1865.304	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	12	.544	3	.082	1	1.217e-2	2	NC	5	NC	3
34			min	-.641	4	-.167	2	.005	10	-2.247e-3	3	403.432	3	2806.772	1
35		18	max	0	12	.291	3	.034	4	1.082e-2	2	NC	5	NC	2
36			min	-.642	4	-.051	1	0	10	-2.164e-3	3	730.164	3	6619.968	4
37		19	max	0	12	.113	2	.01	3	9.473e-3	2	NC	1	NC	1
38			min	-.642	4	-.021	3	-.005	2	-2.081e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.25	3	.009	3	5.511e-3	2	NC	1	NC	1
40			min	-.479	4	-.366	2	-.005	2	-4.355e-3	3	NC	1	NC	1
41		2	max	0	1	.566	3	.023	1	6.577e-3	2	NC	5	NC	1
42			min	-.479	4	-.649	2	-.029	5	-5.284e-3	3	721.321	3	7472.654	5
43		3	max	0	1	.835	3	.065	1	7.642e-3	2	NC	5	NC	3
44			min	-.479	4	-.894	2	-.035	5	-6.213e-3	3	389.822	3	3533.326	1
45		4	max	0	1	1.024	3	.104	1	8.707e-3	2	NC	15	NC	3
46			min	-.479	4	-1.077	2	-.023	5	-7.142e-3	3	294.578	3	2193.838	1
47		5	max	0	1	1.117	3	.127	1	9.773e-3	2	NC	15	NC	3
48			min	-.479	4	-1.184	2	-.003	5	-8.07e-3	3	262.9	3	1807.381	1
49		6	max	0	1	1.115	3	.125	1	1.084e-2	2	NC	15	NC	3
50			min	-.479	4	-1.215	2	.008	10	-8.999e-3	3	263.66	3	1837.308	1
51		7	max	0	1	1.033	3	.099	1	1.19e-2	2	NC	15	NC	3
52			min	-.479	4	-1.18	2	.003	10	-9.928e-3	3	280.339	2	2323.115	1
53		8	max	0	1	.904	3	.059	4	1.297e-2	2	NC	15	NC	2
54			min	-.479	4	-1.102	2	-.003	10	-1.086e-2	3	309.677	2	4003.022	4
55		9	max	0	1	.777	3	.038	4	1.403e-2	2	NC	5	NC	1
56			min	-.479	4	-1.019	2	-.01	2	-1.179e-2	3	349.014	2	6176.206	4
57		10	max	0	1	.718	3	.027	3	1.51e-2	2	NC	5	NC	1
58			min	-.479	4	-.979	2	-.019	2	-1.271e-2	3	372.175	2	NC	1
59		11	max	0	12	.777	3	.028	3	1.403e-2	2	NC	5	NC	1
60			min	-.479	4	-1.019	2	-.029	5	-1.179e-2	3	349.014	2	7952.926	5
61		12	max	0	12	.904	3	.057	1	1.297e-2	2	NC	15	NC	2
62			min	-.479	4	-1.102	2	-.033	5	-1.086e-2	3	309.677	2	4059.894	1
63		13	max	0	12	1.033	3	.099	1	1.19e-2	2	NC	15	NC	3
64			min	-.479	4	-1.18	2	-.02	5	-9.928e-3	3	280.339	2	2323.115	1
65		14	max	0	12	1.115	3	.125	1	1.084e-2	2	NC	15	NC	3
66			min	-.479	4	-1.215	2	0	15	-8.999e-3	3	263.66	3	1837.308	1
67		15	max	0	12	1.117	3	.127	1	9.773e-3	2	NC	15	NC	3
68			min	-.479	4	-1.184	2	.01	10	-8.07e-3	3	262.9	3	1807.381	1
69		16	max	0	12	1.024	3	.104	1	8.707e-3	2	NC	15	NC	3
70			min	-.479	4	-1.077	2	.008	10	-7.142e-3	3	294.578	3	2193.838	1
71		17	max	0	12	.835	3	.065	1	7.642e-3	2	NC	5	NC	3
72			min	-.479	4	-.894	2	.004	10	-6.213e-3	3	389.822	3	3533.326	1
73		18	max	0	12	.566	3	.04	4	6.577e-3	2	NC	5	NC	1
74			min	-.479	4	-.649	2	0	10	-5.284e-3	3	721.321	3	5746.153	4
75		19	max	0	12	.25	3	.009	3	5.511e-3	2	NC	1	NC	1
76			min	-.479	4	-.366	2	-.005	2	-4.355e-3	3	NC	1	NC	1
77	M15	1	max	0	12	.255	3	.008	3	3.78e-3	3	NC	1	NC	1
78			min	-.391	4	-.365	2	-.005	2	-5.766e-3	2	NC	1	NC	1
79		2	max	0	12	.462	3	.023	1	4.592e-3	3	NC	5	NC	1
80			min	-.391	4	-.733	2	-.038	5	-6.886e-3	2	619.403	2	5733.798	5
81		3	max	0	12	.642	3	.065	1	5.404e-3	3	NC	5	NC	3
82			min	-.391	4	-1.048	2	-.046	5	-8.006e-3	2	333.839	2	3522.054	1
83		4	max	0	12	.778	3	.105	1	6.216e-3	3	NC	15	NC	3
84			min	-.391	4	-1.273	2	-.033	5	-9.125e-3	2	251.096	2	2188.008	1
85		5	max	0	12	.86	3	.127	1	7.027e-3	3	NC	15	NC	3
86			min	-.391	4	-1.39	2	-.008	5	-1.025e-2	2	222.475	2	1802.68	1
87		6	max	0	12	.887	3	.125	1	7.839e-3	3	NC	15	NC	3
88			min	-.391	4	-1.398	2	.008	10	-1.136e-2	2	220.685	2	1831.912	1
89		7	max	0	12	.866	3	.099	1	8.651e-3	3	NC	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.391	4	-1.316	2	.004	10	-1.248e-2	2	239.786	2	2313.94	1
91		8	max	0	12	.814	3	.069	4	9.463e-3	3	NC	15	NC	2
92			min	-.391	4	-1.179	2	-.003	10	-1.36e-2	2	280.103	2	3399.353	4
93		9	max	0	12	.758	3	.047	4	1.027e-2	3	NC	5	NC	1
94			min	-.391	4	-1.042	2	-.009	2	-1.472e-2	2	336.889	2	5042.658	4
95		10	max	0	1	.73	3	.025	3	1.109e-2	3	NC	5	NC	1
96			min	-.391	4	-.977	2	-.018	2	-1.584e-2	2	372.796	2	NC	1
97		11	max	0	1	.758	3	.026	3	1.027e-2	3	NC	5	NC	1
98			min	-.391	4	-1.042	2	-.037	5	-1.472e-2	2	336.889	2	6173.838	5
99		12	max	0	1	.814	3	.057	1	9.463e-3	3	NC	15	NC	2
100			min	-.391	4	-1.179	2	-.043	5	-1.36e-2	2	280.103	2	4030.989	1
101		13	max	0	1	.866	3	.099	1	8.651e-3	3	NC	15	NC	3
102			min	-.391	4	-1.316	2	-.028	5	-1.248e-2	2	239.786	2	2313.94	1
103		14	max	0	1	.887	3	.125	1	7.839e-3	3	NC	15	NC	3
104			min	-.391	4	-1.398	2	-.001	5	-1.136e-2	2	220.685	2	1831.912	1
105		15	max	0	1	.86	3	.127	1	7.027e-3	3	NC	15	NC	3
106			min	-.391	4	-1.39	2	.01	10	-1.025e-2	2	222.475	2	1802.68	1
107		16	max	0	1	.778	3	.105	1	6.216e-3	3	NC	15	NC	3
108			min	-.391	4	-1.273	2	.008	10	-9.125e-3	2	251.096	2	2188.008	1
109		17	max	0	1	.642	3	.074	4	5.404e-3	3	NC	5	NC	3
110			min	-.391	4	-1.048	2	.004	10	-8.006e-3	2	333.839	2	3106.004	4
111		18	max	0	1	.462	3	.049	4	4.592e-3	3	NC	5	NC	1
112			min	-.39	4	-.733	2	0	10	-6.886e-3	2	619.403	2	4649.537	4
113		19	max	0	1	.255	3	.008	3	3.78e-3	3	NC	1	NC	1
114			min	-.39	4	-.365	2	-.005	2	-5.766e-3	2	NC	1	NC	1
115	M16	1	max	0	12	.1	2	.007	3	6.715e-3	3	NC	1	NC	1
116			min	-.138	4	-.083	3	-.004	2	-7.803e-3	2	NC	1	NC	1
117		2	max	0	12	.023	3	.034	1	7.864e-3	3	NC	5	NC	2
118			min	-.138	4	-.147	2	-.03	5	-8.76e-3	2	921.437	2	6850.454	1
119		3	max	0	12	.106	3	.081	1	9.012e-3	3	NC	5	NC	3
120			min	-.138	4	-.345	2	-.037	5	-9.718e-3	2	512.775	2	2812.778	1
121		4	max	0	12	.149	3	.123	1	1.016e-2	3	NC	5	NC	3
122			min	-.138	4	-.458	2	-.028	5	-1.067e-2	2	408.598	2	1864.926	1
123		5	max	0	12	.145	3	.144	1	1.131e-2	3	NC	5	NC	3
124			min	-.138	4	-.472	2	-.009	5	-1.163e-2	2	398.53	2	1591.224	1
125		6	max	0	12	.096	3	.138	1	1.246e-2	3	NC	5	NC	3
126			min	-.138	4	-.39	2	.007	15	-1.259e-2	2	465.638	2	1651.753	1
127		7	max	0	12	.012	3	.108	1	1.361e-2	3	NC	5	NC	3
128			min	-.138	4	-.231	2	.006	10	-1.355e-2	2	687.708	2	2113.572	1
129		8	max	0	12	.016	9	.062	1	1.475e-2	3	NC	3	NC	2
130			min	-.138	4	-.087	3	-.001	10	-1.45e-2	2	1666.694	2	3698.085	1
131		9	max	0	12	.138	1	.033	4	1.59e-2	3	NC	4	NC	1
132			min	-.138	4	-.175	3	-.008	10	-1.546e-2	2	2482.552	3	7068.063	4
133		10	max	0	1	.216	2	.022	3	1.705e-2	3	NC	4	NC	1
134			min	-.138	4	-.214	3	-.017	2	-1.642e-2	2	1743.231	3	NC	1
135		11	max	0	1	.138	1	.023	3	1.59e-2	3	NC	4	NC	1
136			min	-.138	4	-.175	3	-.024	5	-1.546e-2	2	2482.552	3	9644.636	5
137		12	max	0	1	.016	9	.062	1	1.475e-2	3	NC	3	NC	2
138			min	-.137	4	-.087	3	-.025	5	-1.45e-2	2	1666.694	2	3698.085	1
139		13	max	0	1	.012	3	.108	1	1.361e-2	3	NC	5	NC	3
140			min	-.137	4	-.231	2	-.011	5	-1.355e-2	2	687.708	2	2113.572	1
141		14	max	0	1	.096	3	.138	1	1.246e-2	3	NC	5	NC	3
142			min	-.137	4	-.39	2	.007	15	-1.259e-2	2	465.638	2	1651.753	1
143		15	max	0	1	.145	3	.144	1	1.131e-2	3	NC	5	NC	3
144			min	-.137	4	-.472	2	.013	10	-1.163e-2	2	398.53	2	1591.224	1
145		16	max	0	1	.149	3	.123	1	1.016e-2	3	NC	5	NC	3
146			min	-.137	4	-.458	2	.011	10	-1.067e-2	2	408.598	2	1864.926	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.106	3	.081	1	9.012e-3	3	NC	5	NC	3
148			min	-.137	4	-.345	2	.006	10	-9.718e-3	2	512.775	2	2812.778	1
149		18	max	0	1	.023	3	.044	4	7.864e-3	3	NC	5	NC	2
150			min	-.137	4	-.147	2	0	10	-8.76e-3	2	921.437	2	5133.03	4
151		19	max	0	1	.1	2	.007	3	6.715e-3	3	NC	1	NC	1
152			min	-.137	4	-.083	3	-.004	2	-7.803e-3	2	NC	1	NC	1
153	M2	1	max	.007	2	.009	2	.008	1	1.525e-3	5	NC	1	NC	2
154			min	-.01	3	-.014	3	-.601	4	-2.153e-4	1	7982.141	2	116.345	4
155		2	max	.007	2	.008	2	.007	1	1.605e-3	5	NC	1	NC	2
156			min	-.009	3	-.014	3	-.553	4	-2.031e-4	1	9198.847	2	126.579	4
157		3	max	.006	2	.006	2	.006	1	1.686e-3	5	NC	1	NC	1
158			min	-.009	3	-.013	3	-.504	4	-1.908e-4	1	NC	1	138.715	4
159		4	max	.006	2	.005	2	.006	1	1.766e-3	5	NC	1	NC	1
160			min	-.008	3	-.013	3	-.456	4	-1.785e-4	1	NC	1	153.243	4
161		5	max	.006	2	.004	2	.005	1	1.847e-3	5	NC	1	NC	1
162			min	-.007	3	-.012	3	-.409	4	-1.662e-4	1	NC	1	170.828	4
163		6	max	.005	2	.003	2	.005	1	1.927e-3	5	NC	1	NC	1
164			min	-.007	3	-.012	3	-.364	4	-1.539e-4	1	NC	1	192.393	4
165		7	max	.005	2	.002	2	.004	1	2.007e-3	5	NC	1	NC	1
166			min	-.006	3	-.011	3	-.319	4	-1.417e-4	1	NC	1	219.238	4
167		8	max	.004	2	.001	2	.003	1	2.088e-3	5	NC	1	NC	1
168			min	-.006	3	-.01	3	-.276	4	-1.294e-4	1	NC	1	253.256	4
169		9	max	.004	2	0	2	.003	1	2.168e-3	5	NC	1	NC	1
170			min	-.005	3	-.01	3	-.235	4	-1.171e-4	1	NC	1	297.281	4
171		10	max	.004	2	0	2	.002	1	2.248e-3	5	NC	1	NC	1
172			min	-.005	3	-.009	3	-.197	4	-1.048e-4	1	NC	1	355.724	4
173		11	max	.003	2	0	2	.002	1	2.332e-3	4	NC	1	NC	1
174			min	-.004	3	-.008	3	-.161	4	-9.255e-5	1	NC	1	435.752	4
175		12	max	.003	2	0	15	.002	1	2.417e-3	4	NC	1	NC	1
176			min	-.004	3	-.007	3	-.127	4	-8.027e-5	1	NC	1	549.678	4
177		13	max	.002	2	0	15	.001	1	2.501e-3	4	NC	1	NC	1
178			min	-.003	3	-.006	3	-.097	4	-6.799e-5	1	NC	1	720.14	4
179		14	max	.002	2	0	15	0	1	2.586e-3	4	NC	1	NC	1
180			min	-.003	3	-.005	3	-.07	4	-5.571e-5	1	NC	1	992.659	4
181		15	max	.002	2	0	15	0	1	2.67e-3	4	NC	1	NC	1
182			min	-.002	3	-.004	3	-.048	4	-4.343e-5	1	NC	1	1470.526	4
183		16	max	.001	2	0	15	0	1	2.755e-3	4	NC	1	NC	1
184			min	-.002	3	-.003	3	-.029	4	-3.115e-5	1	NC	1	2432.944	4
185		17	max	0	2	0	15	0	1	2.84e-3	4	NC	1	NC	1
186			min	-.001	3	-.002	3	-.014	4	-1.887e-5	1	NC	1	4879.517	4
187		18	max	0	2	0	15	0	1	2.924e-3	4	NC	1	NC	1
188			min	0	3	-.001	3	-.005	4	-6.588e-6	1	NC	1	NC	1
189		19	max	0	1	0	1	0	1	3.009e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	1.193e-7	12	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	-1.007e-7	12	NC	1	NC	1
192			min	0	1	0	1	0	1	-7.564e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.014	4	1.838e-5	1	NC	1	NC	1
194			min	0	2	-.002	6	0	12	-1.273e-4	5	NC	1	6365.028	4
195		3	max	0	3	0	15	.027	4	5.092e-4	4	NC	1	NC	1
196			min	0	2	-.004	6	0	12	2.398e-6	12	NC	1	3321.799	4
197		4	max	.001	3	-.001	15	.039	4	1.142e-3	4	NC	1	NC	1
198			min	-.001	2	-.006	6	0	12	3.647e-6	12	NC	1	2309.237	4
199		5	max	.002	3	-.002	15	.05	4	1.775e-3	4	NC	1	NC	1
200			min	-.001	2	-.008	6	0	12	4.896e-6	12	NC	1	1803.531	4
201		6	max	.002	3	-.002	15	.06	4	2.408e-3	4	NC	1	NC	1
202			min	-.002	2	-.009	6	0	12	6.145e-6	12	9775.121	6	1499.744	4
203		7	max	.003	3	-.002	15	.07	4	3.04e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.002	2	-.011	6	0	12	7.394e-6	12	8409.992	6	1296.08	4
205		8	max	.003	3	-.003	15	.079	4	3.673e-3	4	NC	1	NC	1
206			min	-.003	2	-.012	6	0	12	8.643e-6	12	7568.368	6	1148.786	4
207		9	max	.003	3	-.003	15	.087	4	4.306e-3	4	NC	2	NC	1
208			min	-.003	2	-.013	6	0	12	9.892e-6	12	7072.901	6	1035.884	4
209		10	max	.004	3	-.003	15	.095	4	4.939e-3	4	NC	5	NC	1
210			min	-.003	2	-.013	6	0	12	1.114e-5	12	6837.732	6	945.099	4
211		11	max	.004	3	-.003	15	.104	4	5.572e-3	4	NC	5	NC	1
212			min	-.004	2	-.013	6	0	12	1.239e-5	12	6828.361	6	869.039	4
213		12	max	.005	3	-.003	15	.112	4	6.204e-3	4	NC	2	NC	1
214			min	-.004	2	-.013	6	0	12	1.364e-5	12	7048.418	6	803.015	4
215		13	max	.005	3	-.003	15	.121	4	6.837e-3	4	NC	1	NC	1
216			min	-.004	2	-.012	6	0	12	1.489e-5	12	7542.776	6	743.959	4
217		14	max	.006	3	-.002	15	.131	4	7.47e-3	4	NC	1	NC	1
218			min	-.005	2	-.011	6	0	12	1.614e-5	12	8420.602	6	689.841	4
219		15	max	.006	3	-.002	15	.141	4	8.103e-3	4	NC	1	NC	1
220			min	-.005	2	-.009	6	0	12	1.739e-5	12	9923.08	6	639.339	4
221		16	max	.006	3	-.001	15	.152	4	8.735e-3	4	NC	1	NC	1
222			min	-.005	2	-.007	6	0	12	1.864e-5	12	NC	1	591.628	4
223		17	max	.007	3	0	15	.165	4	9.368e-3	4	NC	1	NC	1
224			min	-.006	2	-.005	1	0	12	1.989e-5	12	NC	1	546.239	4
225		18	max	.007	3	0	15	.179	4	1.e-2	4	NC	1	NC	1
226			min	-.006	2	-.004	1	0	12	2.113e-5	12	NC	1	502.954	4
227		19	max	.008	3	0	5	.195	4	1.063e-2	4	NC	1	NC	1
228			min	-.007	2	-.002	3	0	12	2.238e-5	12	NC	1	461.719	4
229	M4	1	max	.002	1	.006	2	0	12	3.42e-4	4	NC	1	NC	3
230			min	0	5	-.008	3	-.195	4	5.938e-6	12	NC	1	126.95	4
231		2	max	.002	1	.006	2	0	12	3.42e-4	4	NC	1	NC	3
232			min	0	5	-.008	3	-.18	4	5.938e-6	12	NC	1	137.906	4
233		3	max	.002	1	.006	2	0	12	3.42e-4	4	NC	1	NC	3
234			min	0	5	-.007	3	-.164	4	5.938e-6	12	NC	1	150.952	4
235		4	max	.002	1	.005	2	0	12	3.42e-4	4	NC	1	NC	2
236			min	0	5	-.007	3	-.149	4	5.938e-6	12	NC	1	166.63	4
237		5	max	.002	1	.005	2	0	12	3.42e-4	4	NC	1	NC	2
238			min	0	5	-.006	3	-.134	4	5.938e-6	12	NC	1	185.677	4
239		6	max	.002	1	.004	2	0	12	3.42e-4	4	NC	1	NC	2
240			min	0	5	-.006	3	-.119	4	5.938e-6	12	NC	1	209.113	4
241		7	max	.002	1	.004	2	0	12	3.42e-4	4	NC	1	NC	2
242			min	0	5	-.005	3	-.104	4	5.938e-6	12	NC	1	238.388	4
243		8	max	.001	1	.004	2	0	12	3.42e-4	4	NC	1	NC	2
244			min	0	5	-.005	3	-.09	4	5.938e-6	12	NC	1	275.614	4
245		9	max	.001	1	.003	2	0	12	3.42e-4	4	NC	1	NC	2
246			min	0	5	-.004	3	-.077	4	5.938e-6	12	NC	1	323.972	4
247		10	max	.001	1	.003	2	0	12	3.42e-4	4	NC	1	NC	1
248			min	0	5	-.004	3	-.064	4	5.938e-6	12	NC	1	388.435	4
249		11	max	.001	1	.003	2	0	12	3.42e-4	4	NC	1	NC	1
250			min	0	5	-.004	3	-.052	4	5.938e-6	12	NC	1	477.132	4
251		12	max	0	1	.002	2	0	12	3.42e-4	4	NC	1	NC	1
252			min	0	5	-.003	3	-.041	4	5.938e-6	12	NC	1	604.128	4
253		13	max	0	1	.002	2	0	12	3.42e-4	4	NC	1	NC	1
254			min	0	5	-.003	3	-.031	4	5.938e-6	12	NC	1	795.52	4
255		14	max	0	1	.002	2	0	12	3.42e-4	4	NC	1	NC	1
256			min	0	5	-.002	3	-.022	4	5.938e-6	12	NC	1	1104.382	4
257		15	max	0	1	.001	2	0	12	3.42e-4	4	NC	1	NC	1
258			min	0	5	-.002	3	-.015	4	5.938e-6	12	NC	1	1653.026	4
259		16	max	0	1	.001	2	0	12	3.42e-4	4	NC	1	NC	1
260			min	0	5	-.001	3	-.009	4	5.938e-6	12	NC	1	2779.413	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	3.42e-4	4	NC	1	NC	1
262			min	0	5	0	3	-.004	4	5.938e-6	12	NC	1	5735.864	4
263		18	max	0	1	0	2	0	12	3.42e-4	4	NC	1	NC	1
264			min	0	5	0	3	-.001	4	5.938e-6	12	NC	1	NC	1
265		19	max	0	1	0	1	0	1	3.42e-4	4	NC	1	NC	1
266			min	0	1	0	1	0	1	5.938e-6	12	NC	1	NC	1
267	M6	1	max	.023	2	.032	2	0	1	1.612e-3	4	NC	4	NC	1
268			min	-.031	3	-.045	3	-.607	4	0	1	1550.986	3	115.261	4
269		2	max	.021	2	.029	2	0	1	1.691e-3	4	NC	4	NC	1
270			min	-.03	3	-.043	3	-.558	4	0	1	1644.604	3	125.402	4
271		3	max	.02	2	.027	2	0	1	1.769e-3	4	NC	4	NC	1
272			min	-.028	3	-.04	3	-.509	4	0	1	1750.274	3	137.427	4
273		4	max	.019	2	.024	2	0	1	1.847e-3	4	NC	4	NC	1
274			min	-.026	3	-.037	3	-.461	4	0	1	1870.492	3	151.823	4
275		5	max	.018	2	.021	2	0	1	1.925e-3	4	NC	4	NC	1
276			min	-.024	3	-.035	3	-.413	4	0	1	2008.468	3	169.249	4
277		6	max	.016	2	.019	2	0	1	2.004e-3	4	NC	4	NC	1
278			min	-.023	3	-.032	3	-.367	4	0	1	2168.402	3	190.619	4
279		7	max	.015	2	.016	2	0	1	2.082e-3	4	NC	1	NC	1
280			min	-.021	3	-.03	3	-.322	4	0	1	2355.9	3	217.224	4
281		8	max	.014	2	.014	2	0	1	2.16e-3	4	NC	1	NC	1
282			min	-.019	3	-.027	3	-.279	4	0	1	2578.609	3	250.937	4
283		9	max	.013	2	.012	2	0	1	2.238e-3	4	NC	1	NC	1
284			min	-.017	3	-.025	3	-.237	4	0	1	2847.243	3	294.57	4
285		10	max	.011	2	.01	2	0	1	2.317e-3	4	NC	1	NC	1
286			min	-.016	3	-.022	3	-.198	4	0	1	3177.284	3	352.495	4
287		11	max	.01	2	.008	2	0	1	2.395e-3	4	NC	1	NC	1
288			min	-.014	3	-.019	3	-.162	4	0	1	3591.969	3	431.819	4
289		12	max	.009	2	.006	2	0	1	2.473e-3	4	NC	1	NC	1
290			min	-.012	3	-.017	3	-.128	4	0	1	4127.83	3	544.749	4
291		13	max	.008	2	.005	2	0	1	2.551e-3	4	NC	1	NC	1
292			min	-.01	3	-.014	3	-.098	4	0	1	4845.773	3	713.737	4
293		14	max	.006	2	.003	2	0	1	2.629e-3	4	NC	1	NC	1
294			min	-.009	3	-.012	3	-.071	4	0	1	5855.461	3	983.93	4
295		15	max	.005	2	.002	2	0	1	2.708e-3	4	NC	1	NC	1
296			min	-.007	3	-.009	3	-.048	4	0	1	7376.271	3	1457.787	4
297		16	max	.004	2	.001	2	0	1	2.786e-3	4	NC	1	NC	1
298			min	-.005	3	-.007	3	-.029	4	0	1	9920.151	3	2412.342	4
299		17	max	.003	2	0	2	0	1	2.864e-3	4	NC	1	NC	1
300			min	-.003	3	-.005	3	-.014	4	0	1	NC	1	4839.787	4
301		18	max	.001	2	0	2	0	1	2.942e-3	4	NC	1	NC	1
302			min	-.002	3	-.002	3	-.005	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	3.021e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-7.59e-4	4	NC	1	NC	1
307		2	max	.001	3	0	2	.014	4	0	1	NC	1	NC	1
308			min	-.001	2	-.003	3	0	1	-1.427e-4	4	NC	1	NC	1
309		3	max	.003	3	0	2	.027	4	4.736e-4	4	NC	1	NC	1
310			min	-.003	2	-.006	3	0	1	0	1	NC	1	NC	1
311		4	max	.004	3	-.001	15	.039	4	1.09e-3	4	NC	1	NC	1
312			min	-.004	2	-.008	3	0	1	0	1	NC	1	NC	1
313		5	max	.005	3	-.002	15	.05	4	1.706e-3	4	NC	1	NC	1
314			min	-.005	2	-.01	3	0	1	0	1	NC	1	NC	1
315		6	max	.007	3	-.002	15	.06	4	2.322e-3	4	NC	1	NC	1
316			min	-.007	2	-.012	3	0	1	0	1	8605.604	3	NC	1
317		7	max	.008	3	-.003	15	.07	4	2.939e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.008	2	-.014	3	0	1	0	1	7694.216	3	NC	1
319		8	max	.009	3	-.003	15	.078	4	3.555e-3	4	NC	1	NC	1
320			min	-.009	2	-.015	3	0	1	0	1	7156.187	3	NC	1
321		9	max	.011	3	-.003	15	.087	4	4.171e-3	4	NC	1	NC	1
322			min	-.011	2	-.016	3	0	1	0	1	6880.208	3	NC	1
323		10	max	.012	3	-.003	15	.095	4	4.788e-3	4	NC	1	NC	1
324			min	-.012	2	-.016	3	0	1	0	1	6816.525	3	NC	1
325		11	max	.014	3	-.003	15	.103	4	5.404e-3	4	NC	1	NC	1
326			min	-.013	2	-.017	3	0	1	0	1	6856.128	4	NC	1
327		12	max	.015	3	-.003	15	.111	4	6.02e-3	4	NC	1	NC	1
328			min	-.014	2	-.016	3	0	1	0	1	7075.794	4	NC	1
329		13	max	.016	3	-.003	15	.12	4	6.636e-3	4	NC	1	NC	1
330			min	-.016	2	-.016	3	0	1	0	1	7570.915	4	NC	1
331		14	max	.018	3	-.003	15	.129	4	7.253e-3	4	NC	1	NC	1
332			min	-.017	2	-.015	3	0	1	0	1	8450.938	4	NC	1
333		15	max	.019	3	-.002	15	.138	4	7.869e-3	4	NC	1	NC	1
334			min	-.018	2	-.013	3	0	1	0	1	9957.793	4	NC	1
335		16	max	.02	3	-.002	15	.149	4	8.485e-3	4	NC	1	NC	1
336			min	-.02	2	-.012	3	0	1	0	1	NC	1	NC	1
337		17	max	.022	3	-.001	15	.161	4	9.101e-3	4	NC	1	NC	1
338			min	-.021	2	-.01	3	0	1	0	1	NC	1	NC	1
339		18	max	.023	3	0	10	.174	4	9.718e-3	4	NC	1	NC	1
340			min	-.022	2	-.008	3	0	1	0	1	NC	1	NC	1
341		19	max	.024	3	0	10	.189	4	1.033e-2	4	NC	1	NC	1
342			min	-.024	2	-.006	3	0	1	0	1	NC	1	NC	1
343	M8	1	max	.006	1	.023	2	0	1	2.236e-4	4	NC	1	NC	1
344			min	0	3	-.025	3	-.189	4	0	1	NC	1	131.123	4
345		2	max	.006	1	.022	2	0	1	2.236e-4	4	NC	1	NC	1
346			min	0	3	-.024	3	-.174	4	0	1	NC	1	142.447	4
347		3	max	.006	1	.02	2	0	1	2.236e-4	4	NC	1	NC	1
348			min	0	3	-.022	3	-.159	4	0	1	NC	1	155.932	4
349		4	max	.005	1	.019	2	0	1	2.236e-4	4	NC	1	NC	1
350			min	0	3	-.021	3	-.144	4	0	1	NC	1	172.138	4
351		5	max	.005	1	.018	2	0	1	2.236e-4	4	NC	1	NC	1
352			min	0	3	-.02	3	-.129	4	0	1	NC	1	191.825	4
353		6	max	.005	1	.017	2	0	1	2.236e-4	4	NC	1	NC	1
354			min	0	3	-.018	3	-.115	4	0	1	NC	1	216.048	4
355		7	max	.004	1	.015	2	0	1	2.236e-4	4	NC	1	NC	1
356			min	0	3	-.017	3	-.101	4	0	1	NC	1	246.305	4
357		8	max	.004	1	.014	2	0	1	2.236e-4	4	NC	1	NC	1
358			min	0	3	-.015	3	-.087	4	0	1	NC	1	284.781	4
359		9	max	.004	1	.013	2	0	1	2.236e-4	4	NC	1	NC	1
360			min	0	3	-.014	3	-.074	4	0	1	NC	1	334.762	4
361		10	max	.003	1	.011	2	0	1	2.236e-4	4	NC	1	NC	1
362			min	0	3	-.013	3	-.062	4	0	1	NC	1	401.388	4
363		11	max	.003	1	.01	2	0	1	2.236e-4	4	NC	1	NC	1
364			min	0	3	-.011	3	-.05	4	0	1	NC	1	493.063	4
365		12	max	.002	1	.009	2	0	1	2.236e-4	4	NC	1	NC	1
366			min	0	3	-.01	3	-.04	4	0	1	NC	1	624.323	4
367		13	max	.002	1	.008	2	0	1	2.236e-4	4	NC	1	NC	1
368			min	0	3	-.008	3	-.03	4	0	1	NC	1	822.143	4
369		14	max	.002	1	.006	2	0	1	2.236e-4	4	NC	1	NC	1
370			min	0	3	-.007	3	-.022	4	0	1	NC	1	1141.384	4
371		15	max	.001	1	.005	2	0	1	2.236e-4	4	NC	1	NC	1
372			min	0	3	-.006	3	-.015	4	0	1	NC	1	1708.473	4
373		16	max	.001	1	.004	2	0	1	2.236e-4	4	NC	1	NC	1
374			min	0	3	-.004	3	-.009	4	0	1	NC	1	2872.756	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	1	.003	2	0	1	2.236e-4	4	NC	1	NC	1
376			min	0	3	-.003	3	-.004	4	0	1	NC	1	5928.765	4
377		18	max	0	1	.001	2	0	1	2.236e-4	4	NC	1	NC	1
378			min	0	3	-.001	3	-.001	4	0	1	NC	1	NC	1
379		19	max	0	1	0	1	0	1	2.236e-4	4	NC	1	NC	1
380			min	0	1	0	1	0	1	0	1	NC	1	NC	1
381	M10	1	max	.007	2	.009	2	0	12	1.62e-3	4	NC	1	NC	2
382			min	-.01	3	-.014	3	-.606	4	1.517e-5	12	7982.141	2	115.426	4
383		2	max	.007	2	.008	2	0	12	1.697e-3	4	NC	1	NC	2
384			min	-.009	3	-.014	3	-.557	4	1.432e-5	12	9198.847	2	125.582	4
385		3	max	.006	2	.006	2	0	12	1.774e-3	4	NC	1	NC	1
386			min	-.009	3	-.013	3	-.508	4	1.347e-5	12	NC	1	137.625	4
387		4	max	.006	2	.005	2	0	12	1.851e-3	4	NC	1	NC	1
388			min	-.008	3	-.013	3	-.46	4	1.262e-5	12	NC	1	152.043	4
389		5	max	.006	2	.004	2	0	12	1.928e-3	4	NC	1	NC	1
390			min	-.007	3	-.012	3	-.413	4	1.177e-5	12	NC	1	169.496	4
391		6	max	.005	2	.003	2	0	12	2.005e-3	4	NC	1	NC	1
392			min	-.007	3	-.012	3	-.366	4	1.092e-5	12	NC	1	190.898	4
393		7	max	.005	2	.002	2	0	12	2.082e-3	4	NC	1	NC	1
394			min	-.006	3	-.011	3	-.322	4	1.007e-5	12	NC	1	217.544	4
395		8	max	.004	2	.001	2	0	12	2.159e-3	4	NC	1	NC	1
396			min	-.006	3	-.01	3	-.278	4	9.225e-6	12	NC	1	251.31	4
397		9	max	.004	2	0	2	0	12	2.236e-3	4	NC	1	NC	1
398			min	-.005	3	-.01	3	-.237	4	8.375e-6	12	NC	1	295.012	4
399		10	max	.004	2	0	2	0	12	2.313e-3	4	NC	1	NC	1
400			min	-.005	3	-.009	3	-.198	4	7.526e-6	12	NC	1	353.031	4
401		11	max	.003	2	0	2	0	12	2.39e-3	4	NC	1	NC	1
402			min	-.004	3	-.008	3	-.162	4	6.676e-6	12	NC	1	432.486	4
403		12	max	.003	2	-.001	2	0	12	2.467e-3	4	NC	1	NC	1
404			min	-.004	3	-.007	3	-.128	4	5.827e-6	12	NC	1	545.607	4
405		13	max	.002	2	-.001	2	0	12	2.543e-3	4	NC	1	NC	1
406			min	-.003	3	-.006	3	-.098	4	4.977e-6	12	NC	1	714.891	4
407		14	max	.002	2	-.001	15	0	12	2.62e-3	4	NC	1	NC	1
408			min	-.003	3	-.005	3	-.071	4	4.128e-6	12	NC	1	985.577	4
409		15	max	.002	2	-.001	15	0	12	2.697e-3	4	NC	1	NC	1
410			min	-.002	3	-.004	3	-.048	4	3.278e-6	12	NC	1	1460.348	4
411		16	max	.001	2	0	15	0	12	2.774e-3	4	NC	1	NC	1
412			min	-.002	3	-.003	3	-.029	4	2.429e-6	12	NC	1	2416.89	4
413		17	max	0	2	0	15	0	12	2.851e-3	4	NC	1	NC	1
414			min	-.001	3	-.002	4	-.014	4	1.58e-6	12	NC	1	4850.006	4
415		18	max	0	2	0	15	0	12	2.928e-3	4	NC	1	NC	1
416			min	0	3	-.001	4	-.005	4	6.633e-7	10	NC	1	NC	1
417		19	max	0	1	0	1	0	1	3.005e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	-5.692e-6	1	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	2.626e-6	1	NC	1	NC	1
420			min	0	1	0	1	0	1	-7.548e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.014	4	-1.148e-6	12	NC	1	NC	1
422			min	0	2	-.002	4	0	1	-1.35e-4	4	NC	1	6374.816	4
423		3	max	0	3	0	15	.027	4	4.866e-4	5	NC	1	NC	1
424			min	0	2	-.004	4	0	1	-3.938e-5	1	NC	1	3328.756	4
425		4	max	.001	3	-.001	15	.039	4	1.105e-3	4	NC	1	NC	1
426			min	-.001	2	-.006	4	0	1	-6.038e-5	1	NC	1	2315.616	4
427		5	max	.002	3	-.002	15	.05	4	1.724e-3	4	NC	1	NC	1
428			min	-.001	2	-.008	4	0	1	-8.138e-5	1	NC	1	1809.933	4
429		6	max	.002	3	-.002	15	.06	4	2.344e-3	4	NC	1	NC	1
430			min	-.002	2	-.01	4	0	1	-1.024e-4	1	9485.83	4	1506.44	4
431		7	max	.003	3	-.003	15	.069	4	2.964e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.002	2	-.011	4	0	1	-1.234e-4	1	8179.922	4	1303.223	4
433		8	max	.003	3	-.003	15	.078	4	3.584e-3	4	NC	1	NC	1
434			min	-.003	2	-.013	4	0	1	-1.444e-4	1	7375.377	4	1156.473	4
435		9	max	.003	3	-.003	15	.086	4	4.203e-3	4	NC	2	NC	1
436			min	-.003	2	-.014	4	-.001	1	-1.654e-4	1	6903.553	4	1044.174	4
437		10	max	.004	3	-.003	15	.095	4	4.823e-3	4	NC	5	NC	1
438			min	-.003	2	-.014	4	-.001	1	-1.864e-4	1	6682.995	4	954.019	4
439		11	max	.004	3	-.004	15	.103	4	5.443e-3	4	NC	5	NC	1
440			min	-.004	2	-.014	4	-.002	1	-2.074e-4	1	6681.43	4	878.583	4
441		12	max	.005	3	-.003	15	.111	4	6.063e-3	4	NC	2	NC	1
442			min	-.004	2	-.014	4	-.002	1	-2.284e-4	1	6903.392	4	813.147	4
443		13	max	.005	3	-.003	15	.12	4	6.683e-3	4	NC	1	NC	1
444			min	-.004	2	-.013	4	-.003	1	-2.494e-4	1	7393.569	4	754.608	4
445		14	max	.006	3	-.003	15	.129	4	7.302e-3	4	NC	1	NC	1
446			min	-.005	2	-.012	4	-.003	1	-2.704e-4	1	8259.609	4	700.908	4
447		15	max	.006	3	-.003	15	.139	4	7.922e-3	4	NC	1	NC	1
448			min	-.005	2	-.01	4	-.004	1	-2.914e-4	1	9738.739	4	650.697	4
449		16	max	.006	3	-.002	15	.15	4	8.542e-3	4	NC	1	NC	1
450			min	-.005	2	-.008	4	-.005	1	-3.124e-4	1	NC	1	603.133	4
451		17	max	.007	3	-.002	15	.162	4	9.162e-3	4	NC	1	NC	1
452			min	-.006	2	-.006	4	-.005	1	-3.334e-4	1	NC	1	557.735	4
453		18	max	.007	3	-.001	15	.175	4	9.781e-3	4	NC	1	NC	1
454			min	-.006	2	-.004	4	-.006	1	-3.544e-4	1	NC	1	514.286	4
455		19	max	.008	3	0	10	.191	4	1.04e-2	4	NC	1	NC	1
456			min	-.007	2	-.002	3	-.007	1	-3.754e-4	1	NC	1	472.741	4
457	M12	1	max	.002	1	.006	2	.007	1	3.006e-4	5	NC	1	NC	3
458			min	0	3	-.008	3	-.191	4	-9.272e-5	1	NC	1	129.981	4
459		2	max	.002	1	.006	2	.007	1	3.006e-4	5	NC	1	NC	3
460			min	0	3	-.008	3	-.176	4	-9.272e-5	1	NC	1	141.199	4
461		3	max	.002	1	.006	2	.006	1	3.006e-4	5	NC	1	NC	3
462			min	0	3	-.007	3	-.16	4	-9.272e-5	1	NC	1	154.559	4
463		4	max	.002	1	.005	2	.006	1	3.006e-4	5	NC	1	NC	2
464			min	0	3	-.007	3	-.145	4	-9.272e-5	1	NC	1	170.614	4
465		5	max	.002	1	.005	2	.005	1	3.006e-4	5	NC	1	NC	2
466			min	0	3	-.006	3	-.13	4	-9.272e-5	1	NC	1	190.118	4
467		6	max	.002	1	.004	2	.004	1	3.006e-4	5	NC	1	NC	2
468			min	0	3	-.006	3	-.116	4	-9.272e-5	1	NC	1	214.117	4
469		7	max	.002	1	.004	2	.004	1	3.006e-4	5	NC	1	NC	2
470			min	0	3	-.005	3	-.102	4	-9.272e-5	1	NC	1	244.094	4
471		8	max	.001	1	.004	2	.003	1	3.006e-4	5	NC	1	NC	2
472			min	0	3	-.005	3	-.088	4	-9.272e-5	1	NC	1	282.213	4
473		9	max	.001	1	.003	2	.003	1	3.006e-4	5	NC	1	NC	2
474			min	0	3	-.004	3	-.075	4	-9.272e-5	1	NC	1	331.732	4
475		10	max	.001	1	.003	2	.002	1	3.006e-4	5	NC	1	NC	1
476			min	0	3	-.004	3	-.062	4	-9.272e-5	1	NC	1	397.741	4
477		11	max	.001	1	.003	2	.002	1	3.006e-4	5	NC	1	NC	1
478			min	0	3	-.004	3	-.051	4	-9.272e-5	1	NC	1	488.567	4
479		12	max	0	1	.002	2	.002	1	3.006e-4	5	NC	1	NC	1
480			min	0	3	-.003	3	-.04	4	-9.272e-5	1	NC	1	618.611	4
481		13	max	0	1	.002	2	.001	1	3.006e-4	5	NC	1	NC	1
482			min	0	3	-.003	3	-.03	4	-9.272e-5	1	NC	1	814.595	4
483		14	max	0	1	.002	2	0	1	3.006e-4	5	NC	1	NC	1
484			min	0	3	-.002	3	-.022	4	-9.272e-5	1	NC	1	1130.871	4
485		15	max	0	1	.001	2	0	1	3.006e-4	5	NC	1	NC	1
486			min	0	3	-.002	3	-.015	4	-9.272e-5	1	NC	1	1692.684	4
487		16	max	0	1	.001	2	0	1	3.006e-4	5	NC	1	NC	1
488			min	0	3	-.001	3	-.009	4	-9.272e-5	1	NC	1	2846.114	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	3.006e-4	5	NC	1	NC	1
490			min	0	3	0	3	-.004	4	-9.272e-5	1	NC	1	5873.558	4
491		18	max	0	1	0	2	0	1	3.006e-4	5	NC	1	NC	1
492			min	0	3	0	3	-.001	4	-9.272e-5	1	NC	1	NC	1
493		19	max	0	1	0	1	0	1	3.006e-4	5	NC	1	NC	1
494			min	0	1	0	1	0	1	-9.272e-5	1	NC	1	NC	1
495	M1	1	max	.01	3	.113	2	.642	4	1.293e-2	2	NC	1	NC	1
496			min	-.005	2	-.021	3	0	12	-2.558e-2	3	NC	1	NC	1
497		2	max	.01	3	.053	2	.621	4	7.207e-3	4	NC	4	NC	1
498			min	-.005	2	-.007	3	-.005	1	-1.266e-2	3	1916.205	2	NC	1
499		3	max	.01	3	.015	3	.601	4	1.212e-2	4	NC	5	NC	1
500			min	-.005	2	-.011	2	-.008	1	-1.468e-4	1	924.219	2	6669.804	5
501		4	max	.009	3	.052	3	.58	4	1.051e-2	4	NC	5	NC	1
502			min	-.005	2	-.084	2	-.007	1	-4.866e-3	3	584.045	2	4807.177	5
503		5	max	.009	3	.098	3	.558	4	8.908e-3	4	NC	5	NC	1
504			min	-.005	2	-.16	2	-.005	1	-9.598e-3	3	421.894	2	3873.645	5
505		6	max	.009	3	.149	3	.535	4	1.271e-2	2	NC	15	NC	1
506			min	-.005	2	-.233	2	-.002	1	-1.433e-2	3	332.514	2	3310.146	5
507		7	max	.009	3	.197	3	.513	4	1.694e-2	2	NC	15	NC	1
508			min	-.005	2	-.299	2	0	12	-1.906e-2	3	279.728	2	2909.418	4
509		8	max	.009	3	.238	3	.489	4	2.117e-2	2	9909.069	15	NC	1
510			min	-.005	2	-.35	2	0	12	-2.38e-2	3	248.494	2	2611.948	4
511		9	max	.008	3	.264	3	.464	4	2.418e-2	2	9263.369	15	NC	1
512			min	-.005	2	-.383	2	0	1	-2.401e-2	3	232.231	2	2419.911	4
513		10	max	.008	3	.273	3	.438	4	2.637e-2	2	9066.57	15	NC	1
514			min	-.005	2	-.394	2	0	12	-2.121e-2	3	227.473	2	2358.867	4
515		11	max	.008	3	.266	3	.409	4	2.856e-2	2	9262.959	15	NC	1
516			min	-.005	2	-.383	2	0	12	-1.842e-2	3	233.076	2	2402.388	4
517		12	max	.008	3	.244	3	.378	4	2.769e-2	2	9908.135	15	NC	1
518			min	-.005	2	-.349	2	0	1	-1.551e-2	3	251.067	2	2560.116	4
519		13	max	.008	3	.208	3	.343	4	2.221e-2	2	NC	15	NC	1
520			min	-.005	2	-.294	2	0	1	-1.241e-2	3	285.993	2	2986.787	4
521		14	max	.008	3	.162	3	.306	4	1.673e-2	2	NC	15	NC	1
522			min	-.005	2	-.226	2	0	12	-9.318e-3	3	345.902	2	3885.979	4
523		15	max	.007	3	.11	3	.269	4	1.125e-2	2	NC	5	NC	1
524			min	-.004	2	-.151	2	0	12	-6.223e-3	3	449.45	2	5835.353	4
525		16	max	.007	3	.056	3	.231	4	8.629e-3	4	NC	5	NC	1
526			min	-.004	2	-.075	2	0	12	-3.128e-3	3	642.159	2	NC	1
527		17	max	.007	3	.005	3	.196	4	9.807e-3	4	NC	5	NC	1
528			min	-.004	2	-.006	2	0	12	-3.314e-5	3	1056.077	2	NC	1
529		18	max	.007	3	.05	2	.165	4	1.013e-2	2	NC	4	NC	1
530			min	-.004	2	-.04	3	0	12	-4.32e-3	3	2252.142	2	NC	1
531		19	max	.007	3	.1	2	.137	4	2.032e-2	2	NC	1	NC	1
532			min	-.004	2	-.083	3	0	1	-8.78e-3	3	NC	1	NC	1
533	M5	1	max	.03	3	.257	2	.641	4	0	1	NC	1	NC	1
534			min	-.021	2	-.02	3	0	1	-5.86e-6	4	NC	1	NC	1
535		2	max	.03	3	.118	2	.626	4	6.226e-3	4	NC	5	NC	1
536			min	-.021	2	0	3	0	1	0	1	836.622	2	9235.063	4
537		3	max	.03	3	.048	3	.606	4	1.226e-2	4	NC	5	NC	1
538			min	-.021	2	-.037	2	0	1	0	1	394.569	2	5403.72	4
539		4	max	.029	3	.145	3	.585	4	9.991e-3	4	NC	15	NC	1
540			min	-.021	2	-.221	2	0	1	0	1	242.287	2	4175.37	4
541		5	max	.029	3	.275	3	.561	4	7.719e-3	4	7730.011	15	NC	1
542			min	-.02	2	-.419	2	0	1	0	1	170.976	2	3587.716	4
543		6	max	.028	3	.421	3	.537	4	5.447e-3	4	5949.606	15	NC	1
544			min	-.02	2	-.616	2	0	1	0	1	132.411	2	3228.022	4
545		7	max	.028	3	.563	3	.512	4	3.175e-3	4	4921.788	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.02	2	-.793	2	0	1	0	1	109.994	2	2942.782	4
547		8	max	.027	3	.681	3	.488	4	9.028e-4	4	4324.328	15	NC	1
548			min	-.019	2	-.936	2	0	1	0	1	96.897	2	2658.98	4
549		9	max	.026	3	.757	3	.465	4	0	1	4018.004	15	NC	1
550			min	-.019	2	-1.026	2	0	1	-4.186e-6	5	90.158	2	2414.158	4
551		10	max	.026	3	.784	3	.437	4	0	1	3925.736	15	NC	1
552			min	-.019	2	-1.056	2	0	1	-4.059e-6	5	88.191	2	2374.27	4
553		11	max	.025	3	.764	3	.408	4	0	1	4018.16	15	NC	1
554			min	-.018	2	-1.026	2	0	1	-3.932e-6	5	90.502	2	2430.527	4
555		12	max	.025	3	.698	3	.379	4	6.942e-4	4	4324.695	15	NC	1
556			min	-.018	2	-.931	2	0	1	0	1	98.021	2	2513.662	4
557		13	max	.024	3	.592	3	.344	4	2.442e-3	4	4922.531	15	NC	1
558			min	-.018	2	-.78	2	0	1	0	1	112.907	2	2938.119	4
559		14	max	.023	3	.458	3	.306	4	4.191e-3	4	5951.052	15	NC	1
560			min	-.018	2	-.593	2	0	1	0	1	138.975	2	4059.674	4
561		15	max	.023	3	.309	3	.265	4	5.939e-3	4	7732.86	15	NC	1
562			min	-.017	2	-.39	2	0	1	0	1	185.271	2	7247.771	4
563		16	max	.022	3	.158	3	.226	4	7.687e-3	4	NC	15	NC	1
564			min	-.017	2	-.193	2	0	1	0	1	274.561	2	NC	1
565		17	max	.022	3	.016	3	.19	4	9.436e-3	4	NC	5	NC	1
566			min	-.017	2	-.02	2	0	1	0	1	474.044	2	NC	1
567		18	max	.022	3	.11	2	.16	4	4.791e-3	4	NC	5	NC	1
568			min	-.017	2	-.105	3	0	1	0	1	1051.879	2	NC	1
569		19	max	.022	3	.216	2	.138	4	0	1	NC	1	NC	1
570			min	-.017	2	-.214	3	0	1	-3.482e-6	4	NC	1	NC	1
571	M9	1	max	.01	3	.113	2	.641	4	2.558e-2	3	NC	1	NC	1
572			min	-.005	2	-.021	3	0	1	-1.293e-2	2	NC	1	NC	1
573		2	max	.01	3	.053	2	.625	4	1.266e-2	3	NC	4	NC	1
574			min	-.005	2	-.007	3	0	12	-6.343e-3	2	1916.205	2	9636.889	4
575		3	max	.01	3	.015	3	.606	4	1.224e-2	4	NC	5	NC	1
576			min	-.005	2	-.011	2	0	12	-2.718e-5	10	924.219	2	5560.932	4
577		4	max	.009	3	.052	3	.584	4	9.642e-3	5	NC	5	NC	1
578			min	-.005	2	-.084	2	0	12	-4.237e-3	2	584.045	2	4234.008	4
579		5	max	.009	3	.098	3	.561	4	9.598e-3	3	NC	5	NC	1
580			min	-.005	2	-.16	2	0	12	-8.471e-3	2	421.894	2	3589.511	4
581		6	max	.009	3	.149	3	.537	4	1.433e-2	3	NC	15	NC	1
582			min	-.005	2	-.233	2	0	12	-1.271e-2	2	332.514	2	3198.004	4
583		7	max	.009	3	.197	3	.512	4	1.906e-2	3	NC	15	NC	1
584			min	-.005	2	-.299	2	0	1	-1.694e-2	2	279.728	2	2904.887	4
585		8	max	.009	3	.238	3	.488	4	2.38e-2	3	9885.364	15	NC	1
586			min	-.005	2	-.35	2	0	1	-2.117e-2	2	248.494	2	2637.63	4
587		9	max	.008	3	.264	3	.464	4	2.401e-2	3	9241.482	15	NC	1
588			min	-.005	2	-.383	2	0	12	-2.418e-2	2	232.231	2	2412.669	4
589		10	max	.008	3	.273	3	.438	4	2.121e-2	3	9045.212	15	NC	1
590			min	-.005	2	-.394	2	0	1	-2.637e-2	2	227.473	2	2360.136	4
591		11	max	.008	3	.266	3	.409	4	1.842e-2	3	9241.07	15	NC	1
592			min	-.005	2	-.383	2	0	1	-2.856e-2	2	233.076	2	2411.616	4
593		12	max	.008	3	.244	3	.378	4	1.551e-2	3	9884.553	15	NC	1
594			min	-.005	2	-.349	2	0	12	-2.769e-2	2	251.067	2	2536.154	4
595		13	max	.008	3	.208	3	.344	4	1.241e-2	3	NC	15	NC	1
596			min	-.005	2	-.294	2	0	12	-2.221e-2	2	285.993	2	2987.467	4
597		14	max	.008	3	.162	3	.305	4	9.318e-3	3	NC	15	NC	1
598			min	-.005	2	-.226	2	-.002	1	-1.673e-2	2	345.902	2	4029.373	5
599		15	max	.007	3	.11	3	.266	4	6.223e-3	3	NC	5	NC	1
600			min	-.004	2	-.151	2	-.005	1	-1.125e-2	2	449.45	2	6519.01	5
601		16	max	.007	3	.056	3	.227	4	7.591e-3	5	NC	5	NC	1
602			min	-.004	2	-.075	2	-.007	1	-5.771e-3	2	642.159	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.007	3	.005	3	.192	4	9.527e-3	4	NC	5	NC	1
604			min	-.004	2	-.006	2	-.007	1	-5.061e-4	1	1056.077	2	NC	1
605		18	max	.007	3	.05	2	.162	4	4.578e-3	5	NC	4	NC	1
606			min	-.004	2	-.04	3	-.005	1	-1.013e-2	2	2252.142	2	NC	1
607		19	max	.007	3	.1	2	.138	4	8.78e-3	3	NC	1	NC	1
608			min	-.004	2	-.083	3	0	12	-2.032e-2	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

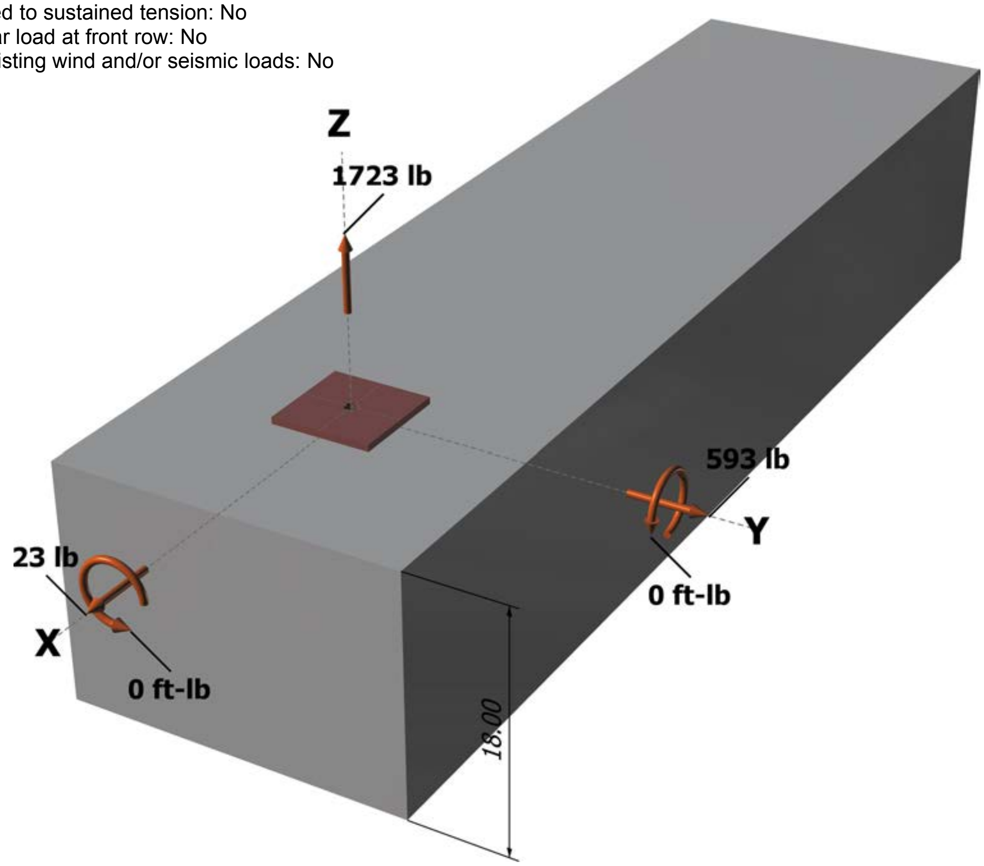
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>

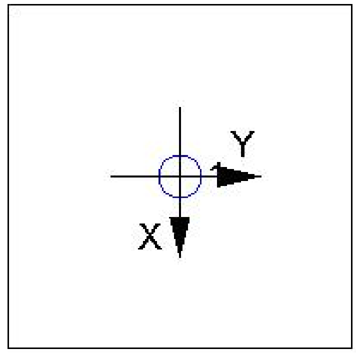
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1723.0	23.0	593.0	593.4
Sum	1723.0	23.0	593.0	593.4

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1723
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, øN_n (lb)	Ratio	Status
Steel	1723	6071	0.28	Pass
Concrete breakout	1723	5710	0.30	Pass
Adhesive	**1723**	**5365**	**0.32**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, øV_n (lb)	Ratio	Status
Steel	**593**	**3156**	**0.19**	**Pass (Governs)**
T Concrete breakout y+	593	3934	0.15	Pass
T Concrete breakout x+	23	3018	0.01	Pass
|| Concrete breakout y+	23	8508	0.00	Pass
|| Concrete breakout x+	593	6875	0.09	Pass
Concrete breakout, combined	-	-	0.15	Pass
Pryout	593	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.32	0.00	32.1 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

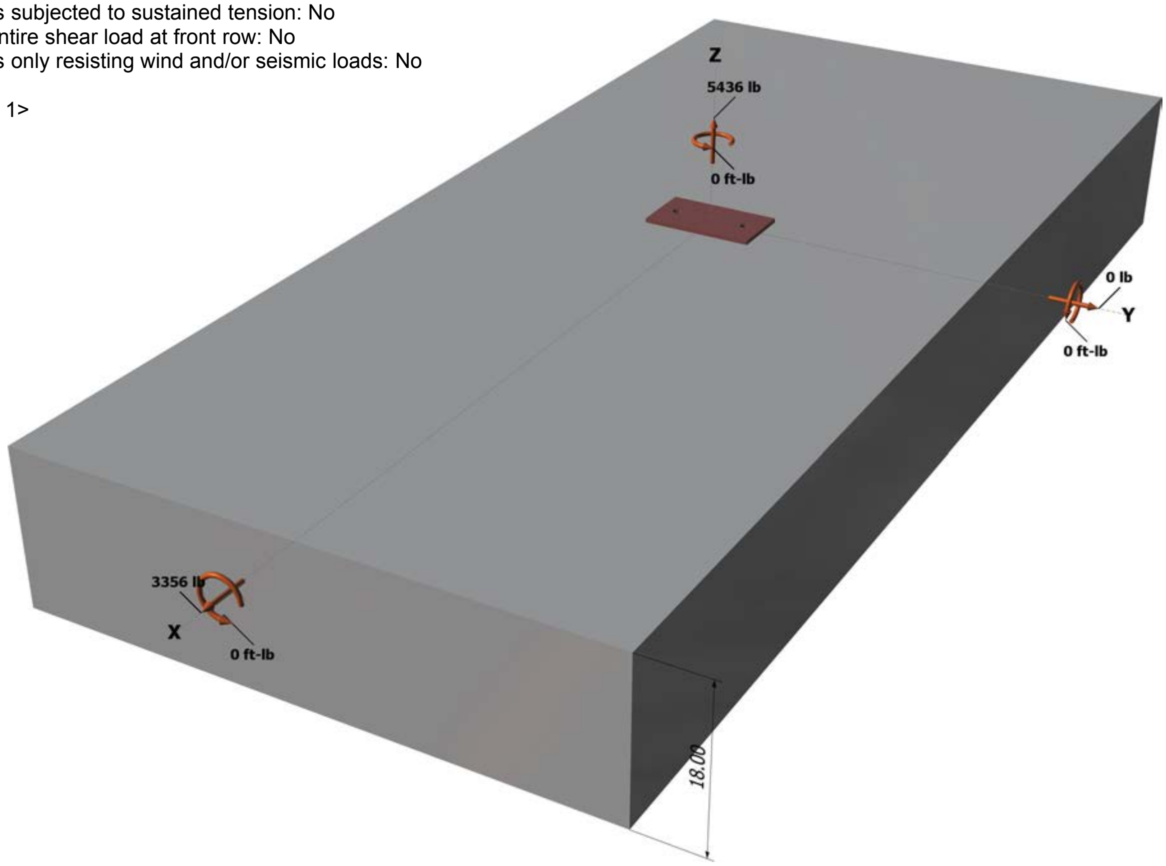
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

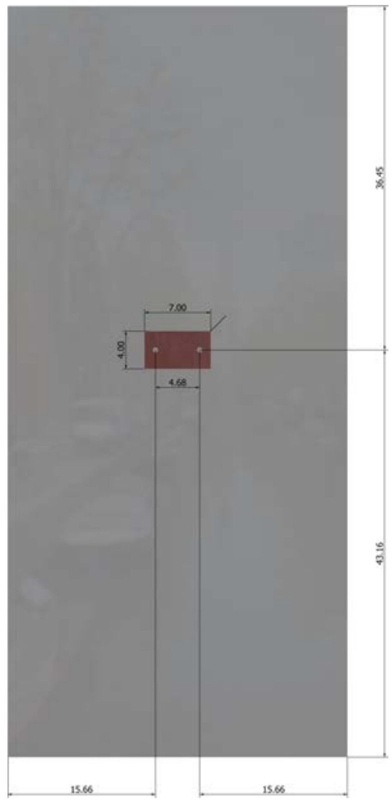
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



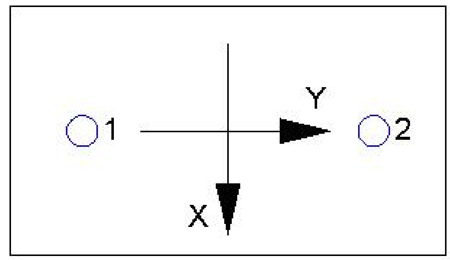
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2718.0	1678.0	0.0	1678.0
2	2718.0	1678.0	0.0	1678.0
Sum	5436.0	3356.0	0.0	3356.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 5436
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
408.24	324.00	1.000	1.000	1.00	1.000	12492	0.65	10231

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi (A_{Na} / A_{Na0}) \Psi_{ed,Na} \Psi_{g,Na} \Psi_{ec,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\,(A_{Vc} / A_{Vco})\,\Psi_{ec,V}\,\Psi_{ed,V}\,\Psi_{c,V}\,\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
648.00	648.00	1.000	0.961	1.000	1.000	15593	0.70	10490

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	15.66	23247

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\,\Psi_{c,V}\,\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
845.64	1103.56	1.000	1.000	1.000	23247	0.70	24939

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
408.24	324.00	1.000	1.000	1.000	1.000	12492	15740	0.70

ϕV_{cpg} (lb)
20601

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	2718	6071	0.45	Pass
Concrete breakout	5436	10231	0.53	Pass
Adhesive	**5436**	**8093**	**0.67**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**1678**	**3156**	**0.53**	**Pass (Governs)**
T Concrete breakout x+	3356	10490	0.32	Pass
|| Concrete breakout y-	1678	24939	0.07	Pass
Pryout	3356	20601	0.16	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.67	0.53	120.3 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.