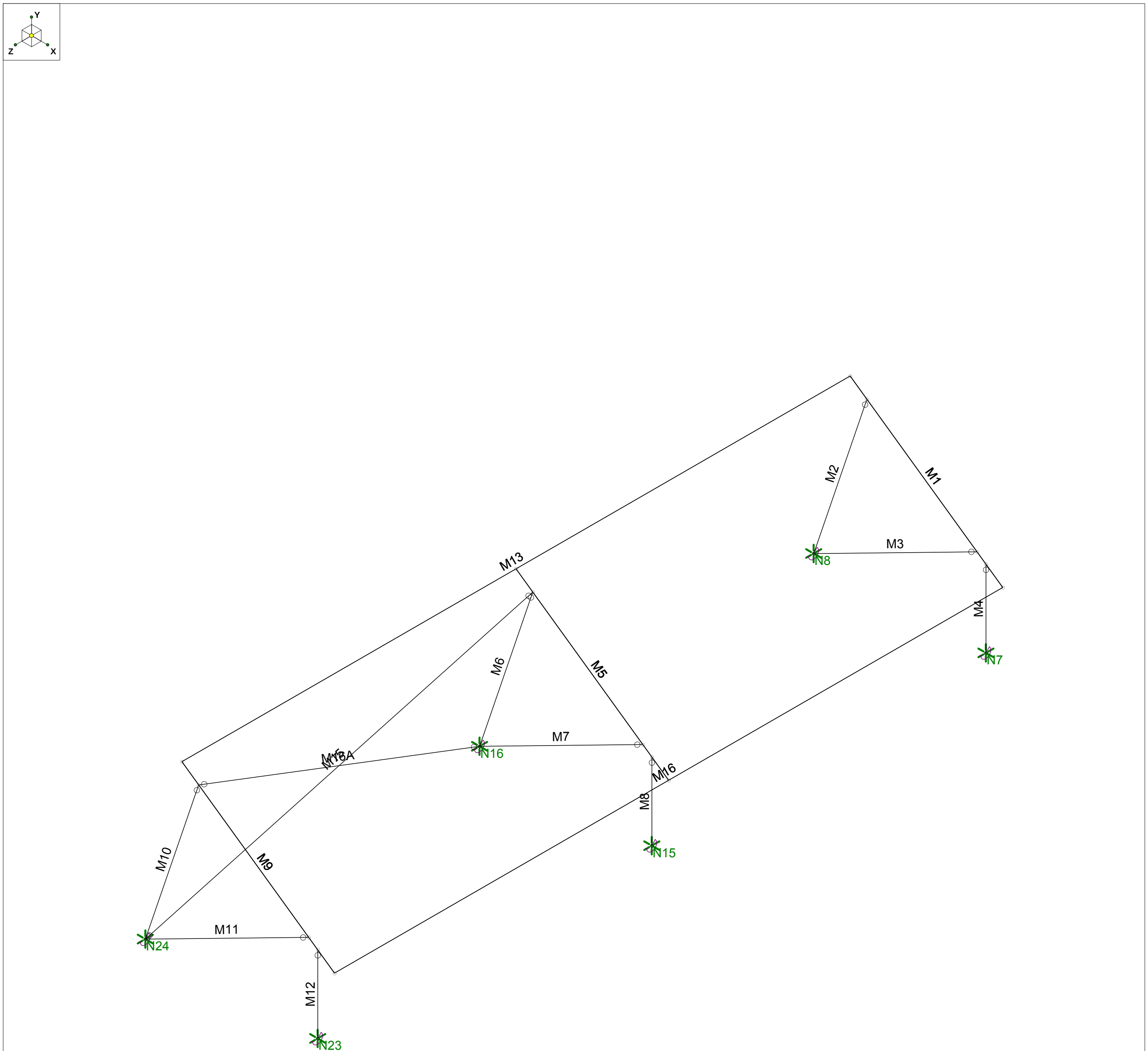


Schletter, Inc.		35° Tilt w/ Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

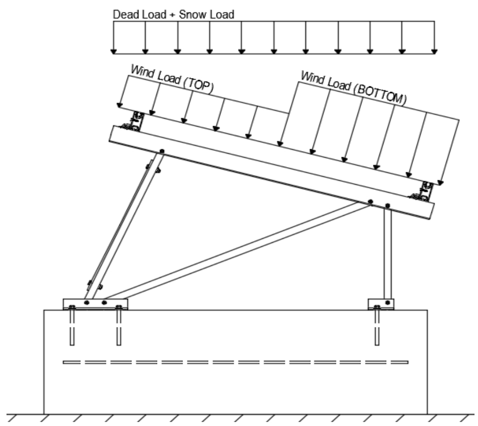
1.1 Project Description
The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

1.2 Construction
Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 1
Module Tilt = 35°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes
- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads
g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads
Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 14.43 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 0.64
C_e = 0.90
C_t = 1.20

2.3 Wind Loads
Design Wind Speed, V = 115 mph
Height ≤ 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 20.76 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.2	(Pressure)
$Cf+_{BOTTOM}$	=	2	
$Cf-_{TOP}$	=	-2.4	(Suction)
$Cf-_{BOTTOM}$	=	-1.2	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W ^{M}
1.54D + 1.3E + 0.2S ^{R}
0.56D + 1.3E ^{R}
1.54D + 1.25E + 0.2S ^{O}
0.56D + 1.25E ^{O}

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W ^{M}
1.238D + 0.875E ^{O}
1.1785D + 0.65625E + 0.75S ^{O}
0.362D + 0.875E ^{O}

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

^{M} *Uses the minimum allowable module dead load.*
^{R} *Include redundancy factor of 1.3.*
^{O} *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	Diagonal Struts	Location	Front Reactions	Location
M13	Top	M3	Outer	N7	Outer
M16	Bottom	M7	Inner	N15	Inner
		M11	Outer	N23	Outer

Girders	Location	Rear Struts	Location	Rear Reactions	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

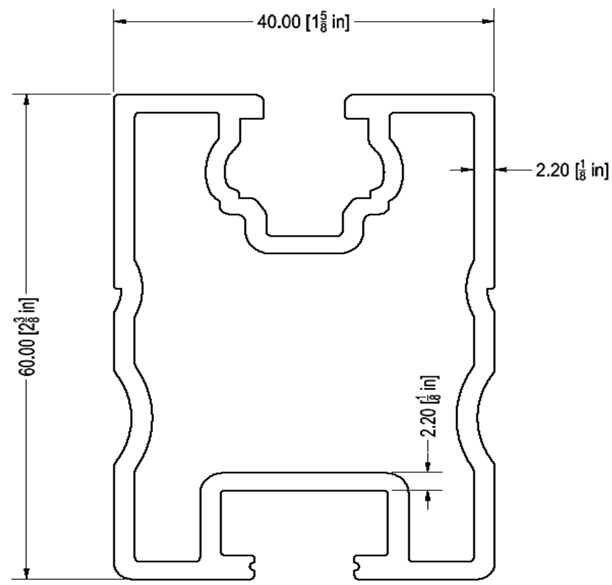
Front Struts	Location	Bracing
M4	Outer	M15
M8	Inner	M16A
M12	Outer	

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

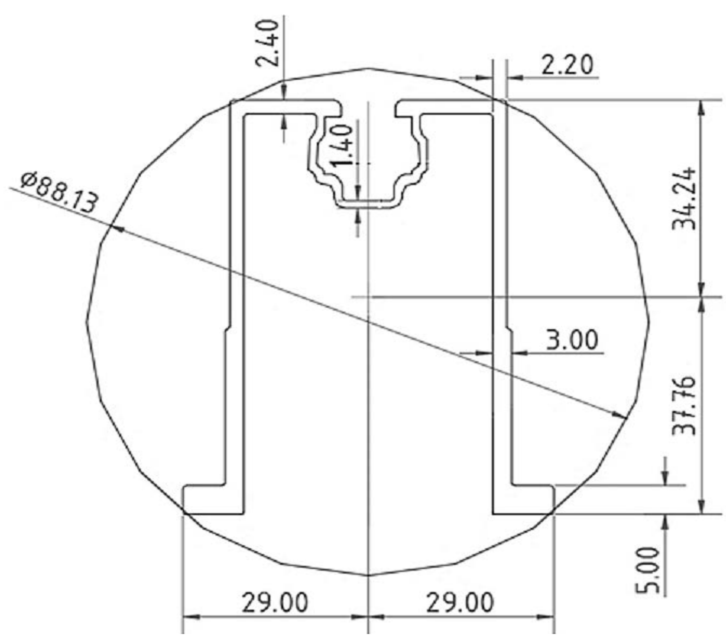
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	81	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	28.63	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	0.668	k-ft
M_z =	0.184	k-ft
$M_{y\ allowable}$ =	1.218	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	76%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

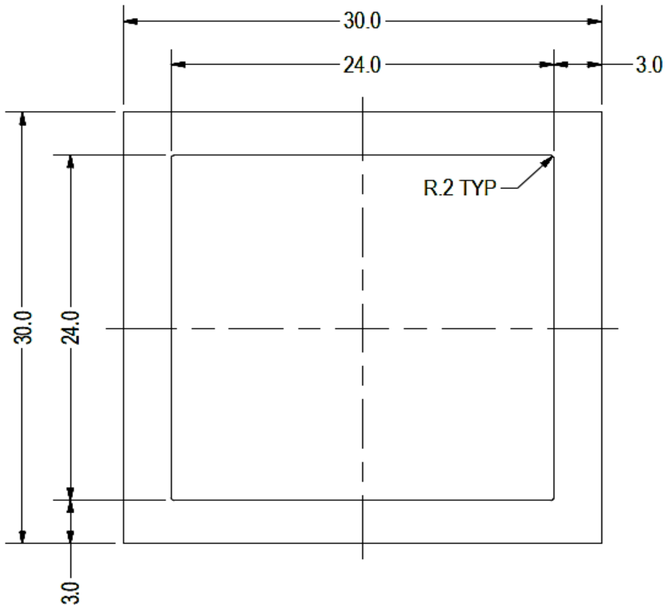
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.46	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	0.640	k-ft
M_z =	0.000	k-ft
P_n =	0.295	k
$M_{y\ allowable}$ =	1.446	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	47%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

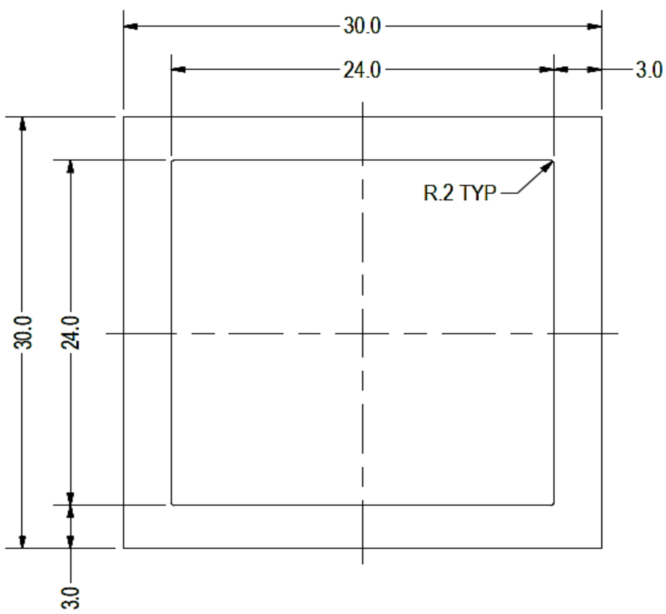
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.047	k-ft
P_n =	0.222	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	13%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

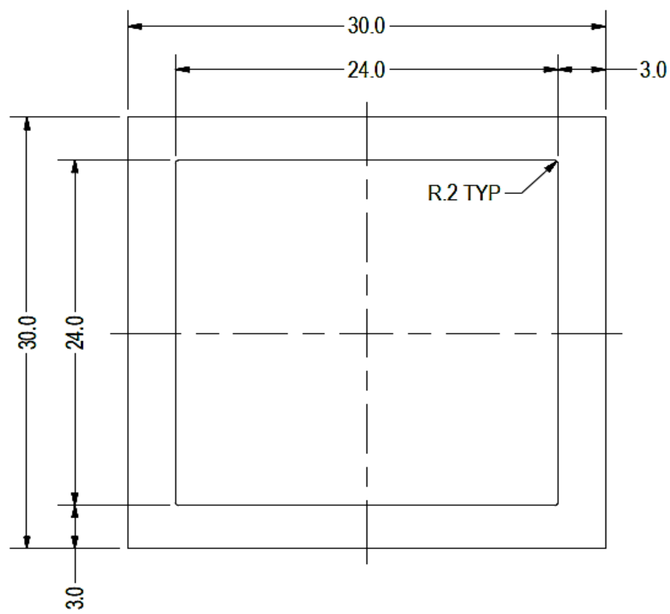
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.787	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	21%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

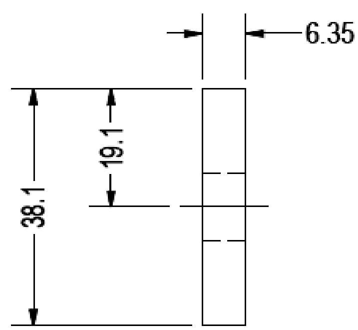
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	42.32	in
$\Phi F_{ty\ AXIAL}$ =	8.86	ksi
$\Phi F_{ty\ BENDING}$ =	29.96	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.811	k
$M_{y\ allowable}$ =	0.406	k-ft
$M_{z\ allowable}$ =	0.406	k-ft
$P_{n\ allowable}$ =	4.450	k
Utilization =	18%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.006	k-ft
P_n =	0.235	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	15%	



A cross brace kit is required every 13 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

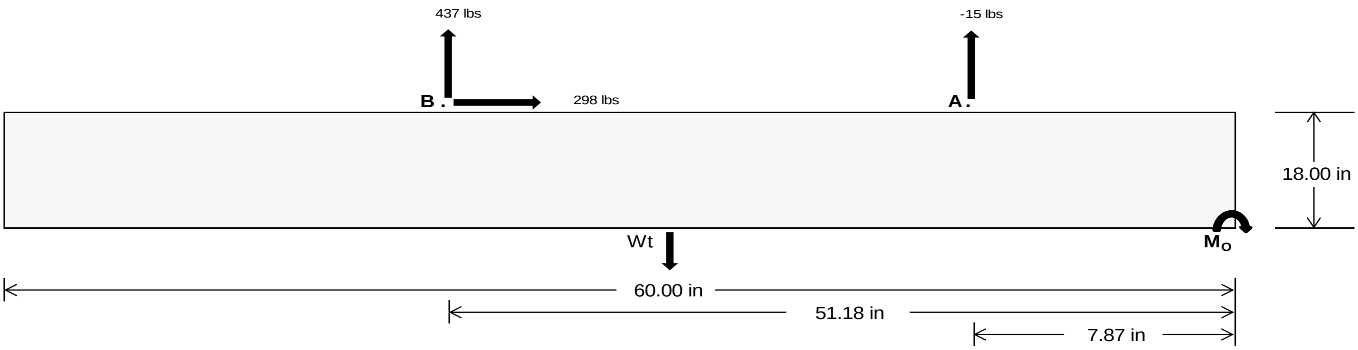
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	17.09	1900.04	k
Compressive Load =	1229.85	1368.90	k
Lateral Load =	38.29	1291.70	k
Moment (Weak Axis) =	0.06	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

Footing Reinforcement

Use fiber reinforcing with (1) #5 rebar.

Overturning Check

M_O =	27626.0 in-lbs
Resisting Force Required =	920.87 lbs
S.F. =	1.67
Weight Required =	1534.78 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.

Sliding

Force =	297.85 lbs
Friction =	0.4
Weight Required =	744.63 lbs
Resisting Weight =	1903.13 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion

Sliding Force =	297.85 lbs
Cohesion =	130 psf
Area =	8.75 ft^2
Resisting =	951.56 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	21 in	22 in	23 in	24 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.75 ft) =	1903 lbs	1994 lbs	2084 lbs	2175 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in
F_A	480 lbs	480 lbs	480 lbs	480 lbs	356 lbs	356 lbs	356 lbs	356 lbs	579 lbs	579 lbs	579 lbs	579 lbs	30 lbs	30 lbs	30 lbs	30 lbs
F_B	323 lbs	323 lbs	323 lbs	323 lbs	573 lbs	573 lbs	573 lbs	573 lbs	639 lbs	639 lbs	639 lbs	639 lbs	-875 lbs	-875 lbs	-875 lbs	-875 lbs
F_V	62 lbs	62 lbs	62 lbs	62 lbs	545 lbs	545 lbs	545 lbs	545 lbs	450 lbs	450 lbs	450 lbs	450 lbs	-596 lbs	-596 lbs	-596 lbs	-596 lbs
P_{total}	2707 lbs	2797 lbs	2888 lbs	2979 lbs	2833 lbs	2924 lbs	3014 lbs	3105 lbs	3121 lbs	3212 lbs	3303 lbs	3393 lbs	297 lbs	352 lbs	406 lbs	460 lbs
M	408 lbs-ft	408 lbs-ft	408 lbs-ft	408 lbs-ft	463 lbs-ft	463 lbs-ft	463 lbs-ft	463 lbs-ft	616 lbs-ft	616 lbs-ft	616 lbs-ft	616 lbs-ft	706 lbs-ft	706 lbs-ft	706 lbs-ft	706 lbs-ft
e	0.15 ft	0.15 ft	0.14 ft	0.14 ft	0.16 ft	0.16 ft	0.15 ft	0.15 ft	0.20 ft	0.19 ft	0.19 ft	0.18 ft	2.37 ft	2.01 ft	1.74 ft	1.53 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	253.3 psf	251.7 psf	250.2 psf	248.9 psf	260.2 psf	258.3 psf	256.5 psf	254.9 psf	272.3 psf	269.8 psf	267.5 psf	265.5 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	365.3 psf	358.6 psf	352.5 psf	346.8 psf	387.3 psf	379.6 psf	372.5 psf	366.1 psf	441.2 psf	431.0 psf	421.7 psf	413.2 psf	898.7 psf	259.3 psf	185.4 psf	158.7 psf

Maximum Bearing Pressure = 899 psf
Allowable Bearing Pressure = 1500 psf

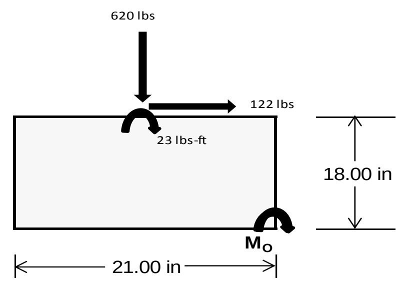
Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O =	335.8 ft-lbs
Resisting Force Required =	383.74 lbs
S.F. =	1.67
Weight Required =	639.56 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	21 in			21 in			21 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	145 lbs	132 lbs	82 lbs	293 lbs	620 lbs	245 lbs	88 lbs	-11 lbs	28 lbs
F_V	20 lbs	162 lbs	21 lbs	14 lbs	122 lbs	16 lbs	21 lbs	162 lbs	21 lbs
P_{total}	2502 lbs	2488 lbs	2438 lbs	2536 lbs	2863 lbs	2487 lbs	777 lbs	678 lbs	717 lbs
M	59 lbs-ft	275 lbs-ft	63 lbs-ft	39 lbs-ft	207 lbs-ft	50 lbs-ft	60 lbs-ft	274 lbs-ft	63 lbs-ft
e	0.02 ft	0.11 ft	0.03 ft	0.02 ft	0.07 ft	0.02 ft	0.08 ft	0.40 ft	0.09 ft
L/6	0.29 ft	1.53 ft	1.70 ft	1.72 ft	1.61 ft	1.71 ft	1.59 ft	0.94 ft	1.58 ft
f_{min}	262.9 sqft	176.7 sqft	254.1 sqft	274.8 sqft	246.2 sqft	264.8 sqft	65.2 sqft	-30.0 sqft	57.4 sqft
f_{max}	308.9 psf	392.0 psf	303.2 psf	304.9 psf	408.1 psf	303.7 psf	112.4 psf	185.0 psf	106.4 psf

Maximum Bearing Pressure = 408 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 21in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

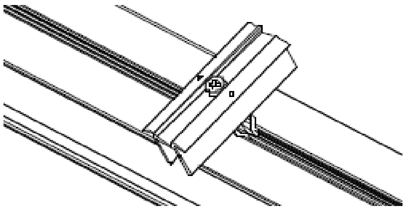
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

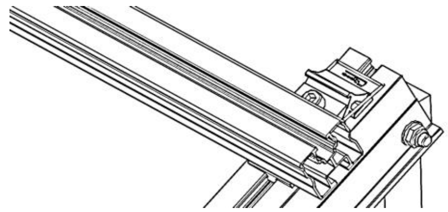
Fastening of Modules to Purlins

Maximum Uplifting Force =	0.464	k
Allowable Uplift =	1.214	k
Utilization =	38%	



Fastening of Purlins to Girders

Maximum Uplifting Force =	1.112	k
Allowable Uplift =	1.116	k
Utilization =	100%	



6.2 Bolted Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut

Maximum Axial Load =	0.946	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	17%	

Rear Strut

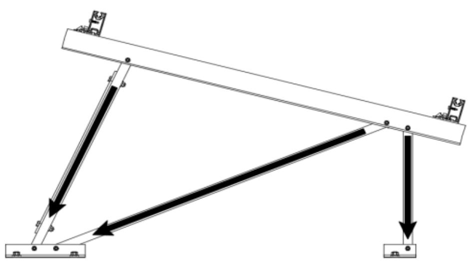
Maximum Axial Load =	1.189	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	21%	

Diagonal Strut

Maximum Axial Load =	0.787	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	14%	

Bracing

Maximum Axial Load =	0.235	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	3%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

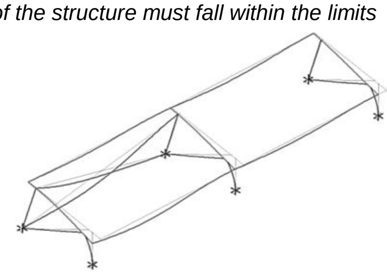
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	33.11	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	0.662	in
Max Drift, Δ_{MAX} =	0.099	in

$0.099 \leq 0.662$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus**

Strong Axis:

3.4.14

$L_b =$ 81.00 in

J = 0.255

210.919

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.6 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

$L_b =$ 81.00 in

J = 0.255

219.027

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.5

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 30

Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 28.6 ksi

Ix = 250988 mm^4

0.603 in^4

y = 30 mm

Sx = 0.511 in^3

$M_{max}St$ = 1.218 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 20

Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi

Iy = 120291 mm^4

0.289 in^4

x = 20 mm

Sy = 0.367 in^3

$M_{max}Wk$ = 0.871 k-ft

<u>Compression</u>

3.4.9

b/t = 7.4

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 23.9

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.47 ksi

A = 578.06 mm^2

0.90 in^2

P_{max} = 25.51 kips

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.13

23.1371

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b} Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.5 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.13

24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b} Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.5 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7

F_{UT}= (φbk2*√(BpE))/(5.1b/t)

F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

F_{ST}= φb[Bp-1.6Dp*b/t]

F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = 1.17φyFcy

φF_L = 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.5 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.446 k-ft

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.8

b/t = 24.46
S1 = 3.83
S2 = 10.30
φF_L= (φck2*√(BpE))/(5.1b/t)
φF_L= 10.4 ksi

3.4.9

b/t = 4.29
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 24.46
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.9.1

b/t = 24.46
t = 2.6
ds = 6.05
rs = 3.49
S = 21.70
ρst = 0.22
F_{UT}= 10.43
F_{ST}= 28.24
φF_L= Fut + (Fst - Fut)ρst < Fst
φF_L= 14.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 14.29 ksi
A = 576.21 mm^2
0.89 in^2
P_{max} = 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 31.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.2 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.423 k-ft

Compression

3.4.7

λ = 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83792

φF_L= φcc(Bc-Dc*λ)

φF_L= 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 24.52 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.404 k-ft

Weak Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.85841

φF_L= (φccFcy)/(λ²)

φF_L= 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 7.60 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 42.32 in

J = 0.16

111.025

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.0 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.0 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.406 k-ft

Weak Axis:

3.4.14

L_b = 42.32 in

J = 0.16

111.025

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.0

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.81475

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83406

φF_L= (φccFcy)/(λ²)

φF_L= 8.86409 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 8.86 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 4.45 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-40.249	-40.249	0	0
2	M16	Y	-40.249	-40.249	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-69.488	-69.488	0	0
2	M16	y	-115.813	-115.813	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	138.975	138.975	0	0
2	M16	y	69.488	69.488	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6																
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45																
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6														
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875														
14	LATERAL - ASD 1.1785D + 0.65..	Yes	Y		1	1.1...	3	.75			6	.656														
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875														

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	253.551	2	309.659	2	-.011	10	0	4	0	1	0	1
2		min	-310.321	3	-445.279	3	-2.288	4	0	3	0	1	0	1
3	N7	max	.027	3	377.896	1	-.208	10	0	12	0	1	0	1
4		min	-.169	2	24.915	15	-29.203	4	-.047	4	0	1	0	1
5	N15	max	.209	3	946.038	1	.653	1	.001	1	0	1	0	1
6		min	-1.678	2	33.251	15	-29.45	5	-.047	4	0	1	0	1
7	N16	max	929.339	2	1052.997	2	-.105	10	0	1	0	1	0	1
8		min	-993.612	3	-1461.571	3	-211.98	4	0	3	0	1	0	1
9	N23	max	.027	3	377.552	1	3.203	1	.006	1	0	1	0	1
10		min	-.169	2	8.204	15	-27.256	5	-.043	5	0	1	0	1
11	N24	max	253.963	2	313.661	2	58.408	3	.002	4	0	1	0	1
12		min	-310.517	3	-443.061	3	-3.749	5	0	3	0	1	0	1
13	Totals:	max	1434.838	2	3112.117	1	0	1						
14		min	-1614.188	3	-2138.873	3	-302.283	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	250.271	1	.676	6	1.405	4	0	10	0	12	0	1
2			min	-367.893	3	.158	15	-.034	3	0	1	0	1	0	1
3		2	max	250.405	1	.619	6	1.282	4	0	10	0	5	0	15
4			min	-367.792	3	.145	15	-.034	3	0	1	0	1	0	6
5		3	max	250.54	1	.561	6	1.159	4	0	10	0	5	0	15
6			min	-367.69	3	.131	15	-.034	3	0	1	0	1	0	6
7		4	max	250.675	1	.504	6	1.036	4	0	10	0	4	0	15
8			min	-367.589	3	.118	15	-.034	3	0	1	0	1	0	6
9		5	max	250.81	1	.446	6	.912	4	0	10	0	4	0	15
10			min	-367.488	3	.104	15	-.034	3	0	1	0	3	0	6
11		6	max	250.945	1	.389	6	.789	4	0	10	0	4	0	15
12			min	-367.387	3	.091	15	-.034	3	0	1	0	3	0	6
13		7	max	251.08	1	.331	6	.666	4	0	10	.001	4	0	15
14			min	-367.286	3	.077	15	-.034	3	0	1	0	3	0	6
15		8	max	251.215	1	.274	6	.543	4	0	10	.001	4	0	15
16			min	-367.185	3	.064	15	-.034	3	0	1	0	3	0	6
17		9	max	251.349	1	.216	6	.432	1	0	10	.001	4	0	15
18			min	-367.084	3	.05	15	-.034	3	0	1	0	3	0	6
19		10	max	251.484	1	.159	6	.432	1	0	10	.001	4	0	15
20			min	-366.982	3	.037	15	-.034	3	0	1	0	3	0	6
21		11	max	251.619	1	.109	2	.432	1	0	10	.001	4	0	15
22			min	-366.881	3	.016	12	-.034	3	0	1	0	3	0	6
23		12	max	251.754	1	.064	2	.432	1	0	10	.001	4	0	15
24			min	-366.78	3	-.013	3	-.062	5	0	1	0	3	0	6
25		13	max	251.889	1	.019	2	.432	1	0	10	.001	4	0	15
26			min	-366.679	3	-.047	3	-.185	5	0	1	0	3	0	6
27		14	max	252.024	1	-.017	15	.432	1	0	10	.001	4	0	15
28			min	-366.578	3	-.081	3	-.308	5	0	1	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	252.159	1	-.031	15	.432	1	0	10	.001	4	0	15
30			min	-366.477	3	-.129	4	-.432	5	0	1	0	3	0	6
31		16	max	252.294	1	-.044	15	.432	1	0	10	.001	4	0	15
32			min	-366.376	3	-.186	4	-.555	5	0	1	0	3	0	6
33		17	max	252.428	1	-.058	15	.432	1	0	10	.001	4	0	15
34			min	-366.274	3	-.244	4	-.678	5	0	1	0	3	0	6
35		18	max	252.563	1	-.071	15	.432	1	0	10	.001	1	0	15
36			min	-366.173	3	-.301	4	-.801	5	0	1	0	3	0	6
37		19	max	252.698	1	-.085	15	.432	1	0	10	.001	1	0	15
38			min	-366.072	3	-.359	4	-.924	5	0	1	0	3	0	6
39	M3	1	max	205.435	2	1.734	6	-.035	12	0	5	.002	1	0	6
40			min	-217.878	3	.407	15	-1.399	4	0	1	0	12	0	15
41		2	max	205.365	2	1.557	6	-.035	12	0	5	.002	1	0	2
42			min	-217.931	3	.366	15	-1.265	4	0	1	0	12	0	3
43		3	max	205.295	2	1.381	6	-.035	12	0	5	.001	1	0	2
44			min	-217.983	3	.324	15	-1.132	4	0	1	0	15	0	3
45		4	max	205.225	2	1.204	6	-.035	12	0	5	.001	1	0	15
46			min	-218.036	3	.283	15	-.998	4	0	1	0	5	0	4
47		5	max	205.155	2	1.028	6	-.035	12	0	5	.001	1	0	15
48			min	-218.088	3	.241	15	-.864	4	0	1	0	5	0	4
49		6	max	205.085	2	.852	6	-.035	12	0	5	.001	1	0	15
50			min	-218.141	3	.2	15	-.731	4	0	1	0	5	0	4
51		7	max	205.015	2	.675	6	-.035	12	0	5	.001	1	0	15
52			min	-218.193	3	.158	15	-.597	4	0	1	0	5	0	4
53		8	max	204.945	2	.499	6	-.035	12	0	5	0	1	0	15
54			min	-218.246	3	.117	15	-.484	1	0	1	0	5	-.001	4
55		9	max	204.875	2	.323	6	-.035	12	0	5	0	1	0	15
56			min	-218.298	3	.075	15	-.484	1	0	1	0	5	-.001	4
57		10	max	204.805	2	.146	6	-.035	12	0	5	0	1	0	15
58			min	-218.351	3	.034	15	-.484	1	0	1	0	5	-.001	4
59		11	max	204.735	2	.004	2	.049	5	0	5	0	1	0	15
60			min	-218.403	3	-.054	3	-.484	1	0	1	0	5	-.001	4
61		12	max	204.665	2	-.049	15	.182	5	0	5	0	1	0	15
62			min	-218.456	3	-.207	4	-.484	1	0	1	0	5	-.001	4
63		13	max	204.595	2	-.09	15	.316	5	0	5	0	1	0	15
64			min	-218.508	3	-.383	4	-.484	1	0	1	0	5	-.001	4
65		14	max	204.525	2	-.132	15	.45	5	0	5	0	1	0	15
66			min	-218.561	3	-.559	4	-.484	1	0	1	0	5	-.001	4
67		15	max	204.455	2	-.173	15	.583	5	0	5	0	1	0	15
68			min	-218.613	3	-.736	4	-.484	1	0	1	0	5	0	4
69		16	max	204.385	2	-.215	15	.717	5	0	5	0	1	0	15
70			min	-218.666	3	-.912	4	-.484	1	0	1	0	5	0	4
71		17	max	204.315	2	-.256	15	.851	5	0	5	0	12	0	15
72			min	-218.718	3	-1.088	4	-.484	1	0	1	0	5	0	4
73		18	max	204.245	2	-.298	15	.984	5	0	5	0	12	0	15
74			min	-218.771	3	-1.265	4	-.484	1	0	1	0	1	0	4
75		19	max	204.175	2	-.339	15	1.118	5	0	5	0	5	0	1
76			min	-218.823	3	-1.441	4	-.484	1	0	1	0	1	0	1
77	M4	1	max	376.731	1	0	1	-.212	10	0	1	0	5	0	1
78			min	24.564	15	0	1	-28.73	4	0	1	0	2	0	1
79		2	max	376.796	1	0	1	-.212	10	0	1	0	12	0	1
80			min	24.583	15	0	1	-28.786	4	0	1	-.003	4	0	1
81		3	max	376.86	1	0	1	-.212	10	0	1	0	12	0	1
82			min	24.603	15	0	1	-28.842	4	0	1	-.005	4	0	1
83		4	max	376.925	1	0	1	-.212	10	0	1	0	12	0	1
84			min	24.622	15	0	1	-28.898	4	0	1	-.008	4	0	1
85		5	max	376.99	1	0	1	-.212	10	0	1	0	12	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	24.642	15	0	1	-28.954	4	0	1	-.01	4	0	1
87		6	max	377.054	1	0	1	-.212	10	0	1	0	12	0	1
88			min	24.661	15	0	1	-29.01	4	0	1	-.013	4	0	1
89		7	max	377.119	1	0	1	-.212	10	0	1	0	12	0	1
90			min	24.681	15	0	1	-29.066	4	0	1	-.015	4	0	1
91		8	max	377.184	1	0	1	-.212	10	0	1	0	12	0	1
92			min	24.7	15	0	1	-29.122	4	0	1	-.018	4	0	1
93		9	max	377.248	1	0	1	-.212	10	0	1	0	12	0	1
94			min	24.72	15	0	1	-29.178	4	0	1	-.021	4	0	1
95		10	max	377.313	1	0	1	-.212	10	0	1	0	12	0	1
96			min	24.739	15	0	1	-29.234	4	0	1	-.023	4	0	1
97		11	max	377.378	1	0	1	-.212	10	0	1	0	12	0	1
98			min	24.759	15	0	1	-29.291	4	0	1	-.026	4	0	1
99		12	max	377.443	1	0	1	-.212	10	0	1	0	12	0	1
100			min	24.778	15	0	1	-29.347	4	0	1	-.029	4	0	1
101		13	max	377.507	1	0	1	-.212	10	0	1	0	12	0	1
102			min	24.798	15	0	1	-29.403	4	0	1	-.031	4	0	1
103		14	max	377.572	1	0	1	-.212	10	0	1	0	12	0	1
104			min	24.817	15	0	1	-29.459	4	0	1	-.034	4	0	1
105		15	max	377.637	1	0	1	-.212	10	0	1	0	12	0	1
106			min	24.837	15	0	1	-29.515	4	0	1	-.036	4	0	1
107		16	max	377.701	1	0	1	-.212	10	0	1	0	12	0	1
108			min	24.856	15	0	1	-29.571	4	0	1	-.039	4	0	1
109		17	max	377.766	1	0	1	-.212	10	0	1	0	12	0	1
110			min	24.876	15	0	1	-29.627	4	0	1	-.042	4	0	1
111		18	max	377.831	1	0	1	-.212	10	0	1	0	12	0	1
112			min	24.895	15	0	1	-29.683	4	0	1	-.044	4	0	1
113		19	max	377.896	1	0	1	-.212	10	0	1	0	12	0	1
114			min	24.915	15	0	1	-29.739	4	0	1	-.047	4	0	1
115	M6	1	max	808.612	1	.664	6	1.274	4	0	3	0	3	0	1
116			min	-1188.565	3	.148	15	-.163	3	0	5	0	1	0	1
117		2	max	808.747	1	.607	6	1.151	4	0	3	0	4	0	15
118			min	-1188.464	3	.134	15	-.163	3	0	5	0	11	0	6
119		3	max	808.882	1	.549	6	1.027	4	0	3	0	4	0	15
120			min	-1188.363	3	.121	15	-.163	3	0	5	0	11	0	6
121		4	max	809.017	1	.493	2	.904	4	0	3	0	4	0	15
122			min	-1188.262	3	.107	15	-.163	3	0	5	0	10	0	6
123		5	max	809.152	1	.448	2	.781	4	0	3	0	4	0	15
124			min	-1188.161	3	.094	15	-.163	3	0	5	0	10	0	6
125		6	max	809.287	1	.403	2	.658	4	0	3	.001	4	0	15
126			min	-1188.06	3	.076	12	-.163	3	0	5	0	10	0	6
127		7	max	809.422	1	.359	2	.535	4	0	3	.001	4	0	15
128			min	-1187.959	3	.054	12	-.163	3	0	5	0	10	0	2
129		8	max	809.556	1	.314	2	.412	4	0	3	.001	4	0	15
130			min	-1187.857	3	.032	12	-.163	3	0	5	0	3	0	2
131		9	max	809.691	1	.269	2	.288	4	0	3	.001	4	0	15
132			min	-1187.756	3	.001	3	-.163	3	0	5	0	3	0	2
133		10	max	809.826	1	.224	2	.165	4	0	3	.001	4	0	15
134			min	-1187.655	3	-.032	3	-.163	3	0	5	0	3	0	2
135		11	max	809.961	1	.179	2	.137	1	0	3	.001	4	0	12
136			min	-1187.554	3	-.066	3	-.163	3	0	5	0	3	0	2
137		12	max	810.096	1	.135	2	.137	1	0	3	.001	4	0	12
138			min	-1187.453	3	-.1	3	-.163	3	0	5	0	3	0	2
139		13	max	810.231	1	.09	2	.137	1	0	3	.001	4	0	12
140			min	-1187.352	3	-.133	3	-.244	5	0	5	0	3	0	2
141		14	max	810.366	1	.045	2	.137	1	0	3	.001	4	0	12
142			min	-1187.251	3	-.167	3	-.368	5	0	5	0	3	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	810.501	1	0	2	.137	1	0	3	.001	4	0	12
144			min	-1187.149	3	-.2	3	-.491	5	0	5	0	3	0	2
145		16	max	810.635	1	-.045	2	.137	1	0	3	.001	4	0	3
146			min	-1187.048	3	-.234	3	-.614	5	0	5	0	3	0	2
147		17	max	810.77	1	-.069	15	.137	1	0	3	.001	4	0	3
148			min	-1186.947	3	-.268	3	-.737	5	0	5	0	3	0	2
149		18	max	810.905	1	-.082	15	.137	1	0	3	0	4	0	3
150			min	-1186.846	3	-.314	4	-.86	5	0	5	0	3	0	2
151		19	max	811.04	1	-.096	15	.137	1	0	3	0	4	0	3
152			min	-1186.745	3	-.371	4	-.983	5	0	5	0	3	0	2
153	M7	1	max	787.071	2	1.756	4	.03	3	0	14	0	4	0	2
154			min	-682.521	3	.42	15	-1.291	5	0	3	0	3	0	3
155		2	max	787.001	2	1.58	4	.03	3	0	14	0	4	0	2
156			min	-682.573	3	.378	15	-1.157	5	0	3	0	3	0	3
157		3	max	786.931	2	1.403	4	.03	3	0	14	0	2	0	2
158			min	-682.626	3	.337	15	-1.023	5	0	3	0	3	0	3
159		4	max	786.861	2	1.227	4	.03	3	0	14	0	2	0	2
160			min	-682.678	3	.295	15	-.89	5	0	3	0	5	0	3
161		5	max	786.791	2	1.051	4	.03	3	0	14	0	2	0	15
162			min	-682.731	3	.254	15	-.756	5	0	3	0	5	0	3
163		6	max	786.721	2	.874	4	.03	3	0	14	0	2	0	15
164			min	-682.783	3	.212	15	-.622	5	0	3	0	5	0	3
165		7	max	786.651	2	.698	4	.03	3	0	14	0	2	0	15
166			min	-682.836	3	.171	15	-.489	5	0	3	0	5	0	6
167		8	max	786.581	2	.521	4	.03	3	0	14	0	2	0	15
168			min	-682.888	3	.122	12	-.355	5	0	3	0	5	-.001	6
169		9	max	786.511	2	.349	2	.03	3	0	14	0	2	0	15
170			min	-682.941	3	.054	12	-.221	5	0	3	0	5	-.001	6
171		10	max	786.441	2	.212	2	.03	3	0	14	0	2	0	15
172			min	-682.993	3	-.035	3	-.088	5	0	3	0	5	-.001	6
173		11	max	786.371	2	.075	2	.047	4	0	14	0	2	0	15
174			min	-683.046	3	-.138	3	-.008	2	0	3	0	5	-.001	6
175		12	max	786.301	2	-.036	15	.181	4	0	14	0	2	0	15
176			min	-683.098	3	-.241	3	-.008	2	0	3	0	5	-.001	6
177		13	max	786.231	2	-.078	15	.315	4	0	14	0	2	0	15
178			min	-683.151	3	-.361	6	-.008	2	0	3	0	5	-.001	6
179		14	max	786.161	2	-.119	15	.448	4	0	14	0	11	0	15
180			min	-683.203	3	-.537	6	-.008	2	0	3	0	5	-.001	6
181		15	max	786.091	2	-.161	15	.582	4	0	14	0	11	0	15
182			min	-683.256	3	-.714	6	-.008	2	0	3	0	5	0	6
183		16	max	786.021	2	-.202	15	.716	4	0	14	0	11	0	15
184			min	-683.308	3	-.89	6	-.008	2	0	3	0	5	0	6
185		17	max	785.951	2	-.244	15	.849	4	0	14	0	11	0	15
186			min	-683.361	3	-1.067	6	-.008	2	0	3	0	5	0	6
187		18	max	785.881	2	-.285	15	.983	4	0	14	0	1	0	15
188			min	-683.413	3	-1.243	6	-.008	2	0	3	0	3	0	6
189		19	max	785.811	2	-.327	15	1.117	4	0	14	0	14	0	1
190			min	-683.466	3	-1.419	6	-.008	2	0	3	0	3	0	1
191	M8	1	max	944.874	1	0	1	.771	1	0	1	0	4	0	1
192			min	32.9	15	0	1	-28.749	4	0	1	0	1	0	1
193		2	max	944.938	1	0	1	.771	1	0	1	0	1	0	1
194			min	32.919	15	0	1	-28.805	4	0	1	-.003	4	0	1
195		3	max	945.003	1	0	1	.771	1	0	1	0	1	0	1
196			min	32.939	15	0	1	-28.861	4	0	1	-.005	4	0	1
197		4	max	945.068	1	0	1	.771	1	0	1	0	1	0	1
198			min	32.958	15	0	1	-28.917	4	0	1	-.008	4	0	1
199		5	max	945.133	1	0	1	.771	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	32.978	15	0	1	-28.974	4	0	1	-.01	4	0	1
201		6	max	945.197	1	0	1	.771	1	0	1	0	1	0	1
202			min	32.997	15	0	1	-29.03	4	0	1	-.013	4	0	1
203		7	max	945.262	1	0	1	.771	1	0	1	0	1	0	1
204			min	33.017	15	0	1	-29.086	4	0	1	-.015	4	0	1
205		8	max	945.327	1	0	1	.771	1	0	1	0	1	0	1
206			min	33.036	15	0	1	-29.142	4	0	1	-.018	4	0	1
207		9	max	945.391	1	0	1	.771	1	0	1	0	1	0	1
208			min	33.056	15	0	1	-29.198	4	0	1	-.021	4	0	1
209		10	max	945.456	1	0	1	.771	1	0	1	0	1	0	1
210			min	33.075	15	0	1	-29.254	4	0	1	-.023	4	0	1
211		11	max	945.521	1	0	1	.771	1	0	1	0	1	0	1
212			min	33.095	15	0	1	-29.31	4	0	1	-.026	4	0	1
213		12	max	945.585	1	0	1	.771	1	0	1	0	1	0	1
214			min	33.114	15	0	1	-29.366	4	0	1	-.029	4	0	1
215		13	max	945.65	1	0	1	.771	1	0	1	0	1	0	1
216			min	33.134	15	0	1	-29.422	4	0	1	-.031	4	0	1
217		14	max	945.715	1	0	1	.771	1	0	1	0	1	0	1
218			min	33.153	15	0	1	-29.478	4	0	1	-.034	4	0	1
219		15	max	945.78	1	0	1	.771	1	0	1	0	1	0	1
220			min	33.173	15	0	1	-29.534	4	0	1	-.036	4	0	1
221		16	max	945.844	1	0	1	.771	1	0	1	.001	1	0	1
222			min	33.192	15	0	1	-29.59	4	0	1	-.039	4	0	1
223		17	max	945.909	1	0	1	.771	1	0	1	.001	1	0	1
224			min	33.212	15	0	1	-29.646	4	0	1	-.042	4	0	1
225		18	max	945.974	1	0	1	.771	1	0	1	.001	1	0	1
226			min	33.231	15	0	1	-29.703	4	0	1	-.044	4	0	1
227		19	max	946.038	1	0	1	.771	1	0	1	.001	1	0	1
228			min	33.251	15	0	1	-29.759	4	0	1	-.047	4	0	1
229	M10	1	max	259.781	1	.707	4	1.442	5	0	1	0	1	0	1
230			min	-336.233	3	.179	15	-.185	1	-.002	5	0	5	0	1
231		2	max	259.916	1	.65	4	1.319	5	0	1	0	1	0	15
232			min	-336.132	3	.166	15	-.185	1	-.002	5	0	3	0	4
233		3	max	260.051	1	.592	4	1.196	5	0	1	0	4	0	15
234			min	-336.031	3	.152	15	-.185	1	-.002	5	0	3	0	4
235		4	max	260.186	1	.535	4	1.072	5	0	1	0	4	0	15
236			min	-335.929	3	.139	15	-.185	1	-.002	5	0	3	0	4
237		5	max	260.321	1	.477	4	.949	5	0	1	0	4	0	15
238			min	-335.828	3	.125	15	-.185	1	-.002	5	0	3	0	4
239		6	max	260.456	1	.42	4	.826	5	0	1	0	4	0	15
240			min	-335.727	3	.112	15	-.185	1	-.002	5	0	3	0	4
241		7	max	260.591	1	.362	4	.703	5	0	1	.001	4	0	15
242			min	-335.626	3	.098	15	-.185	1	-.002	5	0	3	0	4
243		8	max	260.725	1	.305	4	.58	5	0	1	.001	4	0	15
244			min	-335.525	3	.085	15	-.185	1	-.002	5	0	3	0	4
245		9	max	260.86	1	.247	4	.457	5	0	1	.001	4	0	15
246			min	-335.424	3	.071	15	-.185	1	-.002	5	0	3	0	4
247		10	max	260.995	1	.19	4	.333	5	0	1	.001	4	0	15
248			min	-335.323	3	.052	12	-.185	1	-.002	5	0	3	0	4
249		11	max	261.13	1	.132	4	.21	5	0	1	.001	4	0	15
250			min	-335.221	3	.03	12	-.185	1	-.002	5	0	3	0	4
251		12	max	261.265	1	.075	4	.087	5	0	1	.001	4	0	15
252			min	-335.12	3	.008	12	-.185	1	-.002	5	0	3	0	4
253		13	max	261.4	1	.025	5	.006	3	0	1	.001	4	0	15
254			min	-335.019	3	-.024	3	-.185	1	-.002	5	0	3	0	4
255		14	max	261.535	1	.004	5	.006	3	0	1	.001	4	0	15
256			min	-334.918	3	-.066	1	-.193	4	-.002	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	261.669	1	-.01	15	.006	3	0	1	.001	5	0	15
258			min	-334.817	3	-.11	1	-.317	4	-.002	5	0	3	0	4
259		16	max	261.804	1	-.023	15	.006	3	0	1	.001	5	0	15
260			min	-334.716	3	-.156	6	-.44	4	-.002	5	0	1	0	4
261		17	max	261.939	1	-.037	15	.006	3	0	1	.001	5	0	15
262			min	-334.614	3	-.214	6	-.563	4	-.002	5	0	1	0	4
263		18	max	262.074	1	-.05	15	.006	3	0	1	.001	5	0	12
264			min	-334.513	3	-.271	6	-.686	4	-.002	5	0	1	0	4
265		19	max	262.209	1	-.064	15	.006	3	0	1	0	5	0	12
266			min	-334.412	3	-.329	6	-.809	4	-.002	5	0	1	0	4
267	M11	1	max	205.12	2	1.721	6	.549	1	.002	4	0	5	0	1
268			min	-218.539	3	.398	15	-1.216	5	0	10	-.002	1	0	15
269		2	max	205.05	2	1.545	6	.549	1	.002	4	0	5	0	1
270			min	-218.592	3	.357	15	-1.082	5	0	10	-.002	1	0	3
271		3	max	204.98	2	1.368	6	.549	1	.002	4	0	5	0	1
272			min	-218.644	3	.315	15	-.949	5	0	10	-.001	1	0	3
273		4	max	204.91	2	1.192	6	.549	1	.002	4	0	3	0	15
274			min	-218.697	3	.274	15	-.815	5	0	10	-.001	1	0	4
275		5	max	204.84	2	1.015	6	.549	1	.002	4	0	3	0	15
276			min	-218.749	3	.232	15	-.681	5	0	10	-.001	1	0	4
277		6	max	204.77	2	.839	6	.549	1	.002	4	0	3	0	15
278			min	-218.802	3	.191	15	-.548	5	0	10	-.001	1	0	4
279		7	max	204.7	2	.663	6	.549	1	.002	4	0	3	0	15
280			min	-218.854	3	.149	15	-.414	5	0	10	-.001	1	-.001	4
281		8	max	204.63	2	.486	6	.549	1	.002	4	0	3	0	15
282			min	-218.907	3	.108	15	-.28	5	0	10	0	1	-.001	4
283		9	max	204.56	2	.31	6	.549	1	.002	4	0	3	0	15
284			min	-218.959	3	.066	15	-.147	5	0	10	0	1	-.001	4
285		10	max	204.49	2	.143	1	.549	1	.002	4	0	3	0	15
286			min	-219.012	3	.025	15	-.02	3	0	10	0	1	-.001	4
287		11	max	204.42	2	.005	1	.549	1	.002	4	0	3	0	15
288			min	-219.064	3	-.071	3	-.02	3	0	10	0	1	-.001	4
289		12	max	204.35	2	-.058	15	.549	1	.002	4	0	3	0	15
290			min	-219.117	3	-.22	4	-.02	3	0	10	0	1	-.001	4
291		13	max	204.28	2	-.099	15	.549	1	.002	4	0	3	0	15
292			min	-219.169	3	-.396	4	-.02	3	0	10	0	1	-.001	4
293		14	max	204.21	2	-.141	15	.643	4	.002	4	0	3	0	15
294			min	-219.222	3	-.572	4	-.02	3	0	10	0	1	-.001	4
295		15	max	204.14	2	-.182	15	.777	4	.002	4	0	3	0	15
296			min	-219.274	3	-.749	4	-.02	3	0	10	0	1	0	4
297		16	max	204.07	2	-.224	15	.91	4	.002	4	0	3	0	15
298			min	-219.327	3	-.925	4	-.02	3	0	10	0	10	0	4
299		17	max	204	2	-.265	15	1.044	4	.002	4	0	4	0	15
300			min	-219.379	3	-1.102	4	-.02	3	0	10	0	10	0	4
301		18	max	203.93	2	-.307	15	1.178	4	.002	4	0	4	0	15
302			min	-219.432	3	-1.278	4	-.02	3	0	10	0	10	0	4
303		19	max	203.86	2	-.348	15	1.311	4	.002	4	0	4	0	1
304			min	-219.484	3	-1.454	4	-.02	3	0	10	0	10	0	1
305	M12	1	max	376.387	1	0	1	3.415	1	0	1	0	4	0	1
306			min	7.853	15	0	1	-26.303	5	0	1	0	3	0	1
307		2	max	376.452	1	0	1	3.415	1	0	1	0	1	0	1
308			min	7.872	15	0	1	-26.359	5	0	1	-.002	5	0	1
309		3	max	376.517	1	0	1	3.415	1	0	1	0	1	0	1
310			min	7.892	15	0	1	-26.415	5	0	1	-.005	5	0	1
311		4	max	376.581	1	0	1	3.415	1	0	1	0	1	0	1
312			min	7.911	15	0	1	-26.471	5	0	1	-.007	5	0	1
313		5	max	376.646	1	0	1	3.415	1	0	1	.001	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	7.931	15	0	1	-26.527	5	0	1	-.009	5	0	1
315		6	max	376.711	1	0	1	3.415	1	0	1	.002	1	0	1
316			min	7.95	15	0	1	-26.583	5	0	1	-.012	5	0	1
317		7	max	376.775	1	0	1	3.415	1	0	1	.002	1	0	1
318			min	7.97	15	0	1	-26.639	5	0	1	-.014	5	0	1
319		8	max	376.84	1	0	1	3.415	1	0	1	.002	1	0	1
320			min	7.989	15	0	1	-26.695	5	0	1	-.017	5	0	1
321		9	max	376.905	1	0	1	3.415	1	0	1	.002	1	0	1
322			min	8.009	15	0	1	-26.751	5	0	1	-.019	5	0	1
323		10	max	376.969	1	0	1	3.415	1	0	1	.003	1	0	1
324			min	8.029	15	0	1	-26.807	5	0	1	-.021	5	0	1
325		11	max	377.034	1	0	1	3.415	1	0	1	.003	1	0	1
326			min	8.048	15	0	1	-26.864	5	0	1	-.024	5	0	1
327		12	max	377.099	1	0	1	3.415	1	0	1	.003	1	0	1
328			min	8.068	15	0	1	-26.92	5	0	1	-.026	5	0	1
329		13	max	377.164	1	0	1	3.415	1	0	1	.004	1	0	1
330			min	8.087	15	0	1	-26.976	5	0	1	-.029	5	0	1
331		14	max	377.228	1	0	1	3.415	1	0	1	.004	1	0	1
332			min	8.107	15	0	1	-27.032	5	0	1	-.031	5	0	1
333		15	max	377.293	1	0	1	3.415	1	0	1	.004	1	0	1
334			min	8.126	15	0	1	-27.088	5	0	1	-.033	5	0	1
335		16	max	377.358	1	0	1	3.415	1	0	1	.005	1	0	1
336			min	8.146	15	0	1	-27.144	5	0	1	-.036	5	0	1
337		17	max	377.422	1	0	1	3.415	1	0	1	.005	1	0	1
338			min	8.165	15	0	1	-27.2	5	0	1	-.038	5	0	1
339		18	max	377.487	1	0	1	3.415	1	0	1	.005	1	0	1
340			min	8.185	15	0	1	-27.256	5	0	1	-.041	5	0	1
341		19	max	377.552	1	0	1	3.415	1	0	1	.006	1	0	1
342			min	8.204	15	0	1	-27.312	5	0	1	-.043	5	0	1
343	M1	1	max	139.552	1	343.696	3	-4.092	12	0	1	.134	1	0	2
344			min	7.324	12	-247.179	1	-67.78	1	0	3	.009	12	0	3
345		2	max	139.712	1	343.524	3	-4.092	12	0	1	.119	1	.054	1
346			min	7.404	12	-247.408	1	-67.78	1	0	3	.008	12	-.075	3
347		3	max	116.94	3	6.523	9	-4.115	12	0	12	.103	1	.107	1
348			min	-15.095	10	-28.599	2	-67.693	1	0	1	.007	12	-.148	3
349		4	max	117.06	3	6.332	9	-4.115	12	0	12	.089	1	.111	2
350			min	-14.961	10	-28.828	2	-67.693	1	0	1	.006	12	-.146	3
351		5	max	117.18	3	6.142	9	-4.115	12	0	12	.074	1	.117	2
352			min	-14.828	10	-29.057	2	-67.693	1	0	1	.005	12	-.144	3
353		6	max	117.3	3	5.951	9	-4.115	12	0	12	.059	1	.124	2
354			min	-14.694	10	-29.286	2	-67.693	1	0	1	.004	12	-.142	3
355		7	max	117.42	3	5.76	9	-4.115	12	0	12	.044	1	.13	2
356			min	-14.561	10	-29.514	2	-67.693	1	0	1	.003	12	-.14	3
357		8	max	117.54	3	5.57	9	-4.115	12	0	12	.03	1	.137	2
358			min	-14.427	10	-29.743	2	-67.693	1	0	1	.003	12	-.137	3
359		9	max	117.66	3	5.379	9	-4.115	12	0	12	.015	1	.143	2
360			min	-14.294	10	-29.972	2	-67.693	1	0	1	.002	10	-.135	3
361		10	max	117.781	3	5.189	9	-4.115	12	0	12	.002	4	.15	2
362			min	-14.16	10	-30.201	2	-67.693	1	0	1	0	10	-.133	3
363		11	max	117.901	3	4.998	9	-4.115	12	0	12	0	3	.156	2
364			min	-14.027	10	-30.429	2	-67.693	1	0	1	-.014	1	-.131	3
365		12	max	118.021	3	4.807	9	-4.115	12	0	12	-.001	12	.163	2
366			min	-13.893	10	-30.658	2	-67.693	1	0	1	-.029	1	-.129	3
367		13	max	118.141	3	4.617	9	-4.115	12	0	12	-.002	12	.169	2
368			min	-13.76	10	-30.887	2	-67.693	1	0	1	-.044	1	-.126	3
369		14	max	118.261	3	4.426	9	-4.115	12	0	12	-.003	12	.176	2
370			min	-13.627	10	-31.115	2	-67.693	1	0	1	-.058	1	-.124	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	118.381	3	4.236	9	-4.115	12	0	12	-.004	12	.183	2
372			min	-13.493	10	-31.344	2	-67.693	1	0	1	-.073	1	-.121	3
373		16	max	92.421	2	148.547	2	-4.152	12	0	1	-.005	12	.188	2
374			min	2.765	15	-204.991	3	-68.088	1	0	5	-.088	1	-.117	3
375		17	max	92.581	2	148.318	2	-4.152	12	0	1	-.006	12	.156	2
376			min	2.813	15	-205.163	3	-68.088	1	0	5	-.103	1	-.073	3
377		18	max	-6.563	12	361.084	2	-4.372	12	0	3	-.006	12	.079	2
378			min	-139.403	1	-167.186	3	-69.819	1	0	2	-.118	1	-.036	3
379		19	max	-6.483	12	360.855	2	-4.372	12	0	3	-.007	12	0	2
380			min	-139.243	1	-167.358	3	-69.819	1	0	2	-.133	1	0	3
381	M5	1	max	307.906	1	1134.094	3	-.036	10	0	1	.04	4	0	3
382			min	10.891	15	-816.354	1	-52.155	3	0	5	0	10	0	2
383		2	max	308.066	1	1133.923	3	-.036	10	0	1	.035	4	.177	1
384			min	10.94	15	-816.583	1	-52.155	3	0	5	-.006	3	-.246	3
385		3	max	365.846	3	5.51	9	5.992	3	0	3	.029	4	.351	1
386			min	-76.513	2	-105.42	2	-21.862	4	0	4	-.016	3	-.486	3
387		4	max	365.966	3	5.32	9	5.992	3	0	3	.024	4	.367	2
388			min	-76.353	2	-105.649	2	-21.62	4	0	4	-.015	3	-.479	3
389		5	max	366.087	3	5.129	9	5.992	3	0	3	.02	4	.39	2
390			min	-76.193	2	-105.877	2	-21.378	4	0	4	-.014	3	-.471	3
391		6	max	366.207	3	4.938	9	5.992	3	0	3	.015	4	.413	2
392			min	-76.033	2	-106.106	2	-21.136	4	0	4	-.012	3	-.463	3
393		7	max	366.327	3	4.748	9	5.992	3	0	3	.01	4	.436	2
394			min	-75.873	2	-106.335	2	-20.894	4	0	4	-.011	3	-.455	3
395		8	max	366.447	3	4.557	9	5.992	3	0	3	.006	4	.459	2
396			min	-75.713	2	-106.564	2	-20.652	4	0	4	-.01	3	-.447	3
397		9	max	366.567	3	4.367	9	5.992	3	0	3	.002	4	.483	2
398			min	-75.552	2	-106.792	2	-20.41	4	0	4	-.009	3	-.439	3
399		10	max	366.687	3	4.176	9	5.992	3	0	3	0	10	.506	2
400			min	-75.392	2	-107.021	2	-20.168	4	0	4	-.007	3	-.431	3
401		11	max	366.807	3	3.985	9	5.992	3	0	3	0	10	.529	2
402			min	-75.232	2	-107.25	2	-19.926	4	0	4	-.007	4	-.423	3
403		12	max	366.927	3	3.795	9	5.992	3	0	3	0	10	.552	2
404			min	-75.072	2	-107.478	2	-19.684	4	0	4	-.012	4	-.415	3
405		13	max	367.048	3	3.604	9	5.992	3	0	3	0	10	.576	2
406			min	-74.912	2	-107.707	2	-19.442	4	0	4	-.016	4	-.407	3
407		14	max	367.168	3	3.414	9	5.992	3	0	3	0	10	.599	2
408			min	-74.752	2	-107.936	2	-19.2	4	0	4	-.02	4	-.399	3
409		15	max	367.288	3	3.223	9	5.992	3	0	3	0	10	.622	2
410			min	-74.591	2	-108.165	2	-18.958	4	0	4	-.024	4	-.391	3
411		16	max	294.994	2	588.949	2	5.974	3	0	1	0	3	.64	2
412			min	3.4	15	-642.455	3	-17.613	4	0	4	-.028	4	-.377	3
413		17	max	295.154	2	588.72	2	5.974	3	0	1	.001	3	.512	2
414			min	3.449	15	-642.627	3	-17.371	4	0	4	-.032	4	-.238	3
415		18	max	-12.491	12	1187.333	2	5.449	3	0	4	.003	3	.257	2
416			min	-308.477	1	-547.928	3	-44.936	5	0	1	-.041	4	-.119	3
417		19	max	-12.411	12	1187.104	2	5.449	3	0	4	.004	3	0	3
418			min	-308.317	1	-548.1	3	-44.694	5	0	1	-.051	4	0	2
419	M9	1	max	138.946	1	343.655	3	192.178	4	0	3	-.003	15	0	2
420			min	4.367	15	-247.17	1	7.373	10	0	1	-.132	1	0	3
421		2	max	139.107	1	343.484	3	192.42	4	0	3	.034	5	.054	1
422			min	4.415	15	-247.399	1	7.373	10	0	1	-.115	1	-.075	3
423		3	max	117.087	3	6.503	9	64.965	1	0	1	.07	5	.106	1
424			min	-14.563	10	-28.607	2	-27.21	5	0	5	-.097	1	-.148	3
425		4	max	117.207	3	6.313	9	64.965	1	0	1	.064	5	.111	2
426			min	-14.429	10	-28.836	2	-26.968	5	0	5	-.083	1	-.146	3
427		5	max	117.327	3	6.122	9	64.965	1	0	1	.058	5	.117	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-14.296	10	-29.065	2	-26.726	5	0	5	-.069	1	-.144	3
429		6	max	117.447	3	5.931	9	64.965	1	0	1	.052	5	.124	2
430			min	-14.162	10	-29.294	2	-26.484	5	0	5	-.055	1	-.142	3
431		7	max	117.567	3	5.741	9	64.965	1	0	1	.047	5	.13	2
432			min	-14.029	10	-29.522	2	-26.242	5	0	5	-.04	1	-.14	3
433		8	max	117.687	3	5.55	9	64.965	1	0	1	.041	5	.137	2
434			min	-13.895	10	-29.751	2	-26	5	0	5	-.026	1	-.137	3
435		9	max	117.807	3	5.359	9	64.965	1	0	1	.035	5	.143	2
436			min	-13.762	10	-29.98	2	-25.758	5	0	5	-.012	1	-.135	3
437		10	max	117.928	3	5.169	9	64.965	1	0	1	.03	4	.15	2
438			min	-13.628	10	-30.209	2	-25.516	5	0	5	0	2	-.133	3
439		11	max	118.048	3	4.978	9	64.965	1	0	1	.028	4	.156	2
440			min	-13.495	10	-30.437	2	-25.274	5	0	5	.002	10	-.131	3
441		12	max	118.168	3	4.788	9	64.965	1	0	1	.03	1	.163	2
442			min	-13.361	10	-30.666	2	-25.032	5	0	5	.003	10	-.129	3
443		13	max	118.288	3	4.597	9	64.965	1	0	1	.044	1	.169	2
444			min	-13.228	10	-30.895	2	-24.79	5	0	5	.005	10	-.126	3
445		14	max	118.408	3	4.406	9	64.965	1	0	1	.058	1	.176	2
446			min	-13.094	10	-31.124	2	-24.548	5	0	5	.005	15	-.124	3
447		15	max	118.528	3	4.216	9	64.965	1	0	1	.072	1	.183	2
448			min	-12.961	10	-31.352	2	-24.306	5	0	5	.002	15	-.122	3
449		16	max	92.776	2	148.261	2	65.418	1	0	10	.087	1	.188	2
450			min	4.393	15	-205.504	3	-22.879	5	0	4	0	5	-.117	3
451		17	max	92.937	2	148.033	2	65.418	1	0	10	.101	1	.156	2
452			min	4.441	15	-205.675	3	-22.637	5	0	4	-.006	5	-.073	3
453		18	max	-.015	15	361.085	2	68.926	1	0	2	.116	1	.079	2
454			min	-139.004	1	-167.181	3	-48.622	5	0	3	-.016	5	-.036	3
455		19	max	.033	15	360.856	2	68.926	1	0	2	.131	1	0	2
456			min	-138.844	1	-167.353	3	-48.38	5	0	3	-.027	5	0	3
457	M13	1	max	192.193	4	246.786	1	-4.367	15	0	2	.132	1	0	1
458			min	7.376	10	-343.657	3	-138.93	1	0	3	.003	15	0	3
459		2	max	184.827	4	174.201	1	-2.896	15	0	2	.04	1	.22	3
460			min	7.376	10	-242.482	3	-106.352	1	0	3	0	15	-.158	1
461		3	max	177.461	4	101.617	1	-1.426	15	0	2	.004	3	.364	3
462			min	7.376	10	-141.307	3	-73.773	1	0	3	-.027	1	-.261	1
463		4	max	170.095	4	29.033	1	.045	15	0	2	0	3	.432	3
464			min	7.376	10	-40.132	3	-41.195	1	0	3	-.07	1	-.31	1
465		5	max	162.728	4	61.043	3	2.235	5	0	2	-.002	15	.424	3
466			min	7.376	10	-43.552	1	-8.617	1	0	3	-.089	1	-.305	1
467		6	max	155.362	4	162.218	3	23.961	1	0	2	0	15	.34	3
468			min	7.376	10	-116.136	1	-.124	3	0	3	-.083	1	-.245	1
469		7	max	147.996	4	263.392	3	56.539	1	0	2	.004	5	.181	3
470			min	7.376	10	-188.72	1	1.455	12	0	3	-.053	1	-.131	1
471		8	max	140.63	4	364.567	3	89.117	1	0	2	.01	4	.038	1
472			min	7.376	10	-261.304	1	2.881	12	0	3	0	3	-.055	3
473		9	max	133.264	4	465.742	3	121.695	1	0	2	.081	1	.261	1
474			min	7.376	10	-333.889	1	4.308	12	0	3	.002	12	-.366	3
475		10	max	125.897	4	566.917	3	154.273	1	0	2	.184	1	.539	1
476			min	7.376	10	-406.473	1	5.735	12	0	3	.006	12	-.754	3
477		11	max	93.159	4	333.888	1	-.552	15	0	3	.078	1	.261	1
478			min	4.093	12	-465.742	3	-121.087	1	0	2	-.014	5	-.366	3
479		12	max	85.793	4	261.304	1	1.131	5	0	3	.002	2	.038	1
480			min	4.093	12	-364.567	3	-88.509	1	0	2	-.014	4	-.055	3
481		13	max	78.426	4	188.72	1	3.406	5	0	3	-.005	12	.181	3
482			min	4.093	12	-263.392	3	-55.931	1	0	2	-.055	1	-.131	1
483		14	max	71.06	4	116.136	1	5.681	5	0	3	-.005	12	.34	3
484			min	4.093	12	-162.218	3	-23.352	1	0	2	-.084	1	-.245	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	68.006	1	43.551	1	10.27	4	0	3	-.002	15	.424	3
486			min	4.093	12	-61.043	3	.433	10	0	2	-.09	1	-.305	1
487		16	max	68.006	1	40.132	3	41.804	1	0	3	.004	5	.432	3
488			min	4.093	12	-29.033	1	3.044	12	0	2	-.07	1	-.31	1
489		17	max	68.006	1	141.307	3	74.382	1	0	3	.012	5	.364	3
490			min	4.093	12	-101.617	1	4.471	12	0	2	-.027	1	-.261	1
491		18	max	68.006	1	242.482	3	106.96	1	0	3	.041	1	.22	3
492			min	4.093	12	-174.201	1	5.897	12	0	2	.003	10	-.158	1
493		19	max	68.006	1	343.657	3	139.538	1	0	3	.134	1	0	1
494			min	4.093	12	-246.786	1	7.324	12	0	2	.009	12	0	3
495	M16	1	max	48.381	5	361.091	2	.033	15	0	3	.131	1	0	2
496			min	-68.682	1	-167.386	3	-138.858	1	0	2	-.027	5	0	3
497		2	max	41.015	5	254.905	2	1.948	5	0	3	.039	1	.107	3
498			min	-68.682	1	-118.326	3	-106.28	1	0	2	-.026	5	-.231	2
499		3	max	33.648	5	148.719	2	4.223	5	0	3	0	12	.177	3
500			min	-68.682	1	-69.267	3	-73.702	1	0	2	-.03	4	-.382	2
501		4	max	26.282	5	42.533	2	6.498	5	0	3	-.003	12	.211	3
502			min	-68.682	1	-20.207	3	-41.124	1	0	2	-.071	1	-.454	2
503		5	max	18.916	5	28.852	3	8.773	5	0	3	-.005	12	.208	3
504			min	-68.682	1	-63.652	2	-8.546	1	0	2	-.09	1	-.446	2
505		6	max	11.55	5	77.912	3	24.032	1	0	3	-.004	15	.168	3
506			min	-68.682	1	-169.838	2	.347	12	0	2	-.084	1	-.359	2
507		7	max	4.184	5	126.972	3	56.61	1	0	3	.003	5	.091	3
508			min	-68.682	1	-276.024	2	1.774	12	0	2	-.054	1	-.191	2
509		8	max	-1.086	12	176.031	3	89.188	1	0	3	.014	4	.055	2
510			min	-68.682	1	-382.209	2	3.201	12	0	2	-.004	3	-.023	3
511		9	max	-1.086	12	225.091	3	121.766	1	0	3	.08	1	.382	2
512			min	-68.682	1	-488.395	2	4.627	12	0	2	0	3	-.173	3
513		10	max	26.811	5	-11.759	15	154.344	1	0	14	.184	1	.788	2
514			min	-69.599	1	-594.581	2	-9.478	3	0	2	.007	12	-.36	3
515		11	max	19.445	5	488.395	2	-.586	15	0	2	.08	1	.382	2
516			min	-69.599	1	-225.091	3	-121.366	1	0	3	-.012	5	-.173	3
517		12	max	12.078	5	382.209	2	1.078	5	0	2	.002	2	.055	2
518			min	-69.599	1	-176.031	3	-88.788	1	0	3	-.012	4	-.023	3
519		13	max	4.712	5	276.024	2	3.353	5	0	2	-.002	12	.091	3
520			min	-69.599	1	-126.972	3	-56.21	1	0	3	-.054	1	-.191	2
521		14	max	-1.659	15	169.838	2	5.628	5	0	2	-.003	12	.168	3
522			min	-69.599	1	-77.912	3	-23.632	1	0	3	-.084	1	-.359	2
523		15	max	-4.372	12	63.652	2	10.192	4	0	2	-.001	15	.208	3
524			min	-69.599	1	-28.852	3	.444	10	0	3	-.089	1	-.446	2
525		16	max	-4.372	12	20.207	3	41.524	1	0	2	.005	5	.211	3
526			min	-69.599	1	-42.533	2	2.202	12	0	3	-.07	1	-.454	2
527		17	max	-4.372	12	69.267	3	74.102	1	0	2	.014	5	.177	3
528			min	-69.599	1	-148.719	2	3.629	12	0	3	-.027	1	-.382	2
529		18	max	-4.372	12	118.326	3	106.68	1	0	2	.041	1	.107	3
530			min	-69.599	1	-254.905	2	5.056	12	0	3	.003	12	-.231	2
531		19	max	-4.372	12	167.386	3	139.258	1	0	2	.133	1	0	2
532			min	-69.599	1	-361.091	2	6.483	12	0	3	.007	12	0	3
533	M15	1	max	0	2	1.847	1	.05	3	0	1	0	1	0	1
534			min	-65.259	3	0	2	-.04	1	0	3	0	3	0	1
535		2	max	0	2	1.642	1	.05	3	0	1	0	1	0	2
536			min	-65.334	3	0	2	-.04	1	0	3	0	3	0	1
537		3	max	0	2	1.437	1	.05	3	0	1	0	1	0	2
538			min	-65.41	3	0	2	-.04	1	0	3	0	3	-.001	1
539		4	max	0	2	1.231	1	.05	3	0	1	0	1	0	2
540			min	-65.485	3	0	2	-.04	1	0	3	0	3	-.002	1
541		5	max	0	2	1.026	1	.05	3	0	1	0	1	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-65.561	3	0	2	-.04	1	0	3	0	3	-.002	1
543		6	max	0	2	.821	1	.05	3	0	1	0	1	0	2
544			min	-65.637	3	0	2	-.04	1	0	3	0	3	-.003	1
545		7	max	0	2	.616	1	.05	3	0	1	0	3	0	2
546			min	-65.712	3	0	2	-.04	1	0	3	0	1	-.003	1
547		8	max	0	2	.41	1	.05	3	0	1	0	3	0	2
548			min	-65.788	3	0	2	-.04	1	0	3	0	1	-.003	1
549		9	max	0	2	.205	1	.05	3	0	1	0	3	0	2
550			min	-65.863	3	0	2	-.04	1	0	3	0	1	-.003	1
551		10	max	0	2	0	1	.05	3	0	1	0	3	0	2
552			min	-65.939	3	0	1	-.04	1	0	3	0	1	-.004	1
553		11	max	0	2	0	2	.05	3	0	1	0	3	0	2
554			min	-66.014	3	-.205	1	-.04	1	0	3	0	1	-.003	1
555		12	max	0	2	0	2	.05	3	0	1	0	3	0	2
556			min	-66.09	3	-.41	1	-.04	1	0	3	0	1	-.003	1
557		13	max	0	2	0	2	.05	3	0	1	0	3	0	2
558			min	-66.165	3	-.616	1	-.04	1	0	3	0	1	-.003	1
559		14	max	0	2	0	2	.05	3	0	1	0	3	0	2
560			min	-66.241	3	-.821	1	-.04	1	0	3	0	1	-.003	1
561		15	max	0	2	0	2	.05	3	0	1	0	3	0	2
562			min	-66.316	3	-1.026	1	-.04	1	0	3	0	1	-.002	1
563		16	max	0	2	0	2	.05	3	0	1	0	3	0	2
564			min	-66.392	3	-1.231	1	-.04	1	0	3	0	1	-.002	1
565		17	max	0	2	0	2	.05	3	0	1	0	3	0	2
566			min	-66.467	3	-1.437	1	-.04	1	0	3	0	1	-.001	1
567		18	max	0	2	0	2	.05	3	0	1	0	3	0	2
568			min	-66.543	3	-1.642	1	-.04	1	0	3	0	1	0	1
569		19	max	0	2	0	2	.05	3	0	1	0	3	0	1
570			min	-66.618	3	-1.847	1	-.04	1	0	3	0	1	0	1
571	M16A	1	max	-.866	10	3.146	4	.32	4	0	3	0	3	0	1
572			min	-234.383	4	.924	12	-.02	3	0	2	0	4	0	1
573		2	max	-.782	10	2.796	4	.288	4	0	3	0	3	0	12
574			min	-234.429	4	.821	12	-.02	3	0	2	0	4	-.001	4
575		3	max	-.698	10	2.447	4	.255	4	0	3	0	3	0	12
576			min	-234.475	4	.718	12	-.02	3	0	2	0	4	-.002	4
577		4	max	-.614	10	2.097	4	.223	4	0	3	0	3	0	12
578			min	-234.521	4	.616	12	-.02	3	0	2	0	4	-.003	4
579		5	max	-.531	10	1.748	4	.191	4	0	3	0	3	-.001	12
580			min	-234.568	4	.513	12	-.02	3	0	2	0	1	-.004	4
581		6	max	-.447	10	1.398	4	.159	4	0	3	0	5	-.001	12
582			min	-234.614	4	.41	12	-.02	3	0	2	0	1	-.005	4
583		7	max	-.363	10	1.049	4	.126	4	0	3	0	5	-.002	12
584			min	-234.66	4	.308	12	-.02	3	0	2	0	1	-.005	4
585		8	max	-.279	10	.699	4	.094	4	0	3	0	5	-.002	12
586			min	-234.706	4	.205	12	-.02	3	0	2	0	1	-.006	4
587		9	max	-.195	10	.35	4	.062	4	0	3	0	5	-.002	12
588			min	-234.753	4	.103	12	-.02	3	0	2	0	1	-.006	4
589		10	max	-.111	10	0	1	.029	4	0	3	0	5	-.002	12
590			min	-234.799	4	0	1	-.02	3	0	2	0	1	-.006	4
591		11	max	-.027	10	-.103	12	.023	1	0	3	0	5	-.002	12
592			min	-234.845	4	-.35	4	-.02	3	0	2	0	1	-.006	4
593		12	max	.057	10	-.205	12	.023	1	0	3	0	5	-.002	12
594			min	-234.891	4	-.699	4	-.039	5	0	2	0	1	-.006	4
595		13	max	.141	10	-.308	12	.023	1	0	3	0	5	-.002	12
596			min	-234.938	4	-1.049	4	-.071	5	0	2	0	3	-.005	4
597		14	max	.225	10	-.41	12	.023	1	0	3	0	4	-.001	12
598			min	-234.984	4	-1.398	4	-.103	5	0	2	0	3	-.005	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.309	10	-.513	12	.023	1	0	3	0	4	-.001	12
600			min	-235.03	4	-1.748	4	-.136	5	0	2	0	3	-.004	4
601		16	max	.393	10	-.616	12	.023	1	0	3	0	4	0	12
602			min	-235.076	4	-2.097	4	-.168	5	0	2	0	3	-.003	4
603		17	max	.477	10	-.718	12	.023	1	0	3	0	1	0	12
604			min	-235.123	4	-2.447	4	-.2	5	0	2	0	5	-.002	4
605		18	max	.56	10	-.821	12	.023	1	0	3	0	1	0	12
606			min	-235.169	4	-2.796	4	-.232	5	0	2	0	5	-.001	4
607		19	max	.644	10	-.924	12	.023	1	0	3	0	1	0	1
608			min	-235.215	4	-3.146	4	-.265	5	0	2	0	5	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.003	1	.011	2	.013	1	1.703e-3	5	NC	3	NC	3
2			min	-.004	3	-.011	3	-.016	5	-1.12e-3	1	4001.118	2	3194.791	1
3		2	max	.002	1	.01	2	.012	1	1.725e-3	5	NC	3	NC	3
4			min	-.004	3	-.011	3	-.016	5	-1.07e-3	1	4377.777	2	3429.527	1
5		3	max	.002	1	.009	2	.011	1	1.747e-3	5	NC	1	NC	2
6			min	-.003	3	-.01	3	-.016	5	-1.021e-3	1	4827.78	2	3707.617	1
7		4	max	.002	1	.008	2	.011	1	1.77e-3	5	NC	1	NC	2
8			min	-.003	3	-.01	3	-.015	5	-9.718e-4	1	5369.131	2	4039.245	1
9		5	max	.002	1	.007	2	.01	1	1.792e-3	5	NC	1	NC	2
10			min	-.003	3	-.009	3	-.015	5	-9.226e-4	1	6025.911	2	4438.011	1
11		6	max	.002	1	.006	2	.009	1	1.814e-3	5	NC	1	NC	2
12			min	-.003	3	-.009	3	-.014	5	-8.733e-4	1	6830.855	2	4922.396	1
13		7	max	.002	1	.005	2	.008	1	1.836e-3	5	NC	1	NC	2
14			min	-.003	3	-.008	3	-.014	5	-8.24e-4	1	7829.304	2	5518.018	1
15		8	max	.002	1	.005	2	.007	1	1.859e-3	5	NC	1	NC	2
16			min	-.002	3	-.008	3	-.013	5	-7.748e-4	1	9085.454	2	6261.232	1
17		9	max	.001	1	.004	2	.006	1	1.881e-3	5	NC	1	NC	2
18			min	-.002	3	-.007	3	-.012	5	-7.255e-4	1	NC	1	7205.066	1
19		10	max	.001	1	.003	2	.005	1	1.903e-3	5	NC	1	NC	2
20			min	-.002	3	-.007	3	-.012	5	-6.763e-4	1	NC	1	8429.431	1
21		11	max	.001	1	.003	2	.004	1	1.925e-3	5	NC	1	NC	1
22			min	-.002	3	-.006	3	-.011	5	-6.27e-4	1	NC	1	NC	1
23		12	max	.001	1	.002	2	.003	1	1.948e-3	5	NC	1	NC	1
24			min	-.001	3	-.005	3	-.01	5	-5.778e-4	1	NC	1	NC	1
25		13	max	0	1	.002	2	.003	1	1.97e-3	5	NC	1	NC	1
26			min	-.001	3	-.005	3	-.009	5	-5.285e-4	1	NC	1	NC	1
27		14	max	0	1	.001	2	.002	1	1.992e-3	5	NC	1	NC	1
28			min	-.001	3	-.004	3	-.007	5	-4.792e-4	1	NC	1	NC	1
29		15	max	0	1	0	2	.001	1	2.015e-3	5	NC	1	NC	1
30			min	0	3	-.003	3	-.006	5	-4.3e-4	1	NC	1	NC	1
31		16	max	0	1	0	2	0	1	2.037e-3	5	NC	1	NC	1
32			min	0	3	-.002	3	-.005	5	-3.807e-4	1	NC	1	NC	1
33		17	max	0	1	0	2	0	1	2.059e-3	5	NC	1	NC	1
34			min	0	3	-.002	3	-.003	5	-3.315e-4	1	NC	1	NC	1
35		18	max	0	1	0	2	0	1	2.081e-3	5	NC	1	NC	1
36			min	0	3	0	3	-.002	5	-2.822e-4	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	2.104e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-2.33e-4	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	1.116e-4	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-1.006e-3	5	NC	1	NC	1
41		2	max	0	3	0	2	.005	5	1.349e-4	1	NC	1	NC	1
42			min	0	2	0	3	0	1	-1.022e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	3	0	2	.01	5	1.582e-4	1	NC	1	NC	1
44			min	0	2	-.002	3	0	1	-1.037e-3	5	NC	1	9633.166	14
45		4	max	0	3	0	2	.015	5	1.815e-4	1	NC	1	NC	1
46			min	0	2	-.003	3	0	1	-1.053e-3	5	NC	1	6314.433	14
47		5	max	0	3	0	2	.02	5	2.048e-4	1	NC	1	NC	1
48			min	0	2	-.004	3	-.001	1	-1.068e-3	5	NC	1	4667.904	14
49		6	max	0	3	0	2	.025	5	2.281e-4	1	NC	1	NC	1
50			min	0	2	-.004	3	0	1	-1.084e-3	5	NC	1	3688.928	14
51		7	max	0	3	0	2	.03	4	2.514e-4	1	NC	1	NC	1
52			min	0	2	-.005	3	0	1	-1.099e-3	5	NC	1	3042.793	14
53		8	max	0	3	0	2	.035	4	2.747e-4	1	NC	1	NC	1
54			min	0	2	-.006	3	0	1	-1.115e-3	5	NC	1	2586.165	14
55		9	max	.001	3	.001	2	.04	4	2.98e-4	1	NC	1	NC	1
56			min	-.001	2	-.007	3	0	1	-1.13e-3	5	NC	1	2247.454	14
57		10	max	.001	3	.002	2	.045	4	3.213e-4	1	NC	1	NC	1
58			min	-.001	2	-.007	3	0	10	-1.146e-3	5	NC	1	1986.942	14
59		11	max	.001	3	.002	2	.05	4	3.446e-4	1	NC	1	NC	1
60			min	-.001	2	-.008	3	0	10	-1.161e-3	5	NC	1	1780.834	14
61		12	max	.002	3	.003	2	.055	4	3.679e-4	1	NC	1	NC	1
62			min	-.001	2	-.008	3	0	10	-1.177e-3	5	NC	1	1614.016	14
63		13	max	.002	3	.004	2	.06	4	3.912e-4	1	NC	1	NC	1
64			min	-.002	2	-.008	3	0	12	-1.192e-3	5	NC	1	1476.427	14
65		14	max	.002	3	.004	2	.064	4	4.145e-4	1	NC	1	NC	1
66			min	-.002	2	-.009	3	0	12	-1.208e-3	5	NC	1	1361.115	14
67		15	max	.002	3	.005	2	.069	4	4.379e-4	1	NC	1	NC	1
68			min	-.002	2	-.009	3	0	12	-1.223e-3	5	8579.816	2	1263.12	14
69		16	max	.002	3	.006	2	.074	4	4.612e-4	1	NC	1	NC	1
70			min	-.002	2	-.009	3	0	12	-1.239e-3	5	7277.571	2	1178.812	14
71		17	max	.002	3	.007	2	.078	4	4.845e-4	1	NC	1	NC	2
72			min	-.002	2	-.009	3	0	12	-1.254e-3	5	6269.042	2	1105.469	14
73		18	max	.002	3	.008	2	.083	4	5.078e-4	1	NC	1	NC	2
74			min	-.002	2	-.009	3	0	12	-1.27e-3	5	5478.987	2	1041.01	14
75		19	max	.002	3	.009	2	.087	4	5.311e-4	1	NC	3	NC	2
76			min	-.002	2	-.009	3	0	12	-1.285e-3	5	4854.497	2	983.817	14
77	M4	1	max	.002	1	.012	2	0	12	7.036e-3	5	NC	1	NC	3
78			min	0	15	-.011	3	-.092	4	-8.637e-4	1	NC	1	210.456	4
79		2	max	.002	1	.012	2	0	12	7.036e-3	5	NC	1	NC	3
80			min	0	15	-.01	3	-.084	4	-8.637e-4	1	NC	1	229.422	4
81		3	max	.002	1	.011	2	0	12	7.036e-3	5	NC	1	NC	2
82			min	0	15	-.01	3	-.077	4	-8.637e-4	1	NC	1	251.998	4
83		4	max	.001	1	.01	2	0	12	7.036e-3	5	NC	1	NC	2
84			min	0	15	-.009	3	-.069	4	-8.637e-4	1	NC	1	279.132	4
85		5	max	.001	1	.01	2	0	12	7.036e-3	5	NC	1	NC	2
86			min	0	15	-.009	3	-.062	4	-8.637e-4	1	NC	1	312.12	4
87		6	max	.001	1	.009	2	0	12	7.036e-3	5	NC	1	NC	2
88			min	0	15	-.008	3	-.055	4	-8.637e-4	1	NC	1	352.761	4
89		7	max	.001	1	.008	2	0	12	7.036e-3	5	NC	1	NC	2
90			min	0	15	-.007	3	-.048	4	-8.637e-4	1	NC	1	403.621	4
91		8	max	.001	1	.008	2	0	12	7.036e-3	5	NC	1	NC	2
92			min	0	15	-.007	3	-.041	4	-8.637e-4	1	NC	1	468.455	4
93		9	max	0	1	.007	2	0	12	7.036e-3	5	NC	1	NC	1
94			min	0	15	-.006	3	-.035	4	-8.637e-4	1	NC	1	552.941	4
95		10	max	0	1	.006	2	0	12	7.036e-3	5	NC	1	NC	1
96			min	0	15	-.005	3	-.029	4	-8.637e-4	1	NC	1	666.007	4
97		11	max	0	1	.006	2	0	12	7.036e-3	5	NC	1	NC	1
98			min	0	15	-.005	3	-.024	4	-8.637e-4	1	NC	1	822.359	4
99		12	max	0	1	.005	2	0	12	7.036e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	15	-.004	3	-.018	4	-8.637e-4	1	NC	1	1047.643	4
101		13	max	0	1	.004	2	0	12	7.036e-3	5	NC	1	NC	1
102			min	0	15	-.004	3	-.014	4	-8.637e-4	1	NC	1	1389.97	4
103		14	max	0	1	.003	2	0	12	7.036e-3	5	NC	1	NC	1
104			min	0	15	-.003	3	-.01	4	-8.637e-4	1	NC	1	1948.575	4
105		15	max	0	1	.003	2	0	12	7.036e-3	5	NC	1	NC	1
106			min	0	15	-.002	3	-.007	4	-8.637e-4	1	NC	1	2956.598	4
107		16	max	0	1	.002	2	0	12	7.036e-3	5	NC	1	NC	1
108			min	0	15	-.002	3	-.004	4	-8.637e-4	1	NC	1	5076.805	4
109		17	max	0	1	.001	2	0	12	7.036e-3	5	NC	1	NC	1
110			min	0	15	-.001	3	-.002	4	-8.637e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	12	7.036e-3	5	NC	1	NC	1
112			min	0	15	0	3	0	4	-8.637e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	7.036e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-8.637e-4	1	NC	1	NC	1
115	M6	1	max	.008	1	.038	2	.005	1	1.865e-3	4	NC	3	NC	2
116			min	-.012	3	-.035	3	-.016	5	2.828e-7	10	1122.043	2	8815.358	1
117		2	max	.008	1	.035	2	.004	1	1.884e-3	4	NC	3	NC	2
118			min	-.012	3	-.034	3	-.016	5	-3.041e-7	10	1201.087	2	9525.123	1
119		3	max	.008	1	.033	2	.004	1	1.903e-3	4	NC	3	NC	1
120			min	-.011	3	-.032	3	-.016	5	-1.937e-6	2	1291.711	2	NC	1
121		4	max	.007	1	.03	2	.004	1	1.922e-3	4	NC	3	NC	1
122			min	-.01	3	-.03	3	-.016	5	-4.254e-6	2	1396.222	2	NC	1
123		5	max	.007	1	.028	2	.003	1	1.941e-3	4	NC	3	NC	1
124			min	-.01	3	-.028	3	-.015	5	-6.571e-6	2	1517.59	2	NC	1
125		6	max	.006	1	.026	2	.003	1	1.96e-3	4	NC	3	NC	1
126			min	-.009	3	-.026	3	-.015	5	-8.888e-6	2	1659.702	2	NC	1
127		7	max	.006	1	.023	2	.003	1	1.979e-3	4	NC	3	NC	1
128			min	-.008	3	-.024	3	-.014	5	-1.121e-5	2	1827.74	2	NC	1
129		8	max	.005	1	.021	2	.002	1	1.998e-3	4	NC	3	NC	1
130			min	-.008	3	-.022	3	-.014	5	-1.352e-5	2	2028.771	2	NC	1
131		9	max	.005	1	.019	2	.002	1	2.017e-3	4	NC	3	NC	1
132			min	-.007	3	-.02	3	-.013	5	-1.584e-5	2	2272.684	2	NC	1
133		10	max	.004	1	.016	2	.002	1	2.036e-3	4	NC	3	NC	1
134			min	-.006	3	-.018	3	-.012	5	-1.816e-5	2	2573.753	2	9931.28	4
135		11	max	.004	1	.014	2	.001	1	2.055e-3	4	NC	3	NC	1
136			min	-.006	3	-.016	3	-.011	5	-2.047e-5	2	2953.375	2	9983.507	4
137		12	max	.003	1	.012	2	.001	1	2.074e-3	4	NC	3	NC	1
138			min	-.005	3	-.014	3	-.01	5	-2.279e-5	2	3445.155	2	NC	1
139		13	max	.003	1	.01	2	0	1	2.093e-3	4	NC	3	NC	1
140			min	-.004	3	-.012	3	-.009	5	-2.511e-5	2	4105.064	2	NC	1
141		14	max	.002	1	.008	2	0	1	2.112e-3	4	NC	3	NC	1
142			min	-.003	3	-.01	3	-.008	5	-2.742e-5	2	5033.8	2	NC	1
143		15	max	.002	1	.007	2	0	1	2.131e-3	4	NC	1	NC	1
144			min	-.003	3	-.008	3	-.006	5	-3.077e-5	11	6432.682	2	NC	1
145		16	max	.001	1	.005	2	0	1	2.15e-3	4	NC	1	NC	1
146			min	-.002	3	-.006	3	-.005	5	-3.698e-5	1	8771.331	2	NC	1
147		17	max	0	1	.003	2	0	1	2.169e-3	5	NC	1	NC	1
148			min	-.001	3	-.004	3	-.003	5	-4.618e-5	1	NC	1	NC	1
149		18	max	0	1	.002	2	0	1	2.189e-3	5	NC	1	NC	1
150			min	0	3	-.002	3	-.002	5	-5.538e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	2.21e-3	5	NC	1	NC	1
152			min	0	1	0	1	0	1	-6.458e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	3.054e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-1.057e-3	5	NC	1	NC	1
155		2	max	0	3	.002	2	.005	5	2.694e-5	1	NC	1	NC	1
156			min	0	2	-.002	3	0	1	-1.058e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	3	.003	2	.011	5	2.334e-5	1	NC	1	NC	1
158			min	0	2	-.004	3	0	1	-1.061e-3	4	NC	1	NC	1
159		4	max	.001	3	.005	2	.016	5	1.974e-5	1	NC	1	NC	1
160			min	-.001	2	-.007	3	0	1	-1.064e-3	4	9878.85	2	NC	1
161		5	max	.002	3	.006	2	.021	5	1.614e-5	1	NC	1	NC	1
162			min	-.002	2	-.009	3	0	1	-1.066e-3	4	7453.79	2	NC	1
163		6	max	.002	3	.008	2	.027	5	2.566e-5	3	NC	1	NC	1
164			min	-.002	2	-.011	3	0	1	-1.069e-3	4	5970.08	2	NC	1
165		7	max	.003	3	.009	2	.032	5	4.545e-5	3	NC	3	NC	1
166			min	-.003	2	-.012	3	0	1	-1.072e-3	4	4959.261	2	NC	1
167		8	max	.003	3	.011	2	.037	5	6.524e-5	3	NC	3	NC	1
168			min	-.003	2	-.014	3	-.001	1	-1.074e-3	4	4221.03	2	NC	1
169		9	max	.003	3	.013	2	.042	5	8.503e-5	3	NC	3	NC	1
170			min	-.004	2	-.016	3	-.001	1	-1.077e-3	4	3655.486	2	NC	1
171		10	max	.004	3	.014	2	.047	5	1.048e-4	3	NC	3	NC	1
172			min	-.004	2	-.018	3	-.001	1	-1.08e-3	4	3207.215	2	NC	1
173		11	max	.004	3	.016	2	.052	5	1.246e-4	3	NC	3	NC	1
174			min	-.005	2	-.019	3	-.001	1	-1.083e-3	4	2842.948	2	NC	1
175		12	max	.005	3	.018	2	.056	4	1.444e-4	3	NC	3	NC	1
176			min	-.005	2	-.021	3	-.002	1	-1.085e-3	4	2541.42	2	NC	1
177		13	max	.005	3	.02	2	.061	4	1.642e-4	3	NC	3	NC	1
178			min	-.006	2	-.022	3	-.002	1	-1.088e-3	4	2288.333	2	NC	1
179		14	max	.006	3	.022	2	.065	4	1.84e-4	3	NC	3	NC	1
180			min	-.006	2	-.023	3	-.002	1	-1.091e-3	4	2073.651	2	NC	1
181		15	max	.006	3	.024	2	.07	4	2.038e-4	3	NC	3	NC	1
182			min	-.007	2	-.024	3	-.002	1	-1.093e-3	4	1890.073	2	NC	1
183		16	max	.006	3	.027	2	.074	4	2.236e-4	3	NC	3	NC	1
184			min	-.007	2	-.026	3	-.002	1	-1.096e-3	4	1732.128	2	NC	1
185		17	max	.007	3	.029	2	.079	4	2.433e-4	3	NC	3	NC	1
186			min	-.008	2	-.027	3	-.002	1	-1.099e-3	4	1595.611	2	NC	1
187		18	max	.007	3	.031	2	.083	4	2.631e-4	3	NC	3	NC	1
188			min	-.008	2	-.028	3	-.002	1	-1.101e-3	4	1477.229	2	NC	1
189		19	max	.008	3	.034	2	.087	4	2.829e-4	3	NC	3	NC	1
190			min	-.009	2	-.029	3	-.002	1	-1.104e-3	4	1374.36	2	NC	1
191	M8	1	max	.005	1	.044	2	.002	1	6.859e-3	4	NC	1	NC	2
192			min	0	15	-.035	3	-.092	4	-2.266e-4	3	NC	1	210.35	4
193		2	max	.004	1	.041	2	.002	1	6.859e-3	4	NC	1	NC	2
194			min	0	15	-.033	3	-.084	4	-2.266e-4	3	NC	1	229.306	4
195		3	max	.004	1	.039	2	.002	1	6.859e-3	4	NC	1	NC	2
196			min	0	15	-.031	3	-.077	4	-2.266e-4	3	NC	1	251.869	4
197		4	max	.004	1	.037	2	.002	1	6.859e-3	4	NC	1	NC	1
198			min	0	15	-.029	3	-.069	4	-2.266e-4	3	NC	1	278.989	4
199		5	max	.004	1	.034	2	.002	1	6.859e-3	4	NC	1	NC	1
200			min	0	15	-.027	3	-.062	4	-2.266e-4	3	NC	1	311.958	4
201		6	max	.003	1	.032	2	.001	1	6.859e-3	4	NC	1	NC	1
202			min	0	15	-.025	3	-.055	4	-2.266e-4	3	NC	1	352.577	4
203		7	max	.003	1	.029	2	.001	1	6.859e-3	4	NC	1	NC	1
204			min	0	15	-.023	3	-.048	4	-2.266e-4	3	NC	1	403.41	4
205		8	max	.003	1	.027	2	.001	1	6.859e-3	4	NC	1	NC	1
206			min	0	15	-.021	3	-.041	4	-2.266e-4	3	NC	1	468.207	4
207		9	max	.003	1	.024	2	0	1	6.859e-3	4	NC	1	NC	1
208			min	0	15	-.019	3	-.035	4	-2.266e-4	3	NC	1	552.647	4
209		10	max	.002	1	.022	2	0	1	6.859e-3	4	NC	1	NC	1
210			min	0	15	-.017	3	-.029	4	-2.266e-4	3	NC	1	665.652	4
211		11	max	.002	1	.019	2	0	1	6.859e-3	4	NC	1	NC	1
212			min	0	15	-.016	3	-.024	4	-2.266e-4	3	NC	1	821.917	4
213		12	max	.002	1	.017	2	0	1	6.859e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	15	-.014	3	-.018	4	-2.266e-4	3	NC	1	1047.078	4
215		13	max	.002	1	.015	2	0	1	6.859e-3	4	NC	1	NC	1
216			min	0	15	-.012	3	-.014	4	-2.266e-4	3	NC	1	1389.216	4
217		14	max	.001	1	.012	2	0	1	6.859e-3	4	NC	1	NC	1
218			min	0	15	-.01	3	-.01	4	-2.266e-4	3	NC	1	1947.513	4
219		15	max	.001	1	.01	2	0	1	6.859e-3	4	NC	1	NC	1
220			min	0	15	-.008	3	-.007	4	-2.266e-4	3	NC	1	2954.979	4
221		16	max	0	1	.007	2	0	1	6.859e-3	4	NC	1	NC	1
222			min	0	15	-.006	3	-.004	4	-2.266e-4	3	NC	1	5074.011	4
223		17	max	0	1	.005	2	0	1	6.859e-3	4	NC	1	NC	1
224			min	0	15	-.004	3	-.002	4	-2.266e-4	3	NC	1	NC	1
225		18	max	0	1	.002	2	0	1	6.859e-3	4	NC	1	NC	1
226			min	0	15	-.002	3	0	4	-2.266e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	6.859e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-2.266e-4	3	NC	1	NC	1
229	M10	1	max	.003	1	.011	2	0	3	1.004e-3	1	NC	3	NC	1
230			min	-.004	3	-.011	3	-.007	4	-3.985e-4	3	4003.347	2	NC	1
231		2	max	.003	1	.01	2	0	3	9.532e-4	1	NC	3	NC	1
232			min	-.003	3	-.011	3	-.008	4	-3.849e-4	3	4380.316	2	NC	1
233		3	max	.002	1	.009	2	0	3	9.019e-4	1	NC	3	NC	1
234			min	-.003	3	-.01	3	-.008	4	-3.712e-4	3	4830.71	2	NC	1
235		4	max	.002	1	.008	2	0	3	8.506e-4	1	NC	1	NC	1
236			min	-.003	3	-.01	3	-.008	4	-3.575e-4	3	5372.559	2	NC	1
237		5	max	.002	1	.007	2	0	3	8.283e-4	4	NC	1	NC	1
238			min	-.003	3	-.009	3	-.008	4	-3.438e-4	3	6029.98	2	NC	1
239		6	max	.002	1	.006	2	0	3	8.954e-4	4	NC	1	NC	1
240			min	-.003	3	-.009	3	-.008	4	-3.301e-4	3	6835.761	2	NC	1
241		7	max	.002	1	.005	2	0	3	9.625e-4	4	NC	1	NC	1
242			min	-.002	3	-.008	3	-.008	4	-3.164e-4	3	7835.318	2	NC	1
243		8	max	.002	1	.005	2	0	3	1.03e-3	4	NC	1	NC	1
244			min	-.002	3	-.008	3	-.008	4	-3.028e-4	3	9092.963	2	NC	1
245		9	max	.002	1	.004	2	0	3	1.097e-3	4	NC	1	NC	1
246			min	-.002	3	-.007	3	-.008	4	-2.891e-4	3	NC	1	NC	1
247		10	max	.001	1	.003	2	0	3	1.164e-3	4	NC	1	NC	1
248			min	-.002	3	-.007	3	-.008	4	-2.754e-4	3	NC	1	9787.098	4
249		11	max	.001	1	.003	2	0	3	1.231e-3	4	NC	1	NC	1
250			min	-.002	3	-.006	3	-.008	4	-2.617e-4	3	NC	1	9771.077	4
251		12	max	.001	1	.002	2	0	3	1.298e-3	4	NC	1	NC	1
252			min	-.001	3	-.006	3	-.007	4	-2.48e-4	3	NC	1	NC	1
253		13	max	0	1	.002	2	0	3	1.365e-3	4	NC	1	NC	1
254			min	-.001	3	-.005	3	-.006	4	-2.343e-4	3	NC	1	NC	1
255		14	max	0	1	.001	2	0	3	1.432e-3	4	NC	1	NC	1
256			min	0	3	-.004	3	-.006	4	-2.207e-4	3	NC	1	NC	1
257		15	max	0	1	0	2	0	3	1.499e-3	4	NC	1	NC	1
258			min	0	3	-.003	3	-.005	4	-2.07e-4	3	NC	1	NC	1
259		16	max	0	1	0	2	0	3	1.567e-3	4	NC	1	NC	1
260			min	0	3	-.003	3	-.004	4	-1.933e-4	3	NC	1	NC	1
261		17	max	0	1	0	2	0	3	1.634e-3	4	NC	1	NC	1
262			min	0	3	-.002	3	-.003	4	-1.796e-4	3	NC	1	NC	1
263		18	max	0	1	0	2	0	3	1.701e-3	4	NC	1	NC	1
264			min	0	3	0	3	-.001	4	-1.659e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.768e-3	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-1.522e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	7.283e-5	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-8.466e-4	4	NC	1	NC	1
269		2	max	0	3	0	2	.004	4	5.203e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-9.404e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	3	0	2	.009	4	3.122e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-1.034e-3	4	NC	1	NC	1
273		4	max	0	3	0	2	.013	4	1.042e-5	3	NC	1	NC	1
274			min	0	2	-.003	3	0	3	-1.128e-3	4	NC	1	NC	1
275		5	max	0	3	0	2	.017	4	-7.224e-6	12	NC	1	NC	1
276			min	0	2	-.004	3	-.001	3	-1.222e-3	4	NC	1	NC	1
277		6	max	0	3	0	2	.021	5	-1.991e-5	12	NC	1	NC	1
278			min	0	2	-.005	3	-.001	3	-1.316e-3	4	NC	1	NC	1
279		7	max	0	3	0	2	.026	5	-2.905e-5	10	NC	1	NC	1
280			min	0	2	-.005	3	-.002	3	-1.409e-3	4	NC	1	NC	1
281		8	max	0	3	0	2	.03	5	-3.276e-5	10	NC	1	NC	1
282			min	0	2	-.006	3	-.002	1	-1.503e-3	4	NC	1	NC	1
283		9	max	.001	3	.001	2	.034	5	-3.647e-5	10	NC	1	NC	1
284			min	-.001	2	-.007	3	-.003	1	-1.597e-3	4	NC	1	NC	1
285		10	max	.001	3	.002	2	.039	5	-4.018e-5	10	NC	1	NC	1
286			min	-.001	2	-.007	3	-.004	1	-1.691e-3	4	NC	1	NC	1
287		11	max	.001	3	.002	2	.043	5	-4.389e-5	10	NC	1	NC	2
288			min	-.001	2	-.008	3	-.005	1	-1.784e-3	4	NC	1	9652.606	1
289		12	max	.002	3	.003	2	.047	5	-4.761e-5	10	NC	1	NC	2
290			min	-.001	2	-.008	3	-.006	1	-1.878e-3	4	NC	1	8017.068	1
291		13	max	.002	3	.004	2	.051	5	-5.132e-5	10	NC	1	NC	2
292			min	-.002	2	-.008	3	-.007	1	-1.972e-3	4	NC	1	6812.205	1
293		14	max	.002	3	.004	2	.055	5	-5.503e-5	10	NC	1	NC	2
294			min	-.002	2	-.009	3	-.008	1	-2.066e-3	4	NC	1	5898.828	1
295		15	max	.002	3	.005	2	.06	5	-5.874e-5	10	NC	1	NC	2
296			min	-.002	2	-.009	3	-.009	1	-2.159e-3	4	8591.743	2	5190.347	1
297		16	max	.002	3	.006	2	.064	5	-6.245e-5	10	NC	1	NC	2
298			min	-.002	2	-.009	3	-.01	1	-2.253e-3	4	7286.83	2	4630.538	1
299		17	max	.002	3	.007	2	.068	5	-6.616e-5	10	NC	1	NC	2
300			min	-.002	2	-.009	3	-.011	1	-2.347e-3	4	6276.417	2	4181.583	1
301		18	max	.002	3	.008	2	.072	5	-6.988e-5	10	NC	1	NC	2
302			min	-.002	2	-.009	3	-.012	1	-2.441e-3	4	5485.008	2	3817.29	1
303		19	max	.002	3	.009	2	.076	5	-7.359e-5	10	NC	3	NC	3
304			min	-.002	2	-.009	3	-.013	1	-2.535e-3	4	4859.528	2	3519.072	1
305	M12	1	max	.002	1	.012	2	.011	1	8.221e-3	4	NC	1	NC	3
306			min	0	15	-.011	3	-.084	5	8.244e-5	10	NC	1	229.699	5
307		2	max	.002	1	.012	2	.01	1	8.221e-3	4	NC	1	NC	3
308			min	0	15	-.01	3	-.077	5	8.244e-5	10	NC	1	250.394	5
309		3	max	.002	1	.011	2	.009	1	8.221e-3	4	NC	1	NC	3
310			min	0	15	-.01	3	-.07	5	8.244e-5	10	NC	1	275.027	5
311		4	max	.001	1	.01	2	.008	1	8.221e-3	4	NC	1	NC	3
312			min	0	15	-.009	3	-.063	5	8.244e-5	10	NC	1	304.632	5
313		5	max	.001	1	.01	2	.007	1	8.221e-3	4	NC	1	NC	3
314			min	0	15	-.009	3	-.057	5	8.244e-5	10	NC	1	340.625	5
315		6	max	.001	1	.009	2	.006	1	8.221e-3	4	NC	1	NC	3
316			min	0	15	-.008	3	-.05	5	8.244e-5	10	NC	1	384.967	5
317		7	max	.001	1	.008	2	.006	1	8.221e-3	4	NC	1	NC	3
318			min	0	15	-.007	3	-.044	5	8.244e-5	10	NC	1	440.458	5
319		8	max	.001	1	.008	2	.005	1	8.221e-3	4	NC	1	NC	2
320			min	0	15	-.007	3	-.038	5	8.244e-5	10	NC	1	511.194	5
321		9	max	0	1	.007	2	.004	1	8.221e-3	4	NC	1	NC	2
322			min	0	15	-.006	3	-.032	5	8.244e-5	10	NC	1	603.37	5
323		10	max	0	1	.006	2	.003	1	8.221e-3	4	NC	1	NC	2
324			min	0	15	-.005	3	-.027	5	8.244e-5	10	NC	1	726.726	5
325		11	max	0	1	.006	2	.003	1	8.221e-3	4	NC	1	NC	2
326			min	0	15	-.005	3	-.022	5	8.244e-5	10	NC	1	897.304	5
327		12	max	0	1	.005	2	.002	1	8.221e-3	4	NC	1	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	15	-.004	3	-.017	5	8.244e-5	10	NC	1	1143.083	5
329		13	max	0	1	.004	2	.002	1	8.221e-3	4	NC	1	NC	1
330			min	0	15	-.004	3	-.013	5	8.244e-5	10	NC	1	1516.546	5
331		14	max	0	1	.003	2	.001	1	8.221e-3	4	NC	1	NC	1
332			min	0	15	-.003	3	-.009	5	8.244e-5	10	NC	1	2125.95	5
333		15	max	0	1	.003	2	0	1	8.221e-3	4	NC	1	NC	1
334			min	0	15	-.002	3	-.006	5	8.244e-5	10	NC	1	3225.622	5
335		16	max	0	1	.002	2	0	1	8.221e-3	4	NC	1	NC	1
336			min	0	15	-.002	3	-.003	5	8.244e-5	10	NC	1	5538.556	5
337		17	max	0	1	.001	2	0	1	8.221e-3	4	NC	1	NC	1
338			min	0	15	-.001	3	-.002	5	8.244e-5	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	8.221e-3	4	NC	1	NC	1
340			min	0	15	0	3	0	5	8.244e-5	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	8.221e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	8.244e-5	10	NC	1	NC	1
343	M1	1	max	.01	3	.027	3	.009	5	1.561e-2	1	NC	1	NC	1
344			min	-.009	2	-.024	2	-.005	1	-2.157e-2	3	NC	1	NC	1
345		2	max	.01	3	.016	3	.012	5	7.538e-3	2	NC	4	NC	2
346			min	-.009	2	-.014	2	-.01	1	-1.069e-2	3	4918.447	2	8999.253	1
347		3	max	.01	3	.007	3	.016	5	6.187e-4	5	NC	4	NC	2
348			min	-.009	2	-.005	2	-.013	1	-6.829e-4	1	2524.292	2	5462.176	1
349		4	max	.01	3	.003	1	.021	5	6.377e-4	5	NC	4	NC	2
350			min	-.009	2	-.002	3	-.015	1	-5.913e-4	1	1765.44	2	3972.562	5
351		5	max	.009	3	.01	2	.025	5	6.568e-4	5	NC	4	NC	2
352			min	-.009	2	-.008	3	-.015	1	-4.998e-4	1	1398.791	2	2840.641	5
353		6	max	.009	3	.016	2	.03	5	6.758e-4	5	NC	4	NC	2
354			min	-.009	2	-.014	3	-.014	1	-4.082e-4	1	1190.043	2	2180.736	5
355		7	max	.009	3	.02	2	.036	5	6.949e-4	5	NC	5	NC	2
356			min	-.009	2	-.018	3	-.013	1	-3.167e-4	1	1062.219	2	1753.883	5
357		8	max	.009	3	.024	2	.041	5	7.14e-4	5	NC	5	NC	2
358			min	-.009	2	-.021	3	-.01	1	-2.251e-4	1	983.271	2	1458.316	5
359		9	max	.009	3	.026	2	.047	5	7.33e-4	5	NC	5	NC	1
360			min	-.009	2	-.023	3	-.007	1	-1.336e-4	1	938.254	2	1242.218	4
361		10	max	.009	3	.027	2	.052	5	7.521e-4	5	NC	5	NC	1
362			min	-.009	2	-.024	3	-.004	1	-4.201e-5	1	920.35	2	1061.167	4
363		11	max	.009	3	.027	2	.058	4	7.852e-4	4	NC	5	NC	1
364			min	-.009	2	-.023	3	-.001	1	1.465e-5	10	927.7	2	925.568	4
365		12	max	.009	3	.025	2	.064	4	8.264e-4	4	NC	5	NC	2
366			min	-.009	2	-.021	3	0	10	2.403e-5	10	962.746	2	821.69	4
367		13	max	.009	3	.022	2	.071	4	8.676e-4	4	NC	4	NC	2
368			min	-.009	2	-.018	3	0	10	3.175e-5	12	1033.563	2	740.766	4
369		14	max	.009	3	.017	2	.077	4	9.088e-4	4	NC	4	NC	2
370			min	-.009	2	-.014	3	0	12	3.551e-5	12	1158.587	2	676.994	4
371		15	max	.009	3	.01	2	.082	4	9.5e-4	4	NC	4	NC	2
372			min	-.009	2	-.008	3	0	12	3.927e-5	12	1380.917	2	626.422	4
373		16	max	.009	3	.002	1	.087	4	1.322e-3	4	NC	4	NC	2
374			min	-.009	2	-.002	3	0	12	4.201e-5	12	1820.607	2	586.301	4
375		17	max	.009	3	.006	3	.092	4	9.58e-3	4	NC	4	NC	2
376			min	-.009	2	-.008	2	0	12	-1.632e-4	1	2628.442	1	554.721	4
377		18	max	.009	3	.014	3	.096	4	1.13e-2	2	NC	2	NC	2
378			min	-.009	2	-.02	2	0	10	-5.365e-3	3	5081.519	1	530.257	4
379		19	max	.009	3	.023	3	.099	4	2.287e-2	2	NC	1	NC	1
380			min	-.009	2	-.032	2	-.003	1	-1.086e-2	3	5809.236	2	512.547	4
381	M5	1	max	.03	3	.088	3	.008	5	1.054e-5	4	NC	1	NC	1
382			min	-.034	2	-.08	2	-.006	1	4.251e-8	10	3512.132	3	NC	1
383		2	max	.03	3	.053	3	.012	5	3.136e-4	5	NC	5	NC	1
384			min	-.034	2	-.048	2	-.005	1	-5.824e-5	1	1470.691	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.03	3	.021	3	.016	5	6.117e-4	5	NC	5	NC	1
386			min	-.034	2	-.018	2	-.005	1	-1.16e-4	1	754.373	2	NC	1
387		4	max	.03	3	.009	2	.021	5	6.394e-4	5	NC	5	NC	1
388			min	-.034	2	-.005	3	-.004	1	-1.112e-4	1	527.073	2	NC	1
389		5	max	.03	3	.033	2	.026	5	6.671e-4	5	NC	5	NC	1
390			min	-.034	2	-.028	3	-.004	1	-1.065e-4	1	417.208	2	NC	1
391		6	max	.03	3	.052	2	.032	5	6.948e-4	5	NC	5	NC	1
392			min	-.034	2	-.046	3	-.004	1	-1.017e-4	1	354.629	2	NC	1
393		7	max	.03	3	.068	2	.037	5	7.226e-4	5	NC	15	NC	1
394			min	-.034	2	-.06	3	-.004	1	-9.699e-5	1	316.281	2	NC	1
395		8	max	.03	3	.08	2	.043	5	7.503e-4	5	NC	15	NC	1
396			min	-.034	2	-.07	3	-.003	1	-9.223e-5	1	292.563	2	9948.71	3
397		9	max	.03	3	.088	2	.049	5	7.78e-4	5	NC	15	NC	1
398			min	-.034	2	-.075	3	-.003	1	-8.748e-5	1	278.996	2	NC	1
399		10	max	.03	3	.092	2	.055	5	8.057e-4	5	NC	15	NC	1
400			min	-.034	2	-.077	3	-.003	1	-8.273e-5	1	273.534	2	NC	1
401		11	max	.03	3	.09	2	.061	5	8.335e-4	5	NC	15	NC	1
402			min	-.034	2	-.074	3	-.003	1	-7.798e-5	1	275.617	2	NC	1
403		12	max	.029	3	.084	2	.067	5	8.612e-4	5	NC	15	NC	1
404			min	-.034	2	-.068	3	-.003	1	-7.322e-5	1	285.971	2	NC	1
405		13	max	.029	3	.073	2	.072	5	8.889e-4	5	NC	15	NC	1
406			min	-.034	2	-.058	3	-.003	1	-6.847e-5	1	307.015	2	NC	1
407		14	max	.029	3	.056	2	.078	5	9.166e-4	5	NC	5	NC	1
408			min	-.034	2	-.044	3	-.003	1	-6.372e-5	1	344.282	2	NC	1
409		15	max	.029	3	.034	2	.083	4	9.444e-4	5	NC	5	NC	1
410			min	-.034	2	-.027	3	-.002	1	-5.896e-5	1	410.753	2	NC	1
411		16	max	.029	3	.007	2	.087	4	1.302e-3	5	NC	5	NC	1
412			min	-.034	2	-.006	3	-.002	1	-6.096e-5	1	542.817	2	NC	1
413		17	max	.029	3	.019	3	.092	4	9.556e-3	4	NC	5	NC	1
414			min	-.034	2	-.027	2	-.002	1	-2.237e-4	1	851.264	3	NC	1
415		18	max	.029	3	.046	3	.096	4	4.901e-3	4	NC	5	NC	1
416			min	-.034	2	-.066	2	-.002	1	-1.145e-4	1	1669.537	3	NC	1
417		19	max	.029	3	.074	3	.099	4	2.509e-6	5	NC	3	NC	1
418			min	-.034	2	-.108	2	-.002	1	-4.737e-7	3	1681.937	2	NC	1
419	M9	1	max	.01	3	.027	3	.007	5	2.158e-2	3	NC	1	NC	1
420			min	-.009	2	-.024	2	-.006	1	-1.561e-2	1	NC	1	NC	1
421		2	max	.01	3	.016	3	.007	5	1.066e-2	3	NC	4	NC	2
422			min	-.009	2	-.014	2	-.001	1	-7.601e-3	2	4920.175	2	9862.87	1
423		3	max	.01	3	.006	3	.007	4	2.777e-4	1	NC	4	NC	2
424			min	-.009	2	-.005	2	0	3	-6.62e-5	3	2525.202	2	6066.281	1
425		4	max	.01	3	.003	2	.009	4	2.002e-4	1	NC	4	NC	2
426			min	-.009	2	-.002	3	-.001	3	-7.046e-5	3	1766.079	2	5092.085	1
427		5	max	.01	3	.01	2	.012	4	1.228e-4	1	NC	4	NC	2
428			min	-.009	2	-.009	3	-.002	3	-7.471e-5	3	1399.281	2	4982.95	1
429		6	max	.009	3	.016	2	.015	4	8.437e-5	4	NC	4	NC	2
430			min	-.009	2	-.014	3	-.003	3	-7.897e-5	3	1190.439	2	4839.668	4
431		7	max	.009	3	.02	2	.019	4	9.87e-5	4	NC	4	NC	2
432			min	-.009	2	-.019	3	-.003	3	-8.323e-5	3	1062.548	2	3474.297	4
433		8	max	.009	3	.024	2	.023	4	1.302e-4	5	NC	5	NC	1
434			min	-.009	2	-.022	3	-.004	3	-1.095e-4	1	983.55	2	2623.417	4
435		9	max	.009	3	.026	2	.028	5	1.616e-4	5	NC	5	NC	1
436			min	-.009	2	-.023	3	-.004	3	-1.869e-4	1	938.492	2	2058.034	4
437		10	max	.009	3	.027	2	.034	5	1.931e-4	5	NC	5	NC	1
438			min	-.009	2	-.024	3	-.005	1	-2.643e-4	1	920.55	2	1663.306	4
439		11	max	.009	3	.027	2	.041	5	2.245e-4	5	NC	5	NC	1
440			min	-.009	2	-.023	3	-.008	1	-3.418e-4	1	927.861	2	1376.721	4
441		12	max	.009	3	.025	2	.047	5	2.56e-4	5	NC	5	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.009	2	-.021	3	-.01	1	-4.192e-4	1	962.861	2	1161.954	4
443		13	max	.009	3	.022	2	.054	5	2.875e-4	5	NC	5	NC	2
444			min	-.009	2	-.018	3	-.012	1	-4.966e-4	1	1033.612	2	989.683	5
445		14	max	.009	3	.017	2	.062	5	3.189e-4	5	NC	4	NC	2
446			min	-.009	2	-.014	3	-.013	1	-5.74e-4	1	1158.527	2	857.744	5
447		15	max	.009	3	.01	2	.069	5	3.504e-4	5	NC	4	NC	2
448			min	-.009	2	-.008	3	-.014	1	-6.515e-4	1	1380.632	2	755.321	5
449		16	max	.009	3	.002	1	.077	5	7.418e-4	5	NC	4	NC	2
450			min	-.009	2	-.002	3	-.013	1	-7.073e-4	1	1819.721	2	674.33	5
451		17	max	.009	3	.006	3	.084	5	9.728e-3	4	NC	4	NC	2
452			min	-.009	2	-.008	2	-.011	1	-2.495e-4	1	2628.231	1	608.204	4
453		18	max	.009	3	.014	3	.091	5	5.422e-3	3	NC	2	NC	2
454			min	-.009	2	-.019	2	-.007	1	-1.137e-2	2	5081.126	1	549.539	4
455		19	max	.009	3	.023	3	.099	4	1.086e-2	3	NC	1	NC	1
456			min	-.009	2	-.032	2	-.002	1	-2.287e-2	2	5831.622	2	500.321	4
457	M13	1	max	.006	1	.027	3	.01	3	3.953e-3	3	NC	1	NC	1
458			min	-.007	5	-.024	2	-.009	2	-3.618e-3	2	NC	1	NC	1
459		2	max	.006	1	.214	3	.033	1	4.95e-3	3	NC	5	NC	2
460			min	-.007	5	-.158	2	-.002	10	-4.561e-3	2	863.766	3	4324.279	1
461		3	max	.006	1	.368	3	.085	1	5.947e-3	3	NC	5	NC	3
462			min	-.007	5	-.269	2	0	5	-5.504e-3	2	474.945	3	1818.398	1
463		4	max	.006	1	.464	3	.128	1	6.944e-3	3	NC	5	NC	3
464			min	-.008	5	-.339	2	-.002	5	-6.446e-3	2	370.123	3	1223.691	1
465		5	max	.006	1	.493	3	.149	1	7.942e-3	3	NC	5	NC	3
466			min	-.008	5	-.361	2	-.004	5	-7.389e-3	2	347.258	3	1058.846	1
467		6	max	.006	1	.455	3	.14	1	8.939e-3	3	NC	5	NC	3
468			min	-.008	5	-.336	2	-.006	5	-8.332e-3	2	377.8	3	1119.555	1
469		7	max	.006	1	.365	3	.105	1	9.936e-3	3	NC	5	NC	3
470			min	-.008	5	-.273	2	-.009	5	-9.275e-3	2	479.442	3	1480.627	1
471		8	max	.006	1	.246	3	.053	1	1.093e-2	3	NC	5	NC	2
472			min	-.008	5	-.191	2	-.011	5	-1.022e-2	2	738.969	3	2832.791	1
473		9	max	.006	1	.137	3	.028	3	1.193e-2	3	NC	4	NC	1
474			min	-.008	5	-.114	2	-.023	2	-1.116e-2	2	1468.527	3	8847.995	3
475		10	max	.006	1	.088	3	.03	3	1.293e-2	3	NC	4	NC	4
476			min	-.008	5	-.08	2	-.034	2	-1.21e-2	2	2665.59	3	6600.805	2
477		11	max	.006	1	.137	3	.034	3	1.193e-2	3	NC	4	NC	1
478			min	-.008	5	-.114	2	-.023	2	-1.116e-2	2	1468.525	3	6552.381	3
479		12	max	.005	1	.246	3	.056	1	1.094e-2	3	NC	5	NC	2
480			min	-.008	5	-.191	2	-.009	10	-1.022e-2	2	738.968	3	2688.159	1
481		13	max	.005	1	.365	3	.109	1	9.939e-3	3	NC	5	NC	5
482			min	-.009	5	-.273	2	0	10	-9.276e-3	2	479.442	3	1434.727	1
483		14	max	.005	1	.456	3	.144	1	8.943e-3	3	NC	5	NC	5
484			min	-.009	5	-.336	2	.005	10	-8.333e-3	2	377.8	3	1093.979	1
485		15	max	.005	1	.493	3	.152	1	7.947e-3	3	NC	5	NC	5
486			min	-.009	5	-.361	2	.005	15	-7.39e-3	2	347.258	3	1039.305	1
487		16	max	.005	1	.465	3	.13	1	6.951e-3	3	NC	5	NC	5
488			min	-.009	5	-.339	2	0	15	-6.447e-3	2	370.122	3	1204.285	1
489		17	max	.005	1	.368	3	.086	1	5.955e-3	3	NC	5	NC	3
490			min	-.009	5	-.269	2	-.004	5	-5.505e-3	2	474.945	3	1792.15	1
491		18	max	.005	1	.214	3	.034	1	4.959e-3	3	NC	5	NC	2
492			min	-.009	5	-.158	2	-.006	5	-4.562e-3	2	863.766	3	4262.488	1
493		19	max	.005	1	.027	3	.01	3	3.964e-3	3	NC	1	NC	1
494			min	-.009	5	-.024	2	-.009	2	-3.619e-3	2	NC	1	NC	1
495	M16	1	max	.002	1	.023	3	.009	3	4.647e-3	2	NC	1	NC	1
496			min	-.099	4	-.032	2	-.009	2	-3.315e-3	3	NC	1	NC	1
497		2	max	.002	1	.118	3	.034	1	5.871e-3	2	NC	5	NC	2
498			min	-.099	4	-.231	2	-.002	10	-4.134e-3	3	814.749	2	4176.297	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	.002	1	.196	3	.087	1	7.095e-3	2	NC	5	NC	3
500			min	-.099	4	-.394	2	.004	10	-4.953e-3	3	447.606	2	1773.04	1
501		4	max	.002	1	.246	3	.131	1	8.319e-3	2	NC	5	NC	10
502			min	-.099	4	-.497	2	.008	10	-5.773e-3	3	348.27	2	1197.702	1
503		5	max	.002	1	.263	3	.151	1	9.543e-3	2	NC	5	NC	10
504			min	-.099	4	-.529	2	.008	10	-6.592e-3	3	325.89	2	1037.645	1
505		6	max	.002	1	.247	3	.143	1	1.077e-2	2	NC	5	NC	10
506			min	-.099	4	-.491	2	.006	10	-7.411e-3	3	352.926	2	1096.394	1
507		7	max	.002	1	.205	3	.107	1	1.199e-2	2	NC	5	NC	5
508			min	-.099	4	-.397	2	0	10	-8.231e-3	3	444	2	1445.191	1
509		8	max	.002	1	.15	3	.055	1	1.322e-2	2	NC	5	NC	2
510			min	-.099	4	-.273	2	-.009	10	-9.05e-3	3	671.429	2	2736.057	1
511		9	max	.002	1	.098	3	.032	3	1.444e-2	2	NC	4	NC	1
512			min	-.099	4	-.159	2	-.023	2	-9.869e-3	3	1269.759	2	7157.119	3
513		10	max	.002	1	.074	3	.029	3	1.566e-2	2	NC	4	NC	4
514			min	-.099	4	-.108	2	-.034	2	-1.069e-2	3	2137.066	2	6655.428	2
515		11	max	.003	1	.098	3	.028	3	1.444e-2	2	NC	4	NC	1
516			min	-.099	4	-.159	2	-.023	2	-9.868e-3	3	1269.759	2	8442.285	3
517		12	max	.003	1	.15	3	.054	1	1.322e-2	2	NC	5	NC	2
518			min	-.099	4	-.273	2	-.009	10	-9.048e-3	3	671.429	2	2770.073	1
519		13	max	.003	1	.205	3	.106	1	1.199e-2	2	NC	5	NC	5
520			min	-.099	4	-.397	2	0	10	-8.227e-3	3	444	2	1461.282	1
521		14	max	.003	1	.247	3	.141	1	1.077e-2	2	NC	5	NC	5
522			min	-.099	4	-.491	2	.005	15	-7.407e-3	3	352.926	2	1109.187	1
523		15	max	.003	1	.263	3	.149	1	9.545e-3	2	NC	5	NC	5
524			min	-.099	4	-.529	2	.001	15	-6.586e-3	3	325.89	2	1051.363	1
525		16	max	.003	1	.246	3	.128	1	8.321e-3	2	NC	5	NC	3
526			min	-.099	4	-.497	2	-.004	5	-5.766e-3	3	348.27	2	1216.891	1
527		17	max	.003	1	.195	3	.085	1	7.097e-3	2	NC	5	NC	3
528			min	-.099	4	-.394	2	-.008	5	-4.945e-3	3	447.606	2	1810.528	1
529		18	max	.003	1	.118	3	.033	1	5.873e-3	2	NC	5	NC	2
530			min	-.099	4	-.231	2	-.008	5	-4.125e-3	3	814.75	2	4311.243	1
531		19	max	.003	1	.023	3	.009	3	4.649e-3	2	NC	1	NC	1
532			min	-.099	4	-.032	2	-.009	2	-3.304e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	4.061e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-7.235e-4	5	NC	1	NC	1
535		2	max	0	3	0	15	.011	4	9.259e-4	3	NC	3	NC	1
536			min	0	5	-.011	1	0	3	-7.49e-4	5	7992.014	2	8271.858	4
537		3	max	0	3	0	15	.025	4	1.446e-3	3	NC	5	NC	1
538			min	-.002	5	-.023	1	-.004	3	-1.129e-3	2	4066.863	2	3680.672	4
539		4	max	0	3	0	15	.04	4	1.965e-3	3	NC	5	NC	9
540			min	-.002	5	-.033	1	-.008	3	-1.662e-3	2	2790.106	2	2308.85	4
541		5	max	0	3	0	15	.054	4	2.485e-3	3	NC	5	NC	9
542			min	-.003	5	-.042	1	-.013	3	-2.195e-3	2	2177.148	2	1698.286	4
543		6	max	0	3	0	15	.066	4	3.005e-3	3	NC	5	9977.038	9
544			min	-.004	5	-.05	1	-.019	3	-2.728e-3	2	1832.3	2	1378.514	4
545		7	max	0	3	0	15	.076	4	3.525e-3	3	NC	5	7922.298	9
546			min	-.005	5	-.056	1	-.025	3	-3.261e-3	2	1624.92	2	1201.328	4
547		8	max	0	3	0	15	.082	4	4.044e-3	3	NC	5	6611.605	9
548			min	-.006	5	-.061	1	-.031	3	-3.794e-3	2	1500.46	2	1108.32	4
549		9	max	0	3	0	15	.085	4	4.564e-3	3	NC	5	5746.038	9
550			min	-.007	5	-.064	1	-.037	3	-4.327e-3	2	1433.469	2	1074.833	4
551		10	max	0	3	.001	15	.084	4	5.084e-3	3	NC	5	5173.026	9
552			min	-.007	5	-.065	1	-.041	3	-4.86e-3	2	1412.276	2	1092.811	4
553		11	max	0	3	.001	15	.078	4	5.604e-3	3	NC	5	4811.976	9
554			min	-.008	5	-.064	1	-.044	3	-5.393e-3	2	1433.469	2	1166.03	4
555		12	max	0	3	.002	15	.07	4	6.123e-3	3	NC	5	4623.651	9

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.009	5	-.061	1	-.044	3	-5.926e-3	2	1500.46	2	1312.008	4
557		13	max	.001	3	.002	15	.058	4	6.643e-3	3	NC	5	4599.033	9
558			min	-.01	5	-.056	1	-.043	3	-6.459e-3	2	1624.92	2	1343.727	3
559		14	max	.001	3	.003	5	.045	4	7.163e-3	3	NC	5	4761.425	9
560			min	-.011	5	-.05	1	-.039	3	-6.992e-3	2	1832.3	2	1386.44	3
561		15	max	.001	3	.003	5	.03	4	7.683e-3	3	NC	5	5674.545	15
562			min	-.011	5	-.042	1	-.031	3	-7.525e-3	2	2177.148	2	1506.058	3
563		16	max	.001	3	.004	5	.019	1	8.202e-3	3	NC	5	NC	15
564			min	-.012	5	-.033	1	-.02	3	-8.058e-3	2	2790.106	2	1761.255	3
565		17	max	.001	3	.005	5	.008	1	8.722e-3	3	NC	5	NC	4
566			min	-.013	5	-.023	1	-.006	3	-8.591e-3	2	4066.863	2	2335.985	3
567		18	max	.002	3	.006	5	.014	3	9.242e-3	3	NC	3	NC	4
568			min	-.014	5	-.012	9	-.016	2	-9.124e-3	2	7992.014	2	4160.655	3
569		19	max	.002	3	.007	5	.038	3	9.762e-3	3	NC	1	NC	1
570			min	-.015	5	-.003	9	-.038	2	-9.658e-3	2	NC	1	NC	1
571	M16A	1	max	0	10	.001	2	.011	3	2.858e-3	3	NC	1	NC	1
572			min	-.006	4	-.004	4	-.011	2	-2.679e-3	2	NC	1	NC	1
573		2	max	0	10	-.006	12	.004	9	2.746e-3	3	NC	3	NC	1
574			min	-.005	4	-.024	4	-.005	5	-2.563e-3	2	4693.191	4	NC	1
575		3	max	0	10	-.012	12	.01	1	2.634e-3	3	8133.727	12	NC	4
576			min	-.005	4	-.042	4	-.013	5	-2.446e-3	2	2388.205	4	5766.723	1
577		4	max	0	10	-.017	12	.016	1	2.521e-3	3	5580.212	12	NC	10
578			min	-.005	4	-.06	4	-.026	5	-2.33e-3	2	1638.448	4	3738.822	5
579		5	max	0	10	-.021	12	.019	1	2.409e-3	3	4354.296	12	9549.905	10
580			min	-.004	4	-.075	4	-.041	5	-2.213e-3	2	1278.498	4	2325.265	5
581		6	max	0	10	-.025	12	.022	1	2.297e-3	3	3664.6	12	8927.306	10
582			min	-.004	4	-.088	4	-.056	5	-2.097e-3	2	1075.991	4	1677.513	5
583		7	max	0	10	-.029	12	.022	1	2.185e-3	3	3249.839	12	8808.466	10
584			min	-.004	4	-.099	4	-.07	5	-1.981e-3	2	954.21	4	1333.157	5
585		8	max	0	10	-.031	12	.022	1	2.073e-3	3	3000.92	12	9080.49	10
586			min	-.003	4	-.107	4	-.082	5	-1.864e-3	2	881.123	4	1137.167	5
587		9	max	0	10	-.032	12	.021	1	1.961e-3	3	2866.937	12	9737.816	10
588			min	-.003	4	-.111	4	-.09	5	-1.748e-3	2	841.783	4	1026.404	5
589		10	max	0	10	-.033	12	.019	1	1.849e-3	3	2824.552	12	NC	10
590			min	-.003	4	-.112	4	-.095	5	-1.631e-3	2	829.338	4	972.723	5
591		11	max	0	10	-.032	12	.017	1	1.737e-3	3	2866.937	12	NC	10
592			min	-.003	4	-.111	4	-.096	5	-1.515e-3	2	841.783	4	964.447	5
593		12	max	0	10	-.031	12	.014	1	1.625e-3	3	3000.92	12	NC	9
594			min	-.002	4	-.106	4	-.092	5	-1.399e-3	2	881.123	4	1000.138	5
595		13	max	0	10	-.028	12	.011	1	1.512e-3	3	3249.839	12	NC	9
596			min	-.002	4	-.097	4	-.085	5	-1.282e-3	2	954.21	4	1088.033	5
597		14	max	0	10	-.025	12	.008	1	1.4e-3	3	3664.6	12	NC	2
598			min	-.002	4	-.086	4	-.074	5	-1.166e-3	2	1075.991	4	1250.727	5
599		15	max	0	10	-.021	12	.005	1	1.288e-3	3	4354.296	12	NC	1
600			min	-.001	4	-.073	4	-.06	5	-1.049e-3	2	1278.498	4	1540.546	5
601		16	max	0	10	-.016	12	.003	1	1.176e-3	3	5580.212	12	NC	1
602			min	0	4	-.057	4	-.044	5	-9.33e-4	2	1638.448	4	2088.98	5
603		17	max	0	10	-.011	12	.001	9	1.064e-3	3	8133.727	12	NC	1
604			min	0	4	-.039	4	-.028	5	-8.166e-4	2	2388.205	4	3310.481	5
605		18	max	0	10	-.006	12	0	3	1.092e-3	4	NC	3	NC	1
606			min	0	4	-.02	4	-.013	5	-7.002e-4	2	4693.191	4	7355.616	5
607		19	max	0	1	0	1	0	1	1.166e-3	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-5.838e-4	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

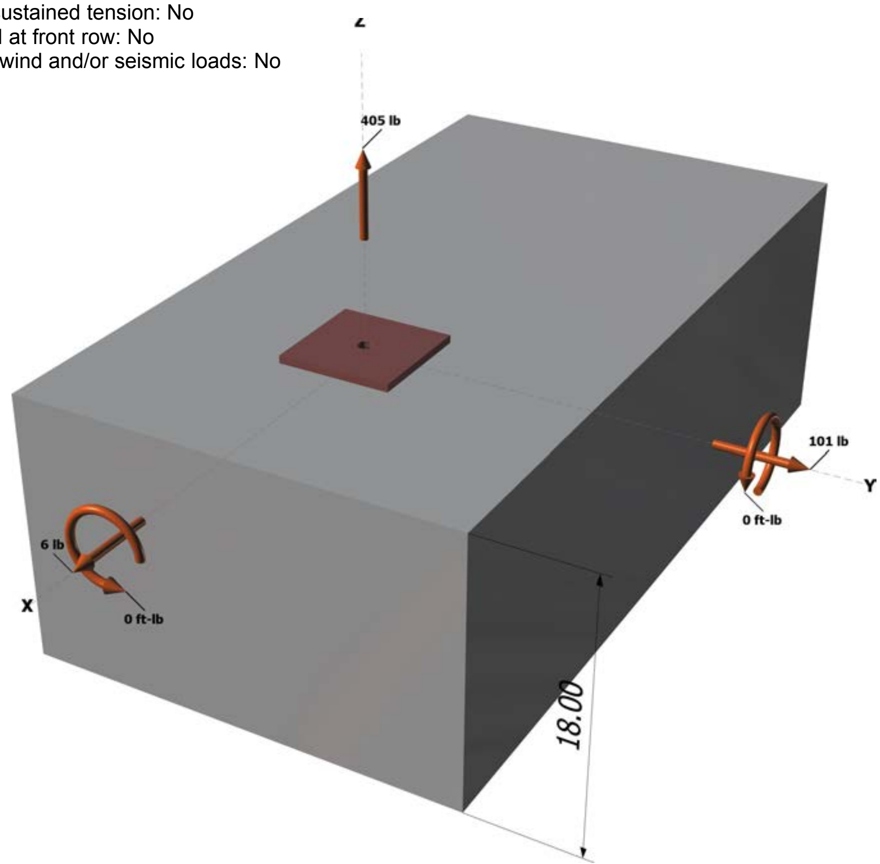
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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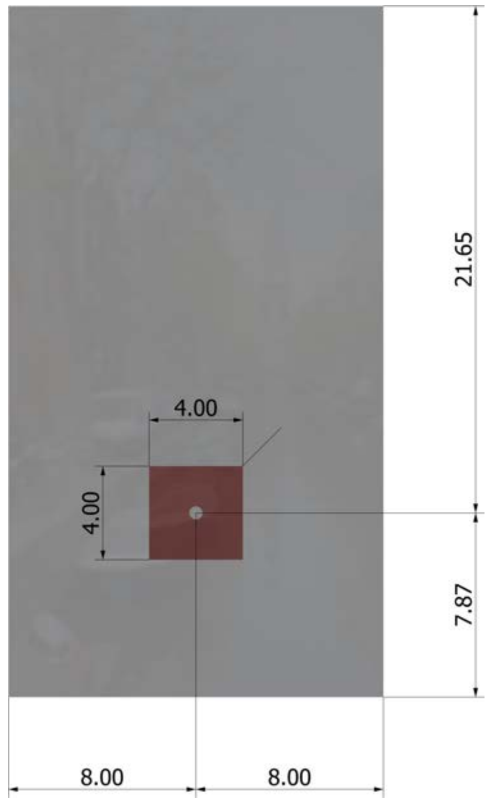


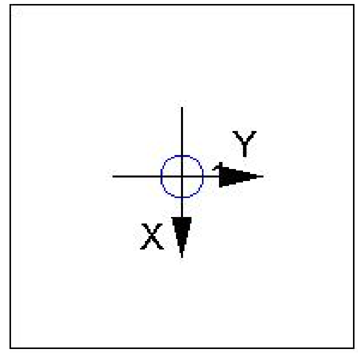
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\,(A_{Nc}/A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in²)	A_{Nco} (in²)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na}/A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in²)	A_{Na0} (in²)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

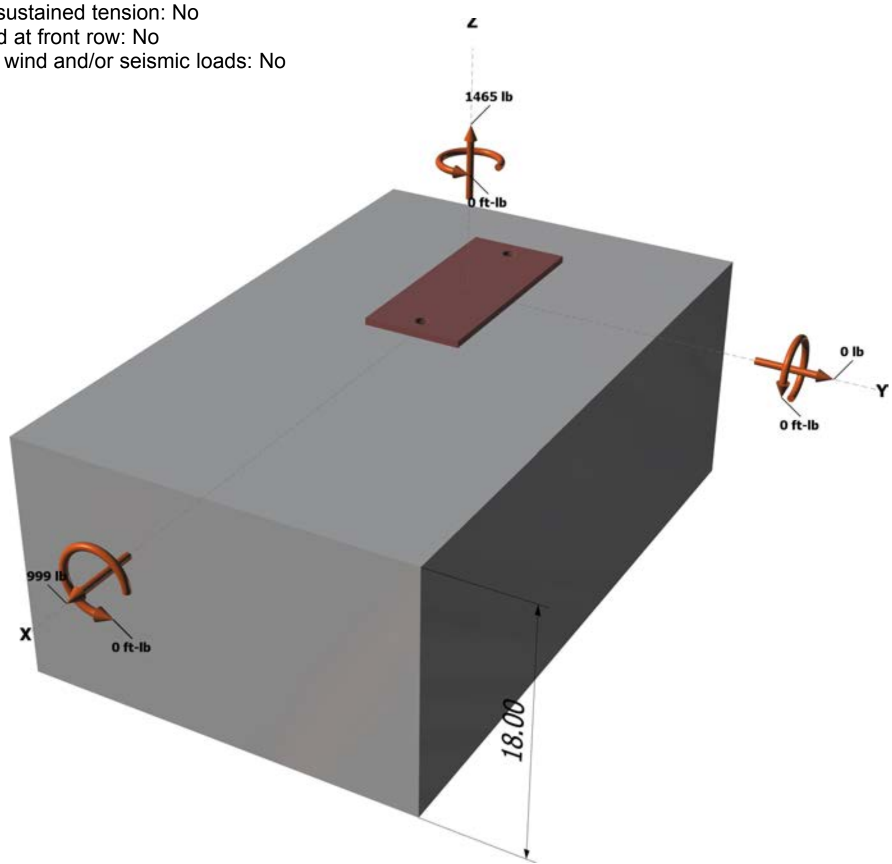
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

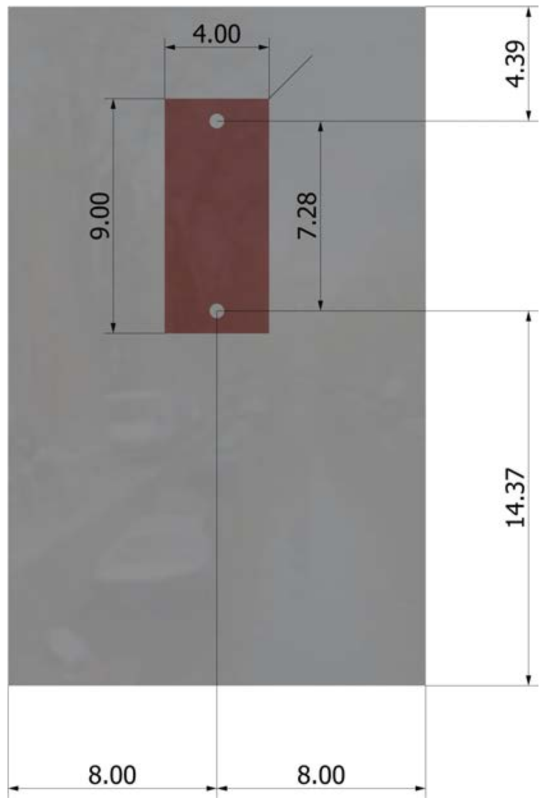
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>



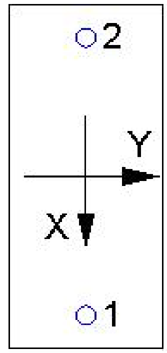
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc}/A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc}/A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\min|k_{cp}(A_{Na}/A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc}/A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.