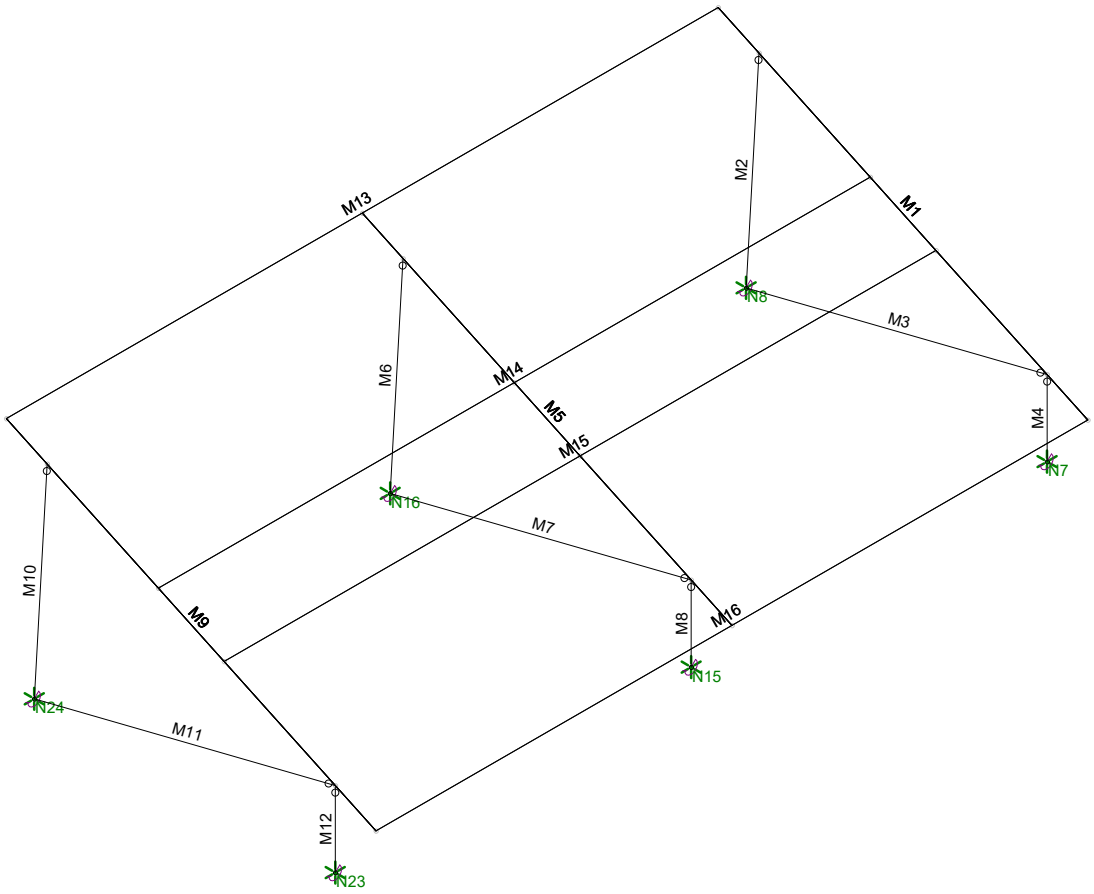


Schletter, Inc.		25° Tilt w/ Seismic Design
HCV	Standard PVMax Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMax ground mount system.

1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

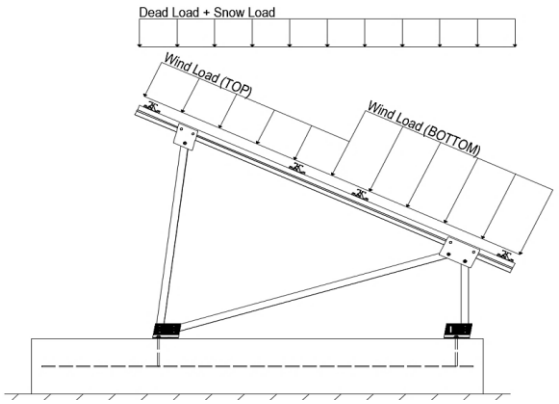
PV modules are required to meet the following specifications:

	Maximum		Minimum	
Height =	2000	mm	1900	mm
Width =	1050	mm	970	mm
Dead Load =	3.00	psf	1.75	psf

Modules Per Row =	2
Module Tilt =	25°
Maximum Height Above Grade =	3 ft

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	18.56	psf	*(ASCE 7-10, Eq. 7.4-1)*
I_s =	1.00		
C_s =	0.82		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	140	mph	Exposure Category = C
Height <	15	ft	Importance Category = II
Peak Velocity Pressure, q_z =	30.77	psf	*Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.100	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.700	
$Cf-_{TOP, OUTER PURLIN}$	=	-2.500	
$Cf-_{TOP, INNER PURLIN}$	=	-1.900	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.000	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25	*ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.*
S_{DS} =	1.67	C_S =	0.8	
S_1 =	1.00	ρ =	1.3	
S_{D1} =	1.00	Ω =	1.25	
T_a =	0.06	C_d =	1.25	

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M13	Top
M14	Mid-Top
M15	Mid-Bottom
M16	Bottom

Diagonal Struts	Location
M3	Outer
M7	Inner
M11	Outer

Front Reactions	Location
N7	Outer
N15	Inner
N23	Outer

Girders	Location
M1	Outer
M5	Inner
M9	Outer

Rear Struts	Location
M2	Outer
M6	Inner
M10	Outer

Rear Reactions	Location
N8	Outer
N16	Inner
N24	Outer

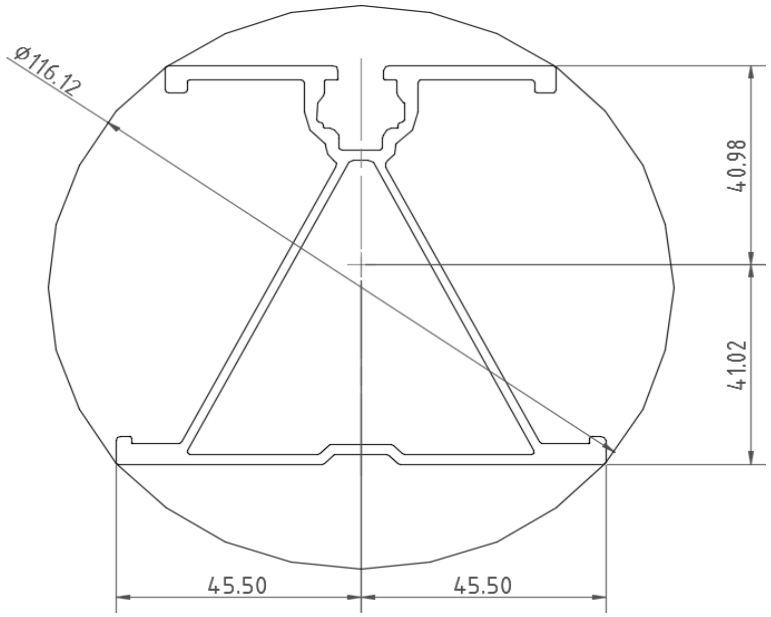
Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	96	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.495	k-ft
M_z =	0.256	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	76%	

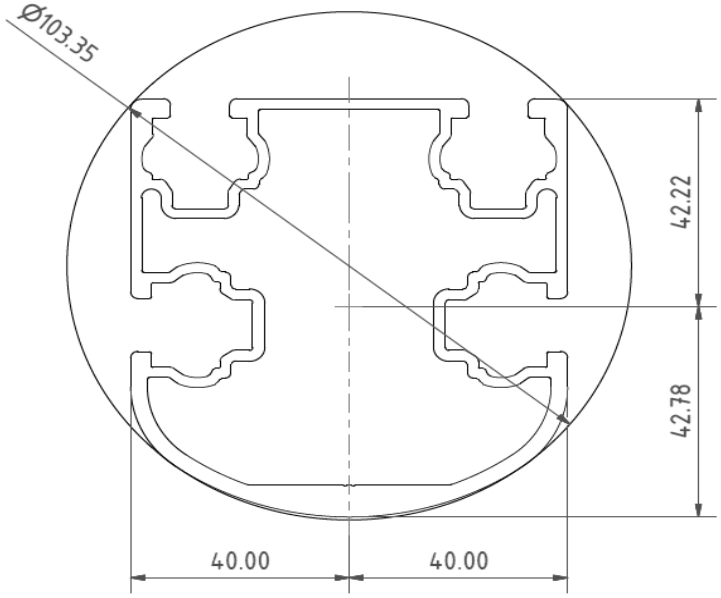


DETAIL VIEW

4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

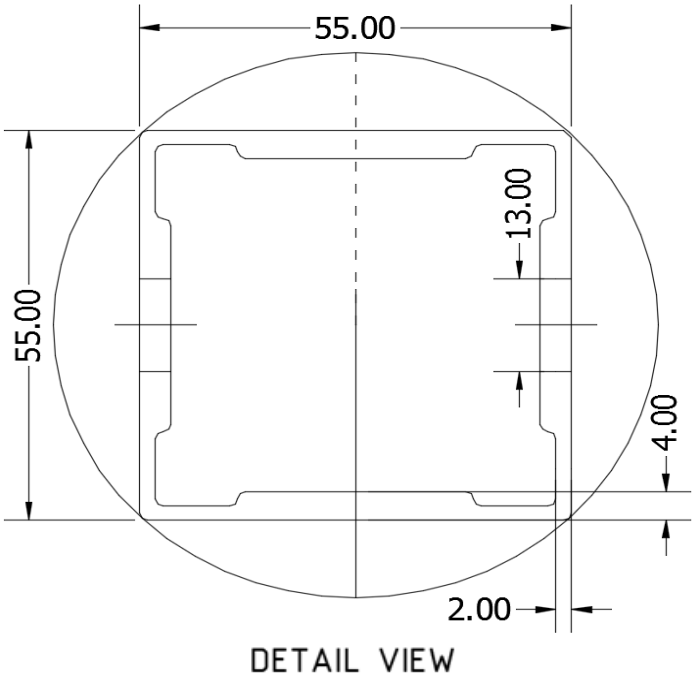
Girder Type =	**BF0**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	104.56	in
$\Phi F_{ty\ AXIAL}$ =	31.09	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.00	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	33.25	ksi
S_y =	1.42	in^3
S_x =	1.41	in^3
E =	10100	ksi
I_y =	2.39	in^4
I_x =	2.22	in^4
A =	1.88	in^2
g =	2.26	lbs/ft
M_y =	-3.359	k-ft
M_z =	0.000	k-ft
P_n =	-0.896	k
$M_{y\ allowable}$ =	3.422	k-ft
$M_{z\ allowable}$ =	3.907	k-ft
$P_{n\ allowable}$ =	58.535	k
Utilization =	100%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M12 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

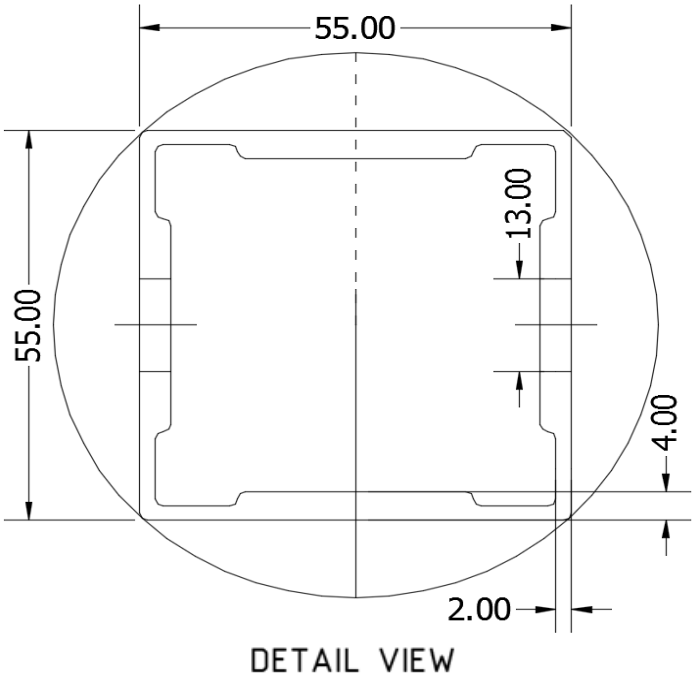
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	24.80	in
$\Phi F_{ty\ AXIAL}$ =	28.03	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.507	k-ft
P_n =	0.564	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	27.532	k
Utilization =	38%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M12 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

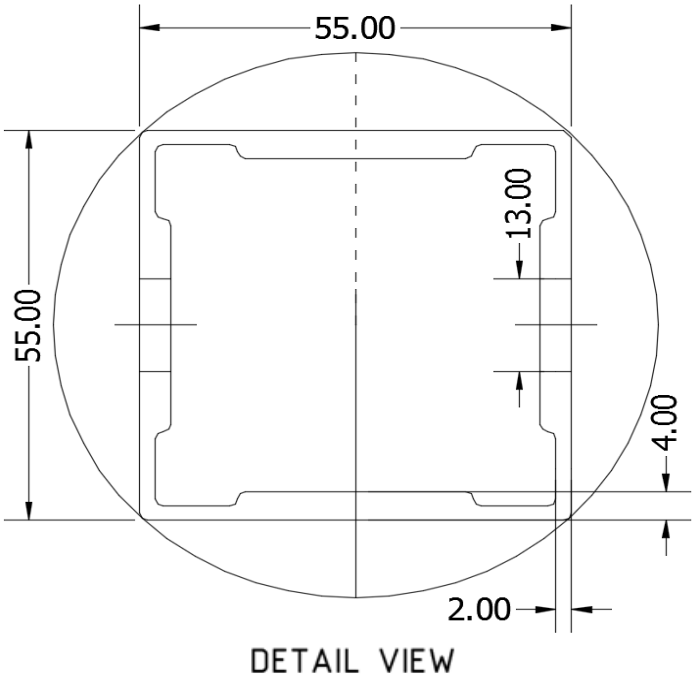
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	98.03	in
$\Phi F_{ty\ AXIAL}$ =	6.11	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.012	k-ft
M_z =	0.000	k-ft
P_n =	2.279	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	6.000	k
Utilization =	39%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M12 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	69.80	in
$\Phi F_{ty\ AXIAL}$ =	10.82	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	-0.012	k-ft
M_z =	0.000	k-ft
P_n =	3.278	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	10.629	k
Utilization =	32%	



5. FOUNDATION DESIGN CALCULATIONS

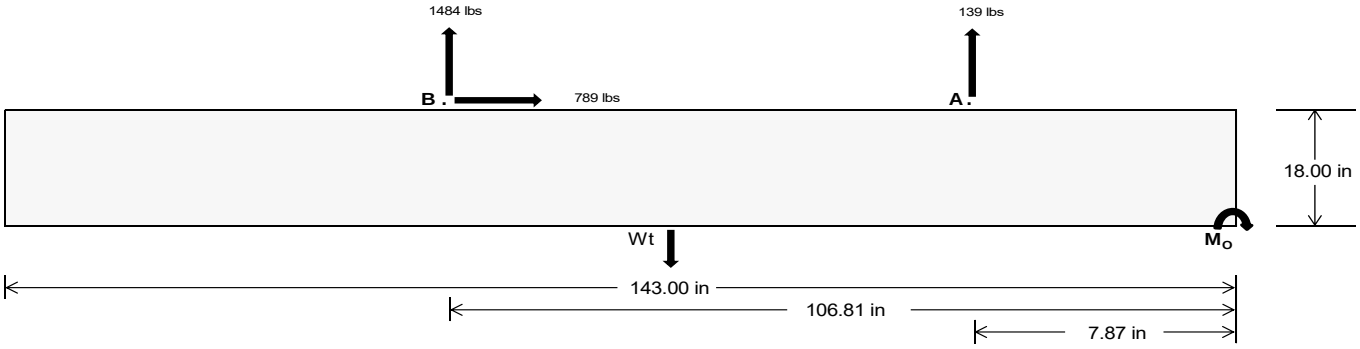
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	622.62	6448.19	k
Compressive Load =	3785.26	4984.13	k
Lateral Load =	343.70	3419.93	k
Moment (Weak Axis) =	0.69	0.30	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

Overturning Check

M_O =	173805.2 in-lbs
Resisting Force Required =	2430.84 lbs
S.F. =	1.67
Weight Required =	4051.40 lbs
Minimum Width =	35 in
Weight Provided =	7559.64 lbs

Sliding

Force =	789.12 lbs
Friction =	0.4
Weight Required =	1972.80 lbs
Resisting Weight =	7559.64 lbs
Additional Weight Required =	0 lbs

Cohesion

Sliding Force =	789.12 lbs
Cohesion =	130 psf
Area =	34.76 ft^2
Resisting =	3779.82 lbs
Additional Weight Required =	0 lbs

Shear Key

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Footing Reinforcement

Use fiber reinforcing with (2) #5 rebar.

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.

Use a 143in long x 35in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Use a 143in long x 35in wide x 18in tall ballast foundation. Cohesion is OK.

Shear key is not required.

Bearing Pressure

	Ballast Width			
	35 in	36 in	37 in	38 in
P_{ftg} = (145 pcf)(11.92 ft)(1.5 ft)(2.92 ft) =	7560 lbs	7776 lbs	7992 lbs	8208 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in	35 in	36 in	37 in	38 in
F_A	1261 lbs	1261 lbs	1261 lbs	1261 lbs	1422 lbs	1422 lbs	1422 lbs	1422 lbs	1895 lbs	1895 lbs	1895 lbs	1895 lbs	-278 lbs	-278 lbs	-278 lbs	-278 lbs
F_B	1303 lbs	1303 lbs	1303 lbs	1303 lbs	2048 lbs	2048 lbs	2048 lbs	2048 lbs	2393 lbs	2393 lbs	2393 lbs	2393 lbs	-2968 lbs	-2968 lbs	-2968 lbs	-2968 lbs
F_V	151 lbs	151 lbs	151 lbs	151 lbs	1414 lbs	1414 lbs	1414 lbs	1414 lbs	1161 lbs	1161 lbs	1161 lbs	1161 lbs	-1578 lbs	-1578 lbs	-1578 lbs	-1578 lbs
P_{total}	10123 lbs	10339 lbs	10555 lbs	10771 lbs	11030 lbs	11246 lbs	11462 lbs	11678 lbs	11848 lbs	12064 lbs	12280 lbs	12495 lbs	1289 lbs	1419 lbs	1549 lbs	1678 lbs
M	3080 lbs-ft	3080 lbs-ft	3080 lbs-ft	3080 lbs-ft	3634 lbs-ft	3634 lbs-ft	3634 lbs-ft	3634 lbs-ft	4748 lbs-ft	4748 lbs-ft	4748 lbs-ft	4748 lbs-ft	4890 lbs-ft	4890 lbs-ft	4890 lbs-ft	4890 lbs-ft
e	0.30 ft	0.30 ft	0.29 ft	0.29 ft	0.33 ft	0.32 ft	0.32 ft	0.31 ft	0.40 ft	0.39 ft	0.39 ft	0.38 ft	3.79 ft	3.45 ft	3.16 ft	2.91 ft
L/6	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft	1.99 ft
f_{min}	246.6 psf	245.8 psf	245.1 psf	244.3 psf	264.7 psf	263.4 psf	262.1 psf	261.0 psf	272.1 psf	270.6 psf	269.1 psf	267.8 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	335.9 psf	332.6 psf	329.5 psf	326.5 psf	370.0 psf	365.7 psf	361.7 psf	357.9 psf	409.6 psf	404.3 psf	399.3 psf	394.5 psf	136.1 psf	125.5 psf	119.6 psf	116.0 psf

Maximum Bearing Pressure = 410 psf
Allowable Bearing Pressure = 1500 psf

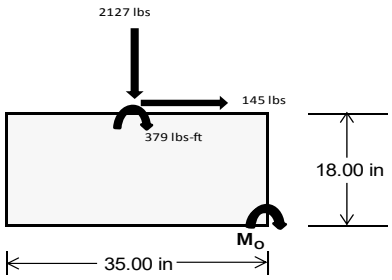
Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O =	2505.3 ft-lbs
Resisting Force Required =	1717.91 lbs
S.F. =	1.67
Weight Required =	2863.19 lbs
Minimum Width =	35 in in
Weight Provided =	7559.64 lbs

A minimum 143in long x 35in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	35 in			35 in			35 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	290 lbs	588 lbs	190 lbs	808 lbs	2127 lbs	731 lbs	120 lbs	172 lbs	21 lbs
F_V	202 lbs	197 lbs	205 lbs	148 lbs	145 lbs	160 lbs	202 lbs	198 lbs	204 lbs
P_{total}	9649 lbs	9947 lbs	9549 lbs	9717 lbs	11036 lbs	9640 lbs	2856 lbs	2909 lbs	2757 lbs
M	800 lbs-ft	787 lbs-ft	810 lbs-ft	596 lbs-ft	596 lbs-ft	635 lbs-ft	799 lbs-ft	785 lbs-ft	804 lbs-ft
e	0.08 ft	0.08 ft	0.08 ft	0.06 ft	0.05 ft	0.07 ft	0.28 ft	0.27 ft	0.29 ft
L/6	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft	0.49 ft
f_{min}	230.3 psf	239.6 psf	226.8 psf	244.3 psf	282.2 psf	239.8 psf	34.9 psf	37.2 psf	31.8 psf
f_{max}	324.9 psf	332.8 psf	322.7 psf	314.9 psf	352.8 psf	314.9 psf	129.5 psf	130.1 psf	126.9 psf

Maximum Bearing Pressure = 353 psf
Allowable Bearing Pressure = 1500 psf

Use a 143in long x 35in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 143in long x 32in wide x 18in tall ballast foundation and fiber reinforcing with (2) #5 rebar.

5.3 Foundation Anchors

Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

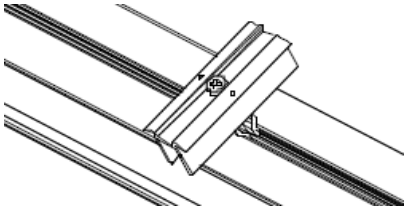
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 80mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

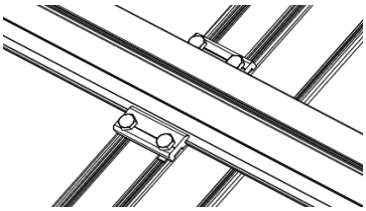
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.852 k
Allowable Uplift	=	1.214 k
Utilization	=	70%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	2.430 k
Allowable Uplift	=	4.357 k
Utilization	=	56%



6.2 Strut Connections

The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Single M12 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut

Maximum Axial Load	=	2.912 k
M12 Bolt Capacity	=	12.808 k
Strut Bearing Capacity	=	7.421 k
Utilization	=	39%

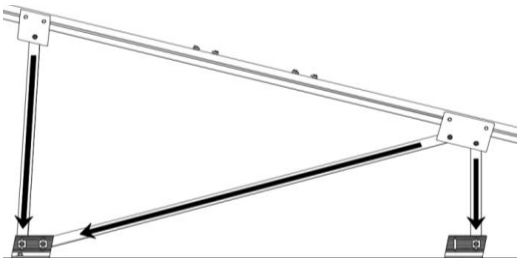
Rear Strut

Maximum Axial Load	=	4.388 k
M12 Bolt Capacity	=	12.808 k
Strut Bearing Capacity	=	7.421 k
Utilization	=	59%

Diagonal Strut

Maximum Axial Load	=	2.435 k
M12 Bolt Shear Capacity	=	12.808 k
Strut Bearing Capacity	=	7.421 k
Utilization	=	33%

Bolt and bearing capacities are accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)



Struts under compression are shown to demonstrate the load transfer from the girder. Single M12 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

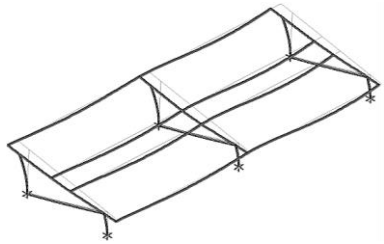
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	56.48 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.130 in
Max Drift, Δ_{MAX}	=	0.677 in

0.677 ≤ 1.13, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 96 in

J = 0.432

265.581

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.0 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

$\varphi F_L St$= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

$M_{max}St$ = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 96

J = 0.432

168.894

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.1

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

$M_{max}Wk$ = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **BF0**

Strong Axis:

3.4.14

L_b = 104.56 in
J = 1.08
179.85

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 29.0 ksi

3.4.16

b/t = 16.2

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

Weak Axis:

3.4.14

L_b = 104.56
J = 1.08
190.335

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 28.9

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

3.4.16.1 Used

Rb/t = 18.1

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 31.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 35.2

m = 0.68

C_0 = 41.067

Cc = 43.717

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 73.8

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 29.0 ksi

Ix = 984962 mm^4

2.366 in^4

y = 43.717 mm

Sx = 1.375 in^3

$M_{max}St$ = 3.323 k-ft

3.4.18

h/t = 16.2

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40

Cc = 40

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 33.3 ksi

Iy = 923544 mm^4

2.219 in^4

x = 40 mm

Sy = 1.409 in^3

$M_{max}Wk$ = 3.904 k-ft

Compression

3.4.9

b/t = 16.2

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

b/t = 7.4

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 18.1

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 31.09 ksi

φF_L= 31.09 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.55 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 24.8 in

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 24.8

J = 0.942

38.7028

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 0.57371

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

S1* = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

S2* = 1.23671

φcc = 0.87952

φF_L = φcc(Bc-Dc*λ)

φF_L = 28.0279 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 28.03 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 28.85 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 98.03 in

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L = 29.4 ksi

Weak Axis:

3.4.14

L_b = 98.03

J = 0.942

152.985

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L = 29.4

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17 \frac{\theta_y}{\theta_b} Fcy}{1.6Dt} \right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 2.26776

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi} \sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.89749

φF_L= (φccFcy)/(λ²)

φF_L= 6.10803 ksi

3.4.9

b/t = 24.5
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

b/t = 24.5
S1 = 12.21
S2 = 32.70
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 6.11 ksi
A = 663.99 mm^2
1.03 in^2
P_{max} = 6.29 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 69.80 in
J = 0.942
108.93

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.0 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

Weak Axis:

3.4.14

L_b = 69.8
J = 0.942
108.93

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.0

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.61471

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.80606

φF_L= (φccFcy)/(λ²)

φF_L= 10.8205 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi y Fcy$

φF_L = 33.25 ksi

φF_L = 10.82 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 11.14 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL			.8			8		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-9.843	-9.843	0	0
2	M14	Y	-9.843	-9.843	0	0
3	M15	Y	-9.843	-9.843	0	0
4	M16	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-5.454	-5.454	0	0
2	M14	Y	-5.454	-5.454	0	0
3	M15	Y	-5.454	-5.454	0	0
4	M16	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-55.176	-55.176	0	0
2	M14	Y	-55.176	-55.176	0	0
3	M15	Y	-55.176	-55.176	0	0
4	M16	Y	-55.176	-55.176	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-111.061	-111.061	0	0
2	M14	y	-111.061	-111.061	0	0
3	M15	y	-171.639	-171.639	0	0
4	M16	y	-171.639	-171.639	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	252.41	252.41	0	0
2	M14	y	191.832	191.832	0	0
3	M15	y	100.964	100.964	0	0
4	M16	y	100.964	100.964	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	7.874	7.874	0	0
2	M14	Z	7.874	7.874	0	0
3	M15	Z	7.874	7.874	0	0
4	M16	Z	7.874	7.874	0	0
5	M13	Z	0	0	0	0
6	M14	Z	0	0	0	0
7	M15	Z	0	0	0	0
8	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	708.623	2	1243.031	2	.632	1	.003	1	0	1	0	1
2		min	-869.033	3	-1577.122	3	-43.434	5	-.229	4	0	1	0	1
3	N7	max	.028	9	1085.391	1	-.7	12	-.001	12	0	1	0	1
4		min	-.235	2	-126.61	3	-264.385	4	-.527	4	0	1	0	1
5	N15	max	0	4	2911.738	1	0	2	0	9	0	1	0	1
6		min	-2.391	2	-478.939	3	-250.54	4	-.507	4	0	1	0	1
7	N16	max	2408.79	2	3833.948	2	0	12	0	12	0	1	0	1
8		min	-2630.712	3	-4960.145	3	-43.476	5	-.231	4	0	1	0	1
9	N23	max	.04	14	1085.391	1	10.733	1	.021	1	0	1	0	1
10		min	-.235	2	-126.61	3	-256.388	5	-.514	4	0	1	0	1
11	N24	max	708.623	2	1243.031	2	-.056	12	0	12	0	1	0	1
12		min	-869.033	3	-1577.122	3	-44.133	5	-.23	4	0	1	0	1
13	Totals:	max	3823.174	2	10999.549	2	0	9						
14		min	-4369.332	3	-8846.548	3	-897.049	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M13	1	max	69.838	4	433.993	2	-8.22	12	0	15	.179	1	0	4
2			min	4.692	12	-743.679	3	-162.463	1	-.015	2	.013	12	0	3
3		2	max	64.114	1	302.317	1	-6.652	12	0	15	.109	4	.564	3
4			min	4.692	12	-524.359	3	-124.183	1	-.015	2	.003	10	-.327	1
5		3	max	64.114	1	170.867	1	-5.084	12	0	15	.065	5	.932	3
6			min	4.692	12	-305.04	3	-85.904	1	-.015	2	-.042	1	-.537	1
7		4	max	64.114	1	39.417	1	-3.515	12	0	15	.036	5	1.106	3
8			min	4.692	12	-85.72	3	-47.625	1	-.015	2	-.101	1	-.631	1
9		5	max	64.114	1	133.599	3	-.032	10	0	15	.01	5	1.085	3
10			min	4.692	12	-93.669	2	-31.218	4	-.015	2	-.126	1	-.608	1
11		6	max	64.114	1	352.919	3	28.933	1	0	15	-.006	12	.868	3
12			min	1.789	15	-225.585	2	-26.059	5	-.015	2	-.118	1	-.467	1
13		7	max	64.114	1	572.238	3	67.212	1	0	15	-.006	12	.457	3
14			min	-7.663	5	-357.5	2	-23.671	5	-.015	2	-.075	1	-.21	1
15		8	max	64.114	1	791.558	3	105.491	1	0	15	.004	2	.172	2
16			min	-18.153	5	-489.416	2	-21.284	5	-.015	2	-.057	4	-.149	3
17		9	max	64.114	1	1010.877	3	143.77	1	0	15	.113	1	.666	2
18			min	-28.642	5	-621.331	2	-18.897	5	-.015	2	-.074	5	-.95	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
19		10	max	64.114	1	753.247	2	-5.895	12	.015	2	.257	1	1.277	2
20			min	4.692	12	-1230.197	3	-182.05	1	-.004	3	.004	12	-1.946	3
21		11	max	64.114	1	621.331	2	-4.326	12	.015	2	.113	4	.666	2
22			min	4.692	12	-1010.877	3	-143.77	1	0	15	-.002	3	-.95	3
23		12	max	64.114	1	489.416	2	-2.758	12	.015	2	.057	4	.172	2
24			min	4.692	12	-791.558	3	-105.491	1	0	15	-.006	3	-.149	3
25		13	max	64.114	1	357.5	2	-1.19	12	.015	2	.027	5	.457	3
26			min	4.692	12	-572.238	3	-67.212	1	0	15	-.075	1	-.21	1
27		14	max	64.114	1	225.585	2	.818	3	.015	2	0	15	.868	3
28			min	3.407	15	-352.919	3	-36.176	4	0	15	-.118	1	-.467	1
29		15	max	64.114	1	93.669	2	9.346	1	.015	2	-.005	12	1.085	3
30			min	-5.328	5	-133.599	3	-27.164	5	0	15	-.126	1	-.608	1
31		16	max	64.114	1	85.72	3	47.625	1	.015	2	-.002	12	1.106	3
32			min	-15.818	5	-39.417	1	-24.777	5	0	15	-.101	1	-.631	1
33		17	max	64.114	1	305.04	3	85.904	1	.015	2	.003	3	.932	3
34			min	-26.307	5	-170.867	1	-22.39	5	0	15	-.08	4	-.537	1
35		18	max	64.114	1	524.359	3	124.183	1	.015	2	.052	1	.564	3
36			min	-36.796	5	-302.317	1	-20.002	5	0	15	-.089	5	-.327	1
37		19	max	64.114	1	743.679	3	162.463	1	.015	2	.179	1	0	1
38			min	-47.286	5	-433.993	2	-17.615	5	0	15	-.105	5	0	3
39	M14	1	max	45.684	4	502.636	2	-8.531	12	.013	3	.247	4	0	1
40			min	2.498	12	-600.634	3	-169.367	1	-.016	2	.015	12	0	3
41		2	max	40.037	1	370.72	2	-6.963	12	.013	3	.169	4	.46	3
42			min	2.498	12	-435.162	3	-131.088	1	-.016	2	.006	10	-.388	2
43		3	max	40.037	1	238.804	2	-5.395	12	.013	3	.101	5	.774	3
44			min	2.498	12	-269.69	3	-92.809	1	-.016	2	-.017	1	-.659	2
45		4	max	40.037	1	106.889	2	-3.826	12	.013	3	.057	5	.94	3
46			min	2.498	12	-104.217	3	-61.471	4	-.016	2	-.083	1	-.813	2
47		5	max	40.037	1	61.255	3	-.75	10	.013	3	.015	5	.959	3
48			min	-4.997	5	-28.907	1	-50.761	4	-.016	2	-.114	1	-.849	2
49		6	max	40.037	1	226.727	3	22.029	1	.013	3	-.005	12	.831	3
50			min	-15.486	5	-160.357	1	-43.722	5	-.016	2	-.112	1	-.768	2
51		7	max	40.037	1	392.2	3	60.308	1	.013	3	-.005	12	.556	3
52			min	-25.976	5	-291.808	1	-41.334	5	-.016	2	-.081	4	-.57	2
53		8	max	40.037	1	557.672	3	98.587	1	.013	3	.002	10	.134	3
54			min	-36.465	5	-423.258	1	-38.947	5	-.016	2	-.102	4	-.255	2
55		9	max	40.037	1	723.145	3	136.866	1	.013	3	.1	1	.206	1
56			min	-46.954	5	-554.708	1	-36.56	5	-.016	2	-.132	5	-.436	3
57		10	max	70.934	4	686.159	1	-5.584	12	.016	2	.248	4	.757	1
58			min	2.498	12	-888.617	3	-175.145	1	-.013	3	.003	12	-1.152	3
59		11	max	60.445	4	554.708	1	-4.016	12	.016	2	.168	4	.206	1
60			min	2.498	12	-723.145	3	-136.866	1	-.013	3	-.002	3	-.436	3
61		12	max	49.956	4	423.258	1	-2.447	12	.016	2	.098	4	.134	3
62			min	2.498	12	-557.672	3	-98.587	1	-.013	3	-.006	3	-.255	2
63		13	max	40.037	1	291.808	1	-.879	12	.016	2	.053	5	.556	3
64			min	2.498	12	-392.2	3	-62.544	4	-.013	3	-.075	1	-.57	2
65		14	max	40.037	1	160.357	1	1.289	3	.016	2	.011	5	.831	3
66			min	2.498	12	-226.727	3	-51.834	4	-.013	3	-.112	1	-.768	2
67		15	max	40.037	1	28.907	1	16.25	1	.016	2	-.004	12	.959	3
68			min	2.498	12	-61.255	3	-43.962	5	-.013	3	-.114	1	-.849	2
69		16	max	40.037	1	104.217	3	54.53	1	.016	2	-.001	12	.94	3
70			min	-.974	5	-106.889	2	-41.575	5	-.013	3	-.086	4	-.813	2
71		17	max	40.037	1	269.69	3	92.809	1	.016	2	.005	3	.774	3
72			min	-11.464	5	-238.804	2	-39.188	5	-.013	3	-.108	4	-.659	2
73		18	max	40.037	1	435.162	3	131.088	1	.016	2	.082	1	.46	3
74			min	-21.953	5	-370.72	2	-36.801	5	-.013	3	-.137	5	-.388	2
75		19	max	40.037	1	600.634	3	169.367	1	.016	2	.216	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
76			min	-32.442	5	-502.636	2	-34.414	5	-.013	3	-.168	5	0	3
77	M15	1	max	83.092	5	684.454	2	-8.396	12	.016	2	.314	4	0	2
78			min	-42.293	1	-328.919	3	-169.346	1	-.011	3	.015	12	0	3
79		2	max	72.602	5	498.691	2	-6.828	12	.016	2	.221	4	.255	3
80			min	-42.293	1	-244.218	3	-131.067	1	-.011	3	.006	10	-.526	2
81		3	max	62.113	5	312.928	2	-5.259	12	.016	2	.139	5	.434	3
82			min	-42.293	1	-159.518	3	-92.788	1	-.011	3	-.017	1	-.887	2
83		4	max	51.624	5	127.166	2	-3.691	12	.016	2	.08	5	.538	3
84			min	-42.293	1	-74.817	3	-77.692	4	-.011	3	-.083	1	-1.082	2
85		5	max	41.134	5	9.884	3	-.813	10	.016	2	.024	5	.567	3
86			min	-42.293	1	-58.597	2	-66.982	4	-.011	3	-.114	1	-1.113	2
87		6	max	30.645	5	94.585	3	22.05	1	.016	2	-.005	12	.521	3
88			min	-42.293	1	-244.36	2	-59.902	5	-.011	3	-.112	1	-.978	2
89		7	max	20.156	5	179.286	3	60.329	1	.016	2	-.005	12	.399	3
90			min	-42.293	1	-430.122	2	-57.515	5	-.011	3	-.101	4	-.678	2
91		8	max	9.666	5	263.986	3	98.608	1	.016	2	.002	10	.202	3
92			min	-42.293	1	-615.885	2	-55.128	5	-.011	3	-.136	4	-.213	2
93		9	max	-.46	15	348.687	3	136.887	1	.016	2	.1	1	.417	2
94			min	-42.293	1	-801.648	2	-52.741	5	-.011	3	-.181	5	-.07	3
95		10	max	-3.163	12	837.64	1	72.293	2	.011	3	.311	4	1.212	2
96			min	-42.293	1	-987.41	2	-175.166	1	-.016	2	.004	12	-.418	3
97		11	max	-3.163	12	801.648	2	-4.151	12	.011	3	.217	4	.417	2
98			min	-42.293	1	-348.687	3	-136.887	1	-.016	2	-.001	3	-.07	3
99		12	max	-3.163	12	615.885	2	-2.582	12	.011	3	.133	4	.202	3
100			min	-42.293	1	-263.986	3	-98.608	1	-.016	2	-.006	3	-.213	2
101		13	max	-3.163	12	430.122	2	-1.014	12	.011	3	.073	5	.399	3
102			min	-42.293	1	-179.286	3	-78.802	4	-.016	2	-.075	1	-.678	2
103		14	max	-3.163	12	244.36	2	1.064	3	.011	3	.017	5	.521	3
104			min	-46.659	4	-94.585	3	-68.092	4	-.016	2	-.112	1	-.978	2
105		15	max	-3.163	12	58.597	2	16.229	1	.011	3	-.004	12	.567	3
106			min	-57.148	4	-9.884	3	-60.145	5	-.016	2	-.114	1	-1.113	2
107		16	max	-3.163	12	74.817	3	54.508	1	.011	3	-.002	12	.538	3
108			min	-67.637	4	-127.166	2	-57.758	5	-.016	2	-.109	4	-1.082	2
109		17	max	-3.163	12	159.518	3	92.788	1	.011	3	.004	3	.434	3
110			min	-78.127	4	-312.928	2	-55.371	5	-.016	2	-.146	4	-.887	2
111		18	max	-3.163	12	244.218	3	131.067	1	.011	3	.082	1	.255	3
112			min	-88.616	4	-498.691	2	-52.984	5	-.016	2	-.189	5	-.526	2
113		19	max	-3.163	12	328.919	3	169.346	1	.011	3	.216	1	0	2
114			min	-99.105	4	-684.454	2	-50.597	5	-.016	2	-.235	5	0	5
115	M16	1	max	77.924	5	618.918	2	-7.797	12	.01	1	.223	4	0	2
116			min	-71.958	1	-275.243	3	-163.027	1	-.013	3	.012	12	0	3
117		2	max	67.435	5	433.155	2	-6.229	12	.01	1	.15	4	.207	3
118			min	-71.958	1	-190.542	3	-124.748	1	-.013	3	.004	10	-.468	2
119		3	max	56.945	5	247.393	2	-4.66	12	.01	1	.094	5	.339	3
120			min	-71.958	1	-105.841	3	-86.469	1	-.013	3	-.04	1	-.77	2
121		4	max	46.456	5	61.63	2	-3.092	12	.01	1	.055	5	.395	3
122			min	-71.958	1	-21.14	3	-54.507	4	-.013	3	-.1	1	-.907	2
123		5	max	35.967	5	63.56	3	-.308	10	.01	1	.018	5	.376	3
124			min	-71.958	1	-124.133	2	-43.797	4	-.013	3	-.126	1	-.88	2
125		6	max	25.477	5	148.261	3	28.369	1	.01	1	-.006	12	.282	3
126			min	-71.958	1	-309.895	2	-38.454	5	-.013	3	-.118	1	-.687	2
127		7	max	14.988	5	232.962	3	66.648	1	.01	1	-.005	12	.113	3
128			min	-71.958	1	-495.658	2	-36.067	5	-.013	3	-.075	1	-.329	2
129		8	max	4.499	5	317.663	3	104.927	1	.01	1	.003	2	.194	2
130			min	-71.958	1	-681.421	2	-33.68	5	-.013	3	-.083	4	-.132	3
131		9	max	-3.977	15	402.364	3	143.206	1	.01	1	.111	1	.883	2
132			min	-71.958	1	-867.184	2	-31.293	5	-.013	3	-.111	5	-.452	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
133		10	max	-4.671	12	1052.946	2	-6.318	12	.013	3	.256	1	1.736	2
134			min	-71.958	1	-487.064	3	-181.485	1	-.01	1	.006	12	-.847	3
135		11	max	-1.87	15	867.184	2	-4.75	12	.013	3	.15	4	.883	2
136			min	-71.958	1	-402.364	3	-143.206	1	-.01	1	0	3	-.452	3
137		12	max	-4.671	12	681.421	2	-3.181	12	.013	3	.083	4	.194	2
138			min	-71.958	1	-317.663	3	-104.927	1	-.01	1	-.004	3	-.132	3
139		13	max	-4.671	12	495.658	2	-1.613	12	.013	3	.041	5	.113	3
140			min	-71.958	1	-232.962	3	-66.648	1	-.01	1	-.075	1	-.329	2
141		14	max	-4.671	12	309.895	2	.111	3	.013	3	.003	5	.282	3
142			min	-71.958	1	-148.261	3	-48.568	4	-.01	1	-.118	1	-.687	2
143		15	max	-4.671	12	124.133	2	9.91	1	.013	3	-.005	12	.376	3
144			min	-71.958	1	-63.56	3	-39.533	5	-.01	1	-.126	1	-.88	2
145		16	max	-4.671	12	21.14	3	48.189	1	.013	3	-.003	12	.395	3
146			min	-72.115	4	-61.63	2	-37.146	5	-.01	1	-.1	1	-.907	2
147		17	max	-4.671	12	105.841	3	86.469	1	.013	3	.001	3	.339	3
148			min	-82.604	4	-247.393	2	-34.759	5	-.01	1	-.109	4	-.77	2
149		18	max	-4.671	12	190.542	3	124.748	1	.013	3	.054	1	.207	3
150			min	-93.094	4	-433.155	2	-32.372	5	-.01	1	-.129	5	-.468	2
151		19	max	-4.671	12	275.243	3	163.027	1	.013	3	.182	1	0	2
152			min	-103.583	4	-618.918	2	-29.985	5	-.01	1	-.157	5	0	5
153	M2	1	max	1068.235	2	2.07	4	.51	1	0	3	0	3	0	1
154			min	-1394.536	3	.506	15	-36.684	4	0	4	0	1	0	1
155		2	max	1068.708	2	2.032	4	.51	1	0	3	0	1	0	15
156			min	-1394.18	3	.497	15	-37.095	4	0	4	-.012	4	0	4
157		3	max	1069.182	2	1.995	4	.51	1	0	3	0	1	0	15
158			min	-1393.825	3	.489	15	-37.507	4	0	4	-.024	4	-.001	4
159		4	max	1069.656	2	1.958	4	.51	1	0	3	0	1	0	15
160			min	-1393.47	3	.48	15	-37.918	4	0	4	-.036	4	-.002	4
161		5	max	1070.13	2	1.921	4	.51	1	0	3	0	1	0	15
162			min	-1393.115	3	.471	15	-38.329	4	0	4	-.048	4	-.003	4
163		6	max	1070.603	2	1.884	4	.51	1	0	3	0	1	0	15
164			min	-1392.759	3	.462	15	-38.741	4	0	4	-.06	4	-.003	4
165		7	max	1071.077	2	1.847	4	.51	1	0	3	0	1	0	15
166			min	-1392.404	3	.454	15	-39.152	4	0	4	-.073	4	-.004	4
167		8	max	1071.551	2	1.81	4	.51	1	0	3	.001	1	-.001	15
168			min	-1392.049	3	.445	15	-39.563	4	0	4	-.085	4	-.004	4
169		9	max	1072.025	2	1.773	4	.51	1	0	3	.001	1	-.001	15
170			min	-1391.693	3	.436	15	-39.975	4	0	4	-.098	4	-.005	4
171		10	max	1072.498	2	1.736	4	.51	1	0	3	.001	1	-.001	15
172			min	-1391.338	3	.428	15	-40.386	4	0	4	-.111	4	-.005	4
173		11	max	1072.972	2	1.699	4	.51	1	0	3	.002	1	-.001	15
174			min	-1390.983	3	.419	15	-40.797	4	0	4	-.124	4	-.006	4
175		12	max	1073.446	2	1.662	4	.51	1	0	3	.002	1	-.002	15
176			min	-1390.627	3	.41	15	-41.209	4	0	4	-.137	4	-.007	4
177		13	max	1073.919	2	1.625	4	.51	1	0	3	.002	1	-.002	15
178			min	-1390.272	3	.401	15	-41.62	4	0	4	-.15	4	-.007	4
179		14	max	1074.393	2	1.588	4	.51	1	0	3	.002	1	-.002	15
180			min	-1389.917	3	.393	15	-42.031	4	0	4	-.164	4	-.008	4
181		15	max	1074.867	2	1.551	4	.51	1	0	3	.002	1	-.002	15
182			min	-1389.562	3	.384	15	-42.443	4	0	4	-.177	4	-.008	4
183		16	max	1075.341	2	1.514	4	.51	1	0	3	.002	1	-.002	15
184			min	-1389.206	3	.372	12	-42.854	4	0	4	-.191	4	-.009	4
185		17	max	1075.814	2	1.477	4	.51	1	0	3	.003	1	-.002	15
186			min	-1388.851	3	.358	12	-43.265	4	0	4	-.205	4	-.009	4
187		18	max	1076.288	2	1.44	4	.51	1	0	3	.003	1	-.002	15
188			min	-1388.496	3	.343	12	-43.677	4	0	4	-.219	4	-.01	4
189		19	max	1076.762	2	1.403	4	.51	1	0	3	.003	1	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
190			min	-1388.14	3	.329	12	-44.088	4	0	4	-.233	4	-.01	4
191	M3	1	max	663.645	2	9.024	4	.233	1	0	12	0	1	.01	4
192			min	-807.796	3	2.135	15	-.621	5	0	4	-.015	4	.002	15
193		2	max	663.475	2	8.152	4	.233	1	0	12	0	1	.006	4
194			min	-807.923	3	1.93	15	-.014	15	0	4	-.015	4	.001	12
195		3	max	663.305	2	7.28	4	.705	4	0	12	0	1	.003	2
196			min	-808.051	3	1.725	15	.015	12	0	4	-.014	4	0	3
197		4	max	663.134	2	6.408	4	1.312	4	0	12	0	1	0	2
198			min	-808.179	3	1.52	15	.015	12	0	4	-.014	4	-.002	3
199		5	max	662.964	2	5.536	4	1.919	4	0	12	0	1	0	15
200			min	-808.307	3	1.315	15	.015	12	0	4	-.013	5	-.004	3
201		6	max	662.794	2	4.664	4	2.527	4	0	12	0	1	-.001	15
202			min	-808.434	3	1.11	15	.015	12	0	4	-.012	5	-.006	6
203		7	max	662.623	2	3.792	4	3.134	4	0	12	0	1	-.002	15
204			min	-808.562	3	.905	15	.015	12	0	4	-.011	5	-.008	6
205		8	max	662.453	2	2.92	4	3.741	4	0	12	0	1	-.002	15
206			min	-808.69	3	.7	15	.015	12	0	4	-.009	5	-.01	6
207		9	max	662.283	2	2.048	4	4.348	4	0	12	.001	1	-.003	15
208			min	-808.818	3	.495	15	.015	12	0	4	-.008	5	-.011	6
209		10	max	662.112	2	1.176	4	4.955	4	0	12	.001	1	-.003	15
210			min	-808.945	3	.29	15	.015	12	0	4	-.005	5	-.012	6
211		11	max	661.942	2	.377	2	5.562	4	0	12	.001	1	-.003	15
212			min	-809.073	3	-.066	3	.015	12	0	4	-.003	5	-.012	6
213		12	max	661.772	2	-.12	15	6.169	4	0	12	.001	1	-.003	15
214			min	-809.201	3	-.576	3	.015	12	0	4	0	5	-.012	6
215		13	max	661.601	2	-.325	15	6.776	4	0	12	.003	4	-.003	15
216			min	-809.329	3	-1.441	6	.015	12	0	4	0	12	-.011	6
217		14	max	661.431	2	-.53	15	7.384	4	0	12	.007	4	-.002	15
218			min	-809.456	3	-2.313	6	.015	12	0	4	0	12	-.011	6
219		15	max	661.261	2	-.735	15	7.991	4	0	12	.01	4	-.002	15
220			min	-809.584	3	-3.185	6	.015	12	0	4	0	12	-.009	6
221		16	max	661.09	2	-.94	15	8.598	4	0	12	.014	4	-.002	15
222			min	-809.712	3	-4.057	6	.015	12	0	4	0	12	-.008	6
223		17	max	660.92	2	-1.145	15	9.205	4	0	12	.018	4	-.001	15
224			min	-809.84	3	-4.929	6	.015	12	0	4	0	12	-.005	6
225		18	max	660.75	2	-1.35	15	9.812	4	0	12	.023	4	0	15
226			min	-809.968	3	-5.801	6	.015	12	0	4	0	12	-.003	6
227		19	max	660.579	2	-1.555	15	10.419	4	0	12	.028	4	0	1
228			min	-810.095	3	-6.673	6	.015	12	0	4	0	12	0	1
229	M4	1	max	1082.325	1	0	1	-.699	12	0	1	.019	4	0	1
230			min	-128.91	3	0	1	-262.71	4	0	1	0	12	0	1
231		2	max	1082.495	1	0	1	-.699	12	0	1	0	1	0	1
232			min	-128.782	3	0	1	-262.858	4	0	1	-.011	4	0	1
233		3	max	1082.666	1	0	1	-.699	12	0	1	0	12	0	1
234			min	-128.654	3	0	1	-263.006	4	0	1	-.041	4	0	1
235		4	max	1082.836	1	0	1	-.699	12	0	1	0	12	0	1
236			min	-128.527	3	0	1	-263.153	4	0	1	-.071	4	0	1
237		5	max	1083.006	1	0	1	-.699	12	0	1	0	12	0	1
238			min	-128.399	3	0	1	-263.301	4	0	1	-.102	4	0	1
239		6	max	1083.177	1	0	1	-.699	12	0	1	0	12	0	1
240			min	-128.271	3	0	1	-263.448	4	0	1	-.132	4	0	1
241		7	max	1083.347	1	0	1	-.699	12	0	1	0	12	0	1
242			min	-128.143	3	0	1	-263.596	4	0	1	-.162	4	0	1
243		8	max	1083.517	1	0	1	-.699	12	0	1	0	12	0	1
244			min	-128.016	3	0	1	-263.744	4	0	1	-.192	4	0	1
245		9	max	1083.688	1	0	1	-.699	12	0	1	0	12	0	1
246			min	-127.888	3	0	1	-263.891	4	0	1	-.223	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
247		10	max	1083.858	1	0	1	-.699	12	0	1	0	12	0	1
248			min	-127.76	3	0	1	-264.039	4	0	1	-.253	4	0	1
249		11	max	1084.028	1	0	1	-.699	12	0	1	0	12	0	1
250			min	-127.632	3	0	1	-264.187	4	0	1	-.283	4	0	1
251		12	max	1084.199	1	0	1	-.699	12	0	1	0	12	0	1
252			min	-127.505	3	0	1	-264.334	4	0	1	-.314	4	0	1
253		13	max	1084.369	1	0	1	-.699	12	0	1	0	12	0	1
254			min	-127.377	3	0	1	-264.482	4	0	1	-.344	4	0	1
255		14	max	1084.539	1	0	1	-.699	12	0	1	0	12	0	1
256			min	-127.249	3	0	1	-264.63	4	0	1	-.374	4	0	1
257		15	max	1084.71	1	0	1	-.699	12	0	1	-.001	12	0	1
258			min	-127.121	3	0	1	-264.777	4	0	1	-.405	4	0	1
259		16	max	1084.88	1	0	1	-.699	12	0	1	-.001	12	0	1
260			min	-126.994	3	0	1	-264.925	4	0	1	-.435	4	0	1
261		17	max	1085.051	1	0	1	-.699	12	0	1	-.001	12	0	1
262			min	-126.866	3	0	1	-265.072	4	0	1	-.466	4	0	1
263		18	max	1085.221	1	0	1	-.699	12	0	1	-.001	12	0	1
264			min	-126.738	3	0	1	-265.22	4	0	1	-.496	4	0	1
265		19	max	1085.391	1	0	1	-.699	12	0	1	-.001	12	0	1
266			min	-126.61	3	0	1	-265.368	4	0	1	-.527	4	0	1
267	M6	1	max	3269.952	2	2.386	2	0	1	0	1	0	4	0	1
268			min	-4387.712	3	.162	3	-37.088	4	0	4	0	1	0	1
269		2	max	3270.426	2	2.357	2	0	1	0	1	0	1	0	3
270			min	-4387.357	3	.141	3	-37.499	4	0	4	-.012	4	0	2
271		3	max	3270.9	2	2.328	2	0	1	0	1	0	1	0	3
272			min	-4387.002	3	.119	3	-37.911	4	0	4	-.024	4	-.002	2
273		4	max	3271.374	2	2.3	2	0	1	0	1	0	1	0	3
274			min	-4386.646	3	.097	3	-38.322	4	0	4	-.036	4	-.002	2
275		5	max	3271.847	2	2.271	2	0	1	0	1	0	1	0	3
276			min	-4386.291	3	.076	3	-38.733	4	0	4	-.049	4	-.003	2
277		6	max	3272.321	2	2.242	2	0	1	0	1	0	1	0	3
278			min	-4385.936	3	.054	3	-39.145	4	0	4	-.061	4	-.004	2
279		7	max	3272.795	2	2.213	2	0	1	0	1	0	1	0	3
280			min	-4385.581	3	.032	3	-39.556	4	0	4	-.074	4	-.004	2
281		8	max	3273.269	2	2.184	2	0	1	0	1	0	1	0	3
282			min	-4385.225	3	.011	3	-39.967	4	0	4	-.086	4	-.005	2
283		9	max	3273.742	2	2.155	2	0	1	0	1	0	1	0	3
284			min	-4384.87	3	-.011	3	-40.379	4	0	4	-.099	4	-.006	2
285		10	max	3274.216	2	2.126	2	0	1	0	1	0	1	0	3
286			min	-4384.515	3	-.033	3	-40.79	4	0	4	-.112	4	-.006	2
287		11	max	3274.69	2	2.097	2	0	1	0	1	0	1	0	3
288			min	-4384.159	3	-.054	3	-41.201	4	0	4	-.125	4	-.007	2
289		12	max	3275.164	2	2.069	2	0	1	0	1	0	1	0	3
290			min	-4383.804	3	-.076	3	-41.613	4	0	4	-.138	4	-.008	2
291		13	max	3275.637	2	2.04	2	0	1	0	1	0	1	0	3
292			min	-4383.449	3	-.097	3	-42.024	4	0	4	-.152	4	-.008	2
293		14	max	3276.111	2	2.011	2	0	1	0	1	0	1	0	3
294			min	-4383.093	3	-.119	3	-42.435	4	0	4	-.165	4	-.009	2
295		15	max	3276.585	2	1.982	2	0	1	0	1	0	1	0	3
296			min	-4382.738	3	-.141	3	-42.847	4	0	4	-.179	4	-.01	2
297		16	max	3277.059	2	1.953	2	0	1	0	1	0	1	0	3
298			min	-4382.383	3	-.162	3	-43.258	4	0	4	-.193	4	-.01	2
299		17	max	3277.532	2	1.924	2	0	1	0	1	0	1	0	3
300			min	-4382.027	3	-.184	3	-43.669	4	0	4	-.207	4	-.011	2
301		18	max	3278.006	2	1.895	2	0	1	0	1	0	1	0	3
302			min	-4381.672	3	-.206	3	-44.081	4	0	4	-.221	4	-.012	2
303		19	max	3278.48	2	1.867	2	0	1	0	1	0	1	0	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
304			min	-4381.317	3	-.227	3	-44.492	4	0	4	-.235	4	-.012	2
305	M7	1	max	2279.285	2	9.023	6	0	1	0	1	0	1	.012	2
306			min	-2433.109	3	2.118	15	-.891	5	0	4	-.015	4	0	3
307		2	max	2279.115	2	8.151	6	0	1	0	1	0	1	.009	2
308			min	-2433.236	3	1.913	15	-.284	5	0	4	-.015	4	-.002	3
309		3	max	2278.944	2	7.279	6	.379	4	0	1	0	1	.006	2
310			min	-2433.364	3	1.709	15	0	1	0	4	-.015	4	-.004	3
311		4	max	2278.774	2	6.407	6	.986	4	0	1	0	1	.003	2
312			min	-2433.492	3	1.504	15	0	1	0	4	-.015	4	-.006	3
313		5	max	2278.604	2	5.535	6	1.593	4	0	1	0	1	0	2
314			min	-2433.62	3	1.299	15	0	1	0	4	-.014	4	-.007	3
315		6	max	2278.433	2	4.663	6	2.2	4	0	1	0	1	-.001	15
316			min	-2433.747	3	1.094	15	0	1	0	4	-.013	4	-.008	3
317		7	max	2278.263	2	3.791	6	2.807	4	0	1	0	1	-.002	15
318			min	-2433.875	3	.889	15	0	1	0	4	-.012	4	-.009	3
319		8	max	2278.093	2	2.919	6	3.414	4	0	1	0	1	-.002	15
320			min	-2434.003	3	.684	15	0	1	0	4	-.01	4	-.01	4
321		9	max	2277.922	2	2.12	2	4.021	4	0	1	0	1	-.003	15
322			min	-2434.131	3	.371	12	0	1	0	4	-.009	4	-.011	4
323		10	max	2277.752	2	1.441	2	4.629	4	0	1	0	1	-.003	15
324			min	-2434.258	3	-.022	3	0	1	0	4	-.007	4	-.012	4
325		11	max	2277.581	2	.761	2	5.236	4	0	1	0	1	-.003	15
326			min	-2434.386	3	-.532	3	0	1	0	4	-.004	5	-.012	4
327		12	max	2277.411	2	.082	2	5.843	4	0	1	0	1	-.003	15
328			min	-2434.514	3	-1.041	3	0	1	0	4	-.002	5	-.012	4
329		13	max	2277.241	2	-.341	15	6.45	4	0	1	.001	4	-.003	15
330			min	-2434.642	3	-1.551	3	0	1	0	4	0	1	-.011	4
331		14	max	2277.07	2	-.546	15	7.057	4	0	1	.004	4	-.002	15
332			min	-2434.769	3	-2.313	4	0	1	0	4	0	1	-.011	4
333		15	max	2276.9	2	-.751	15	7.664	4	0	1	.008	4	-.002	15
334			min	-2434.897	3	-3.185	4	0	1	0	4	0	1	-.009	4
335		16	max	2276.73	2	-.956	15	8.271	4	0	1	.012	4	-.002	15
336			min	-2435.025	3	-4.057	4	0	1	0	4	0	1	-.008	4
337		17	max	2276.559	2	-1.161	15	8.878	4	0	1	.016	4	-.001	15
338			min	-2435.153	3	-4.929	4	0	1	0	4	0	1	-.005	4
339		18	max	2276.389	2	-1.366	15	9.485	4	0	1	.02	4	0	15
340			min	-2435.28	3	-5.801	4	0	1	0	4	0	1	-.003	4
341		19	max	2276.219	2	-1.571	15	10.093	4	0	1	.025	4	0	1
342			min	-2435.408	3	-6.673	4	0	1	0	4	0	1	0	1
343	M8	1	max	2908.672	1	0	1	0	1	0	1	.017	4	0	1
344			min	-481.239	3	0	1	-252.147	4	0	1	0	1	0	1
345		2	max	2908.842	1	0	1	0	1	0	1	0	1	0	1
346			min	-481.111	3	0	1	-252.295	4	0	1	-.012	4	0	1
347		3	max	2909.013	1	0	1	0	1	0	1	0	1	0	1
348			min	-480.983	3	0	1	-252.443	4	0	1	-.041	4	0	1
349		4	max	2909.183	1	0	1	0	1	0	1	0	1	0	1
350			min	-480.856	3	0	1	-252.59	4	0	1	-.07	4	0	1
351		5	max	2909.353	1	0	1	0	1	0	1	0	1	0	1
352			min	-480.728	3	0	1	-252.738	4	0	1	-.099	4	0	1
353		6	max	2909.524	1	0	1	0	1	0	1	0	1	0	1
354			min	-480.6	3	0	1	-252.885	4	0	1	-.128	4	0	1
355		7	max	2909.694	1	0	1	0	1	0	1	0	1	0	1
356			min	-480.472	3	0	1	-253.033	4	0	1	-.157	4	0	1
357		8	max	2909.864	1	0	1	0	1	0	1	0	1	0	1
358			min	-480.344	3	0	1	-253.181	4	0	1	-.186	4	0	1
359		9	max	2910.035	1	0	1	0	1	0	1	0	1	0	1
360			min	-480.217	3	0	1	-253.328	4	0	1	-.215	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
361		10	max	2910.205	1	0	1	0	1	0	1	0	1	0	1
362			min	-480.089	3	0	1	-253.476	4	0	1	-.244	4	0	1
363		11	max	2910.375	1	0	1	0	1	0	1	0	1	0	1
364			min	-479.961	3	0	1	-253.624	4	0	1	-.273	4	0	1
365		12	max	2910.546	1	0	1	0	1	0	1	0	1	0	1
366			min	-479.833	3	0	1	-253.771	4	0	1	-.302	4	0	1
367		13	max	2910.716	1	0	1	0	1	0	1	0	1	0	1
368			min	-479.706	3	0	1	-253.919	4	0	1	-.332	4	0	1
369		14	max	2910.886	1	0	1	0	1	0	1	0	1	0	1
370			min	-479.578	3	0	1	-254.067	4	0	1	-.361	4	0	1
371		15	max	2911.057	1	0	1	0	1	0	1	0	1	0	1
372			min	-479.45	3	0	1	-254.214	4	0	1	-.39	4	0	1
373		16	max	2911.227	1	0	1	0	1	0	1	0	1	0	1
374			min	-479.322	3	0	1	-254.362	4	0	1	-.419	4	0	1
375		17	max	2911.397	1	0	1	0	1	0	1	0	1	0	1
376			min	-479.195	3	0	1	-254.509	4	0	1	-.448	4	0	1
377		18	max	2911.568	1	0	1	0	1	0	1	0	1	0	1
378			min	-479.067	3	0	1	-254.657	4	0	1	-.478	4	0	1
379		19	max	2911.738	1	0	1	0	1	0	1	0	1	0	1
380			min	-478.939	3	0	1	-254.805	4	0	1	-.507	4	0	1
381	M10	1	max	1068.235	2	1.98	6	-.036	12	0	1	0	4	0	1
382			min	-1394.536	3	.446	15	-36.975	4	0	5	0	3	0	1
383		2	max	1068.708	2	1.943	6	-.036	12	0	1	0	10	0	15
384			min	-1394.18	3	.437	15	-37.386	4	0	5	-.012	4	0	6
385		3	max	1069.182	2	1.906	6	-.036	12	0	1	0	10	0	15
386			min	-1393.825	3	.429	15	-37.797	4	0	5	-.024	4	-.001	6
387		4	max	1069.656	2	1.869	6	-.036	12	0	1	0	10	0	15
388			min	-1393.47	3	.42	15	-38.209	4	0	5	-.036	4	-.002	6
389		5	max	1070.13	2	1.832	6	-.036	12	0	1	0	12	0	15
390			min	-1393.115	3	.411	15	-38.62	4	0	5	-.048	4	-.002	6
391		6	max	1070.603	2	1.795	6	-.036	12	0	1	0	12	0	15
392			min	-1392.759	3	.402	15	-39.031	4	0	5	-.061	4	-.003	6
393		7	max	1071.077	2	1.758	6	-.036	12	0	1	0	12	0	15
394			min	-1392.404	3	.394	15	-39.443	4	0	5	-.073	4	-.004	6
395		8	max	1071.551	2	1.721	6	-.036	12	0	1	0	12	0	15
396			min	-1392.049	3	.385	15	-39.854	4	0	5	-.086	4	-.004	6
397		9	max	1072.025	2	1.684	6	-.036	12	0	1	0	12	-.001	15
398			min	-1391.693	3	.376	15	-40.265	4	0	5	-.099	4	-.005	6
399		10	max	1072.498	2	1.647	6	-.036	12	0	1	0	12	-.001	15
400			min	-1391.338	3	.368	15	-40.677	4	0	5	-.112	4	-.005	6
401		11	max	1072.972	2	1.61	6	-.036	12	0	1	0	12	-.001	15
402			min	-1390.983	3	.359	15	-41.088	4	0	5	-.125	4	-.006	6
403		12	max	1073.446	2	1.573	6	-.036	12	0	1	0	12	-.001	15
404			min	-1390.627	3	.35	15	-41.499	4	0	5	-.138	4	-.006	6
405		13	max	1073.919	2	1.536	6	-.036	12	0	1	0	12	-.002	15
406			min	-1390.272	3	.341	15	-41.911	4	0	5	-.151	4	-.007	6
407		14	max	1074.393	2	1.499	6	-.036	12	0	1	0	12	-.002	15
408			min	-1389.917	3	.333	15	-42.322	4	0	5	-.165	4	-.007	6
409		15	max	1074.867	2	1.462	6	-.036	12	0	1	0	12	-.002	15
410			min	-1389.562	3	.324	15	-42.733	4	0	5	-.178	4	-.008	6
411		16	max	1075.341	2	1.425	6	-.036	12	0	1	0	12	-.002	15
412			min	-1389.206	3	.315	15	-43.145	4	0	5	-.192	4	-.008	6
413		17	max	1075.814	2	1.388	6	-.036	12	0	1	0	12	-.002	15
414			min	-1388.851	3	.307	15	-43.556	4	0	5	-.206	4	-.009	6
415		18	max	1076.288	2	1.351	6	-.036	12	0	1	0	12	-.002	15
416			min	-1388.496	3	.298	15	-43.967	4	0	5	-.22	4	-.009	6
417		19	max	1076.762	2	1.314	6	-.036	12	0	1	0	12	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
418			min	-1388.14	3	.289	15	-44.379	4	0	5	-.234	4	-.009	6
419	M11	1	max	663.645	2	8.964	6	-.015	12	0	1	0	12	.009	6
420			min	-807.796	3	2.094	15	-.65	5	0	4	-.015	4	.002	15
421		2	max	663.475	2	8.092	6	-.015	12	0	1	0	12	.006	2
422			min	-807.923	3	1.889	15	-.233	1	0	4	-.015	4	.001	12
423		3	max	663.305	2	7.22	6	.574	4	0	1	0	12	.003	2
424			min	-808.051	3	1.684	15	-.233	1	0	4	-.015	4	0	3
425		4	max	663.134	2	6.348	6	1.181	4	0	1	0	12	0	2
426			min	-808.179	3	1.479	15	-.233	1	0	4	-.014	4	-.002	3
427		5	max	662.964	2	5.476	6	1.788	4	0	1	0	12	-.001	15
428			min	-808.307	3	1.274	15	-.233	1	0	4	-.014	4	-.004	4
429		6	max	662.794	2	4.604	6	2.395	4	0	1	0	12	-.002	15
430			min	-808.434	3	1.069	15	-.233	1	0	4	-.013	4	-.007	4
431		7	max	662.623	2	3.732	6	3.002	4	0	1	0	12	-.002	15
432			min	-808.562	3	.864	15	-.233	1	0	4	-.011	4	-.009	4
433		8	max	662.453	2	2.86	6	3.609	4	0	1	0	12	-.002	15
434			min	-808.69	3	.659	15	-.233	1	0	4	-.01	4	-.01	4
435		9	max	662.283	2	1.988	6	4.216	4	0	1	0	12	-.003	15
436			min	-808.818	3	.454	15	-.233	1	0	4	-.008	4	-.011	4
437		10	max	662.112	2	1.116	6	4.823	4	0	1	0	12	-.003	15
438			min	-808.945	3	.249	15	-.233	1	0	4	-.006	4	-.012	4
439		11	max	661.942	2	.377	2	5.43	4	0	1	0	12	-.003	15
440			min	-809.073	3	-.066	3	-.233	1	0	4	-.003	4	-.012	4
441		12	max	661.772	2	-.161	15	6.038	4	0	1	0	12	-.003	15
442			min	-809.201	3	-.629	4	-.233	1	0	4	-.001	1	-.012	4
443		13	max	661.601	2	-.366	15	6.645	4	0	1	.003	5	-.003	15
444			min	-809.329	3	-1.501	4	-.233	1	0	4	-.002	1	-.012	4
445		14	max	661.431	2	-.571	15	7.252	4	0	1	.006	5	-.003	15
446			min	-809.456	3	-2.373	4	-.233	1	0	4	-.002	1	-.011	4
447		15	max	661.261	2	-.776	15	7.859	4	0	1	.009	5	-.002	15
448			min	-809.584	3	-3.245	4	-.233	1	0	4	-.002	1	-.009	4
449		16	max	661.09	2	-.981	15	8.466	4	0	1	.013	5	-.002	15
450			min	-809.712	3	-4.117	4	-.233	1	0	4	-.002	1	-.008	4
451		17	max	660.92	2	-1.186	15	9.073	4	0	1	.017	5	-.001	15
452			min	-809.84	3	-4.989	4	-.233	1	0	4	-.002	1	-.006	4
453		18	max	660.75	2	-1.391	15	9.68	4	0	1	.022	5	0	15
454			min	-809.968	3	-5.861	4	-.233	1	0	4	-.002	1	-.003	4
455		19	max	660.579	2	-1.596	15	10.287	4	0	1	.027	5	0	1
456			min	-810.095	3	-6.733	4	-.233	1	0	4	-.002	1	0	1
457	M12	1	max	1082.325	1	0	1	11.074	1	0	1	.018	5	0	1
458			min	-128.91	3	0	1	-256.38	4	0	1	-.001	1	0	1
459		2	max	1082.495	1	0	1	11.074	1	0	1	0	10	0	1
460			min	-128.782	3	0	1	-256.528	4	0	1	-.011	4	0	1
461		3	max	1082.666	1	0	1	11.074	1	0	1	.001	1	0	1
462			min	-128.654	3	0	1	-256.676	4	0	1	-.041	4	0	1
463		4	max	1082.836	1	0	1	11.074	1	0	1	.002	1	0	1
464			min	-128.527	3	0	1	-256.823	4	0	1	-.07	4	0	1
465		5	max	1083.006	1	0	1	11.074	1	0	1	.004	1	0	1
466			min	-128.399	3	0	1	-256.971	4	0	1	-.1	4	0	1
467		6	max	1083.177	1	0	1	11.074	1	0	1	.005	1	0	1
468			min	-128.271	3	0	1	-257.119	4	0	1	-.129	4	0	1
469		7	max	1083.347	1	0	1	11.074	1	0	1	.006	1	0	1
470			min	-128.143	3	0	1	-257.266	4	0	1	-.159	4	0	1
471		8	max	1083.517	1	0	1	11.074	1	0	1	.007	1	0	1
472			min	-128.016	3	0	1	-257.414	4	0	1	-.188	4	0	1
473		9	max	1083.688	1	0	1	11.074	1	0	1	.009	1	0	1
474			min	-127.888	3	0	1	-257.561	4	0	1	-.218	4	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
475		10	max	1083.858	1	0	1	11.074	1	0	1	.01	1	0	1
476			min	-127.76	3	0	1	-257.709	4	0	1	-.247	4	0	1
477		11	max	1084.028	1	0	1	11.074	1	0	1	.011	1	0	1
478			min	-127.632	3	0	1	-257.857	4	0	1	-.277	4	0	1
479		12	max	1084.199	1	0	1	11.074	1	0	1	.012	1	0	1
480			min	-127.505	3	0	1	-258.004	4	0	1	-.307	4	0	1
481		13	max	1084.369	1	0	1	11.074	1	0	1	.014	1	0	1
482			min	-127.377	3	0	1	-258.152	4	0	1	-.336	4	0	1
483		14	max	1084.539	1	0	1	11.074	1	0	1	.015	1	0	1
484			min	-127.249	3	0	1	-258.3	4	0	1	-.366	4	0	1
485		15	max	1084.71	1	0	1	11.074	1	0	1	.016	1	0	1
486			min	-127.121	3	0	1	-258.447	4	0	1	-.396	4	0	1
487		16	max	1084.88	1	0	1	11.074	1	0	1	.018	1	0	1
488			min	-126.994	3	0	1	-258.595	4	0	1	-.425	4	0	1
489		17	max	1085.051	1	0	1	11.074	1	0	1	.019	1	0	1
490			min	-126.866	3	0	1	-258.743	4	0	1	-.455	4	0	1
491		18	max	1085.221	1	0	1	11.074	1	0	1	.02	1	0	1
492			min	-126.738	3	0	1	-258.89	4	0	1	-.485	4	0	1
493		19	max	1085.391	1	0	1	11.074	1	0	1	.021	1	0	1
494			min	-126.61	3	0	1	-259.038	4	0	1	-.514	4	0	1
495	M1	1	max	162.468	1	743.618	3	47.239	5	0	1	.179	1	0	15
496			min	-17.615	5	-433.067	2	-64.016	1	0	3	-.105	5	-.015	2
497		2	max	163.18	1	742.473	3	48.699	5	0	1	.139	1	.256	1
498			min	-17.283	5	-434.594	2	-64.016	1	0	3	-.076	5	-.466	3
499		3	max	525.563	3	552.411	2	14.409	5	0	3	.1	1	.514	1
500			min	-324.539	2	-560.908	3	-63.684	1	0	2	-.045	5	-.912	3
501		4	max	526.097	3	550.884	2	15.869	5	0	3	.06	1	.187	1
502			min	-323.827	2	-562.053	3	-63.684	1	0	2	-.036	5	-.563	3
503		5	max	526.631	3	549.357	2	17.329	5	0	3	.021	1	-.005	15
504			min	-323.115	2	-563.198	3	-63.684	1	0	2	-.026	5	-.214	3
505		6	max	527.165	3	547.83	2	18.789	5	0	3	-.001	12	.136	3
506			min	-322.403	2	-564.344	3	-63.684	1	0	2	-.019	1	-.51	2
507		7	max	527.699	3	546.303	2	20.249	5	0	3	-.002	15	.486	3
508			min	-321.691	2	-565.489	3	-63.684	1	0	2	-.058	1	-.85	2
509		8	max	528.233	3	544.776	2	21.709	5	0	3	.011	5	.838	3
510			min	-320.979	2	-566.634	3	-63.684	1	0	2	-.098	1	-1.188	2
511		9	max	541.818	3	45.683	2	55.451	5	0	9	.063	1	.978	3
512			min	-253.335	2	.458	15	-103.768	1	0	3	-.132	5	-1.357	2
513		10	max	542.352	3	44.156	2	56.911	5	0	9	0	10	.955	3
514			min	-252.623	2	-.007	5	-103.768	1	0	3	-.098	4	-1.384	2
515		11	max	542.886	3	42.629	2	58.371	5	0	9	-.005	12	.933	3
516			min	-251.911	2	-1.918	4	-103.768	1	0	3	-.076	4	-1.411	2
517		12	max	556.247	3	369.15	3	148.52	5	0	2	.096	1	.816	3
518			min	-184.183	2	-640.684	2	-61.5	1	0	3	-.237	5	-1.252	2
519		13	max	556.781	3	368.005	3	149.98	5	0	2	.058	1	.588	3
520			min	-183.471	2	-642.211	2	-61.5	1	0	3	-.144	5	-.853	2
521		14	max	557.315	3	366.86	3	151.44	5	0	2	.02	1	.36	3
522			min	-182.759	2	-643.738	2	-61.5	1	0	3	-.051	5	-.454	2
523		15	max	557.849	3	365.714	3	152.901	5	0	2	.044	5	.132	3
524			min	-182.047	2	-645.265	2	-61.5	1	0	3	-.018	1	-.079	1
525		16	max	558.383	3	364.569	3	154.361	5	0	2	.139	5	.347	2
526			min	-181.335	2	-646.792	2	-61.5	1	0	3	-.056	1	-.094	3
527		17	max	558.917	3	363.424	3	155.821	5	0	2	.235	5	.748	2
528			min	-180.623	2	-648.319	2	-61.5	1	0	3	-.095	1	-.32	3
529		18	max	29.652	5	621.267	2	-4.672	12	0	5	.211	5	.376	2
530			min	-163.734	1	-274.213	3	-105.068	4	0	2	-.137	1	-.157	3
531		19	max	29.984	5	619.74	2	-4.672	12	0	5	.157	5	.013	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
532			min	-163.022	1	-275.358	3	-103.608	4	0	2	-.182	1	-.01	1
533	M5	1	max	364.088	1	2460.337	3	86.305	5	0	1	0	1	.029	2
534			min	11.79	12	-1502.367	2	0	1	0	4	-.215	4	0	15
535		2	max	364.8	1	2459.192	3	87.765	5	0	1	0	1	.962	2
536			min	12.146	12	-1503.894	2	0	1	0	4	-.161	4	-1.518	3
537		3	max	1624.832	3	1497.525	2	56.477	4	0	4	0	1	1.863	2
538			min	-1046.712	2	-1662.384	3	0	1	0	1	-.107	4	-2.998	3
539		4	max	1625.366	3	1495.998	2	57.937	4	0	4	0	1	.952	1
540			min	-1046	2	-1663.529	3	0	1	0	1	-.072	4	-1.966	3
541		5	max	1625.9	3	1494.471	2	59.397	4	0	4	0	1	.06	1
542			min	-1045.288	2	-1664.674	3	0	1	0	1	-.035	4	-.934	3
543		6	max	1626.434	3	1492.944	2	60.857	4	0	4	.002	4	.1	3
544			min	-1044.576	2	-1665.819	3	0	1	0	1	0	1	-.921	2
545		7	max	1626.968	3	1491.417	2	62.317	4	0	4	.04	4	1.134	3
546			min	-1043.864	2	-1666.964	3	0	1	0	1	0	1	-1.847	2
547		8	max	1627.502	3	1489.89	2	63.777	4	0	4	.079	4	2.169	3
548			min	-1043.152	2	-1668.11	3	0	1	0	1	0	1	-2.772	2
549		9	max	1644.28	3	154.432	2	185.247	4	0	1	0	1	2.504	3
550			min	-897.684	2	.461	15	0	1	0	1	-.2	4	-3.169	2
551		10	max	1644.814	3	152.905	2	186.707	4	0	1	0	1	2.415	3
552			min	-896.972	2	0	15	0	1	0	1	-.084	4	-3.264	2
553		11	max	1645.348	3	151.378	2	188.167	4	0	1	.032	4	2.326	3
554			min	-896.26	2	-1.717	6	0	1	0	1	0	1	-3.359	2
555		12	max	1662.573	3	1049.451	3	205.644	4	0	1	0	1	2.035	3
556			min	-750.959	2	-1799.04	2	0	1	0	4	-.337	4	-3	2
557		13	max	1663.107	3	1048.306	3	207.104	4	0	1	0	1	1.384	3
558			min	-750.247	2	-1800.567	2	0	1	0	4	-.209	4	-1.883	2
559		14	max	1663.641	3	1047.161	3	208.564	4	0	1	0	1	.734	3
560			min	-749.535	2	-1802.094	2	0	1	0	4	-.08	4	-.765	2
561		15	max	1664.175	3	1046.015	3	210.024	4	0	1	.05	4	.354	2
562			min	-748.823	2	-1803.621	2	0	1	0	4	0	1	0	15
563		16	max	1664.709	3	1044.87	3	211.484	4	0	1	.181	4	1.474	2
564			min	-748.111	2	-1805.148	2	0	1	0	4	0	1	-.564	3
565		17	max	1665.243	3	1043.725	3	212.945	4	0	1	.313	4	2.595	2
566			min	-747.399	2	-1806.675	2	0	1	0	4	0	1	-1.213	3
567		18	max	-12.991	12	2110.69	2	0	1	0	4	.326	4	1.327	2
568			min	-363.692	1	-973.4	3	-25.504	5	0	1	0	1	-.631	3
569		19	max	-12.635	12	2109.163	2	0	1	0	4	.311	4	.02	1
570			min	-362.98	1	-974.545	3	-24.044	5	0	1	0	1	-.026	3
571	M9	1	max	162.468	1	743.618	3	70.031	4	0	3	-.013	12	0	15
572			min	8.22	12	-433.067	2	4.692	12	0	4	-.179	1	-.015	2
573		2	max	163.18	1	742.473	3	71.491	4	0	3	-.01	12	.256	1
574			min	8.576	12	-434.594	2	4.692	12	0	4	-.139	1	-.466	3
575		3	max	525.563	3	552.411	2	63.684	1	0	2	-.007	12	.514	1
576			min	-324.539	2	-560.908	3	4.654	12	0	3	-.1	1	-.912	3
577		4	max	526.097	3	550.884	2	63.684	1	0	2	-.005	12	.187	1
578			min	-323.827	2	-562.053	3	4.654	12	0	3	-.06	1	-.563	3
579		5	max	526.631	3	549.357	2	63.684	1	0	2	-.002	12	-.005	15
580			min	-323.115	2	-563.198	3	4.654	12	0	3	-.033	4	-.214	3
581		6	max	527.165	3	547.83	2	63.684	1	0	2	.019	1	.136	3
582			min	-322.403	2	-564.344	3	4.654	12	0	3	-.012	5	-.51	2
583		7	max	527.699	3	546.303	2	63.684	1	0	2	.058	1	.486	3
584			min	-321.691	2	-565.489	3	4.654	12	0	3	.003	15	-.85	2
585		8	max	528.233	3	544.776	2	63.684	1	0	2	.098	1	.838	3
586			min	-320.979	2	-566.634	3	4.654	12	0	3	.007	12	-1.188	2
587		9	max	541.818	3	45.683	2	103.768	1	0	3	-.004	12	.978	3
588			min	-253.335	2	.473	15	7.146	12	0	9	-.155	4	-1.357	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
589		10	max	542.352	3	44.156	2	103.768	1	0	3	.001	1	.955	3
590			min	-252.623	2	.012	15	7.146	12	0	9	-.097	4	-1.384	2
591		11	max	542.886	3	42.629	2	103.768	1	0	3	.065	1	.933	3
592			min	-251.911	2	-1.799	6	7.146	12	0	9	-.053	5	-1.411	2
593		12	max	556.247	3	369.15	3	172.115	4	0	3	-.006	12	.816	3
594			min	-184.183	2	-640.684	2	3.988	12	0	2	-.274	4	-1.252	2
595		13	max	556.781	3	368.005	3	173.575	4	0	3	-.004	12	.588	3
596			min	-183.471	2	-642.211	2	3.988	12	0	2	-.166	4	-.853	2
597		14	max	557.315	3	366.86	3	175.035	4	0	3	-.001	12	.36	3
598			min	-182.759	2	-643.738	2	3.988	12	0	2	-.058	4	-.454	2
599		15	max	557.849	3	365.714	3	176.495	4	0	3	.051	4	.132	3
600			min	-182.047	2	-645.265	2	3.988	12	0	2	.001	12	-.079	1
601		16	max	558.383	3	364.569	3	177.955	4	0	3	.161	4	.347	2
602			min	-181.335	2	-646.792	2	3.988	12	0	2	.004	12	-.094	3
603		17	max	558.917	3	363.424	3	179.415	4	0	3	.272	4	.748	2
604			min	-180.623	2	-648.319	2	3.988	12	0	2	.006	12	-.32	3
605		18	max	-8.153	12	621.267	2	72.051	1	0	2	.262	4	.376	2
606			min	-163.734	1	-274.213	3	-79.589	5	0	3	.009	12	-.157	3
607		19	max	-7.797	12	619.74	2	72.051	1	0	2	.223	4	.013	3
608			min	-163.022	1	-275.358	3	-78.129	5	0	3	.012	12	-.01	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M13	1	max	0	1	.21	2	.01	3	1.434e-2	2	NC	1	NC	1
2			min	-.703	4	-.051	3	-.006	2	-3.343e-3	3	NC	1	NC	1
3		2	max	0	1	.136	3	.021	1	1.549e-2	2	NC	4	NC	2
4			min	-.703	4	.004	15	-.014	5	-2.992e-3	3	1029.284	3	9000.816	1
5		3	max	0	1	.288	3	.049	1	1.664e-2	2	NC	5	NC	2
6			min	-.703	4	.002	15	-.018	5	-2.641e-3	3	566.776	3	3876.137	1
7		4	max	0	1	.383	3	.073	1	1.779e-2	2	NC	5	NC	3
8			min	-.703	4	-.006	9	-.014	5	-2.29e-3	3	442.856	3	2635.774	1
9		5	max	0	1	.409	3	.083	1	1.895e-2	2	NC	5	NC	3
10			min	-.703	4	-.004	9	-.005	5	-1.939e-3	3	417.372	3	2291.587	1
11		6	max	0	1	.369	3	.079	1	2.01e-2	2	NC	5	NC	3
12			min	-.703	4	.002	15	0	10	-1.589e-3	3	457.677	3	2425.27	1
13		7	max	0	1	.275	3	.06	1	2.125e-2	2	NC	4	NC	2
14			min	-.704	4	.004	15	-.004	10	-1.238e-3	3	589.734	3	3195.435	1
15		8	max	0	1	.255	2	.032	1	2.24e-2	2	NC	4	NC	2
16			min	-.704	4	.006	15	-.008	10	-8.869e-4	3	941.24	3	6013.901	1
17		9	max	0	1	.331	2	.031	3	2.355e-2	2	NC	4	NC	1
18			min	-.704	4	.008	15	-.016	2	-5.361e-4	3	1579.993	2	9333.725	3
19		10	max	0	1	.365	2	.031	3	2.471e-2	2	NC	5	NC	1
20			min	-.704	4	-.009	3	-.021	2	-1.852e-4	3	1236.932	2	9401.639	3
21		11	max	0	12	.331	2	.031	3	2.355e-2	2	NC	4	NC	1
22			min	-.704	4	.008	15	-.016	2	-5.361e-4	3	1579.993	2	9333.725	3
23		12	max	0	12	.255	2	.032	1	2.24e-2	2	NC	4	NC	2
24			min	-.704	4	.006	15	-.011	5	-8.869e-4	3	941.24	3	6013.901	1
25		13	max	0	12	.275	3	.06	1	2.125e-2	2	NC	4	NC	2
26			min	-.704	4	.004	15	-.004	5	-1.238e-3	3	589.734	3	3195.435	1
27		14	max	0	12	.369	3	.079	1	2.01e-2	2	NC	5	NC	3
28			min	-.704	4	.002	15	0	10	-1.589e-3	3	457.677	3	2425.27	1
29		15	max	0	12	.409	3	.083	1	1.895e-2	2	NC	5	NC	3
30			min	-.704	4	-.004	9	.002	10	-1.939e-3	3	417.372	3	2291.587	1
31		16	max	0	12	.383	3	.073	1	1.779e-2	2	NC	5	NC	3
32			min	-.704	4	-.006	9	.002	10	-2.29e-3	3	442.856	3	2635.774	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
33		17	max	0	12	.288	3	.049	1	1.664e-2	2	NC	5	NC	2
34			min	-.704	4	.001	15	0	10	-2.641e-3	3	566.776	3	3876.137	1
35		18	max	0	12	.136	3	.023	4	1.549e-2	2	NC	4	NC	2
36			min	-.704	4	.003	15	-.002	10	-2.992e-3	3	1029.284	3	7967.475	4
37		19	max	0	12	.21	2	.01	3	1.434e-2	2	NC	1	NC	1
38			min	-.704	4	-.051	3	-.006	2	-3.343e-3	3	NC	1	NC	1
39	M14	1	max	0	1	.406	3	.009	3	8.064e-3	2	NC	1	NC	1
40			min	-.527	4	-.627	2	-.005	2	-6.162e-3	3	NC	1	NC	1
41		2	max	0	1	.635	3	.013	1	9.278e-3	2	NC	5	NC	1
42			min	-.527	4	-.864	2	-.022	5	-7.214e-3	3	811.149	2	9697.719	5
43		3	max	0	1	.837	3	.037	1	1.049e-2	2	NC	5	NC	2
44			min	-.527	4	-1.077	2	-.027	5	-8.266e-3	3	426.973	2	5146.003	1
45		4	max	0	1	.991	3	.06	1	1.17e-2	2	NC	15	NC	3
46			min	-.527	4	-1.249	2	-.019	5	-9.318e-3	3	308.71	2	3226.914	1
47		5	max	0	1	1.087	3	.072	1	1.292e-2	2	NC	15	NC	3
48			min	-.527	4	-1.371	2	-.005	5	-1.037e-2	3	258.111	2	2680.978	1
49		6	max	0	1	1.123	3	.07	1	1.413e-2	2	NC	15	NC	3
50			min	-.527	4	-1.44	2	0	10	-1.142e-2	3	236.115	2	2754.837	1
51		7	max	0	1	1.108	3	.054	1	1.534e-2	2	NC	15	NC	2
52			min	-.527	4	-1.462	2	-.003	10	-1.247e-2	3	229.965	2	3551.42	1
53		8	max	0	1	1.059	3	.04	4	1.656e-2	2	NC	15	NC	2
54			min	-.527	4	-1.449	2	-.007	10	-1.353e-2	3	233.712	2	4713.208	4
55		9	max	0	1	1.002	3	.027	4	1.777e-2	2	NC	15	NC	1
56			min	-.527	4	-1.42	2	-.014	2	-1.458e-2	3	242.186	2	6753.536	4
57		10	max	0	1	.974	3	.027	3	1.899e-2	2	NC	15	NC	1
58			min	-.527	4	-1.403	2	-.019	2	-1.563e-2	3	247.484	2	NC	1
59		11	max	0	12	1.002	3	.027	3	1.777e-2	2	NC	15	NC	1
60			min	-.527	4	-1.42	2	-.022	5	-1.458e-2	3	242.186	2	9571.036	5
61		12	max	0	12	1.059	3	.029	1	1.656e-2	2	NC	15	NC	2
62			min	-.528	4	-1.449	2	-.026	5	-1.353e-2	3	233.712	2	6546.685	1
63		13	max	0	12	1.108	3	.054	1	1.534e-2	2	NC	15	NC	2
64			min	-.528	4	-1.462	2	-.017	5	-1.247e-2	3	229.965	2	3551.42	1
65		14	max	0	12	1.123	3	.07	1	1.413e-2	2	NC	15	NC	3
66			min	-.528	4	-1.44	2	-.002	5	-1.142e-2	3	236.115	2	2754.837	1
67		15	max	0	12	1.087	3	.072	1	1.292e-2	2	NC	15	NC	3
68			min	-.528	4	-1.371	2	.001	10	-1.037e-2	3	258.111	2	2680.978	1
69		16	max	0	12	.991	3	.06	1	1.17e-2	2	NC	15	NC	3
70			min	-.528	4	-1.249	2	.001	10	-9.318e-3	3	308.71	2	3226.914	1
71		17	max	0	12	.837	3	.042	4	1.049e-2	2	NC	5	NC	2
72			min	-.528	4	-1.077	2	0	10	-8.266e-3	3	426.973	2	4477.625	4
73		18	max	0	12	.635	3	.028	4	9.278e-3	2	NC	5	NC	1
74			min	-.528	4	-.864	2	-.002	10	-7.214e-3	3	811.149	2	6617.468	4
75		19	max	0	12	.406	3	.009	3	8.064e-3	2	NC	1	NC	1
76			min	-.528	4	-.627	2	-.005	2	-6.162e-3	3	NC	1	NC	1
77	M15	1	max	0	12	.416	3	.008	3	5.172e-3	3	NC	1	NC	1
78			min	-.429	4	-.626	2	-.005	2	-8.358e-3	2	NC	1	NC	1
79		2	max	0	12	.581	3	.014	1	6.045e-3	3	NC	5	NC	1
80			min	-.429	4	-.907	2	-.031	5	-9.624e-3	2	683.837	2	6574.95	5
81		3	max	0	12	.732	3	.038	1	6.917e-3	3	NC	5	NC	2
82			min	-.429	4	-1.155	2	-.039	5	-1.089e-2	2	362.654	2	5113.178	1
83		4	max	0	12	.855	3	.06	1	7.79e-3	3	NC	15	NC	3
84			min	-.429	4	-1.349	2	-.029	5	-1.215e-2	2	265.426	2	3209.382	1
85		5	max	0	12	.945	3	.072	1	8.663e-3	3	NC	15	NC	3
86			min	-.429	4	-1.476	2	-.01	5	-1.342e-2	2	225.799	2	2666.425	1
87		6	max	0	12	1	3	.07	1	9.535e-3	3	NC	15	NC	3
88			min	-.429	4	-1.534	2	0	10	-1.468e-2	2	211.369	2	2737.579	1
89		7	max	0	12	1.023	3	.055	1	1.041e-2	3	NC	15	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
90			min	-.429	4	-1.532	2	-.003	10	-1.595e-2	2	211.931	2	3520.619	1
91		8	max	0	12	1.021	3	.049	4	1.128e-2	3	NC	15	NC	2
92			min	-.429	4	-1.488	2	-.006	10	-1.721e-2	2	222.767	2	3851.313	4
93		9	max	0	12	1.007	3	.035	4	1.215e-2	3	NC	15	NC	1
94			min	-.429	4	-1.431	2	-.013	2	-1.848e-2	2	238.418	2	5327.622	4
95		10	max	0	1	.998	3	.025	3	1.303e-2	3	NC	15	NC	1
96			min	-.429	4	-1.402	2	-.018	2	-1.974e-2	2	247.513	2	NC	1
97		11	max	0	1	1.007	3	.025	3	1.215e-2	3	NC	15	NC	1
98			min	-.429	4	-1.431	2	-.03	5	-1.848e-2	2	238.418	2	6903.271	5
99		12	max	0	1	1.021	3	.03	1	1.128e-2	3	NC	15	NC	2
100			min	-.429	4	-1.488	2	-.035	5	-1.721e-2	2	222.767	2	5783.17	5
101		13	max	0	1	1.023	3	.055	1	1.041e-2	3	NC	15	NC	2
102			min	-.429	4	-1.532	2	-.024	5	-1.595e-2	2	211.931	2	3520.619	1
103		14	max	0	1	1	3	.07	1	9.535e-3	3	NC	15	NC	3
104			min	-.429	4	-1.534	2	-.003	5	-1.468e-2	2	211.369	2	2737.579	1
105		15	max	0	1	.945	3	.072	1	8.663e-3	3	NC	15	NC	3
106			min	-.429	4	-1.476	2	.002	10	-1.342e-2	2	225.799	2	2666.425	1
107		16	max	0	1	.855	3	.06	1	7.79e-3	3	NC	15	NC	3
108			min	-.429	4	-1.349	2	.001	10	-1.215e-2	2	265.426	2	3209.382	1
109		17	max	0	1	.732	3	.054	4	6.917e-3	3	NC	5	NC	2
110			min	-.429	4	-1.155	2	0	10	-1.089e-2	2	362.654	2	3494.776	4
111		18	max	0	1	.581	3	.037	4	6.045e-3	3	NC	5	NC	1
112			min	-.429	4	-.907	2	-.002	10	-9.624e-3	2	683.837	2	5008.655	4
113		19	max	0	1	.416	3	.008	3	5.172e-3	3	NC	1	NC	1
114			min	-.429	4	-.626	2	-.005	2	-8.358e-3	2	NC	1	NC	1
115	M16	1	max	0	12	.188	2	.007	3	9.864e-3	3	NC	1	NC	1
116			min	-.132	4	-.147	3	-.005	2	-1.225e-2	2	NC	1	NC	1
117		2	max	0	12	.073	1	.021	1	1.09e-2	3	NC	4	NC	2
118			min	-.132	4	-.102	3	-.022	5	-1.294e-2	2	1440.339	2	9089.26	1
119		3	max	0	12	.012	9	.049	1	1.193e-2	3	NC	5	NC	2
120			min	-.132	4	-.069	3	-.028	5	-1.364e-2	2	806.217	2	3888.22	1
121		4	max	0	12	.005	4	.073	1	1.297e-2	3	NC	5	NC	3
122			min	-.132	4	-.107	2	-.023	5	-1.433e-2	2	649.576	2	2632.242	1
123		5	max	0	12	.006	4	.084	1	1.4e-2	3	NC	5	NC	3
124			min	-.132	4	-.109	2	-.011	5	-1.502e-2	2	646.52	2	2278.419	1
125		6	max	0	12	.019	9	.08	1	1.503e-2	3	NC	5	NC	3
126			min	-.132	4	-.106	3	.002	10	-1.571e-2	2	786.618	2	2396.741	1
127		7	max	0	12	.077	1	.061	1	1.607e-2	3	NC	3	NC	2
128			min	-.132	4	-.159	3	-.001	10	-1.647e-2	1	1288.617	2	3122.222	1
129		8	max	0	12	.176	1	.034	1	1.71e-2	3	NC	1	NC	2
130			min	-.132	4	-.219	3	-.005	10	-1.723e-2	1	2654.435	3	5689.416	1
131		9	max	0	12	.264	1	.022	3	1.813e-2	3	NC	4	NC	1
132			min	-.132	4	-.27	3	-.011	2	-1.8e-2	1	1554.177	3	8422.924	4
133		10	max	0	1	.304	1	.022	3	1.917e-2	3	NC	5	NC	1
134			min	-.132	4	-.293	3	-.016	2	-1.876e-2	1	1314.967	3	NC	1
135		11	max	0	1	.264	1	.022	3	1.813e-2	3	NC	4	NC	1
136			min	-.132	4	-.27	3	-.016	5	-1.8e-2	1	1554.177	3	NC	1
137		12	max	0	1	.176	1	.034	1	1.71e-2	3	NC	1	NC	2
138			min	-.132	4	-.219	3	-.017	5	-1.723e-2	1	2654.435	3	5689.416	1
139		13	max	0	1	.077	1	.061	1	1.607e-2	3	NC	3	NC	2
140			min	-.132	4	-.159	3	-.008	5	-1.647e-2	1	1288.617	2	3122.222	1
141		14	max	0	1	.019	9	.08	1	1.503e-2	3	NC	5	NC	3
142			min	-.132	4	-.106	3	.002	10	-1.571e-2	2	786.618	2	2396.741	1
143		15	max	0	1	.005	6	.084	1	1.4e-2	3	NC	5	NC	3
144			min	-.132	4	-.109	2	.003	10	-1.502e-2	2	646.52	2	2278.419	1
145		16	max	0	1	.004	13	.073	1	1.297e-2	3	NC	5	NC	3
146			min	-.132	4	-.107	2	.003	10	-1.433e-2	2	649.576	2	2632.242	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
147		17	max	0	1	.012	9	.049	1	1.193e-2	3	NC	5	NC	2
148			min	-.132	4	-.069	3	.001	10	-1.364e-2	2	806.217	2	3888.22	1
149		18	max	0	1	.073	1	.031	4	1.09e-2	3	NC	4	NC	2
150			min	-.132	4	-.102	3	-.001	10	-1.294e-2	2	1440.339	2	6113.093	4
151		19	max	0	1	.188	2	.007	3	9.864e-3	3	NC	1	NC	1
152			min	-.132	4	-.147	3	-.005	2	-1.225e-2	2	NC	1	NC	1
153	M2	1	max	.007	2	.009	2	.008	1	2.276e-3	5	NC	1	NC	2
154			min	-.009	3	-.015	3	-.661	4	-1.863e-4	1	7475.926	2	104.599	4
155		2	max	.007	2	.008	2	.008	1	2.299e-3	5	NC	1	NC	2
156			min	-.009	3	-.014	3	-.607	4	-1.759e-4	1	8671.147	2	113.919	4
157		3	max	.006	2	.007	2	.007	1	2.321e-3	5	NC	1	NC	2
158			min	-.008	3	-.014	3	-.553	4	-1.655e-4	1	NC	1	124.993	4
159		4	max	.006	2	.005	2	.006	1	2.343e-3	5	NC	1	NC	1
160			min	-.008	3	-.013	3	-.5	4	-1.551e-4	1	NC	1	138.28	4
161		5	max	.006	2	.004	2	.006	1	2.365e-3	5	NC	1	NC	1
162			min	-.007	3	-.013	3	-.448	4	-1.447e-4	1	NC	1	154.403	4
163		6	max	.005	2	.003	2	.005	1	2.387e-3	5	NC	1	NC	1
164			min	-.007	3	-.012	3	-.397	4	-1.343e-4	1	NC	1	174.231	4
165		7	max	.005	2	.002	2	.004	1	2.41e-3	5	NC	1	NC	1
166			min	-.006	3	-.012	3	-.347	4	-1.239e-4	1	NC	1	198.992	4
167		8	max	.004	2	.001	2	.004	1	2.433e-3	4	NC	1	NC	1
168			min	-.006	3	-.011	3	-.3	4	-1.135e-4	1	NC	1	230.487	4
169		9	max	.004	2	0	2	.003	1	2.458e-3	4	NC	1	NC	1
170			min	-.005	3	-.01	3	-.255	4	-1.031e-4	1	NC	1	271.425	4
171		10	max	.004	2	0	2	.003	1	2.484e-3	4	NC	1	NC	1
172			min	-.005	3	-.01	3	-.212	4	-9.268e-5	1	NC	1	326.053	4
173		11	max	.003	2	0	15	.002	1	2.509e-3	4	NC	1	NC	1
174			min	-.004	3	-.009	3	-.172	4	-8.228e-5	1	NC	1	401.335	4
175		12	max	.003	2	0	15	.002	1	2.534e-3	4	NC	1	NC	1
176			min	-.004	3	-.008	3	-.136	4	-7.188e-5	1	NC	1	509.358	4
177		13	max	.002	2	0	15	.001	1	2.559e-3	4	NC	1	NC	1
178			min	-.003	3	-.007	3	-.103	4	-6.148e-5	1	NC	1	672.643	4
179		14	max	.002	2	0	15	0	1	2.584e-3	4	NC	1	NC	1
180			min	-.003	3	-.006	3	-.074	4	-5.108e-5	1	NC	1	937.255	4
181		15	max	.002	2	0	15	0	1	2.61e-3	4	NC	1	NC	1
182			min	-.002	3	-.005	3	-.049	4	-4.068e-5	1	NC	1	1410.174	4
183		16	max	.001	2	0	15	0	1	2.635e-3	4	NC	1	NC	1
184			min	-.002	3	-.004	3	-.029	4	-3.028e-5	1	NC	1	2390.37	4
185		17	max	0	2	0	15	0	1	2.66e-3	4	NC	1	NC	1
186			min	-.001	3	-.003	3	-.014	4	-1.988e-5	1	NC	1	5006.37	4
187		18	max	0	2	0	15	0	1	2.685e-3	4	NC	1	NC	1
188			min	0	3	-.001	6	-.004	4	-9.478e-6	1	NC	1	NC	1
189		19	max	0	1	0	1	0	1	2.711e-3	4	NC	1	NC	1
190			min	0	1	0	1	0	1	-5.302e-7	3	NC	1	NC	1
191	M3	1	max	0	1	0	1	0	1	0	3	NC	1	NC	1
192			min	0	1	0	1	0	1	-5.626e-4	4	NC	1	NC	1
193		2	max	0	3	0	15	.015	4	8.626e-5	4	NC	1	NC	1
194			min	0	2	-.003	6	0	3	1.389e-6	12	NC	1	NC	1
195		3	max	0	3	-.001	15	.029	4	7.351e-4	4	NC	1	NC	1
196			min	0	2	-.005	6	0	3	2.791e-6	12	NC	1	NC	1
197		4	max	.001	3	-.002	15	.042	4	1.384e-3	4	NC	1	NC	1
198			min	-.001	2	-.008	6	0	3	4.193e-6	12	NC	1	NC	1
199		5	max	.002	3	-.002	15	.054	4	2.033e-3	4	NC	1	NC	1
200			min	-.001	2	-.011	6	0	12	5.595e-6	12	8984.265	6	9560.104	5
201		6	max	.002	3	-.003	15	.065	4	2.682e-3	4	NC	2	NC	1
202			min	-.002	2	-.014	6	0	12	6.997e-6	12	7238.336	6	8970.067	5
203		7	max	.003	3	-.004	15	.076	4	3.33e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
204			min	-.002	2	-.016	6	0	12	8.399e-6	12	6189.035	6	8966.399	5
205		8	max	.003	3	-.004	15	.086	4	3.979e-3	4	NC	5	NC	1
206			min	-.003	2	-.018	6	0	12	9.801e-6	12	5541.403	6	9482.736	5
207		9	max	.004	3	-.004	15	.096	4	4.628e-3	4	NC	5	NC	1
208			min	-.003	2	-.02	6	0	12	1.12e-5	12	5156.773	6	NC	1
209		10	max	.004	3	-.005	15	.105	4	5.277e-3	4	NC	5	NC	1
210			min	-.003	2	-.021	6	0	12	1.261e-5	12	4967.672	6	NC	1
211		11	max	.004	3	-.005	15	.114	4	5.926e-3	4	NC	5	NC	1
212			min	-.004	2	-.021	6	0	12	1.401e-5	12	4946.078	6	NC	1
213		12	max	.005	3	-.004	15	.123	4	6.574e-3	4	NC	5	NC	1
214			min	-.004	2	-.02	6	0	12	1.541e-5	12	5092.648	6	NC	1
215		13	max	.005	3	-.004	15	.132	4	7.223e-3	4	NC	5	NC	1
216			min	-.004	2	-.019	6	0	12	1.681e-5	12	5438.333	6	NC	1
217		14	max	.006	3	-.004	15	.14	4	7.872e-3	4	NC	5	NC	1
218			min	-.005	2	-.017	6	0	12	1.821e-5	12	6060.589	6	NC	1
219		15	max	.006	3	-.003	15	.15	4	8.521e-3	4	NC	3	NC	1
220			min	-.005	2	-.014	6	0	12	1.962e-5	12	7131.75	6	NC	1
221		16	max	.007	3	-.002	15	.16	4	9.17e-3	4	NC	1	NC	1
222			min	-.005	2	-.011	6	0	12	2.102e-5	12	9069.696	6	NC	1
223		17	max	.007	3	-.001	15	.17	4	9.819e-3	4	NC	1	NC	1
224			min	-.006	2	-.008	1	0	12	2.242e-5	12	NC	1	NC	1
225		18	max	.007	3	0	15	.182	4	1.047e-2	4	NC	1	NC	1
226			min	-.006	2	-.005	1	0	12	2.382e-5	12	NC	1	NC	1
227		19	max	.008	3	0	5	.195	4	1.112e-2	4	NC	1	NC	1
228			min	-.006	2	-.002	1	0	12	2.522e-5	12	NC	1	NC	1
229	M4	1	max	.003	1	.006	2	0	12	1.069e-4	1	NC	1	NC	3
230			min	0	3	-.008	3	-.195	4	-3.603e-4	5	NC	1	127.008	4
231		2	max	.002	1	.006	2	0	12	1.069e-4	1	NC	1	NC	3
232			min	0	3	-.008	3	-.18	4	-3.603e-4	5	NC	1	138.175	4
233		3	max	.002	1	.005	2	0	12	1.069e-4	1	NC	1	NC	3
234			min	0	3	-.007	3	-.164	4	-3.603e-4	5	NC	1	151.461	4
235		4	max	.002	1	.005	2	0	12	1.069e-4	1	NC	1	NC	2
236			min	0	3	-.007	3	-.148	4	-3.603e-4	5	NC	1	167.417	4
237		5	max	.002	1	.005	2	0	12	1.069e-4	1	NC	1	NC	2
238			min	0	3	-.006	3	-.133	4	-3.603e-4	5	NC	1	186.791	4
239		6	max	.002	1	.004	2	0	12	1.069e-4	1	NC	1	NC	2
240			min	0	3	-.006	3	-.118	4	-3.603e-4	5	NC	1	210.622	4
241		7	max	.002	1	.004	2	0	12	1.069e-4	1	NC	1	NC	2
242			min	0	3	-.005	3	-.103	4	-3.603e-4	5	NC	1	240.385	4
243		8	max	.002	1	.004	2	0	12	1.069e-4	1	NC	1	NC	2
244			min	0	3	-.005	3	-.089	4	-3.603e-4	5	NC	1	278.229	4
245		9	max	.001	1	.003	2	0	12	1.069e-4	1	NC	1	NC	2
246			min	0	3	-.005	3	-.076	4	-3.603e-4	5	NC	1	327.39	4
247		10	max	.001	1	.003	2	0	12	1.069e-4	1	NC	1	NC	2
248			min	0	3	-.004	3	-.063	4	-3.603e-4	5	NC	1	392.929	4
249		11	max	.001	1	.003	2	0	12	1.069e-4	1	NC	1	NC	1
250			min	0	3	-.004	3	-.051	4	-3.603e-4	5	NC	1	483.123	4
251		12	max	.001	1	.002	2	0	12	1.069e-4	1	NC	1	NC	1
252			min	0	3	-.003	3	-.041	4	-3.603e-4	5	NC	1	612.291	4
253		13	max	0	1	.002	2	0	12	1.069e-4	1	NC	1	NC	1
254			min	0	3	-.003	3	-.031	4	-3.603e-4	5	NC	1	807.012	4
255		14	max	0	1	.002	2	0	12	1.069e-4	1	NC	1	NC	1
256			min	0	3	-.002	3	-.022	4	-3.603e-4	5	NC	1	1121.356	4
257		15	max	0	1	.001	2	0	12	1.069e-4	1	NC	1	NC	1
258			min	0	3	-.002	3	-.015	4	-3.603e-4	5	NC	1	1679.976	4
259		16	max	0	1	.001	2	0	12	1.069e-4	1	NC	1	NC	1
260			min	0	3	-.001	3	-.009	4	-3.603e-4	5	NC	1	2827.463	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
261		17	max	0	1	0	2	0	12	1.069e-4	1	NC	1	NC	1
262			min	0	3	0	3	-.004	4	-3.603e-4	5	NC	1	5841.543	4
263		18	max	0	1	0	2	0	12	1.069e-4	1	NC	1	NC	1
264			min	0	3	0	3	-.001	4	-3.603e-4	5	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.069e-4	1	NC	1	NC	1
266			min	0	1	0	1	0	1	-3.603e-4	5	NC	1	NC	1
267	M6	1	max	.022	2	.032	2	0	1	2.379e-3	4	NC	3	NC	1
268			min	-.029	3	-.044	3	-.667	4	0	1	2179.272	2	103.54	4
269		2	max	.021	2	.029	2	0	1	2.399e-3	4	NC	3	NC	1
270			min	-.028	3	-.042	3	-.613	4	0	1	2388.454	2	112.767	4
271		3	max	.019	2	.026	2	0	1	2.419e-3	4	NC	3	NC	1
272			min	-.026	3	-.04	3	-.559	4	0	1	2640.058	2	123.73	4
273		4	max	.018	2	.023	2	0	1	2.439e-3	4	NC	3	NC	1
274			min	-.024	3	-.037	3	-.505	4	0	1	2945.955	2	136.883	4
275		5	max	.017	2	.021	2	0	1	2.459e-3	4	NC	3	NC	1
276			min	-.023	3	-.035	3	-.452	4	0	1	3322.617	2	152.846	4
277		6	max	.016	2	.018	2	0	1	2.479e-3	4	NC	3	NC	1
278			min	-.021	3	-.032	3	-.401	4	0	1	3793.433	2	172.475	4
279		7	max	.015	2	.016	2	0	1	2.499e-3	4	NC	3	NC	1
280			min	-.019	3	-.03	3	-.351	4	0	1	4392.533	2	196.989	4
281		8	max	.013	2	.013	2	0	1	2.519e-3	4	NC	1	NC	1
282			min	-.018	3	-.027	3	-.303	4	0	1	5171.326	2	228.169	4
283		9	max	.012	2	.011	2	0	1	2.539e-3	4	NC	1	NC	1
284			min	-.016	3	-.025	3	-.257	4	0	1	6210.245	2	268.699	4
285		10	max	.011	2	.009	2	0	1	2.559e-3	4	NC	1	NC	1
286			min	-.015	3	-.022	3	-.214	4	0	1	7641.034	2	322.782	4
287		11	max	.01	2	.007	2	0	1	2.578e-3	4	NC	1	NC	1
288			min	-.013	3	-.02	3	-.174	4	0	1	9692.049	2	397.315	4
289		12	max	.008	2	.005	2	0	1	2.598e-3	4	NC	1	NC	1
290			min	-.011	3	-.017	3	-.137	4	0	1	NC	1	504.262	4
291		13	max	.007	2	.004	2	0	1	2.618e-3	4	NC	1	NC	1
292			min	-.01	3	-.015	3	-.104	4	0	1	NC	1	665.922	4
293		14	max	.006	2	.003	2	0	1	2.638e-3	4	NC	1	NC	1
294			min	-.008	3	-.012	3	-.074	4	0	1	NC	1	927.904	4
295		15	max	.005	2	.002	2	0	1	2.658e-3	4	NC	1	NC	1
296			min	-.006	3	-.01	3	-.049	4	0	1	NC	1	1396.124	4
297		16	max	.004	2	0	2	0	1	2.678e-3	4	NC	1	NC	1
298			min	-.005	3	-.007	3	-.029	4	0	1	NC	1	2366.586	4
299		17	max	.002	2	0	2	0	1	2.698e-3	4	NC	1	NC	1
300			min	-.003	3	-.005	3	-.014	4	0	1	NC	1	4956.618	4
301		18	max	.001	2	0	2	0	1	2.718e-3	4	NC	1	NC	1
302			min	-.002	3	-.002	3	-.004	4	0	1	NC	1	NC	1
303		19	max	0	1	0	1	0	1	2.738e-3	4	NC	1	NC	1
304			min	0	1	0	1	0	1	0	1	NC	1	NC	1
305	M7	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	-5.683e-4	4	NC	1	NC	1
307		2	max	.001	3	0	15	.015	4	6.146e-5	4	NC	1	NC	1
308			min	-.001	2	-.004	3	0	1	0	1	NC	1	NC	1
309		3	max	.003	3	-.001	15	.029	4	6.912e-4	4	NC	1	NC	1
310			min	-.002	2	-.007	3	0	1	0	1	NC	1	NC	1
311		4	max	.004	3	-.002	15	.042	4	1.321e-3	4	NC	1	NC	1
312			min	-.004	2	-.01	3	0	1	0	1	NC	1	9657.717	4
313		5	max	.005	3	-.003	15	.054	4	1.951e-3	4	NC	1	NC	1
314			min	-.005	2	-.013	3	0	1	0	1	8274.487	3	8225.401	4
315		6	max	.007	3	-.003	15	.066	4	2.58e-3	4	NC	1	NC	1
316			min	-.006	2	-.016	3	0	1	0	1	6969.224	3	7587.477	4
317		7	max	.008	3	-.004	15	.076	4	3.21e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
318			min	-.007	2	-.018	3	0	1	0	1	6184.595	3	7423.431	4
319		8	max	.009	3	-.004	15	.087	4	3.84e-3	4	NC	2	NC	1
320			min	-.009	2	-.02	3	0	1	0	1	5541.347	4	7635.217	4
321		9	max	.011	3	-.005	15	.096	4	4.47e-3	4	NC	2	NC	1
322			min	-.01	2	-.021	3	0	1	0	1	5156.725	4	8236.791	4
323		10	max	.012	3	-.005	15	.105	4	5.099e-3	4	NC	5	NC	1
324			min	-.011	2	-.021	3	0	1	0	1	4967.629	4	9346.487	4
325		11	max	.013	3	-.005	15	.114	4	5.729e-3	4	NC	5	NC	1
326			min	-.012	2	-.021	4	0	1	0	1	4946.037	4	NC	1
327		12	max	.015	3	-.005	15	.122	4	6.359e-3	4	NC	5	NC	1
328			min	-.014	2	-.021	4	0	1	0	1	5092.608	4	NC	1
329		13	max	.016	3	-.005	15	.13	4	6.989e-3	4	NC	5	NC	1
330			min	-.015	2	-.02	3	0	1	0	1	5438.292	4	NC	1
331		14	max	.017	3	-.004	15	.139	4	7.618e-3	4	NC	2	NC	1
332			min	-.016	2	-.018	3	0	1	0	1	6060.545	4	NC	1
333		15	max	.019	3	-.004	15	.147	4	8.248e-3	4	NC	1	NC	1
334			min	-.017	2	-.016	3	0	1	0	1	7131.699	4	NC	1
335		16	max	.02	3	-.003	15	.156	4	8.878e-3	4	NC	1	NC	1
336			min	-.019	2	-.014	3	0	1	0	1	9069.632	4	NC	1
337		17	max	.021	3	-.002	15	.166	4	9.507e-3	4	NC	1	NC	1
338			min	-.02	2	-.011	3	0	1	0	1	NC	1	NC	1
339		18	max	.023	3	-.001	15	.176	4	1.014e-2	4	NC	1	NC	1
340			min	-.021	2	-.008	3	0	1	0	1	NC	1	NC	1
341		19	max	.024	3	0	10	.188	4	1.077e-2	4	NC	1	NC	1
342			min	-.022	2	-.005	3	0	1	0	1	NC	1	NC	1
343	M8	1	max	.007	1	.021	2	0	1	0	1	NC	1	NC	1
344			min	-.001	3	-.024	3	-.188	4	-4.978e-4	4	NC	1	131.813	4
345		2	max	.007	1	.02	2	0	1	0	1	NC	1	NC	1
346			min	-.001	3	-.023	3	-.173	4	-4.978e-4	4	NC	1	143.418	4
347		3	max	.006	1	.019	2	0	1	0	1	NC	1	NC	1
348			min	-.001	3	-.022	3	-.158	4	-4.978e-4	4	NC	1	157.223	4
349		4	max	.006	1	.018	2	0	1	0	1	NC	1	NC	1
350			min	0	3	-.02	3	-.143	4	-4.978e-4	4	NC	1	173.802	4
351		5	max	.005	1	.017	2	0	1	0	1	NC	1	NC	1
352			min	0	3	-.019	3	-.128	4	-4.978e-4	4	NC	1	193.932	4
353		6	max	.005	1	.015	2	0	1	0	1	NC	1	NC	1
354			min	0	3	-.018	3	-.113	4	-4.978e-4	4	NC	1	218.693	4
355		7	max	.005	1	.014	2	0	1	0	1	NC	1	NC	1
356			min	0	3	-.016	3	-.099	4	-4.978e-4	4	NC	1	249.616	4
357		8	max	.004	1	.013	2	0	1	0	1	NC	1	NC	1
358			min	0	3	-.015	3	-.086	4	-4.978e-4	4	NC	1	288.936	4
359		9	max	.004	1	.012	2	0	1	0	1	NC	1	NC	1
360			min	0	3	-.014	3	-.073	4	-4.978e-4	4	NC	1	340.014	4
361		10	max	.003	1	.011	2	0	1	0	1	NC	1	NC	1
362			min	0	3	-.012	3	-.061	4	-4.978e-4	4	NC	1	408.108	4
363		11	max	.003	1	.01	2	0	1	0	1	NC	1	NC	1
364			min	0	3	-.011	3	-.049	4	-4.978e-4	4	NC	1	501.82	4
365		12	max	.003	1	.008	2	0	1	0	1	NC	1	NC	1
366			min	0	3	-.009	3	-.039	4	-4.978e-4	4	NC	1	636.028	4
367		13	max	.002	1	.007	2	0	1	0	1	NC	1	NC	1
368			min	0	3	-.008	3	-.03	4	-4.978e-4	4	NC	1	838.35	4
369		14	max	.002	1	.006	2	0	1	0	1	NC	1	NC	1
370			min	0	3	-.007	3	-.021	4	-4.978e-4	4	NC	1	1164.973	4
371		15	max	.002	1	.005	2	0	1	0	1	NC	1	NC	1
372			min	0	3	-.005	3	-.014	4	-4.978e-4	4	NC	1	1745.431	4
373		16	max	.001	1	.004	2	0	1	0	1	NC	1	NC	1
374			min	0	3	-.004	3	-.008	4	-4.978e-4	4	NC	1	2937.822	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
375		17	max	0	1	.002	2	0	1	0	1	NC	1	NC	1
376			min	0	3	-.003	3	-.004	4	-4.978e-4	4	NC	1	6070.015	4
377		18	max	0	1	.001	2	0	1	0	1	NC	1	NC	1
378			min	0	3	-.001	3	-.001	4	-4.978e-4	4	NC	1	NC	1
379		19	max	0	1	0	1	0	1	0	1	NC	1	NC	1
380			min	0	1	0	1	0	1	-4.978e-4	4	NC	1	NC	1
381	M10	1	max	.007	2	.009	2	0	12	2.363e-3	4	NC	1	NC	2
382			min	-.009	3	-.015	3	-.665	4	1.476e-5	12	7475.926	2	103.85	4
383		2	max	.007	2	.008	2	0	12	2.382e-3	4	NC	1	NC	2
384			min	-.009	3	-.014	3	-.611	4	1.396e-5	12	8671.147	2	113.104	4
385		3	max	.006	2	.007	2	0	12	2.401e-3	4	NC	1	NC	2
386			min	-.008	3	-.014	3	-.557	4	1.315e-5	12	NC	1	124.1	4
387		4	max	.006	2	.005	2	0	12	2.421e-3	4	NC	1	NC	1
388			min	-.008	3	-.013	3	-.503	4	1.235e-5	12	NC	1	137.293	4
389		5	max	.006	2	.004	2	0	12	2.44e-3	4	NC	1	NC	1
390			min	-.007	3	-.013	3	-.451	4	1.155e-5	12	NC	1	153.304	4
391		6	max	.005	2	.003	2	0	12	2.459e-3	4	NC	1	NC	1
392			min	-.007	3	-.012	3	-.399	4	1.075e-5	12	NC	1	172.992	4
393		7	max	.005	2	.002	2	0	12	2.479e-3	4	NC	1	NC	1
394			min	-.006	3	-.012	3	-.35	4	9.944e-6	12	NC	1	197.581	4
395		8	max	.004	2	.001	2	0	12	2.498e-3	4	NC	1	NC	1
396			min	-.006	3	-.011	3	-.302	4	9.142e-6	12	NC	1	228.857	4
397		9	max	.004	2	0	2	0	12	2.517e-3	4	NC	1	NC	1
398			min	-.005	3	-.01	3	-.256	4	8.34e-6	12	NC	1	269.511	4
399		10	max	.004	2	0	2	0	12	2.536e-3	4	NC	1	NC	1
400			min	-.005	3	-.01	3	-.213	4	7.537e-6	12	NC	1	323.762	4
401		11	max	.003	2	-.001	2	0	12	2.556e-3	4	NC	1	NC	1
402			min	-.004	3	-.009	3	-.173	4	6.735e-6	12	NC	1	398.526	4
403		12	max	.003	2	-.002	2	0	12	2.575e-3	4	NC	1	NC	1
404			min	-.004	3	-.008	3	-.137	4	5.933e-6	12	NC	1	505.81	4
405		13	max	.002	2	-.002	15	0	12	2.594e-3	4	NC	1	NC	1
406			min	-.003	3	-.007	3	-.103	4	5.13e-6	12	NC	1	667.985	4
407		14	max	.002	2	-.002	15	0	12	2.613e-3	4	NC	1	NC	1
408			min	-.003	3	-.006	3	-.074	4	4.328e-6	12	NC	1	930.817	4
409		15	max	.002	2	-.001	15	0	12	2.633e-3	4	NC	1	NC	1
410			min	-.002	3	-.005	3	-.049	4	3.424e-6	10	NC	1	1400.594	4
411		16	max	.001	2	-.001	15	0	12	2.652e-3	4	NC	1	NC	1
412			min	-.002	3	-.004	4	-.029	4	2.508e-6	10	NC	1	2374.406	4
413		17	max	0	2	0	15	0	12	2.671e-3	4	NC	1	NC	1
414			min	-.001	3	-.003	4	-.014	4	1.592e-6	10	NC	1	4973.957	4
415		18	max	0	2	0	15	0	12	2.69e-3	4	NC	1	NC	1
416			min	0	3	-.002	4	-.004	4	6.752e-7	10	NC	1	NC	1
417		19	max	0	1	0	1	0	1	2.71e-3	4	NC	1	NC	1
418			min	0	1	0	1	0	1	-9.226e-7	1	NC	1	NC	1
419	M11	1	max	0	1	0	1	0	1	1.456e-6	1	NC	1	NC	1
420			min	0	1	0	1	0	1	-5.616e-4	4	NC	1	NC	1
421		2	max	0	3	0	15	.015	4	7.622e-5	5	NC	1	NC	1
422			min	0	2	-.003	4	0	1	-2.129e-5	1	NC	1	NC	1
423		3	max	0	3	-.001	15	.028	4	7.1e-4	4	NC	1	NC	1
424			min	0	2	-.006	4	0	1	-4.403e-5	1	NC	1	NC	1
425		4	max	.001	3	-.002	15	.041	4	1.346e-3	4	NC	1	NC	1
426			min	-.001	2	-.009	4	0	1	-6.677e-5	1	NC	1	NC	1
427		5	max	.002	3	-.003	15	.054	4	1.982e-3	4	NC	1	NC	1
428			min	-.001	2	-.012	4	0	1	-8.952e-5	1	8615.912	4	9058.911	4
429		6	max	.002	3	-.004	15	.065	4	2.617e-3	4	NC	2	NC	1
430			min	-.002	2	-.015	4	0	1	-1.123e-4	1	6968.443	4	8456.237	4
431		7	max	.003	3	-.004	15	.076	4	3.253e-3	4	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
432			min	-.002	2	-.018	4	0	1	-1.35e-4	1	5976.861	4	8396.734	4
433		8	max	.003	3	-.005	15	.086	4	3.889e-3	4	NC	5	NC	1
434			min	-.003	2	-.02	4	0	1	-1.577e-4	1	5365.112	4	8801.737	4
435		9	max	.004	3	-.005	15	.095	4	4.525e-3	4	NC	5	NC	1
436			min	-.003	2	-.021	4	0	1	-1.805e-4	1	5003.302	4	9738.298	4
437		10	max	.004	3	-.005	15	.104	4	5.161e-3	4	NC	5	NC	1
438			min	-.003	2	-.022	4	-.001	1	-2.032e-4	1	4828.374	4	NC	1
439		11	max	.004	3	-.005	15	.113	4	5.796e-3	4	NC	5	NC	1
440			min	-.004	2	-.022	4	-.002	1	-2.26e-4	1	4814.549	4	NC	1
441		12	max	.005	3	-.005	15	.122	4	6.432e-3	4	NC	5	NC	1
442			min	-.004	2	-.021	4	-.002	1	-2.487e-4	1	4963.437	4	NC	1
443		13	max	.005	3	-.005	15	.13	4	7.068e-3	4	NC	5	NC	1
444			min	-.004	2	-.02	4	-.003	1	-2.715e-4	1	5305.925	4	NC	1
445		14	max	.006	3	-.005	15	.139	4	7.704e-3	4	NC	5	NC	1
446			min	-.005	2	-.018	4	-.003	1	-2.942e-4	1	5918.197	4	NC	1
447		15	max	.006	3	-.004	15	.148	4	8.34e-3	4	NC	3	NC	1
448			min	-.005	2	-.016	4	-.004	1	-3.169e-4	1	6969.147	4	NC	1
449		16	max	.007	3	-.003	15	.157	4	8.975e-3	4	NC	1	NC	1
450			min	-.005	2	-.013	4	-.005	1	-3.397e-4	1	8867.865	4	NC	1
451		17	max	.007	3	-.002	15	.167	4	9.611e-3	4	NC	1	NC	1
452			min	-.006	2	-.009	4	-.006	1	-3.624e-4	1	NC	1	NC	1
453		18	max	.007	3	-.002	15	.178	4	1.025e-2	4	NC	1	NC	1
454			min	-.006	2	-.005	4	-.007	1	-3.852e-4	1	NC	1	NC	1
455		19	max	.008	3	0	10	.191	4	1.088e-2	4	NC	1	NC	1
456			min	-.006	2	-.002	1	-.008	1	-4.079e-4	1	NC	1	NC	1
457	M12	1	max	.003	1	.006	2	.008	1	-7.275e-6	12	NC	1	NC	3
458			min	0	3	-.008	3	-.191	4	-4.003e-4	4	NC	1	129.984	4
459		2	max	.002	1	.006	2	.007	1	-7.275e-6	12	NC	1	NC	3
460			min	0	3	-.008	3	-.175	4	-4.003e-4	4	NC	1	141.417	4
461		3	max	.002	1	.005	2	.007	1	-7.275e-6	12	NC	1	NC	3
462			min	0	3	-.007	3	-.16	4	-4.003e-4	4	NC	1	155.019	4
463		4	max	.002	1	.005	2	.006	1	-7.275e-6	12	NC	1	NC	2
464			min	0	3	-.007	3	-.145	4	-4.003e-4	4	NC	1	171.354	4
465		5	max	.002	1	.005	2	.005	1	-7.275e-6	12	NC	1	NC	2
466			min	0	3	-.006	3	-.13	4	-4.003e-4	4	NC	1	191.189	4
467		6	max	.002	1	.004	2	.005	1	-7.275e-6	12	NC	1	NC	2
468			min	0	3	-.006	3	-.115	4	-4.003e-4	4	NC	1	215.587	4
469		7	max	.002	1	.004	2	.004	1	-7.275e-6	12	NC	1	NC	2
470			min	0	3	-.005	3	-.101	4	-4.003e-4	4	NC	1	246.057	4
471		8	max	.002	1	.004	2	.004	1	-7.275e-6	12	NC	1	NC	2
472			min	0	3	-.005	3	-.087	4	-4.003e-4	4	NC	1	284.801	4
473		9	max	.001	1	.003	2	.003	1	-7.275e-6	12	NC	1	NC	2
474			min	0	3	-.005	3	-.074	4	-4.003e-4	4	NC	1	335.13	4
475		10	max	.001	1	.003	2	.003	1	-7.275e-6	12	NC	1	NC	2
476			min	0	3	-.004	3	-.062	4	-4.003e-4	4	NC	1	402.227	4
477		11	max	.001	1	.003	2	.002	1	-7.275e-6	12	NC	1	NC	1
478			min	0	3	-.004	3	-.05	4	-4.003e-4	4	NC	1	494.565	4
479		12	max	.001	1	.002	2	.002	1	-7.275e-6	12	NC	1	NC	1
480			min	0	3	-.003	3	-.04	4	-4.003e-4	4	NC	1	626.804	4
481		13	max	0	1	.002	2	.001	1	-7.275e-6	12	NC	1	NC	1
482			min	0	3	-.003	3	-.03	4	-4.003e-4	4	NC	1	826.154	4
483		14	max	0	1	.002	2	0	1	-7.275e-6	12	NC	1	NC	1
484			min	0	3	-.002	3	-.022	4	-4.003e-4	4	NC	1	1147.976	4
485		15	max	0	1	.001	2	0	1	-7.275e-6	12	NC	1	NC	1
486			min	0	3	-.002	3	-.014	4	-4.003e-4	4	NC	1	1719.887	4
487		16	max	0	1	.001	2	0	1	-7.275e-6	12	NC	1	NC	1
488			min	0	3	-.001	3	-.009	4	-4.003e-4	4	NC	1	2894.691	4

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
489		17	max	0	1	0	2	0	1	-7.275e-6	12	NC	1	NC	1
490			min	0	3	0	3	-.004	4	-4.003e-4	4	NC	1	5980.57	4
491		18	max	0	1	0	2	0	1	-7.275e-6	12	NC	1	NC	1
492			min	0	3	0	3	-.001	4	-4.003e-4	4	NC	1	NC	1
493		19	max	0	1	0	1	0	1	-7.275e-6	12	NC	1	NC	1
494			min	0	1	0	1	0	1	-4.003e-4	4	NC	1	NC	1
495	M1	1	max	.01	3	.21	2	.704	4	8.341e-3	1	NC	1	NC	1
496			min	-.006	2	-.051	3	0	12	-1.814e-2	3	NC	1	NC	1
497		2	max	.01	3	.102	2	.683	4	7.769e-3	4	NC	5	NC	1
498			min	-.006	2	-.024	3	-.006	1	-9.003e-3	3	1262.68	2	NC	1
499		3	max	.01	3	.015	3	.66	4	1.389e-2	4	NC	5	NC	1
500			min	-.006	2	-.012	2	-.008	1	-1.646e-4	1	611.031	2	6139.082	5
501		4	max	.01	3	.077	3	.637	4	1.2e-2	4	NC	15	NC	1
502			min	-.006	2	-.139	2	-.008	1	-4.165e-3	3	388.41	2	4436.998	5
503		5	max	.01	3	.155	3	.613	4	1.01e-2	4	NC	15	NC	1
504			min	-.006	2	-.271	2	-.005	1	-8.23e-3	3	281.849	2	3572.722	5
505		6	max	.01	3	.239	3	.589	4	1.256e-2	2	8299.51	15	NC	1
506			min	-.006	2	-.398	2	-.002	1	-1.229e-2	3	222.895	2	3041.89	5
507		7	max	.009	3	.318	3	.563	4	1.675e-2	2	7014.126	15	NC	1
508			min	-.005	2	-.511	2	0	3	-1.636e-2	3	187.983	2	2660.378	4
509		8	max	.009	3	.385	3	.538	4	2.094e-2	2	6252.448	15	NC	1
510			min	-.005	2	-.6	2	0	12	-2.042e-2	3	167.289	2	2367.333	4
511		9	max	.009	3	.428	3	.512	4	2.342e-2	2	5853.434	15	NC	1
512			min	-.005	2	-.657	2	0	1	-2.089e-2	3	156.488	2	2164.94	4
513		10	max	.009	3	.444	3	.482	4	2.476e-2	2	5731.345	15	NC	1
514			min	-.005	2	-.675	2	0	10	-1.894e-2	3	153.314	2	2095.645	4
515		11	max	.009	3	.434	3	.449	4	2.611e-2	2	5853.136	15	NC	1
516			min	-.005	2	-.656	2	0	12	-1.7e-2	3	156.998	2	2124.048	4
517		12	max	.008	3	.398	3	.414	4	2.493e-2	2	6251.74	15	NC	1
518			min	-.005	2	-.598	2	0	1	-1.466e-2	3	168.79	2	2251.788	4
519		13	max	.008	3	.339	3	.373	4	2.e-2	2	7012.744	15	NC	1
520			min	-.005	2	-.505	2	0	1	-1.173e-2	3	191.533	2	2655.682	4
521		14	max	.008	3	.264	3	.328	4	1.506e-2	2	8296.981	15	NC	1
522			min	-.005	2	-.388	2	0	12	-8.798e-3	3	230.328	2	3577.894	4
523		15	max	.008	3	.18	3	.282	4	1.013e-2	2	NC	15	NC	1
524			min	-.005	2	-.259	2	0	12	-5.868e-3	3	296.862	2	5812.16	4
525		16	max	.007	3	.091	3	.237	4	8.939e-3	4	NC	15	NC	1
526			min	-.005	2	-.128	2	0	12	-2.938e-3	3	419.411	2	NC	1
527		17	max	.007	3	.005	3	.196	4	1.014e-2	4	NC	5	NC	1
528			min	-.005	2	-.007	2	0	12	-7.614e-6	3	679.582	2	NC	1
529		18	max	.007	3	.096	2	.161	4	6.549e-3	2	NC	5	NC	1
530			min	-.005	2	-.073	3	0	12	-2.195e-3	3	1435.023	2	NC	1
531		19	max	.007	3	.188	2	.132	4	1.304e-2	2	NC	1	NC	1
532			min	-.005	2	-.147	3	0	1	-4.473e-3	3	NC	1	NC	1
533	M5	1	max	.031	3	.365	2	.704	4	0	1	NC	1	NC	1
534			min	-.021	2	-.009	3	0	1	-1.086e-5	4	NC	1	NC	1
535		2	max	.031	3	.178	2	.688	4	7.111e-3	4	NC	5	NC	1
536			min	-.021	2	-.003	3	0	1	0	1	730.12	2	8453.059	4
537		3	max	.031	3	.045	3	.667	4	1.406e-2	4	NC	15	NC	1
538			min	-.022	2	-.036	2	0	1	0	1	340.347	2	4978.222	4
539		4	max	.03	3	.169	3	.643	4	1.146e-2	4	8605.452	15	NC	1
540			min	-.021	2	-.296	2	0	1	0	1	206.067	2	3857.115	4
541		5	max	.029	3	.347	3	.617	4	8.853e-3	4	5978.225	15	NC	1
542			min	-.021	2	-.582	2	0	1	0	1	143.677	2	3313.462	4
543		6	max	.029	3	.55	3	.59	4	6.249e-3	4	4577.922	15	NC	1
544			min	-.02	2	-.868	2	0	1	0	1	110.269	2	2971.176	4
545		7	max	.028	3	.751	3	.563	4	3.644e-3	4	3773.678	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
546			min	-.02	2	-1.129	2	0	1	0	1	91.012	2	2689.427	4
547		8	max	.027	3	.921	3	.537	4	1.04e-3	4	3308.118	15	NC	1
548			min	-.019	2	-1.339	2	0	1	0	1	79.836	2	2403.578	4
549		9	max	.027	3	1.031	3	.512	4	0	1	3069.857	15	NC	1
550			min	-.019	2	-1.472	2	0	1	-6.298e-6	5	74.107	2	2157.858	4
551		10	max	.026	3	1.071	3	.481	4	0	1	2998.09	15	NC	1
552			min	-.019	2	-1.518	2	0	1	-6.037e-6	5	72.432	2	2114.673	4
553		11	max	.025	3	1.044	3	.448	4	0	1	3070.035	15	NC	1
554			min	-.018	2	-1.473	2	0	1	-5.776e-6	5	74.376	2	2156.406	4
555		12	max	.025	3	.953	3	.415	4	7.174e-4	4	3308.536	15	NC	1
556			min	-.018	2	-1.335	2	0	1	0	1	80.724	2	2207.827	4
557		13	max	.024	3	.806	3	.375	4	2.515e-3	4	3774.51	15	NC	1
558			min	-.018	2	-1.114	2	0	1	0	1	93.339	2	2583.775	4
559		14	max	.024	3	.621	3	.328	4	4.312e-3	4	4579.521	15	NC	1
560			min	-.017	2	-.841	2	0	1	0	1	115.589	2	3637.939	4
561		15	max	.023	3	.415	3	.279	4	6.11e-3	4	5981.354	15	NC	1
562			min	-.017	2	-.547	2	0	1	0	1	155.488	2	6893.839	4
563		16	max	.022	3	.207	3	.231	4	7.907e-3	4	8611.983	15	NC	1
564			min	-.017	2	-.262	2	0	1	0	1	233.406	2	NC	1
565		17	max	.022	3	.014	3	.189	4	9.705e-3	4	NC	15	NC	1
566			min	-.017	2	-.019	2	0	1	0	1	409.611	2	NC	1
567		18	max	.022	3	.16	1	.156	4	4.909e-3	4	NC	5	NC	1
568			min	-.017	2	-.148	3	0	1	0	1	922.906	2	NC	1
569		19	max	.022	3	.304	1	.132	4	0	1	NC	1	NC	1
570			min	-.016	2	-.293	3	0	1	-5.902e-6	4	NC	1	NC	1
571	M9	1	max	.01	3	.21	2	.703	4	1.814e-2	3	NC	1	NC	1
572			min	-.006	2	-.051	3	0	1	-8.341e-3	1	NC	1	NC	1
573		2	max	.01	3	.102	2	.686	4	9.003e-3	3	NC	5	NC	1
574			min	-.006	2	-.024	3	0	12	-4.014e-3	1	1262.68	2	9290.856	4
575		3	max	.01	3	.015	3	.665	4	1.401e-2	4	NC	5	NC	1
576			min	-.006	2	-.012	2	0	12	-1.824e-5	10	611.031	2	5339.567	4
577		4	max	.01	3	.077	3	.641	4	1.104e-2	5	NC	15	NC	1
578			min	-.006	2	-.139	2	0	12	-4.177e-3	2	388.41	2	4027.999	4
579		5	max	.01	3	.155	3	.616	4	8.346e-3	5	NC	15	NC	1
580			min	-.006	2	-.271	2	0	12	-8.367e-3	2	281.849	2	3373.994	4
581		6	max	.01	3	.239	3	.59	4	1.229e-2	3	8262.789	15	NC	1
582			min	-.006	2	-.398	2	0	12	-1.256e-2	2	222.895	2	2966.071	4
583		7	max	.009	3	.318	3	.563	4	1.636e-2	3	6983.957	15	NC	1
584			min	-.005	2	-.511	2	0	1	-1.675e-2	2	187.983	2	2657.948	4
585		8	max	.009	3	.385	3	.538	4	2.042e-2	3	6226.077	15	NC	1
586			min	-.005	2	-.6	2	0	1	-2.094e-2	2	167.289	2	2383.634	4
587		9	max	.009	3	.428	3	.512	4	2.089e-2	3	5829	15	NC	1
588			min	-.005	2	-.657	2	0	12	-2.342e-2	2	156.488	2	2158.549	4
589		10	max	.009	3	.444	3	.482	4	1.894e-2	3	5707.462	15	NC	1
590			min	-.005	2	-.675	2	0	1	-2.476e-2	2	153.314	2	2096.55	4
591		11	max	.009	3	.434	3	.449	4	1.7e-2	3	5828.654	15	NC	1
592			min	-.005	2	-.656	2	0	1	-2.611e-2	2	156.998	2	2131.563	4
593		12	max	.008	3	.398	3	.414	4	1.466e-2	3	6225.404	15	NC	1
594			min	-.005	2	-.598	2	0	12	-2.493e-2	2	168.79	2	2236.867	4
595		13	max	.008	3	.339	3	.373	4	1.173e-2	3	6982.897	15	NC	1
596			min	-.005	2	-.505	2	0	10	-2.e-2	2	191.533	2	2653.501	4
597		14	max	.008	3	.264	3	.327	4	8.798e-3	3	8261.162	15	NC	1
598			min	-.005	2	-.388	2	-.002	1	-1.506e-2	2	230.328	2	3665.564	5
599		15	max	.008	3	.18	3	.279	4	5.883e-3	5	NC	15	NC	1
600			min	-.005	2	-.259	2	-.005	1	-1.013e-2	2	296.862	2	6300.443	5
601		16	max	.007	3	.091	3	.233	4	7.853e-3	5	NC	15	NC	1
602			min	-.005	2	-.128	2	-.007	1	-5.193e-3	2	419.411	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
603		17	max	.007	3	.005	3	.191	4	9.864e-3	4	NC	5	NC	1
604			min	-.005	2	-.007	2	-.008	1	-5.266e-4	1	679.582	2	NC	1
605		18	max	.007	3	.096	2	.158	4	4.807e-3	5	NC	5	NC	1
606			min	-.005	2	-.073	3	-.006	1	-6.549e-3	2	1435.023	2	NC	1
607		19	max	.007	3	.188	2	.132	4	4.473e-3	3	NC	1	NC	1
608			min	-.005	2	-.147	3	0	12	-1.304e-2	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

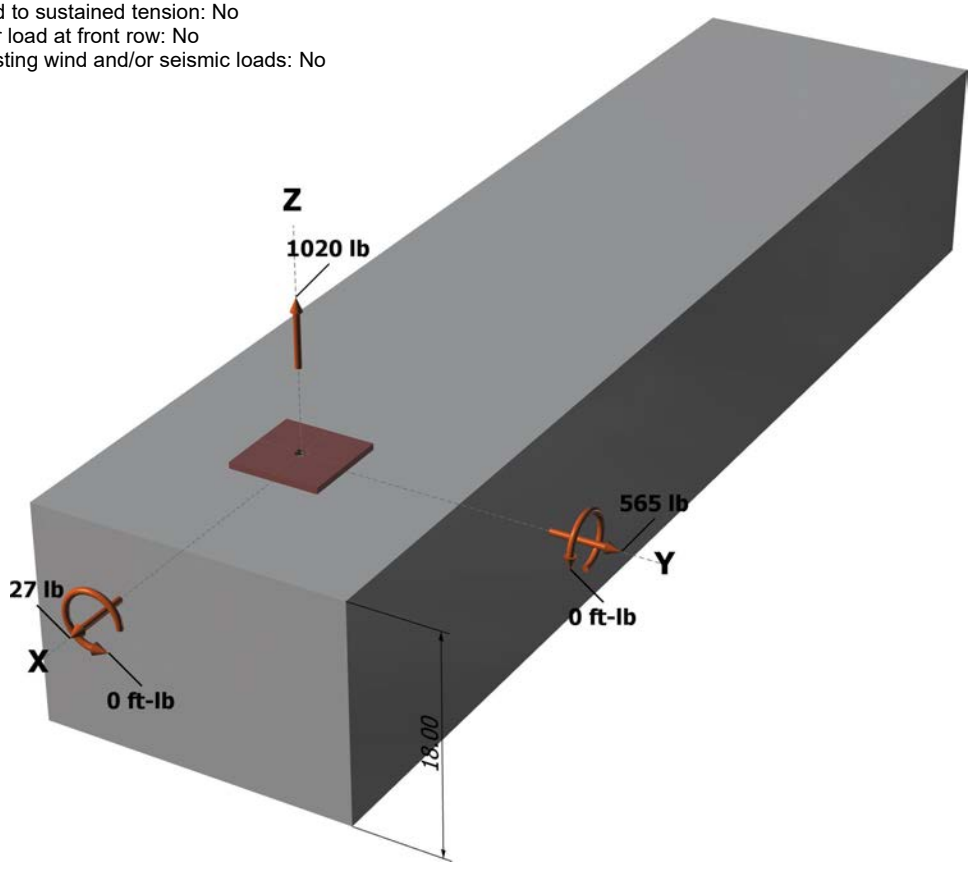
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>

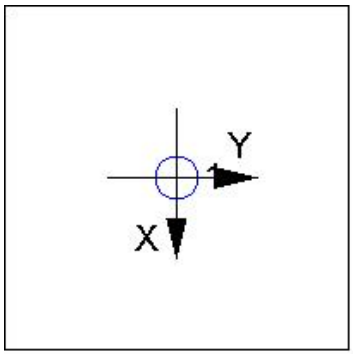
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	1020.0	27.0	565.0	565.6
Sum	1020.0	27.0	565.0	565.6

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1020
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.247	10215

$\phi N_{cb} = \phi (A_{Nc} / A_{Nco}) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
220.36	247.75	0.967	1.00	1.000	10215	0.65	5710

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi (A_{Na} / A_{Na0}) \Psi_{ed,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\,\Psi_{c,V}\,\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
192.89	220.50	0.925	1.000	1.000	6947	0.70	3934

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\,\Psi_{c,V}\,\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
165.27	278.72	0.878	1.000	1.000	8282	0.70	3018

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	7.00	6947

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\,\Psi_{c,V}\,\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
192.89	220.50	1.000	1.000	1.000	6947	0.70	8508

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\,\Psi_{c,V}\,\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
165.27	278.72	1.000	1.000	1.000	8282	0.70	6875

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi \min|k_{cp}N_a\,;\, k_{cp}N_{cb}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na}N_{a0}\,;\, k_{cp}(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
220.36	247.75	0.967	1.000	1.000	10215	8785	0.70	12298

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	1020	6071	0.17	Pass
Concrete breakout	1020	5710	0.18	Pass
Adhesive	**1020**	**5365**	**0.19**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	**566**	**3156**	**0.18**	**Pass (Governs)**
T Concrete breakout y+	565	3934	0.14	Pass
T Concrete breakout x+	27	3018	0.01	Pass
|| Concrete breakout y+	27	8508	0.00	Pass
|| Concrete breakout x+	565	6875	0.08	Pass
Concrete breakout, combined	-	-	0.14	Pass
Pryout	566	12298	0.05	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.19	0.00	19.0 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

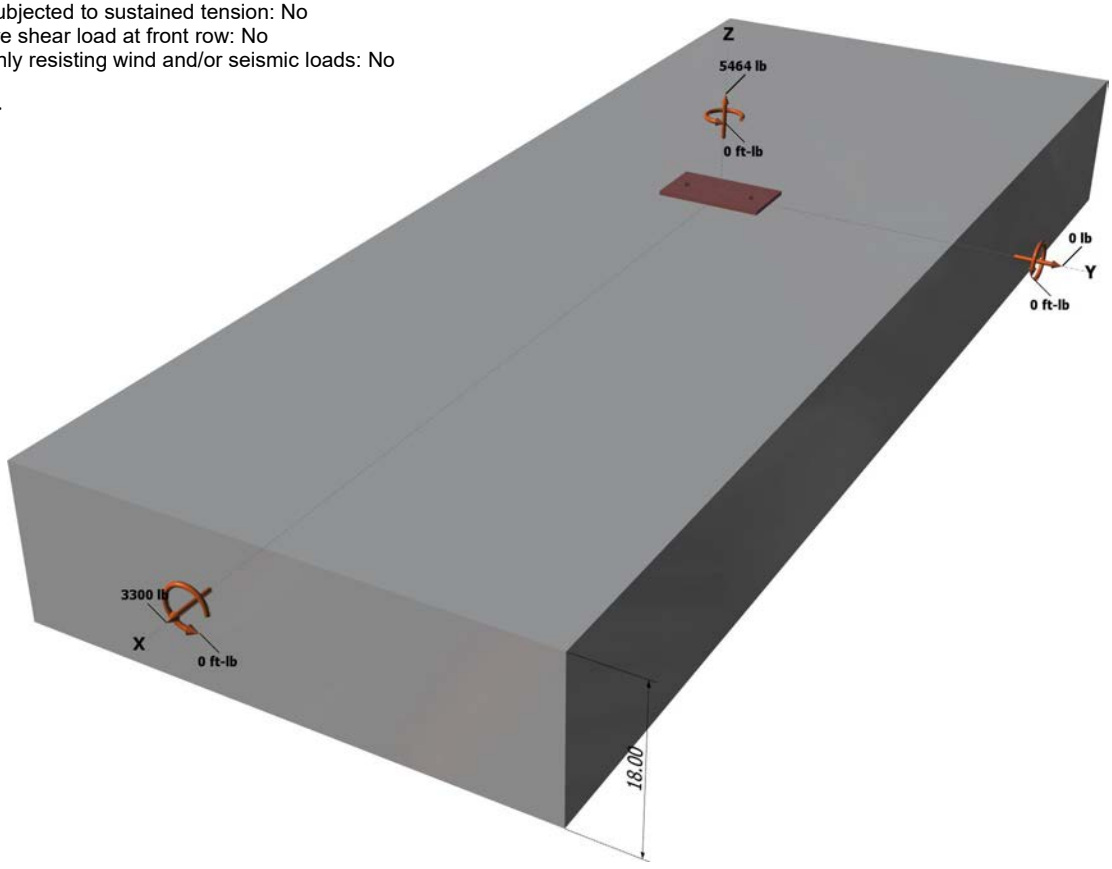
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

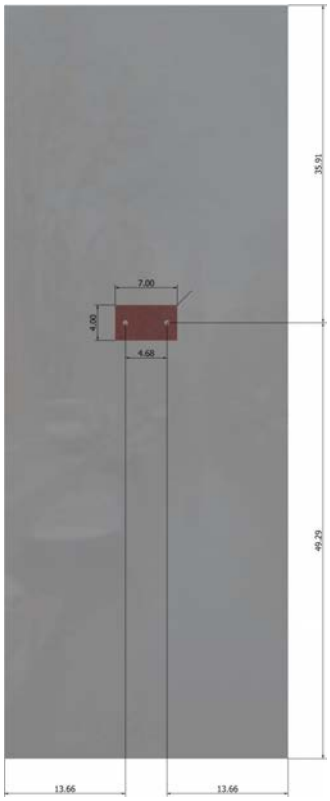
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 7.00 x 0.28

<Figure 1>



<Figure 2>



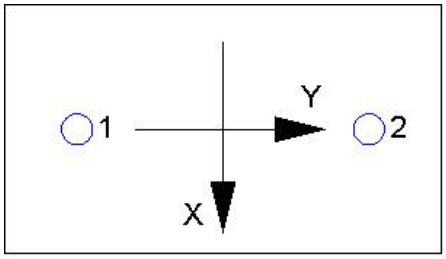
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	2732.0	1650.0	0.0	1650.0
2	2732.0	1650.0	0.0	1650.0
Sum	5464.0	3300.0	0.0	3300.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 5464
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	6.000	12492

$\phi N_{cbg} = \phi (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in²)	A_{Nco} (in²)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
408.24	324.00	1.000	1.000	1.00	1.000	12492	0.65	10231

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi (A_{Na} / A_{Na0}) \Psi_{ed,Na} \Psi_{g,Na} \Psi_{ec,Na} \Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in²)	A_{Na0} (in²)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
158.66	109.66	1.000	1.043	1.000	1.000	9755	0.55	8093

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbgx} = \phi\,(A_{Vc} / A_{Vco})\,\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-22)

A_{Vc} (in²)	A_{Vco} (in²)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
576.00	648.00	1.000	0.928	1.000	1.000	15593	0.70	9001

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	13.66	18939

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\,\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in²)	A_{Vco} (in²)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
737.64	839.68	1.000	1.000	1.000	18939	0.70	23292

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi \min|k_{cp}N_{ag}\,;\, k_{cp}N_{cbg}| = \phi \min|k_{cp}(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\, k_{cp}(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in²)	A_{Na0} (in²)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	158.66	109.66	1.000	1.043	1.000	1.000	9755	14715

A_{Nc} (in²)	A_{Nco} (in²)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
408.24	324.00	1.000	1.000	1.000	1.000	12492	15740	0.70

ϕV_{cpg} (lb)
20601

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, øN_n (lb)	Ratio	Status
Steel	2732	6071	0.45	Pass
Concrete breakout	5464	10231	0.53	Pass
Adhesive	**5464**	**8093**	**0.68**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, øV_n (lb)	Ratio	Status
Steel	**1650**	**3156**	**0.52**	**Pass (Governs)**
T Concrete breakout x+	3300	9001	0.37	Pass

|| Concrete breakout y-	1650	23292	0.07	Pass
Pryout	3300	20601	0.16	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.3	0.68	0.52	119.8 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.