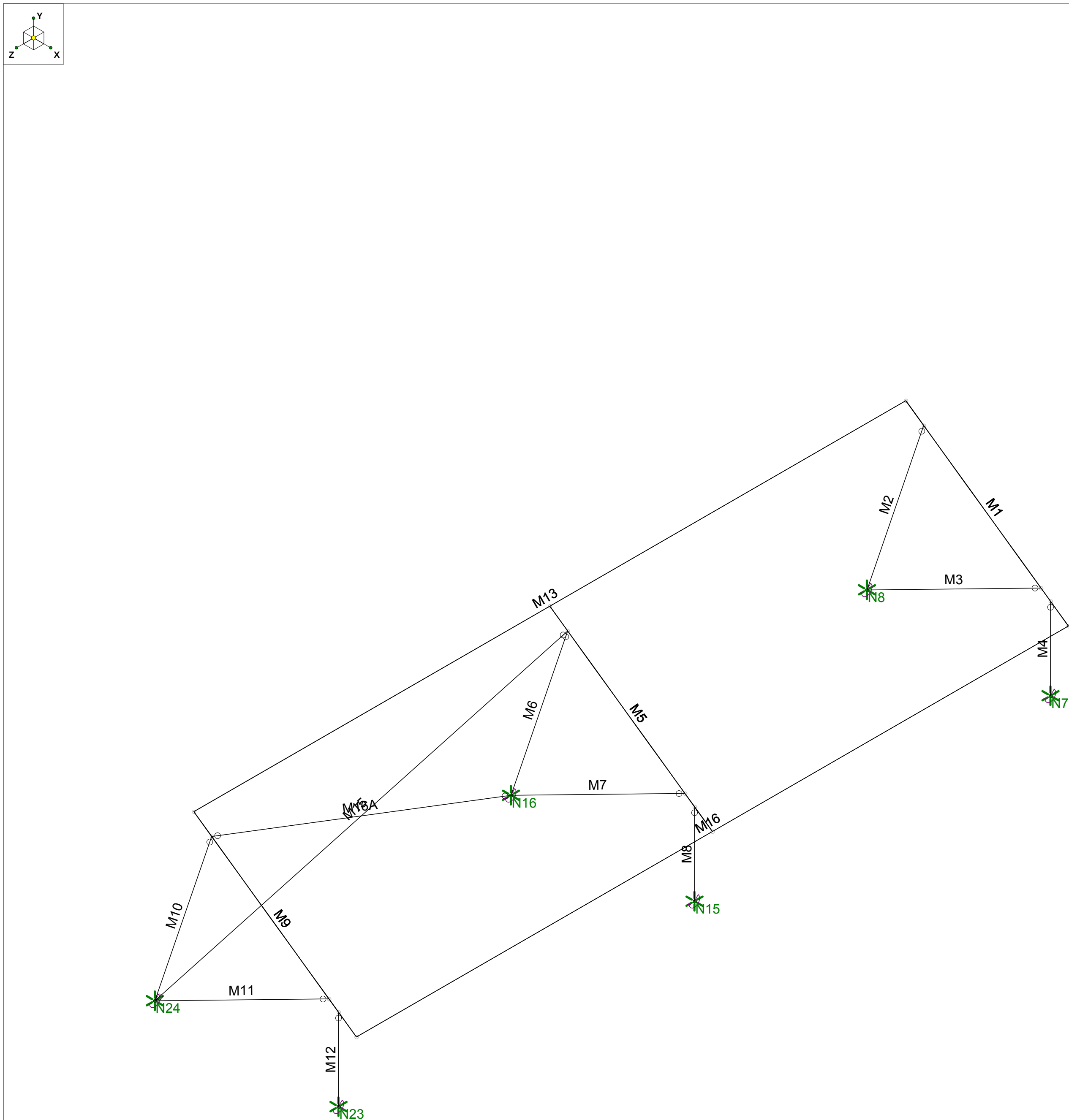


Schletter, Inc.		35° Tilt w/ Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

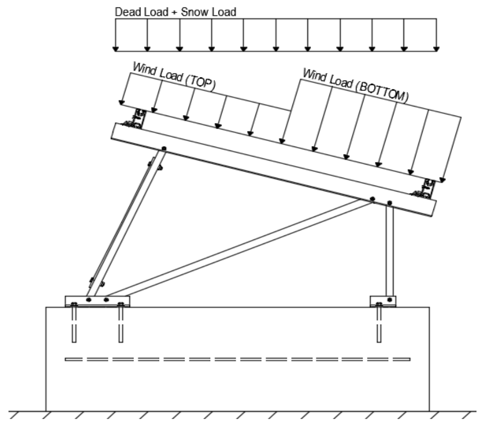
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row =	1
Module Tilt =	35°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	14.43	psf	*(ASCE 7-10, Eq. 7.4-1)*
I_s =	1.00		
C_s =	0.64		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	140	mph	Exposure Category = C
Height ≤	15	ft	Importance Category = II

Peak Velocity Pressure, q_z = 30.77 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.2	*(Pressure)*
$Cf+_{BOTTOM}$	=	2	
$Cf-_{TOP}$	=	-2.4	*(Suction)*
$Cf-_{BOTTOM}$	=	-1.2	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	Diagonal Struts	Location	Front Reactions	Location
M13	Top	M3	Outer	N7	Outer
M16	Bottom	M7	Inner	N15	Inner
		M11	Outer	N23	Outer

Girders	Location	Rear Struts	Location	Rear Reactions	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

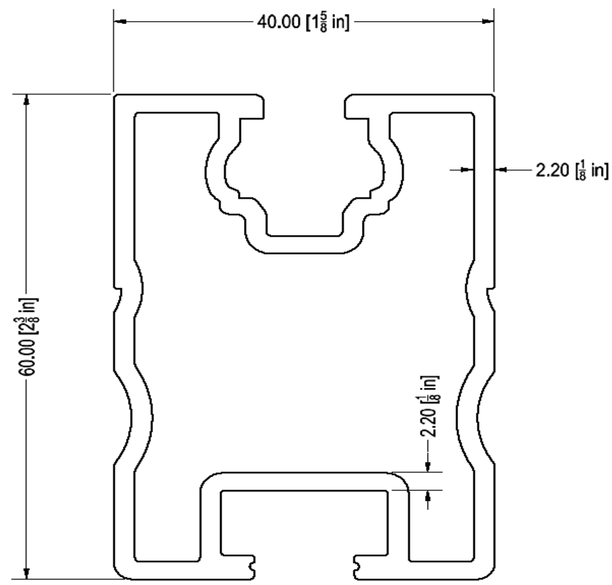
Front Struts	Location	Bracing
M4	Outer	M15
M8	Inner	M16A
M12	Outer	

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

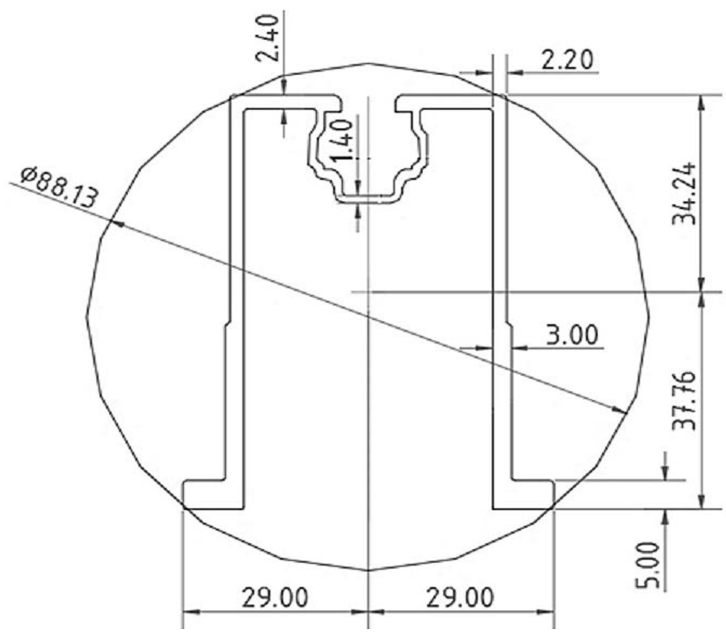
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	54	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.52	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	0.463	k-ft
M_z =	0.044	k-ft
$M_{y\ allowable}$ =	1.256	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	42%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

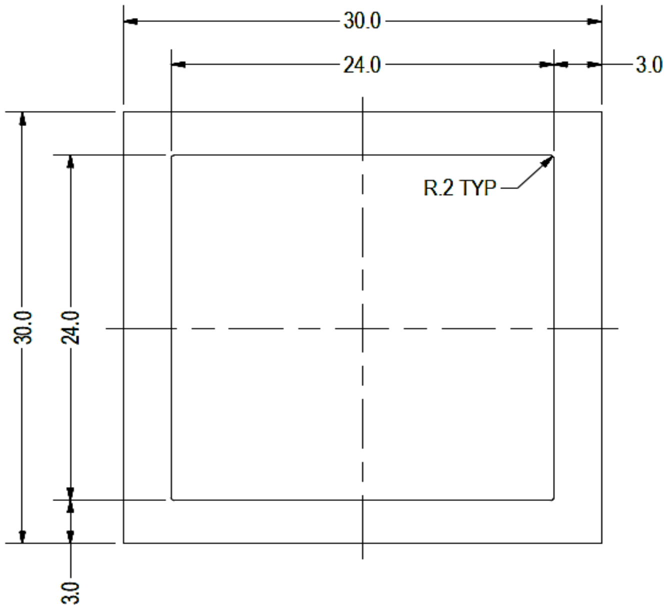
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.61	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	0.595	k-ft
M_z =	0.000	k-ft
P_n =	0.275	k
$M_{y\ allowable}$ =	1.453	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	43%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

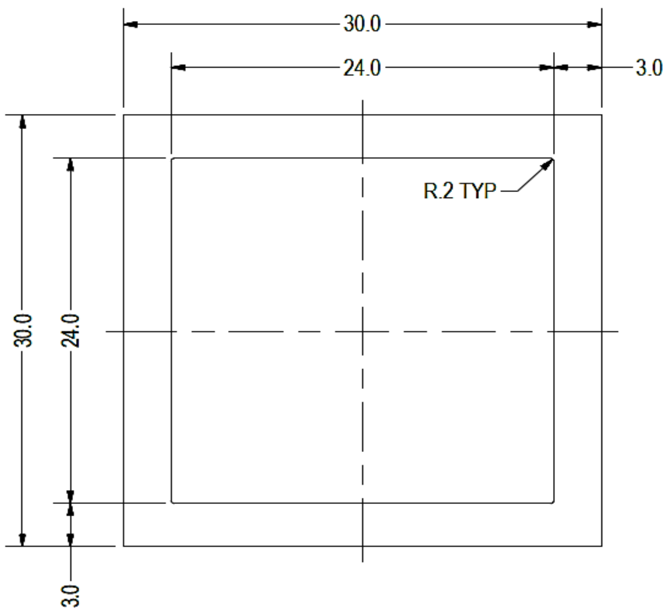
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.030	k-ft
P_n =	0.151	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	8%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

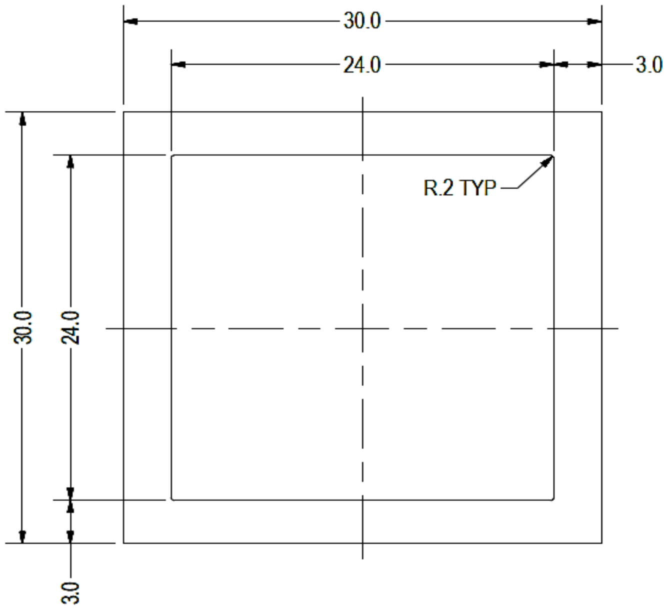
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.766	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	20%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

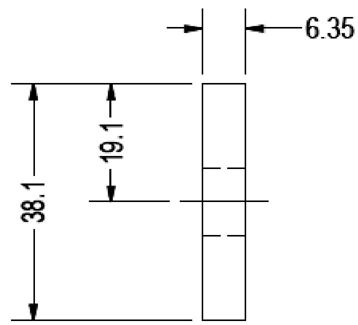
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	42.32	in
$\Phi F_{ty\ AXIAL}$ =	8.86	ksi
$\Phi F_{ty\ BENDING}$ =	29.96	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.640	k
$M_{y\ allowable}$ =	0.406	k-ft
$M_{z\ allowable}$ =	0.406	k-ft
$P_{n\ allowable}$ =	4.450	k
Utilization =	14%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.003	k-ft
P_n =	0.188	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	8%	



A cross brace kit is required every 24 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

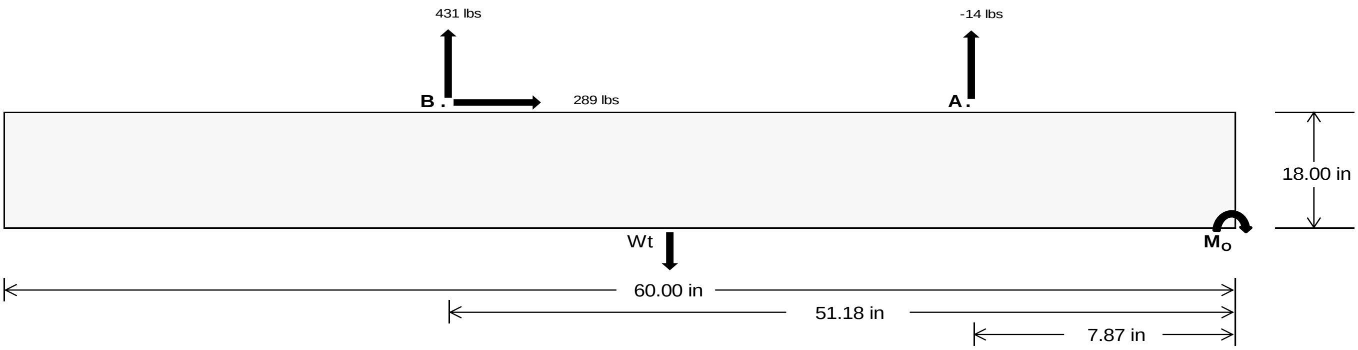
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	5.36	1868.84	k
Compressive Load =	926.13	1246.42	k
Lateral Load =	24.61	1254.29	k
Moment (Weak Axis) =	0.04	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



<u>Concrete Properties</u>

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

<u>Footing Reinforcement</u>

Use fiber reinforcing with (1) #5 rebar.

<u>Overturning Check</u>

M_O =	27132.9 in-lbs
Resisting Force Required =	904.43 lbs
S.F. =	1.67
Weight Required =	1507.38 lbs
Minimum Width =	<u>21 in</u> in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.

<u>Sliding</u>

Force =	289.32 lbs
Friction =	0.4
Weight Required =	723.29 lbs
Resisting Weight =	1903.13 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

<u>Cohesion</u>

Sliding Force =	289.32 lbs
Cohesion =	130 psf
Area =	8.75 ft^2
Resisting =	951.56 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation. Cohesion is OK.

<u>Shear Key</u>

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

<u>Bearing Pressure</u>

	Ballast Width			
	21 in	22 in	23 in	24 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.75 ft) =	1903 lbs	1994 lbs	2084 lbs	2175 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in
F_A	326 lbs	326 lbs	326 lbs	326 lbs	327 lbs	327 lbs	327 lbs	327 lbs	457 lbs	457 lbs	457 lbs	457 lbs	28 lbs	28 lbs	28 lbs	28 lbs
F_B	213 lbs	213 lbs	213 lbs	213 lbs	537 lbs	537 lbs	537 lbs	537 lbs	540 lbs	540 lbs	540 lbs	540 lbs	-861 lbs	-861 lbs	-861 lbs	-861 lbs
F_V	35 lbs	35 lbs	35 lbs	35 lbs	523 lbs	523 lbs	523 lbs	523 lbs	415 lbs	415 lbs	415 lbs	415 lbs	-579 lbs	-579 lbs	-579 lbs	-579 lbs
P_{total}	2442 lbs	2533 lbs	2623 lbs	2714 lbs	2768 lbs	2859 lbs	2949 lbs	3040 lbs	2900 lbs	2991 lbs	3081 lbs	3172 lbs	309 lbs	363 lbs	417 lbs	472 lbs
M	279 lbs-ft	279 lbs-ft	279 lbs-ft	279 lbs-ft	439 lbs-ft	439 lbs-ft	439 lbs-ft	439 lbs-ft	512 lbs-ft	512 lbs-ft	512 lbs-ft	512 lbs-ft	703 lbs-ft	703 lbs-ft	703 lbs-ft	703 lbs-ft
e	0.11 ft	0.11 ft	0.11 ft	0.10 ft	0.16 ft	0.15 ft	0.15 ft	0.14 ft	0.18 ft	0.17 ft	0.17 ft	0.16 ft	2.28 ft	1.94 ft	1.68 ft	1.49 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	240.8 psf	239.8 psf	238.8 psf	237.9 psf	256.1 psf	254.4 psf	252.7 psf	251.3 psf	261.2 psf	259.2 psf	257.4 psf	255.8 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	317.4 psf	312.8 psf	308.7 psf	304.9 psf	376.6 psf	369.3 psf	362.7 psf	356.7 psf	401.7 psf	393.3 psf	385.6 psf	378.6 psf	530.1 psf	234.4 psf	178.0 psf	155.8 psf

Maximum Bearing Pressure =	530 psf
Allowable Bearing Pressure =	1500 psf

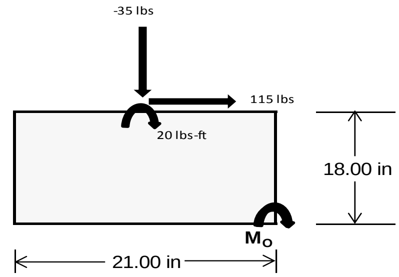
Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O = 222.0 ft-lbs
Resisting Force Required = 253.69 lbs
S.F. = 1.67
Weight Required = 422.82 lbs
Minimum Width = 21 in in
Weight Provided = 1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	21 in			21 in			21 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	127 lbs	64 lbs	62 lbs	219 lbs	396 lbs	169 lbs	86 lbs	-35 lbs	23 lbs
F_V	14 lbs	115 lbs	14 lbs	10 lbs	86 lbs	11 lbs	14 lbs	115 lbs	14 lbs
P_{total}	2483 lbs	2420 lbs	2418 lbs	2462 lbs	2639 lbs	2412 lbs	775 lbs	654 lbs	712 lbs
M	39 lbs-ft	192 lbs-ft	41 lbs-ft	28 lbs-ft	144 lbs-ft	31 lbs-ft	39 lbs-ft	192 lbs-ft	41 lbs-ft
e	0.02 ft	0.08 ft	0.02 ft	0.01 ft	0.05 ft	0.01 ft	0.05 ft	0.29 ft	0.06 ft
L/6	0.29 ft	1.59 ft	1.72 ft	1.73 ft	1.64 ft	1.72 ft	1.65 ft	1.16 ft	1.63 ft
f_{min}	268.5 sqft	201.4 sqft	260.2 sqft	270.4 sqft	244.9 sqft	263.4 sqft	73.1 sqft	-0.4 sqft	65.2 sqft
f_{max}	299.1 psf	351.8 psf	292.4 psf	292.2 psf	358.2 psf	287.9 psf	103.9 psf	149.9 psf	97.4 psf

Maximum Bearing Pressure = 358 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 21in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

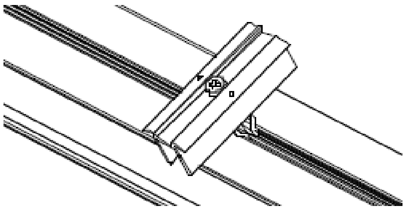
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

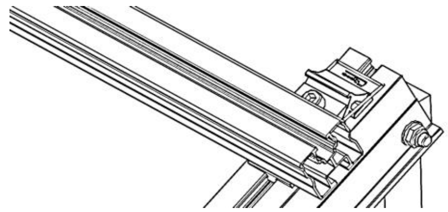
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.694	k
Allowable Uplift =	1.214	k
Utilization =	57%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	1.118	k
Allowable Uplift =	1.116	k
Utilization =	100%	



6.2 Bolted Connections

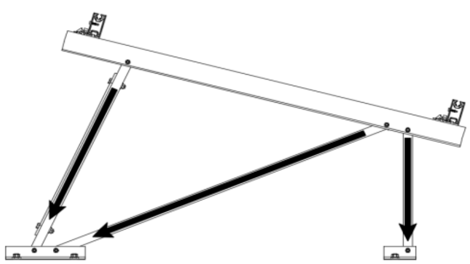
The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	0.712	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	13%	

Rear Strut		
Maximum Axial Load =	1.138	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	20%	

Diagonal Strut		
Maximum Axial Load =	0.766	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	13%	

Bracing		
Maximum Axial Load =	0.188	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	2%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

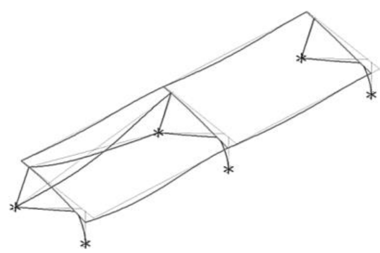
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	33.11	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	0.662	in
Max Drift, Δ_{MAX} =	0.062	in

$0.062 \leq 0.662$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus**

Strong Axis:

3.4.14

L_b = 54.00 in

J = 0.255

140.613

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.5 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 54.00 in

J = 0.255

146.018

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 30

Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 29.5 ksi

Ix = 250988 mm^4

0.603 in^4

y = 30 mm

Sx = 0.511 in^3

$M_{max}St$ = 1.256 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 20

Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi

Iy = 120291 mm^4

0.289 in^4

x = 20 mm

Sy = 0.367 in^3

$M_{max}Wk$ = 0.871 k-ft

Compression

3.4.9

b/t = 7.4

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 23.9

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.47 ksi

A = 578.06 mm^2

0.90 in^2

P_{max} = 25.51 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.22

22.2924

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.6 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.22

24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b}Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.6 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7

F_{UT}= (φbk2*√(BpE))/(5.1b/t)

F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

F_{ST}= φb[Bp-1.6Dp*b/t]

F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = 1.17φyFcy

φF_L = 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 29.6 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

$M_{max}St$ = 1.453 k-ft

$\varphi F_L Wk$= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

$M_{max}Wk$ = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.8

b/t = 24.46
S1 = 3.83
S2 = 10.30
φF_L = (φck2*√(BpE))/(5.1b/t)
φF_L = 10.4 ksi

3.4.9

b/t = 4.29
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φyFcy
φF_L = 33.3 ksi

b/t = 24.46
S1 = 12.21
S2 = 32.70
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 28.2 ksi

3.4.9.1

b/t = 24.46
t = 2.6
ds = 6.05
rs = 3.49
S = 21.70
ρst = 0.22
F_{UT} = 10.43
F_{ST} = 28.24
φF_L = Fut + (Fst - Fut)ρst < Fst
φF_L = 14.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 14.29 ksi
A = 576.21 mm^2
0.89 in^2
P_{max} = 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in
J = 0.16
47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0
φF_L= 1.17φyFcy
φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LSt= 31.2 ksi
Ix = 39958.2 mm^4
0.096 in^4
y = 15 mm
Sx = 0.163 in^3
M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in
J = 0.16
47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LWk= 31.2 ksi
Iy = 39958.2 mm^4
0.096 in^4
x = 15 mm
Sy = 0.163 in^3
M_{max}Wk = 0.423 k-ft

Compression

3.4.7

$\lambda =$ 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.83792

$\varphi F_L = \varphi cc(Bc - Dc^*\lambda)$

$\varphi F_L =$ 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 24.52 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.404 k-ft

Weak Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.85841

φF_L= (φccFcy)/(λ²)

φF_L= 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 7.60 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 42.32 in

J = 0.16

111.025

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.0 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.0 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.406 k-ft

Weak Axis:

3.4.14

L_b = 42.32 in

J = 0.16

111.025

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.0

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.81475

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83406

φF_L = (φccFcy)/(λ²)

φF_L = 8.86409 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L = φyFcy

φF_L = 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 8.86 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 4.45 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-40.249	-40.249	0	0
2	M16	Y	-40.249	-40.249	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-102.983	-102.983	0	0
2	M16	y	-171.639	-171.639	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	205.967	205.967	0	0
2	M16	y	102.983	102.983	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65..	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	268.073	2	299.305	2	0	10	0	10	0	1	0	1
2		min	-314.832	3	-450.581	3	-2.39	4	0	3	0	1	0	1
3	N7	max	.025	3	269.686	1	-.03	10	0	10	0	1	0	1
4		min	-.139	2	21.901	15	-18.584	4	-.029	4	0	1	0	1
5	N15	max	.16	3	712.406	1	.229	9	0	1	0	1	0	1
6		min	-1.369	2	21.912	15	-18.927	5	-.03	4	0	1	0	1
7	N16	max	883.149	2	958.785	2	0	2	0	9	0	1	0	1
8		min	-964.835	3	-1437.566	3	-151.766	4	0	3	0	1	0	1
9	N23	max	.026	3	269.782	1	1.138	1	.002	1	0	1	0	1
10		min	-.139	2	2.326	15	-17.576	5	-.027	5	0	1	0	1
11	N24	max	268.074	2	301.919	2	88.329	3	0	4	0	1	0	1
12		min	-315.402	3	-449.61	3	-3.551	5	0	3	0	1	0	1
13	Totals:	max	1417.65	2	2631.596	2	0	9						
14		min	-1594.858	3	-2157.577	3	-212.113	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	201.668	2	.677	6	1.195	4	0	10	0	10	0	1
2			min	-371.708	3	.158	15	-.056	3	0	4	0	4	0	1
3		2	max	201.803	2	.619	6	1.071	4	0	10	0	5	0	15
4			min	-371.606	3	.145	15	-.056	3	0	4	0	1	0	6
5		3	max	201.938	2	.562	6	.948	4	0	10	0	5	0	15
6			min	-371.505	3	.131	15	-.056	3	0	4	0	3	0	6
7		4	max	202.073	2	.504	6	.825	4	0	10	0	5	0	15
8			min	-371.404	3	.118	15	-.056	3	0	4	0	3	0	6
9		5	max	202.208	2	.447	6	.702	4	0	10	0	4	0	15
10			min	-371.303	3	.104	15	-.056	3	0	4	0	3	0	6
11		6	max	202.342	2	.389	6	.579	4	0	10	0	4	0	15
12			min	-371.202	3	.091	15	-.056	3	0	4	0	3	0	6
13		7	max	202.477	2	.332	6	.456	4	0	10	0	4	0	15
14			min	-371.101	3	.077	15	-.056	3	0	4	0	3	0	6
15		8	max	202.612	2	.274	6	.333	4	0	10	0	4	0	15
16			min	-371	3	.064	15	-.056	3	0	4	0	3	0	6
17		9	max	202.747	2	.217	6	.209	4	0	10	0	4	0	15
18			min	-370.898	3	.05	15	-.056	3	0	4	0	3	0	6
19		10	max	202.882	2	.159	6	.151	1	0	10	0	4	0	15
20			min	-370.797	3	.037	15	-.056	3	0	4	0	3	0	6
21		11	max	203.017	2	.11	2	.151	1	0	10	0	4	0	15
22			min	-370.696	3	.016	12	-.079	5	0	4	0	3	0	6
23		12	max	203.152	2	.066	2	.151	1	0	10	0	4	0	15
24			min	-370.595	3	-.014	3	-.202	5	0	4	0	3	0	6
25		13	max	203.287	2	.021	2	.151	1	0	10	0	4	0	15
26			min	-370.494	3	-.048	3	-.325	5	0	4	0	3	0	6
27		14	max	203.421	2	-.017	15	.151	1	0	10	0	4	0	15
28			min	-370.393	3	-.081	3	-.449	5	0	4	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	203.556	2	-.031	15	.151	1	0	10	0	4	0	15
30			min	-370.292	3	-.128	4	-.572	5	0	4	0	3	0	6
31		16	max	203.691	2	-.044	15	.151	1	0	10	0	4	0	15
32			min	-370.19	3	-.186	4	-.695	5	0	4	0	3	0	6
33		17	max	203.826	2	-.058	15	.151	1	0	10	0	4	0	15
34			min	-370.089	3	-.243	4	-.818	5	0	4	0	3	0	6
35		18	max	203.961	2	-.071	15	.151	1	0	10	0	1	0	15
36			min	-369.988	3	-.301	4	-.941	5	0	4	0	3	0	6
37		19	max	204.096	2	-.085	15	.151	1	0	10	0	1	0	15
38			min	-369.887	3	-.358	4	-1.064	5	0	4	0	3	0	6
39	M3	1	max	229.694	2	1.734	6	-.008	10	0	5	0	1	0	6
40			min	-221.587	3	.407	15	-1.33	4	0	1	0	10	0	15
41		2	max	229.624	2	1.558	6	-.008	10	0	5	0	1	0	2
42			min	-221.64	3	.366	15	-1.197	4	0	1	0	10	0	3
43		3	max	229.554	2	1.381	6	-.008	10	0	5	0	1	0	2
44			min	-221.692	3	.324	15	-1.063	4	0	1	0	5	0	3
45		4	max	229.484	2	1.205	6	-.008	10	0	5	0	1	0	15
46			min	-221.745	3	.283	15	-.929	4	0	1	0	5	0	4
47		5	max	229.414	2	1.029	6	-.008	10	0	5	0	1	0	15
48			min	-221.797	3	.241	15	-.796	4	0	1	0	5	0	4
49		6	max	229.344	2	.852	6	-.008	10	0	5	0	1	0	15
50			min	-221.85	3	.2	15	-.662	4	0	1	0	5	0	4
51		7	max	229.274	2	.676	6	-.008	10	0	5	0	1	0	15
52			min	-221.902	3	.158	15	-.528	4	0	1	0	5	0	4
53		8	max	229.204	2	.499	6	-.008	10	0	5	0	1	0	15
54			min	-221.955	3	.117	15	-.395	4	0	1	0	5	-.001	4
55		9	max	229.134	2	.323	6	-.008	10	0	5	0	1	0	15
56			min	-222.007	3	.075	15	-.261	4	0	1	0	5	-.001	4
57		10	max	229.064	2	.147	6	-.008	10	0	5	0	1	0	15
58			min	-222.06	3	.034	15	-.185	1	0	1	0	5	-.001	4
59		11	max	228.994	2	.006	2	.052	5	0	5	0	1	0	15
60			min	-222.112	3	-.054	3	-.185	1	0	1	0	5	-.001	4
61		12	max	228.924	2	-.049	15	.185	5	0	5	0	1	0	15
62			min	-222.165	3	-.206	4	-.185	1	0	1	0	5	-.001	4
63		13	max	228.854	2	-.091	15	.319	5	0	5	0	1	0	15
64			min	-222.217	3	-.382	4	-.185	1	0	1	0	5	-.001	4
65		14	max	228.784	2	-.132	15	.453	5	0	5	0	1	0	15
66			min	-222.27	3	-.559	4	-.185	1	0	1	0	5	-.001	4
67		15	max	228.714	2	-.173	15	.586	5	0	5	0	1	0	15
68			min	-222.322	3	-.735	4	-.185	1	0	1	0	5	0	4
69		16	max	228.644	2	-.215	15	.72	5	0	5	0	1	0	15
70			min	-222.375	3	-.912	4	-.185	1	0	1	0	5	0	4
71		17	max	228.574	2	-.256	15	.854	5	0	5	0	10	0	15
72			min	-222.427	3	-1.088	4	-.185	1	0	1	0	4	0	4
73		18	max	228.504	2	-.298	15	.987	5	0	5	0	10	0	15
74			min	-222.48	3	-1.264	4	-.185	1	0	1	0	4	0	4
75		19	max	228.434	2	-.339	15	1.121	5	0	5	0	5	0	1
76			min	-222.532	3	-1.441	4	-.185	1	0	1	0	1	0	1
77	M4	1	max	268.521	1	0	1	-.03	10	0	1	0	5	0	1
78			min	21.55	15	0	1	-17.823	4	0	1	0	2	0	1
79		2	max	268.586	1	0	1	-.03	10	0	1	0	10	0	1
80			min	21.569	15	0	1	-17.88	4	0	1	-.002	4	0	1
81		3	max	268.65	1	0	1	-.03	10	0	1	0	10	0	1
82			min	21.589	15	0	1	-17.936	4	0	1	-.003	4	0	1
83		4	max	268.715	1	0	1	-.03	10	0	1	0	10	0	1
84			min	21.608	15	0	1	-17.992	4	0	1	-.005	4	0	1
85		5	max	268.78	1	0	1	-.03	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	21.628	15	0	1	-18.048	4	0	1	-.006	4	0	1
87		6	max	268.844	1	0	1	-.03	10	0	1	0	10	0	1
88			min	21.647	15	0	1	-18.104	4	0	1	-.008	4	0	1
89		7	max	268.909	1	0	1	-.03	10	0	1	0	10	0	1
90			min	21.667	15	0	1	-18.16	4	0	1	-.01	4	0	1
91		8	max	268.974	1	0	1	-.03	10	0	1	0	10	0	1
92			min	21.687	15	0	1	-18.216	4	0	1	-.011	4	0	1
93		9	max	269.039	1	0	1	-.03	10	0	1	0	10	0	1
94			min	21.706	15	0	1	-18.272	4	0	1	-.013	4	0	1
95		10	max	269.103	1	0	1	-.03	10	0	1	0	10	0	1
96			min	21.726	15	0	1	-18.328	4	0	1	-.015	4	0	1
97		11	max	269.168	1	0	1	-.03	10	0	1	0	10	0	1
98			min	21.745	15	0	1	-18.384	4	0	1	-.016	4	0	1
99		12	max	269.233	1	0	1	-.03	10	0	1	0	10	0	1
100			min	21.765	15	0	1	-18.44	4	0	1	-.018	4	0	1
101		13	max	269.297	1	0	1	-.03	10	0	1	0	10	0	1
102			min	21.784	15	0	1	-18.496	4	0	1	-.019	4	0	1
103		14	max	269.362	1	0	1	-.03	10	0	1	0	10	0	1
104			min	21.804	15	0	1	-18.552	4	0	1	-.021	4	0	1
105		15	max	269.427	1	0	1	-.03	10	0	1	0	10	0	1
106			min	21.823	15	0	1	-18.609	4	0	1	-.023	4	0	1
107		16	max	269.492	1	0	1	-.03	10	0	1	0	10	0	1
108			min	21.843	15	0	1	-18.665	4	0	1	-.024	4	0	1
109		17	max	269.556	1	0	1	-.03	10	0	1	0	10	0	1
110			min	21.862	15	0	1	-18.721	4	0	1	-.026	4	0	1
111		18	max	269.621	1	0	1	-.03	10	0	1	0	10	0	1
112			min	21.882	15	0	1	-18.777	4	0	1	-.028	4	0	1
113		19	max	269.686	1	0	1	-.03	10	0	1	0	10	0	1
114			min	21.901	15	0	1	-18.833	4	0	1	-.029	4	0	1
115	M6	1	max	637.602	2	.66	6	1.118	4	0	3	0	3	0	1
116			min	-1137.862	3	.146	15	-.25	3	0	5	0	2	0	1
117		2	max	637.737	2	.603	6	.994	4	0	3	0	3	0	15
118			min	-1137.761	3	.132	15	-.25	3	0	5	0	2	0	6
119		3	max	637.872	2	.545	6	.871	4	0	3	0	4	0	15
120			min	-1137.66	3	.119	15	-.25	3	0	5	0	2	0	6
121		4	max	638.007	2	.491	2	.748	4	0	3	0	4	0	15
122			min	-1137.559	3	.105	15	-.25	3	0	5	0	2	0	6
123		5	max	638.142	2	.446	2	.625	4	0	3	0	4	0	15
124			min	-1137.458	3	.092	15	-.25	3	0	5	0	2	0	6
125		6	max	638.276	2	.401	2	.502	4	0	3	0	4	0	15
126			min	-1137.356	3	.077	12	-.25	3	0	5	0	2	0	6
127		7	max	638.411	2	.357	2	.379	4	0	3	0	4	0	15
128			min	-1137.255	3	.054	12	-.25	3	0	5	0	2	0	2
129		8	max	638.546	2	.312	2	.255	4	0	3	.001	4	0	15
130			min	-1137.154	3	.032	12	-.25	3	0	5	0	3	0	2
131		9	max	638.681	2	.267	2	.132	4	0	3	.001	4	0	15
132			min	-1137.053	3	.002	3	-.25	3	0	5	0	3	0	2
133		10	max	638.816	2	.222	2	.03	9	0	3	.001	4	0	15
134			min	-1136.952	3	-.032	3	-.25	3	0	5	0	3	0	2
135		11	max	638.951	2	.177	2	.03	9	0	3	.001	4	0	12
136			min	-1136.851	3	-.065	3	-.25	3	0	5	0	3	0	2
137		12	max	639.086	2	.133	2	.03	9	0	3	.001	4	0	12
138			min	-1136.75	3	-.099	3	-.25	3	0	5	0	3	0	2
139		13	max	639.22	2	.088	2	.03	9	0	3	0	4	0	12
140			min	-1136.648	3	-.133	3	-.373	5	0	5	0	3	0	2
141		14	max	639.355	2	.043	2	.03	9	0	3	0	4	0	12
142			min	-1136.547	3	-.166	3	-.496	5	0	5	0	3	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	639.49	2	-.002	2	.03	9	0	3	0	4	0	12
144			min	-1136.446	3	-.2	3	-.619	5	0	5	0	3	0	2
145		16	max	639.625	2	-.047	2	.03	9	0	3	0	4	0	3
146			min	-1136.345	3	-.233	3	-.742	5	0	5	0	3	0	2
147		17	max	639.76	2	-.07	15	.03	9	0	3	0	4	0	3
148			min	-1136.244	3	-.267	3	-.866	5	0	5	0	3	0	2
149		18	max	639.895	2	-.084	15	.03	9	0	3	0	4	0	3
150			min	-1136.143	3	-.318	4	-.989	5	0	5	0	3	0	2
151		19	max	640.03	2	-.097	15	.03	9	0	3	0	14	0	3
152			min	-1136.042	3	-.375	4	-1.112	5	0	5	0	3	0	2
153	M7	1	max	766.468	2	1.757	4	.048	3	0	1	0	4	0	2
154			min	-654.73	3	.421	15	-1.298	4	0	3	0	3	0	3
155		2	max	766.398	2	1.581	4	.048	3	0	1	0	4	0	2
156			min	-654.783	3	.38	15	-1.164	4	0	3	0	3	0	3
157		3	max	766.328	2	1.405	4	.048	3	0	1	0	1	0	2
158			min	-654.835	3	.338	15	-1.03	4	0	3	0	3	0	3
159		4	max	766.258	2	1.228	4	.048	3	0	1	0	1	0	2
160			min	-654.888	3	.297	15	-.897	4	0	3	0	3	0	3
161		5	max	766.188	2	1.052	4	.048	3	0	1	0	1	0	15
162			min	-654.94	3	.255	15	-.763	4	0	3	0	5	0	3
163		6	max	766.118	2	.875	4	.048	3	0	1	0	1	0	15
164			min	-654.993	3	.214	15	-.629	4	0	3	0	5	0	3
165		7	max	766.048	2	.699	4	.048	3	0	1	0	1	0	15
166			min	-655.045	3	.172	15	-.496	4	0	3	0	5	0	6
167		8	max	765.978	2	.523	4	.048	3	0	1	0	1	0	15
168			min	-655.098	3	.128	12	-.362	4	0	3	0	5	-.001	6
169		9	max	765.908	2	.346	4	.048	3	0	1	0	1	0	15
170			min	-655.15	3	.059	12	-.228	4	0	3	0	5	-.001	6
171		10	max	765.838	2	.205	2	.048	3	0	1	0	1	0	15
172			min	-655.203	3	-.026	3	-.095	4	0	3	-.001	5	-.001	6
173		11	max	765.768	2	.067	2	.048	3	0	1	0	1	0	15
174			min	-655.255	3	-.129	3	-.011	1	0	3	-.001	5	-.001	6
175		12	max	765.698	2	-.035	15	.173	5	0	1	0	1	0	15
176			min	-655.308	3	-.232	3	-.011	1	0	3	0	5	-.001	6
177		13	max	765.628	2	-.076	15	.307	5	0	1	0	1	0	15
178			min	-655.36	3	-.36	6	-.011	1	0	3	0	5	-.001	6
179		14	max	765.558	2	-.118	15	.44	5	0	1	0	1	0	15
180			min	-655.413	3	-.536	6	-.011	1	0	3	0	5	-.001	6
181		15	max	765.488	2	-.159	15	.574	5	0	1	0	1	0	15
182			min	-655.465	3	-.713	6	-.011	1	0	3	0	5	0	6
183		16	max	765.418	2	-.201	15	.708	5	0	1	0	1	0	15
184			min	-655.518	3	-.889	6	-.011	1	0	3	0	5	0	6
185		17	max	765.348	2	-.242	15	.841	5	0	1	0	1	0	15
186			min	-655.57	3	-1.065	6	-.011	1	0	3	0	5	0	6
187		18	max	765.278	2	-.284	15	.975	5	0	1	0	1	0	15
188			min	-655.623	3	-1.242	6	-.011	1	0	3	0	3	0	6
189		19	max	765.208	2	-.325	15	1.109	5	0	1	0	1	0	1
190			min	-655.675	3	-1.418	6	-.011	1	0	3	0	3	0	1
191	M8	1	max	711.241	1	0	1	.243	1	0	1	0	4	0	1
192			min	21.561	15	0	1	-18.053	4	0	1	0	3	0	1
193		2	max	711.306	1	0	1	.243	1	0	1	0	1	0	1
194			min	21.58	15	0	1	-18.109	4	0	1	-.002	4	0	1
195		3	max	711.371	1	0	1	.243	1	0	1	0	1	0	1
196			min	21.6	15	0	1	-18.165	4	0	1	-.003	4	0	1
197		4	max	711.435	1	0	1	.243	1	0	1	0	1	0	1
198			min	21.619	15	0	1	-18.221	4	0	1	-.005	4	0	1
199		5	max	711.5	1	0	1	.243	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	21.639	15	0	1	-18.278	4	0	1	-.006	4	0	1
201		6	max	711.565	1	0	1	.243	1	0	1	0	1	0	1
202			min	21.658	15	0	1	-18.334	4	0	1	-.008	4	0	1
203		7	max	711.629	1	0	1	.243	1	0	1	0	1	0	1
204			min	21.678	15	0	1	-18.39	4	0	1	-.01	4	0	1
205		8	max	711.694	1	0	1	.243	1	0	1	0	1	0	1
206			min	21.697	15	0	1	-18.446	4	0	1	-.011	4	0	1
207		9	max	711.759	1	0	1	.243	1	0	1	0	1	0	1
208			min	21.717	15	0	1	-18.502	4	0	1	-.013	4	0	1
209		10	max	711.823	1	0	1	.243	1	0	1	0	1	0	1
210			min	21.737	15	0	1	-18.558	4	0	1	-.015	4	0	1
211		11	max	711.888	1	0	1	.243	1	0	1	0	1	0	1
212			min	21.756	15	0	1	-18.614	4	0	1	-.016	4	0	1
213		12	max	711.953	1	0	1	.243	1	0	1	0	1	0	1
214			min	21.776	15	0	1	-18.67	4	0	1	-.018	4	0	1
215		13	max	712.018	1	0	1	.243	1	0	1	0	1	0	1
216			min	21.795	15	0	1	-18.726	4	0	1	-.02	4	0	1
217		14	max	712.082	1	0	1	.243	1	0	1	0	1	0	1
218			min	21.815	15	0	1	-18.782	4	0	1	-.021	4	0	1
219		15	max	712.147	1	0	1	.243	1	0	1	0	1	0	1
220			min	21.834	15	0	1	-18.838	4	0	1	-.023	4	0	1
221		16	max	712.212	1	0	1	.243	1	0	1	0	1	0	1
222			min	21.854	15	0	1	-18.894	4	0	1	-.025	4	0	1
223		17	max	712.276	1	0	1	.243	1	0	1	0	1	0	1
224			min	21.873	15	0	1	-18.95	4	0	1	-.026	4	0	1
225		18	max	712.341	1	0	1	.243	1	0	1	0	1	0	1
226			min	21.893	15	0	1	-19.007	4	0	1	-.028	4	0	1
227		19	max	712.406	1	0	1	.243	1	0	1	0	1	0	1
228			min	21.912	15	0	1	-19.063	4	0	1	-.03	4	0	1
229	M10	1	max	203.023	2	.711	4	1.238	5	0	1	0	1	0	1
230			min	-302.046	3	.181	15	-.116	1	-.001	5	0	3	0	1
231		2	max	203.158	2	.653	4	1.115	5	0	1	0	1	0	15
232			min	-301.944	3	.168	15	-.116	1	-.001	5	0	3	0	4
233		3	max	203.292	2	.596	4	.992	5	0	1	0	4	0	15
234			min	-301.843	3	.154	15	-.116	1	-.001	5	0	3	0	4
235		4	max	203.427	2	.538	4	.869	5	0	1	0	4	0	15
236			min	-301.742	3	.141	15	-.116	1	-.001	5	0	3	0	4
237		5	max	203.562	2	.481	4	.746	5	0	1	0	4	0	15
238			min	-301.641	3	.127	15	-.116	1	-.001	5	0	3	0	4
239		6	max	203.697	2	.423	4	.622	5	0	1	0	4	0	15
240			min	-301.54	3	.114	15	-.116	1	-.001	5	0	3	0	4
241		7	max	203.832	2	.366	4	.499	5	0	1	0	4	0	15
242			min	-301.439	3	.1	15	-.116	1	-.001	5	0	3	0	4
243		8	max	203.967	2	.308	4	.376	5	0	1	0	4	0	15
244			min	-301.338	3	.087	15	-.116	1	-.001	5	0	3	0	4
245		9	max	204.102	2	.251	4	.253	5	0	1	.001	4	0	15
246			min	-301.236	3	.07	12	-.116	1	-.001	5	0	3	0	4
247		10	max	204.236	2	.193	4	.13	5	0	1	.001	4	0	15
248			min	-301.135	3	.048	12	-.116	1	-.001	5	0	3	0	4
249		11	max	204.371	2	.136	4	.007	5	0	1	.001	4	0	15
250			min	-301.034	3	.025	12	-.116	1	-.001	5	0	3	0	4
251		12	max	204.506	2	.078	4	.006	3	0	1	.001	5	0	15
252			min	-300.933	3	.002	3	-.135	4	-.001	5	0	3	0	4
253		13	max	204.641	2	.028	5	.006	3	0	1	.001	5	0	15
254			min	-300.832	3	-.032	3	-.258	4	-.001	5	0	3	0	4
255		14	max	204.776	2	.007	5	.006	3	0	1	0	5	0	15
256			min	-300.731	3	-.065	3	-.381	4	-.001	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	204.911	2	-.008	15	.006	3	0	1	0	5	0	15
258			min	-300.63	3	-.099	3	-.505	4	-.001	5	0	3	0	4
259		16	max	205.046	2	-.021	15	.006	3	0	1	0	5	0	15
260			min	-300.528	3	-.153	6	-.628	4	-.001	5	0	3	0	4
261		17	max	205.181	2	-.035	15	.006	3	0	1	0	5	0	12
262			min	-300.427	3	-.21	6	-.751	4	-.001	5	0	3	0	4
263		18	max	205.315	2	-.049	15	.006	3	0	1	0	5	0	12
264			min	-300.326	3	-.268	6	-.874	4	-.001	5	0	3	0	4
265		19	max	205.45	2	-.062	15	.006	3	0	1	0	5	0	12
266			min	-300.225	3	-.325	6	-.997	4	-.001	5	0	1	0	4
267	M11	1	max	229.216	2	1.72	6	.195	1	0	4	0	5	0	2
268			min	-222.4	3	.397	15	-1.256	5	0	10	0	1	0	15
269		2	max	229.146	2	1.544	6	.195	1	0	4	0	3	0	2
270			min	-222.452	3	.356	15	-1.123	5	0	10	0	1	0	3
271		3	max	229.076	2	1.368	6	.195	1	0	4	0	3	0	2
272			min	-222.505	3	.314	15	-.989	5	0	10	0	1	0	3
273		4	max	229.006	2	1.191	6	.195	1	0	4	0	3	0	15
274			min	-222.557	3	.273	15	-.855	5	0	10	0	1	0	4
275		5	max	228.936	2	1.015	6	.195	1	0	4	0	3	0	15
276			min	-222.61	3	.232	15	-.722	5	0	10	0	1	0	4
277		6	max	228.866	2	.839	6	.195	1	0	4	0	3	0	15
278			min	-222.662	3	.19	15	-.588	5	0	10	0	4	0	4
279		7	max	228.796	2	.662	6	.195	1	0	4	0	3	0	15
280			min	-222.715	3	.149	15	-.454	5	0	10	0	4	-.001	4
281		8	max	228.726	2	.486	6	.195	1	0	4	0	3	0	15
282			min	-222.767	3	.107	15	-.321	5	0	10	0	4	-.001	4
283		9	max	228.656	2	.309	6	.195	1	0	4	0	3	0	15
284			min	-222.82	3	.066	15	-.187	5	0	10	0	4	-.001	4
285		10	max	228.586	2	.143	2	.195	1	0	4	0	3	0	15
286			min	-222.872	3	.024	15	-.062	3	0	10	0	4	-.001	4
287		11	max	228.516	2	.006	2	.195	1	0	4	0	3	0	15
288			min	-222.925	3	-.062	3	-.062	3	0	10	0	4	-.001	4
289		12	max	228.446	2	-.059	15	.262	4	0	4	0	3	0	15
290			min	-222.977	3	-.22	4	-.062	3	0	10	0	4	-.001	4
291		13	max	228.376	2	-.1	15	.396	4	0	4	0	3	0	15
292			min	-223.03	3	-.397	4	-.062	3	0	10	0	4	-.001	4
293		14	max	228.306	2	-.142	15	.529	4	0	4	0	3	0	15
294			min	-223.082	3	-.573	4	-.062	3	0	10	0	4	-.001	4
295		15	max	228.236	2	-.183	15	.663	4	0	4	0	3	0	15
296			min	-223.135	3	-.749	4	-.062	3	0	10	0	4	0	4
297		16	max	228.166	2	-.225	15	.797	4	0	4	0	3	0	15
298			min	-223.187	3	-.926	4	-.062	3	0	10	0	5	0	4
299		17	max	228.096	2	-.266	15	.93	4	0	4	0	3	0	15
300			min	-223.24	3	-1.102	4	-.062	3	0	10	0	10	0	4
301		18	max	228.026	2	-.307	15	1.064	4	0	4	0	3	0	15
302			min	-223.292	3	-1.279	4	-.062	3	0	10	0	10	0	4
303		19	max	227.956	2	-.349	15	1.198	4	0	4	0	4	0	1
304			min	-223.345	3	-1.455	4	-.062	3	0	10	0	10	0	1
305	M12	1	max	268.617	1	0	1	1.191	1	0	1	0	4	0	1
306			min	1.975	15	0	1	-16.577	5	0	1	0	3	0	1
307		2	max	268.682	1	0	1	1.191	1	0	1	0	1	0	1
308			min	1.994	15	0	1	-16.633	5	0	1	-.001	5	0	1
309		3	max	268.747	1	0	1	1.191	1	0	1	0	1	0	1
310			min	2.014	15	0	1	-16.689	5	0	1	-.003	5	0	1
311		4	max	268.811	1	0	1	1.191	1	0	1	0	1	0	1
312			min	2.033	15	0	1	-16.745	5	0	1	-.004	5	0	1
313		5	max	268.876	1	0	1	1.191	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	2.053	15	0	1	-16.801	5	0	1	-.006	5	0	1
315		6	max	268.941	1	0	1	1.191	1	0	1	0	1	0	1
316			min	2.072	15	0	1	-16.857	5	0	1	-.007	5	0	1
317		7	max	269.005	1	0	1	1.191	1	0	1	0	1	0	1
318			min	2.092	15	0	1	-16.913	5	0	1	-.009	5	0	1
319		8	max	269.07	1	0	1	1.191	1	0	1	0	1	0	1
320			min	2.111	15	0	1	-16.969	5	0	1	-.01	5	0	1
321		9	max	269.135	1	0	1	1.191	1	0	1	0	1	0	1
322			min	2.131	15	0	1	-17.025	5	0	1	-.012	5	0	1
323		10	max	269.199	1	0	1	1.191	1	0	1	0	1	0	1
324			min	2.15	15	0	1	-17.082	5	0	1	-.014	5	0	1
325		11	max	269.264	1	0	1	1.191	1	0	1	.001	1	0	1
326			min	2.17	15	0	1	-17.138	5	0	1	-.015	5	0	1
327		12	max	269.329	1	0	1	1.191	1	0	1	.001	1	0	1
328			min	2.189	15	0	1	-17.194	5	0	1	-.017	5	0	1
329		13	max	269.394	1	0	1	1.191	1	0	1	.001	1	0	1
330			min	2.209	15	0	1	-17.25	5	0	1	-.018	5	0	1
331		14	max	269.458	1	0	1	1.191	1	0	1	.001	1	0	1
332			min	2.228	15	0	1	-17.306	5	0	1	-.02	5	0	1
333		15	max	269.523	1	0	1	1.191	1	0	1	.002	1	0	1
334			min	2.248	15	0	1	-17.362	5	0	1	-.021	5	0	1
335		16	max	269.588	1	0	1	1.191	1	0	1	.002	1	0	1
336			min	2.267	15	0	1	-17.418	5	0	1	-.023	5	0	1
337		17	max	269.652	1	0	1	1.191	1	0	1	.002	1	0	1
338			min	2.287	15	0	1	-17.474	5	0	1	-.024	5	0	1
339		18	max	269.717	1	0	1	1.191	1	0	1	.002	1	0	1
340			min	2.306	15	0	1	-17.53	5	0	1	-.026	5	0	1
341		19	max	269.782	1	0	1	1.191	1	0	1	.002	1	0	1
342			min	2.326	15	0	1	-17.586	5	0	1	-.027	5	0	1
343	M1	1	max	89.33	1	347.778	3	-1.048	10	0	2	.05	1	0	2
344			min	7.484	12	-223.307	2	-25.6	1	0	3	.002	10	0	3
345		2	max	89.491	1	347.606	3	-1.048	10	0	2	.045	1	.049	2
346			min	7.564	12	-223.536	2	-25.6	1	0	3	.002	10	-.076	3
347		3	max	118.652	3	4.877	14	-1.041	10	0	10	.039	1	.096	2
348			min	-22.824	2	-30.264	2	-25.531	1	0	1	.002	10	-.15	3
349		4	max	118.772	3	4.652	14	-1.041	10	0	10	.033	1	.103	2
350			min	-22.664	2	-30.492	2	-25.531	1	0	1	.001	10	-.148	3
351		5	max	118.892	3	4.427	14	-1.041	10	0	10	.028	1	.11	2
352			min	-22.504	2	-30.721	2	-25.531	1	0	1	.001	10	-.146	3
353		6	max	119.012	3	4.202	14	-1.041	10	0	10	.022	1	.116	2
354			min	-22.344	2	-30.95	2	-25.531	1	0	1	0	10	-.144	3
355		7	max	119.132	3	3.978	14	-1.041	10	0	10	.017	1	.123	2
356			min	-22.184	2	-31.179	2	-25.531	1	0	1	0	10	-.142	3
357		8	max	119.253	3	3.753	14	-1.041	10	0	10	.011	1	.13	2
358			min	-22.024	2	-31.407	2	-25.531	1	0	1	0	10	-.14	3
359		9	max	119.373	3	3.528	14	-1.041	10	0	10	.006	1	.137	2
360			min	-21.863	2	-31.636	2	-25.531	1	0	1	0	10	-.138	3
361		10	max	119.493	3	3.304	14	-1.041	10	0	10	.002	3	.144	2
362			min	-21.703	2	-31.865	2	-25.531	1	0	1	0	10	-.136	3
363		11	max	119.613	3	3.079	14	-1.041	10	0	10	0	3	.151	2
364			min	-21.543	2	-32.093	2	-25.531	1	0	1	-.005	1	-.133	3
365		12	max	119.733	3	2.878	9	-1.041	10	0	10	0	12	.158	2
366			min	-21.383	2	-32.322	2	-25.531	1	0	1	-.011	1	-.131	3
367		13	max	119.853	3	2.687	9	-1.041	10	0	10	0	10	.165	2
368			min	-21.223	2	-32.551	2	-25.531	1	0	1	-.017	1	-.129	3
369		14	max	119.973	3	2.497	9	-1.041	10	0	10	0	10	.172	2
370			min	-21.063	2	-32.78	2	-25.531	1	0	1	-.022	1	-.127	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	120.093	3	2.306	9	-1.041	10	0	10	-.001	10	.179	2
372			min	-20.902	2	-33.008	2	-25.531	1	0	1	-.028	1	-.124	3
373		16	max	87.457	2	168.271	2	-1.048	10	0	1	-.001	10	.184	2
374			min	2.524	15	-207.844	3	-25.69	1	0	5	-.033	1	-.12	3
375		17	max	87.617	2	168.042	2	-1.048	10	0	1	-.002	10	.148	2
376			min	2.572	15	-208.015	3	-25.69	1	0	5	-.039	1	-.075	3
377		18	max	-5.315	12	341.393	2	-1.079	10	0	3	-.002	10	.074	2
378			min	-89.49	1	-172.559	3	-31.441	4	0	2	-.045	1	-.038	3
379		19	max	-5.235	12	341.164	2	-1.079	10	0	3	-.002	10	0	2
380			min	-89.33	1	-172.73	3	-31.199	4	0	2	-.05	1	0	3
381	M5	1	max	212.478	1	1121.689	3	0	2	0	9	.031	4	0	3
382			min	2.63	12	-713.397	2	-79.243	3	0	5	0	10	0	2
383		2	max	212.638	1	1121.518	3	0	2	0	9	.027	4	.154	2
384			min	2.71	12	-713.626	2	-79.243	3	0	5	-.006	3	-.243	3
385		3	max	348.664	3	4.63	9	8.736	3	0	3	.022	4	.307	2
386			min	-86.918	2	-103.072	2	-17.411	4	0	4	-.023	3	-.481	3
387		4	max	348.785	3	4.439	9	8.736	3	0	3	.019	4	.329	2
388			min	-86.758	2	-103.3	2	-17.169	4	0	4	-.021	3	-.473	3
389		5	max	348.905	3	4.248	9	8.736	3	0	3	.015	4	.351	2
390			min	-86.598	2	-103.529	2	-16.927	4	0	4	-.019	3	-.465	3
391		6	max	349.025	3	4.058	9	8.736	3	0	3	.011	4	.374	2
392			min	-86.437	2	-103.758	2	-16.685	4	0	4	-.017	3	-.457	3
393		7	max	349.145	3	3.867	9	8.736	3	0	3	.008	4	.396	2
394			min	-86.277	2	-103.987	2	-16.443	4	0	4	-.015	3	-.449	3
395		8	max	349.265	3	3.676	9	8.736	3	0	3	.004	4	.419	2
396			min	-86.117	2	-104.215	2	-16.201	4	0	4	-.013	3	-.441	3
397		9	max	349.385	3	3.486	9	8.736	3	0	3	0	4	.442	2
398			min	-85.957	2	-104.444	2	-15.959	4	0	4	-.011	3	-.433	3
399		10	max	349.505	3	3.295	9	8.736	3	0	3	0	2	.464	2
400			min	-85.797	2	-104.673	2	-15.717	4	0	4	-.009	3	-.425	3
401		11	max	349.625	3	3.105	9	8.736	3	0	3	0	2	.487	2
402			min	-85.637	2	-104.902	2	-15.475	4	0	4	-.008	3	-.417	3
403		12	max	349.746	3	2.914	9	8.736	3	0	3	0	2	.51	2
404			min	-85.476	2	-105.13	2	-15.233	4	0	4	-.009	4	-.408	3
405		13	max	349.866	3	2.723	9	8.736	3	0	3	0	2	.533	2
406			min	-85.316	2	-105.359	2	-14.991	4	0	4	-.013	4	-.4	3
407		14	max	349.986	3	2.533	9	8.736	3	0	3	0	2	.556	2
408			min	-85.156	2	-105.588	2	-14.749	4	0	4	-.016	4	-.392	3
409		15	max	350.106	3	2.342	9	8.736	3	0	3	0	3	.578	2
410			min	-84.996	2	-105.816	2	-14.507	4	0	4	-.019	4	-.384	3
411		16	max	274.967	2	572.54	2	8.717	3	0	3	.001	3	.595	2
412			min	.908	15	-618.402	3	-13.164	4	0	4	-.022	4	-.37	3
413		17	max	275.127	2	572.311	2	8.717	3	0	3	.003	3	.471	2
414			min	.956	15	-618.573	3	-12.922	4	0	4	-.025	4	-.236	3
415		18	max	-6.004	12	1092.919	2	7.975	3	0	4	.005	3	.236	2
416			min	-212.639	1	-544.402	3	-30.339	5	0	1	-.032	4	-.118	3
417		19	max	-5.924	12	1092.69	2	7.975	3	0	4	.007	3	0	3
418			min	-212.479	1	-544.574	3	-30.097	5	0	1	-.038	4	0	2
419	M9	1	max	89.128	1	347.687	3	128.982	4	0	3	0	15	0	2
420			min	2.147	15	-223.307	2	1.048	10	0	2	-.05	1	0	3
421		2	max	89.288	1	347.516	3	129.224	4	0	3	.025	5	.049	2
422			min	2.196	15	-223.536	2	1.048	10	0	2	-.044	1	-.076	3
423		3	max	118.238	3	4.58	9	25.112	1	0	1	.05	5	.096	2
424			min	-22.326	2	-30.232	2	-22.062	5	0	5	-.038	1	-.149	3
425		4	max	118.358	3	4.39	9	25.112	1	0	1	.045	5	.103	2
426			min	-22.166	2	-30.461	2	-21.82	5	0	5	-.033	1	-.148	3
427		5	max	118.478	3	4.199	9	25.112	1	0	1	.041	5	.11	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-22.006	2	-30.689	2	-21.578	5	0	5	-.027	1	-.146	3
429		6	max	118.598	3	4.008	9	25.112	1	0	1	.036	5	.116	2
430			min	-21.846	2	-30.918	2	-21.336	5	0	5	-.022	1	-.144	3
431		7	max	118.718	3	3.818	9	25.112	1	0	1	.031	5	.123	2
432			min	-21.685	2	-31.147	2	-21.094	5	0	5	-.016	1	-.142	3
433		8	max	118.838	3	3.627	9	25.112	1	0	1	.027	5	.13	2
434			min	-21.525	2	-31.375	2	-20.852	5	0	5	-.011	1	-.14	3
435		9	max	118.959	3	3.436	9	25.112	1	0	1	.022	5	.137	2
436			min	-21.365	2	-31.604	2	-20.61	5	0	5	-.005	1	-.138	3
437		10	max	119.079	3	3.246	9	25.112	1	0	1	.018	4	.144	2
438			min	-21.205	2	-31.833	2	-20.368	5	0	5	0	1	-.136	3
439		11	max	119.199	3	3.055	9	25.112	1	0	1	.015	4	.151	2
440			min	-21.045	2	-32.062	2	-20.126	5	0	5	0	10	-.133	3
441		12	max	119.319	3	2.865	9	25.112	1	0	1	.012	4	.157	2
442			min	-20.885	2	-32.29	2	-19.884	5	0	5	0	10	-.131	3
443		13	max	119.439	3	2.674	9	25.112	1	0	1	.016	1	.165	2
444			min	-20.724	2	-32.519	2	-19.642	5	0	5	0	10	-.129	3
445		14	max	119.559	3	2.483	9	25.112	1	0	1	.022	1	.172	2
446			min	-20.564	2	-32.748	2	-19.4	5	0	5	0	15	-.127	3
447		15	max	119.679	3	2.293	9	25.112	1	0	1	.027	1	.179	2
448			min	-20.404	2	-32.977	2	-19.158	5	0	5	-.004	5	-.125	3
449		16	max	87.73	2	167.881	2	25.277	1	0	10	.033	1	.184	2
450			min	4.346	15	-208.45	3	-17.766	5	0	4	-.007	5	-.12	3
451		17	max	87.89	2	167.652	2	25.277	1	0	10	.038	1	.148	2
452			min	4.395	15	-208.621	3	-17.524	5	0	4	-.011	5	-.075	3
453		18	max	4.671	5	341.393	2	26.489	1	0	2	.044	1	.074	2
454			min	-89.287	1	-172.547	3	-33.845	5	0	3	-.018	5	-.038	3
455		19	max	4.745	5	341.164	2	26.489	1	0	2	.05	1	0	2
456			min	-89.127	1	-172.719	3	-33.603	5	0	3	-.025	5	0	3
457	M13	1	max	128.983	4	223.198	2	-2.147	15	0	2	.05	1	0	2
458			min	1.048	10	-347.737	3	-89.121	1	0	3	0	15	0	3
459		2	max	124.072	4	158.823	2	-1.167	15	0	2	.015	3	.149	3
460			min	1.048	10	-246.791	3	-67.402	1	0	3	-.002	10	-.095	2
461		3	max	119.161	4	94.447	2	-.186	15	0	2	.011	3	.247	3
462			min	1.048	10	-145.845	3	-45.684	1	0	3	-.018	1	-.159	2
463		4	max	114.25	4	30.072	2	1.114	5	0	2	.007	3	.294	3
464			min	1.048	10	-44.899	3	-23.965	1	0	3	-.035	1	-.19	2
465		5	max	109.34	4	56.047	3	2.631	5	0	2	.004	3	.292	3
466			min	1.048	10	-34.304	2	-5.328	3	0	3	-.042	1	-.189	2
467		6	max	104.429	4	156.993	3	19.473	1	0	2	.002	5	.238	3
468			min	1.048	10	-98.679	2	-3.901	3	0	3	-.037	1	-.156	2
469		7	max	99.518	4	257.939	3	41.191	1	0	2	.005	5	.135	3
470			min	1.048	10	-163.055	2	-2.475	3	0	3	-.022	1	-.09	2
471		8	max	94.607	4	358.885	3	62.91	1	0	2	.008	4	.008	1
472			min	1.048	10	-227.43	2	-1.048	3	0	3	0	3	-.02	3
473		9	max	89.696	4	459.831	3	84.629	1	0	2	.041	1	.137	2
474			min	1.048	10	-291.805	2	.379	3	0	3	-.001	3	-.224	3
475		10	max	84.785	4	560.777	3	106.347	1	0	2	.089	1	.299	2
476			min	1.048	10	-356.181	2	1.542	12	0	3	-.011	3	-.479	3
477		11	max	59.53	4	291.805	2	3.221	5	0	3	.041	1	.137	2
478			min	1.048	10	-459.831	3	-84.426	1	0	2	-.013	5	-.224	3
479		12	max	54.619	4	227.43	2	4.738	5	0	3	.006	2	.008	1
480			min	1.048	10	-358.885	3	-62.707	1	0	2	-.011	3	-.02	3
481		13	max	49.708	4	163.055	2	6.255	5	0	3	0	10	.135	3
482			min	1.048	10	-257.939	3	-40.988	1	0	2	-.022	1	-.09	2
483		14	max	44.797	4	98.679	2	7.771	5	0	3	-.003	15	.238	3
484			min	1.048	10	-156.993	3	-19.27	1	0	2	-.037	1	-.156	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	39.886	4	34.304	2	10.36	4	0	3	0	15	.292	3
486			min	1.048	10	-56.047	3	-2.013	2	0	2	-.041	1	-.189	2
487		16	max	34.976	4	44.899	3	24.168	1	0	3	.005	5	.294	3
488			min	1.048	10	-30.072	2	.979	10	0	2	-.035	1	-.19	2
489		17	max	30.065	4	145.845	3	45.887	1	0	3	.01	5	.247	3
490			min	1.048	10	-94.447	2	3.688	10	0	2	-.017	1	-.159	2
491		18	max	25.654	1	246.791	3	67.605	1	0	3	.02	4	.149	3
492			min	1.048	10	-158.823	2	6.396	10	0	2	-.002	10	-.095	2
493		19	max	25.654	1	347.737	3	89.324	1	0	3	.05	1	0	2
494			min	1.048	10	-223.198	2	7.485	12	0	2	.002	10	0	3
495	M16	1	max	33.595	5	341.306	2	4.745	5	0	3	.05	1	0	2
496			min	-26.433	1	-172.752	3	-89.134	1	0	2	-.025	5	0	3
497		2	max	28.685	5	242.602	2	6.262	5	0	3	.011	1	.074	3
498			min	-26.433	1	-123.298	3	-67.415	1	0	2	-.022	5	-.146	2
499		3	max	23.774	5	143.899	2	7.779	5	0	3	0	3	.123	3
500			min	-26.433	1	-73.844	3	-45.697	1	0	2	-.023	4	-.243	2
501		4	max	18.863	5	45.195	2	9.295	5	0	3	-.002	12	.148	3
502			min	-26.433	1	-24.39	3	-23.978	1	0	2	-.035	1	-.29	2
503		5	max	13.952	5	25.063	3	10.812	5	0	3	-.003	12	.148	3
504			min	-26.433	1	-53.508	2	-3.568	3	0	2	-.042	1	-.288	2
505		6	max	9.041	5	74.517	3	19.459	1	0	3	-.003	15	.123	3
506			min	-26.433	1	-152.212	2	-2.141	3	0	2	-.037	1	-.236	2
507		7	max	4.13	5	123.971	3	41.178	1	0	3	.003	5	.073	3
508			min	-26.433	1	-250.915	2	-.714	3	0	2	-.022	1	-.136	2
509		8	max	2.023	3	173.425	3	62.897	1	0	3	.01	4	.015	2
510			min	-26.433	1	-349.619	2	.696	12	0	2	-.007	3	-.001	3
511		9	max	2.023	3	222.879	3	84.615	1	0	3	.041	1	.214	2
512			min	-26.433	1	-448.322	2	1.647	12	0	2	-.006	3	-.1	3
513		10	max	19.507	5	-7.752	15	106.334	1	0	14	.089	1	.463	2
514			min	-26.433	1	-547.026	2	-4.788	3	0	2	-.005	3	-.224	3
515		11	max	14.596	5	448.322	2	2.523	5	0	2	.041	1	.214	2
516			min	-26.369	1	-222.879	3	-84.413	1	0	3	-.01	5	-.1	3
517		12	max	9.685	5	349.619	2	4.04	5	0	2	.006	2	.015	2
518			min	-26.369	1	-173.425	3	-62.694	1	0	3	-.008	5	-.001	3
519		13	max	4.774	5	250.915	2	5.556	5	0	2	0	10	.073	3
520			min	-26.369	1	-123.971	3	-40.975	1	0	3	-.022	1	-.136	2
521		14	max	-.044	15	152.212	2	7.073	5	0	2	-.001	12	.123	3
522			min	-26.369	1	-74.517	3	-19.257	1	0	3	-.037	1	-.236	2
523		15	max	-1.079	10	53.508	2	9.64	4	0	2	.001	5	.148	3
524			min	-26.369	1	-25.063	3	-1.975	2	0	3	-.041	1	-.288	2
525		16	max	-1.079	10	24.391	3	24.181	1	0	2	.006	5	.148	3
526			min	-26.369	1	-45.195	2	1	10	0	3	-.035	1	-.29	2
527		17	max	-1.079	10	73.844	3	45.899	1	0	2	.011	5	.123	3
528			min	-26.369	1	-143.899	2	3.331	12	0	3	-.017	1	-.243	2
529		18	max	-1.079	10	123.298	3	67.618	1	0	2	.021	4	.074	3
530			min	-26.369	1	-242.602	2	4.283	12	0	3	-.002	10	-.146	2
531		19	max	-1.079	10	172.752	3	89.337	1	0	2	.05	1	0	2
532			min	-31.228	4	-341.306	2	5.234	12	0	3	.002	10	0	3
533	M15	1	max	0	1	.939	3	.114	3	0	1	0	1	0	1
534			min	-111.709	3	0	1	0	1	0	3	0	3	0	1
535		2	max	0	1	.834	3	.114	3	0	1	0	1	0	1
536			min	-111.785	3	0	1	0	1	0	3	0	3	0	3
537		3	max	0	1	.73	3	.114	3	0	1	0	1	0	1
538			min	-111.86	3	0	1	0	1	0	3	0	3	0	3
539		4	max	0	1	.626	3	.114	3	0	1	0	1	0	1
540			min	-111.936	3	0	1	0	1	0	3	0	3	0	3
541		5	max	0	1	.522	3	.114	3	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-112.011	3	0	1	0	1	0	3	0	3	0	3
543		6	max	0	1	.417	3	.114	3	0	1	0	1	0	1
544			min	-112.087	3	0	1	0	1	0	3	0	3	-.001	3
545		7	max	0	1	.313	3	.114	3	0	1	0	3	0	1
546			min	-112.162	3	0	1	0	1	0	3	0	1	-.001	3
547		8	max	0	1	.209	3	.114	3	0	1	0	3	0	1
548			min	-112.238	3	0	1	0	1	0	3	0	1	-.001	3
549		9	max	0	1	.104	3	.114	3	0	1	0	3	0	1
550			min	-112.314	3	0	1	0	1	0	3	0	1	-.001	3
551		10	max	0	1	0	1	.114	3	0	1	0	3	0	1
552			min	-112.389	3	0	1	0	1	0	3	0	1	-.001	3
553		11	max	0	1	0	1	.114	3	0	1	0	3	0	1
554			min	-112.465	3	-.104	3	0	1	0	3	0	1	-.001	3
555		12	max	0	1	0	1	.114	3	0	1	0	3	0	1
556			min	-112.54	3	-.209	3	0	1	0	3	0	1	-.001	3
557		13	max	0	1	0	1	.114	3	0	1	0	3	0	1
558			min	-112.616	3	-.313	3	0	1	0	3	0	1	-.001	3
559		14	max	0	1	0	1	.114	3	0	1	0	3	0	1
560			min	-112.691	3	-.417	3	0	1	0	3	0	1	-.001	3
561		15	max	0	1	0	1	.114	3	0	1	0	3	0	1
562			min	-112.767	3	-.522	3	0	1	0	3	0	1	0	3
563		16	max	0	1	0	1	.114	3	0	1	0	3	0	1
564			min	-112.842	3	-.626	3	0	1	0	3	0	1	0	3
565		17	max	0	1	0	1	.114	3	0	1	0	3	0	1
566			min	-112.918	3	-.73	3	0	1	0	3	0	1	0	3
567		18	max	0	1	0	1	.114	3	0	1	0	3	0	1
568			min	-112.993	3	-.834	3	0	1	0	3	0	1	0	3
569		19	max	0	1	0	1	.114	3	0	1	0	3	0	1
570			min	-113.069	3	-.939	3	0	1	0	3	0	1	0	1
571	M16A	1	max	0	2	2.369	4	.35	4	0	3	0	3	0	1
572			min	-188.402	4	0	2	-.047	3	0	1	0	4	0	1
573		2	max	0	2	2.106	4	.315	4	0	3	0	3	0	2
574			min	-188.39	4	0	2	-.047	3	0	1	0	4	0	4
575		3	max	0	2	1.842	4	.279	4	0	3	0	3	0	2
576			min	-188.377	4	0	2	-.047	3	0	1	0	4	-.001	4
577		4	max	0	2	1.579	4	.243	4	0	3	0	3	0	2
578			min	-188.365	4	0	2	-.047	3	0	1	0	1	-.002	4
579		5	max	0	2	1.316	4	.207	4	0	3	0	3	0	2
580			min	-188.353	4	0	2	-.047	3	0	1	0	1	-.002	4
581		6	max	0	2	1.053	4	.171	4	0	3	0	3	0	2
582			min	-188.341	4	0	2	-.047	3	0	1	0	1	-.003	4
583		7	max	0	2	.79	4	.136	4	0	3	0	5	0	2
584			min	-188.328	4	0	2	-.047	3	0	1	0	1	-.003	4
585		8	max	0	2	.526	4	.1	4	0	3	0	5	0	2
586			min	-188.316	4	0	2	-.047	3	0	1	0	1	-.003	4
587		9	max	0	2	.263	4	.064	4	0	3	0	5	0	2
588			min	-188.304	4	0	2	-.047	3	0	1	0	1	-.003	4
589		10	max	0	2	0	1	.032	1	0	3	0	5	0	2
590			min	-188.292	4	0	1	-.047	3	0	1	0	1	-.003	4
591		11	max	0	2	0	2	.032	1	0	3	0	5	0	2
592			min	-188.28	4	-.263	4	-.047	3	0	1	0	1	-.003	4
593		12	max	0	2	0	2	.032	1	0	3	0	5	0	2
594			min	-188.267	4	-.526	4	-.047	3	0	1	0	1	-.003	4
595		13	max	0	2	0	2	.032	1	0	3	0	5	0	2
596			min	-188.255	4	-.79	4	-.082	5	0	1	0	3	-.003	4
597		14	max	.078	11	0	2	.032	1	0	3	0	5	0	2
598			min	-188.243	4	-1.053	4	-.118	5	0	1	0	3	-.003	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.162	11	0	2	.032	1	0	3	0	5	0	2
600			min	-188.231	4	-1.316	4	-.153	5	0	1	0	3	-.002	4
601		16	max	.246	11	0	2	.032	1	0	3	0	1	0	2
602			min	-188.218	4	-1.579	4	-.189	5	0	1	0	3	-.002	4
603		17	max	.33	11	0	2	.032	1	0	3	0	1	0	2
604			min	-188.206	4	-1.842	4	-.225	5	0	1	0	3	-.001	4
605		18	max	.413	11	0	2	.032	1	0	3	0	1	0	2
606			min	-188.194	4	-2.106	4	-.261	5	0	1	0	5	0	4
607		19	max	.497	11	0	2	.032	1	0	3	0	1	0	1
608			min	-188.201	5	-2.369	4	-.296	5	0	1	0	5	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	2	.011	2	.004	1	1.035e-3	5	NC	3	NC	2
2			min	-.004	3	-.011	3	-.011	5	-4.193e-4	1	3918.474	2	9529.987	1
3		2	max	.002	2	.01	2	.004	1	1.057e-3	5	NC	3	NC	1
4			min	-.004	3	-.011	3	-.011	5	-4.004e-4	1	4285.139	2	NC	1
5		3	max	.002	2	.009	2	.004	1	1.078e-3	5	NC	3	NC	1
6			min	-.003	3	-.01	3	-.011	5	-3.815e-4	1	4722.761	2	NC	1
7		4	max	.002	2	.008	2	.004	1	1.1e-3	5	NC	1	NC	1
8			min	-.003	3	-.01	3	-.011	5	-3.625e-4	1	5248.652	2	NC	1
9		5	max	.002	2	.007	2	.003	1	1.121e-3	5	NC	1	NC	1
10			min	-.003	3	-.009	3	-.01	5	-3.436e-4	1	5885.93	2	NC	1
11		6	max	.002	2	.006	2	.003	1	1.143e-3	5	NC	1	NC	1
12			min	-.003	3	-.009	3	-.01	5	-3.247e-4	1	6665.97	2	NC	1
13		7	max	.001	2	.006	2	.003	1	1.164e-3	5	NC	1	NC	1
14			min	-.003	3	-.008	3	-.01	5	-3.057e-4	1	7632.156	2	NC	1
15		8	max	.001	2	.005	2	.002	1	1.186e-3	5	NC	1	NC	1
16			min	-.002	3	-.008	3	-.009	5	-2.868e-4	1	8845.8	2	NC	1
17		9	max	.001	2	.004	2	.002	1	1.207e-3	5	NC	1	NC	1
18			min	-.002	3	-.007	3	-.009	5	-2.678e-4	1	NC	1	NC	1
19		10	max	.001	2	.003	2	.002	1	1.228e-3	5	NC	1	NC	1
20			min	-.002	3	-.007	3	-.008	5	-2.489e-4	1	NC	1	NC	1
21		11	max	0	2	.003	2	.001	1	1.25e-3	5	NC	1	NC	1
22			min	-.002	3	-.006	3	-.008	5	-2.3e-4	1	NC	1	NC	1
23		12	max	0	2	.002	2	.001	1	1.271e-3	5	NC	1	NC	1
24			min	-.002	3	-.005	3	-.007	5	-2.11e-4	1	NC	1	NC	1
25		13	max	0	2	.002	2	0	1	1.293e-3	5	NC	1	NC	1
26			min	-.001	3	-.005	3	-.006	5	-1.921e-4	1	NC	1	NC	1
27		14	max	0	2	.001	2	0	1	1.314e-3	5	NC	1	NC	1
28			min	-.001	3	-.004	3	-.005	5	-1.732e-4	1	NC	1	NC	1
29		15	max	0	2	0	2	0	1	1.336e-3	5	NC	1	NC	1
30			min	0	3	-.003	3	-.004	5	-1.542e-4	1	NC	1	NC	1
31		16	max	0	2	0	2	0	1	1.357e-3	5	NC	1	NC	1
32			min	0	3	-.002	3	-.003	5	-1.353e-4	1	NC	1	NC	1
33		17	max	0	2	0	2	0	1	1.379e-3	5	NC	1	NC	1
34			min	0	3	-.002	3	-.002	5	-1.164e-4	1	NC	1	NC	1
35		18	max	0	2	0	2	0	1	1.4e-3	5	NC	1	NC	1
36			min	0	3	0	3	-.001	5	-9.743e-5	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	1.422e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-7.849e-5	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	3.764e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-6.798e-4	5	NC	1	NC	1
41		2	max	0	3	0	2	.003	5	4.741e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	1	-6.86e-4	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	3	0	2	.007	5	5.719e-5	1	NC	1	NC	1
44			min	0	2	-.002	3	0	1	-6.923e-4	5	NC	1	NC	1
45		4	max	0	3	0	2	.01	5	6.697e-5	1	NC	1	NC	1
46			min	0	2	-.003	3	0	1	-6.986e-4	5	NC	1	NC	1
47		5	max	0	3	0	2	.014	5	7.674e-5	1	NC	1	NC	1
48			min	0	2	-.004	3	0	1	-7.049e-4	5	NC	1	NC	1
49		6	max	0	3	0	2	.017	4	8.652e-5	1	NC	1	NC	1
50			min	0	2	-.005	3	0	9	-7.111e-4	5	NC	1	NC	1
51		7	max	0	3	0	2	.02	4	9.63e-5	1	NC	1	NC	1
52			min	0	2	-.005	3	0	9	-7.174e-4	5	NC	1	NC	1
53		8	max	0	3	.001	2	.024	4	1.061e-4	1	NC	1	NC	1
54			min	-.001	2	-.006	3	0	9	-7.237e-4	5	NC	1	NC	1
55		9	max	.001	3	.001	2	.027	4	1.159e-4	1	NC	1	NC	1
56			min	-.001	2	-.007	3	0	9	-7.299e-4	5	NC	1	NC	1
57		10	max	.001	3	.002	2	.03	4	1.256e-4	1	NC	1	NC	1
58			min	-.001	2	-.007	3	0	10	-7.362e-4	5	NC	1	NC	1
59		11	max	.001	3	.002	2	.033	4	1.354e-4	1	NC	1	NC	1
60			min	-.001	2	-.008	3	0	10	-7.425e-4	5	NC	1	NC	1
61		12	max	.002	3	.003	2	.036	4	1.452e-4	1	NC	1	NC	1
62			min	-.002	2	-.008	3	0	10	-7.487e-4	5	NC	1	NC	1
63		13	max	.002	3	.004	2	.039	4	1.55e-4	1	NC	1	NC	1
64			min	-.002	2	-.008	3	0	10	-7.55e-4	5	NC	1	NC	1
65		14	max	.002	3	.005	2	.042	4	1.647e-4	1	NC	1	NC	1
66			min	-.002	2	-.009	3	0	10	-7.613e-4	5	NC	1	NC	1
67		15	max	.002	3	.005	2	.044	4	1.745e-4	1	NC	1	NC	1
68			min	-.002	2	-.009	3	0	10	-7.675e-4	5	8441.435	2	NC	1
69		16	max	.002	3	.006	2	.047	4	1.843e-4	1	NC	1	NC	1
70			min	-.002	2	-.009	3	0	10	-7.738e-4	5	7173.344	2	NC	1
71		17	max	.002	3	.007	2	.049	4	1.941e-4	1	NC	1	NC	1
72			min	-.002	2	-.009	3	0	10	-7.801e-4	5	6188.35	2	NC	1
73		18	max	.002	3	.009	2	.052	4	2.038e-4	1	NC	1	NC	1
74			min	-.002	2	-.009	3	0	10	-7.863e-4	5	5414.852	2	NC	1
75		19	max	.003	3	.01	2	.054	4	2.136e-4	1	NC	3	NC	1
76			min	-.003	2	-.009	3	0	10	-7.926e-4	5	4802.213	2	NC	1
77	M4	1	max	.001	1	.013	2	0	10	4.34e-3	5	NC	1	NC	2
78			min	0	15	-.011	3	-.057	4	-3.195e-4	1	NC	1	336.573	4
79		2	max	.001	1	.012	2	0	10	4.34e-3	5	NC	1	NC	2
80			min	0	15	-.011	3	-.053	4	-3.195e-4	1	NC	1	366.877	4
81		3	max	.001	1	.011	2	0	10	4.34e-3	5	NC	1	NC	1
82			min	0	15	-.01	3	-.048	4	-3.195e-4	1	NC	1	402.941	4
83		4	max	.001	1	.01	2	0	10	4.34e-3	5	NC	1	NC	1
84			min	0	15	-.009	3	-.043	4	-3.195e-4	1	NC	1	446.283	4
85		5	max	0	1	.01	2	0	10	4.34e-3	5	NC	1	NC	1
86			min	0	15	-.009	3	-.039	4	-3.195e-4	1	NC	1	498.969	4
87		6	max	0	1	.009	2	0	10	4.34e-3	5	NC	1	NC	1
88			min	0	15	-.008	3	-.034	4	-3.195e-4	1	NC	1	563.873	4
89		7	max	0	1	.008	2	0	10	4.34e-3	5	NC	1	NC	1
90			min	0	15	-.007	3	-.03	4	-3.195e-4	1	NC	1	645.089	4
91		8	max	0	1	.008	2	0	10	4.34e-3	5	NC	1	NC	1
92			min	0	15	-.007	3	-.026	4	-3.195e-4	1	NC	1	748.608	4
93		9	max	0	1	.007	2	0	10	4.34e-3	5	NC	1	NC	1
94			min	0	15	-.006	3	-.022	4	-3.195e-4	1	NC	1	883.496	4
95		10	max	0	1	.006	2	0	10	4.34e-3	5	NC	1	NC	1
96			min	0	15	-.006	3	-.018	4	-3.195e-4	1	NC	1	1063.998	4
97		11	max	0	1	.006	2	0	10	4.34e-3	5	NC	1	NC	1
98			min	0	15	-.005	3	-.015	4	-3.195e-4	1	NC	1	1313.579	4
99		12	max	0	1	.005	2	0	10	4.34e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	15	-.004	3	-.012	4	-3.195e-4	1	NC	1	1673.165	4
101		13	max	0	1	.004	2	0	10	4.34e-3	5	NC	1	NC	1
102			min	0	15	-.004	3	-.009	4	-3.195e-4	1	NC	1	2219.522	4
103		14	max	0	1	.003	2	0	10	4.34e-3	5	NC	1	NC	1
104			min	0	15	-.003	3	-.006	4	-3.195e-4	1	NC	1	3110.984	4
105		15	max	0	1	.003	2	0	10	4.34e-3	5	NC	1	NC	1
106			min	0	15	-.002	3	-.004	4	-3.195e-4	1	NC	1	4719.516	4
107		16	max	0	1	.002	2	0	10	4.34e-3	5	NC	1	NC	1
108			min	0	15	-.002	3	-.002	4	-3.195e-4	1	NC	1	8102.488	4
109		17	max	0	1	.001	2	0	10	4.34e-3	5	NC	1	NC	1
110			min	0	15	-.001	3	-.001	4	-3.195e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	10	4.34e-3	5	NC	1	NC	1
112			min	0	15	0	3	0	4	-3.195e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	4.34e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-3.195e-4	1	NC	1	NC	1
115	M6	1	max	.007	2	.036	2	.001	9	1.107e-3	4	NC	3	NC	1
116			min	-.012	3	-.034	3	-.011	5	-2.057e-7	1	1194.202	2	6282.727	3
117		2	max	.006	2	.033	2	.001	9	1.128e-3	4	NC	3	NC	1
118			min	-.011	3	-.033	3	-.011	5	-2.185e-6	1	1279.162	2	6640.973	3
119		3	max	.006	2	.031	2	.001	9	1.15e-3	4	NC	3	NC	1
120			min	-.011	3	-.031	3	-.011	5	-4.165e-6	1	1376.682	2	7070.571	3
121		4	max	.006	2	.029	2	.001	9	1.171e-3	4	NC	3	NC	1
122			min	-.01	3	-.029	3	-.011	5	-6.145e-6	1	1489.273	2	7586.143	3
123		5	max	.005	2	.026	2	.001	9	1.192e-3	4	NC	3	NC	1
124			min	-.009	3	-.027	3	-.011	5	-8.124e-6	1	1620.167	2	8207.203	3
125		6	max	.005	2	.024	2	0	9	1.214e-3	4	NC	3	NC	1
126			min	-.009	3	-.025	3	-.01	5	-1.01e-5	1	1773.597	2	8960.102	3
127		7	max	.004	2	.022	2	0	9	1.235e-3	4	NC	3	NC	1
128			min	-.008	3	-.023	3	-.01	5	-1.208e-5	1	1955.206	2	9881.01	3
129		8	max	.004	2	.02	2	0	9	1.257e-3	4	NC	3	NC	1
130			min	-.007	3	-.022	3	-.01	5	-1.406e-5	1	2172.69	2	NC	1
131		9	max	.004	2	.017	2	0	1	1.278e-3	4	NC	3	NC	1
132			min	-.007	3	-.02	3	-.009	5	-1.604e-5	1	2436.821	2	NC	1
133		10	max	.003	2	.015	2	0	1	1.3e-3	4	NC	3	NC	1
134			min	-.006	3	-.018	3	-.009	5	-1.802e-5	1	2763.146	2	NC	1
135		11	max	.003	2	.013	2	0	1	1.321e-3	4	NC	3	NC	1
136			min	-.005	3	-.016	3	-.008	5	-2.e-5	1	3174.974	2	NC	1
137		12	max	.003	2	.011	2	0	1	1.343e-3	4	NC	3	NC	1
138			min	-.005	3	-.014	3	-.007	5	-2.198e-5	1	3708.909	2	NC	1
139		13	max	.002	2	.01	2	0	1	1.364e-3	4	NC	3	NC	1
140			min	-.004	3	-.012	3	-.006	5	-2.396e-5	1	4425.916	2	NC	1
141		14	max	.002	2	.008	2	0	1	1.386e-3	4	NC	1	NC	1
142			min	-.003	3	-.01	3	-.005	5	-2.594e-5	1	5435.677	2	NC	1
143		15	max	.001	2	.006	2	0	1	1.407e-3	4	NC	1	NC	1
144			min	-.003	3	-.008	3	-.004	5	-2.792e-5	1	6957.464	2	NC	1
145		16	max	.001	2	.004	2	0	1	1.429e-3	4	NC	1	NC	1
146			min	-.002	3	-.006	3	-.003	5	-2.99e-5	1	9502.76	2	NC	1
147		17	max	0	2	.003	2	0	1	1.45e-3	4	NC	1	NC	1
148			min	-.001	3	-.004	3	-.002	5	-3.188e-5	1	NC	1	NC	1
149		18	max	0	2	.001	2	0	1	1.472e-3	5	NC	1	NC	1
150			min	0	3	-.002	3	-.001	5	-3.386e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.494e-3	5	NC	1	NC	1
152			min	0	1	0	1	0	1	-3.584e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	1.707e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-7.141e-4	5	NC	1	NC	1
155		2	max	0	3	.001	2	.004	5	1.511e-5	1	NC	1	NC	1
156			min	0	2	-.002	3	0	1	-7.095e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	3	.003	2	.007	5	1.316e-5	1	NC	1	NC	1
158			min	0	2	-.004	3	0	1	-7.052e-4	4	NC	1	NC	1
159		4	max	.001	3	.004	2	.011	5	1.12e-5	1	NC	1	NC	1
160			min	-.001	2	-.006	3	0	1	-7.009e-4	4	NC	1	NC	1
161		5	max	.002	3	.006	2	.014	5	9.24e-6	1	NC	1	NC	1
162			min	-.002	2	-.008	3	0	1	-6.966e-4	4	8129.703	2	NC	1
163		6	max	.002	3	.007	2	.018	5	2.906e-5	3	NC	1	NC	1
164			min	-.002	2	-.01	3	0	1	-6.923e-4	4	6506.65	2	NC	1
165		7	max	.002	3	.009	2	.021	4	5.537e-5	3	NC	1	NC	1
166			min	-.003	2	-.012	3	0	1	-6.881e-4	4	5399.098	2	NC	1
167		8	max	.003	3	.01	2	.025	4	8.168e-5	3	NC	3	NC	1
168			min	-.003	2	-.014	3	0	1	-6.838e-4	4	4589.053	2	NC	1
169		9	max	.003	3	.012	2	.028	4	1.08e-4	3	NC	3	NC	1
170			min	-.004	2	-.016	3	0	1	-6.795e-4	4	3967.812	2	NC	1
171		10	max	.004	3	.013	2	.031	4	1.343e-4	3	NC	3	NC	1
172			min	-.004	2	-.017	3	0	1	-6.752e-4	4	3475.07	2	NC	1
173		11	max	.004	3	.015	2	.034	4	1.606e-4	3	NC	3	NC	1
174			min	-.005	2	-.019	3	0	1	-6.709e-4	4	3074.595	2	NC	1
175		12	max	.005	3	.017	2	.037	4	1.869e-4	3	NC	3	NC	1
176			min	-.005	2	-.02	3	0	1	-6.667e-4	4	2743.195	2	NC	1
177		13	max	.005	3	.019	2	.04	4	2.132e-4	3	NC	3	NC	1
178			min	-.006	2	-.022	3	0	1	-6.624e-4	4	2465.238	2	NC	1
179		14	max	.005	3	.021	2	.043	4	2.396e-4	3	NC	3	NC	1
180			min	-.006	2	-.023	3	0	1	-6.581e-4	4	2229.722	2	NC	1
181		15	max	.006	3	.023	2	.045	4	2.659e-4	3	NC	3	NC	1
182			min	-.007	2	-.024	3	0	1	-6.538e-4	4	2028.617	2	NC	1
183		16	max	.006	3	.025	2	.048	4	2.922e-4	3	NC	3	NC	1
184			min	-.007	2	-.025	3	0	1	-6.495e-4	4	1855.884	2	NC	1
185		17	max	.007	3	.027	2	.051	4	3.185e-4	3	NC	3	NC	1
186			min	-.008	2	-.026	3	0	1	-6.453e-4	4	1706.872	2	NC	1
187		18	max	.007	3	.029	2	.053	4	3.448e-4	3	NC	3	NC	1
188			min	-.008	2	-.027	3	0	1	-6.41e-4	4	1577.926	2	NC	1
189		19	max	.007	3	.031	2	.056	4	3.711e-4	3	NC	3	NC	1
190			min	-.009	2	-.028	3	0	9	-6.367e-4	4	1466.13	2	NC	1
191	M8	1	max	.003	1	.041	2	0	1	4.18e-3	4	NC	1	NC	1
192			min	0	15	-.034	3	-.058	4	-2.793e-4	3	NC	1	332.399	4
193		2	max	.003	1	.039	2	0	1	4.18e-3	4	NC	1	NC	1
194			min	0	15	-.032	3	-.053	4	-2.793e-4	3	NC	1	362.327	4
195		3	max	.003	1	.037	2	0	1	4.18e-3	4	NC	1	NC	1
196			min	0	15	-.03	3	-.049	4	-2.793e-4	3	NC	1	397.944	4
197		4	max	.003	1	.034	2	0	1	4.18e-3	4	NC	1	NC	1
198			min	0	15	-.028	3	-.044	4	-2.793e-4	3	NC	1	440.749	4
199		5	max	.003	1	.032	2	0	1	4.18e-3	4	NC	1	NC	1
200			min	0	15	-.027	3	-.039	4	-2.793e-4	3	NC	1	492.783	4
201		6	max	.002	1	.03	2	0	1	4.18e-3	4	NC	1	NC	1
202			min	0	15	-.025	3	-.035	4	-2.793e-4	3	NC	1	556.885	4
203		7	max	.002	1	.027	2	0	1	4.18e-3	4	NC	1	NC	1
204			min	0	15	-.023	3	-.03	4	-2.793e-4	3	NC	1	637.095	4
205		8	max	.002	1	.025	2	0	1	4.18e-3	4	NC	1	NC	1
206			min	0	15	-.021	3	-.026	4	-2.793e-4	3	NC	1	739.334	4
207		9	max	.002	1	.023	2	0	1	4.18e-3	4	NC	1	NC	1
208			min	0	15	-.019	3	-.022	4	-2.793e-4	3	NC	1	872.554	4
209		10	max	.002	1	.021	2	0	1	4.18e-3	4	NC	1	NC	1
210			min	0	15	-.017	3	-.018	4	-2.793e-4	3	NC	1	1050.824	4
211		11	max	.002	1	.018	2	0	1	4.18e-3	4	NC	1	NC	1
212			min	0	15	-.015	3	-.015	4	-2.793e-4	3	NC	1	1297.32	4
213		12	max	.001	1	.016	2	0	1	4.18e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	15	-.013	3	-.012	4	-2.793e-4	3	NC	1	1652.463	4
215		13	max	.001	1	.014	2	0	1	4.18e-3	4	NC	1	NC	1
216			min	0	15	-.011	3	-.009	4	-2.793e-4	3	NC	1	2192.069	4
217		14	max	0	1	.011	2	0	1	4.18e-3	4	NC	1	NC	1
218			min	0	15	-.009	3	-.006	4	-2.793e-4	3	NC	1	3072.518	4
219		15	max	0	1	.009	2	0	1	4.18e-3	4	NC	1	NC	1
220			min	0	15	-.008	3	-.004	4	-2.793e-4	3	NC	1	4661.183	4
221		16	max	0	1	.007	2	0	1	4.18e-3	4	NC	1	NC	1
222			min	0	15	-.006	3	-.002	4	-2.793e-4	3	NC	1	8002.378	4
223		17	max	0	1	.005	2	0	1	4.18e-3	4	NC	1	NC	1
224			min	0	15	-.004	3	-.001	4	-2.793e-4	3	NC	1	NC	1
225		18	max	0	1	.002	2	0	1	4.18e-3	4	NC	1	NC	1
226			min	0	15	-.002	3	0	4	-2.793e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	4.18e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-2.793e-4	3	NC	1	NC	1
229	M10	1	max	.002	2	.011	2	0	12	4.126e-4	1	NC	3	NC	1
230			min	-.003	3	-.011	3	-.006	4	-5.975e-4	3	3922.025	2	NC	1
231		2	max	.002	2	.01	2	0	3	3.917e-4	1	NC	3	NC	1
232			min	-.003	3	-.011	3	-.006	4	-5.761e-4	3	4289.148	2	NC	1
233		3	max	.002	2	.009	2	0	3	3.708e-4	1	NC	3	NC	1
234			min	-.003	3	-.01	3	-.006	4	-5.547e-4	3	4727.342	2	NC	1
235		4	max	.002	2	.008	2	0	3	3.727e-4	4	NC	1	NC	1
236			min	-.003	3	-.01	3	-.006	4	-5.333e-4	3	5253.953	2	NC	1
237		5	max	.002	2	.007	2	0	3	4.286e-4	4	NC	1	NC	1
238			min	-.002	3	-.009	3	-.006	4	-5.119e-4	3	5892.148	2	NC	1
239		6	max	.002	2	.006	2	0	3	4.845e-4	4	NC	1	NC	1
240			min	-.002	3	-.009	3	-.006	4	-4.905e-4	3	6673.37	2	NC	1
241		7	max	.001	2	.006	2	0	3	5.404e-4	4	NC	1	NC	1
242			min	-.002	3	-.008	3	-.006	4	-4.691e-4	3	7641.103	2	NC	1
243		8	max	.001	2	.005	2	0	3	5.964e-4	4	NC	1	NC	1
244			min	-.002	3	-.008	3	-.006	4	-4.477e-4	3	8856.808	2	NC	1
245		9	max	.001	2	.004	2	0	3	6.523e-4	4	NC	1	NC	1
246			min	-.002	3	-.007	3	-.006	4	-4.263e-4	3	NC	1	NC	1
247		10	max	.001	2	.003	2	0	3	7.082e-4	4	NC	1	NC	1
248			min	-.002	3	-.007	3	-.006	4	-4.049e-4	3	NC	1	NC	1
249		11	max	0	2	.003	2	0	3	7.641e-4	4	NC	1	NC	1
250			min	-.001	3	-.006	3	-.006	4	-3.835e-4	3	NC	1	NC	1
251		12	max	0	2	.002	2	0	3	8.2e-4	4	NC	1	NC	1
252			min	-.001	3	-.005	3	-.005	4	-3.621e-4	3	NC	1	NC	1
253		13	max	0	2	.002	2	0	3	8.76e-4	4	NC	1	NC	1
254			min	-.001	3	-.005	3	-.005	4	-3.407e-4	3	NC	1	NC	1
255		14	max	0	2	.001	2	0	3	9.319e-4	4	NC	1	NC	1
256			min	0	3	-.004	3	-.004	4	-3.193e-4	3	NC	1	NC	1
257		15	max	0	2	0	2	0	3	9.878e-4	4	NC	1	NC	1
258			min	0	3	-.003	3	-.003	4	-2.979e-4	3	NC	1	NC	1
259		16	max	0	2	0	2	0	3	1.044e-3	4	NC	1	NC	1
260			min	0	3	-.003	3	-.003	4	-2.766e-4	3	NC	1	NC	1
261		17	max	0	2	0	2	0	3	1.1e-3	4	NC	1	NC	1
262			min	0	3	-.002	3	-.002	4	-2.552e-4	3	NC	1	NC	1
263		18	max	0	2	0	2	0	3	1.156e-3	4	NC	1	NC	1
264			min	0	3	0	3	0	4	-2.338e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	1.211e-3	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-2.124e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	1.017e-4	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-5.797e-4	4	NC	1	NC	1
269		2	max	0	3	0	2	.003	4	7.606e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-6.3e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	3	0	2	.006	4	5.046e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-6.803e-4	4	NC	1	NC	1
273		4	max	0	3	0	2	.009	4	2.486e-5	3	NC	1	NC	1
274			min	0	2	-.003	3	-.001	3	-7.306e-4	4	NC	1	NC	1
275		5	max	0	3	0	2	.012	4	-7.485e-7	3	NC	1	NC	1
276			min	0	2	-.004	3	-.002	3	-7.809e-4	4	NC	1	NC	1
277		6	max	0	3	0	2	.015	5	-3.642e-6	10	NC	1	NC	1
278			min	0	2	-.005	3	-.002	3	-8.312e-4	4	NC	1	NC	1
279		7	max	0	3	0	2	.018	5	-4.155e-6	10	NC	1	NC	1
280			min	0	2	-.005	3	-.002	3	-8.816e-4	4	NC	1	NC	1
281		8	max	0	3	.001	2	.021	5	-4.668e-6	10	NC	1	NC	1
282			min	-.001	2	-.006	3	-.002	3	-9.319e-4	4	NC	1	NC	1
283		9	max	.001	3	.001	2	.023	5	-5.181e-6	10	NC	1	NC	1
284			min	-.001	2	-.007	3	-.003	3	-9.822e-4	4	NC	1	NC	1
285		10	max	.001	3	.002	2	.026	5	-5.694e-6	10	NC	1	NC	1
286			min	-.001	2	-.007	3	-.003	3	-1.032e-3	4	NC	1	NC	1
287		11	max	.001	3	.002	2	.029	5	-6.207e-6	10	NC	1	NC	1
288			min	-.001	2	-.008	3	-.003	3	-1.083e-3	4	NC	1	NC	1
289		12	max	.002	3	.003	2	.031	5	-6.72e-6	10	NC	1	NC	1
290			min	-.002	2	-.008	3	-.003	3	-1.133e-3	4	NC	1	NC	1
291		13	max	.002	3	.004	2	.034	5	-7.233e-6	10	NC	1	NC	1
292			min	-.002	2	-.009	3	-.003	3	-1.183e-3	4	NC	1	NC	1
293		14	max	.002	3	.005	2	.037	5	-7.745e-6	10	NC	1	NC	1
294			min	-.002	2	-.009	3	-.003	3	-1.234e-3	4	NC	1	NC	1
295		15	max	.002	3	.005	2	.039	5	-8.258e-6	10	NC	1	NC	1
296			min	-.002	2	-.009	3	-.003	1	-1.284e-3	4	8453.801	2	NC	1
297		16	max	.002	3	.006	2	.041	5	-8.771e-6	10	NC	1	NC	1
298			min	-.002	2	-.009	3	-.003	1	-1.334e-3	4	7182.902	2	NC	1
299		17	max	.002	3	.007	2	.044	5	-9.284e-6	10	NC	1	NC	1
300			min	-.002	2	-.009	3	-.004	1	-1.385e-3	4	6195.932	2	NC	1
301		18	max	.002	3	.008	2	.046	5	-9.797e-6	10	NC	1	NC	1
302			min	-.002	2	-.009	3	-.004	1	-1.435e-3	4	5421.015	2	NC	1
303		19	max	.003	3	.01	2	.049	5	-1.031e-5	10	NC	3	NC	1
304			min	-.003	2	-.009	3	-.005	1	-1.485e-3	4	4807.342	2	NC	1
305	M12	1	max	.001	1	.013	2	.004	1	4.975e-3	4	NC	1	NC	2
306			min	0	15	-.011	3	-.053	5	1.196e-5	10	NC	1	361.429	5
307		2	max	.001	1	.012	2	.003	1	4.975e-3	4	NC	1	NC	2
308			min	0	15	-.011	3	-.049	5	1.196e-5	10	NC	1	393.961	5
309		3	max	.001	1	.011	2	.003	1	4.975e-3	4	NC	1	NC	2
310			min	0	15	-.01	3	-.045	5	1.196e-5	10	NC	1	432.677	5
311		4	max	.001	1	.01	2	.003	1	4.975e-3	4	NC	1	NC	2
312			min	0	15	-.009	3	-.04	5	1.196e-5	10	NC	1	479.204	5
313		5	max	0	1	.01	2	.003	1	4.975e-3	4	NC	1	NC	2
314			min	0	15	-.009	3	-.036	5	1.196e-5	10	NC	1	535.761	5
315		6	max	0	1	.009	2	.002	1	4.975e-3	4	NC	1	NC	2
316			min	0	15	-.008	3	-.032	5	1.196e-5	10	NC	1	605.434	5
317		7	max	0	1	.008	2	.002	1	4.975e-3	4	NC	1	NC	2
318			min	0	15	-.007	3	-.028	5	1.196e-5	10	NC	1	692.613	5
319		8	max	0	1	.008	2	.002	1	4.975e-3	4	NC	1	NC	1
320			min	0	15	-.007	3	-.024	5	1.196e-5	10	NC	1	803.733	5
321		9	max	0	1	.007	2	.001	1	4.975e-3	4	NC	1	NC	1
322			min	0	15	-.006	3	-.02	5	1.196e-5	10	NC	1	948.521	5
323		10	max	0	1	.006	2	.001	1	4.975e-3	4	NC	1	NC	1
324			min	0	15	-.006	3	-.017	5	1.196e-5	10	NC	1	1142.269	5
325		11	max	0	1	.006	2	0	1	4.975e-3	4	NC	1	NC	1
326			min	0	15	-.005	3	-.014	5	1.196e-5	10	NC	1	1410.16	5
327		12	max	0	1	.005	2	0	1	4.975e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	15	-.004	3	-.011	5	1.196e-5	10	NC	1	1796.12	5
329		13	max	0	1	.004	2	0	1	4.975e-3	4	NC	1	NC	1
330			min	0	15	-.004	3	-.008	5	1.196e-5	10	NC	1	2382.538	5
331		14	max	0	1	.003	2	0	1	4.975e-3	4	NC	1	NC	1
332			min	0	15	-.003	3	-.006	5	1.196e-5	10	NC	1	3339.346	5
333		15	max	0	1	.003	2	0	1	4.975e-3	4	NC	1	NC	1
334			min	0	15	-.002	3	-.004	5	1.196e-5	10	NC	1	5065.756	5
335		16	max	0	1	.002	2	0	1	4.975e-3	4	NC	1	NC	1
336			min	0	15	-.002	3	-.002	5	1.196e-5	10	NC	1	8696.564	5
337		17	max	0	1	.001	2	0	1	4.975e-3	4	NC	1	NC	1
338			min	0	15	-.001	3	-.001	5	1.196e-5	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	4.975e-3	4	NC	1	NC	1
340			min	0	15	0	3	0	5	1.196e-5	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	4.975e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	1.196e-5	10	NC	1	NC	1
343	M1	1	max	.01	3	.027	3	.007	5	7.186e-3	2	NC	1	NC	1
344			min	-.01	2	-.023	2	-.001	9	-1.072e-2	3	NC	1	NC	1
345		2	max	.01	3	.017	3	.009	5	3.532e-3	2	NC	4	NC	1
346			min	-.01	2	-.014	2	-.003	1	-5.296e-3	3	5208.248	2	NC	1
347		3	max	.01	3	.007	3	.011	5	3.643e-4	5	NC	4	NC	1
348			min	-.01	2	-.005	2	-.004	1	-2.39e-4	1	2671.152	2	NC	1
349		4	max	.01	3	.003	2	.014	5	3.723e-4	5	NC	4	NC	1
350			min	-.01	2	-.002	3	-.005	1	-2.05e-4	1	1865.479	2	6563.959	5
351		5	max	.01	3	.009	2	.017	5	3.803e-4	5	NC	4	NC	1
352			min	-.01	2	-.009	3	-.005	1	-1.711e-4	1	1458.549	3	4662.777	5
353		6	max	.01	3	.015	2	.02	5	3.883e-4	5	NC	4	NC	1
354			min	-.01	2	-.014	3	-.005	1	-1.371e-4	1	1238.862	3	3561.443	5
355		7	max	.01	3	.019	2	.023	5	3.963e-4	5	NC	4	NC	1
356			min	-.01	2	-.019	3	-.004	1	-1.031e-4	1	1110.418	3	2853.277	5
357		8	max	.01	3	.023	2	.027	5	4.043e-4	5	NC	4	NC	1
358			min	-.01	2	-.022	3	-.003	1	-6.915e-5	1	1033.535	2	2365.627	5
359		9	max	.01	3	.025	2	.03	5	4.122e-4	5	NC	4	NC	1
360			min	-.01	2	-.024	3	-.002	1	-3.664e-5	9	985.176	2	2013.159	5
361		10	max	.009	3	.026	2	.034	5	4.202e-4	5	NC	4	NC	1
362			min	-.01	2	-.024	3	-.001	9	-1.2e-5	9	965.508	2	1730.818	4
363		11	max	.009	3	.026	2	.037	4	4.364e-4	4	NC	4	NC	1
364			min	-.01	2	-.023	3	0	9	3.388e-6	10	972.541	2	1515.689	4
365		12	max	.009	3	.024	2	.041	4	4.532e-4	4	NC	4	NC	1
366			min	-.01	2	-.021	3	0	10	4.643e-6	10	1008.859	2	1349.879	4
367		13	max	.009	3	.021	2	.045	4	4.699e-4	4	NC	4	NC	1
368			min	-.01	2	-.018	3	0	10	5.899e-6	10	1083.063	2	1219.952	4
369		14	max	.009	3	.016	2	.048	4	4.866e-4	4	NC	4	NC	1
370			min	-.01	2	-.014	3	0	10	7.154e-6	10	1214.89	2	1116.949	4
371		15	max	.009	3	.01	2	.052	4	5.034e-4	4	NC	4	NC	1
372			min	-.01	2	-.008	3	0	10	8.41e-6	10	1450.816	2	1034.73	4
373		16	max	.009	3	.002	2	.055	4	7.306e-4	4	NC	4	NC	1
374			min	-.01	2	-.002	3	0	10	9.315e-6	10	1855.89	3	968.985	4
375		17	max	.009	3	.006	3	.057	4	5.968e-3	4	NC	4	NC	1
376			min	-.01	2	-.008	2	0	10	-4.447e-5	9	2693.278	3	916.707	4
377		18	max	.009	3	.015	3	.06	4	5.354e-3	2	NC	1	NC	1
378			min	-.01	2	-.019	2	0	10	-2.852e-3	3	5281.559	3	875.567	4
379		19	max	.009	3	.023	3	.062	4	1.08e-2	2	NC	1	NC	1
380			min	-.01	2	-.031	2	0	1	-5.83e-3	3	5656.836	2	844.968	4
381	M5	1	max	.03	3	.086	3	.007	5	1.713e-5	4	NC	1	NC	1
382			min	-.032	2	-.072	2	-.002	9	4.25e-8	11	3674.07	3	NC	1
383		2	max	.03	3	.052	3	.009	5	1.813e-4	5	NC	4	NC	1
384			min	-.032	2	-.044	2	-.001	9	-2.336e-5	9	1621.013	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.03	3	.021	3	.011	5	3.428e-4	5	NC	5	NC	1
386			min	-.032	2	-.016	2	-.001	9	-4.642e-5	9	831.05	2	NC	1
387		4	max	.029	3	.008	2	.014	5	3.592e-4	5	NC	5	NC	1
388			min	-.032	2	-.006	3	-.001	9	-4.439e-5	9	580.067	2	NC	1
389		5	max	.029	3	.03	2	.017	5	3.756e-4	5	NC	5	NC	1
390			min	-.032	2	-.028	3	-.001	9	-4.237e-5	9	458.701	2	8870.913	3
391		6	max	.029	3	.048	2	.021	5	3.919e-4	5	NC	5	NC	1
392			min	-.032	2	-.046	3	-.001	9	-4.034e-5	9	389.529	2	8000.338	3
393		7	max	.029	3	.063	2	.024	5	4.083e-4	5	NC	5	NC	1
394			min	-.032	2	-.059	3	-.001	9	-3.832e-5	9	347.101	2	7595.849	3
395		8	max	.029	3	.074	2	.028	5	4.246e-4	5	NC	5	NC	1
396			min	-.032	2	-.069	3	-.001	9	-3.629e-5	9	320.815	2	7500.76	3
397		9	max	.029	3	.081	2	.032	5	4.41e-4	5	NC	5	NC	1
398			min	-.032	2	-.074	3	-.001	9	-3.427e-5	9	305.721	2	7655.493	3
399		10	max	.029	3	.084	2	.036	5	4.574e-4	5	NC	5	NC	1
400			min	-.032	2	-.076	3	-.001	9	-3.225e-5	9	299.559	2	8052.157	3
401		11	max	.029	3	.083	2	.039	5	4.737e-4	5	NC	5	NC	1
402			min	-.032	2	-.074	3	-.001	9	-3.022e-5	9	301.707	2	8723.047	3
403		12	max	.029	3	.077	2	.043	5	4.901e-4	5	NC	5	NC	1
404			min	-.032	2	-.067	3	0	9	-2.82e-5	9	312.971	2	9747.142	3
405		13	max	.029	3	.067	2	.046	5	5.064e-4	5	NC	5	NC	1
406			min	-.032	2	-.057	3	0	9	-2.617e-5	9	336.029	2	NC	1
407		14	max	.028	3	.052	2	.05	4	5.228e-4	5	NC	5	NC	1
408			min	-.032	2	-.044	3	0	9	-2.415e-5	9	377.042	2	NC	1
409		15	max	.028	3	.032	2	.053	4	5.392e-4	5	NC	5	NC	1
410			min	-.032	2	-.026	3	0	9	-2.212e-5	9	450.535	2	NC	1
411		16	max	.028	3	.006	2	.056	4	7.635e-4	5	NC	5	NC	1
412			min	-.032	2	-.006	3	0	9	-2.182e-5	9	595.279	3	NC	1
413		17	max	.028	3	.019	3	.058	4	5.953e-3	4	NC	5	NC	1
414			min	-.032	2	-.025	2	0	1	-6.327e-5	1	863.565	3	NC	1
415		18	max	.028	3	.045	3	.06	4	3.055e-3	4	NC	4	NC	1
416			min	-.032	2	-.061	2	0	1	-3.242e-5	1	1693.439	3	NC	1
417		19	max	.028	3	.073	3	.062	4	4.632e-6	5	NC	3	NC	1
418			min	-.032	2	-.1	2	0	1	-1.428e-6	3	1732.74	2	NC	1
419	M9	1	max	.01	3	.026	3	.006	5	1.074e-2	3	NC	1	NC	1
420			min	-.01	2	-.023	2	-.002	9	-7.186e-3	2	NC	1	NC	1
421		2	max	.01	3	.016	3	.005	5	5.269e-3	3	NC	4	NC	1
422			min	-.01	2	-.014	2	0	9	-3.532e-3	2	5208.782	2	NC	1
423		3	max	.01	3	.006	3	.006	4	1.368e-4	1	NC	4	NC	1
424			min	-.01	2	-.005	2	0	12	-9.755e-5	3	2664.431	3	NC	1
425		4	max	.01	3	.003	2	.007	4	1.071e-4	1	NC	4	NC	1
426			min	-.01	2	-.002	3	-.001	3	-9.916e-5	3	1807.51	3	NC	1
427		5	max	.01	3	.009	2	.008	4	7.736e-5	1	NC	4	NC	1
428			min	-.01	2	-.009	3	-.003	3	-1.008e-4	3	1424.033	3	8736.491	3
429		6	max	.01	3	.015	2	.01	4	4.762e-5	1	NC	4	NC	1
430			min	-.01	2	-.015	3	-.004	3	-1.024e-4	3	1215.651	3	7584.921	3
431		7	max	.01	3	.019	2	.013	4	2.041e-5	4	NC	4	NC	1
432			min	-.01	2	-.019	3	-.004	3	-1.04e-4	3	1093.148	3	6545.38	4
433		8	max	.01	3	.023	2	.015	4	3.656e-5	5	NC	4	NC	1
434			min	-.01	2	-.022	3	-.005	3	-1.056e-4	3	1021.27	3	4653.276	4
435		9	max	.01	3	.025	2	.019	4	5.636e-5	5	NC	4	NC	1
436			min	-.01	2	-.024	3	-.005	3	-1.072e-4	3	984.102	3	3508.869	4
437		10	max	.01	3	.026	2	.023	5	7.616e-5	5	NC	4	NC	1
438			min	-.01	2	-.024	3	-.005	3	-1.088e-4	3	965.604	2	2762.42	4
439		11	max	.009	3	.026	2	.027	5	9.596e-5	5	NC	4	NC	1
440			min	-.01	2	-.024	3	-.005	3	-1.104e-4	3	972.621	2	2247.696	4
441		12	max	.009	3	.024	2	.031	5	1.158e-4	5	NC	4	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.01	2	-.022	3	-.005	3	-1.308e-4	1	1008.916	2	1870.813	5
443		13	max	.009	3	.021	2	.035	5	1.356e-4	5	NC	4	NC	1
444			min	-.01	2	-.018	3	-.005	3	-1.606e-4	1	1083.081	2	1587.909	5
445		14	max	.009	3	.016	2	.04	5	1.554e-4	5	NC	4	NC	1
446			min	-.01	2	-.014	3	-.004	1	-1.903e-4	1	1214.832	2	1376.297	5
447		15	max	.009	3	.01	2	.045	5	1.752e-4	5	NC	4	NC	1
448			min	-.01	2	-.009	3	-.005	1	-2.201e-4	1	1450.587	2	1214.154	5
449		16	max	.009	3	.002	2	.049	5	4.213e-4	5	NC	4	NC	1
450			min	-.01	2	-.002	3	-.005	1	-2.424e-4	1	1843.18	3	1087.569	5
451		17	max	.009	3	.006	3	.053	5	6.064e-3	4	NC	4	NC	1
452			min	-.01	2	-.008	2	-.004	1	-8.957e-5	1	2675.462	3	987.22	5
453		18	max	.009	3	.015	3	.058	5	2.991e-3	5	NC	1	NC	1
454			min	-.01	2	-.019	2	-.003	1	-5.354e-3	2	5247.311	3	902.558	4
455		19	max	.009	3	.024	3	.062	4	5.827e-3	3	NC	1	NC	1
456			min	-.01	2	-.031	2	0	9	-1.08e-2	2	5673.149	2	831.268	4
457	M13	1	max	.002	9	.026	3	.01	3	4.002e-3	3	NC	1	NC	1
458			min	-.006	5	-.023	2	-.01	2	-3.419e-3	2	NC	1	NC	1
459		2	max	.002	9	.089	3	.008	3	4.973e-3	3	NC	4	NC	1
460			min	-.006	5	-.064	2	-.007	2	-4.259e-3	2	1733.98	3	NC	1
461		3	max	.002	9	.141	3	.013	1	5.944e-3	3	NC	4	NC	2
462			min	-.006	5	-.1	2	-.006	10	-5.1e-3	2	944.531	3	6025.952	1
463		4	max	.002	9	.176	3	.021	1	6.915e-3	3	NC	5	NC	2
464			min	-.006	5	-.124	2	-.006	10	-5.94e-3	2	723.749	3	4271.749	1
465		5	max	.002	9	.19	3	.023	1	7.886e-3	3	NC	5	NC	2
466			min	-.006	5	-.135	2	-.008	10	-6.781e-3	2	660.352	3	3912.62	1
467		6	max	.002	9	.184	3	.02	9	8.857e-3	3	NC	5	NC	2
468			min	-.006	5	-.132	2	-.01	2	-7.621e-3	2	685.634	3	4516.094	1
469		7	max	.002	9	.162	3	.019	3	9.828e-3	3	NC	5	NC	2
470			min	-.006	5	-.119	2	-.016	2	-8.462e-3	2	800.581	3	7213.187	9
471		8	max	.002	9	.13	3	.023	3	1.08e-2	3	NC	4	NC	1
472			min	-.006	5	-.1	2	-.023	2	-9.302e-3	2	1048.074	3	7988.595	2
473		9	max	.002	9	.1	3	.026	3	1.177e-2	3	NC	4	NC	1
474			min	-.006	5	-.081	2	-.029	2	-1.014e-2	2	1482.075	3	5500.238	2
475		10	max	.002	9	.086	3	.03	3	1.274e-2	3	NC	4	NC	4
476			min	-.007	5	-.072	2	-.032	2	-1.098e-2	2	1834.541	3	4833.182	2
477		11	max	.002	9	.1	3	.032	3	1.177e-2	3	NC	4	NC	1
478			min	-.007	5	-.081	2	-.029	2	-1.014e-2	2	1482.073	3	4873.598	3
479		12	max	.001	9	.13	3	.033	3	1.08e-2	3	NC	4	NC	1
480			min	-.007	5	-.1	2	-.023	2	-9.302e-3	2	1048.072	3	4735.454	3
481		13	max	.001	9	.162	3	.032	3	9.836e-3	3	NC	5	NC	2
482			min	-.007	5	-.119	2	-.016	2	-8.462e-3	2	800.58	3	4945.42	3
483		14	max	.001	9	.185	3	.029	3	8.868e-3	3	NC	5	NC	2
484			min	-.007	5	-.132	2	-.01	2	-7.621e-3	2	685.634	3	4512.772	1
485		15	max	.001	9	.191	3	.026	3	7.899e-3	3	NC	5	NC	2
486			min	-.007	5	-.135	2	-.008	10	-6.781e-3	2	660.351	3	3917.226	1
487		16	max	.001	9	.176	3	.021	3	6.931e-3	3	NC	5	NC	2
488			min	-.007	5	-.124	2	-.006	10	-5.94e-3	2	723.748	3	4284.334	1
489		17	max	.001	9	.142	3	.017	3	5.962e-3	3	NC	4	NC	2
490			min	-.007	5	-.1	2	-.006	10	-5.1e-3	2	944.53	3	6057.316	1
491		18	max	.001	9	.09	3	.013	3	4.994e-3	3	NC	4	NC	1
492			min	-.007	5	-.064	2	-.008	2	-4.259e-3	2	1733.978	3	NC	1
493		19	max	.001	9	.027	3	.01	3	4.026e-3	3	NC	1	NC	1
494			min	-.007	5	-.023	2	-.01	2	-3.419e-3	2	NC	1	NC	1
495	M16	1	max	0	9	.024	3	.009	3	4.483e-3	2	NC	1	NC	1
496			min	-.062	4	-.031	2	-.01	2	-3.402e-3	3	NC	1	NC	1
497		2	max	0	9	.058	3	.013	3	5.592e-3	2	NC	4	NC	1
498			min	-.062	4	-.094	2	-.007	2	-4.195e-3	3	1721.106	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	0	9	.086	3	.017	3	6.7e-3	2	NC	4	NC	2
500			min	-.062	4	-.146	2	-.005	10	-4.987e-3	3	935.424	2	6033.072	1
501		4	max	0	9	.107	3	.021	3	7.809e-3	2	NC	5	NC	2
502			min	-.062	4	-.182	2	-.006	10	-5.78e-3	3	713.939	2	4276.321	1
503		5	max	0	9	.117	3	.024	3	8.917e-3	2	NC	5	NC	2
504			min	-.062	4	-.198	2	-.007	10	-6.573e-3	3	647.264	2	3917.029	1
505		6	max	0	9	.116	3	.027	3	1.003e-2	2	NC	5	NC	2
506			min	-.062	4	-.193	2	-.01	2	-7.366e-3	3	665.226	2	4522.571	1
507		7	max	0	9	.107	3	.029	3	1.113e-2	2	NC	5	NC	2
508			min	-.062	4	-.172	2	-.016	2	-8.159e-3	3	763.794	2	5503.783	3
509		8	max	0	9	.093	3	.03	3	1.224e-2	2	NC	4	NC	1
510			min	-.062	4	-.142	2	-.023	2	-8.951e-3	3	971.757	2	5288.388	3
511		9	max	0	1	.08	3	.029	3	1.335e-2	2	NC	4	NC	1
512			min	-.062	4	-.113	2	-.029	2	-9.744e-3	3	1313.852	2	5356.303	3
513		10	max	0	1	.073	3	.028	3	1.446e-2	2	NC	4	NC	4
514			min	-.062	4	-.1	2	-.032	2	-1.054e-2	3	1571.773	2	4873.24	2
515		11	max	0	1	.08	3	.027	3	1.335e-2	2	NC	4	NC	1
516			min	-.062	4	-.113	2	-.029	2	-9.742e-3	3	1313.852	2	5550.442	2
517		12	max	0	1	.093	3	.025	3	1.224e-2	2	NC	4	NC	1
518			min	-.062	4	-.142	2	-.023	2	-8.946e-3	3	971.757	2	6847.591	3
519		13	max	0	1	.107	3	.023	3	1.113e-2	2	NC	5	NC	2
520			min	-.062	4	-.172	2	-.016	2	-8.151e-3	3	763.794	2	7243.388	9
521		14	max	0	1	.116	3	.021	3	1.003e-2	2	NC	5	NC	2
522			min	-.062	4	-.193	2	-.01	2	-7.356e-3	3	665.226	2	4528.76	1
523		15	max	0	1	.116	3	.023	1	8.918e-3	2	NC	5	NC	2
524			min	-.062	4	-.198	2	-.007	10	-6.561e-3	3	647.264	2	3928.8	1
525		16	max	0	1	.107	3	.02	1	7.81e-3	2	NC	5	NC	2
526			min	-.062	4	-.182	2	-.006	10	-5.765e-3	3	713.939	2	4296.621	1
527		17	max	0	1	.086	3	.013	3	6.702e-3	2	NC	4	NC	2
528			min	-.062	4	-.146	2	-.005	10	-4.97e-3	3	935.424	2	6076.449	1
529		18	max	0	1	.057	3	.011	3	5.593e-3	2	NC	4	NC	1
530			min	-.062	4	-.094	2	-.007	2	-4.175e-3	3	1721.106	2	NC	1
531		19	max	0	1	.023	3	.009	3	4.485e-3	2	NC	1	NC	1
532			min	-.062	4	-.031	2	-.01	2	-3.38e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	4.26e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-6.666e-4	5	NC	1	NC	1
535		2	max	0	3	0	5	.005	4	8.674e-4	3	NC	1	NC	1
536			min	0	4	-.003	1	0	3	-6.78e-4	5	NC	1	NC	1
537		3	max	0	3	.002	5	.012	4	1.309e-3	3	NC	1	NC	1
538			min	-.001	4	-.006	1	-.004	3	-9.143e-4	2	NC	1	5631.931	4
539		4	max	0	3	.002	5	.02	4	1.75e-3	3	NC	4	NC	9
540			min	-.002	4	-.009	1	-.008	3	-1.344e-3	2	7298.553	2	3522.21	4
541		5	max	0	3	.003	5	.027	4	2.192e-3	3	NC	5	NC	9
542			min	-.002	4	-.011	1	-.013	3	-1.774e-3	2	5695.135	1	2581.729	4
543		6	max	0	3	.004	5	.033	4	2.633e-3	3	NC	5	NC	9
544			min	-.003	4	-.013	1	-.018	3	-2.204e-3	2	4793.058	2	2087.063	4
545		7	max	0	3	.004	5	.038	4	3.074e-3	3	NC	5	8535.12	9
546			min	-.003	4	-.015	1	-.024	3	-2.634e-3	2	4250.578	1	1810.049	4
547		8	max	0	3	.005	5	.042	4	3.516e-3	3	NC	5	7143.206	9
548			min	-.004	4	-.016	1	-.03	3	-3.064e-3	2	3925.008	1	1547.932	3
549		9	max	0	3	.005	5	.043	4	3.957e-3	3	NC	5	6222.24	9
550			min	-.004	4	-.017	1	-.035	3	-3.494e-3	2	3749.767	1	1334.697	3
551		10	max	.001	3	.006	5	.043	4	4.399e-3	3	NC	5	5612.304	9
552			min	-.005	4	-.017	1	-.039	3	-3.924e-3	2	3694.329	1	1193.866	3
553		11	max	.001	3	.006	5	.041	4	4.84e-3	3	NC	5	5228.852	9
554			min	-.005	4	-.017	1	-.042	3	-4.354e-3	2	3749.767	1	1104.588	3
555		12	max	.001	3	.006	5	.037	4	5.281e-3	3	NC	5	5030.973	9

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.006	4	-.016	1	-.042	3	-4.784e-3	2	3925.008	1	1056.547	3
557		13	max	.001	3	.007	5	.032	4	5.723e-3	3	NC	5	5009.985	9
558			min	-.006	4	-.014	9	-.041	3	-5.214e-3	2	4250.578	1	1046.839	3
559		14	max	.001	3	.007	5	.028	2	6.164e-3	3	NC	5	5192.118	9
560			min	-.007	4	-.013	9	-.037	3	-5.644e-3	2	4793.058	1	1080.156	3
561		15	max	.002	3	.007	5	.022	2	6.606e-3	3	NC	5	7668.561	15
562			min	-.007	4	-.011	9	-.03	3	-6.075e-3	2	5695.135	1	1173.387	3
563		16	max	.002	3	.007	5	.015	1	7.047e-3	3	NC	4	NC	13
564			min	-.008	4	-.009	9	-.019	3	-6.505e-3	2	7298.553	1	1372.253	3
565		17	max	.002	3	.007	5	.006	4	7.488e-3	3	NC	1	NC	4
566			min	-.008	4	-.007	9	-.005	3	-6.935e-3	2	NC	1	1820.09	3
567		18	max	.002	3	.006	5	.014	3	7.93e-3	3	NC	1	NC	4
568			min	-.009	4	-.004	9	-.015	2	-7.365e-3	2	NC	1	3241.861	3
569		19	max	.002	3	.009	2	.037	3	8.371e-3	3	NC	1	NC	1
570			min	-.009	4	-.001	9	-.035	2	-7.795e-3	2	NC	1	NC	1
571	M16A	1	max	0	2	.002	2	.011	3	2.365e-3	3	NC	1	NC	1
572			min	-.003	4	-.004	4	-.011	2	-2.347e-3	2	NC	1	NC	1
573		2	max	0	2	-.001	10	.003	3	2.278e-3	3	NC	1	NC	1
574			min	-.003	4	-.01	4	-.005	2	-2.243e-3	2	NC	1	9123.984	3
575		3	max	0	2	-.004	10	.004	1	2.191e-3	3	NC	1	NC	4
576			min	-.003	4	-.016	4	-.008	5	-2.138e-3	2	5621.47	4	5170.738	3
577		4	max	0	2	-.006	12	.007	1	2.104e-3	3	NC	12	NC	9
578			min	-.003	4	-.021	4	-.014	5	-2.033e-3	2	3856.657	4	3940.028	3
579		5	max	0	2	-.007	12	.009	1	2.017e-3	3	NC	12	NC	9
580			min	-.003	4	-.026	4	-.021	5	-1.928e-3	2	3009.389	4	3410.058	3
581		6	max	0	2	-.008	12	.011	1	1.929e-3	3	9586.116	12	NC	9
582			min	-.002	4	-.03	4	-.028	5	-1.823e-3	2	2532.719	4	2625.833	5
583		7	max	0	2	-.009	12	.011	1	1.842e-3	3	8501.155	12	NC	9
584			min	-.002	4	-.033	4	-.034	5	-1.719e-3	2	2246.064	4	2100.263	5
585		8	max	0	2	-.01	12	.011	1	1.755e-3	3	7850.016	12	NC	9
586			min	-.002	4	-.036	4	-.04	5	-1.614e-3	2	2074.029	4	1800.245	5
587		9	max	0	2	-.01	12	.011	1	1.668e-3	3	7499.534	12	NC	9
588			min	-.002	4	-.037	4	-.043	5	-1.509e-3	2	1981.429	4	1631.378	5
589		10	max	0	2	-.01	12	.01	1	1.581e-3	3	7388.658	12	NC	9
590			min	-.002	4	-.037	4	-.045	5	-1.404e-3	2	1952.135	4	1551.44	5
591		11	max	0	2	-.01	12	.008	1	1.494e-3	3	7499.534	12	NC	9
592			min	-.002	4	-.037	4	-.045	5	-1.299e-3	2	1981.429	4	1543.21	5
593		12	max	0	2	-.009	12	.007	1	1.407e-3	3	7850.016	12	NC	9
594			min	-.001	4	-.035	4	-.044	5	-1.195e-3	2	2074.029	4	1605.406	5
595		13	max	0	2	-.009	12	.005	1	1.32e-3	3	8501.155	12	NC	2
596			min	-.001	4	-.032	4	-.04	5	-1.09e-3	2	2246.064	4	1752.272	5
597		14	max	0	2	-.008	12	.004	1	1.233e-3	3	9586.116	12	NC	1
598			min	0	4	-.028	4	-.035	5	-9.85e-4	2	2532.719	4	2021.632	5
599		15	max	0	2	-.006	12	.002	1	1.145e-3	3	NC	12	NC	1
600			min	0	4	-.024	4	-.028	5	-8.802e-4	2	3009.389	4	2500.687	5
601		16	max	0	2	-.005	12	.001	9	1.058e-3	3	NC	12	NC	1
602			min	0	4	-.019	4	-.021	5	-7.754e-4	2	3856.657	4	3408.89	5
603		17	max	0	2	-.003	12	0	9	9.712e-4	3	NC	1	NC	1
604			min	0	4	-.013	4	-.013	5	-6.706e-4	2	5621.47	4	5440.434	5
605		18	max	0	2	-.002	12	0	3	9.953e-4	4	NC	1	NC	1
606			min	0	4	-.006	4	-.006	5	-5.658e-4	2	NC	1	NC	1
607		19	max	0	1	0	1	0	1	1.062e-3	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-4.61e-4	2	NC	1	NC	1

Anchor Designer™ Software Version 2.4.5673.0	Company:	Schletter, Inc.	Date:	12/10/2015
	Engineer:	HCV	Page:	1/5
	Project:	Standard PVMini - Worst Case		
	Address:			
	Phone:			
	E-mail:			

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

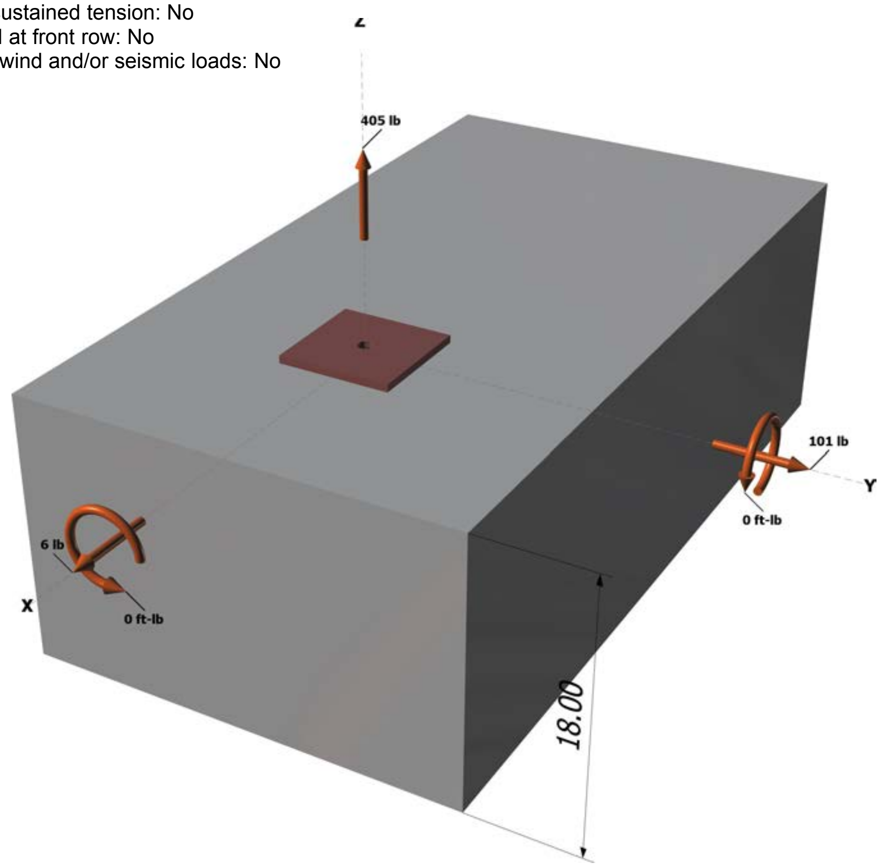
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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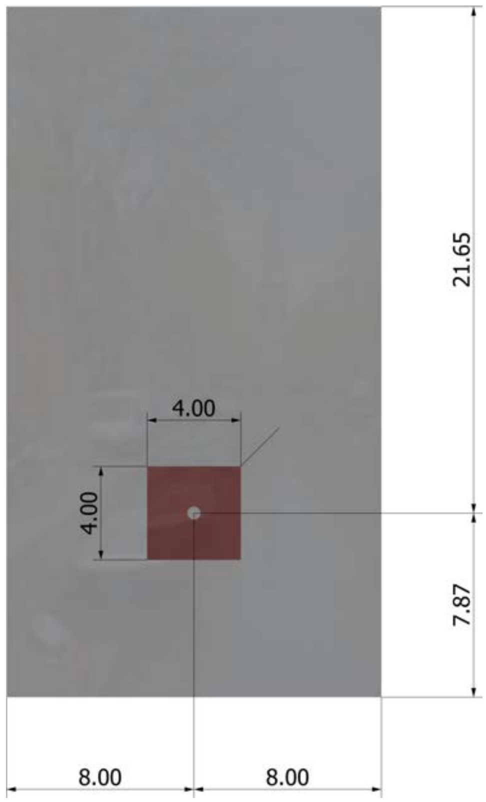


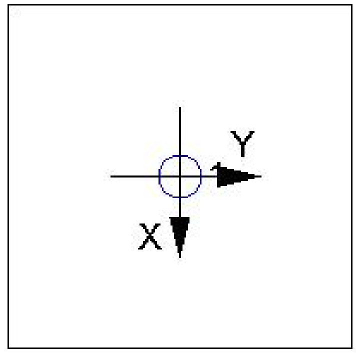
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\,(A_{Nc}/A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na}/A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

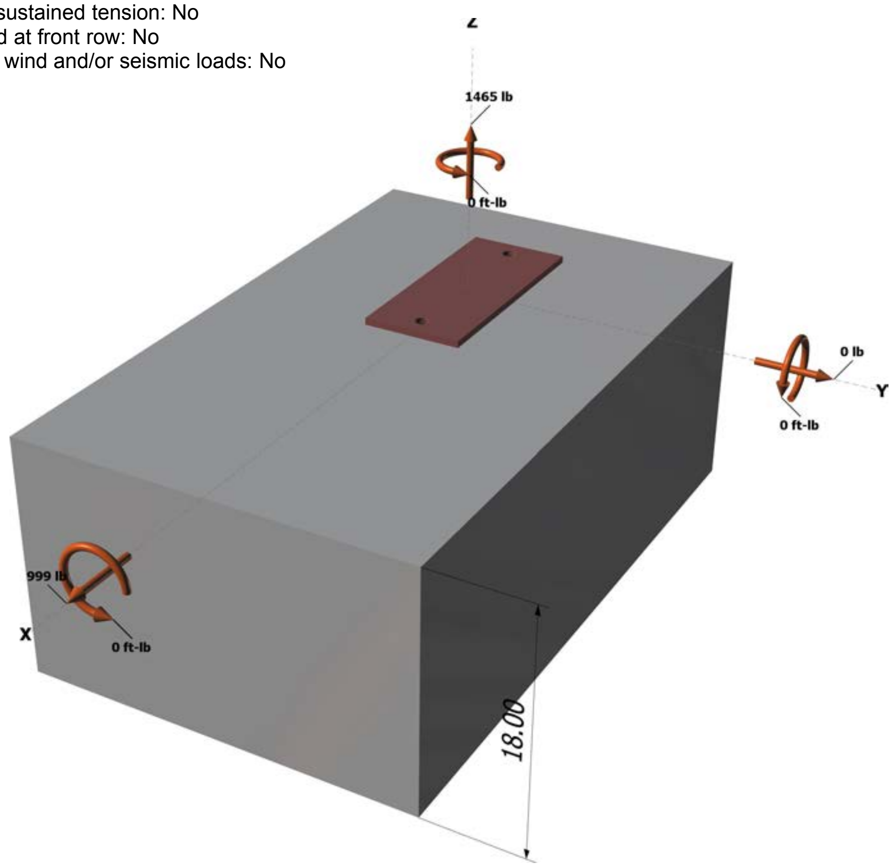
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



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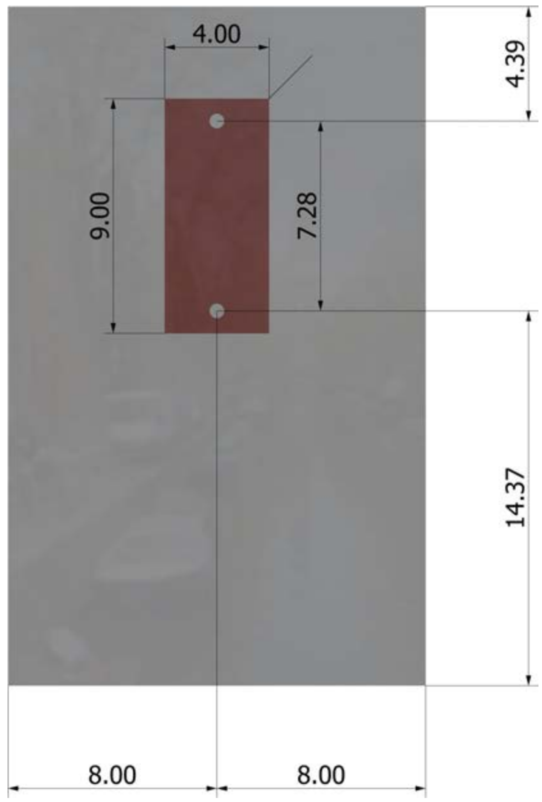


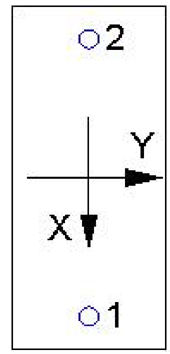
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\,(A_{Nc}/A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na}/A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\min|k_{cp}N_{ag}\ ;\ k_{cp}N_{cbg}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\ ;\ k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.