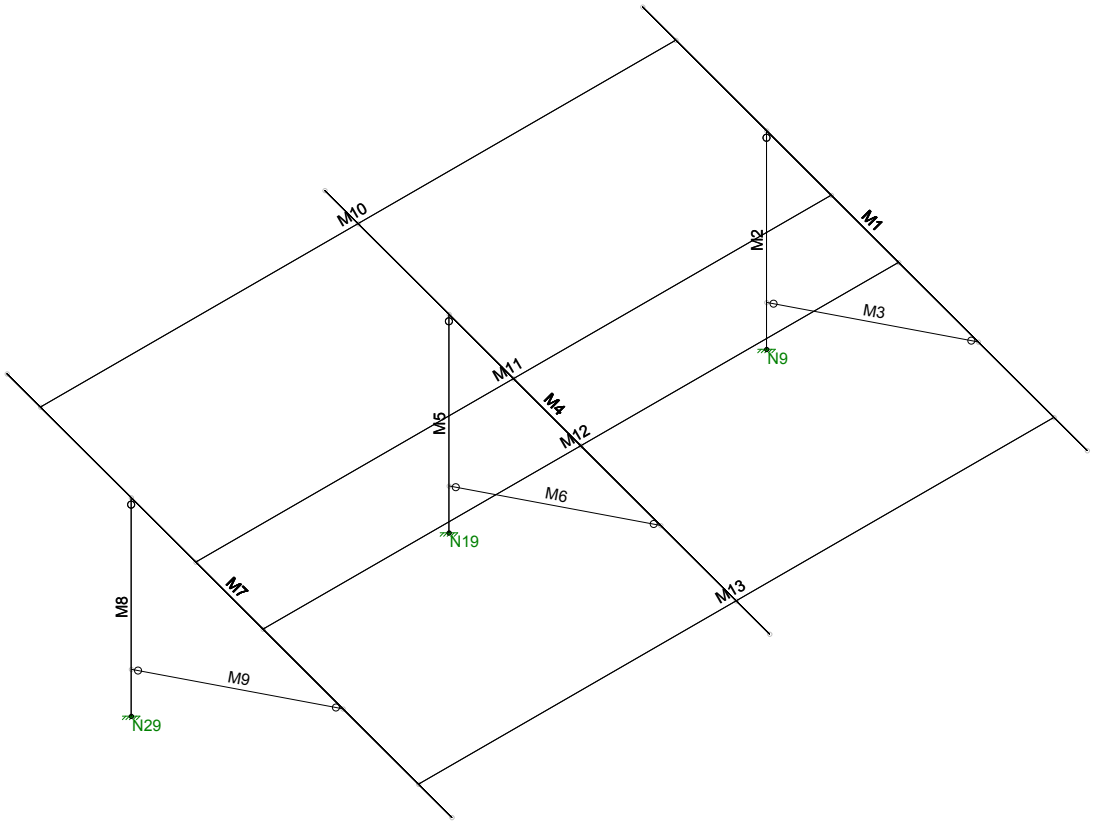


Schletter, Inc.		20° Tilt w/o Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

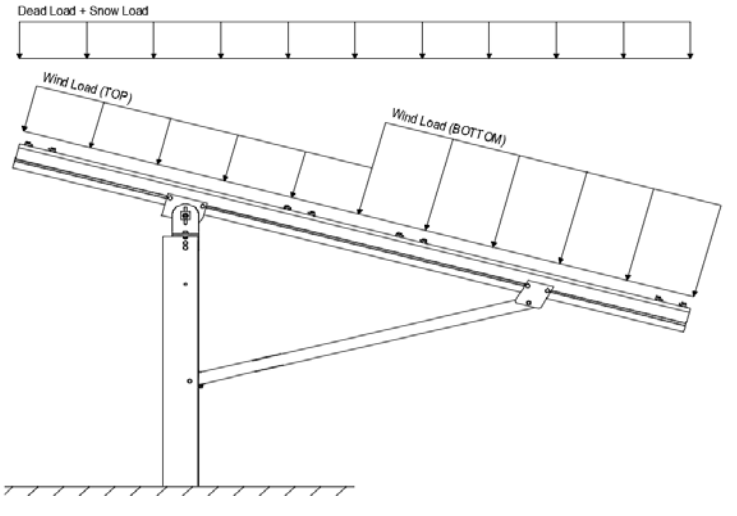
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row =	2
Module Tilt =	20°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	
g_{MIN} =	1.75	psf	*Self-weight of the PV modules.*

2.2 Snow Loads

Ground Snow Load, P_g =	20.00	psf	
Sloped Roof Snow Load, P_s =	13.75	psf	*(ASCE 7-05, Eq. 7-2)*
I_s =	1.00		
C_s =	0.91		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	130	mph	Exposure Category = C
Height <	15	ft	Importance Category = II
Peak Velocity Pressure, q_z =	26.53	psf	*Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.05		*(Pressure)*
$Cf+_{BOTTOM}$ =	1.65		
$Cf-_{TOP}$ =	-2.12		*(Suction)*
$Cf-_{BOTTOM}$ =	-1		

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.

2.4 Seismic Loads - N/A

S_S =	0.00	R =	1.25
S_{DS} =	0.00	C_S =	0
S_1 =	0.00	ρ =	1.3
S_{D1} =	0.00	Ω =	1.25
T_a =	0.00	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W	
1.2D + 1.6W + 0.5S	
0.9D + 1.6W [M]	
1.54D + 1.3E + 0.2S [R]	*(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)*
0.56D + 1.3E [R]	
1.54D + 1.25E + 0.2S [O]	
0.56D + 1.25E [O]	

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S	
1.0D + 1.0W	
1.0D + 0.75L + 0.75W + 0.75S	
0.6D + 1.0W [M]	*(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)*
1.238D + 0.875E [O]	
1.1785D + 0.65625E + 0.75S [O]	
0.362D + 0.875E [O]	

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

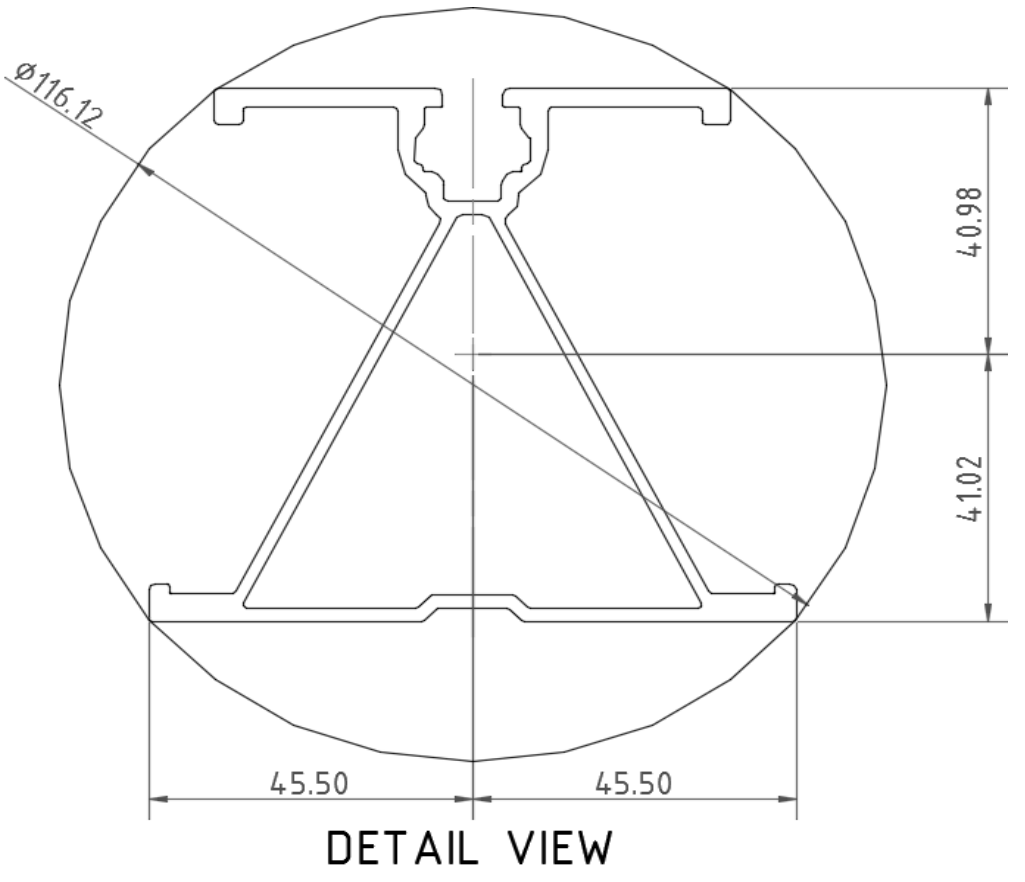
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	84	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.6	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.205	k-ft
M_z =	0.147	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	56%	

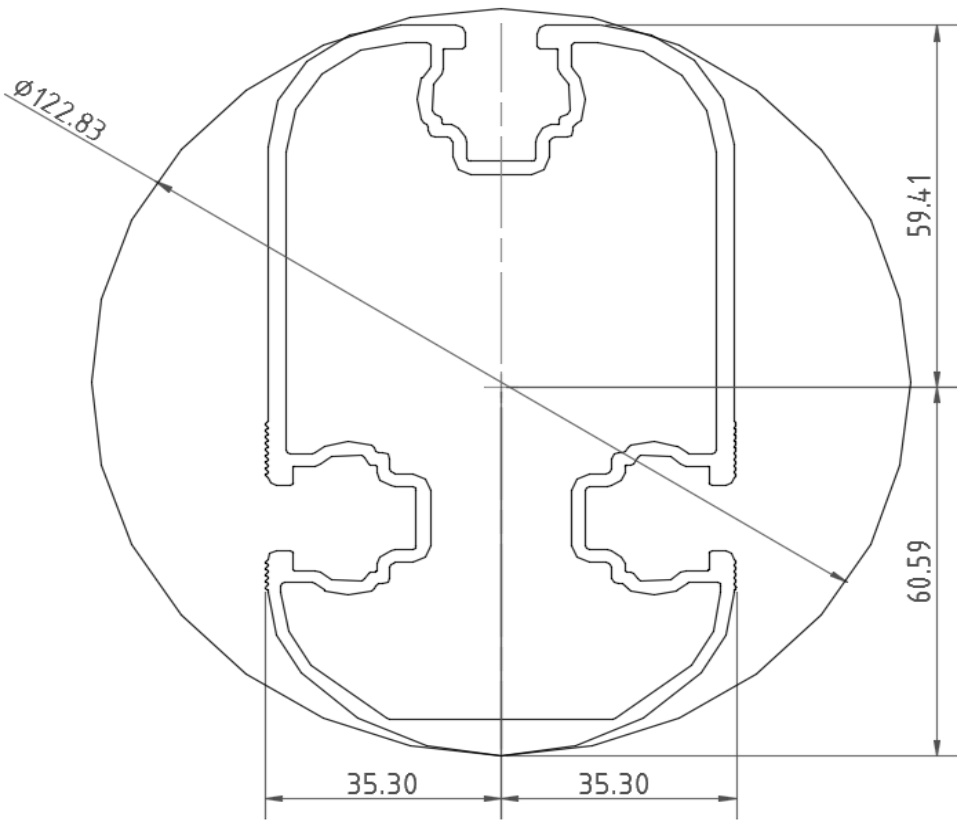


DETAIL VIEW

4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

Girder Type =	**T5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	63.82	in
$\Phi F_{ty\ AXIAL}$ =	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	30.46	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	31.56	ksi
S_y =	1.98	in^3
S_x =	1.32	in^3
E =	10100	ksi
I_y =	4.74	in^4
I_x =	1.83	in^4
A =	1.93	in^2
g =	2.32	lbs/ft
M_y =	4.373	k-ft
M_z =	0.000	k-ft
P_n =	0.030	k
$M_{y\ allowable}$ =	5.026	k-ft
$M_{z\ allowable}$ =	3.472	k-ft
$P_{n\ allowable}$ =	59.439	k
Utilization =	87%	

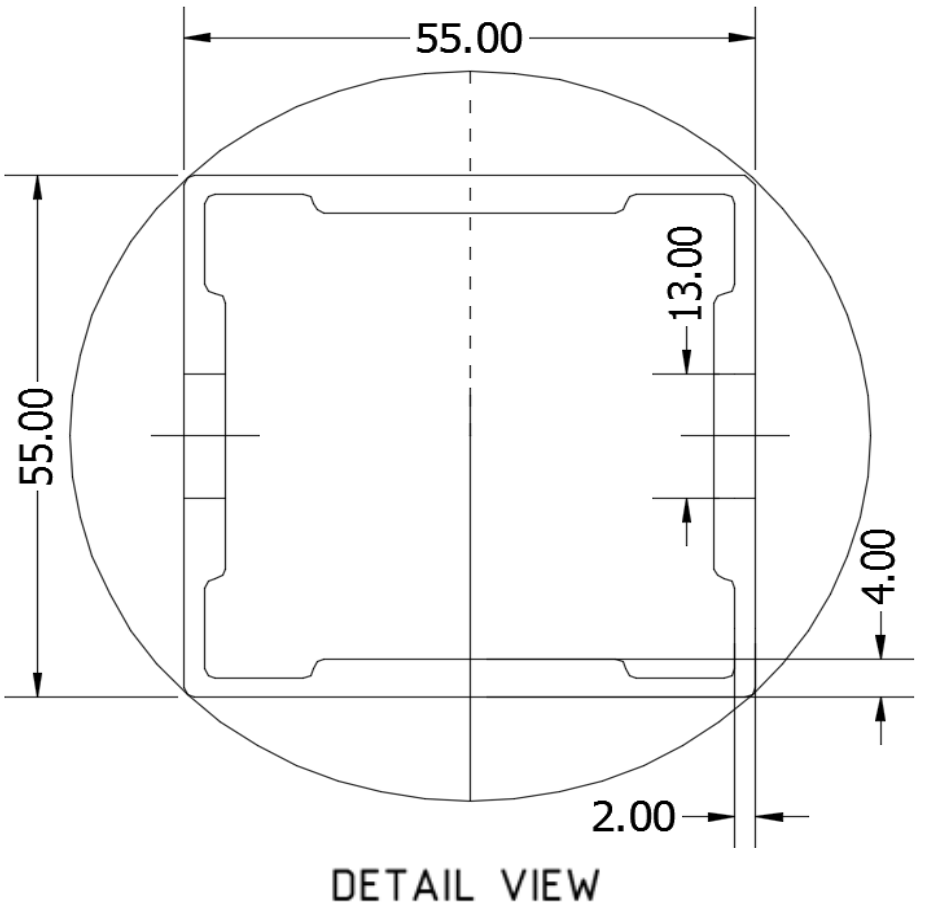


DETAIL VIEW

4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

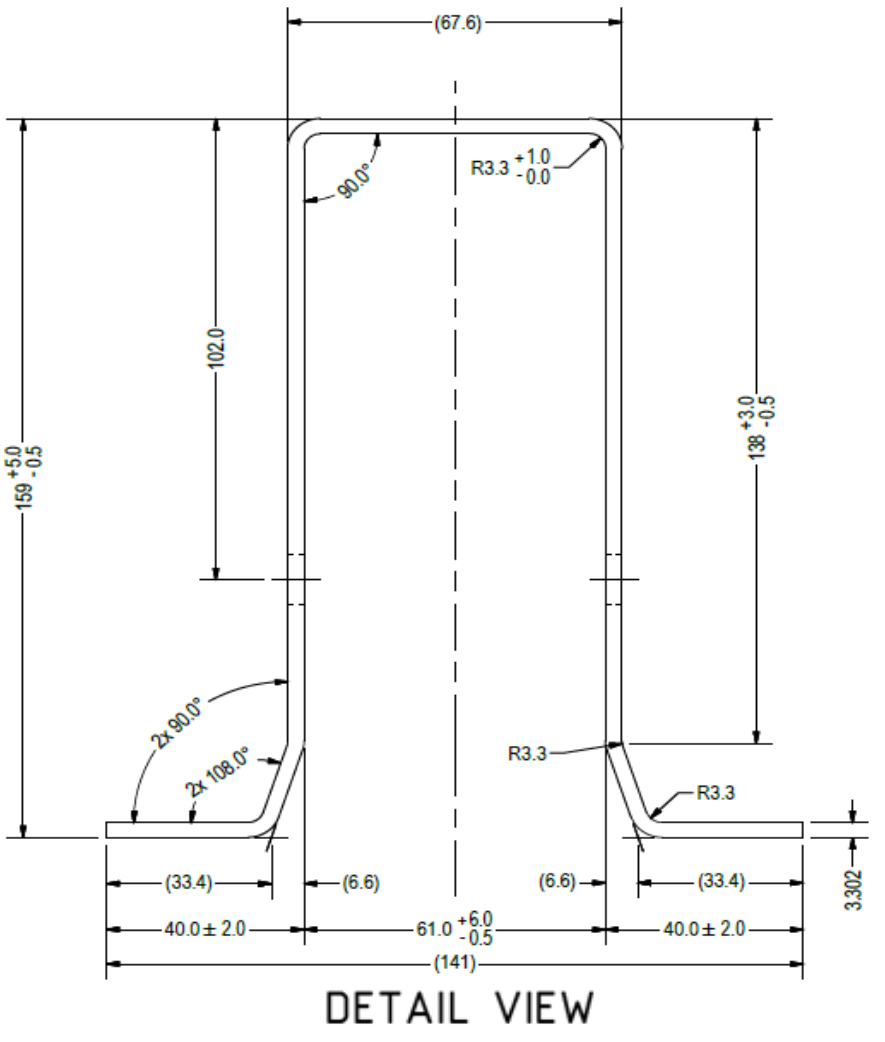
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.00	in
$\Phi F_{ty\ AXIAL}$ =	13.67	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.005	k-ft
M_z =	0.000	k-ft
P_n =	5.424	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.425	k
Utilization =	41%	



4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	65.62	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	10.148	k-ft
M_z =	0.000	k-ft
P_r =	5.866	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	46.025	k
Utilization =	66%	



5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	7.12	k
Maximum Lateral Load =	2.87	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

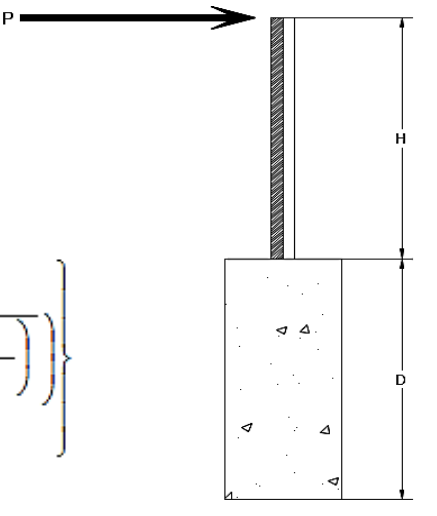
Lateral Force @ Top of Pole, P =	1.22	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1 + \sqrt{1 + \left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

Non-Constrained

Lateral Force @ Top of Pole, P =	1.22	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	6.57	
Required Footing Depth, D =	9.82	ft
2nd Trial @ D_2 =	6.54	ft
Lateral Soil Bearing @ D/3, S_1 =	0.44	ksf
Lateral Soil Bearing @ D, S_3 =	1.31	ksf
Constant 2.34P/(S_1B), A =	3.27	
Required Footing Depth, D =	5.94	ft
3rd Trial @ D_3 =	6.24	ft
Lateral Soil Bearing @ D/3, S_1 =	0.42	ksf
Lateral Soil Bearing @ D, S_3 =	1.25	ksf
Constant 2.34P/(S_1B), A =	3.42	
Required Footing Depth, D =	6.14	ft
4th Trial @ D_4 =	6.19	ft
Lateral Soil Bearing @ D/3, S_1 =	0.41	ksf
Lateral Soil Bearing @ D, S_3 =	1.24	ksf
Constant 2.34P/(S_1B), A =	3.45	
Required Footing Depth, D =	6.17	ft
5th Trial @ D_5 =	6.18	ft
Lateral Soil Bearing @ D/3, S_1 =	0.41	ksf
Lateral Soil Bearing @ D, S_3 =	1.24	ksf
Constant 2.34P/(S_1B), A =	3.45	
Required Footing Depth, D =	6.25	ft

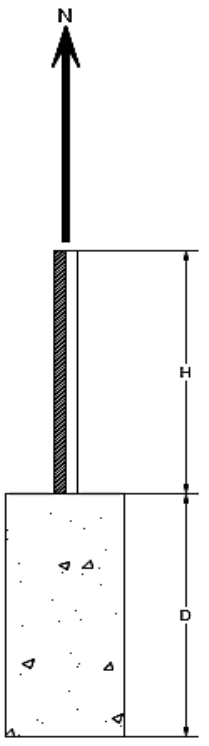
A 2ft diameter x 6.25ft deep footing unrestrained at ground level is required for the racking structure.

5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	3.41	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	2.23	k
Required Concrete Volume, V =	15.38	ft^3
Required Footing Depth, D =	5.00	ft

A 2ft diameter x 5ft deep footing unrestrained at ground level is required for the racking structure.



Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	7.39
2	0.4	0.2	118.10	7.28
3	0.6	0.2	118.10	7.18
4	0.8	0.2	118.10	7.07
5	1	0.2	118.10	6.97
6	1.2	0.2	118.10	6.87
7	1.4	0.2	118.10	6.76
8	1.6	0.2	118.10	6.66
9	1.8	0.2	118.10	6.56
10	2	0.2	118.10	6.45
11	2.2	0.2	118.10	6.35
12	2.4	0.2	118.10	6.24
13	2.6	0.2	118.10	6.14
14	2.8	0.2	118.10	6.04
15	3	0.2	118.10	5.93
16	3.2	0.2	118.10	5.83
17	3.4	0.2	118.10	5.73
18	3.6	0.2	118.10	5.62
19	3.8	0.2	118.10	5.52
20	4	0.2	118.10	5.42
21	4.2	0.2	118.10	5.31
22	4.4	0.2	118.10	5.21
23	4.6	0.2	118.10	5.10
24	4.8	0.2	118.10	5.00
25	5	0.2	118.10	4.90
26	0	0.0	0.00	4.90
27	0	0.0	0.00	4.90
28	0	0.0	0.00	4.90
29	0	0.0	0.00	4.90
30	0	0.0	0.00	4.90
31	0	0.0	0.00	4.90
32	0	0.0	0.00	4.90
33	0	0.0	0.00	4.90
34	0	0.0	0.00	4.90
Max	5	Sum	1.18	

5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	6.25	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	3.52	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	20.42	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

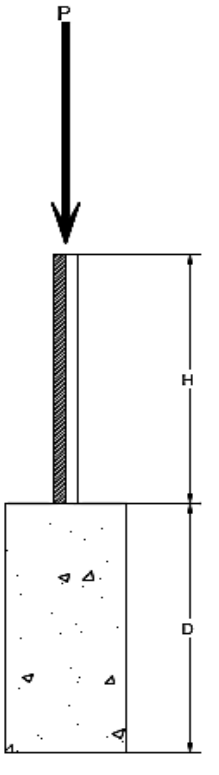
Weight of Concrete

Footing Volume	19.63	ft^3
Weight	2.85	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	3.06	k
1/3 Increase for Wind =	1.33	
Total Resistance =	10.37	k
Applied Force =	6.37	k
Utilization =	61%	

A 2ft diameter footing passes at a depth of 6.25ft.



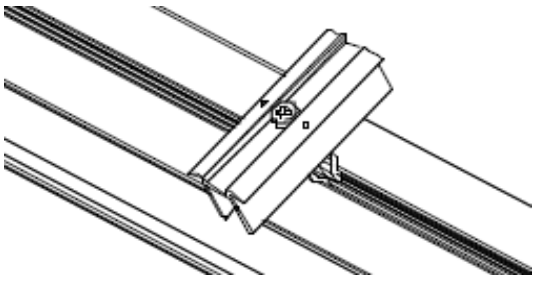
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

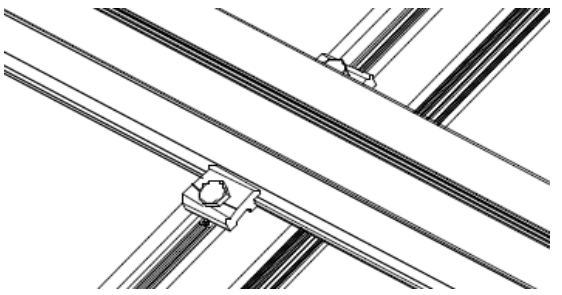
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.850 k
Allowable Uplift	=	1.214 k
Utilization	=	70%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	2.124 k
Allowable Uplift	=	2.180 k
Utilization	=	97%

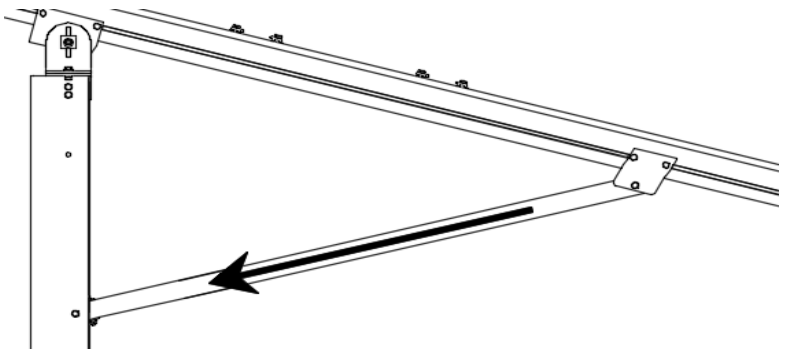


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load	=	5.424 k
M10 Bolt Shear Capacity	=	8.894 k
Utilization	=	61%

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

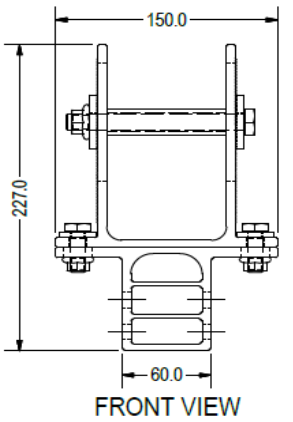


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

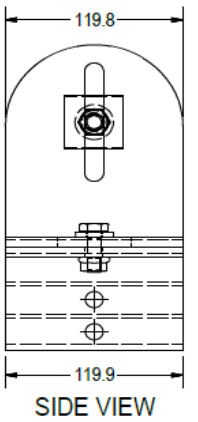
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

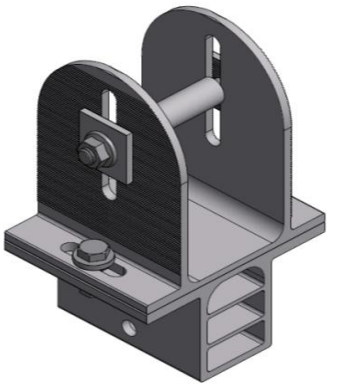
Maximum Tensile Load	=	4.489 k
Allowable Load	=	5.649 k
Utilization	=	79%



FRONT VIEW



SIDE VIEW



7. SEISMIC DESIGN

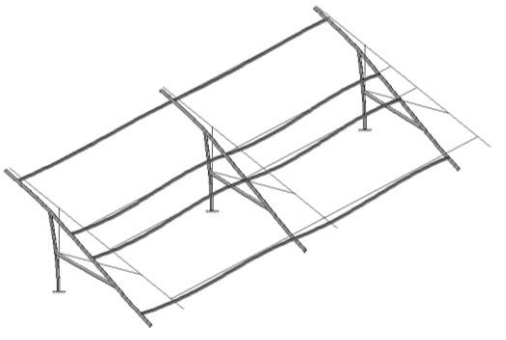
7.1 Seismic Drift - N/A

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	65.92 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.318 in
Max Drift, Δ_{MAX}	=	0 in

N/A

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 84 in

J = 0.432

232.383

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.4 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 84

J = 0.432

147.782

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.4

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 63.8189 in
J = 1.98
82.1278

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.5 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 63.8189
J = 1.98
89.1294

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.3

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = φb[Bt-Dt*√(Rb/t)]

φF_L = 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L St$ = 30.5 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 5.001 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L Wk$ = 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φc[Bt-Dt*√(Rb/t)]

φF_L = 30.80 ksi

φF_L = 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 61 in

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St$ = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 61

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk$ = 1.460 k-ft

Compression

3.4.7

λ = 1.41113

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.77756

φF_L = (φccFcy)/(λ²)

φF_L = 13.6667 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 13.67 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 14.07 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	65.62	in	
Pr =	5.87	k	(LRFD Factored Load)
Mr (Strong) =	10.15	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	94.42		
4.71√(E/Fy) =	103.55	=> kL/r	≤ 4.71√(E/Fy)
Fcr =	27.44	ksi	
Fe =	32.10	ksi	
Pn =	61.196	k	

Torsional/Flexural Torsional Buckling:

Fcr =	20.6391	ksi
Fey =	81.8881	ksi
Fez =	26.2099	ksi
Pn =	46.0252	k

Bending (Strong Axis):

Yielding:

Mn =	21.95	k-ft		
Flange Local Buckling:				
Mn =	19.207	k-ft		
Pr/Pc =	0.1416	<	0.2	
Utilization =	0.66	<	1.0	OK

Bending (Weak Axis):

Yielding:

Mn =	14.65	k-ft		
Flange Local Buckling:				
Mn =	14.39	k-ft		
Pr/Pc =	0.142	<	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 66%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL								

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-8.366	-8.366	0	0
2	M11	Y	-8.366	-8.366	0	0
3	M12	Y	-8.366	-8.366	0	0
4	M13	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-4.45	-4.45	0	0
2	M11	Y	-4.45	-4.45	0	0
3	M12	Y	-4.45	-4.45	0	0
4	M13	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-54.031	-54.031	0	0
2	M11	Y	-54.031	-54.031	0	0
3	M12	Y	-54.031	-54.031	0	0
4	M13	Y	-54.031	-54.031	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-77.697	-77.697	0	0
2	M11	y	-77.697	-77.697	0	0
3	M12	y	-122.096	-122.096	0	0
4	M13	y	-122.096	-122.096	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	156.875	156.875	0	0
2	M11	y	156.875	156.875	0	0
3	M12	y	73.997	73.997	0	0
4	M13	y	73.997	73.997	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8																
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6																
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6														
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3														
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3														
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25														
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25														

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
8																										
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																		
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1																
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75																
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1														
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875														
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656														
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875														

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	442.365	2	2321.87	2	155.316	2	.163	1	.002	3	5.438	1
2		min	-707.826	3	-1883.61	3	-181.429	3	-.19	3	-.004	2	.153	15
3	N19	max	2176.599	2	6182.328	2	0	3	0	2	0	15	9.411	1
4		min	-2121.884	3	-5472.748	3	0	2	0	3	0	2	.241	15
5	N29	max	442.365	2	2321.87	2	181.429	3	.19	3	.004	2	5.438	1
6		min	-707.826	3	-1883.61	3	-155.316	2	-.163	1	-.002	3	.153	15
7	Totals:	max	3061.329	2	10826.068	2	0	2						
8		min	-3537.537	3	-9239.967	3	0	3						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.006	2	0	3	0	1	0	1	0	1
2			min	0	1	-.002	3	0	1	0	1	0	1	0	1
3		2	max	-.179	15	-.49	15	0	3	0	1	0	3	0	4
4			min	-.76	4	-2.086	4	0	1	0	1	0	1	0	15
5		3	max	-.865	12	333.753	3	15.378	3	.069	3	.181	1	.32	2
6			min	-149.745	1	-722.52	2	-115.86	1	-.192	2	-.008	3	-.147	3
7		4	max	-1.161	12	332.533	3	15.378	3	.069	3	.109	1	.768	2
8			min	-150.337	1	-724.146	2	-115.86	1	-.192	2	.001	12	-.354	3
9		5	max	-1.457	12	331.314	3	15.378	3	.069	3	.037	1	1.218	2
10			min	-150.929	1	-725.772	2	-115.86	1	-.192	2	.001	15	-.56	3
11		6	max	639.581	3	614.433	2	32.248	3	0	15	.079	2	1.177	2
12			min	-1772.602	2	-186.387	3	-148.385	1	-.028	2	-.033	3	-.575	3
13		7	max	639.137	3	612.807	2	32.248	3	0	15	0	10	.796	2
14			min	-1773.194	2	-187.607	3	-148.385	1	-.028	2	-.021	1	-.459	3
15		8	max	638.694	3	611.181	2	32.248	3	0	15	.007	3	.416	2
16			min	-1773.785	2	-188.826	3	-148.385	1	-.028	2	-.113	1	-.343	3
17		9	max	639.576	3	94.757	3	41.813	3	-.002	15	.075	1	.193	2
18			min	-1868.106	2	-42.329	2	-169.406	1	-.146	2	.002	15	-.291	3
19		10	max	639.132	3	93.538	3	41.813	3	-.002	15	.035	3	.22	2
20			min	-1868.698	2	-43.955	2	-169.406	1	-.146	2	-.033	2	-.35	3
21		11	max	638.689	3	92.318	3	41.813	3	-.002	15	.061	3	.247	2
22			min	-1869.29	2	-45.581	2	-169.406	1	-.146	2	-.135	1	-.408	3
23		12	max	635.156	3	790.56	3	39.721	2	.217	3	.097	1	.46	2
24			min	-1958.652	2	-485.586	2	-156.25	3	-.202	2	.003	15	-.744	3
25		13	max	634.712	3	789.34	3	39.721	2	.217	3	.104	1	.761	2
26			min	-1959.244	2	-487.212	2	-156.25	3	-.202	2	-.089	3	-1.234	3
27		14	max	151.304	1	462.159	2	8.549	3	.133	2	.002	3	1.051	2
28			min	.938	3	-738.569	3	-100.379	1	-.294	3	-.003	1	-1.703	3
29		15	max	150.712	1	460.532	2	8.549	3	.133	2	.007	3	.765	2
30			min	.494	3	-739.789	3	-100.379	1	-.294	3	-.065	1	-1.244	3
31		16	max	150.12	1	458.906	2	8.549	3	.133	2	.012	3	.48	2
32			min	.05	3	-741.008	3	-100.379	1	-.294	3	-.128	1	-.784	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
33		17	max	149.528	1	457.28	2	8.549	3	.133	2	.017	3	.195	2
34			min	-.394	3	-742.228	3	-100.379	1	-.294	3	-.19	1	-.324	3
35		18	max	.76	4	2.087	4	0	1	0	1	0	15	0	4
36			min	.179	15	.491	15	0	5	0	1	0	1	0	15
37		19	max	0	1	0	2	0	1	0	1	0	1	0	1
38			min	0	1	-.003	3	0	5	0	1	0	1	0	1
39	M4	1	max	0	1	.012	2	0	1	0	1	0	1	0	1
40			min	0	1	-.004	3	0	1	0	1	0	1	0	1
41		2	max	-.179	15	-.49	15	0	1	0	1	0	1	0	4
42			min	-.76	4	-2.085	4	0	1	0	1	0	1	0	15
43		3	max	17.929	10	911.875	3	0	1	0	1	0	1	.679	2
44			min	-174.719	1	-1808.015	2	0	1	0	1	0	1	-.344	3
45		4	max	17.436	10	910.656	3	0	1	0	1	0	1	1.802	2
46			min	-175.311	1	-1809.641	2	0	1	0	1	0	1	-.909	3
47		5	max	16.943	10	909.436	3	0	1	0	1	0	1	2.926	2
48			min	-175.903	1	-1811.267	2	0	1	0	1	0	1	-1.474	3
49		6	max	2026.519	3	1710.374	2	0	1	0	1	0	1	2.757	2
50			min	-4446.948	2	-735.44	3	0	1	0	1	0	1	-1.435	3
51		7	max	2026.075	3	1708.748	2	0	1	0	1	0	1	1.696	2
52			min	-4447.54	2	-736.66	3	0	1	0	1	0	1	-.978	3
53		8	max	2025.631	3	1707.122	2	0	1	0	1	0	1	.636	2
54			min	-4448.131	2	-737.879	3	0	1	0	1	0	1	-.521	3
55		9	max	1996.875	3	269.745	3	0	1	0	1	0	1	.033	1
56			min	-4447.337	2	-258.051	2	0	1	0	1	0	1	-.283	3
57		10	max	1996.431	3	268.526	3	0	1	0	1	0	1	.183	1
58			min	-4447.929	2	-259.677	2	0	1	0	1	0	1	-.45	3
59		11	max	1995.987	3	267.306	3	0	1	0	1	0	1	.333	1
60			min	-4448.52	2	-261.303	2	0	1	0	1	0	1	-.616	3
61		12	max	1976.062	3	2295.608	3	0	1	0	1	0	1	1.019	2
62			min	-4457.641	2	-1659.216	2	0	1	0	1	0	1	-1.583	3
63		13	max	1975.618	3	2294.389	3	0	1	0	1	0	1	2.049	2
64			min	-4458.233	2	-1660.843	2	0	1	0	1	0	1	-3.007	3
65		14	max	176.928	1	1351.923	2	0	1	0	1	0	1	3.039	2
66			min	-16.276	10	-1948.724	3	0	1	0	1	0	1	-4.373	3
67		15	max	176.337	1	1350.297	2	0	1	0	1	0	1	2.201	2
68			min	-16.769	10	-1949.944	3	0	1	0	1	0	1	-3.163	3
69		16	max	175.745	1	1348.671	2	0	1	0	1	0	1	1.363	2
70			min	-17.262	10	-1951.163	3	0	1	0	1	0	1	-1.952	3
71		17	max	175.153	1	1347.045	2	0	1	0	1	0	1	.527	2
72			min	-17.755	10	-1952.383	3	0	1	0	1	0	1	-.741	3
73		18	max	.76	4	2.087	4	0	1	0	1	0	1	0	4
74			min	.179	15	.491	15	0	1	0	1	0	1	0	15
75		19	max	0	1	.003	2	0	1	0	1	0	1	0	1
76			min	0	1	-.008	3	0	1	0	1	0	1	0	1
77	M7	1	max	0	1	.006	2	0	1	0	1	0	1	0	1
78			min	0	1	-.002	3	0	3	0	1	0	1	0	1
79		2	max	-.179	15	-.49	15	0	1	0	1	0	1	0	4
80			min	-.76	4	-2.086	4	0	3	0	1	0	3	0	15
81		3	max	-.865	12	333.753	3	115.86	1	.192	2	.008	3	.32	2
82			min	-149.745	1	-722.52	2	-15.378	3	-.069	3	-.181	1	-.147	3
83		4	max	-1.161	12	332.533	3	115.86	1	.192	2	-.001	12	.768	2
84			min	-150.337	1	-724.146	2	-15.378	3	-.069	3	-.109	1	-.354	3
85		5	max	-1.457	12	331.314	3	115.86	1	.192	2	-.001	15	1.218	2
86			min	-150.929	1	-725.772	2	-15.378	3	-.069	3	-.037	1	-.56	3
87		6	max	639.581	3	614.433	2	148.385	1	.028	2	.033	3	1.177	2
88			min	-1772.602	2	-186.387	3	-32.248	3	0	15	-.079	2	-.575	3
89		7	max	639.137	3	612.807	2	148.385	1	.028	2	.021	1	.796	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
90			min	-1773.194	2	-187.607	3	-32.248	3	0	15	0	10	-.459	3
91		8	max	638.694	3	611.181	2	148.385	1	.028	2	.113	1	.416	2
92			min	-1773.785	2	-188.826	3	-32.248	3	0	15	-.007	3	-.343	3
93		9	max	639.576	3	94.757	3	169.406	1	.146	2	-.002	15	.193	2
94			min	-1868.106	2	-42.329	2	-41.813	3	.002	15	-.075	1	-.291	3
95		10	max	639.132	3	93.538	3	169.406	1	.146	2	.033	2	.22	2
96			min	-1868.698	2	-43.955	2	-41.813	3	.002	15	-.035	3	-.35	3
97		11	max	638.689	3	92.318	3	169.406	1	.146	2	.135	1	.247	2
98			min	-1869.29	2	-45.581	2	-41.813	3	.002	15	-.061	3	-.408	3
99		12	max	635.156	3	790.56	3	156.25	3	.202	2	-.003	15	.46	2
100			min	-1958.652	2	-485.586	2	-39.721	2	-.217	3	-.097	1	-.744	3
101		13	max	634.712	3	789.34	3	156.25	3	.202	2	.089	3	.761	2
102			min	-1959.244	2	-487.212	2	-39.721	2	-.217	3	-.104	1	-1.234	3
103		14	max	151.304	1	462.159	2	100.379	1	.294	3	.003	1	1.051	2
104			min	.938	3	-738.569	3	-8.549	3	-.133	2	-.002	3	-1.703	3
105		15	max	150.712	1	460.532	2	100.379	1	.294	3	.065	1	.765	2
106			min	.494	3	-739.789	3	-8.549	3	-.133	2	-.007	3	-1.244	3
107		16	max	150.12	1	458.906	2	100.379	1	.294	3	.128	1	.48	2
108			min	.05	3	-741.008	3	-8.549	3	-.133	2	-.012	3	-.784	3
109		17	max	149.528	1	457.28	2	100.379	1	.294	3	.19	1	.195	2
110			min	-.394	3	-742.228	3	-8.549	3	-.133	2	-.017	3	-.324	3
111		18	max	.76	4	2.087	4	0	5	0	1	0	1	0	4
112			min	.179	15	.491	15	0	1	0	1	0	15	0	15
113		19	max	0	1	0	2	0	5	0	1	0	1	0	1
114			min	0	1	-.003	3	0	1	0	1	0	1	0	1
115	M10	1	max	100.379	1	453.994	2	1.279	3	.01	1	.231	1	.133	2
116			min	-8.549	3	-744.633	3	-148.583	1	-.024	3	-.021	3	-.294	3
117		2	max	100.379	1	328.903	2	2.704	3	.01	1	.125	1	.211	3
118			min	-8.549	3	-553.327	3	-122.435	1	-.024	3	-.019	3	-.172	2
119		3	max	100.379	1	203.812	2	4.13	3	.01	1	.061	2	.567	3
120			min	-8.549	3	-362.021	3	-96.287	1	-.024	3	-.017	3	-.379	2
121		4	max	100.379	1	78.721	2	5.555	3	.01	1	.015	2	.774	3
122			min	-8.549	3	-170.716	3	-70.139	1	-.024	3	-.026	9	-.489	2
123		5	max	100.379	1	20.59	3	6.981	3	.01	1	-.003	15	.833	3
124			min	-8.549	3	-46.37	2	-43.992	1	-.024	3	-.069	1	-.502	2
125		6	max	100.379	1	211.896	3	8.406	3	.01	1	-.001	12	.742	3
126			min	-8.549	3	-171.461	2	-32.688	2	-.024	3	-.093	1	-.417	2
127		7	max	100.379	1	403.202	3	15.886	9	.01	1	.005	3	.503	3
128			min	-8.549	3	-296.552	2	-22.351	2	-.024	3	-.097	1	-.235	2
129		8	max	100.379	1	594.507	3	34.451	1	.01	1	.013	3	.115	3
130			min	-8.549	3	-421.643	2	-14.673	10	-.024	3	-.086	2	0	15
131		9	max	100.379	1	785.813	3	60.599	1	.01	1	.023	3	.421	2
132			min	-8.549	3	-546.734	2	-12.047	10	-.024	3	-.092	2	-.422	3
133		10	max	100.379	1	671.825	2	9.421	10	.024	3	.048	9	.895	2
134			min	-8.549	3	-977.119	3	-86.747	1	0	15	-.089	2	-1.107	3
135		11	max	100.379	1	546.734	2	12.047	10	.024	3	.023	3	.421	2
136			min	-8.549	3	-785.813	3	-60.599	1	-.01	1	-.092	2	-.422	3
137		12	max	100.379	1	421.643	2	14.673	10	.024	3	.013	3	.115	3
138			min	-8.549	3	-594.507	3	-34.451	1	-.01	1	-.086	2	0	15
139		13	max	100.379	1	296.552	2	22.351	2	.024	3	.005	3	.503	3
140			min	-8.549	3	-403.202	3	-15.886	9	-.01	1	-.097	1	-.235	2
141		14	max	100.379	1	171.461	2	32.688	2	.024	3	-.001	12	.742	3
142			min	-8.549	3	-211.896	3	-8.406	3	-.01	1	-.093	1	-.417	2
143		15	max	100.379	1	46.37	2	43.992	1	.024	3	-.003	15	.833	3
144			min	-8.549	3	-20.59	3	-6.981	3	-.01	1	-.069	1	-.502	2
145		16	max	100.379	1	170.716	3	70.139	1	.024	3	.015	2	.774	3
146			min	-8.549	3	-78.721	2	-5.555	3	-.01	1	-.026	9	-.489	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
147		17	max	100.379	1	362.021	3	96.287	1	.024	3	.061	2	.567	3
148			min	-8.549	3	-203.812	2	-4.13	3	-.01	1	-.017	3	-.379	2
149		18	max	100.379	1	553.327	3	122.435	1	.024	3	.125	1	.211	3
150			min	-8.549	3	-328.903	2	-2.704	3	-.01	1	-.019	3	-.172	2
151		19	max	100.379	1	744.633	3	148.583	1	.024	3	.231	1	.133	2
152			min	-8.549	3	-453.994	2	-1.279	3	-.01	1	-.021	3	-.294	3
153	M11	1	max	181.089	1	435.344	2	-2.269	12	.002	3	.266	1	.076	1
154			min	-197.911	3	-701.406	3	-156.168	1	-.01	2	0	3	-.275	3
155		2	max	181.089	1	310.253	2	-1.318	12	.002	3	.154	1	.196	3
156			min	-197.911	3	-510.1	3	-130.02	1	-.01	2	-.002	3	-.234	2
157		3	max	181.089	1	185.162	2	-.31	3	.002	3	.075	2	.518	3
158			min	-197.911	3	-318.795	3	-103.873	1	-.01	2	-.003	3	-.427	2
159		4	max	181.089	1	62.01	1	1.115	3	.002	3	.026	2	.692	3
160			min	-197.911	3	-127.489	3	-77.725	1	-.01	2	-.017	9	-.522	2
161		5	max	181.089	1	63.817	3	2.541	3	.002	3	0	10	.717	3
162			min	-197.911	3	-65.02	2	-51.577	1	-.01	2	-.058	1	-.52	2
163		6	max	181.089	1	255.122	3	3.966	3	.002	3	.002	3	.593	3
164			min	-197.911	3	-190.111	2	-37.525	2	-.01	2	-.088	1	-.421	2
165		7	max	181.089	1	446.428	3	11.715	9	.002	3	.005	3	.32	3
166			min	-197.911	3	-315.202	2	-27.188	2	-.01	2	-.097	1	-.224	2
167		8	max	181.089	1	637.734	3	28.714	9	.002	3	.01	3	.07	2
168			min	-197.911	3	-440.293	2	-16.85	2	-.01	2	-.091	2	-.102	3
169		9	max	181.089	1	829.04	3	53.013	1	.002	3	.016	3	.461	2
170			min	-197.911	3	-565.384	2	-14.086	10	-.01	2	-.1	2	-.672	3
171		10	max	181.089	1	-14.223	15	79.161	1	.01	2	.038	9	.949	2
172			min	-197.911	3	-1020.345	3	-11.46	10	0	15	-.101	2	-1.391	3
173		11	max	181.089	1	565.384	2	14.086	10	.01	2	.016	3	.461	2
174			min	-197.911	3	-829.04	3	-53.013	1	-.002	3	-.1	2	-.672	3
175		12	max	181.089	1	440.293	2	16.85	2	.01	2	.01	3	.07	2
176			min	-197.911	3	-637.734	3	-28.714	9	-.002	3	-.091	2	-.102	3
177		13	max	181.089	1	315.202	2	27.188	2	.01	2	.005	3	.32	3
178			min	-197.911	3	-446.428	3	-11.715	9	-.002	3	-.097	1	-.224	2
179		14	max	181.089	1	190.111	2	37.525	2	.01	2	.002	3	.593	3
180			min	-197.911	3	-255.122	3	-3.966	3	-.002	3	-.088	1	-.421	2
181		15	max	181.089	1	65.02	2	51.577	1	.01	2	0	10	.717	3
182			min	-197.911	3	-63.817	3	-2.541	3	-.002	3	-.058	1	-.52	2
183		16	max	181.089	1	127.489	3	77.725	1	.01	2	.026	2	.692	3
184			min	-197.911	3	-62.01	1	-1.115	3	-.002	3	-.017	9	-.522	2
185		17	max	181.089	1	318.795	3	103.873	1	.01	2	.075	2	.518	3
186			min	-197.911	3	-185.162	2	.31	3	-.002	3	-.003	3	-.427	2
187		18	max	181.089	1	510.1	3	130.02	1	.01	2	.154	1	.196	3
188			min	-197.911	3	-310.253	2	1.318	12	-.002	3	-.002	3	-.234	2
189		19	max	181.089	1	701.406	3	156.168	1	.01	2	.266	1	.076	1
190			min	-197.911	3	-435.344	2	2.269	12	-.002	3	0	3	-.275	3
191	M12	1	max	9.653	3	648.552	2	1.33	3	.003	3	.284	1	.119	2
192			min	-20.326	1	-286.056	3	-160.314	1	-.009	2	-.02	3	.001	15
193		2	max	9.653	3	468.209	2	2.756	3	.003	3	.17	1	.243	3
194			min	-20.326	1	-197.887	3	-134.166	1	-.009	2	-.019	3	-.316	2
195		3	max	9.653	3	287.866	2	4.181	3	.003	3	.089	2	.362	3
196			min	-20.326	1	-109.718	3	-108.018	1	-.009	2	-.016	3	-.61	2
197		4	max	9.653	3	107.523	2	5.607	3	.003	3	.036	2	.413	3
198			min	-20.326	1	-21.55	3	-81.871	1	-.009	2	-.013	9	-.763	2
199		5	max	9.653	3	66.619	3	7.032	3	.003	3	.003	10	.396	3
200			min	-20.326	1	-72.821	2	-55.723	1	-.009	2	-.052	1	-.777	2
201		6	max	9.653	3	154.788	3	8.458	3	.003	3	-.001	12	.31	3
202			min	-20.326	1	-253.164	2	-42.054	2	-.009	2	-.085	1	-.65	2
203		7	max	9.653	3	242.956	3	10.19	9	.003	3	.006	3	.155	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
204			min	-20.326	1	-433.507	2	-31.717	2	-.009	2	-.098	1	-.383	2
205		8	max	9.653	3	331.125	3	27.188	9	.003	3	.014	3	.024	2
206			min	-20.326	1	-613.85	2	-21.38	2	-.009	2	-.095	2	-.068	3
207		9	max	9.653	3	419.293	3	48.868	1	.003	3	.023	3	.572	2
208			min	-20.326	1	-794.193	2	-16.572	10	-.009	2	-.107	2	-.36	3
209		10	max	9.653	3	-14.184	15	75.015	1	.009	2	.034	9	1.26	2
210			min	-20.326	1	-974.536	2	-14.16	3	0	15	-.112	2	-.721	3
211		11	max	9.653	3	794.193	2	16.572	10	.009	2	.023	3	.572	2
212			min	-20.326	1	-419.293	3	-48.868	1	-.003	3	-.107	2	-.36	3
213		12	max	9.653	3	613.85	2	21.38	2	.009	2	.014	3	.024	2
214			min	-20.326	1	-331.125	3	-27.188	9	-.003	3	-.095	2	-.068	3
215		13	max	9.653	3	433.507	2	31.717	2	.009	2	.006	3	.155	3
216			min	-20.326	1	-242.956	3	-10.19	9	-.003	3	-.098	1	-.383	2
217		14	max	9.653	3	253.164	2	42.054	2	.009	2	-.001	12	.31	3
218			min	-20.326	1	-154.788	3	-8.458	3	-.003	3	-.085	1	-.65	2
219		15	max	9.653	3	72.821	2	55.723	1	.009	2	.003	10	.396	3
220			min	-20.326	1	-66.619	3	-7.032	3	-.003	3	-.052	1	-.777	2
221		16	max	9.653	3	21.55	3	81.871	1	.009	2	.036	2	.413	3
222			min	-20.326	1	-107.523	2	-5.607	3	-.003	3	-.013	9	-.763	2
223		17	max	9.653	3	109.718	3	108.018	1	.009	2	.089	2	.362	3
224			min	-20.326	1	-287.866	2	-4.181	3	-.003	3	-.016	3	-.61	2
225		18	max	9.653	3	197.887	3	134.166	1	.009	2	.17	1	.243	3
226			min	-20.326	1	-468.209	2	-2.756	3	-.003	3	-.019	3	-.316	2
227		19	max	9.653	3	286.056	3	160.314	1	.009	2	.284	1	.119	2
228			min	-20.326	1	-648.552	2	-1.33	3	-.003	3	-.02	3	.001	15
229	M13	1	max	15.378	3	719.715	2	.015	3	.012	3	.227	1	.192	2
230			min	-115.796	1	-336.238	3	-148.277	1	-.026	2	-.014	3	-.069	3
231		2	max	15.378	3	539.372	2	1.441	3	.012	3	.122	1	.158	3
232			min	-115.796	1	-248.069	3	-122.129	1	-.026	2	-.013	3	-.298	2
233		3	max	15.378	3	359.029	2	2.866	3	.012	3	.058	2	.317	3
234			min	-115.796	1	-159.901	3	-95.982	1	-.026	2	-.012	3	-.647	2
235		4	max	15.378	3	178.686	2	4.292	3	.012	3	.014	10	.407	3
236			min	-115.796	1	-71.732	3	-69.834	1	-.026	2	-.027	9	-.856	2
237		5	max	15.378	3	16.437	3	5.717	3	.012	3	-.003	15	.428	3
238			min	-115.796	1	-2.125	10	-43.686	1	-.026	2	-.071	1	-.925	2
239		6	max	15.378	3	104.605	3	7.143	3	.012	3	0	3	.381	3
240			min	-115.796	1	-182.001	2	-32.572	2	-.026	2	-.095	1	-.854	2
241		7	max	15.378	3	192.774	3	16.089	9	.012	3	.006	3	.265	3
242			min	-115.796	1	-362.344	2	-22.235	2	-.026	2	-.098	1	-.642	2
243		8	max	15.378	3	280.942	3	34.757	1	.012	3	.013	3	.081	3
244			min	-115.796	1	-542.687	2	-14.641	10	-.026	2	-.088	2	-.29	2
245		9	max	15.378	3	369.111	3	60.904	1	.012	3	.022	3	.202	2
246			min	-115.796	1	-723.03	2	-12.015	10	-.026	2	-.094	2	-.172	3
247		10	max	15.378	3	-12.84	15	87.052	1	.026	2	.048	9	.835	2
248			min	-115.796	1	-903.373	2	-12.845	3	0	15	-.091	2	-.493	3
249		11	max	15.378	3	723.03	2	12.015	10	.026	2	.022	3	.202	2
250			min	-115.796	1	-369.111	3	-60.904	1	-.012	3	-.094	2	-.172	3
251		12	max	15.378	3	542.687	2	14.641	10	.026	2	.013	3	.081	3
252			min	-115.796	1	-280.942	3	-34.757	1	-.012	3	-.088	2	-.29	2
253		13	max	15.378	3	362.344	2	22.235	2	.026	2	.006	3	.265	3
254			min	-115.796	1	-192.774	3	-16.089	9	-.012	3	-.098	1	-.642	2
255		14	max	15.378	3	182.001	2	32.572	2	.026	2	0	3	.381	3
256			min	-115.796	1	-104.605	3	-7.143	3	-.012	3	-.095	1	-.854	2
257		15	max	15.378	3	2.125	10	43.686	1	.026	2	-.003	15	.428	3
258			min	-115.796	1	-16.437	3	-5.717	3	-.012	3	-.071	1	-.925	2
259		16	max	15.378	3	71.732	3	69.834	1	.026	2	.014	10	.407	3
260			min	-115.796	1	-178.686	2	-4.292	3	-.012	3	-.027	9	-.856	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
261		17	max	15.378	3	159.901	3	95.982	1	.026	2	.058	2	.317	3
262			min	-115.796	1	-359.029	2	-2.866	3	-.012	3	-.012	3	-.647	2
263		18	max	15.378	3	248.069	3	122.129	1	.026	2	.122	1	.158	3
264			min	-115.796	1	-539.372	2	-1.441	3	-.012	3	-.013	3	-.298	2
265		19	max	15.378	3	336.238	3	148.277	1	.026	2	.227	1	.192	2
266			min	-115.796	1	-719.715	2	-.015	3	-.012	3	-.014	3	-.069	3
267	M2	1	max	2321.87	2	707.691	3	155.471	2	.002	3	.19	3	5.438	1
268			min	-1883.61	3	-439.71	2	-181.277	3	-.004	2	-.163	1	.153	15
269		2	max	2319.609	2	707.691	3	155.471	2	.002	3	.145	3	5.463	1
270			min	-1885.305	3	-439.71	2	-181.277	3	-.004	2	-.127	1	.152	15
271		3	max	2317.349	2	707.691	3	155.471	2	.002	3	.1	3	5.488	1
272			min	-1887.001	3	-439.71	2	-181.277	3	-.004	2	-.091	1	.055	12
273		4	max	2315.088	2	707.691	3	155.471	2	.002	3	.055	3	5.539	2
274			min	-1888.696	3	-439.71	2	-181.277	3	-.004	2	-.055	1	-.103	3
275		5	max	1632.277	2	1604.512	2	116.573	2	.001	2	.03	3	5.577	2
276			min	-1628.999	3	-72.265	3	-164.925	3	0	3	-.055	1	-.251	3
277		6	max	1630.017	2	1604.512	2	116.573	2	.001	2	0	15	5.178	2
278			min	-1630.695	3	-72.265	3	-164.925	3	0	3	-.027	1	-.233	3
279		7	max	1627.756	2	1604.512	2	116.573	2	.001	2	.009	2	4.78	2
280			min	-1632.39	3	-72.265	3	-164.925	3	0	3	-.051	3	-.215	3
281		8	max	1625.496	2	1604.512	2	116.573	2	.001	2	.038	2	4.382	2
282			min	-1634.086	3	-72.265	3	-164.925	3	0	3	-.092	3	-.197	3
283		9	max	1623.235	2	1604.512	2	116.573	2	.001	2	.066	2	3.983	2
284			min	-1635.781	3	-72.265	3	-164.925	3	0	3	-.133	3	-.179	3
285		10	max	1620.974	2	1604.512	2	116.573	2	.001	2	.095	2	3.585	2
286			min	-1637.477	3	-72.265	3	-164.925	3	0	3	-.174	3	-.161	3
287		11	max	1618.714	2	1604.512	2	116.573	2	.001	2	.124	2	3.187	2
288			min	-1639.172	3	-72.265	3	-164.925	3	0	3	-.215	3	-.144	3
289		12	max	1616.453	2	1604.512	2	116.573	2	.001	2	.153	2	2.788	2
290			min	-1640.867	3	-72.265	3	-164.925	3	0	3	-.256	3	-.126	3
291		13	max	1614.193	2	1604.512	2	116.573	2	.001	2	.182	2	2.39	2
292			min	-1642.563	3	-72.265	3	-164.925	3	0	3	-.297	3	-.108	3
293		14	max	1611.932	2	1604.512	2	116.573	2	.001	2	.211	2	1.992	2
294			min	-1644.258	3	-72.265	3	-164.925	3	0	3	-.338	3	-.09	3
295		15	max	1609.671	2	1604.512	2	116.573	2	.001	2	.24	2	1.593	2
296			min	-1645.954	3	-72.265	3	-164.925	3	0	3	-.379	3	-.072	3
297		16	max	1607.411	2	1604.512	2	116.573	2	.001	2	.269	2	1.195	2
298			min	-1647.649	3	-72.265	3	-164.925	3	0	3	-.42	3	-.054	3
299		17	max	1605.15	2	1604.512	2	116.573	2	.001	2	.298	2	.797	2
300			min	-1649.345	3	-72.265	3	-164.925	3	0	3	-.461	3	-.036	3
301		18	max	1602.89	2	1604.512	2	116.573	2	.001	2	.327	2	.398	2
302			min	-1651.04	3	-72.265	3	-164.925	3	0	3	-.502	3	-.018	3
303		19	max	1600.629	2	1604.512	2	116.573	2	.001	2	.356	2	0	1
304			min	-1652.736	3	-72.265	3	-164.925	3	0	3	-.543	3	0	1
305	M5	1	max	6182.328	2	2121.352	3	0	1	0	1	0	1	9.411	1
306			min	-5472.748	3	-2163.846	2	0	1	0	1	0	1	.241	15
307		2	max	6180.068	2	2121.352	3	0	1	0	1	0	1	9.742	2
308			min	-5474.443	3	-2163.846	2	0	1	0	1	0	1	.141	12
309		3	max	6177.807	2	2121.352	3	0	1	0	1	0	1	10.279	2
310			min	-5476.139	3	-2163.846	2	0	1	0	1	0	1	-.321	3
311		4	max	6175.547	2	2121.352	3	0	1	0	1	0	1	10.817	2
312			min	-5477.834	3	-2163.846	2	0	1	0	1	0	1	-.848	3
313		5	max	4430.017	2	3212.761	2	0	1	0	1	0	1	11.166	2
314			min	-4633.828	3	-370.475	3	0	1	0	1	0	1	-1.288	3
315		6	max	4427.756	2	3212.761	2	0	1	0	1	0	1	10.369	2
316			min	-4635.524	3	-370.475	3	0	1	0	1	0	1	-1.196	3
317		7	max	4425.496	2	3212.761	2	0	1	0	1	0	1	9.571	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
318			min	-4637.219	3	-370.475	3	0	1	0	1	0	1	-1.104	3
319		8	max	4423.235	2	3212.761	2	0	1	0	1	0	1	8.774	2
320			min	-4638.915	3	-370.475	3	0	1	0	1	0	1	-1.012	3
321		9	max	4420.974	2	3212.761	2	0	1	0	1	0	1	7.976	2
322			min	-4640.61	3	-370.475	3	0	1	0	1	0	1	-.92	3
323		10	max	4418.714	2	3212.761	2	0	1	0	1	0	1	7.178	2
324			min	-4642.306	3	-370.475	3	0	1	0	1	0	1	-.828	3
325		11	max	4416.453	2	3212.761	2	0	1	0	1	0	1	6.381	2
326			min	-4644.001	3	-370.475	3	0	1	0	1	0	1	-.736	3
327		12	max	4414.193	2	3212.761	2	0	1	0	1	0	1	5.583	2
328			min	-4645.697	3	-370.475	3	0	1	0	1	0	1	-.644	3
329		13	max	4411.932	2	3212.761	2	0	1	0	1	0	1	4.786	2
330			min	-4647.392	3	-370.475	3	0	1	0	1	0	1	-.552	3
331		14	max	4409.671	2	3212.761	2	0	1	0	1	0	1	3.988	2
332			min	-4649.087	3	-370.475	3	0	1	0	1	0	1	-.46	3
333		15	max	4407.411	2	3212.761	2	0	1	0	1	0	1	3.19	2
334			min	-4650.783	3	-370.475	3	0	1	0	1	0	1	-.368	3
335		16	max	4405.15	2	3212.761	2	0	1	0	1	0	1	2.393	2
336			min	-4652.478	3	-370.475	3	0	1	0	1	0	1	-.276	3
337		17	max	4402.89	2	3212.761	2	0	1	0	1	0	1	1.595	2
338			min	-4654.174	3	-370.475	3	0	1	0	1	0	1	-.184	3
339		18	max	4400.629	2	3212.761	2	0	1	0	1	0	1	.798	2
340			min	-4655.869	3	-370.475	3	0	1	0	1	0	1	-.092	3
341		19	max	4398.368	2	3212.761	2	0	1	0	1	0	1	0	1
342			min	-4657.565	3	-370.475	3	0	1	0	1	0	1	0	1
343	M8	1	max	2321.87	2	707.691	3	181.277	3	.004	2	.163	1	5.438	1
344			min	-1883.61	3	-439.71	2	-155.471	2	-.002	3	-.19	3	.153	15
345		2	max	2319.609	2	707.691	3	181.277	3	.004	2	.127	1	5.463	1
346			min	-1885.305	3	-439.71	2	-155.471	2	-.002	3	-.145	3	.152	15
347		3	max	2317.349	2	707.691	3	181.277	3	.004	2	.091	1	5.488	1
348			min	-1887.001	3	-439.71	2	-155.471	2	-.002	3	-.1	3	.055	12
349		4	max	2315.088	2	707.691	3	181.277	3	.004	2	.055	1	5.539	2
350			min	-1888.696	3	-439.71	2	-155.471	2	-.002	3	-.055	3	-.103	3
351		5	max	1632.277	2	1604.512	2	164.925	3	0	3	.055	1	5.577	2
352			min	-1628.999	3	-72.265	3	-116.573	2	-.001	2	-.03	3	-.251	3
353		6	max	1630.017	2	1604.512	2	164.925	3	0	3	.027	1	5.178	2
354			min	-1630.695	3	-72.265	3	-116.573	2	-.001	2	0	15	-.233	3
355		7	max	1627.756	2	1604.512	2	164.925	3	0	3	.051	3	4.78	2
356			min	-1632.39	3	-72.265	3	-116.573	2	-.001	2	-.009	2	-.215	3
357		8	max	1625.496	2	1604.512	2	164.925	3	0	3	.092	3	4.382	2
358			min	-1634.086	3	-72.265	3	-116.573	2	-.001	2	-.038	2	-.197	3
359		9	max	1623.235	2	1604.512	2	164.925	3	0	3	.133	3	3.983	2
360			min	-1635.781	3	-72.265	3	-116.573	2	-.001	2	-.066	2	-.179	3
361		10	max	1620.974	2	1604.512	2	164.925	3	0	3	.174	3	3.585	2
362			min	-1637.477	3	-72.265	3	-116.573	2	-.001	2	-.095	2	-.161	3
363		11	max	1618.714	2	1604.512	2	164.925	3	0	3	.215	3	3.187	2
364			min	-1639.172	3	-72.265	3	-116.573	2	-.001	2	-.124	2	-.144	3
365		12	max	1616.453	2	1604.512	2	164.925	3	0	3	.256	3	2.788	2
366			min	-1640.867	3	-72.265	3	-116.573	2	-.001	2	-.153	2	-.126	3
367		13	max	1614.193	2	1604.512	2	164.925	3	0	3	.297	3	2.39	2
368			min	-1642.563	3	-72.265	3	-116.573	2	-.001	2	-.182	2	-.108	3
369		14	max	1611.932	2	1604.512	2	164.925	3	0	3	.338	3	1.992	2
370			min	-1644.258	3	-72.265	3	-116.573	2	-.001	2	-.211	2	-.09	3
371		15	max	1609.671	2	1604.512	2	164.925	3	0	3	.379	3	1.593	2
372			min	-1645.954	3	-72.265	3	-116.573	2	-.001	2	-.24	2	-.072	3
373		16	max	1607.411	2	1604.512	2	164.925	3	0	3	.42	3	1.195	2
374			min	-1647.649	3	-72.265	3	-116.573	2	-.001	2	-.269	2	-.054	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
375		17	max	1605.15	2	1604.512	2	164.925	3	0	3	.461	3	.797	2
376			min	-1649.345	3	-72.265	3	-116.573	2	-.001	2	-.298	2	-.036	3
377		18	max	1602.89	2	1604.512	2	164.925	3	0	3	.502	3	.398	2
378			min	-1651.04	3	-72.265	3	-116.573	2	-.001	2	-.327	2	-.018	3
379		19	max	1600.629	2	1604.512	2	164.925	3	0	3	.543	3	0	1
380			min	-1652.736	3	-72.265	3	-116.573	2	-.001	2	-.356	2	0	1
381	M3	1	max	2148.728	2	4.757	4	38.345	2	.02	3	.008	2	0	1
382			min	-822.872	3	1.118	15	-16.858	3	-.042	2	-.004	3	0	1
383		2	max	2148.589	2	4.229	4	38.345	2	.02	3	.019	2	0	15
384			min	-822.977	3	.994	15	-16.858	3	-.042	2	-.009	3	-.001	4
385		3	max	2148.449	2	3.7	4	38.345	2	.02	3	.03	2	0	15
386			min	-823.081	3	.87	15	-16.858	3	-.042	2	-.014	3	-.002	4
387		4	max	2148.31	2	3.171	4	38.345	2	.02	3	.042	2	0	15
388			min	-823.186	3	.745	15	-16.858	3	-.042	2	-.019	3	-.003	4
389		5	max	2148.17	2	2.643	4	38.345	2	.02	3	.053	2	-.001	15
390			min	-823.29	3	.621	15	-16.858	3	-.042	2	-.024	3	-.004	4
391		6	max	2148.031	2	2.114	4	38.345	2	.02	3	.064	2	-.001	15
392			min	-823.395	3	.497	15	-16.858	3	-.042	2	-.028	3	-.005	4
393		7	max	2147.891	2	1.586	4	38.345	2	.02	3	.075	2	-.001	15
394			min	-823.5	3	.373	15	-16.858	3	-.042	2	-.033	3	-.006	4
395		8	max	2147.752	2	1.057	4	38.345	2	.02	3	.087	2	-.001	15
396			min	-823.604	3	.248	15	-16.858	3	-.042	2	-.038	3	-.006	4
397		9	max	2147.613	2	.529	4	38.345	2	.02	3	.098	2	-.001	15
398			min	-823.709	3	.124	15	-16.858	3	-.042	2	-.043	3	-.006	4
399		10	max	2147.473	2	0	1	38.345	2	.02	3	.109	2	-.001	15
400			min	-823.813	3	0	1	-16.858	3	-.042	2	-.048	3	-.006	4
401		11	max	2147.334	2	-.124	15	38.345	2	.02	3	.12	2	-.001	15
402			min	-823.918	3	-.529	4	-16.858	3	-.042	2	-.053	3	-.006	4
403		12	max	2147.194	2	-.248	15	38.345	2	.02	3	.132	2	-.001	15
404			min	-824.022	3	-1.057	4	-16.858	3	-.042	2	-.058	3	-.006	4
405		13	max	2147.055	2	-.373	15	38.345	2	.02	3	.143	2	-.001	15
406			min	-824.127	3	-1.586	4	-16.858	3	-.042	2	-.063	3	-.006	4
407		14	max	2146.916	2	-.497	15	38.345	2	.02	3	.154	2	-.001	15
408			min	-824.231	3	-2.114	4	-16.858	3	-.042	2	-.068	3	-.005	4
409		15	max	2146.776	2	-.621	15	38.345	2	.02	3	.165	2	-.001	15
410			min	-824.336	3	-2.643	4	-16.858	3	-.042	2	-.073	3	-.004	4
411		16	max	2146.637	2	-.745	15	38.345	2	.02	3	.176	2	0	15
412			min	-824.441	3	-3.171	4	-16.858	3	-.042	2	-.078	3	-.003	4
413		17	max	2146.497	2	-.87	15	38.345	2	.02	3	.188	2	0	15
414			min	-824.545	3	-3.7	4	-16.858	3	-.042	2	-.083	3	-.002	4
415		18	max	2146.358	2	-.994	15	38.345	2	.02	3	.199	2	0	15
416			min	-824.65	3	-4.229	4	-16.858	3	-.042	2	-.088	3	-.001	4
417		19	max	2146.219	2	-1.118	15	38.345	2	.02	3	.21	2	0	1
418			min	-824.754	3	-4.757	4	-16.858	3	-.042	2	-.093	3	0	1
419	M6	1	max	5619.583	2	4.757	4	0	1	0	1	0	1	0	1
420			min	-2635.579	3	1.118	15	0	1	0	1	0	1	0	1
421		2	max	5619.443	2	4.229	4	0	1	0	1	0	1	0	15
422			min	-2635.683	3	.994	15	0	1	0	1	0	1	-.001	4
423		3	max	5619.304	2	3.7	4	0	1	0	1	0	1	0	15
424			min	-2635.788	3	.87	15	0	1	0	1	0	1	-.002	4
425		4	max	5619.165	2	3.171	4	0	1	0	1	0	1	0	15
426			min	-2635.892	3	.745	15	0	1	0	1	0	1	-.003	4
427		5	max	5619.025	2	2.643	4	0	1	0	1	0	1	-.001	15
428			min	-2635.997	3	.621	15	0	1	0	1	0	1	-.004	4
429		6	max	5618.886	2	2.114	4	0	1	0	1	0	1	-.001	15
430			min	-2636.101	3	.497	15	0	1	0	1	0	1	-.005	4
431		7	max	5618.746	2	1.586	4	0	1	0	1	0	1	-.001	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
432			min	-2636.206	3	.373	15	0	1	0	1	0	1	-.006	4
433		8	max	5618.607	2	1.057	4	0	1	0	1	0	1	-.001	15
434			min	-2636.31	3	.248	15	0	1	0	1	0	1	-.006	4
435		9	max	5618.467	2	.529	4	0	1	0	1	0	1	-.001	15
436			min	-2636.415	3	.124	15	0	1	0	1	0	1	-.006	4
437		10	max	5618.328	2	0	1	0	1	0	1	0	1	-.001	15
438			min	-2636.52	3	0	1	0	1	0	1	0	1	-.006	4
439		11	max	5618.189	2	-.124	15	0	1	0	1	0	1	-.001	15
440			min	-2636.624	3	-.529	4	0	1	0	1	0	1	-.006	4
441		12	max	5618.049	2	-.248	15	0	1	0	1	0	1	-.001	15
442			min	-2636.729	3	-1.057	4	0	1	0	1	0	1	-.006	4
443		13	max	5617.91	2	-.373	15	0	1	0	1	0	1	-.001	15
444			min	-2636.833	3	-1.586	4	0	1	0	1	0	1	-.006	4
445		14	max	5617.77	2	-.497	15	0	1	0	1	0	1	-.001	15
446			min	-2636.938	3	-2.114	4	0	1	0	1	0	1	-.005	4
447		15	max	5617.631	2	-.621	15	0	1	0	1	0	1	-.001	15
448			min	-2637.042	3	-2.643	4	0	1	0	1	0	1	-.004	4
449		16	max	5617.492	2	-.745	15	0	1	0	1	0	1	0	15
450			min	-2637.147	3	-3.171	4	0	1	0	1	0	1	-.003	4
451		17	max	5617.352	2	-.87	15	0	1	0	1	0	1	0	15
452			min	-2637.251	3	-3.7	4	0	1	0	1	0	1	-.002	4
453		18	max	5617.213	2	-.994	15	0	1	0	1	0	1	0	15
454			min	-2637.356	3	-4.229	4	0	1	0	1	0	1	-.001	4
455		19	max	5617.073	2	-1.118	15	0	1	0	1	0	1	0	1
456			min	-2637.461	3	-4.757	4	0	1	0	1	0	1	0	1
457	M9	1	max	2148.728	2	4.757	4	16.858	3	.042	2	.004	3	0	1
458			min	-822.872	3	1.118	15	-38.345	2	-.02	3	-.008	2	0	1
459		2	max	2148.589	2	4.229	4	16.858	3	.042	2	.009	3	0	15
460			min	-822.977	3	.994	15	-38.345	2	-.02	3	-.019	2	-.001	4
461		3	max	2148.449	2	3.7	4	16.858	3	.042	2	.014	3	0	15
462			min	-823.081	3	.87	15	-38.345	2	-.02	3	-.03	2	-.002	4
463		4	max	2148.31	2	3.171	4	16.858	3	.042	2	.019	3	0	15
464			min	-823.186	3	.745	15	-38.345	2	-.02	3	-.042	2	-.003	4
465		5	max	2148.17	2	2.643	4	16.858	3	.042	2	.024	3	-.001	15
466			min	-823.29	3	.621	15	-38.345	2	-.02	3	-.053	2	-.004	4
467		6	max	2148.031	2	2.114	4	16.858	3	.042	2	.028	3	-.001	15
468			min	-823.395	3	.497	15	-38.345	2	-.02	3	-.064	2	-.005	4
469		7	max	2147.891	2	1.586	4	16.858	3	.042	2	.033	3	-.001	15
470			min	-823.5	3	.373	15	-38.345	2	-.02	3	-.075	2	-.006	4
471		8	max	2147.752	2	1.057	4	16.858	3	.042	2	.038	3	-.001	15
472			min	-823.604	3	.248	15	-38.345	2	-.02	3	-.087	2	-.006	4
473		9	max	2147.613	2	.529	4	16.858	3	.042	2	.043	3	-.001	15
474			min	-823.709	3	.124	15	-38.345	2	-.02	3	-.098	2	-.006	4
475		10	max	2147.473	2	0	1	16.858	3	.042	2	.048	3	-.001	15
476			min	-823.813	3	0	1	-38.345	2	-.02	3	-.109	2	-.006	4
477		11	max	2147.334	2	-.124	15	16.858	3	.042	2	.053	3	-.001	15
478			min	-823.918	3	-.529	4	-38.345	2	-.02	3	-.12	2	-.006	4
479		12	max	2147.194	2	-.248	15	16.858	3	.042	2	.058	3	-.001	15
480			min	-824.022	3	-1.057	4	-38.345	2	-.02	3	-.132	2	-.006	4
481		13	max	2147.055	2	-.373	15	16.858	3	.042	2	.063	3	-.001	15
482			min	-824.127	3	-1.586	4	-38.345	2	-.02	3	-.143	2	-.006	4
483		14	max	2146.916	2	-.497	15	16.858	3	.042	2	.068	3	-.001	15
484			min	-824.231	3	-2.114	4	-38.345	2	-.02	3	-.154	2	-.005	4
485		15	max	2146.776	2	-.621	15	16.858	3	.042	2	.073	3	-.001	15
486			min	-824.336	3	-2.643	4	-38.345	2	-.02	3	-.165	2	-.004	4
487		16	max	2146.637	2	-.745	15	16.858	3	.042	2	.078	3	0	15
488			min	-824.441	3	-3.171	4	-38.345	2	-.02	3	-.176	2	-.003	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
489		17	max	2146.497	2	-.87	15	16.858	3	.042	2	.083	3	0	15
490			min	-824.545	3	-3.7	4	-38.345	2	-.02	3	-.188	2	-.002	4
491		18	max	2146.358	2	-.994	15	16.858	3	.042	2	.088	3	0	15
492			min	-824.65	3	-4.229	4	-38.345	2	-.02	3	-.199	2	-.001	4
493		19	max	2146.219	2	-1.118	15	16.858	3	.042	2	.093	3	0	1
494			min	-824.754	3	-4.757	4	-38.345	2	-.02	3	-.21	2	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	.006	3	.195	3	.017	1	8.413e-3	3	NC	3	NC	3
2			min	-.233	2	-.752	2	-.001	3	-2.007e-2	2	168.576	2	4309	1
3		2	max	.006	3	.151	3	.005	1	8.413e-3	3	7886.18	15	NC	3
4			min	-.233	2	-.641	2	0	3	-2.007e-2	2	195.898	2	6932.036	1
5		3	max	.006	3	.108	3	0	3	7.869e-3	3	9147.649	15	NC	1
6			min	-.233	2	-.53	2	-.005	1	-1.857e-2	2	233.834	2	NC	1
7		4	max	.006	3	.066	3	0	3	7.035e-3	3	NC	15	NC	1
8			min	-.233	2	-.423	2	-.009	1	-1.626e-2	2	287.385	2	NC	1
9		5	max	.006	3	.03	3	.001	3	6.2e-3	3	NC	15	NC	1
10			min	-.233	2	-.327	2	-.009	1	-1.395e-2	2	362.045	2	NC	1
11		6	max	.006	3	0	3	.002	3	5.887e-3	3	NC	5	NC	1
12			min	-.233	2	-.248	2	-.008	1	-1.281e-2	2	452.665	1	NC	1
13		7	max	.005	3	-.005	15	.001	3	5.933e-3	3	NC	5	NC	1
14			min	-.232	2	-.186	2	-.004	2	-1.248e-2	2	566.492	1	NC	1
15		8	max	.005	3	-.004	15	0	3	5.98e-3	3	NC	5	NC	2
16			min	-.232	2	-.135	1	0	2	-1.214e-2	2	586.334	3	9330.742	1
17		9	max	.005	3	-.003	15	0	15	6.264e-3	3	NC	5	NC	2
18			min	-.231	2	-.09	1	0	3	-1.129e-2	2	562.714	3	9337.511	1
19		10	max	.005	3	-.001	15	0	2	6.965e-3	3	NC	5	NC	2
20			min	-.23	2	-.049	3	0	3	-9.533e-3	2	549.684	3	8970.188	1
21		11	max	.004	3	0	15	0	3	7.667e-3	3	NC	4	NC	2
22			min	-.229	2	-.05	3	0	2	-7.772e-3	2	547.873	3	9279.451	1
23		12	max	.004	3	.031	2	.004	3	6.253e-3	3	NC	2	NC	1
24			min	-.229	2	-.045	3	-.003	1	-5.579e-3	2	558.481	3	NC	1
25		13	max	.004	3	.061	2	.007	3	3.643e-3	3	NC	1	NC	1
26			min	-.228	2	-.031	3	-.004	2	-3.142e-3	2	594.991	3	NC	1
27		14	max	.004	3	.081	2	.007	3	1.169e-3	3	NC	4	NC	2
28			min	-.227	2	0	12	-.002	2	-7.939e-4	2	692.91	3	9737.626	1
29		15	max	.004	3	.088	1	.005	3	4.702e-3	3	NC	4	NC	2
30			min	-.227	2	.002	15	0	15	-2.389e-3	2	967.225	3	7235.674	1
31		16	max	.004	3	.128	3	.006	1	8.235e-3	3	NC	4	NC	3
32			min	-.227	2	.002	15	0	15	-3.985e-3	2	2015.534	3	6403.175	1
33		17	max	.004	3	.211	3	.004	1	1.177e-2	3	NC	4	NC	3
34			min	-.227	2	.002	15	0	15	-5.58e-3	2	4805.686	2	7146.007	1
35		18	max	.004	3	.298	3	0	15	1.407e-2	3	NC	1	NC	1
36			min	-.227	2	.002	15	-.004	1	-6.62e-3	2	1293.888	3	NC	1
37		19	max	.004	3	.385	3	0	15	1.407e-2	3	NC	1	NC	1
38			min	-.227	2	.002	15	-.014	1	-6.62e-3	2	703.119	3	NC	1
39	M4	1	max	.04	3	.486	3	0	1	0	1	NC	3	NC	1
40			min	-.457	2	-1.549	2	0	1	0	1	89.142	2	NC	1
41		2	max	.04	3	.386	3	0	1	0	1	5160.111	15	NC	1
42			min	-.457	2	-1.317	2	0	1	0	1	105.442	2	NC	1
43		3	max	.04	3	.285	3	0	1	0	1	6176.098	15	NC	1
44			min	-.457	2	-1.084	2	0	1	0	1	129.115	2	NC	1
45		4	max	.04	3	.189	3	0	1	0	1	7631.689	15	NC	1
46			min	-.457	2	-.859	2	0	1	0	1	164.672	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
47		5	max	.04	3	.106	3	0	1	0	1	9715.825	15	NC	1
48			min	-.457	2	-.66	2	0	1	0	1	218.04	2	NC	1
49		6	max	.039	3	.044	3	0	1	0	1	NC	15	NC	1
50			min	-.456	2	-.502	2	0	1	0	1	293.255	2	NC	1
51		7	max	.038	3	.001	3	0	1	0	1	NC	5	NC	1
52			min	-.454	2	-.384	2	0	1	0	1	276.598	3	NC	1
53		8	max	.038	3	-.007	15	0	1	0	1	NC	5	NC	1
54			min	-.452	2	-.289	2	0	1	0	1	261.194	3	NC	1
55		9	max	.037	3	-.005	15	0	1	0	1	NC	5	NC	1
56			min	-.451	2	-.202	2	0	1	0	1	250.607	3	NC	1
57		10	max	.036	3	-.002	15	0	1	0	1	NC	4	NC	1
58			min	-.449	2	-.115	2	0	1	0	1	242.437	3	NC	1
59		11	max	.035	3	0	15	0	1	0	1	NC	4	NC	1
60			min	-.447	2	-.079	3	0	1	0	1	237.373	3	NC	1
61		12	max	.035	3	.051	1	0	1	0	1	NC	5	NC	1
62			min	-.446	2	-.082	3	0	1	0	1	235.771	3	NC	1
63		13	max	.034	3	.118	2	0	1	0	1	NC	5	NC	1
64			min	-.444	2	-.065	3	0	1	0	1	243.244	3	NC	1
65		14	max	.033	3	.157	2	0	1	0	1	NC	5	NC	1
66			min	-.442	2	-.006	3	0	1	0	1	272.507	3	NC	1
67		15	max	.033	3	.155	2	0	1	0	1	NC	5	NC	1
68			min	-.442	2	.004	15	0	1	0	1	358.708	3	NC	1
69		16	max	.033	3	.274	3	0	1	0	1	NC	5	NC	1
70			min	-.442	2	.003	15	0	1	0	1	633.186	3	NC	1
71		17	max	.033	3	.463	3	0	1	0	1	NC	5	NC	1
72			min	-.442	2	.002	15	0	1	0	1	1152.692	2	NC	1
73		18	max	.033	3	.662	3	0	1	0	1	NC	4	NC	1
74			min	-.442	2	0	15	0	1	0	1	761.541	3	NC	1
75		19	max	.033	3	.86	3	0	1	0	1	NC	1	NC	1
76			min	-.442	2	-.047	1	0	1	0	1	358.338	3	NC	1
77	M7	1	max	.006	3	.195	3	.001	3	2.007e-2	2	NC	3	NC	3
78			min	-.233	2	-.752	2	-.017	1	-8.413e-3	3	168.576	2	4309	1
79		2	max	.006	3	.151	3	0	3	2.007e-2	2	7886.18	15	NC	3
80			min	-.233	2	-.641	2	-.005	1	-8.413e-3	3	195.898	2	6932.036	1
81		3	max	.006	3	.108	3	.005	1	1.857e-2	2	9147.649	15	NC	1
82			min	-.233	2	-.53	2	0	3	-7.869e-3	3	233.834	2	NC	1
83		4	max	.006	3	.066	3	.009	1	1.626e-2	2	NC	15	NC	1
84			min	-.233	2	-.423	2	0	3	-7.035e-3	3	287.385	2	NC	1
85		5	max	.006	3	.03	3	.009	1	1.395e-2	2	NC	15	NC	1
86			min	-.233	2	-.327	2	-.001	3	-6.2e-3	3	362.045	2	NC	1
87		6	max	.006	3	0	3	.008	1	1.281e-2	2	NC	5	NC	1
88			min	-.233	2	-.248	2	-.002	3	-5.887e-3	3	452.665	1	NC	1
89		7	max	.005	3	-.005	15	.004	2	1.248e-2	2	NC	5	NC	1
90			min	-.232	2	-.186	2	-.001	3	-5.933e-3	3	566.492	1	NC	1
91		8	max	.005	3	-.004	15	0	2	1.214e-2	2	NC	5	NC	2
92			min	-.232	2	-.135	1	0	3	-5.98e-3	3	586.334	3	9330.742	1
93		9	max	.005	3	-.003	15	0	3	1.129e-2	2	NC	5	NC	2
94			min	-.231	2	-.09	1	0	15	-6.264e-3	3	562.714	3	9337.511	1
95		10	max	.005	3	-.001	15	0	3	9.533e-3	2	NC	5	NC	2
96			min	-.23	2	-.049	3	0	2	-6.965e-3	3	549.684	3	8970.188	1
97		11	max	.004	3	0	15	0	2	7.772e-3	2	NC	4	NC	2
98			min	-.229	2	-.05	3	0	3	-7.667e-3	3	547.873	3	9279.451	1
99		12	max	.004	3	.031	2	.003	1	5.579e-3	2	NC	2	NC	1
100			min	-.229	2	-.045	3	-.004	3	-6.253e-3	3	558.481	3	NC	1
101		13	max	.004	3	.061	2	.004	2	3.142e-3	2	NC	1	NC	1
102			min	-.228	2	-.031	3	-.007	3	-3.643e-3	3	594.991	3	NC	1
103		14	max	.004	3	.081	2	.002	2	7.939e-4	2	NC	4	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
104			min	-.227	2	0	12	-.007	3	-1.169e-3	3	692.91	3	9737.626	1
105		15	max	.004	3	.088	1	0	15	2.389e-3	2	NC	4	NC	2
106			min	-.227	2	.002	15	-.005	3	-4.702e-3	3	967.225	3	7235.674	1
107		16	max	.004	3	.128	3	0	15	3.985e-3	2	NC	4	NC	3
108			min	-.227	2	.002	15	-.006	1	-8.235e-3	3	2015.534	3	6403.175	1
109		17	max	.004	3	.211	3	0	15	5.58e-3	2	NC	4	NC	3
110			min	-.227	2	.002	15	-.004	1	-1.177e-2	3	4805.686	2	7146.007	1
111		18	max	.004	3	.298	3	.004	1	6.62e-3	2	NC	1	NC	1
112			min	-.227	2	.002	15	0	15	-1.407e-2	3	1293.888	3	NC	1
113		19	max	.004	3	.385	3	.014	1	6.62e-3	2	NC	1	NC	1
114			min	-.227	2	.002	15	0	15	-1.407e-2	3	703.119	3	NC	1
115	M10	1	max	0	1	.268	3	.227	2	1.169e-2	3	NC	1	NC	1
116			min	0	3	.002	15	-.004	3	-1.866e-3	2	NC	1	NC	1
117		2	max	0	1	.402	3	.249	1	1.335e-2	3	NC	4	NC	3
118			min	0	3	-.002	10	-.003	3	-2.523e-3	2	1255.393	3	7551.94	1
119		3	max	0	1	.526	3	.284	1	1.5e-2	3	NC	5	NC	3
120			min	0	3	-.055	2	-.005	3	-3.18e-3	2	650.913	3	2960.761	1
121		4	max	0	1	.624	3	.322	1	1.666e-2	3	NC	5	NC	3
122			min	0	3	-.091	2	-.008	3	-3.837e-3	2	472.254	3	1763.146	1
123		5	max	0	1	.685	3	.358	1	1.831e-2	3	NC	5	NC	3
124			min	0	3	-.104	2	-.013	3	-4.494e-3	2	403.069	3	1276.312	1
125		6	max	0	1	.706	3	.388	1	1.997e-2	3	NC	5	NC	3
126			min	0	3	-.094	2	-.018	3	-5.151e-3	2	383.14	3	1040.273	1
127		7	max	0	1	.693	3	.409	1	2.163e-2	3	NC	5	NC	5
128			min	0	3	-.064	2	-.023	3	-5.808e-3	2	395.184	3	920.22	1
129		8	max	0	1	.656	3	.425	2	2.328e-2	3	NC	4	NC	5
130			min	0	3	-.024	1	-.028	3	-6.465e-3	2	432.771	3	851.596	2
131		9	max	0	1	.614	3	.438	2	2.494e-2	3	NC	4	NC	5
132			min	0	3	0	15	-.032	3	-7.122e-3	2	485.073	3	798.145	2
133		10	max	0	1	.593	3	.442	2	2.66e-2	3	NC	4	NC	5
134			min	0	1	.001	15	-.033	3	-7.78e-3	2	516.418	3	781.663	2
135		11	max	0	3	.614	3	.438	2	2.494e-2	3	NC	4	NC	5
136			min	0	1	0	15	-.032	3	-7.122e-3	2	485.073	3	798.145	2
137		12	max	0	3	.656	3	.425	2	2.328e-2	3	NC	4	NC	5
138			min	0	1	-.024	1	-.028	3	-6.465e-3	2	432.771	3	851.596	2
139		13	max	0	3	.693	3	.409	1	2.163e-2	3	NC	5	NC	5
140			min	0	1	-.064	2	-.023	3	-5.808e-3	2	395.184	3	920.22	1
141		14	max	0	3	.706	3	.388	1	1.997e-2	3	NC	5	NC	3
142			min	0	1	-.094	2	-.018	3	-5.151e-3	2	383.14	3	1040.273	1
143		15	max	0	3	.685	3	.358	1	1.831e-2	3	NC	5	NC	3
144			min	0	1	-.104	2	-.013	3	-4.494e-3	2	403.069	3	1276.312	1
145		16	max	0	3	.624	3	.322	1	1.666e-2	3	NC	5	NC	3
146			min	0	1	-.091	2	-.008	3	-3.837e-3	2	472.254	3	1763.146	1
147		17	max	0	3	.526	3	.284	1	1.5e-2	3	NC	5	NC	3
148			min	0	1	-.055	2	-.005	3	-3.18e-3	2	650.913	3	2960.761	1
149		18	max	0	3	.402	3	.249	1	1.335e-2	3	NC	4	NC	3
150			min	0	1	-.002	10	-.003	3	-2.523e-3	2	1255.393	3	7551.94	1
151		19	max	0	3	.268	3	.227	2	1.169e-2	3	NC	1	NC	1
152			min	0	1	.002	15	-.004	3	-1.866e-3	2	NC	1	NC	1
153	M11	1	max	.001	1	.008	2	.229	2	4.994e-3	1	NC	1	NC	1
154			min	-.001	3	-.049	3	-.004	3	1.369e-4	15	NC	1	NC	1
155		2	max	.001	1	.027	3	.245	1	5.646e-3	2	NC	4	NC	1
156			min	-.001	3	-.057	2	-.008	3	1.49e-4	15	2206.218	3	NC	1
157		3	max	0	1	.094	3	.277	1	6.303e-3	2	NC	5	NC	3
158			min	-.001	3	-.112	2	-.012	3	1.611e-4	15	1170.884	3	3479.51	1
159		4	max	0	1	.137	3	.315	1	6.959e-3	2	NC	5	NC	3
160			min	0	3	-.146	2	-.016	3	1.094e-4	12	900.687	3	1948.539	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
161		5	max	0	1	.148	3	.352	1	7.615e-3	2	NC	5	NC	3
162			min	0	3	-.156	2	-.02	3	3.004e-5	12	853.025	3	1359.068	1
163		6	max	0	1	.125	3	.384	1	8.271e-3	2	NC	5	NC	5
164			min	0	3	-.141	2	-.024	3	-8.635e-5	3	967.977	3	1079.557	1
165		7	max	0	1	.073	3	.408	1	8.928e-3	2	NC	4	NC	5
166			min	0	3	-.106	2	-.028	3	-2.128e-4	3	1373.515	3	936.739	1
167		8	max	0	1	.007	3	.427	2	9.584e-3	2	NC	4	NC	5
168			min	0	3	-.061	2	-.032	3	-3.393e-4	3	2454.801	2	848.37	2
169		9	max	0	1	0	15	.442	2	1.024e-2	2	NC	3	NC	5
170			min	0	3	-.053	3	-.034	3	-4.657e-4	3	6221.128	2	790.402	2
171		10	max	0	1	.002	9	.447	2	1.09e-2	2	NC	1	NC	5
172			min	0	1	-.081	3	-.035	3	-5.922e-4	3	5271.444	3	772.369	2
173		11	max	0	3	0	15	.442	2	1.024e-2	2	NC	3	NC	5
174			min	0	1	-.053	3	-.034	3	-4.657e-4	3	6221.128	2	790.402	2
175		12	max	0	3	.007	3	.427	2	9.584e-3	2	NC	4	NC	5
176			min	0	1	-.061	2	-.032	3	-3.393e-4	3	2454.801	2	848.37	2
177		13	max	0	3	.073	3	.408	1	8.928e-3	2	NC	4	NC	5
178			min	0	1	-.106	2	-.028	3	-2.128e-4	3	1373.515	3	936.739	1
179		14	max	0	3	.125	3	.384	1	8.271e-3	2	NC	5	NC	5
180			min	0	1	-.141	2	-.024	3	-8.635e-5	3	967.977	3	1079.557	1
181		15	max	0	3	.148	3	.352	1	7.615e-3	2	NC	5	NC	3
182			min	0	1	-.156	2	-.02	3	3.004e-5	12	853.025	3	1359.068	1
183		16	max	0	3	.137	3	.315	1	6.959e-3	2	NC	5	NC	3
184			min	0	1	-.146	2	-.016	3	1.094e-4	12	900.687	3	1948.539	1
185		17	max	.001	3	.094	3	.277	1	6.303e-3	2	NC	5	NC	3
186			min	0	1	-.112	2	-.012	3	1.611e-4	15	1170.884	3	3479.51	1
187		18	max	.001	3	.027	3	.245	1	5.646e-3	2	NC	4	NC	1
188			min	-.001	1	-.057	2	-.008	3	1.49e-4	15	2206.218	3	NC	1
189		19	max	.001	3	.008	2	.229	2	4.994e-3	1	NC	1	NC	1
190			min	-.001	1	-.049	3	-.004	3	1.369e-4	15	NC	1	NC	1
191	M12	1	max	0	3	-.003	15	.231	2	6.102e-3	2	NC	1	NC	1
192			min	0	1	-.106	1	-.005	3	-1.223e-3	3	NC	1	NC	1
193		2	max	0	3	.012	3	.244	1	6.725e-3	2	NC	4	NC	1
194			min	0	1	-.216	2	-.005	3	-1.406e-3	3	1525.581	2	NC	1
195		3	max	0	3	.054	3	.274	1	7.348e-3	2	NC	5	NC	3
196			min	0	1	-.311	2	-.007	3	-1.589e-3	3	816.922	2	3809.795	1
197		4	max	0	3	.078	3	.312	1	7.971e-3	2	NC	5	NC	3
198			min	0	1	-.378	2	-.011	3	-1.771e-3	3	616.583	2	2051.807	1
199		5	max	0	3	.083	3	.35	1	8.594e-3	2	NC	5	NC	3
200			min	0	1	-.409	2	-.016	3	-1.954e-3	3	554.092	2	1400.008	1
201		6	max	0	3	.069	3	.384	1	9.217e-3	2	NC	5	NC	3
202			min	0	1	-.403	2	-.021	3	-2.137e-3	3	565.295	2	1095.917	1
203		7	max	0	3	.041	3	.409	1	9.839e-3	2	NC	5	NC	5
204			min	0	1	-.366	2	-.027	3	-2.32e-3	3	644.842	2	940.805	1
205		8	max	0	3	.005	3	.43	2	1.046e-2	2	NC	5	NC	5
206			min	0	1	-.312	2	-.032	3	-2.503e-3	3	815.396	2	844.339	2
207		9	max	0	3	-.006	15	.446	2	1.109e-2	2	NC	3	NC	5
208			min	0	1	-.259	2	-.036	3	-2.686e-3	3	1096.175	2	782.366	2
209		10	max	0	1	-.005	15	.451	2	1.171e-2	2	NC	3	NC	5
210			min	0	1	-.234	2	-.037	3	-2.868e-3	3	1307.483	2	762.978	2
211		11	max	0	1	-.006	15	.446	2	1.109e-2	2	NC	3	NC	5
212			min	0	3	-.259	2	-.036	3	-2.686e-3	3	1096.175	2	782.366	2
213		12	max	0	1	.005	3	.43	2	1.046e-2	2	NC	5	NC	5
214			min	0	3	-.312	2	-.032	3	-2.503e-3	3	815.396	2	844.339	2
215		13	max	0	1	.041	3	.409	1	9.839e-3	2	NC	5	NC	5
216			min	0	3	-.366	2	-.027	3	-2.32e-3	3	644.842	2	940.805	1
217		14	max	0	1	.069	3	.384	1	9.217e-3	2	NC	5	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
218			min	0	3	-.403	2	-.021	3	-2.137e-3	3	565.295	2	1095.917	1
219		15	max	0	1	.083	3	.35	1	8.594e-3	2	NC	5	NC	3
220			min	0	3	-.409	2	-.016	3	-1.954e-3	3	554.092	2	1400.008	1
221		16	max	0	1	.078	3	.312	1	7.971e-3	2	NC	5	NC	3
222			min	0	3	-.378	2	-.011	3	-1.771e-3	3	616.583	2	2051.807	1
223		17	max	0	1	.054	3	.274	1	7.348e-3	2	NC	5	NC	3
224			min	0	3	-.311	2	-.007	3	-1.589e-3	3	816.922	2	3809.795	1
225		18	max	0	1	.012	3	.244	1	6.725e-3	2	NC	4	NC	1
226			min	0	3	-.216	2	-.005	3	-1.406e-3	3	1525.581	2	NC	1
227		19	max	0	1	-.003	15	.231	2	6.102e-3	2	NC	1	NC	1
228			min	0	3	-.106	1	-.005	3	-1.223e-3	3	NC	1	NC	1
229	M13	1	max	0	3	.136	3	.233	2	1.489e-2	2	NC	1	NC	1
230			min	0	1	-.603	2	-.006	3	-5.828e-3	3	NC	1	NC	1
231		2	max	0	3	.214	3	.256	1	1.67e-2	2	NC	5	NC	3
232			min	0	1	-.79	2	-.007	3	-6.675e-3	3	895.626	2	6997.317	1
233		3	max	0	3	.285	3	.292	1	1.852e-2	2	NC	5	NC	3
234			min	0	1	-.964	2	-.01	3	-7.522e-3	3	464.836	2	2801.151	1
235		4	max	0	3	.341	3	.332	1	2.033e-2	2	NC	5	NC	3
236			min	0	1	-1.107	2	-.014	3	-8.369e-3	3	332.841	2	1684.77	1
237		5	max	0	3	.378	3	.369	1	2.215e-2	2	NC	5	NC	3
238			min	0	1	-1.21	2	-.019	3	-9.216e-3	3	276.532	2	1226.153	1
239		6	max	0	3	.394	3	.4	1	2.396e-2	2	NC	5	NC	5
240			min	0	1	-1.269	2	-.025	3	-1.006e-2	3	252.082	2	1002.339	1
241		7	max	0	3	.392	3	.421	1	2.577e-2	2	NC	15	NC	5
242			min	0	1	-1.288	2	-.03	3	-1.091e-2	3	245.274	2	887.936	1
243		8	max	0	3	.378	3	.439	2	2.759e-2	2	NC	15	NC	5
244			min	0	1	-1.276	2	-.035	3	-1.176e-2	3	249.56	2	818.009	2
245		9	max	0	3	.36	3	.452	2	2.94e-2	2	NC	15	NC	5
246			min	0	1	-1.251	2	-.038	3	-1.26e-2	3	259.239	2	767.568	2
247		10	max	0	1	.351	3	.457	2	3.121e-2	2	NC	5	NC	5
248			min	0	1	-1.236	2	-.04	3	-1.345e-2	3	265.327	2	751.999	2
249		11	max	0	1	.36	3	.452	2	2.94e-2	2	NC	15	NC	5
250			min	0	3	-1.251	2	-.038	3	-1.26e-2	3	259.239	2	767.568	2
251		12	max	0	1	.378	3	.439	2	2.759e-2	2	NC	15	NC	5
252			min	0	3	-1.276	2	-.035	3	-1.176e-2	3	249.56	2	818.009	2
253		13	max	0	1	.392	3	.421	1	2.577e-2	2	NC	15	NC	5
254			min	0	3	-1.288	2	-.03	3	-1.091e-2	3	245.274	2	887.936	1
255		14	max	0	1	.394	3	.4	1	2.396e-2	2	NC	5	NC	5
256			min	0	3	-1.269	2	-.025	3	-1.006e-2	3	252.082	2	1002.339	1
257		15	max	0	1	.378	3	.369	1	2.215e-2	2	NC	5	NC	3
258			min	0	3	-1.21	2	-.019	3	-9.216e-3	3	276.532	2	1226.153	1
259		16	max	0	1	.341	3	.332	1	2.033e-2	2	NC	5	NC	3
260			min	0	3	-1.107	2	-.014	3	-8.369e-3	3	332.841	2	1684.77	1
261		17	max	0	1	.285	3	.292	1	1.852e-2	2	NC	5	NC	3
262			min	0	3	-.964	2	-.01	3	-7.522e-3	3	464.836	2	2801.151	1
263		18	max	0	1	.214	3	.256	1	1.67e-2	2	NC	5	NC	3
264			min	0	3	-.79	2	-.007	3	-6.675e-3	3	895.626	2	6997.317	1
265		19	max	0	1	.136	3	.233	2	1.489e-2	2	NC	1	NC	1
266			min	0	3	-.603	2	-.006	3	-5.828e-3	3	NC	1	NC	1
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	3	1.106e-3	2	NC	1	NC	1
270			min	0	2	0	1	0	1	-4.892e-4	3	NC	1	NC	1
271		3	max	0	3	0	15	0	3	2.211e-3	2	NC	1	NC	1
272			min	0	2	-.004	1	0	1	-9.784e-4	3	NC	1	NC	1
273		4	max	0	3	0	15	0	3	3.317e-3	2	NC	3	NC	1
274			min	0	2	-.008	1	0	1	-1.468e-3	3	6526.99	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
275		5	max	0	3	0	15	0	3	4.216e-3	2	NC	3	NC	1
276			min	0	2	-.015	1	0	1	-1.862e-3	3	3654.236	1	NC	1
277		6	max	0	3	0	12	.001	3	3.858e-3	2	NC	3	NC	1
278			min	0	2	-.023	1	-.001	1	-1.68e-3	3	2318.348	1	NC	1
279		7	max	0	3	0	12	.002	3	3.5e-3	2	NC	3	NC	1
280			min	0	2	-.033	1	-.002	1	-1.498e-3	3	1610.685	1	NC	1
281		8	max	0	3	0	12	.002	3	3.142e-3	2	NC	3	NC	1
282			min	0	2	-.045	1	-.002	1	-1.316e-3	3	1190.936	1	NC	1
283		9	max	0	3	0	12	.002	3	2.784e-3	2	NC	3	NC	1
284			min	0	2	-.058	1	-.002	1	-1.134e-3	3	921.154	1	NC	1
285		10	max	0	3	0	12	.002	3	2.426e-3	2	NC	3	NC	1
286			min	0	2	-.073	1	-.003	1	-9.514e-4	3	737.498	1	NC	1
287		11	max	0	3	0	3	.002	3	2.067e-3	2	NC	3	NC	1
288			min	0	2	-.088	1	-.003	1	-7.692e-4	3	606.684	1	NC	1
289		12	max	0	3	0	3	.002	3	1.709e-3	2	NC	3	NC	1
290			min	0	2	-.105	1	-.003	1	-5.87e-4	3	510.115	1	NC	1
291		13	max	0	3	0	3	.002	3	1.351e-3	2	NC	3	NC	1
292			min	-.001	2	-.123	1	-.003	1	-4.048e-4	3	436.781	1	NC	1
293		14	max	.001	3	.001	3	.001	3	9.93e-4	2	NC	3	NC	1
294			min	-.001	2	-.141	1	-.003	1	-2.226e-4	3	379.748	1	NC	1
295		15	max	.001	3	.001	3	0	3	6.348e-4	2	NC	3	NC	1
296			min	-.001	2	-.16	2	-.003	1	-4.044e-5	3	334.443	2	NC	1
297		16	max	.001	3	.002	3	0	15	2.767e-4	2	NC	3	NC	1
298			min	-.001	2	-.18	2	-.002	1	-6.353e-5	9	297.749	2	NC	1
299		17	max	.001	3	.002	3	0	10	3.24e-4	3	NC	3	NC	1
300			min	-.001	2	-.2	2	-.003	3	-2.577e-4	1	267.772	2	NC	1
301		18	max	.001	3	.003	3	0	2	5.062e-4	3	NC	3	NC	1
302			min	-.001	2	-.221	2	-.005	3	-5.752e-4	1	242.984	2	NC	1
303		19	max	.001	3	.003	3	.002	2	6.884e-4	3	NC	3	NC	1
304			min	-.001	2	-.241	2	-.007	3	-8.928e-4	1	222.274	2	7296.287	3
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	1	0	1	NC	1	NC	1
308			min	0	2	-.001	1	0	1	0	1	NC	1	NC	1
309		3	max	0	3	0	15	0	1	0	1	NC	3	NC	1
310			min	0	2	-.006	1	0	1	0	1	8718.324	1	NC	1
311		4	max	0	3	0	15	0	1	0	1	NC	3	NC	1
312			min	0	2	-.014	1	0	1	0	1	3766.428	1	NC	1
313		5	max	.001	3	0	15	0	1	0	1	NC	3	NC	1
314			min	-.001	2	-.026	1	0	1	0	1	2071.312	1	NC	1
315		6	max	.001	3	0	12	0	1	0	1	NC	3	NC	1
316			min	-.001	2	-.042	2	0	1	0	1	1285.379	2	NC	1
317		7	max	.001	3	0	3	0	1	0	1	NC	3	NC	1
318			min	-.002	2	-.061	2	0	1	0	1	876.023	2	NC	1
319		8	max	.002	3	.002	3	0	1	0	1	NC	3	NC	1
320			min	-.002	2	-.084	2	0	1	0	1	639.062	2	NC	1
321		9	max	.002	3	.004	3	0	1	0	1	NC	3	NC	1
322			min	-.002	2	-.11	2	0	1	0	1	489.408	2	NC	1
323		10	max	.002	3	.006	3	0	1	0	1	NC	5	NC	1
324			min	-.002	2	-.138	2	0	1	0	1	388.871	2	NC	1
325		11	max	.002	3	.008	3	0	1	0	1	NC	12	NC	1
326			min	-.002	2	-.169	2	0	1	0	1	317.996	2	NC	1
327		12	max	.003	3	.011	3	0	1	0	1	NC	15	NC	1
328			min	-.003	2	-.202	2	0	1	0	1	266.103	2	NC	1
329		13	max	.003	3	.014	3	0	1	0	1	9689.019	15	NC	1
330			min	-.003	2	-.236	2	0	1	0	1	226.963	2	NC	1
331		14	max	.003	3	.017	3	0	1	0	1	8420.297	15	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
332			min	-.003	2	-.273	2	0	1	0	1	196.693	2	NC	1
333		15	max	.003	3	.02	3	0	1	0	1	7414.61	15	NC	1
334			min	-.003	2	-.31	2	0	1	0	1	172.797	2	NC	1
335		16	max	.003	3	.023	3	0	1	0	1	6604.108	15	NC	1
336			min	-.003	2	-.349	2	0	1	0	1	153.607	2	NC	1
337		17	max	.004	3	.027	3	0	1	0	1	5941.487	15	NC	1
338			min	-.004	2	-.389	2	0	1	0	1	137.967	2	NC	1
339		18	max	.004	3	.03	3	0	1	0	1	5393.237	15	NC	1
340			min	-.004	2	-.429	2	0	1	0	1	125.061	2	NC	1
341		19	max	.004	3	.034	3	0	1	0	1	4934.91	15	NC	1
342			min	-.004	2	-.469	2	0	1	0	1	114.298	2	NC	1
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	15	0	1	4.892e-4	3	NC	1	NC	1
346			min	0	2	0	1	0	3	-1.106e-3	2	NC	1	NC	1
347		3	max	0	3	0	15	0	1	9.784e-4	3	NC	1	NC	1
348			min	0	2	-.004	1	0	3	-2.211e-3	2	NC	1	NC	1
349		4	max	0	3	0	15	0	1	1.468e-3	3	NC	3	NC	1
350			min	0	2	-.008	1	0	3	-3.317e-3	2	6526.99	1	NC	1
351		5	max	0	3	0	15	0	1	1.862e-3	3	NC	3	NC	1
352			min	0	2	-.015	1	0	3	-4.216e-3	2	3654.236	1	NC	1
353		6	max	0	3	0	12	.001	1	1.68e-3	3	NC	3	NC	1
354			min	0	2	-.023	1	-.001	3	-3.858e-3	2	2318.348	1	NC	1
355		7	max	0	3	0	12	.002	1	1.498e-3	3	NC	3	NC	1
356			min	0	2	-.033	1	-.002	3	-3.5e-3	2	1610.685	1	NC	1
357		8	max	0	3	0	12	.002	1	1.316e-3	3	NC	3	NC	1
358			min	0	2	-.045	1	-.002	3	-3.142e-3	2	1190.936	1	NC	1
359		9	max	0	3	0	12	.002	1	1.134e-3	3	NC	3	NC	1
360			min	0	2	-.058	1	-.002	3	-2.784e-3	2	921.154	1	NC	1
361		10	max	0	3	0	12	.003	1	9.514e-4	3	NC	3	NC	1
362			min	0	2	-.073	1	-.002	3	-2.426e-3	2	737.498	1	NC	1
363		11	max	0	3	0	3	.003	1	7.692e-4	3	NC	3	NC	1
364			min	0	2	-.088	1	-.002	3	-2.067e-3	2	606.684	1	NC	1
365		12	max	0	3	0	3	.003	1	5.87e-4	3	NC	3	NC	1
366			min	0	2	-.105	1	-.002	3	-1.709e-3	2	510.115	1	NC	1
367		13	max	0	3	0	3	.003	1	4.048e-4	3	NC	3	NC	1
368			min	-.001	2	-.123	1	-.002	3	-1.351e-3	2	436.781	1	NC	1
369		14	max	.001	3	.001	3	.003	1	2.226e-4	3	NC	3	NC	1
370			min	-.001	2	-.141	1	-.001	3	-9.93e-4	2	379.748	1	NC	1
371		15	max	.001	3	.001	3	.003	1	4.044e-5	3	NC	3	NC	1
372			min	-.001	2	-.16	2	0	3	-6.348e-4	2	334.443	2	NC	1
373		16	max	.001	3	.002	3	.002	1	6.353e-5	9	NC	3	NC	1
374			min	-.001	2	-.18	2	0	15	-2.767e-4	2	297.749	2	NC	1
375		17	max	.001	3	.002	3	.003	3	2.577e-4	1	NC	3	NC	1
376			min	-.001	2	-.2	2	0	10	-3.24e-4	3	267.772	2	NC	1
377		18	max	.001	3	.003	3	.005	3	5.752e-4	1	NC	3	NC	1
378			min	-.001	2	-.221	2	0	2	-5.062e-4	3	242.984	2	NC	1
379		19	max	.001	3	.003	3	.007	3	8.928e-4	1	NC	3	NC	1
380			min	-.001	2	-.241	2	-.002	2	-6.884e-4	3	222.274	2	7296.287	3
381	M3	1	max	.013	1	0	3	0	3	1.278e-3	2	NC	1	NC	1
382			min	0	15	-.005	1	0	1	-4.973e-4	3	NC	1	NC	1
383		2	max	.012	1	0	3	.007	3	1.771e-3	2	NC	1	NC	4
384			min	0	15	-.026	2	-.015	2	-7.278e-4	3	NC	1	4306.953	2
385		3	max	.012	1	0	3	.013	3	2.264e-3	2	NC	1	NC	4
386			min	0	15	-.047	2	-.029	2	-9.582e-4	3	NC	1	2184.554	2
387		4	max	.011	1	.001	3	.019	3	2.757e-3	2	NC	1	NC	4
388			min	0	15	-.068	2	-.042	2	-1.189e-3	3	NC	1	1486.222	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
389		5	max	.01	1	.002	3	.025	3	3.25e-3	2	NC	1	NC	5
390			min	0	15	-.089	2	-.054	2	-1.419e-3	3	NC	1	1144.738	2
391		6	max	.01	1	.003	3	.03	3	3.743e-3	2	NC	1	NC	5
392			min	0	15	-.11	2	-.065	2	-1.65e-3	3	NC	1	946.949	2
393		7	max	.009	1	.003	3	.034	3	4.236e-3	2	NC	1	NC	5
394			min	0	15	-.131	2	-.075	2	-1.88e-3	3	NC	1	822.135	2
395		8	max	.009	1	.004	3	.038	3	4.729e-3	2	NC	1	NC	5
396			min	0	15	-.152	2	-.083	2	-2.111e-3	3	NC	1	740.386	2
397		9	max	.008	1	.005	3	.041	3	5.222e-3	2	NC	1	NC	5
398			min	0	15	-.172	2	-.089	2	-2.341e-3	3	NC	1	687.265	2
399		10	max	.007	1	.006	3	.042	3	5.715e-3	2	NC	1	NC	5
400			min	0	15	-.193	2	-.093	2	-2.571e-3	3	NC	1	655.458	2
401		11	max	.007	1	.007	3	.043	3	6.208e-3	2	NC	1	NC	5
402			min	0	15	-.213	2	-.095	2	-2.802e-3	3	9702.776	3	641.605	2
403		12	max	.006	1	.008	3	.043	3	6.701e-3	2	NC	1	NC	5
404			min	0	15	-.234	2	-.094	2	-3.032e-3	3	8370.792	3	645.171	2
405		13	max	.006	1	.009	3	.041	3	7.194e-3	2	NC	1	NC	5
406			min	0	15	-.254	2	-.09	2	-3.263e-3	3	7295.837	3	668.483	2
407		14	max	.005	1	.01	3	.038	3	7.687e-3	2	NC	1	NC	5
408			min	0	15	-.274	2	-.083	2	-3.493e-3	3	6418.92	3	718.105	2
409		15	max	.005	3	.011	3	.034	3	8.18e-3	2	NC	1	NC	5
410			min	0	15	-.294	2	-.072	2	-3.724e-3	3	5697.081	3	809.074	2
411		16	max	.005	3	.012	3	.027	3	8.673e-3	2	NC	1	NC	5
412			min	0	15	-.314	2	-.058	2	-3.954e-3	3	5098.378	3	978.166	2
413		17	max	.005	3	.014	3	.02	3	9.166e-3	2	NC	1	NC	4
414			min	0	10	-.334	2	-.041	2	-4.185e-3	3	4598.667	3	1337.446	2
415		18	max	.006	3	.015	3	.01	3	9.659e-3	2	NC	1	NC	4
416			min	0	10	-.354	2	-.019	2	-4.415e-3	3	4179.453	3	2449.694	2
417		19	max	.006	3	.017	3	.009	1	1.015e-2	2	NC	1	NC	1
418			min	0	10	-.374	2	-.002	3	-4.646e-3	3	3826.426	3	NC	1
419	M6	1	max	.022	1	0	3	0	1	0	1	NC	1	NC	1
420			min	0	15	-.009	2	0	1	0	1	NC	1	NC	1
421		2	max	.021	1	.005	3	0	1	0	1	NC	1	NC	1
422			min	0	15	-.05	2	0	1	0	1	NC	1	NC	1
423		3	max	.019	1	.009	3	0	1	0	1	NC	1	NC	1
424			min	0	15	-.092	2	0	1	0	1	7477.557	3	NC	1
425		4	max	.018	1	.013	3	0	1	0	1	NC	1	NC	1
426			min	0	15	-.133	2	0	1	0	1	4969.442	3	NC	1
427		5	max	.016	1	.018	3	0	1	0	1	NC	1	NC	1
428			min	0	15	-.175	2	0	1	0	1	3711.576	3	NC	1
429		6	max	.015	1	.022	3	0	1	0	1	NC	1	NC	1
430			min	0	15	-.216	2	0	1	0	1	2954.226	3	NC	1
431		7	max	.013	1	.026	3	0	1	0	1	NC	1	NC	1
432			min	0	15	-.257	2	0	1	0	1	2447.483	3	NC	1
433		8	max	.012	1	.031	3	0	1	0	1	NC	1	NC	1
434			min	0	15	-.299	2	0	1	0	1	2084.239	3	NC	1
435		9	max	.01	1	.036	3	0	1	0	1	NC	1	NC	1
436			min	0	15	-.34	2	0	1	0	1	1810.933	3	NC	1
437		10	max	.009	3	.04	3	0	1	0	1	NC	1	NC	1
438			min	0	15	-.381	2	0	1	0	1	1597.801	3	NC	1
439		11	max	.01	3	.045	3	0	1	0	1	NC	1	NC	1
440			min	0	15	-.422	2	0	1	0	1	1426.975	3	NC	1
441		12	max	.011	3	.05	3	0	1	0	1	NC	1	NC	1
442			min	0	10	-.462	2	0	1	0	1	1287.076	3	NC	1
443		13	max	.012	3	.055	3	0	1	0	1	NC	1	NC	1
444			min	-.001	10	-.503	2	0	1	0	1	1170.51	3	NC	1
445		14	max	.013	3	.06	3	0	1	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
446			min	-.003	2	-.544	2	0	1	0	1	1072.012	3	NC	1
447		15	max	.014	3	.065	3	0	1	0	1	NC	1	NC	1
448			min	-.004	2	-.584	2	0	1	0	1	987.814	3	NC	1
449		16	max	.015	3	.07	3	0	1	0	1	NC	1	NC	1
450			min	-.006	2	-.625	2	0	1	0	1	915.147	3	NC	1
451		17	max	.016	3	.075	3	0	1	0	1	NC	1	NC	1
452			min	-.008	2	-.665	2	0	1	0	1	851.929	3	NC	1
453		18	max	.017	3	.08	3	0	1	0	1	NC	1	NC	1
454			min	-.01	2	-.705	2	0	1	0	1	796.565	3	NC	1
455		19	max	.017	3	.085	3	0	1	0	1	NC	1	NC	1
456			min	-.012	2	-.746	2	0	1	0	1	747.811	3	NC	1
457	M9	1	max	.013	1	0	3	0	1	4.973e-4	3	NC	1	NC	1
458			min	0	15	-.005	1	0	3	-1.278e-3	2	NC	1	NC	1
459		2	max	.012	1	0	3	.015	2	7.278e-4	3	NC	1	NC	4
460			min	0	15	-.026	2	-.007	3	-1.771e-3	2	NC	1	4306.953	2
461		3	max	.012	1	0	3	.029	2	9.582e-4	3	NC	1	NC	4
462			min	0	15	-.047	2	-.013	3	-2.264e-3	2	NC	1	2184.554	2
463		4	max	.011	1	.001	3	.042	2	1.189e-3	3	NC	1	NC	4
464			min	0	15	-.068	2	-.019	3	-2.757e-3	2	NC	1	1486.222	2
465		5	max	.01	1	.002	3	.054	2	1.419e-3	3	NC	1	NC	5
466			min	0	15	-.089	2	-.025	3	-3.25e-3	2	NC	1	1144.738	2
467		6	max	.01	1	.003	3	.065	2	1.65e-3	3	NC	1	NC	5
468			min	0	15	-.11	2	-.03	3	-3.743e-3	2	NC	1	946.949	2
469		7	max	.009	1	.003	3	.075	2	1.88e-3	3	NC	1	NC	5
470			min	0	15	-.131	2	-.034	3	-4.236e-3	2	NC	1	822.135	2
471		8	max	.009	1	.004	3	.083	2	2.111e-3	3	NC	1	NC	5
472			min	0	15	-.152	2	-.038	3	-4.729e-3	2	NC	1	740.386	2
473		9	max	.008	1	.005	3	.089	2	2.341e-3	3	NC	1	NC	5
474			min	0	15	-.172	2	-.041	3	-5.222e-3	2	NC	1	687.265	2
475		10	max	.007	1	.006	3	.093	2	2.571e-3	3	NC	1	NC	5
476			min	0	15	-.193	2	-.042	3	-5.715e-3	2	NC	1	655.458	2
477		11	max	.007	1	.007	3	.095	2	2.802e-3	3	NC	1	NC	5
478			min	0	15	-.213	2	-.043	3	-6.208e-3	2	9702.776	3	641.605	2
479		12	max	.006	1	.008	3	.094	2	3.032e-3	3	NC	1	NC	5
480			min	0	15	-.234	2	-.043	3	-6.701e-3	2	8370.792	3	645.171	2
481		13	max	.006	1	.009	3	.09	2	3.263e-3	3	NC	1	NC	5
482			min	0	15	-.254	2	-.041	3	-7.194e-3	2	7295.837	3	668.483	2
483		14	max	.005	1	.01	3	.083	2	3.493e-3	3	NC	1	NC	5
484			min	0	15	-.274	2	-.038	3	-7.687e-3	2	6418.92	3	718.105	2
485		15	max	.005	3	.011	3	.072	2	3.724e-3	3	NC	1	NC	5
486			min	0	15	-.294	2	-.034	3	-8.18e-3	2	5697.081	3	809.074	2
487		16	max	.005	3	.012	3	.058	2	3.954e-3	3	NC	1	NC	5
488			min	0	15	-.314	2	-.027	3	-8.673e-3	2	5098.378	3	978.166	2
489		17	max	.005	3	.014	3	.041	2	4.185e-3	3	NC	1	NC	4
490			min	0	10	-.334	2	-.02	3	-9.166e-3	2	4598.667	3	1337.446	2
491		18	max	.006	3	.015	3	.019	2	4.415e-3	3	NC	1	NC	4
492			min	0	10	-.354	2	-.01	3	-9.659e-3	2	4179.453	3	2449.694	2
493		19	max	.006	3	.017	3	.002	3	4.646e-3	3	NC	1	NC	1
494			min	0	10	-.374	2	-.009	1	-1.015e-2	2	3826.426	3	NC	1