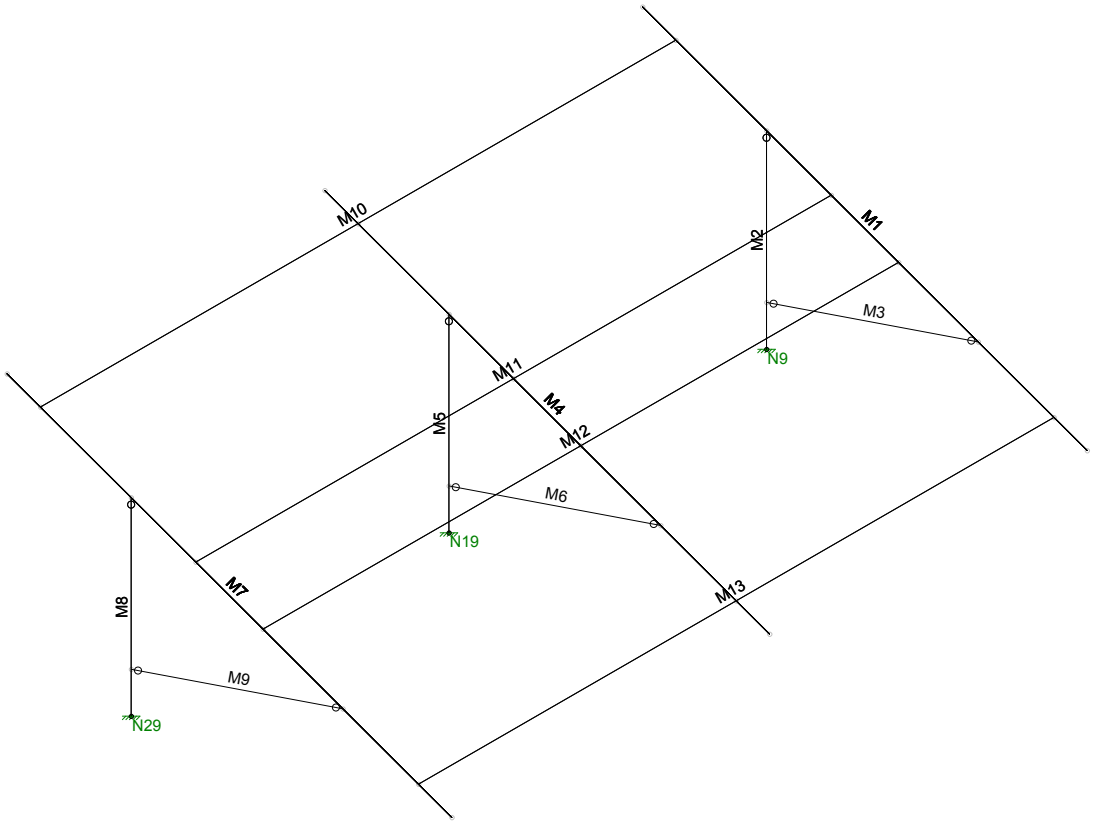


Schletter, Inc.		20° Tilt w/o Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

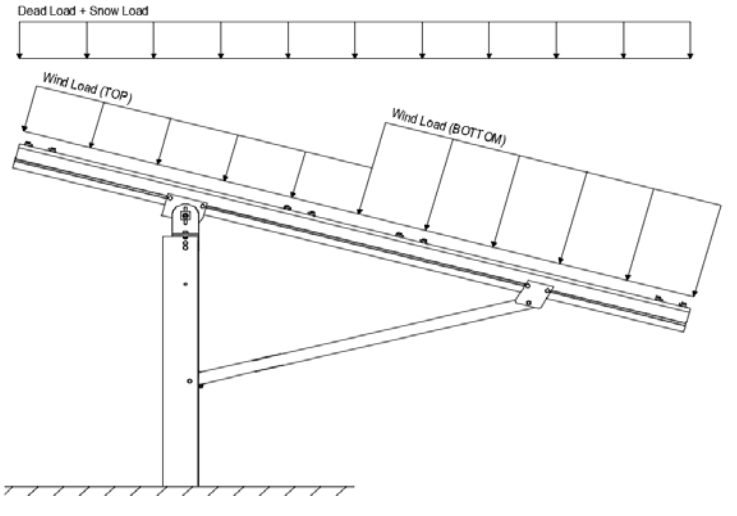
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row =	2
Module Tilt =	20°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	20.62	psf	*(ASCE 7-05, Eq. 7-2)*
I_s =	1.00		
C_s =	0.91		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	85	mph	Exposure Category = C
Height <	15	ft	Importance Category = II
Peak Velocity Pressure, q_z =	11.34	psf	*Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.05	*(Pressure)*	*Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.*
$Cf+_{BOTTOM}$ =	1.65		
$Cf-_{TOP}$ =	-2.12	*(Suction)*	
$Cf-_{BOTTOM}$ =	-1		

2.4 Seismic Loads - N/A

S_S =	0.00	R =	1.25
S_{DS} =	0.00	C_S =	0
S_1 =	0.00	ρ =	1.3
S_{D1} =	0.00	Ω =	1.25
T_a =	0.00	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W	
1.2D + 1.6W + 0.5S	
0.9D + 1.6W [M]	
1.54D + 1.3E + 0.2S [R]	*(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)*
0.56D + 1.3E [R]	
1.54D + 1.25E + 0.2S [O]	
0.56D + 1.25E [O]	

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S	
1.0D + 1.0W	
1.0D + 0.75L + 0.75W + 0.75S	
0.6D + 1.0W [M]	*(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)*
1.238D + 0.875E [O]	
1.1785D + 0.65625E + 0.75S [O]	
0.362D + 0.875E [O]	

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

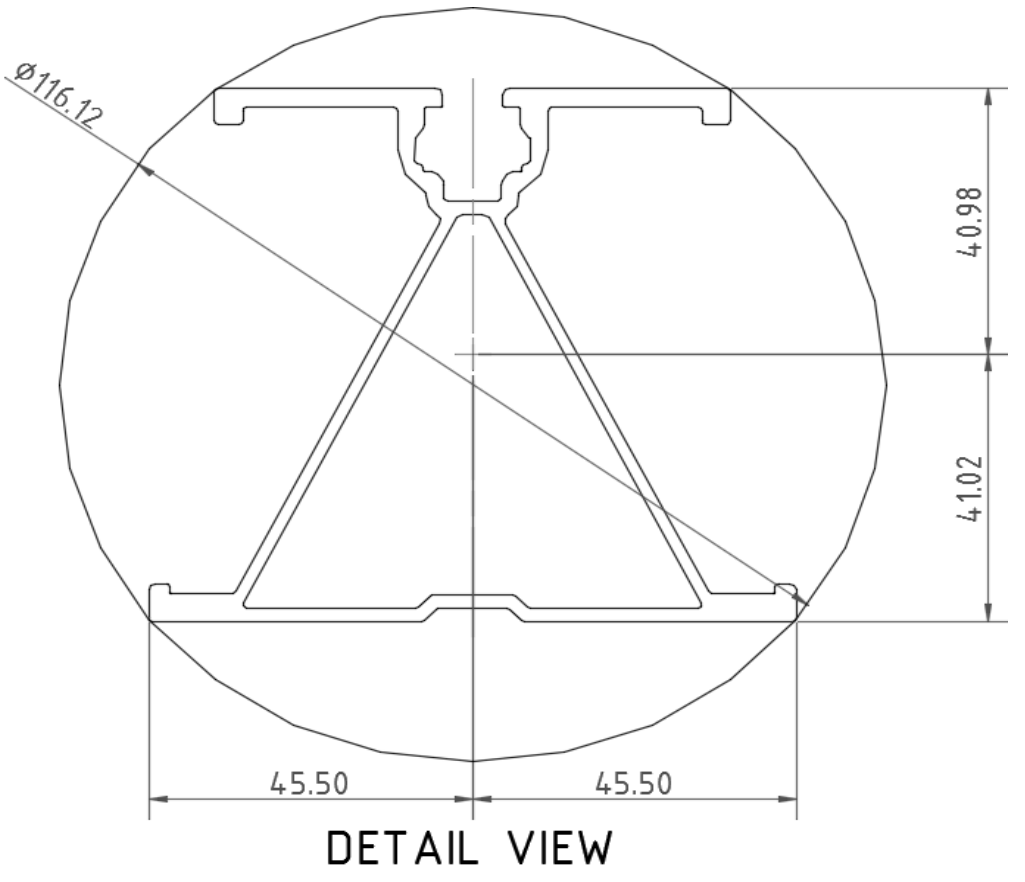
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

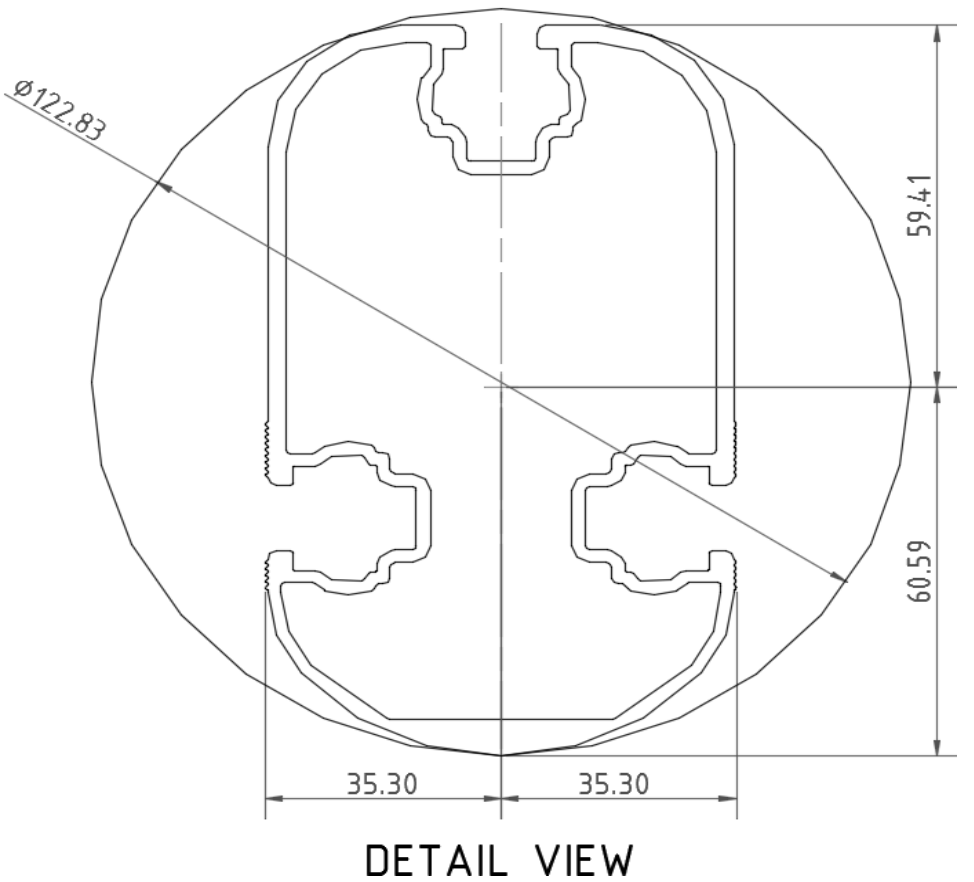
Purlin Type	=	**S1.5**	
Aluminum Type	=	6105-T5	
F_{ty}	=	35	ksi
L_b	=	138	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$	=	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$	=	23.08	ksi
S_y	=	1.33	in^3
S_x	=	0.6	in^3
E	=	10100	ksi
I_y	=	2.16	in^4
I_x	=	1.07	in^4
A	=	1.25	in^2
g	=	1.50	lbs/ft
M_y	=	2.041	k-ft
M_z	=	0.273	k-ft
$M_{y\ allowable}$	=	2.779	k-ft
$M_{z\ allowable}$	=	1.154	k-ft
Utilization	=	97%	



4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

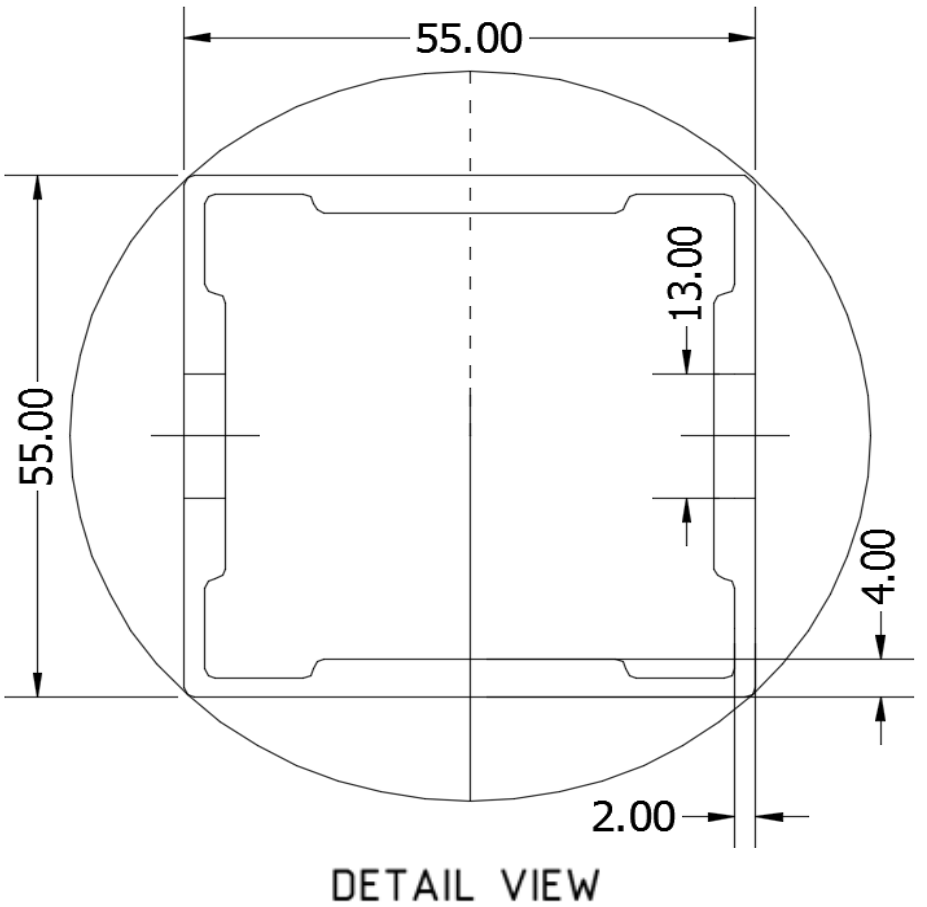
Girder Type	=	**T5**	
Aluminum Type	=	6105-T5	
F_{ty}	=	35	ksi
L_b	=	63.82	in
$\Phi F_{ty\ AXIAL}$	=	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$	=	30.46	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$	=	31.56	ksi
S_y	=	1.98	in^3
S_x	=	1.32	in^3
E	=	10100	ksi
I_y	=	4.74	in^4
I_x	=	1.83	in^4
A	=	1.93	in^2
g	=	2.32	lbs/ft
M_y	=	3.696	k-ft
M_z	=	0.000	k-ft
P_n	=	0.359	k
$M_{y\ allowable}$	=	5.026	k-ft
$M_{z\ allowable}$	=	3.472	k-ft
$P_{n\ allowable}$	=	59.439	k
Utilization	=	74%	



4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	61.00	in
$\Phi F_{ty\ AXIAL}$ =	13.67	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.000	k-ft
M_z =	0.394	k-ft
P_n =	5.399	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	13.425	k
Utilization =	68%	

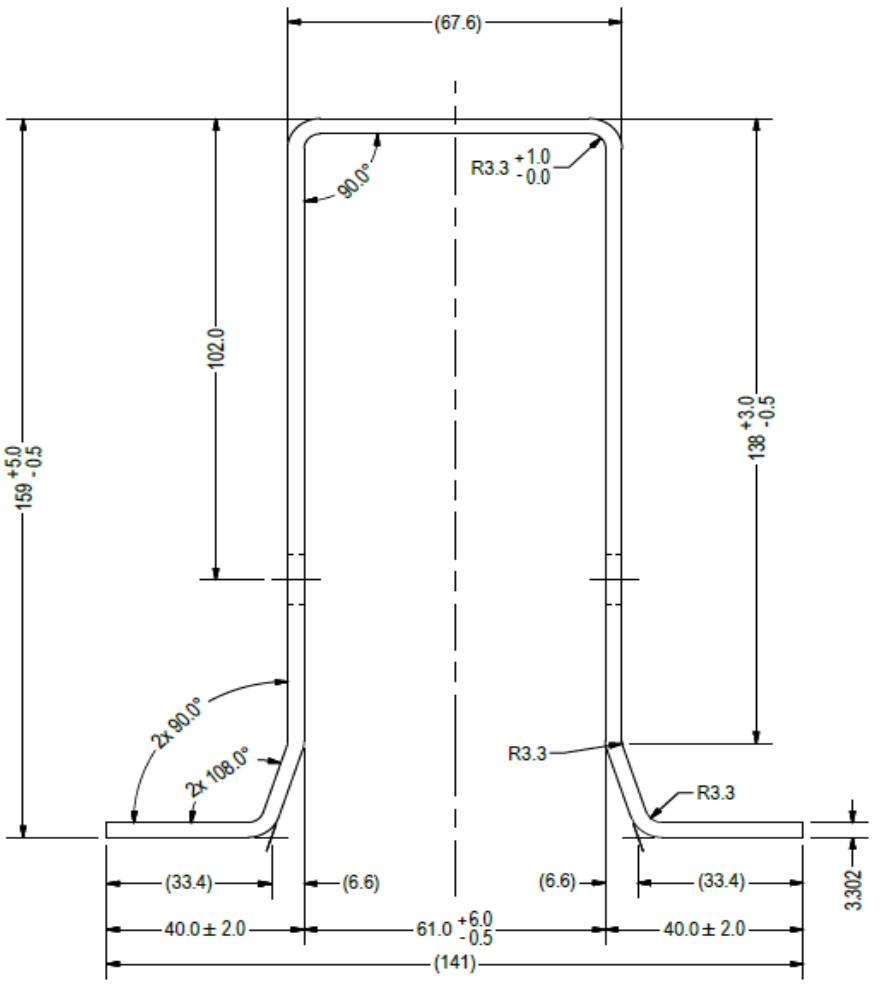


DETAIL VIEW

4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	65.62	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	14.642	k-ft
M_z =	0.000	k-ft
P_r =	7.041	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	46.025	k
Utilization =	93%	



DETAIL VIEW

5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	4.79	k
Maximum Lateral Load =	1.96	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

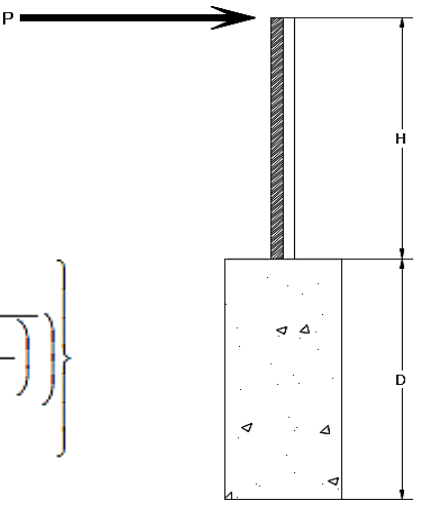
Lateral Force @ Top of Pole, P =	1.87	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1 + \sqrt{1 + \left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

Non-Constrained

Lateral Force @ Top of Pole, P =	1.87	k
Height of Pole Above Grade, H =	4.47	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	10.12	
Required Footing Depth, D =	13.72	ft

2nd Trial @ D_2 =	8.48	ft
Lateral Soil Bearing @ D/3, S_1 =	0.57	ksf
Lateral Soil Bearing @ D, S_3 =	1.70	ksf
Constant 2.34P/(S_1B), A =	3.88	
Required Footing Depth, D =	6.70	ft

3rd Trial @ D_3 =	7.59	ft
Lateral Soil Bearing @ D/3, S_1 =	0.51	ksf
Lateral Soil Bearing @ D, S_3 =	1.52	ksf
Constant 2.34P/(S_1B), A =	4.33	
Required Footing Depth, D =	7.25	ft

4th Trial @ D_4 =	7.42	ft
Lateral Soil Bearing @ D/3, S_1 =	0.49	ksf
Lateral Soil Bearing @ D, S_3 =	1.48	ksf
Constant 2.34P/(S_1B), A =	4.43	
Required Footing Depth, D =	7.37	ft

5th Trial @ D_5 =	7.39	ft
Lateral Soil Bearing @ D/3, S_1 =	0.49	ksf
Lateral Soil Bearing @ D, S_3 =	1.48	ksf
Constant 2.34P/(S_1B), A =	4.45	
Required Footing Depth, D =	7.50	ft

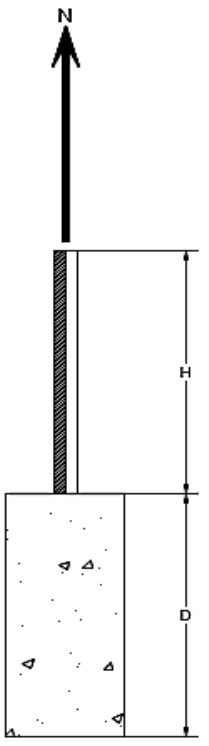
A 2ft diameter x 7.5ft deep footing unrestrained at ground level is required for the racking structure.

5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	2.29	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	1.49	k
Required Concrete Volume, V =	10.24	ft^3
Required Footing Depth, D =	3.50	ft

A 2ft diameter x 3.5ft deep footing unrestrained at ground level is required for the racking structure.



Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	4.92
2	0.4	0.2	118.10	4.82
3	0.6	0.2	118.10	4.71
4	0.8	0.2	118.10	4.61
5	1	0.2	118.10	4.50
6	1.2	0.2	118.10	4.40
7	1.4	0.2	118.10	4.30
8	1.6	0.2	118.10	4.19
9	1.8	0.2	118.10	4.09
10	2	0.2	118.10	3.99
11	2.2	0.2	118.10	3.88
12	2.4	0.2	118.10	3.78
13	2.6	0.2	118.10	3.68
14	2.8	0.2	118.10	3.57
15	3	0.2	118.10	3.47
16	3.2	0.2	118.10	3.36
17	3.4	0.2	118.10	3.26
18	0	0.0	0.00	3.26
19	0	0.0	0.00	3.26
20	0	0.0	0.00	3.26
21	0	0.0	0.00	3.26
22	0	0.0	0.00	3.26
23	0	0.0	0.00	3.26
24	0	0.0	0.00	3.26
25	0	0.0	0.00	3.26
26	0	0.0	0.00	3.26
27	0	0.0	0.00	3.26
28	0	0.0	0.00	3.26
29	0	0.0	0.00	3.26
30	0	0.0	0.00	3.26
31	0	0.0	0.00	3.26
32	0	0.0	0.00	3.26
33	0	0.0	0.00	3.26
34	0	0.0	0.00	3.26
Max	3.4	Sum	0.80	

5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	7.50	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	4.39	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	28.27	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

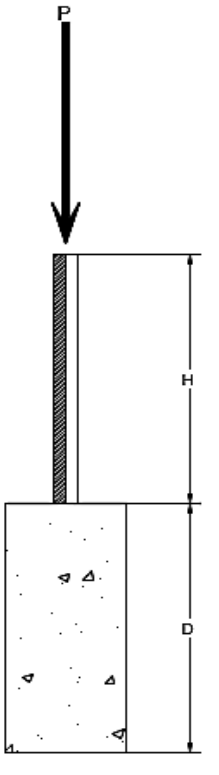
Weight of Concrete

Footing Volume	23.56	ft^3
Weight	3.42	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	4.24	k
1/3 Increase for Wind =	1.33	
Total Resistance =	11.94	k
Applied Force =	7.81	k
Utilization =	65%	

A 2ft diameter footing passes at a depth of 7.5ft.



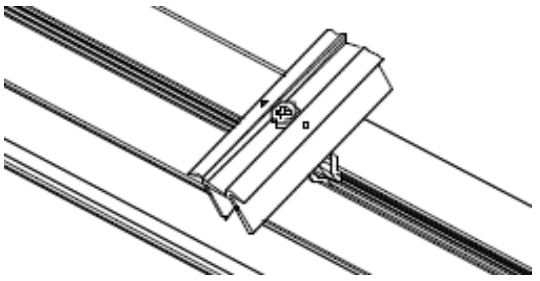
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

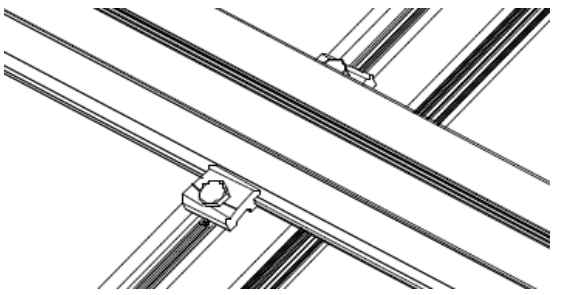
Fastening of Modules to Purlins

Maximum Uplifting Force =	0.355	k
Allowable Uplift =	1.214	k
Utilization =	29%	



Fastening of Purlins to Girders

Maximum Uplifting Force =	1.424	k
Allowable Uplift =	2.180	k
Utilization =	65%	

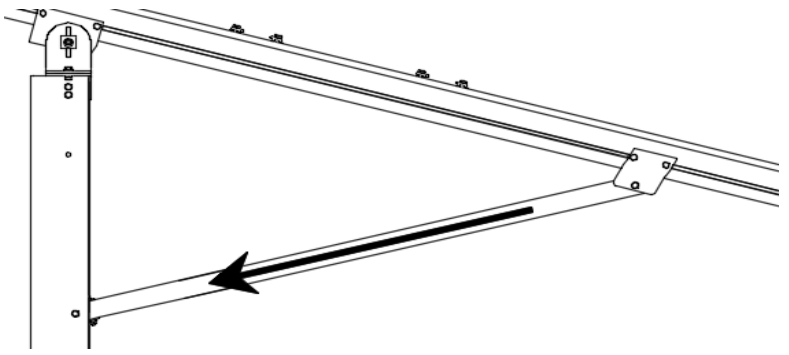


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load =	5.399	k
M10 Bolt Shear Capacity =	8.894	k
Utilization =	61%	

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

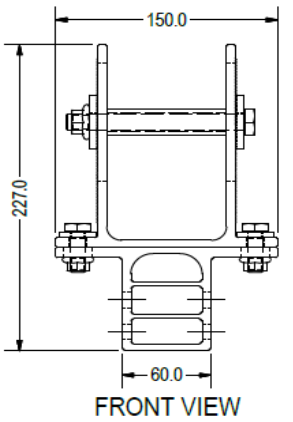


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

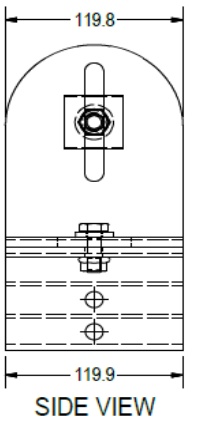
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

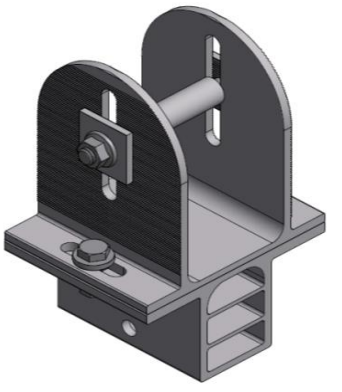
Maximum Tensile Load =	3.077	k
Allowable Load =	5.649	k
Utilization =	54%	



FRONT VIEW



SIDE VIEW



7. SEISMIC DESIGN

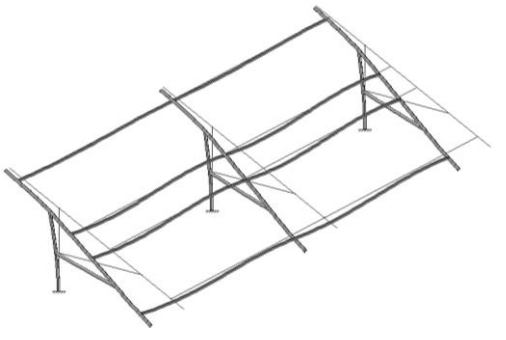
7.1 Seismic Drift - N/A

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =		65.92	in
Allowable Story Drift for All Other Structures, Δ =	{	$0.020h_{sx}$	
		1.318	in
Max Drift, Δ_{MAX} =		0	in

N/A

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:

3.4.14

L_b = 138 in

J = 0.432

381.773

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 27.0 ksi

3.4.16

b/t = 32.195

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 25.1 ksi

3.4.16.1 Not Used

Rb/t =

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 37.0588

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 40.985

Cc = 41.015

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.2

φF_L= φb[Bbr-mDbr*h/t]

φF_L= 43.2 ksi

φF_LSt= 25.1 ksi

Ix = 897074 mm^4

2.155 in^4

y = 41.015 mm

Sx = 1.335 in^3

M_{max}St = 2.788 k-ft

Weak Axis:

3.4.14

L_b = 138

J = 0.432

242.785

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 28.3

3.4.16

b/t = 37.0588

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 23.1 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 32.195

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 45.5

Cc = 45.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 23.1 ksi

Iy = 446476 mm^4

1.073 in^4

x = 45.5 mm

Sy = 0.599 in^3

M_{max}Wk = 1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 63.8189 in
J = 1.98
82.1278

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.5 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 63.8189
J = 1.98
89.1294

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.3

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L = φb[Bt-Dt*√(Rb/t)]

φF_L = 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L St$ = 30.5 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 5.001 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L = 1.3φyFcy

φF_L = 43.2 ksi

$\varphi F_L Wk$ = 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φyFcy

φF_L = 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φc[Bt-Dt*√(Rb/t)]

φF_L = 30.80 ksi

φF_L = 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 61 in

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

$M_{max}St$ = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 61

J = 0.942

95.1963

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

$M_{max}Wk$ = 1.460 k-ft

Compression

3.4.7

λ = 1.41113

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.77756

φF_L = (φccFcy)/(λ²)

φF_L = 13.6667 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

φF_L = φc[Bp-1.6Dp*b/t]

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L = φyFcy

φF_L = 33.25 ksi

φF_L = 13.67 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 14.07 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	65.62	in	
Pr =	7.04	k	(LRFD Factored Load)
Mr (Strong) =	14.64	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	94.42		
4.71√(E/Fy) =	103.55	=> kL/r	≤ 4.71√(E/Fy)
Fcr =	27.44	ksi	
Fe =	32.10	ksi	
Pn =	61.196	k	

Torsional/Flexural Torsional Buckling:

Fcr =	20.6391	ksi
Fey =	81.8881	ksi
Fez =	26.2099	ksi
Pn =	46.0252	k

Bending (Strong Axis):

Yielding:				
Mn =	21.95	k-ft		
Flange Local Buckling:				
Mn =	19.207	k-ft		
Pr/Pc =	0.17	<	0.2	
Utilization =	0.93	<	1.0	OK

Bending (Weak Axis):

Yielding:				
Mn =	14.65	k-ft		
Flange Local Buckling:				
Mn =	14.39	k-ft		
Pr/Pc =	0.170	<	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 93%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL								

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-8.366	-8.366	0	0
2	M11	Y	-8.366	-8.366	0	0
3	M12	Y	-8.366	-8.366	0	0
4	M13	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-4.45	-4.45	0	0
2	M11	Y	-4.45	-4.45	0	0
3	M12	Y	-4.45	-4.45	0	0
4	M13	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-54.031	-54.031	0	0
2	M11	Y	-54.031	-54.031	0	0
3	M12	Y	-54.031	-54.031	0	0
4	M13	Y	-54.031	-54.031	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-33.217	-33.217	0	0
2	M11	y	-33.217	-33.217	0	0
3	M12	y	-52.198	-52.198	0	0
4	M13	y	-52.198	-52.198	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	67.066	67.066	0	0
2	M11	y	67.066	67.066	0	0
3	M12	y	31.635	31.635	0	0
4	M13	y	31.635	31.635	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8																
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6																
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6														
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3														
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3														
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25														
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25														

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
8																										
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																		
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1																
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75																
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1														
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875														
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656														
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875														

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	340.311	2	2583.2	1	372.829	1	.396	1	.003	3	6.247	1
2		min	-511.046	3	-1234.842	3	-249.785	3	-.247	3	-.008	1	.21	15
3	N19	max	1469.502	2	7069.332	1	0	1	0	1	0	1	14.056	1
4		min	-1462.478	3	-3684.363	3	0	12	0	12	0	3	.425	15
5	N29	max	340.311	2	2583.2	1	249.785	3	.247	3	.008	1	6.247	1
6		min	-511.046	3	-1234.842	3	-372.829	1	-.396	1	-.003	3	.21	15
7	Totals:	max	2150.125	2	12235.731	1	0	14						
8		min	-2484.569	3	-6154.048	3	0	3						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.006	1	0	3	0	1	0	1	0	1
2			min	0	1	0	3	-.001	1	0	1	0	1	0	1
3		2	max	-.179	15	-.49	15	0	3	0	1	0	12	0	4
4			min	-.76	4	-2.085	4	-.001	1	0	1	0	1	0	15
5		3	max	-6.743	12	205.754	3	9.285	3	.057	3	.314	1	.28	1
6			min	-203.157	1	-636.484	1	-209.082	1	-.256	1	.01	12	-.089	3
7		4	max	-7.039	12	204.534	3	9.285	3	.057	3	.184	1	.675	1
8			min	-203.749	1	-638.11	1	-209.082	1	-.256	1	.007	15	-.216	3
9		5	max	-7.335	12	203.315	3	9.285	3	.057	3	.055	1	1.072	1
10			min	-204.341	1	-639.736	1	-209.082	1	-.256	1	-.01	10	-.343	3
11		6	max	397.179	3	552.857	1	32.945	3	.043	1	.152	1	1.031	1
12			min	-1707.22	1	-128.24	3	-278.468	1	-.046	3	-.043	3	-.347	3
13		7	max	396.735	3	551.231	1	32.945	3	.043	1	.013	10	.689	1
14			min	-1707.812	1	-129.459	3	-278.468	1	-.046	3	-.023	3	-.268	3
15		8	max	396.291	3	549.605	1	32.945	3	.043	1	-.002	12	.347	1
16			min	-1708.404	1	-130.679	3	-278.468	1	-.046	3	-.194	1	-.187	3
17		9	max	386.808	3	59.226	3	34.014	3	-.004	15	.097	1	.154	1
18			min	-1918.98	1	-69.042	1	-284.245	1	-.217	2	.001	10	-.15	3
19		10	max	386.365	3	58.006	3	34.014	3	-.004	15	.05	3	.197	1
20			min	-1919.572	1	-70.668	1	-284.245	1	-.217	2	-.08	1	-.186	3
21		11	max	385.921	3	56.787	3	34.014	3	-.004	15	.072	3	.242	1
22			min	-1920.164	1	-72.294	1	-284.245	1	-.217	2	-.256	1	-.222	3
23		12	max	374.173	3	551.977	3	142.33	2	.355	3	.165	1	.517	1
24			min	-2125.965	1	-632.165	1	-226.665	3	-.529	1	.006	15	-.454	3
25		13	max	373.729	3	550.758	3	142.33	2	.355	3	.242	1	.909	1
26			min	-2126.557	1	-633.791	1	-226.665	3	-.529	1	-.123	3	-.796	3
27		14	max	205.401	1	567.615	1	-.342	3	.359	1	0	10	1.287	1
28			min	6.913	12	-488.435	3	-178.592	1	-.359	3	-.006	1	-1.123	3
29		15	max	204.809	1	565.989	1	-.342	3	.359	1	-.001	12	.935	1
30			min	6.617	12	-489.654	3	-178.592	1	-.359	3	-.117	1	-.82	3
31		16	max	204.218	1	564.363	1	-.342	3	.359	1	-.002	12	.584	1
32			min	6.321	12	-490.874	3	-178.592	1	-.359	3	-.228	1	-.515	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
33		17	max	203.626	1	562.737	1	-.342	3	.359	1	-.002	12	.235	1
34			min	6.025	12	-492.093	3	-178.592	1	-.359	3	-.339	1	-.21	3
35		18	max	.76	4	2.087	4	0	1	0	1	0	15	0	4
36			min	.179	15	.491	15	0	5	0	1	0	1	0	15
37		19	max	0	1	0	1	0	1	0	1	0	1	0	1
38			min	0	1	-.002	3	0	5	0	1	0	1	0	1
39	M4	1	max	0	1	.014	1	0	1	0	1	0	1	0	1
40			min	0	1	-.003	3	0	1	0	1	0	1	0	1
41		2	max	-.179	15	-.49	15	0	1	0	1	0	1	0	4
42			min	-.76	4	-2.083	4	0	1	0	1	0	1	0	15
43		3	max	-14.117	15	629.25	3	0	1	0	1	0	1	.687	1
44			min	-370.461	1	-1803.781	1	0	1	0	1	0	1	-.242	3
45		4	max	-14.296	15	628.031	3	0	1	0	1	0	1	1.807	1
46			min	-371.053	1	-1805.407	1	0	1	0	1	0	1	-.632	3
47		5	max	-14.474	15	626.811	3	0	1	0	1	0	1	2.928	1
48			min	-371.645	1	-1807.033	1	0	1	0	1	0	1	-1.021	3
49		6	max	1333.286	3	1608.851	1	0	1	0	1	0	1	2.797	1
50			min	-4680.062	1	-463.588	3	0	1	0	1	0	1	-1.01	3
51		7	max	1332.842	3	1607.225	1	0	1	0	1	0	1	1.799	1
52			min	-4680.654	1	-464.808	3	0	1	0	1	0	1	-.722	3
53		8	max	1332.398	3	1605.599	1	0	1	0	1	0	1	.802	1
54			min	-4681.246	1	-466.027	3	0	1	0	1	0	1	-.433	3
55		9	max	1307.878	3	194.664	3	0	1	0	1	0	1	.206	1
56			min	-5035.093	1	-264.636	1	0	1	0	1	0	1	-.289	3
57		10	max	1307.434	3	193.445	3	0	1	0	1	0	1	.371	1
58			min	-5035.684	1	-266.262	1	0	1	0	1	0	1	-.41	3
59		11	max	1306.99	3	192.225	3	0	1	0	1	0	1	.537	1
60			min	-5036.276	1	-267.888	1	0	1	0	1	0	1	-.529	3
61		12	max	1287	3	1543.397	3	0	1	0	1	0	1	1.339	1
62			min	-5399.674	1	-1914.719	1	0	1	0	1	0	1	-1.184	3
63		13	max	1286.556	3	1542.178	3	0	1	0	1	0	1	2.528	1
64			min	-5400.266	1	-1916.345	1	0	1	0	1	0	1	-2.141	3
65		14	max	371.299	1	1626.893	1	0	1	0	1	0	1	3.669	1
66			min	14.569	15	-1357.615	3	0	1	0	1	0	1	-3.058	3
67		15	max	370.707	1	1625.266	1	0	1	0	1	0	1	2.66	1
68			min	14.391	15	-1358.835	3	0	1	0	1	0	1	-2.215	3
69		16	max	370.116	1	1623.64	1	0	1	0	1	0	1	1.652	1
70			min	14.212	15	-1360.054	3	0	1	0	1	0	1	-1.372	3
71		17	max	369.524	1	1622.014	1	0	1	0	1	0	1	.645	1
72			min	14.034	15	-1361.274	3	0	1	0	1	0	1	-.527	3
73		18	max	.76	4	2.088	4	0	1	0	1	0	1	0	4
74			min	.179	15	.491	15	0	1	0	1	0	1	0	15
75		19	max	0	1	.003	1	0	1	0	1	0	1	0	1
76			min	0	1	-.006	3	0	1	0	1	0	1	0	1
77	M7	1	max	0	1	.006	1	.001	1	0	1	0	1	0	1
78			min	0	1	0	3	0	3	0	1	0	1	0	1
79		2	max	-.179	15	-.49	15	.001	1	0	1	0	1	0	4
80			min	-.76	4	-2.085	4	0	3	0	1	0	12	0	15
81		3	max	-6.743	12	205.754	3	209.082	1	.256	1	-.01	12	.28	1
82			min	-203.157	1	-636.484	1	-9.285	3	-.057	3	-.314	1	-.089	3
83		4	max	-7.039	12	204.534	3	209.082	1	.256	1	-.007	15	.675	1
84			min	-203.749	1	-638.11	1	-9.285	3	-.057	3	-.184	1	-.216	3
85		5	max	-7.335	12	203.315	3	209.082	1	.256	1	.01	10	1.072	1
86			min	-204.341	1	-639.736	1	-9.285	3	-.057	3	-.055	1	-.343	3
87		6	max	397.179	3	552.857	1	278.468	1	.046	3	.043	3	1.031	1
88			min	-1707.22	1	-128.24	3	-32.945	3	-.043	1	-.152	1	-.347	3
89		7	max	396.735	3	551.231	1	278.468	1	.046	3	.023	3	.689	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
90			min	-1707.812	1	-129.459	3	-32.945	3	-.043	1	-.013	10	-.268	3
91		8	max	396.291	3	549.605	1	278.468	1	.046	3	.194	1	.347	1
92			min	-1708.404	1	-130.679	3	-32.945	3	-.043	1	.002	12	-.187	3
93		9	max	386.808	3	59.226	3	284.245	1	.217	2	-.001	10	.154	1
94			min	-1918.98	1	-69.042	1	-34.014	3	.004	15	-.097	1	-.15	3
95		10	max	386.365	3	58.006	3	284.245	1	.217	2	.08	1	.197	1
96			min	-1919.572	1	-70.668	1	-34.014	3	.004	15	-.05	3	-.186	3
97		11	max	385.921	3	56.787	3	284.245	1	.217	2	.256	1	.242	1
98			min	-1920.164	1	-72.294	1	-34.014	3	.004	15	-.072	3	-.222	3
99		12	max	374.173	3	551.977	3	226.665	3	.529	1	-.006	15	.517	1
100			min	-2125.965	1	-632.165	1	-142.33	2	-.355	3	-.165	1	-.454	3
101		13	max	373.729	3	550.758	3	226.665	3	.529	1	.123	3	.909	1
102			min	-2126.557	1	-633.791	1	-142.33	2	-.355	3	-.242	1	-.796	3
103		14	max	205.401	1	567.615	1	178.592	1	.359	3	.006	1	1.287	1
104			min	6.913	12	-488.435	3	.342	3	-.359	1	0	10	-1.123	3
105		15	max	204.809	1	565.989	1	178.592	1	.359	3	.117	1	.935	1
106			min	6.617	12	-489.654	3	.342	3	-.359	1	.001	12	-.82	3
107		16	max	204.218	1	564.363	1	178.592	1	.359	3	.228	1	.584	1
108			min	6.321	12	-490.874	3	.342	3	-.359	1	.002	12	-.515	3
109		17	max	203.626	1	562.737	1	178.592	1	.359	3	.339	1	.235	1
110			min	6.025	12	-492.093	3	.342	3	-.359	1	.002	12	-.21	3
111		18	max	.76	4	2.087	4	0	5	0	1	0	1	0	4
112			min	.179	15	.491	15	0	1	0	1	0	15	0	15
113		19	max	0	1	0	1	0	5	0	1	0	1	0	1
114			min	0	1	-.002	3	0	1	0	1	0	1	0	1
115	M10	1	max	178.548	1	559.263	1	-5.433	12	.006	1	.411	1	.359	1
116			min	.346	3	-494.473	3	-202.894	1	-.012	3	.002	12	-.359	3
117		2	max	178.548	1	407.285	1	-3.872	12	.006	1	.179	1	.189	3
118			min	.346	3	-363.794	3	-159.937	1	-.012	3	-.006	3	-.259	1
119		3	max	178.548	1	255.307	1	-2.311	12	.006	1	.022	2	.57	3
120			min	.346	3	-233.116	3	-116.98	1	-.012	3	-.012	3	-.682	1
121		4	max	178.548	1	103.329	1	-.749	12	.006	1	-.003	10	.785	3
122			min	.346	3	-102.438	3	-74.023	1	-.012	3	-.12	1	-.911	1
123		5	max	178.548	1	28.241	3	1.391	3	.006	1	-.007	15	.832	3
124			min	.346	3	-48.65	1	-31.066	1	-.012	3	-.187	1	-.946	1
125		6	max	178.548	1	158.919	3	11.891	1	.006	1	-.007	15	.712	3
126			min	.346	3	-200.628	1	-3.475	10	-.012	3	-.199	1	-.787	1
127		7	max	178.548	1	289.598	3	54.848	1	.006	1	-.003	12	.426	3
128			min	.346	3	-352.606	1	.838	10	-.012	3	-.157	1	-.434	1
129		8	max	178.548	1	420.276	3	97.805	1	.006	1	.004	3	.114	1
130			min	.346	3	-504.585	1	3.715	15	-.012	3	-.059	1	-.028	3
131		9	max	178.548	1	550.954	3	140.762	1	.006	1	.093	1	.856	1
132			min	.346	3	-656.563	1	5.276	15	-.012	3	-.012	10	-.648	3
133		10	max	178.548	1	808.541	1	-6.838	15	.012	3	.301	1	1.792	1
134			min	.346	3	-681.633	3	-183.719	1	-.006	1	.003	10	-1.436	3
135		11	max	178.548	1	656.563	1	-5.276	15	.012	3	.093	1	.856	1
136			min	.346	3	-550.954	3	-140.762	1	-.006	1	-.012	10	-.648	3
137		12	max	178.548	1	504.585	1	-3.715	15	.012	3	.004	3	.114	1
138			min	.346	3	-420.276	3	-97.805	1	-.006	1	-.059	1	-.028	3
139		13	max	178.548	1	352.606	1	-.838	10	.012	3	-.003	12	.426	3
140			min	.346	3	-289.598	3	-54.848	1	-.006	1	-.157	1	-.434	1
141		14	max	178.548	1	200.628	1	3.475	10	.012	3	-.007	15	.712	3
142			min	.346	3	-158.919	3	-11.891	1	-.006	1	-.199	1	-.787	1
143		15	max	178.548	1	48.65	1	31.066	1	.012	3	-.007	15	.832	3
144			min	.346	3	-28.241	3	-1.391	3	-.006	1	-.187	1	-.946	1
145		16	max	178.548	1	102.438	3	74.023	1	.012	3	-.003	10	.785	3
146			min	.346	3	-103.329	1	.749	12	-.006	1	-.12	1	-.911	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
147		17	max	178.548	1	233.116	3	116.98	1	.012	3	.022	2	.57	3
148			min	.346	3	-255.307	1	2.311	12	-.006	1	-.012	3	-.682	1
149		18	max	178.548	1	363.794	3	159.937	1	.012	3	.179	1	.189	3
150			min	.346	3	-407.285	1	3.872	12	-.006	1	-.006	3	-.259	1
151		19	max	178.548	1	494.473	3	202.894	1	.012	3	.411	1	.359	1
152			min	.346	3	-559.263	1	5.433	12	-.006	1	.002	12	-.359	3
153	M11	1	max	407.358	1	555.413	1	-7.356	15	0	3	.436	1	.326	1
154			min	-260.555	3	-497.133	3	-206.248	1	-.008	1	.015	15	-.437	3
155		2	max	407.358	1	403.434	1	-5.795	15	0	3	.2	1	.115	3
156			min	-260.555	3	-366.455	3	-163.291	1	-.008	1	.007	15	-.287	1
157		3	max	407.358	1	251.456	1	-4.233	15	0	3	.024	2	.5	3
158			min	-260.555	3	-235.776	3	-120.334	1	-.008	1	0	15	-.705	1
159		4	max	407.358	1	99.478	1	-2.672	15	0	3	-.001	12	.718	3
160			min	-260.555	3	-105.098	3	-77.378	1	-.008	1	-.107	1	-.929	1
161		5	max	407.358	1	25.581	3	-1.11	15	0	3	-.004	12	.768	3
162			min	-260.555	3	-52.5	1	-34.421	1	-.008	1	-.179	1	-.959	1
163		6	max	407.358	1	156.259	3	8.536	1	0	3	-.005	12	.652	3
164			min	-260.555	3	-204.479	1	-3.168	10	-.008	1	-.195	1	-.795	1
165		7	max	407.358	1	286.937	3	51.493	1	0	3	-.003	12	.369	3
166			min	-260.555	3	-356.457	1	1.146	10	-.008	1	-.157	1	-.437	1
167		8	max	407.358	1	417.616	3	94.45	1	0	3	0	3	.116	1
168			min	-260.555	3	-508.435	1	3.382	12	-.008	1	-.064	1	-.081	3
169		9	max	407.358	1	548.294	3	137.407	1	0	3	.085	1	.862	1
170			min	-260.555	3	-660.414	1	4.944	12	-.008	1	-.011	10	-.698	3
171		10	max	407.358	1	812.392	1	-6.505	12	0	12	.288	1	1.803	1
172			min	-260.555	3	-678.973	3	-180.364	1	-.008	1	.004	10	-1.482	3
173		11	max	407.358	1	660.414	1	-4.944	12	.008	1	.085	1	.862	1
174			min	-260.555	3	-548.294	3	-137.407	1	0	3	-.011	10	-.698	3
175		12	max	407.358	1	508.435	1	-3.382	12	.008	1	0	3	.116	1
176			min	-260.555	3	-417.616	3	-94.45	1	0	3	-.064	1	-.081	3
177		13	max	407.358	1	356.457	1	-1.146	10	.008	1	-.003	12	.369	3
178			min	-260.555	3	-286.937	3	-51.493	1	0	3	-.157	1	-.437	1
179		14	max	407.358	1	204.479	1	3.168	10	.008	1	-.005	12	.652	3
180			min	-260.555	3	-156.259	3	-8.536	1	0	3	-.195	1	-.795	1
181		15	max	407.358	1	52.5	1	34.421	1	.008	1	-.004	12	.768	3
182			min	-260.555	3	-25.581	3	1.11	15	0	3	-.179	1	-.959	1
183		16	max	407.358	1	105.098	3	77.378	1	.008	1	-.001	12	.718	3
184			min	-260.555	3	-99.478	1	2.672	15	0	3	-.107	1	-.929	1
185		17	max	407.358	1	235.776	3	120.334	1	.008	1	.024	2	.5	3
186			min	-260.555	3	-251.456	1	4.233	15	0	3	0	15	-.705	1
187		18	max	407.358	1	366.455	3	163.291	1	.008	1	.2	1	.115	3
188			min	-260.555	3	-403.434	1	5.795	15	0	3	.007	15	-.287	1
189		19	max	407.358	1	497.133	3	206.248	1	.008	1	.436	1	.326	1
190			min	-260.555	3	-555.413	1	7.356	15	0	3	.015	15	-.437	3
191	M12	1	max	32.262	2	615.211	1	-6.112	12	.001	3	.465	1	.25	2
192			min	-16.708	9	-191.549	3	-209.974	1	-.009	1	.008	12	.005	15
193		2	max	32.262	2	443.83	1	-4.551	12	.001	3	.224	1	.243	3
194			min	-16.708	9	-133.307	3	-167.017	1	-.009	1	0	3	-.429	1
195		3	max	32.262	2	272.449	1	-2.99	12	.001	3	.039	2	.376	3
196			min	-16.708	9	-75.066	3	-124.06	1	-.009	1	-.006	3	-.887	1
197		4	max	32.262	2	101.068	1	-1.428	12	.001	3	0	10	.435	3
198			min	-16.708	9	-16.824	3	-81.103	1	-.009	1	-.093	1	-1.126	1
199		5	max	32.262	2	41.418	3	.329	3	.001	3	-.006	15	.419	3
200			min	-16.708	9	-70.313	1	-38.146	1	-.009	1	-.169	1	-1.145	1
201		6	max	32.262	2	99.659	3	6.162	9	.001	3	-.006	12	.329	3
202			min	-16.708	9	-241.695	1	-5.286	2	-.009	1	-.191	1	-.946	1
203		7	max	32.262	2	157.901	3	47.768	1	.001	3	-.003	12	.165	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
204			min	-16.708	9	-413.076	1	-.29	10	-.009	1	-.157	1	-.528	1
205		8	max	32.262	2	216.143	3	90.725	1	.001	3	.003	3	.11	1
206			min	-16.708	9	-584.457	1	3.472	15	-.009	1	-.069	1	-.074	3
207		9	max	32.262	2	274.385	3	133.681	1	.001	3	.075	1	.966	1
208			min	-16.708	9	-755.838	1	5.034	15	-.009	1	-.015	10	-.388	3
209		10	max	32.262	2	927.219	1	-6.595	15	.001	3	.273	1	2.041	1
210			min	-16.708	9	-332.626	3	-176.638	1	-.009	1	-.001	10	-.776	3
211		11	max	32.262	2	755.838	1	-5.034	15	.009	1	.075	1	.966	1
212			min	-16.708	9	-274.385	3	-133.681	1	-.001	3	-.015	10	-.388	3
213		12	max	32.262	2	584.457	1	-3.472	15	.009	1	.003	3	.11	1
214			min	-16.708	9	-216.143	3	-90.725	1	-.001	3	-.069	1	-.074	3
215		13	max	32.262	2	413.076	1	.29	10	.009	1	-.003	12	.165	3
216			min	-16.708	9	-157.901	3	-47.768	1	-.001	3	-.157	1	-.528	1
217		14	max	32.262	2	241.695	1	5.286	2	.009	1	-.006	12	.329	3
218			min	-16.708	9	-99.659	3	-6.162	9	-.001	3	-.191	1	-.946	1
219		15	max	32.262	2	70.313	1	38.146	1	.009	1	-.006	15	.419	3
220			min	-16.708	9	-41.418	3	-.329	3	-.001	3	-.169	1	-1.145	1
221		16	max	32.262	2	16.824	3	81.103	1	.009	1	0	10	.435	3
222			min	-16.708	9	-101.068	1	1.428	12	-.001	3	-.093	1	-1.126	1
223		17	max	32.262	2	75.066	3	124.06	1	.009	1	.039	2	.376	3
224			min	-16.708	9	-272.449	1	2.99	12	-.001	3	-.006	3	-.887	1
225		18	max	32.262	2	133.307	3	167.017	1	.009	1	.224	1	.243	3
226			min	-16.708	9	-443.83	1	4.551	12	-.001	3	0	3	-.429	1
227		19	max	32.262	2	191.549	3	209.974	1	.009	1	.465	1	.25	2
228			min	-16.708	9	-615.211	1	6.112	12	-.001	3	.008	12	.005	15
229	M13	1	max	9.285	3	634.584	1	-6.151	12	.006	3	.399	1	.256	1
230			min	-208.913	1	-208.234	3	-201.43	1	-.022	1	.008	12	-.057	3
231		2	max	9.285	3	463.203	1	-4.589	12	.006	3	.169	1	.172	3
232			min	-208.913	1	-149.993	3	-158.473	1	-.022	1	.001	12	-.445	1
233		3	max	9.285	3	291.822	1	-3.028	12	.006	3	.015	2	.327	3
234			min	-208.913	1	-91.751	3	-115.516	1	-.022	1	-.012	9	-.927	1
235		4	max	9.285	3	120.441	1	-1.467	12	.006	3	-.005	15	.407	3
236			min	-208.913	1	-33.509	3	-72.559	1	-.022	1	-.126	1	-1.191	1
237		5	max	9.285	3	24.732	3	.239	3	.006	3	-.007	15	.412	3
238			min	-208.913	1	-50.94	1	-29.602	1	-.022	1	-.192	1	-1.235	1
239		6	max	9.285	3	82.974	3	13.355	1	.006	3	-.006	12	.344	3
240			min	-208.913	1	-222.321	1	-2.979	10	-.022	1	-.202	1	-1.06	1
241		7	max	9.285	3	141.216	3	56.312	1	.006	3	-.003	12	.2	3
242			min	-208.913	1	-393.702	1	1.335	10	-.022	1	-.158	1	-.667	1
243		8	max	9.285	3	199.457	3	99.268	1	.006	3	.003	3	-.002	15
244			min	-208.913	1	-565.083	1	3.758	15	-.022	1	-.058	1	-.054	1
245		9	max	9.285	3	257.699	3	142.225	1	.006	3	.096	1	.777	1
246			min	-208.913	1	-736.464	1	5.319	15	-.022	1	-.011	10	-.309	3
247		10	max	9.285	3	907.846	1	-6.881	15	.006	3	.305	1	1.828	1
248			min	-208.913	1	-315.941	3	-185.182	1	-.022	1	.005	10	-.676	3
249		11	max	9.285	3	736.464	1	-5.319	15	.022	1	.096	1	.777	1
250			min	-208.913	1	-257.699	3	-142.225	1	-.006	3	-.011	10	-.309	3
251		12	max	9.285	3	565.083	1	-3.758	15	.022	1	.003	3	-.002	15
252			min	-208.913	1	-199.457	3	-99.268	1	-.006	3	-.058	1	-.054	1
253		13	max	9.285	3	393.702	1	-1.335	10	.022	1	-.003	12	.2	3
254			min	-208.913	1	-141.216	3	-56.312	1	-.006	3	-.158	1	-.667	1
255		14	max	9.285	3	222.321	1	2.979	10	.022	1	-.006	12	.344	3
256			min	-208.913	1	-82.974	3	-13.355	1	-.006	3	-.202	1	-1.06	1
257		15	max	9.285	3	50.94	1	29.602	1	.022	1	-.007	15	.412	3
258			min	-208.913	1	-24.732	3	-.239	3	-.006	3	-.192	1	-1.235	1
259		16	max	9.285	3	33.509	3	72.559	1	.022	1	-.005	15	.407	3
260			min	-208.913	1	-120.441	1	1.467	12	-.006	3	-.126	1	-1.191	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
261		17	max	9.285	3	91.751	3	115.516	1	.022	1	.015	2	.327	3
262			min	-208.913	1	-291.822	1	3.028	12	-.006	3	-.012	9	-.927	1
263		18	max	9.285	3	149.993	3	158.473	1	.022	1	.169	1	.172	3
264			min	-208.913	1	-463.203	1	4.589	12	-.006	3	.001	12	-.445	1
265		19	max	9.285	3	208.234	3	201.43	1	.022	1	.399	1	.256	1
266			min	-208.913	1	-634.584	1	6.151	12	-.006	3	.008	12	-.057	3
267	M2	1	max	2583.2	1	510.919	3	373.261	1	.003	3	.247	3	6.247	1
268			min	-1234.842	3	-338.408	2	-249.659	3	-.008	1	-.396	1	.21	15
269		2	max	2580.939	1	510.919	3	373.261	1	.003	3	.185	3	6.256	1
270			min	-1236.538	3	-338.408	2	-249.659	3	-.008	1	-.303	1	.209	15
271		3	max	2578.678	1	510.919	3	373.261	1	.003	3	.123	3	6.265	1
272			min	-1238.233	3	-338.408	2	-249.659	3	-.008	1	-.21	1	.192	12
273		4	max	2576.418	1	510.919	3	373.261	1	.003	3	.061	3	6.273	1
274			min	-1239.929	3	-338.408	2	-249.659	3	-.008	1	-.118	1	.113	12
275		5	max	1968.677	1	1789.201	1	301.638	1	.003	1	.027	3	6.219	1
276			min	-1076.352	3	12.615	12	-226.484	3	-.001	3	-.104	1	.044	12
277		6	max	1966.417	1	1789.201	1	301.638	1	.003	1	0	10	5.774	1
278			min	-1078.047	3	12.615	12	-226.484	3	-.001	3	-.029	1	.041	12
279		7	max	1964.156	1	1789.201	1	301.638	1	.003	1	.049	2	5.33	1
280			min	-1079.743	3	12.615	12	-226.484	3	-.001	3	-.085	3	.038	12
281		8	max	1961.896	1	1789.201	1	301.638	1	.003	1	.12	1	4.886	1
282			min	-1081.438	3	12.615	12	-226.484	3	-.001	3	-.141	3	.034	12
283		9	max	1959.635	1	1789.201	1	301.638	1	.003	1	.195	1	4.442	1
284			min	-1083.134	3	12.615	12	-226.484	3	-.001	3	-.197	3	.031	12
285		10	max	1957.374	1	1789.201	1	301.638	1	.003	1	.27	1	3.998	1
286			min	-1084.829	3	12.615	12	-226.484	3	-.001	3	-.254	3	.028	12
287		11	max	1955.114	1	1789.201	1	301.638	1	.003	1	.345	1	3.553	1
288			min	-1086.525	3	12.615	12	-226.484	3	-.001	3	-.31	3	.025	12
289		12	max	1952.853	1	1789.201	1	301.638	1	.003	1	.42	1	3.109	1
290			min	-1088.22	3	12.615	12	-226.484	3	-.001	3	-.366	3	.022	12
291		13	max	1950.593	1	1789.201	1	301.638	1	.003	1	.495	1	2.665	1
292			min	-1089.915	3	12.615	12	-226.484	3	-.001	3	-.422	3	.019	12
293		14	max	1948.332	1	1789.201	1	301.638	1	.003	1	.57	1	2.221	1
294			min	-1091.611	3	12.615	12	-226.484	3	-.001	3	-.479	3	.016	12
295		15	max	1946.071	1	1789.201	1	301.638	1	.003	1	.645	1	1.777	1
296			min	-1093.306	3	12.615	12	-226.484	3	-.001	3	-.535	3	.013	12
297		16	max	1943.811	1	1789.201	1	301.638	1	.003	1	.719	1	1.333	1
298			min	-1095.002	3	12.615	12	-226.484	3	-.001	3	-.591	3	.009	12
299		17	max	1941.55	1	1789.201	1	301.638	1	.003	1	.794	1	.888	1
300			min	-1096.697	3	12.615	12	-226.484	3	-.001	3	-.647	3	.006	12
301		18	max	1939.29	1	1789.201	1	301.638	1	.003	1	.869	1	.444	1
302			min	-1098.393	3	12.615	12	-226.484	3	-.001	3	-.704	3	.003	12
303		19	max	1937.029	1	1789.201	1	301.638	1	.003	1	.944	1	0	1
304			min	-1100.088	3	12.615	12	-226.484	3	-.001	3	-.76	3	0	1
305	M5	1	max	7069.332	1	1462.042	3	0	1	0	1	0	1	14.056	1
306			min	-3684.363	3	-1456.833	2	0	1	0	1	0	1	.425	15
307		2	max	7067.071	1	1462.042	3	0	1	0	1	0	1	14.298	1
308			min	-3686.059	3	-1456.833	2	0	1	0	1	0	1	.262	12
309		3	max	7064.811	1	1462.042	3	0	1	0	1	0	1	14.54	1
310			min	-3687.754	3	-1456.833	2	0	1	0	1	0	1	.015	3
311		4	max	7062.55	1	1462.042	3	0	1	0	1	0	1	14.782	1
312			min	-3689.45	3	-1456.833	2	0	1	0	1	0	1	-.348	3
313		5	max	5389.25	1	4270.196	1	0	1	0	1	0	1	14.842	1
314			min	-3133.79	3	-188.091	3	0	1	0	1	0	1	-.654	3
315		6	max	5386.99	1	4270.196	1	0	1	0	1	0	1	13.781	1
316			min	-3135.485	3	-188.091	3	0	1	0	1	0	1	-.607	3
317		7	max	5384.729	1	4270.196	1	0	1	0	1	0	1	12.721	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
318			min	-3137.181	3	-188.091	3	0	1	0	1	0	1	-.56	3
319		8	max	5382.469	1	4270.196	1	0	1	0	1	0	1	11.661	1
320			min	-3138.876	3	-188.091	3	0	1	0	1	0	1	-.514	3
321		9	max	5380.208	1	4270.196	1	0	1	0	1	0	1	10.601	1
322			min	-3140.572	3	-188.091	3	0	1	0	1	0	1	-.467	3
323		10	max	5377.947	1	4270.196	1	0	1	0	1	0	1	9.541	1
324			min	-3142.267	3	-188.091	3	0	1	0	1	0	1	-.42	3
325		11	max	5375.687	1	4270.196	1	0	1	0	1	0	1	8.481	1
326			min	-3143.962	3	-188.091	3	0	1	0	1	0	1	-.374	3
327		12	max	5373.426	1	4270.196	1	0	1	0	1	0	1	7.421	1
328			min	-3145.658	3	-188.091	3	0	1	0	1	0	1	-.327	3
329		13	max	5371.166	1	4270.196	1	0	1	0	1	0	1	6.361	1
330			min	-3147.353	3	-188.091	3	0	1	0	1	0	1	-.28	3
331		14	max	5368.905	1	4270.196	1	0	1	0	1	0	1	5.301	1
332			min	-3149.049	3	-188.091	3	0	1	0	1	0	1	-.233	3
333		15	max	5366.644	1	4270.196	1	0	1	0	1	0	1	4.24	1
334			min	-3150.744	3	-188.091	3	0	1	0	1	0	1	-.187	3
335		16	max	5364.384	1	4270.196	1	0	1	0	1	0	1	3.18	1
336			min	-3152.44	3	-188.091	3	0	1	0	1	0	1	-.14	3
337		17	max	5362.123	1	4270.196	1	0	1	0	1	0	1	2.12	1
338			min	-3154.135	3	-188.091	3	0	1	0	1	0	1	-.093	3
339		18	max	5359.863	1	4270.196	1	0	1	0	1	0	1	1.06	1
340			min	-3155.831	3	-188.091	3	0	1	0	1	0	1	-.047	3
341		19	max	5357.602	1	4270.196	1	0	1	0	1	0	1	0	1
342			min	-3157.526	3	-188.091	3	0	1	0	1	0	1	0	1
343	M8	1	max	2583.2	1	510.919	3	249.659	3	.008	1	.396	1	6.247	1
344			min	-1234.842	3	-338.408	2	-373.261	1	-.003	3	-.247	3	.21	15
345		2	max	2580.939	1	510.919	3	249.659	3	.008	1	.303	1	6.256	1
346			min	-1236.538	3	-338.408	2	-373.261	1	-.003	3	-.185	3	.209	15
347		3	max	2578.678	1	510.919	3	249.659	3	.008	1	.21	1	6.265	1
348			min	-1238.233	3	-338.408	2	-373.261	1	-.003	3	-.123	3	.192	12
349		4	max	2576.418	1	510.919	3	249.659	3	.008	1	.118	1	6.273	1
350			min	-1239.929	3	-338.408	2	-373.261	1	-.003	3	-.061	3	.113	12
351		5	max	1968.677	1	1789.201	1	226.484	3	.001	3	.104	1	6.219	1
352			min	-1076.352	3	12.615	12	-301.638	1	-.003	1	-.027	3	.044	12
353		6	max	1966.417	1	1789.201	1	226.484	3	.001	3	.029	1	5.774	1
354			min	-1078.047	3	12.615	12	-301.638	1	-.003	1	0	10	.041	12
355		7	max	1964.156	1	1789.201	1	226.484	3	.001	3	.085	3	5.33	1
356			min	-1079.743	3	12.615	12	-301.638	1	-.003	1	-.049	2	.038	12
357		8	max	1961.896	1	1789.201	1	226.484	3	.001	3	.141	3	4.886	1
358			min	-1081.438	3	12.615	12	-301.638	1	-.003	1	-.12	1	.034	12
359		9	max	1959.635	1	1789.201	1	226.484	3	.001	3	.197	3	4.442	1
360			min	-1083.134	3	12.615	12	-301.638	1	-.003	1	-.195	1	.031	12
361		10	max	1957.374	1	1789.201	1	226.484	3	.001	3	.254	3	3.998	1
362			min	-1084.829	3	12.615	12	-301.638	1	-.003	1	-.27	1	.028	12
363		11	max	1955.114	1	1789.201	1	226.484	3	.001	3	.31	3	3.553	1
364			min	-1086.525	3	12.615	12	-301.638	1	-.003	1	-.345	1	.025	12
365		12	max	1952.853	1	1789.201	1	226.484	3	.001	3	.366	3	3.109	1
366			min	-1088.22	3	12.615	12	-301.638	1	-.003	1	-.42	1	.022	12
367		13	max	1950.593	1	1789.201	1	226.484	3	.001	3	.422	3	2.665	1
368			min	-1089.915	3	12.615	12	-301.638	1	-.003	1	-.495	1	.019	12
369		14	max	1948.332	1	1789.201	1	226.484	3	.001	3	.479	3	2.221	1
370			min	-1091.611	3	12.615	12	-301.638	1	-.003	1	-.57	1	.016	12
371		15	max	1946.071	1	1789.201	1	226.484	3	.001	3	.535	3	1.777	1
372			min	-1093.306	3	12.615	12	-301.638	1	-.003	1	-.645	1	.013	12
373		16	max	1943.811	1	1789.201	1	226.484	3	.001	3	.591	3	1.333	1
374			min	-1095.002	3	12.615	12	-301.638	1	-.003	1	-.719	1	.009	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
375		17	max	1941.55	1	1789.201	1	226.484	3	.001	3	.647	3	.888	1
376			min	-1096.697	3	12.615	12	-301.638	1	-.003	1	-.794	1	.006	12
377		18	max	1939.29	1	1789.201	1	226.484	3	.001	3	.704	3	.444	1
378			min	-1098.393	3	12.615	12	-301.638	1	-.003	1	-.869	1	.003	12
379		19	max	1937.029	1	1789.201	1	226.484	3	.001	3	.76	3	0	1
380			min	-1100.088	3	12.615	12	-301.638	1	-.003	1	-.944	1	0	1
381	M3	1	max	1914.475	1	4.757	4	70.18	1	.028	3	.014	1	0	1
382			min	-523.787	3	1.118	15	-23.662	3	-.076	1	-.005	3	0	1
383		2	max	1914.336	1	4.229	4	70.18	1	.028	3	.035	1	0	15
384			min	-523.892	3	.994	15	-23.662	3	-.076	1	-.012	3	-.001	4
385		3	max	1914.196	1	3.7	4	70.18	1	.028	3	.055	1	0	15
386			min	-523.996	3	.87	15	-23.662	3	-.076	1	-.019	3	-.002	4
387		4	max	1914.057	1	3.171	4	70.18	1	.028	3	.076	1	0	15
388			min	-524.101	3	.745	15	-23.662	3	-.076	1	-.026	3	-.003	4
389		5	max	1913.918	1	2.643	4	70.18	1	.028	3	.097	1	-.001	15
390			min	-524.206	3	.621	15	-23.662	3	-.076	1	-.033	3	-.004	4
391		6	max	1913.778	1	2.114	4	70.18	1	.028	3	.117	1	-.001	15
392			min	-524.31	3	.497	15	-23.662	3	-.076	1	-.04	3	-.005	4
393		7	max	1913.639	1	1.586	4	70.18	1	.028	3	.138	1	-.001	15
394			min	-524.415	3	.373	15	-23.662	3	-.076	1	-.047	3	-.006	4
395		8	max	1913.499	1	1.057	4	70.18	1	.028	3	.158	1	-.001	15
396			min	-524.519	3	.248	15	-23.662	3	-.076	1	-.054	3	-.006	4
397		9	max	1913.36	1	.529	4	70.18	1	.028	3	.179	1	-.001	15
398			min	-524.624	3	.124	15	-23.662	3	-.076	1	-.061	3	-.006	4
399		10	max	1913.221	1	0	1	70.18	1	.028	3	.199	1	-.001	15
400			min	-524.728	3	0	1	-23.662	3	-.076	1	-.068	3	-.006	4
401		11	max	1913.081	1	-.124	15	70.18	1	.028	3	.22	1	-.001	15
402			min	-524.833	3	-.529	4	-23.662	3	-.076	1	-.075	3	-.006	4
403		12	max	1912.942	1	-.248	15	70.18	1	.028	3	.241	1	-.001	15
404			min	-524.937	3	-1.057	4	-23.662	3	-.076	1	-.082	3	-.006	4
405		13	max	1912.802	1	-.373	15	70.18	1	.028	3	.261	1	-.001	15
406			min	-525.042	3	-1.586	4	-23.662	3	-.076	1	-.088	3	-.006	4
407		14	max	1912.663	1	-.497	15	70.18	1	.028	3	.282	1	-.001	15
408			min	-525.147	3	-2.114	4	-23.662	3	-.076	1	-.095	3	-.005	4
409		15	max	1912.524	1	-.621	15	70.18	1	.028	3	.302	1	-.001	15
410			min	-525.251	3	-2.643	4	-23.662	3	-.076	1	-.102	3	-.004	4
411		16	max	1912.384	1	-.745	15	70.18	1	.028	3	.323	1	0	15
412			min	-525.356	3	-3.171	4	-23.662	3	-.076	1	-.109	3	-.003	4
413		17	max	1912.245	1	-.87	15	70.18	1	.028	3	.343	1	0	15
414			min	-525.46	3	-3.7	4	-23.662	3	-.076	1	-.116	3	-.002	4
415		18	max	1912.105	1	-.994	15	70.18	1	.028	3	.364	1	0	15
416			min	-525.565	3	-4.229	4	-23.662	3	-.076	1	-.123	3	-.001	4
417		19	max	1911.966	1	-1.118	15	70.18	1	.028	3	.385	1	0	1
418			min	-525.669	3	-4.757	4	-23.662	3	-.076	1	-.13	3	0	1
419	M6	1	max	5451.449	1	4.757	4	0	1	0	1	0	1	0	1
420			min	-1743.146	3	1.118	15	0	1	0	1	0	1	0	1
421		2	max	5451.309	1	4.229	4	0	1	0	1	0	1	0	15
422			min	-1743.251	3	.994	15	0	1	0	1	0	1	-.001	4
423		3	max	5451.17	1	3.7	4	0	1	0	1	0	1	0	15
424			min	-1743.355	3	.87	15	0	1	0	1	0	1	-.002	4
425		4	max	5451.03	1	3.171	4	0	1	0	1	0	1	0	15
426			min	-1743.46	3	.745	15	0	1	0	1	0	1	-.003	4
427		5	max	5450.891	1	2.643	4	0	1	0	1	0	1	-.001	15
428			min	-1743.564	3	.621	15	0	1	0	1	0	1	-.004	4
429		6	max	5450.752	1	2.114	4	0	1	0	1	0	1	-.001	15
430			min	-1743.669	3	.497	15	0	1	0	1	0	1	-.005	4
431		7	max	5450.612	1	1.586	4	0	1	0	1	0	1	-.001	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
432			min	-1743.773	3	.373	15	0	1	0	1	0	1	-.006	4
433		8	max	5450.473	1	1.057	4	0	1	0	1	0	1	-.001	15
434			min	-1743.878	3	.248	15	0	1	0	1	0	1	-.006	4
435		9	max	5450.333	1	.529	4	0	1	0	1	0	1	-.001	15
436			min	-1743.982	3	.124	15	0	1	0	1	0	1	-.006	4
437		10	max	5450.194	1	0	1	0	1	0	1	0	1	-.001	15
438			min	-1744.087	3	0	1	0	1	0	1	0	1	-.006	4
439		11	max	5450.054	1	-.124	15	0	1	0	1	0	1	-.001	15
440			min	-1744.192	3	-.529	4	0	1	0	1	0	1	-.006	4
441		12	max	5449.915	1	-.248	15	0	1	0	1	0	1	-.001	15
442			min	-1744.296	3	-1.057	4	0	1	0	1	0	1	-.006	4
443		13	max	5449.776	1	-.373	15	0	1	0	1	0	1	-.001	15
444			min	-1744.401	3	-1.586	4	0	1	0	1	0	1	-.006	4
445		14	max	5449.636	1	-.497	15	0	1	0	1	0	1	-.001	15
446			min	-1744.505	3	-2.114	4	0	1	0	1	0	1	-.005	4
447		15	max	5449.497	1	-.621	15	0	1	0	1	0	1	-.001	15
448			min	-1744.61	3	-2.643	4	0	1	0	1	0	1	-.004	4
449		16	max	5449.357	1	-.745	15	0	1	0	1	0	1	0	15
450			min	-1744.714	3	-3.171	4	0	1	0	1	0	1	-.003	4
451		17	max	5449.218	1	-.87	15	0	1	0	1	0	1	0	15
452			min	-1744.819	3	-3.7	4	0	1	0	1	0	1	-.002	4
453		18	max	5449.079	1	-.994	15	0	1	0	1	0	1	0	15
454			min	-1744.923	3	-4.229	4	0	1	0	1	0	1	-.001	4
455		19	max	5448.939	1	-1.118	15	0	1	0	1	0	1	0	1
456			min	-1745.028	3	-4.757	4	0	1	0	1	0	1	0	1
457	M9	1	max	1914.475	1	4.757	4	23.662	3	.076	1	.005	3	0	1
458			min	-523.787	3	1.118	15	-70.18	1	-.028	3	-.014	1	0	1
459		2	max	1914.336	1	4.229	4	23.662	3	.076	1	.012	3	0	15
460			min	-523.892	3	.994	15	-70.18	1	-.028	3	-.035	1	-.001	4
461		3	max	1914.196	1	3.7	4	23.662	3	.076	1	.019	3	0	15
462			min	-523.996	3	.87	15	-70.18	1	-.028	3	-.055	1	-.002	4
463		4	max	1914.057	1	3.171	4	23.662	3	.076	1	.026	3	0	15
464			min	-524.101	3	.745	15	-70.18	1	-.028	3	-.076	1	-.003	4
465		5	max	1913.918	1	2.643	4	23.662	3	.076	1	.033	3	-.001	15
466			min	-524.206	3	.621	15	-70.18	1	-.028	3	-.097	1	-.004	4
467		6	max	1913.778	1	2.114	4	23.662	3	.076	1	.04	3	-.001	15
468			min	-524.31	3	.497	15	-70.18	1	-.028	3	-.117	1	-.005	4
469		7	max	1913.639	1	1.586	4	23.662	3	.076	1	.047	3	-.001	15
470			min	-524.415	3	.373	15	-70.18	1	-.028	3	-.138	1	-.006	4
471		8	max	1913.499	1	1.057	4	23.662	3	.076	1	.054	3	-.001	15
472			min	-524.519	3	.248	15	-70.18	1	-.028	3	-.158	1	-.006	4
473		9	max	1913.36	1	.529	4	23.662	3	.076	1	.061	3	-.001	15
474			min	-524.624	3	.124	15	-70.18	1	-.028	3	-.179	1	-.006	4
475		10	max	1913.221	1	0	1	23.662	3	.076	1	.068	3	-.001	15
476			min	-524.728	3	0	1	-70.18	1	-.028	3	-.199	1	-.006	4
477		11	max	1913.081	1	-.124	15	23.662	3	.076	1	.075	3	-.001	15
478			min	-524.833	3	-.529	4	-70.18	1	-.028	3	-.22	1	-.006	4
479		12	max	1912.942	1	-.248	15	23.662	3	.076	1	.082	3	-.001	15
480			min	-524.937	3	-1.057	4	-70.18	1	-.028	3	-.241	1	-.006	4
481		13	max	1912.802	1	-.373	15	23.662	3	.076	1	.088	3	-.001	15
482			min	-525.042	3	-1.586	4	-70.18	1	-.028	3	-.261	1	-.006	4
483		14	max	1912.663	1	-.497	15	23.662	3	.076	1	.095	3	-.001	15
484			min	-525.147	3	-2.114	4	-70.18	1	-.028	3	-.282	1	-.005	4
485		15	max	1912.524	1	-.621	15	23.662	3	.076	1	.102	3	-.001	15
486			min	-525.251	3	-2.643	4	-70.18	1	-.028	3	-.302	1	-.004	4
487		16	max	1912.384	1	-.745	15	23.662	3	.076	1	.109	3	0	15
488			min	-525.356	3	-3.171	4	-70.18	1	-.028	3	-.323	1	-.003	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
489		17	max	1912.245	1	-.87	15	23.662	3	.076	1	.116	3	0	15
490			min	-525.46	3	-3.7	4	-70.18	1	-.028	3	-.343	1	-.002	4
491		18	max	1912.105	1	-.994	15	23.662	3	.076	1	.123	3	0	15
492			min	-525.565	3	-4.229	4	-70.18	1	-.028	3	-.364	1	-.001	4
493		19	max	1911.966	1	-1.118	15	23.662	3	.076	1	.13	3	0	1
494			min	-525.669	3	-4.757	4	-70.18	1	-.028	3	-.385	1	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	-.004	12	.098	3	.031	1	1.035e-2	3	NC	3	NC	3
2			min	-.264	1	-.776	1	0	12	-3.316e-2	1	163.689	1	2430.542	1
3		2	max	-.004	12	.074	3	.01	1	1.035e-2	3	9064.591	12	NC	3
4			min	-.264	1	-.668	1	0	12	-3.316e-2	1	188.608	1	3928.904	1
5		3	max	-.004	12	.05	3	0	12	9.903e-3	3	6823.231	15	NC	2
6			min	-.264	1	-.56	1	-.008	1	-3.115e-2	1	222.514	1	8351.191	1
7		4	max	-.004	12	.027	3	0	12	9.222e-3	3	8128.093	15	NC	1
8			min	-.264	1	-.455	1	-.016	1	-2.806e-2	1	269.284	1	NC	1
9		5	max	-.004	12	.007	3	0	3	8.54e-3	3	9862.956	15	NC	1
10			min	-.264	1	-.36	1	-.017	1	-2.497e-2	1	333.031	1	NC	1
11		6	max	-.004	12	-.006	12	.002	3	8.591e-3	3	NC	15	NC	1
12			min	-.264	1	-.28	1	-.015	1	-2.402e-2	1	415.754	1	NC	1
13		7	max	-.004	12	-.007	15	.002	3	9.148e-3	3	NC	15	NC	2
14			min	-.263	1	-.214	1	-.007	1	-2.454e-2	1	521.63	1	7796.552	1
15		8	max	-.004	12	-.005	15	0	3	9.705e-3	3	NC	5	NC	2
16			min	-.263	1	-.159	1	-.001	2	-2.507e-2	1	666.684	1	5662.376	1
17		9	max	-.004	12	-.004	15	0	15	1.042e-2	3	NC	5	NC	2
18			min	-.262	1	-.107	1	0	3	-2.452e-2	1	894.97	1	5519.014	1
19		10	max	-.005	12	-.002	15	0	1	1.14e-2	3	NC	5	NC	2
20			min	-.261	1	-.058	1	0	3	-2.206e-2	1	1043.966	3	5368.524	1
21		11	max	-.005	12	0	15	.002	3	1.239e-2	3	NC	5	NC	2
22			min	-.26	1	-.03	3	-.002	1	-1.961e-2	1	1049.414	3	5882.095	1
23		12	max	-.005	12	.032	1	.006	3	1.001e-2	3	NC	1	NC	2
24			min	-.26	1	-.026	3	-.01	1	-1.465e-2	1	1079.829	3	9092.915	1
25		13	max	-.005	12	.069	1	.011	3	5.742e-3	3	NC	4	NC	1
26			min	-.259	1	-.017	3	-.013	1	-8.281e-3	1	1171.63	3	NC	1
27		14	max	-.005	12	.092	1	.012	3	1.659e-3	3	NC	4	NC	2
28			min	-.258	1	.003	12	-.008	2	-2.142e-3	1	1431.376	3	7886.152	1
29		15	max	-.005	12	.099	1	.009	3	5.986e-3	3	NC	4	NC	2
30			min	-.258	1	.003	15	-.002	2	-6.46e-3	1	2322.884	3	4965.578	1
31		16	max	-.005	12	.092	1	.008	1	1.031e-2	3	NC	3	NC	2
32			min	-.258	1	.003	15	0	10	-1.078e-2	1	2691.415	1	4087.694	1
33		17	max	-.005	12	.142	3	.006	1	1.464e-2	3	NC	4	NC	2
34			min	-.258	1	.003	15	0	15	-1.509e-2	1	3047.267	3	4406.99	1
35		18	max	-.005	12	.199	3	0	15	1.746e-2	3	NC	4	NC	2
36			min	-.258	1	.002	15	-.008	1	-1.791e-2	1	1325.151	3	8006.054	1
37		19	max	-.005	12	.256	3	0	15	1.746e-2	3	NC	1	NC	1
38			min	-.258	1	.002	15	-.025	1	-1.791e-2	1	847.212	3	NC	1
39	M4	1	max	.017	3	.332	3	0	1	0	1	NC	3	NC	1
40			min	-.624	1	-1.906	1	0	1	0	1	70.32	1	NC	1
41		2	max	.017	3	.261	3	0	1	0	1	3047.641	12	NC	1
42			min	-.624	1	-1.635	1	0	1	0	1	81.955	1	NC	1
43		3	max	.017	3	.19	3	0	1	0	1	3438.593	15	NC	1
44			min	-.624	1	-1.364	1	0	1	0	1	98.245	1	NC	1
45		4	max	.017	3	.121	3	0	1	0	1	4230.028	15	NC	1
46			min	-.624	1	-1.101	1	0	1	0	1	121.615	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
47		5	max	.017	3	.062	3	0	1	0	1	5352.752	15	NC	1
48			min	-.623	1	-.864	1	0	1	0	1	154.961	1	NC	1
49		6	max	.017	3	.017	3	0	1	0	1	6883.518	15	NC	1
50			min	-.622	1	-.669	1	0	1	0	1	200.243	1	NC	1
51		7	max	.017	3	-.01	12	0	1	0	1	8971.722	15	NC	1
52			min	-.62	1	-.513	1	0	1	0	1	261.003	1	NC	1
53		8	max	.016	3	-.011	15	0	1	0	1	NC	15	NC	1
54			min	-.619	1	-.382	1	0	1	0	1	350.326	1	NC	1
55		9	max	.016	3	-.008	15	0	1	0	1	NC	5	NC	1
56			min	-.617	1	-.261	1	0	1	0	1	350.865	3	NC	1
57		10	max	.015	3	-.004	15	0	1	0	1	NC	5	NC	1
58			min	-.615	1	-.143	1	0	1	0	1	340.925	3	NC	1
59		11	max	.015	3	0	15	0	1	0	1	NC	4	NC	1
60			min	-.613	1	-.066	3	0	1	0	1	336.244	3	NC	1
61		12	max	.014	3	.076	1	0	1	0	1	NC	5	NC	1
62			min	-.611	1	-.065	3	0	1	0	1	337.493	3	NC	1
63		13	max	.014	3	.164	1	0	1	0	1	NC	5	NC	1
64			min	-.609	1	-.048	3	0	1	0	1	353.004	3	NC	1
65		14	max	.013	3	.216	1	0	1	0	1	NC	5	NC	1
66			min	-.607	1	0	3	0	1	0	1	403.045	3	NC	1
67		15	max	.013	3	.22	1	0	1	0	1	NC	5	NC	1
68			min	-.607	1	.006	15	0	1	0	1	549.079	3	NC	1
69		16	max	.013	3	.207	3	0	1	0	1	NC	5	NC	1
70			min	-.607	1	.005	15	0	1	0	1	722.873	1	NC	1
71		17	max	.013	3	.345	3	0	1	0	1	NC	3	NC	1
72			min	-.607	1	.004	15	0	1	0	1	1038.239	1	NC	1
73		18	max	.013	3	.49	3	0	1	0	1	NC	5	NC	1
74			min	-.607	1	.002	15	0	1	0	1	847.93	3	NC	1
75		19	max	.013	3	.635	3	0	1	0	1	NC	1	NC	1
76			min	-.607	1	-.006	9	0	1	0	1	442.897	3	NC	1
77	M7	1	max	-.004	12	.098	3	0	12	3.316e-2	1	NC	3	NC	3
78			min	-.264	1	-.776	1	-.031	1	-1.035e-2	3	163.689	1	2430.542	1
79		2	max	-.004	12	.074	3	0	12	3.316e-2	1	9064.591	12	NC	3
80			min	-.264	1	-.668	1	-.01	1	-1.035e-2	3	188.608	1	3928.904	1
81		3	max	-.004	12	.05	3	.008	1	3.115e-2	1	6823.231	15	NC	2
82			min	-.264	1	-.56	1	0	12	-9.903e-3	3	222.514	1	8351.191	1
83		4	max	-.004	12	.027	3	.016	1	2.806e-2	1	8128.093	15	NC	1
84			min	-.264	1	-.455	1	0	12	-9.222e-3	3	269.284	1	NC	1
85		5	max	-.004	12	.007	3	.017	1	2.497e-2	1	9862.956	15	NC	1
86			min	-.264	1	-.36	1	0	3	-8.54e-3	3	333.031	1	NC	1
87		6	max	-.004	12	-.006	12	.015	1	2.402e-2	1	NC	15	NC	1
88			min	-.264	1	-.28	1	-.002	3	-8.591e-3	3	415.754	1	NC	1
89		7	max	-.004	12	-.007	15	.007	1	2.454e-2	1	NC	15	NC	2
90			min	-.263	1	-.214	1	-.002	3	-9.148e-3	3	521.63	1	7796.552	1
91		8	max	-.004	12	-.005	15	.001	2	2.507e-2	1	NC	5	NC	2
92			min	-.263	1	-.159	1	0	3	-9.705e-3	3	666.684	1	5662.376	1
93		9	max	-.004	12	-.004	15	0	3	2.452e-2	1	NC	5	NC	2
94			min	-.262	1	-.107	1	0	15	-1.042e-2	3	894.97	1	5519.014	1
95		10	max	-.005	12	-.002	15	0	3	2.206e-2	1	NC	5	NC	2
96			min	-.261	1	-.058	1	0	1	-1.14e-2	3	1043.966	3	5368.524	1
97		11	max	-.005	12	0	15	.002	1	1.961e-2	1	NC	5	NC	2
98			min	-.26	1	-.03	3	-.002	3	-1.239e-2	3	1049.414	3	5882.095	1
99		12	max	-.005	12	.032	1	.01	1	1.465e-2	1	NC	1	NC	2
100			min	-.26	1	-.026	3	-.006	3	-1.001e-2	3	1079.829	3	9092.915	1
101		13	max	-.005	12	.069	1	.013	1	8.281e-3	1	NC	4	NC	1
102			min	-.259	1	-.017	3	-.011	3	-5.742e-3	3	1171.63	3	NC	1
103		14	max	-.005	12	.092	1	.008	2	2.142e-3	1	NC	4	NC	2

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
104			min	-.258	1	.003	12	-.012	3	-1.659e-3	3	1431.376	3	7886.152	1
105		15	max	-.005	12	.099	1	.002	2	6.46e-3	1	NC	4	NC	2
106			min	-.258	1	.003	15	-.009	3	-5.986e-3	3	2322.884	3	4965.578	1
107		16	max	-.005	12	.092	1	0	10	1.078e-2	1	NC	3	NC	2
108			min	-.258	1	.003	15	-.008	1	-1.031e-2	3	2691.415	1	4087.694	1
109		17	max	-.005	12	.142	3	0	15	1.509e-2	1	NC	4	NC	2
110			min	-.258	1	.003	15	-.006	1	-1.464e-2	3	3047.267	3	4406.99	1
111		18	max	-.005	12	.199	3	.008	1	1.791e-2	1	NC	4	NC	2
112			min	-.258	1	.002	15	0	15	-1.746e-2	3	1325.151	3	8006.054	1
113		19	max	-.005	12	.256	3	.025	1	1.791e-2	1	NC	1	NC	1
114			min	-.258	1	.002	15	0	15	-1.746e-2	3	847.212	3	NC	1
115	M10	1	max	.002	1	.179	3	.258	1	7.663e-3	3	NC	1	NC	1
116			min	0	3	.003	15	.005	12	-2.355e-3	1	NC	1	NC	1
117		2	max	.002	1	.457	3	.336	1	8.969e-3	3	NC	5	NC	3
118			min	0	3	-.217	1	.009	12	-3.053e-3	1	975.05	1	3568.668	1
119		3	max	.002	1	.712	3	.461	1	1.027e-2	3	NC	5	NC	3
120			min	0	3	-.469	1	.013	12	-3.751e-3	1	516.197	1	1362.97	1
121		4	max	.001	1	.896	3	.588	1	1.158e-2	3	NC	15	NC	3
122			min	0	3	-.634	1	.015	12	-4.449e-3	1	385.211	3	837.838	1
123		5	max	.001	1	.979	3	.685	1	1.289e-2	3	NC	15	NC	3
124			min	0	3	-.683	1	.014	12	-5.147e-3	1	345.067	3	647.382	1
125		6	max	0	1	.956	3	.734	1	1.419e-2	3	NC	15	NC	3
126			min	0	3	-.612	1	.011	12	-5.845e-3	1	355.124	3	580.125	1
127		7	max	0	1	.843	3	.733	1	1.55e-2	3	NC	5	NC	3
128			min	0	3	-.441	1	.006	12	-6.543e-3	1	415.642	3	581.652	1
129		8	max	0	1	.677	3	.692	1	1.68e-2	3	NC	5	NC	3
130			min	0	3	-.216	1	-.002	3	-7.241e-3	1	554.788	3	636.405	1
131		9	max	0	1	.515	3	.637	1	1.811e-2	3	NC	4	NC	3
132			min	0	3	-.009	9	-.01	3	-7.939e-3	1	820.651	3	728.854	1
133		10	max	0	1	.44	3	.607	1	1.941e-2	3	NC	1	NC	3
134			min	0	1	.003	15	-.013	3	-8.637e-3	1	1057.786	3	790.466	1
135		11	max	0	3	.515	3	.637	1	1.811e-2	3	NC	4	NC	3
136			min	0	1	-.009	9	-.01	3	-7.939e-3	1	820.651	3	728.854	1
137		12	max	0	3	.677	3	.692	1	1.68e-2	3	NC	5	NC	3
138			min	0	1	-.216	1	-.002	3	-7.241e-3	1	554.788	3	636.405	1
139		13	max	0	3	.843	3	.733	1	1.55e-2	3	NC	5	NC	3
140			min	0	1	-.441	1	.006	12	-6.543e-3	1	415.642	3	581.652	1
141		14	max	0	3	.956	3	.734	1	1.419e-2	3	NC	15	NC	3
142			min	0	1	-.612	1	.011	12	-5.845e-3	1	355.124	3	580.125	1
143		15	max	0	3	.979	3	.685	1	1.289e-2	3	NC	15	NC	3
144			min	-.001	1	-.683	1	.014	12	-5.147e-3	1	345.067	3	647.382	1
145		16	max	0	3	.896	3	.588	1	1.158e-2	3	NC	15	NC	3
146			min	-.001	1	-.634	1	.015	12	-4.449e-3	1	385.211	3	837.838	1
147		17	max	0	3	.712	3	.461	1	1.027e-2	3	NC	5	NC	3
148			min	-.002	1	-.469	1	.013	12	-3.751e-3	1	516.197	1	1362.97	1
149		18	max	0	3	.457	3	.336	1	8.969e-3	3	NC	5	NC	3
150			min	-.002	1	-.217	1	.009	12	-3.053e-3	1	975.05	1	3568.668	1
151		19	max	0	3	.179	3	.258	1	7.663e-3	3	NC	1	NC	1
152			min	-.002	1	.003	15	.005	12	-2.355e-3	1	NC	1	NC	1
153	M11	1	max	.004	1	.005	1	.26	1	5.873e-3	1	NC	1	NC	1
154			min	-.003	3	-.029	3	.005	12	1.933e-4	15	NC	1	NC	1
155		2	max	.004	1	.182	3	.326	1	6.809e-3	1	NC	5	NC	3
156			min	-.003	3	-.289	1	.001	3	2.18e-4	15	940.246	1	4177.792	1
157		3	max	.003	1	.379	3	.446	1	7.745e-3	1	NC	5	NC	3
158			min	-.002	3	-.547	1	0	3	2.427e-4	15	499.988	1	1488.241	1
159		4	max	.003	1	.514	3	.571	1	8.681e-3	1	NC	15	NC	3
160			min	-.002	3	-.716	1	0	3	2.246e-4	12	382.69	1	887.47	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
161		5	max	.002	1	.557	3	.67	1	9.617e-3	1	NC	15	NC	3
162			min	-.002	3	-.767	1	0	3	2.025e-4	12	357.475	1	673.488	1
163		6	max	.002	1	.503	3	.723	1	1.055e-2	1	NC	15	NC	3
164			min	-.001	3	-.696	1	0	3	1.805e-4	12	393.87	1	595.739	1
165		7	max	.001	1	.366	3	.727	1	1.149e-2	1	NC	5	NC	3
166			min	0	3	-.524	1	-.004	3	1.585e-4	12	522.28	1	590.827	1
167		8	max	0	1	.183	3	.691	1	1.243e-2	1	NC	5	NC	3
168			min	0	3	-.297	1	-.008	3	1.365e-4	12	914.947	1	639.859	1
169		9	max	0	1	.012	3	.64	1	1.336e-2	1	NC	4	NC	3
170			min	0	3	-.087	1	-.012	3	1.145e-4	12	3001.815	1	725.981	1
171		10	max	0	1	.009	1	.612	1	1.43e-2	1	NC	1	NC	3
172			min	0	1	-.067	3	-.014	3	9.245e-5	12	7315.278	3	783.657	1
173		11	max	0	3	.012	3	.64	1	1.336e-2	1	NC	4	NC	3
174			min	0	1	-.087	1	-.012	3	1.145e-4	12	3001.815	1	725.981	1
175		12	max	0	3	.183	3	.691	1	1.243e-2	1	NC	5	NC	3
176			min	0	1	-.297	1	-.008	3	1.365e-4	12	914.947	1	639.859	1
177		13	max	0	3	.366	3	.727	1	1.149e-2	1	NC	5	NC	3
178			min	-.001	1	-.524	1	-.004	3	1.585e-4	12	522.28	1	590.827	1
179		14	max	.001	3	.503	3	.723	1	1.055e-2	1	NC	15	NC	3
180			min	-.002	1	-.696	1	0	3	1.805e-4	12	393.87	1	595.739	1
181		15	max	.002	3	.557	3	.67	1	9.617e-3	1	NC	15	NC	3
182			min	-.002	1	-.767	1	0	3	2.025e-4	12	357.475	1	673.488	1
183		16	max	.002	3	.514	3	.571	1	8.681e-3	1	NC	15	NC	3
184			min	-.003	1	-.716	1	0	3	2.246e-4	12	382.69	1	887.47	1
185		17	max	.002	3	.379	3	.446	1	7.745e-3	1	NC	5	NC	3
186			min	-.003	1	-.547	1	0	3	2.427e-4	15	499.988	1	1488.241	1
187		18	max	.003	3	.182	3	.326	1	6.809e-3	1	NC	5	NC	3
188			min	-.004	1	-.289	1	.001	3	2.18e-4	15	940.246	1	4177.792	1
189		19	max	.003	3	.005	1	.26	1	5.873e-3	1	NC	1	NC	1
190			min	-.004	1	-.029	3	.005	12	1.933e-4	15	NC	1	NC	1
191	M12	1	max	0	2	-.004	15	.262	1	6.872e-3	1	NC	1	NC	1
192			min	0	9	-.126	1	.004	12	-4.943e-4	3	NC	1	NC	1
193		2	max	0	2	.119	3	.316	1	7.906e-3	1	NC	5	NC	2
194			min	0	9	-.515	1	.006	12	-6.565e-4	3	709.143	1	5157.686	1
195		3	max	0	2	.236	3	.429	1	8.94e-3	1	NC	15	NC	3
196			min	0	9	-.851	1	.008	12	-8.188e-4	3	380.625	1	1657.949	1
197		4	max	0	2	.304	3	.553	1	9.974e-3	1	NC	15	NC	3
198			min	0	9	-1.074	1	.01	12	-9.811e-4	3	290.995	1	950.212	1
199		5	max	0	2	.316	3	.653	1	1.101e-2	1	NC	15	NC	3
200			min	0	9	-1.154	1	.009	12	-1.143e-3	3	268.398	1	705.231	1
201		6	max	0	2	.276	3	.711	1	1.204e-2	1	NC	15	NC	3
202			min	0	9	-1.088	1	.007	12	-1.306e-3	3	286.86	1	614.241	1
203		7	max	0	2	.193	3	.721	1	1.307e-2	1	NC	15	NC	3
204			min	0	9	-.901	1	.002	3	-1.468e-3	3	355.785	1	601.518	1
205		8	max	0	2	.09	3	.691	1	1.411e-2	1	NC	5	NC	3
206			min	0	9	-.649	1	-.006	3	-1.63e-3	3	527.376	1	643.93	1
207		9	max	0	2	-.002	12	.644	1	1.514e-2	1	NC	3	NC	3
208			min	0	9	-.413	1	-.013	3	-1.792e-3	3	959.983	1	723.068	1
209		10	max	0	1	-.009	15	.618	1	1.618e-2	1	NC	3	NC	3
210			min	0	1	-.305	1	-.016	3	-1.955e-3	3	1540.421	1	776.525	1
211		11	max	0	9	-.002	12	.644	1	1.514e-2	1	NC	3	NC	3
212			min	0	2	-.413	1	-.013	3	-1.792e-3	3	959.983	1	723.068	1
213		12	max	0	9	.09	3	.691	1	1.411e-2	1	NC	5	NC	3
214			min	0	2	-.649	1	-.006	3	-1.63e-3	3	527.376	1	643.93	1
215		13	max	0	9	.193	3	.721	1	1.307e-2	1	NC	15	NC	3
216			min	0	2	-.901	1	.002	3	-1.468e-3	3	355.785	1	601.518	1
217		14	max	0	9	.276	3	.711	1	1.204e-2	1	NC	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
218			min	0	2	-1.088	1	.007	12	-1.306e-3	3	286.86	1	614.241	1
219		15	max	0	9	.316	3	.653	1	1.101e-2	1	NC	15	NC	3
220			min	0	2	-1.154	1	.009	12	-1.143e-3	3	268.398	1	705.231	1
221		16	max	0	9	.304	3	.553	1	9.974e-3	1	NC	15	NC	3
222			min	0	2	-1.074	1	.01	12	-9.811e-4	3	290.995	1	950.212	1
223		17	max	0	9	.236	3	.429	1	8.94e-3	1	NC	15	NC	3
224			min	0	2	-.851	1	.008	12	-8.188e-4	3	380.625	1	1657.949	1
225		18	max	0	9	.119	3	.316	1	7.906e-3	1	NC	5	NC	2
226			min	0	2	-.515	1	.006	12	-6.565e-4	3	709.143	1	5157.686	1
227		19	max	0	9	-.004	15	.262	1	6.872e-3	1	NC	1	NC	1
228			min	0	2	-.126	1	.004	12	-4.943e-4	3	NC	1	NC	1
229	M13	1	max	0	3	.065	3	.264	1	1.453e-2	1	NC	1	NC	1
230			min	-.002	1	-.631	1	.004	12	-3.227e-3	3	NC	1	NC	1
231		2	max	0	3	.222	3	.349	1	1.695e-2	1	NC	5	NC	3
232			min	-.002	1	-1.139	1	.006	12	-3.931e-3	3	542.945	1	3260.005	1
233		3	max	0	3	.358	3	.479	1	1.937e-2	1	NC	15	NC	3
234			min	-.002	1	-1.592	1	.008	12	-4.636e-3	3	287.081	1	1286.96	1
235		4	max	0	3	.451	3	.608	1	2.18e-2	1	8346.385	15	NC	3
236			min	-.002	1	-1.927	1	.009	12	-5.34e-3	3	212.851	1	802.751	1
237		5	max	0	3	.493	3	.706	1	2.422e-2	1	7292.54	15	NC	3
238			min	-.001	1	-2.111	1	.008	12	-6.045e-3	3	186.479	1	625.202	1
239		6	max	0	3	.482	3	.755	1	2.664e-2	1	7139.124	15	NC	3
240			min	-.001	1	-2.136	1	.006	12	-6.749e-3	3	183.293	1	562.822	1
241		7	max	0	3	.428	3	.752	1	2.907e-2	1	7652.317	15	NC	3
242			min	0	1	-2.027	1	0	3	-7.453e-3	3	197.641	1	565.688	1
243		8	max	0	3	.348	3	.71	1	3.149e-2	1	8807.081	15	NC	3
244			min	0	1	-1.834	1	-.008	3	-8.158e-3	3	229.405	1	619.403	1
245		9	max	0	3	.272	3	.654	1	3.391e-2	1	NC	15	NC	3
246			min	0	1	-1.636	1	-.014	3	-8.862e-3	3	274.606	1	708.911	1
247		10	max	0	1	.236	3	.624	1	3.634e-2	1	NC	15	NC	3
248			min	0	1	-1.541	1	-.017	3	-9.566e-3	3	303.264	1	768.191	1
249		11	max	0	1	.272	3	.654	1	3.391e-2	1	NC	15	NC	3
250			min	0	3	-1.636	1	-.014	3	-8.862e-3	3	274.606	1	708.911	1
251		12	max	0	1	.348	3	.71	1	3.149e-2	1	8807.081	15	NC	3
252			min	0	3	-1.834	1	-.008	3	-8.158e-3	3	229.405	1	619.403	1
253		13	max	0	1	.428	3	.752	1	2.907e-2	1	7652.317	15	NC	3
254			min	0	3	-2.027	1	0	3	-7.453e-3	3	197.641	1	565.688	1
255		14	max	.001	1	.482	3	.755	1	2.664e-2	1	7139.124	15	NC	3
256			min	0	3	-2.136	1	.006	12	-6.749e-3	3	183.293	1	562.822	1
257		15	max	.001	1	.493	3	.706	1	2.422e-2	1	7292.54	15	NC	3
258			min	0	3	-2.111	1	.008	12	-6.045e-3	3	186.479	1	625.202	1
259		16	max	.002	1	.451	3	.608	1	2.18e-2	1	8346.385	15	NC	3
260			min	0	3	-1.927	1	.009	12	-5.34e-3	3	212.851	1	802.751	1
261		17	max	.002	1	.358	3	.479	1	1.937e-2	1	NC	15	NC	3
262			min	0	3	-1.592	1	.008	12	-4.636e-3	3	287.081	1	1286.96	1
263		18	max	.002	1	.222	3	.349	1	1.695e-2	1	NC	5	NC	3
264			min	0	3	-1.139	1	.006	12	-3.931e-3	3	542.945	1	3260.005	1
265		19	max	.002	1	.065	3	.264	1	1.453e-2	1	NC	1	NC	1
266			min	0	3	-.631	1	.004	12	-3.227e-3	3	NC	1	NC	1
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	3	2.002e-3	1	NC	1	NC	1
270			min	0	1	-.001	1	0	1	-6.946e-4	3	NC	1	NC	1
271		3	max	0	3	0	15	0	3	4.003e-3	1	NC	1	NC	1
272			min	0	1	-.004	1	0	1	-1.389e-3	3	NC	1	NC	1
273		4	max	0	3	0	15	0	3	6.005e-3	1	NC	3	NC	1
274			min	0	1	-.009	1	-.001	1	-2.084e-3	3	5682.126	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
275		5	max	0	3	0	15	.001	3	7.629e-3	1	NC	3	NC	1
276			min	0	1	-.017	1	-.002	1	-2.645e-3	3	3187.363	1	NC	1
277		6	max	0	3	0	15	.002	3	6.938e-3	1	NC	3	NC	1
278			min	0	1	-.026	1	-.003	1	-2.389e-3	3	2025.872	1	NC	1
279		7	max	0	3	-.001	15	.002	3	6.248e-3	1	NC	3	NC	2
280			min	0	1	-.038	1	-.004	1	-2.133e-3	3	1409.225	1	8598.184	1
281		8	max	0	3	-.002	12	.002	3	5.557e-3	1	NC	3	NC	2
282			min	0	1	-.051	1	-.004	1	-1.878e-3	3	1042.896	1	7197.52	1
283		9	max	0	3	-.002	12	.003	3	4.867e-3	1	NC	3	NC	2
284			min	0	1	-.066	1	-.005	1	-1.622e-3	3	807.18	1	6263.783	1
285		10	max	0	3	-.002	12	.003	3	4.177e-3	1	NC	3	NC	2
286			min	0	1	-.083	1	-.006	1	-1.366e-3	3	646.576	1	5641.285	1
287		11	max	0	3	-.003	12	.003	3	3.486e-3	1	NC	3	NC	2
288			min	-.001	1	-.101	1	-.006	1	-1.111e-3	3	532.102	1	5246.652	1
289		12	max	0	3	-.003	12	.002	3	2.796e-3	1	NC	3	NC	2
290			min	-.001	1	-.12	1	-.006	1	-8.551e-4	3	447.549	1	5039.567	1
291		13	max	0	3	-.003	12	.001	3	2.112e-3	2	NC	3	NC	2
292			min	-.001	1	-.14	1	-.006	1	-5.994e-4	3	383.312	1	5009.706	1
293		14	max	0	3	-.004	12	0	3	1.539e-3	2	NC	3	NC	2
294			min	-.001	1	-.161	1	-.005	1	-3.437e-4	3	333.334	1	5183.27	1
295		15	max	0	3	-.004	12	0	15	9.661e-4	2	NC	12	NC	2
296			min	-.001	1	-.183	1	-.003	1	-8.807e-5	3	293.679	1	5643.931	1
297		16	max	0	3	-.004	12	0	10	3.93e-4	2	NC	12	NC	2
298			min	-.001	1	-.205	1	-.003	3	-1.318e-4	9	261.695	1	6612.441	1
299		17	max	0	3	-.005	12	.002	2	4.233e-4	3	NC	12	NC	2
300			min	-.002	1	-.228	1	-.005	3	-6.56e-4	1	235.528	1	8786.426	1
301		18	max	0	3	-.005	12	.005	2	6.789e-4	3	NC	12	NC	1
302			min	-.002	1	-.251	1	-.008	3	-1.346e-3	1	213.865	1	6310.996	3
303		19	max	0	3	-.005	12	.008	2	9.346e-4	3	9932.303	12	NC	1
304			min	-.002	1	-.274	1	-.012	3	-2.037e-3	1	195.744	1	4432.468	3
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	1	0	1	NC	1	NC	1
308			min	0	1	-.002	1	0	1	0	1	NC	1	NC	1
309		3	max	0	3	0	15	0	1	0	1	NC	3	NC	1
310			min	0	1	-.009	1	0	1	0	1	5758.157	1	NC	1
311		4	max	0	3	0	15	0	1	0	1	NC	3	NC	1
312			min	0	1	-.021	1	0	1	0	1	2523.653	1	NC	1
313		5	max	0	3	0	12	0	1	0	1	NC	3	NC	1
314			min	-.001	1	-.038	1	0	1	0	1	1402.255	1	NC	1
315		6	max	0	3	0	12	0	1	0	1	NC	3	NC	1
316			min	-.002	1	-.061	1	0	1	0	1	883.291	1	NC	1
317		7	max	0	3	0	12	0	1	0	1	NC	3	NC	1
318			min	-.002	1	-.088	1	0	1	0	1	610.752	1	NC	1
319		8	max	.001	3	0	3	0	1	0	1	NC	3	NC	1
320			min	-.002	1	-.119	1	0	1	0	1	450.063	1	NC	1
321		9	max	.001	3	0	3	0	1	0	1	NC	3	NC	1
322			min	-.002	1	-.154	1	0	1	0	1	347.235	1	NC	1
323		10	max	.001	3	.001	3	0	1	0	1	NC	3	NC	1
324			min	-.003	1	-.193	1	0	1	0	1	277.467	1	NC	1
325		11	max	.002	3	.002	3	0	1	0	1	NC	3	NC	1
326			min	-.003	1	-.235	1	0	1	0	1	227.903	1	NC	1
327		12	max	.002	3	.003	3	0	1	0	1	NC	3	NC	1
328			min	-.003	1	-.28	1	0	1	0	1	191.391	1	NC	1
329		13	max	.002	3	.004	3	0	1	0	1	NC	3	NC	1
330			min	-.003	1	-.328	1	0	1	0	1	163.712	1	NC	1
331		14	max	.002	3	.006	3	0	1	0	1	NC	12	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
332			min	-.004	1	-.377	1	0	1	0	1	142.217	1	NC	1
333		15	max	.002	3	.007	3	0	1	0	1	NC	12	NC	1
334			min	-.004	1	-.428	1	0	1	0	1	125.188	1	NC	1
335		16	max	.002	3	.008	3	0	1	0	1	NC	12	NC	1
336			min	-.004	1	-.481	1	0	1	0	1	111.471	1	NC	1
337		17	max	.002	3	.01	3	0	1	0	1	NC	12	NC	1
338			min	-.004	1	-.535	1	0	1	0	1	100.262	1	NC	1
339		18	max	.003	3	.011	3	0	1	0	1	8796.705	12	NC	1
340			min	-.005	1	-.589	1	0	1	0	1	90.992	1	NC	1
341		19	max	.003	3	.013	3	0	1	0	1	7708.697	12	NC	1
342			min	-.005	1	-.644	1	0	1	0	1	83.245	1	NC	1
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	15	0	1	6.946e-4	3	NC	1	NC	1
346			min	0	1	-.001	1	0	3	-2.002e-3	1	NC	1	NC	1
347		3	max	0	3	0	15	0	1	1.389e-3	3	NC	1	NC	1
348			min	0	1	-.004	1	0	3	-4.003e-3	1	NC	1	NC	1
349		4	max	0	3	0	15	.001	1	2.084e-3	3	NC	3	NC	1
350			min	0	1	-.009	1	0	3	-6.005e-3	1	5682.126	1	NC	1
351		5	max	0	3	0	15	.002	1	2.645e-3	3	NC	3	NC	1
352			min	0	1	-.017	1	-.001	3	-7.629e-3	1	3187.363	1	NC	1
353		6	max	0	3	0	15	.003	1	2.389e-3	3	NC	3	NC	1
354			min	0	1	-.026	1	-.002	3	-6.938e-3	1	2025.872	1	NC	1
355		7	max	0	3	-.001	15	.004	1	2.133e-3	3	NC	3	NC	2
356			min	0	1	-.038	1	-.002	3	-6.248e-3	1	1409.225	1	8598.184	1
357		8	max	0	3	-.002	12	.004	1	1.878e-3	3	NC	3	NC	2
358			min	0	1	-.051	1	-.002	3	-5.557e-3	1	1042.896	1	7197.52	1
359		9	max	0	3	-.002	12	.005	1	1.622e-3	3	NC	3	NC	2
360			min	0	1	-.066	1	-.003	3	-4.867e-3	1	807.18	1	6263.783	1
361		10	max	0	3	-.002	12	.006	1	1.366e-3	3	NC	3	NC	2
362			min	0	1	-.083	1	-.003	3	-4.177e-3	1	646.576	1	5641.285	1
363		11	max	0	3	-.003	12	.006	1	1.111e-3	3	NC	3	NC	2
364			min	-.001	1	-.101	1	-.003	3	-3.486e-3	1	532.102	1	5246.652	1
365		12	max	0	3	-.003	12	.006	1	8.551e-4	3	NC	3	NC	2
366			min	-.001	1	-.12	1	-.002	3	-2.796e-3	1	447.549	1	5039.567	1
367		13	max	0	3	-.003	12	.006	1	5.994e-4	3	NC	3	NC	2
368			min	-.001	1	-.14	1	-.001	3	-2.112e-3	2	383.312	1	5009.706	1
369		14	max	0	3	-.004	12	.005	1	3.437e-4	3	NC	3	NC	2
370			min	-.001	1	-.161	1	0	3	-1.539e-3	2	333.334	1	5183.27	1
371		15	max	0	3	-.004	12	.003	1	8.807e-5	3	NC	12	NC	2
372			min	-.001	1	-.183	1	0	15	-9.661e-4	2	293.679	1	5643.931	1
373		16	max	0	3	-.004	12	.003	3	1.318e-4	9	NC	12	NC	2
374			min	-.001	1	-.205	1	0	10	-3.93e-4	2	261.695	1	6612.441	1
375		17	max	0	3	-.005	12	.005	3	6.56e-4	1	NC	12	NC	2
376			min	-.002	1	-.228	1	-.002	2	-4.233e-4	3	235.528	1	8786.426	1
377		18	max	0	3	-.005	12	.008	3	1.346e-3	1	NC	12	NC	1
378			min	-.002	1	-.251	1	-.005	2	-6.789e-4	3	213.865	1	6310.996	3
379		19	max	0	3	-.005	12	.012	3	2.037e-3	1	9932.303	12	NC	1
380			min	-.002	1	-.274	1	-.008	2	-9.346e-4	3	195.744	1	4432.468	3
381	M3	1	max	.015	1	0	12	.001	3	2.25e-3	1	NC	1	NC	1
382			min	0	15	-.005	1	-.002	1	-7.266e-4	3	NC	1	NC	1
383		2	max	.014	1	0	12	.01	3	3.149e-3	1	NC	1	NC	4
384			min	0	15	-.029	1	-.028	1	-1.052e-3	3	NC	1	2355.821	1
385		3	max	.013	1	-.001	12	.019	3	4.047e-3	1	NC	1	NC	5
386			min	0	15	-.053	1	-.053	1	-1.378e-3	3	NC	1	1194.85	1
387		4	max	.013	1	-.002	12	.027	3	4.946e-3	1	NC	1	NC	5
388			min	0	15	-.076	1	-.077	1	-1.703e-3	3	NC	1	812.857	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
389		5	max	.012	1	-.002	12	.035	3	5.845e-3	1	NC	1	NC	5
390			min	0	15	-.1	1	-.099	1	-2.029e-3	3	NC	1	626.064	1
391		6	max	.011	1	-.002	12	.042	3	6.743e-3	1	NC	1	NC	5
392			min	0	15	-.123	1	-.119	1	-2.354e-3	3	NC	1	517.872	1
393		7	max	.011	1	-.003	12	.048	3	7.642e-3	1	NC	1	NC	5
394			min	0	15	-.146	1	-.137	1	-2.68e-3	3	NC	1	449.597	1
395		8	max	.01	1	-.003	12	.053	3	8.541e-3	1	NC	1	NC	5
396			min	0	15	-.17	1	-.151	1	-3.005e-3	3	NC	1	404.878	1
397		9	max	.009	1	-.003	12	.057	3	9.439e-3	1	NC	1	NC	15
398			min	0	15	-.193	1	-.162	1	-3.331e-3	3	NC	1	375.818	1
399		10	max	.009	1	-.003	12	.06	3	1.034e-2	1	NC	1	NC	15
400			min	0	15	-.216	1	-.169	1	-3.656e-3	3	NC	1	358.414	1
401		11	max	.008	1	-.004	12	.061	3	1.124e-2	1	NC	1	NC	15
402			min	0	15	-.239	1	-.172	1	-3.982e-3	3	NC	1	350.83	1
403		12	max	.008	1	-.004	12	.061	3	1.214e-2	1	NC	1	NC	15
404			min	0	15	-.261	1	-.17	1	-4.307e-3	3	NC	1	352.771	1
405		13	max	.007	1	-.004	12	.059	3	1.303e-2	1	NC	1	NC	15
406			min	0	15	-.284	1	-.163	1	-4.633e-3	3	NC	1	365.509	1
407		14	max	.006	1	-.004	12	.054	3	1.393e-2	1	NC	1	NC	15
408			min	0	15	-.307	1	-.15	1	-4.958e-3	3	NC	1	392.633	1
409		15	max	.006	1	-.004	12	.048	3	1.483e-2	1	NC	1	NC	5
410			min	0	15	-.329	1	-.131	1	-5.284e-3	3	NC	1	442.362	1
411		16	max	.005	1	-.004	12	.04	3	1.573e-2	1	NC	1	NC	5
412			min	0	10	-.352	1	-.105	1	-5.609e-3	3	NC	1	534.803	1
413		17	max	.004	1	-.003	12	.029	3	1.663e-2	1	NC	1	NC	5
414			min	0	10	-.374	1	-.072	1	-5.935e-3	3	NC	1	731.222	1
415		18	max	.004	3	-.003	12	.015	3	1.753e-2	1	NC	1	NC	5
416			min	0	10	-.397	1	-.032	2	-6.26e-3	3	NC	1	1339.299	1
417		19	max	.004	3	-.003	12	.017	1	1.843e-2	1	NC	1	NC	1
418			min	0	10	-.419	1	0	3	-6.586e-3	3	NC	1	NC	1
419	M6	1	max	.033	1	0	3	0	1	0	1	NC	1	NC	1
420			min	0	12	-.013	1	0	1	0	1	NC	1	NC	1
421		2	max	.031	1	.002	3	0	1	0	1	NC	1	NC	1
422			min	0	15	-.068	1	0	1	0	1	NC	1	NC	1
423		3	max	.03	1	.004	3	0	1	0	1	NC	1	NC	1
424			min	0	15	-.123	1	0	1	0	1	NC	1	NC	1
425		4	max	.028	1	.006	3	0	1	0	1	NC	1	NC	1
426			min	0	15	-.178	1	0	1	0	1	NC	1	NC	1
427		5	max	.026	1	.008	3	0	1	0	1	NC	1	NC	1
428			min	0	15	-.234	1	0	1	0	1	8162.033	3	NC	1
429		6	max	.024	1	.01	3	0	1	0	1	NC	1	NC	1
430			min	0	15	-.289	1	0	1	0	1	6457.359	3	NC	1
431		7	max	.022	1	.012	3	0	1	0	1	NC	1	NC	1
432			min	0	15	-.344	1	0	1	0	1	5312.94	3	NC	1
433		8	max	.02	1	.014	3	0	1	0	1	NC	1	NC	1
434			min	0	15	-.399	1	0	1	0	1	4490.328	3	NC	1
435		9	max	.018	1	.017	3	0	1	0	1	NC	1	NC	1
436			min	0	15	-.454	1	0	1	0	1	3870.212	3	NC	1
437		10	max	.017	1	.019	3	0	1	0	1	NC	1	NC	1
438			min	0	15	-.508	1	0	1	0	1	3386.211	3	NC	1
439		11	max	.015	1	.021	3	0	1	0	1	NC	1	NC	1
440			min	0	15	-.563	1	0	1	0	1	2998.4	3	NC	1
441		12	max	.013	1	.024	3	0	1	0	1	NC	1	NC	1
442			min	0	15	-.618	1	0	1	0	1	2681.283	3	NC	1
443		13	max	.011	1	.026	3	0	1	0	1	NC	1	NC	1
444			min	0	15	-.672	1	0	1	0	1	2417.783	3	NC	1
445		14	max	.009	1	.029	3	0	1	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
446			min	0	10	-.726	1	0	1	0	1	2196.008	3	NC	1
447		15	max	.01	3	.032	3	0	1	0	1	NC	1	NC	1
448			min	0	10	-.781	1	0	1	0	1	2007.405	3	NC	1
449		16	max	.01	3	.034	3	0	1	0	1	NC	1	NC	1
450			min	-.002	10	-.835	1	0	1	0	1	1845.656	3	NC	1
451		17	max	.011	3	.037	3	0	1	0	1	NC	1	NC	1
452			min	-.003	2	-.889	1	0	1	0	1	1705.987	3	NC	1
453		18	max	.012	3	.04	3	0	1	0	1	NC	1	NC	1
454			min	-.004	2	-.943	1	0	1	0	1	1584.718	3	NC	1
455		19	max	.012	3	.043	3	0	1	0	1	NC	1	NC	1
456			min	-.006	2	-.997	1	0	1	0	1	1478.969	3	NC	1
457	M9	1	max	.015	1	0	12	.002	1	7.266e-4	3	NC	1	NC	1
458			min	0	15	-.005	1	-.001	3	-2.25e-3	1	NC	1	NC	1
459		2	max	.014	1	0	12	.028	1	1.052e-3	3	NC	1	NC	4
460			min	0	15	-.029	1	-.01	3	-3.149e-3	1	NC	1	2355.821	1
461		3	max	.013	1	-.001	12	.053	1	1.378e-3	3	NC	1	NC	5
462			min	0	15	-.053	1	-.019	3	-4.047e-3	1	NC	1	1194.85	1
463		4	max	.013	1	-.002	12	.077	1	1.703e-3	3	NC	1	NC	5
464			min	0	15	-.076	1	-.027	3	-4.946e-3	1	NC	1	812.857	1
465		5	max	.012	1	-.002	12	.099	1	2.029e-3	3	NC	1	NC	5
466			min	0	15	-.1	1	-.035	3	-5.845e-3	1	NC	1	626.064	1
467		6	max	.011	1	-.002	12	.119	1	2.354e-3	3	NC	1	NC	5
468			min	0	15	-.123	1	-.042	3	-6.743e-3	1	NC	1	517.872	1
469		7	max	.011	1	-.003	12	.137	1	2.68e-3	3	NC	1	NC	5
470			min	0	15	-.146	1	-.048	3	-7.642e-3	1	NC	1	449.597	1
471		8	max	.01	1	-.003	12	.151	1	3.005e-3	3	NC	1	NC	5
472			min	0	15	-.17	1	-.053	3	-8.541e-3	1	NC	1	404.878	1
473		9	max	.009	1	-.003	12	.162	1	3.331e-3	3	NC	1	NC	15
474			min	0	15	-.193	1	-.057	3	-9.439e-3	1	NC	1	375.818	1
475		10	max	.009	1	-.003	12	.169	1	3.656e-3	3	NC	1	NC	15
476			min	0	15	-.216	1	-.06	3	-1.034e-2	1	NC	1	358.414	1
477		11	max	.008	1	-.004	12	.172	1	3.982e-3	3	NC	1	NC	15
478			min	0	15	-.239	1	-.061	3	-1.124e-2	1	NC	1	350.83	1
479		12	max	.008	1	-.004	12	.17	1	4.307e-3	3	NC	1	NC	15
480			min	0	15	-.261	1	-.061	3	-1.214e-2	1	NC	1	352.771	1
481		13	max	.007	1	-.004	12	.163	1	4.633e-3	3	NC	1	NC	15
482			min	0	15	-.284	1	-.059	3	-1.303e-2	1	NC	1	365.509	1
483		14	max	.006	1	-.004	12	.15	1	4.958e-3	3	NC	1	NC	15
484			min	0	15	-.307	1	-.054	3	-1.393e-2	1	NC	1	392.633	1
485		15	max	.006	1	-.004	12	.131	1	5.284e-3	3	NC	1	NC	5
486			min	0	15	-.329	1	-.048	3	-1.483e-2	1	NC	1	442.362	1
487		16	max	.005	1	-.004	12	.105	1	5.609e-3	3	NC	1	NC	5
488			min	0	10	-.352	1	-.04	3	-1.573e-2	1	NC	1	534.803	1
489		17	max	.004	1	-.003	12	.072	1	5.935e-3	3	NC	1	NC	5
490			min	0	10	-.374	1	-.029	3	-1.663e-2	1	NC	1	731.222	1
491		18	max	.004	3	-.003	12	.032	2	6.26e-3	3	NC	1	NC	5
492			min	0	10	-.397	1	-.015	3	-1.753e-2	1	NC	1	1339.299	1
493		19	max	.004	3	-.003	12	0	3	6.586e-3	3	NC	1	NC	1
494			min	0	10	-.419	1	-.017	1	-1.843e-2	1	NC	1	NC	1