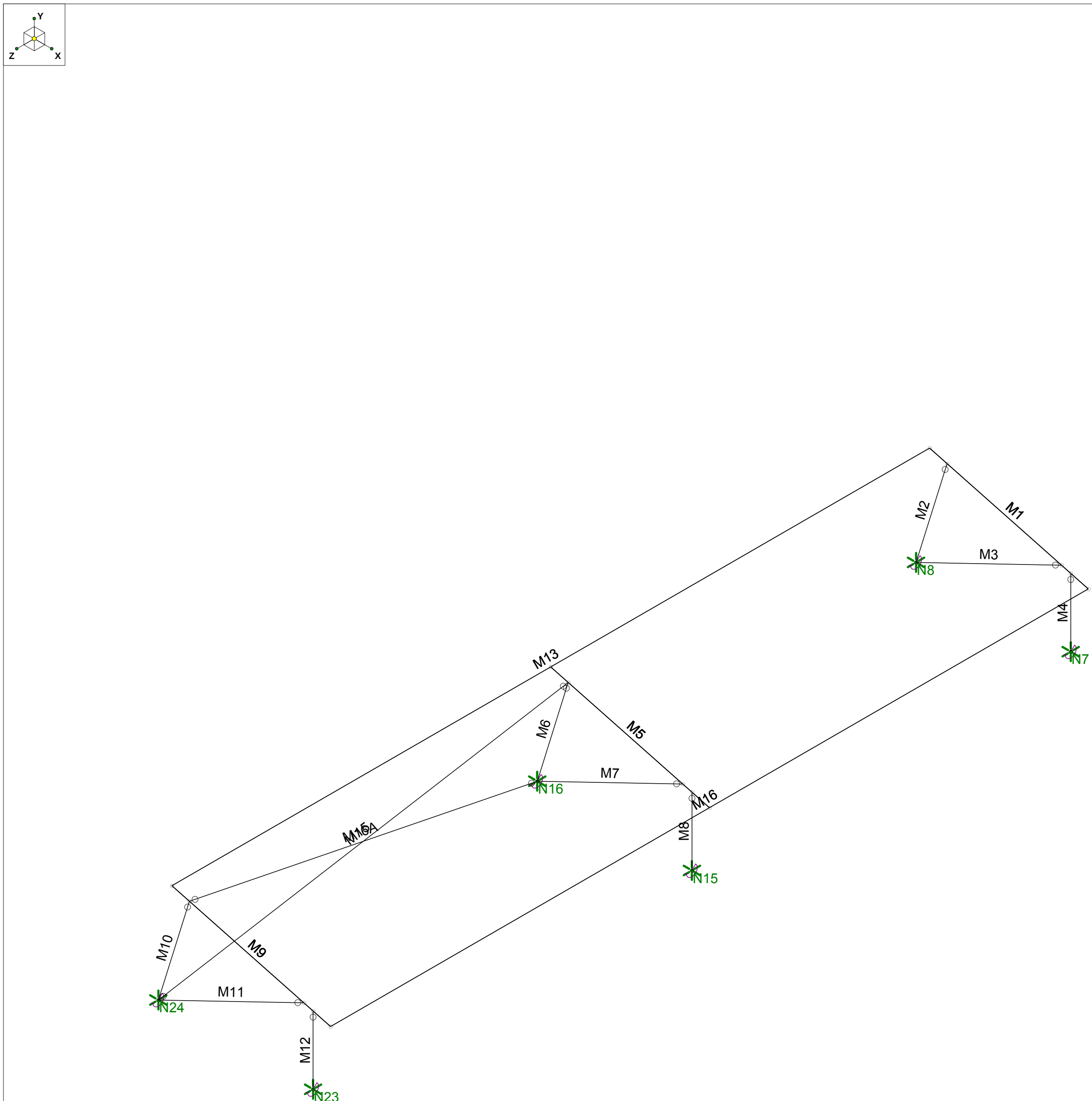


Schletter, Inc.		15° Tilt w/ Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

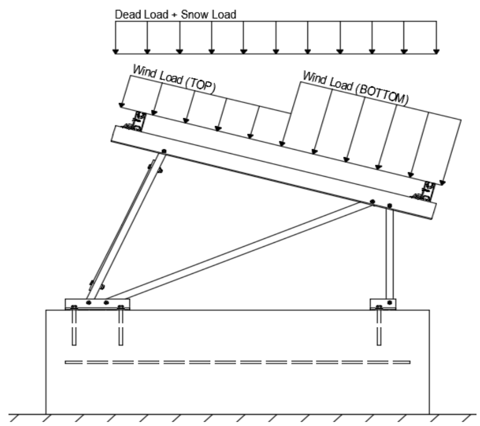
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum
Height =	1700 mm	Height =	1550 mm
Width =	1050 mm	Width =	970 mm
Dead Load =	3.00 psf	Dead Load =	1.75 psf

Modules Per Row = 1
Module Tilt = 15°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} = 3.00 psf
g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads

Ground Snow Load, P_g = 30.00 psf
Sloped Roof Snow Load, P_s = 22.68 psf *(ASCE 7-10, Eq. 7.4-1)*
I_s = 1.00
C_s = 1.00
C_e = 0.90
C_t = 1.20

2.3 Wind Loads

Design Wind Speed, V = 160 mph
Height ≤ 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 40.19 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1	*(Pressure)*
$Cf+_{BOTTOM}$	=	1.6	
$Cf-_{TOP}$	=	-2.04	*(Suction)*
$Cf-_{BOTTOM}$	=	-1	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location	**Diagonal Struts**	Location	**Front Reactions**	Location
M13	Top	M3	Outer	N7	Outer
M16	Bottom	M7	Inner	N15	Inner
		M11	Outer	N23	Outer

Girders	Location	**Rear Struts**	Location	**Rear Reactions**	Location
M1	Outer	M2	Outer	N8	Outer
M5	Inner	M6	Inner	N16	Inner
M9	Outer	M10	Outer	N24	Outer

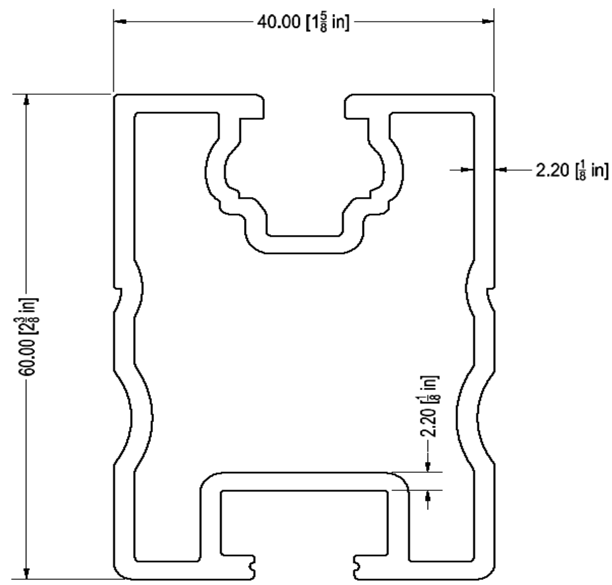
Front Struts	Location	**Bracing**
M4	Outer	M15
M8	Inner	M16A
M12	Outer	

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

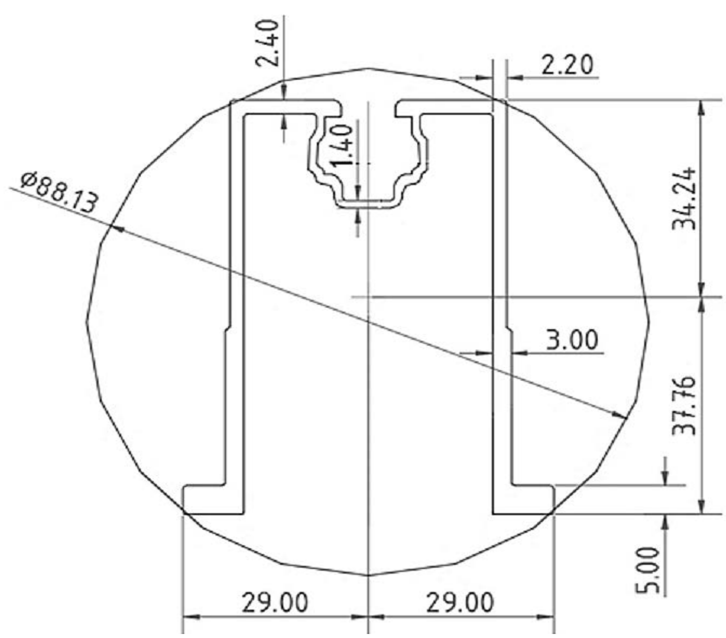
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	48	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.75	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	0.407	k-ft
M_z =	0.024	k-ft
$M_{y\ allowable}$ =	1.266	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	35%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

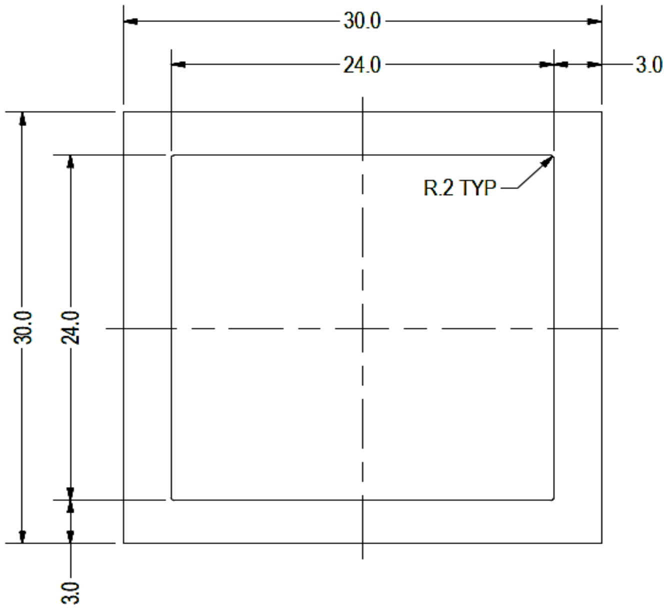
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.88	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	-0.473	k-ft
M_z =	-0.015	k-ft
P_n =	-0.043	k
$M_{y\ allowable}$ =	1.466	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	29.696	k
Utilization =	35%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

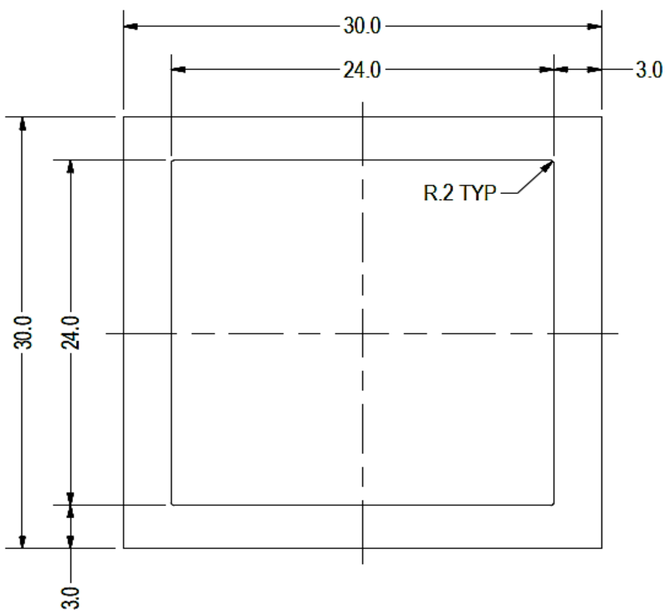
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	1.062	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	9%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

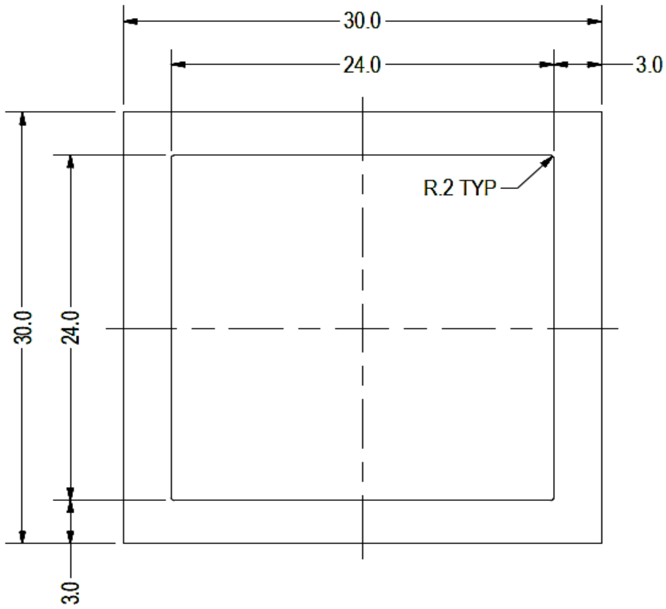
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.188	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	5%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

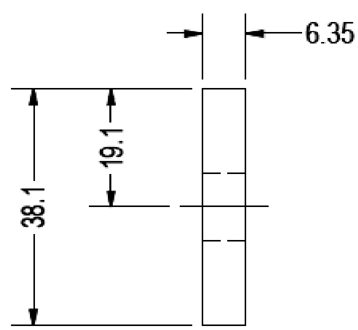
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	29.96	in
$\Phi F_{ty\ AXIAL}$ =	16.11	ksi
$\Phi F_{ty\ BENDING}$ =	30.52	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.794	k
$M_{y\ allowable}$ =	0.413	k-ft
$M_{z\ allowable}$ =	0.413	k-ft
$P_{n\ allowable}$ =	8.089	k
Utilization =	10%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.002	k-ft
P_n =	0.158	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	6%	



A cross brace kit is required every 34 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

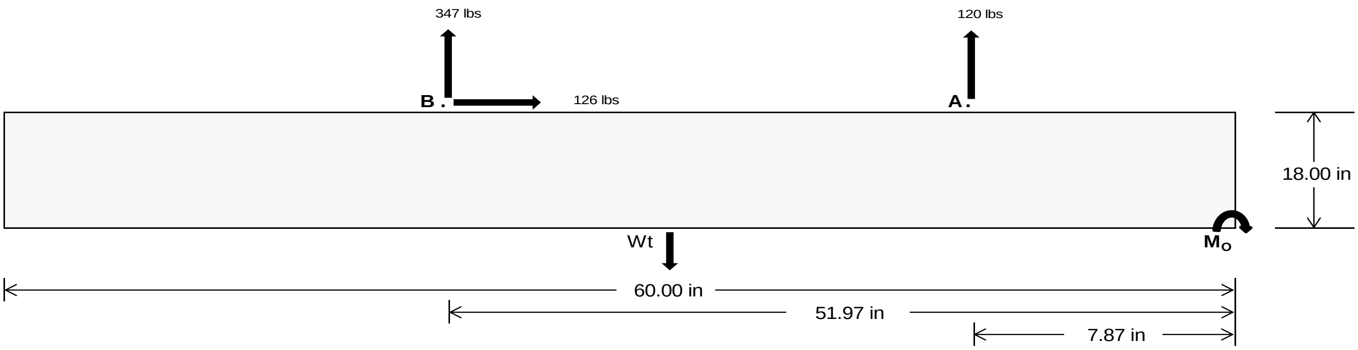
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	523.21	1508.40	k
Compressive Load =	1380.22	985.57	k
Lateral Load =	21.37	547.66	k
Moment (Weak Axis) =	0.03	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties

Weight of Concrete =	145 pcf
Compressive Strength =	2500 psi
Yield Strength =	60000 psi

Footing Reinforcement

Use fiber reinforcing with (1) #5 rebar.

Overturning Check

M_O =	21265.0 in-lbs
Resisting Force Required =	708.83 lbs
S.F. =	1.67
Weight Required =	1181.39 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.

Sliding

Force =	126.37 lbs
Friction =	0.4
Weight Required =	315.94 lbs
Resisting Weight =	1903.13 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion

Sliding Force =	126.37 lbs
Cohesion =	130 psf
Area =	8.75 ft^2
Resisting =	951.56 lbs
Additional Weight Required =	0 lbs

Use a 60in long x 21in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key

Additional Force =	0 lbs
Lateral Bearing Pressure =	200 psf/ft
Required Depth =	0.00 ft
f'_c =	2500 psi
Length =	8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	21 in	22 in	23 in	24 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.75 ft) =	1903 lbs	1994 lbs	2084 lbs	2175 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in	21 in	22 in	23 in	24 in
F_A	419 lbs	419 lbs	419 lbs	419 lbs	546 lbs	546 lbs	546 lbs	546 lbs	694 lbs	694 lbs	694 lbs	694 lbs	-239 lbs	-239 lbs	-239 lbs	-239 lbs
F_B	302 lbs	302 lbs	302 lbs	302 lbs	390 lbs	390 lbs	390 lbs	390 lbs	497 lbs	497 lbs	497 lbs	497 lbs	-695 lbs	-695 lbs	-695 lbs	-695 lbs
F_V	21 lbs	21 lbs	21 lbs	21 lbs	219 lbs	219 lbs	219 lbs	219 lbs	179 lbs	179 lbs	179 lbs	179 lbs	-253 lbs	-253 lbs	-253 lbs	-253 lbs
P_{total}	2624 lbs	2715 lbs	2805 lbs	2896 lbs	2839 lbs	2929 lbs	3020 lbs	3111 lbs	3094 lbs	3184 lbs	3275 lbs	3366 lbs	208 lbs	262 lbs	317 lbs	371 lbs
M	252 lbs-ft	252 lbs-ft	252 lbs-ft	252 lbs-ft	621 lbs-ft	621 lbs-ft	621 lbs-ft	621 lbs-ft	639 lbs-ft	639 lbs-ft	639 lbs-ft	639 lbs-ft	451 lbs-ft	451 lbs-ft	451 lbs-ft	451 lbs-ft
e	0.10 ft	0.09 ft	0.09 ft	0.09 ft	0.22 ft	0.21 ft	0.21 ft	0.20 ft	0.21 ft	0.20 ft	0.20 ft	0.19 ft	2.17 ft	1.72 ft	1.42 ft	1.22 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	265.3 psf	263.2 psf	261.2 psf	259.4 psf	239.2 psf	238.2 psf	237.3 psf	236.5 psf	265.9 psf	263.7 psf	261.7 psf	259.9 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	334.4 psf	329.1 psf	324.2 psf	319.8 psf	409.6 psf	400.9 psf	392.9 psf	385.6 psf	441.2 psf	431.0 psf	421.8 psf	413.3 psf	239.9 psf	122.4 psf	102.5 psf	96.4 psf

Maximum Bearing Pressure =	441 psf
Allowable Bearing Pressure =	1500 psf

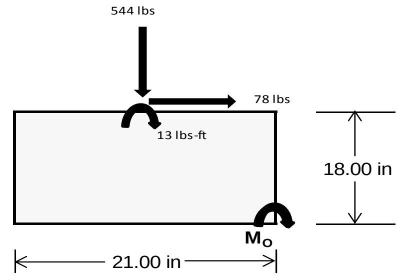
Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O =	346.5 ft-lbs
Resisting Force Required =	396.04 lbs
S.F. =	1.67
Weight Required =	660.07 lbs
Minimum Width =	21 in in
Weight Provided =	1903.13 lbs

A minimum 60in long x 21in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	21 in			21 in			21 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	102 lbs	73 lbs	51 lbs	234 lbs	544 lbs	196 lbs	66 lbs	-17 lbs	17 lbs
F_V	12 lbs	103 lbs	12 lbs	9 lbs	78 lbs	9 lbs	12 lbs	103 lbs	12 lbs
P_{total}	2458 lbs	2429 lbs	2407 lbs	2477 lbs	2787 lbs	2438 lbs	755 lbs	672 lbs	706 lbs
M	34 lbs-ft	172 lbs-ft	35 lbs-ft	25 lbs-ft	129 lbs-ft	27 lbs-ft	34 lbs-ft	172 lbs-ft	35 lbs-ft
e	0.01 ft	0.07 ft	0.01 ft	0.01 ft	0.05 ft	0.01 ft	0.05 ft	0.26 ft	0.05 ft
L/6	0.29 ft	1.61 ft	1.72 ft	1.73 ft	1.66 ft	1.73 ft	1.66 ft	1.24 ft	1.65 ft
f_{min}	267.4 sqft	210.3 sqft	261.2 sqft	273.2 sqft	267.8 sqft	268.1 sqft	72.8 sqft	9.5 sqft	66.9 sqft
f_{max}	294.3 psf	345.0 psf	288.9 psf	293.0 psf	369.2 psf	289.2 psf	99.8 psf	144.1 psf	94.5 psf

Maximum Bearing Pressure = 369 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 21in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 21in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

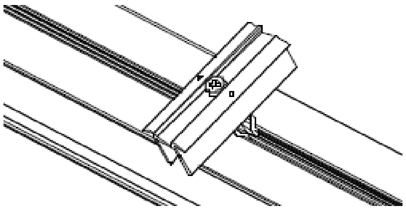
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

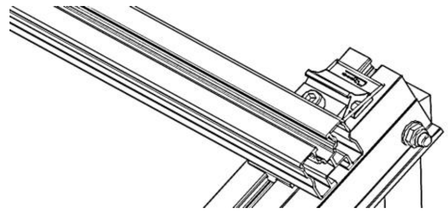
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.773	k
Allowable Uplift =	1.214	k
Utilization =	64%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	1.101	k
Allowable Uplift =	1.116	k
Utilization =	99%	



6.2 Bolted Connections

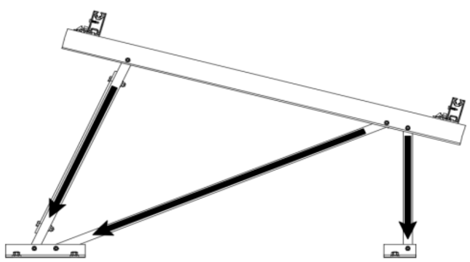
The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	1.062	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	19%	

Rear Strut		
Maximum Axial Load =	1.142	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	20%	

Diagonal Strut		
Maximum Axial Load =	0.188	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	3%	

Bracing		
Maximum Axial Load =	0.158	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	2%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

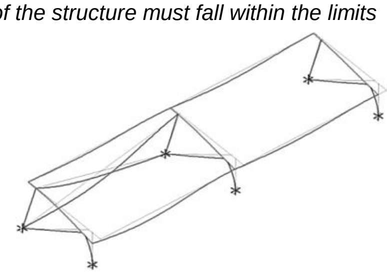
Mean Height, h_{sx} = 28.39 in

Allowable Story Drift for All Other Structures, Δ = { $0.020h_{sx}$; 0.568 in

Max Drift, Δ_{MAX} = 0.053 in

$0.053 \leq 0.568$, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **ProfiPlus**

Strong Axis:

3.4.14

L_b = 48.00 in

J = 0.255

124.989

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.7 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 48.00 in

J = 0.255

129.794

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.7

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 30

Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 29.7 ksi

Ix = 250988 mm^4

0.603 in^4

y = 30 mm

Sx = 0.511 in^3

$M_{max}St$ = 1.266 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 20

Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi

Iy = 120291 mm^4

0.289 in^4

x = 20 mm

Sy = 0.367 in^3

$M_{max}Wk$ = 0.871 k-ft

Compression

3.4.9

b/t = 7.4

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 23.9

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 28.47 ksi

A = 578.06 mm^2

0.90 in^2

P_{max} = 25.51 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **Flex Profi**

Strong Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.41

20.702

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b} Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.9 ksi

3.4.15

N/A for Strong Direction

3.4.16

b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16

N/A for Strong Direction

Weak Axis:

3.4.11

L_b = 33.78 in

ry = 1.374

Cb = 1.41

24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b} Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2

φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))

φF_L= 29.9 ksi

3.4.15

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7

F_{UT}= (φbk2*√(BpE))/(5.1b/t)

F_{UT}= 9.4 ksi

3.4.16

N/A for Weak Direction

3.4.16

b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

F_{ST}= φb[Bp-1.6Dp*b/t]

F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.9 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.466 k-ft

φF_LWk= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.8

b/t = 24.46
S1 = 3.83
S2 = 10.30
φF_L= (φck2*√(BpE))/(5.1b/t)
φF_L= 10.4 ksi

3.4.9

b/t = 4.29
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 24.46
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.9.1

b/t = 24.46
t = 2.6
ds = 6.05
rs = 3.49
S = 21.70
ρst = 0.22
F_{UT}= 10.43
F_{ST}= 28.24
φF_L= Fut + (Fst - Fut)ρst < Fst
φF_L= 14.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 14.29 ksi
A = 576.21 mm^2
0.89 in^2
P_{max} = 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 31.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in

J = 0.16

47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 31.2 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.423 k-ft

Compression

3.4.7

λ = 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.83792

$\varphi F_L = \varphi cc(Bc - Dc^*\lambda)$

$\varphi F_L =$ 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 24.52 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.8 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.404 k-ft

Weak Axis:

3.4.14

L_b = 46.38 in

J = 0.16

121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

$\lambda =$ 1.98863

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.85841

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

$\varphi F_L =$ 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 7.60 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:
3.4.14
L_b = 29.96 in
J = 0.16
78.5957

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 30.5 ksi

3.4.16
b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Not Used
Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0
φF_L= 1.17φyFcy
φF_L= 38.9 ksi

3.4.18
h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LSt= 30.5 ksi
Ix = 39958.2 mm^4
0.096 in^4
y = 15 mm
Sx = 0.163 in^3
M_{max}St = 0.413 k-ft

Weak Axis:
3.4.14
L_b = 29.96 in
J = 0.16
78.5957

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 30.5

3.4.16
b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1
N/A for Weak Direction

3.4.18
h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LWk= 33.3 ksi
Iy = 39958.2 mm^4
0.096 in^4
x = 15 mm
Sy = 0.163 in^3
M_{max}Wk = 0.450 k-ft

Compression

3.4.7

$\lambda =$ 1.28467

$r =$ 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.75985

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

$\varphi F_L =$ 16.1143 ksi

3.4.9

$b/t =$ 7.75

$S1 =$ 12.21 (See 3.4.16 above for formula)

$S2 =$ 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

$b/t =$ 7.75

$S1 =$ 12.21

$S2 =$ 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

$Rb/t =$ 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

$S1 =$ 6.87

$S2 =$ 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 16.11 ksi

$A =$ 323.87 mm^2

0.50 in^2

$P_{max} =$ 8.09 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-63.248	-63.248	0	0
2	M16	Y	-63.248	-63.248	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-112.091	-112.091	0	0
2	M16	y	-179.345	-179.345	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	228.665	228.665	0	0
2	M16	y	112.091	112.091	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	115.378	2	240.1	2	.004	10	0	9	0	1	0	1
2		min	-141.796	3	-363.676	3	-2.105	4	0	3	0	1	0	1
3	N7	max	0	4	348.883	1	.022	10	0	10	0	1	0	1
4		min	-.108	2	-118.369	3	-16.048	4	-.025	4	0	1	0	1
5	N15	max	0	15	1061.707	2	.085	9	0	9	0	1	0	1
6		min	-1.105	2	-402.471	3	-16.44	5	-.026	4	0	1	0	1
7	N16	max	373.999	2	758.131	2	0	11	0	9	0	1	0	1
8		min	-421.28	3	-1160.305	3	-137.18	4	0	3	0	1	0	1
9	N23	max	0	15	349.092	1	.477	1	0	1	0	1	0	1
10		min	-.108	2	-118	3	-15.309	5	-.024	5	0	1	0	1
11	N24	max	115.378	2	242.396	2	59.164	3	0	4	0	1	0	1
12		min	-142.106	3	-362.666	3	-2.927	5	0	3	0	1	0	1
13	Totals:	max	603.433	2	2976.777	2	0	2						
14		min	-705.553	3	-2525.486	3	-189.59	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	250.919	1	.662	6	.841	4	0	10	0	3	0	1
2			min	-364.982	3	.153	15	-.135	3	0	4	0	2	0	1
3		2	max	251.015	1	.624	6	.753	4	0	10	0	4	0	15
4			min	-364.91	3	.144	15	-.135	3	0	4	0	10	0	6
5		3	max	251.112	1	.586	6	.666	4	0	10	0	4	0	15
6			min	-364.837	3	.135	15	-.135	3	0	4	0	3	0	6
7		4	max	251.208	1	.549	6	.579	4	0	10	0	4	0	15
8			min	-364.765	3	.127	15	-.135	3	0	4	0	3	0	6
9		5	max	251.304	1	.511	6	.491	4	0	10	0	4	0	15
10			min	-364.693	3	.118	15	-.135	3	0	4	0	3	0	6
11		6	max	251.401	1	.473	6	.404	4	0	10	0	4	0	15
12			min	-364.621	3	.109	15	-.135	3	0	4	0	3	0	6
13		7	max	251.497	1	.435	6	.317	4	0	10	0	4	0	15
14			min	-364.548	3	.1	15	-.135	3	0	4	0	3	0	6
15		8	max	251.594	1	.397	6	.229	4	0	10	0	4	0	15
16			min	-364.476	3	.091	15	-.135	3	0	4	0	3	0	6
17		9	max	251.69	1	.359	6	.142	4	0	10	0	4	0	15
18			min	-364.404	3	.082	15	-.135	3	0	4	0	3	0	6
19		10	max	251.786	1	.322	6	.121	1	0	10	0	4	0	15
20			min	-364.332	3	.073	15	-.135	3	0	4	0	3	0	6
21		11	max	251.883	1	.284	6	.121	1	0	10	0	4	0	15
22			min	-364.259	3	.064	15	-.135	3	0	4	0	3	0	6
23		12	max	251.979	1	.246	6	.121	1	0	10	0	4	0	15
24			min	-364.187	3	.055	15	-.154	5	0	4	0	3	0	6
25		13	max	252.075	1	.208	6	.121	1	0	10	0	4	0	15
26			min	-364.115	3	.047	15	-.241	5	0	4	0	3	0	6
27		14	max	252.172	1	.17	6	.121	1	0	10	0	4	0	15
28			min	-364.042	3	.038	15	-.329	5	0	4	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	252.268	1	.132	6	.121	1	0	10	0	4	0	15
30			min	-363.97	3	.029	15	-.416	5	0	4	0	3	0	6
31		16	max	252.364	1	.096	2	.121	1	0	10	0	4	0	15
32			min	-363.898	3	.02	15	-.503	5	0	4	0	3	0	6
33		17	max	252.461	1	.066	2	.121	1	0	10	0	4	0	15
34			min	-363.826	3	.011	15	-.591	5	0	4	0	3	0	6
35		18	max	252.557	1	.037	2	.121	1	0	10	0	14	0	15
36			min	-363.753	3	.002	9	-.678	5	0	4	0	3	0	6
37		19	max	252.654	1	.008	10	.121	1	0	10	0	1	0	15
38			min	-363.681	3	-.023	14	-.765	5	0	4	0	3	0	6
39	M3	1	max	56.05	2	1.812	6	.004	10	0	5	0	4	0	6
40			min	-49.447	14	.425	15	-1.346	4	0	1	0	10	0	15
41		2	max	55.983	2	1.634	6	.004	10	0	5	0	1	0	6
42			min	-49.513	14	.383	15	-1.212	4	0	1	0	10	0	15
43		3	max	55.916	2	1.456	6	.004	10	0	5	0	1	0	2
44			min	-49.579	14	.341	15	-1.079	4	0	1	0	10	0	15
45		4	max	55.848	2	1.278	6	.004	10	0	5	0	1	0	15
46			min	-49.645	14	.299	15	-.945	4	0	1	0	5	0	4
47		5	max	55.781	2	1.1	6	.004	10	0	5	0	1	0	15
48			min	-49.711	14	.257	15	-.812	4	0	1	0	5	0	4
49		6	max	55.714	2	.922	6	.004	10	0	5	0	1	0	15
50			min	-49.777	14	.215	15	-.678	4	0	1	0	5	0	4
51		7	max	55.647	2	.744	6	.004	10	0	5	0	1	0	15
52			min	-49.843	14	.173	15	-.545	4	0	1	0	5	0	4
53		8	max	55.58	2	.566	6	.004	10	0	5	0	1	0	15
54			min	-49.909	14	.132	15	-.411	4	0	1	0	5	0	4
55		9	max	55.513	2	.388	6	.004	10	0	5	0	1	0	15
56			min	-49.975	14	.09	15	-.277	4	0	1	0	5	-.001	4
57		10	max	55.446	2	.21	6	.004	10	0	5	0	1	0	15
58			min	-50.041	14	.048	15	-.144	4	0	1	0	5	-.001	4
59		11	max	55.379	2	.04	2	.019	5	0	5	0	1	0	15
60			min	-50.107	14	.006	15	-.138	1	0	1	0	5	-.001	4
61		12	max	55.312	2	-.036	15	.152	5	0	5	0	1	0	15
62			min	-50.172	14	-.146	4	-.138	1	0	1	0	5	-.001	4
63		13	max	55.245	2	-.078	15	.286	5	0	5	0	1	0	15
64			min	-50.238	14	-.324	4	-.138	1	0	1	0	5	-.001	4
65		14	max	55.177	2	-.119	15	.42	5	0	5	0	9	0	15
66			min	-50.304	14	-.502	4	-.138	1	0	1	0	5	-.001	4
67		15	max	55.11	2	-.161	15	.553	5	0	5	0	10	0	15
68			min	-50.37	14	-.68	4	-.138	1	0	1	0	4	0	4
69		16	max	55.043	2	-.203	15	.687	5	0	5	0	10	0	15
70			min	-50.436	14	-.858	4	-.138	1	0	1	0	4	0	4
71		17	max	54.976	2	-.245	15	.82	5	0	5	0	10	0	15
72			min	-50.502	14	-1.036	4	-.138	1	0	1	0	4	0	4
73		18	max	54.909	2	-.287	15	.954	5	0	5	0	10	0	15
74			min	-50.568	14	-1.214	4	-.138	1	0	1	0	4	0	4
75		19	max	54.842	2	-.329	15	1.087	5	0	5	0	5	0	1
76			min	-50.634	14	-1.392	4	-.138	1	0	1	0	1	0	1
77	M4	1	max	347.718	1	0	1	.022	10	0	1	0	5	0	1
78			min	-119.242	3	0	1	-15.223	4	0	1	0	2	0	1
79		2	max	347.783	1	0	1	.022	10	0	1	0	10	0	1
80			min	-119.194	3	0	1	-15.279	4	0	1	-.001	4	0	1
81		3	max	347.848	1	0	1	.022	10	0	1	0	10	0	1
82			min	-119.145	3	0	1	-15.335	4	0	1	-.003	4	0	1
83		4	max	347.912	1	0	1	.022	10	0	1	0	10	0	1
84			min	-119.097	3	0	1	-15.391	4	0	1	-.004	4	0	1
85		5	max	347.977	1	0	1	.022	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	-119.048	3	0	1	-15.447	4	0	1	-.005	4	0	1
87		6	max	348.042	1	0	1	.022	10	0	1	0	10	0	1
88			min	-119	3	0	1	-15.503	4	0	1	-.007	4	0	1
89		7	max	348.106	1	0	1	.022	10	0	1	0	10	0	1
90			min	-118.951	3	0	1	-15.559	4	0	1	-.008	4	0	1
91		8	max	348.171	1	0	1	.022	10	0	1	0	10	0	1
92			min	-118.903	3	0	1	-15.615	4	0	1	-.01	4	0	1
93		9	max	348.236	1	0	1	.022	10	0	1	0	10	0	1
94			min	-118.854	3	0	1	-15.671	4	0	1	-.011	4	0	1
95		10	max	348.3	1	0	1	.022	10	0	1	0	10	0	1
96			min	-118.806	3	0	1	-15.727	4	0	1	-.012	4	0	1
97		11	max	348.365	1	0	1	.022	10	0	1	0	10	0	1
98			min	-118.757	3	0	1	-15.784	4	0	1	-.014	4	0	1
99		12	max	348.43	1	0	1	.022	10	0	1	0	10	0	1
100			min	-118.709	3	0	1	-15.84	4	0	1	-.015	4	0	1
101		13	max	348.495	1	0	1	.022	10	0	1	0	10	0	1
102			min	-118.66	3	0	1	-15.896	4	0	1	-.017	4	0	1
103		14	max	348.559	1	0	1	.022	10	0	1	0	10	0	1
104			min	-118.612	3	0	1	-15.952	4	0	1	-.018	4	0	1
105		15	max	348.624	1	0	1	.022	10	0	1	0	10	0	1
106			min	-118.563	3	0	1	-16.008	4	0	1	-.02	4	0	1
107		16	max	348.689	1	0	1	.022	10	0	1	0	10	0	1
108			min	-118.515	3	0	1	-16.064	4	0	1	-.021	4	0	1
109		17	max	348.753	1	0	1	.022	10	0	1	0	10	0	1
110			min	-118.466	3	0	1	-16.12	4	0	1	-.022	4	0	1
111		18	max	348.818	1	0	1	.022	10	0	1	0	10	0	1
112			min	-118.417	3	0	1	-16.176	4	0	1	-.024	4	0	1
113		19	max	348.883	1	0	1	.022	10	0	1	0	10	0	1
114			min	-118.369	3	0	1	-16.232	4	0	1	-.025	4	0	1
115	M6	1	max	792.418	1	.649	6	.838	4	0	3	0	3	0	1
116			min	-1141.887	3	.15	15	-.289	3	0	5	0	1	0	1
117		2	max	792.514	1	.611	6	.75	4	0	3	0	4	0	15
118			min	-1141.815	3	.141	15	-.289	3	0	5	0	1	0	6
119		3	max	792.61	1	.574	6	.663	4	0	3	0	4	0	15
120			min	-1141.743	3	.132	15	-.289	3	0	5	0	2	0	6
121		4	max	792.707	1	.536	6	.576	4	0	3	0	4	0	15
122			min	-1141.671	3	.124	15	-.289	3	0	5	0	2	0	6
123		5	max	792.803	1	.498	6	.488	4	0	3	0	4	0	15
124			min	-1141.598	3	.115	15	-.289	3	0	5	0	3	0	6
125		6	max	792.899	1	.46	6	.401	4	0	3	0	4	0	15
126			min	-1141.526	3	.106	15	-.289	3	0	5	0	3	0	6
127		7	max	792.996	1	.422	6	.314	4	0	3	0	4	0	15
128			min	-1141.454	3	.097	15	-.289	3	0	5	0	3	0	6
129		8	max	793.092	1	.384	6	.226	4	0	3	0	4	0	15
130			min	-1141.381	3	.088	15	-.289	3	0	5	0	3	0	6
131		9	max	793.189	1	.347	6	.139	4	0	3	0	4	0	15
132			min	-1141.309	3	.079	15	-.289	3	0	5	0	3	0	6
133		10	max	793.285	1	.309	6	.052	4	0	3	0	4	0	15
134			min	-1141.237	3	.07	15	-.289	3	0	5	0	3	0	6
135		11	max	793.381	1	.271	6	.031	9	0	3	0	4	0	15
136			min	-1141.165	3	.061	15	-.289	3	0	5	0	3	0	6
137		12	max	793.478	1	.241	2	.031	9	0	3	0	4	0	15
138			min	-1141.092	3	.052	15	-.289	3	0	5	0	3	0	6
139		13	max	793.574	1	.212	2	.031	9	0	3	0	4	0	15
140			min	-1141.02	3	.044	15	-.289	3	0	5	0	3	0	6
141		14	max	793.67	1	.182	2	.031	9	0	3	0	4	0	15
142			min	-1140.948	3	.035	15	-.31	5	0	5	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	793.767	1	.153	2	.031	9	0	3	0	4	0	15
144			min	-1140.875	3	.026	15	-.397	5	0	5	0	3	0	6
145		16	max	793.863	1	.123	2	.031	9	0	3	0	4	0	15
146			min	-1140.803	3	.017	15	-.484	5	0	5	0	3	0	6
147		17	max	793.959	1	.094	2	.031	9	0	3	0	4	0	15
148			min	-1140.731	3	.002	9	-.572	5	0	5	0	3	0	6
149		18	max	794.056	1	.064	2	.031	9	0	3	0	4	0	15
150			min	-1140.659	3	-.023	9	-.659	5	0	5	0	3	0	6
151		19	max	794.152	1	.035	2	.031	9	0	3	0	4	0	15
152			min	-1140.586	3	-.047	9	-.746	5	0	5	0	3	0	6
153	M7	1	max	187.722	2	1.819	4	0	2	0	9	0	4	0	4
154			min	-91.09	9	.431	15	-1.41	4	0	3	0	3	0	15
155		2	max	187.655	2	1.641	4	0	2	0	9	0	4	0	4
156			min	-91.146	9	.389	15	-1.277	4	0	3	0	3	0	15
157		3	max	187.588	2	1.463	4	0	2	0	9	0	4	0	2
158			min	-91.201	9	.348	15	-1.143	4	0	3	0	3	0	9
159		4	max	187.521	2	1.285	4	0	2	0	9	0	1	0	15
160			min	-91.257	9	.306	15	-1.01	4	0	3	0	3	0	9
161		5	max	187.454	2	1.107	4	0	2	0	9	0	1	0	15
162			min	-91.313	9	.264	15	-.876	4	0	3	0	3	0	6
163		6	max	187.387	2	.929	4	0	2	0	9	0	1	0	15
164			min	-91.369	9	.222	15	-.743	4	0	3	0	5	0	6
165		7	max	187.32	2	.751	4	0	2	0	9	0	1	0	15
166			min	-91.425	9	.18	15	-.609	4	0	3	0	5	0	6
167		8	max	187.252	2	.573	4	0	2	0	9	0	1	0	15
168			min	-91.481	9	.138	15	-.475	4	0	3	0	5	0	6
169		9	max	187.185	2	.395	4	0	2	0	9	0	1	0	15
170			min	-91.537	9	.096	15	-.342	4	0	3	0	5	-.001	6
171		10	max	187.118	2	.217	4	0	2	0	9	0	1	0	15
172			min	-91.593	9	.055	15	-.208	4	0	3	0	5	-.001	6
173		11	max	187.051	2	.057	2	0	2	0	9	0	1	0	15
174			min	-91.649	9	.001	9	-.075	4	0	3	0	5	-.001	6
175		12	max	186.984	2	-.029	15	.061	5	0	9	0	1	0	15
176			min	-91.705	9	-.14	6	-.018	1	0	3	0	5	-.001	6
177		13	max	186.917	2	-.071	15	.195	5	0	9	0	1	0	15
178			min	-91.761	9	-.318	6	-.018	1	0	3	0	5	-.001	6
179		14	max	186.85	2	-.113	15	.328	5	0	9	0	1	0	15
180			min	-91.816	9	-.496	6	-.018	1	0	3	0	5	-.001	6
181		15	max	186.783	2	-.155	15	.462	5	0	9	0	1	0	15
182			min	-91.872	9	-.674	6	-.018	1	0	3	0	5	0	6
183		16	max	186.716	2	-.196	15	.595	5	0	9	0	1	0	15
184			min	-91.928	9	-.852	6	-.018	1	0	3	0	5	0	6
185		17	max	186.649	2	-.238	15	.729	5	0	9	0	9	0	15
186			min	-91.984	9	-1.03	6	-.018	1	0	3	0	5	0	6
187		18	max	186.582	2	-.28	15	.862	5	0	9	0	9	0	15
188			min	-92.04	9	-1.208	6	-.018	1	0	3	0	5	0	6
189		19	max	186.514	2	-.322	15	.996	5	0	9	0	9	0	1
190			min	-92.096	9	-1.386	6	-.018	1	0	3	0	3	0	1
191	M8	1	max	1060.542	2	0	1	.091	9	0	1	0	4	0	1
192			min	-403.345	3	0	1	-15.581	4	0	1	0	3	0	1
193		2	max	1060.607	2	0	1	.091	9	0	1	0	9	0	1
194			min	-403.296	3	0	1	-15.637	4	0	1	-.001	4	0	1
195		3	max	1060.671	2	0	1	.091	9	0	1	0	9	0	1
196			min	-403.248	3	0	1	-15.693	4	0	1	-.003	4	0	1
197		4	max	1060.736	2	0	1	.091	9	0	1	0	9	0	1
198			min	-403.199	3	0	1	-15.749	4	0	1	-.004	4	0	1
199		5	max	1060.801	2	0	1	.091	9	0	1	0	9	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	-403.151	3	0	1	-15.805	4	0	1	-.006	4	0	1
201		6	max	1060.865	2	0	1	.091	9	0	1	0	9	0	1
202			min	-403.102	3	0	1	-15.861	4	0	1	-.007	4	0	1
203		7	max	1060.93	2	0	1	.091	9	0	1	0	9	0	1
204			min	-403.054	3	0	1	-15.917	4	0	1	-.008	4	0	1
205		8	max	1060.995	2	0	1	.091	9	0	1	0	9	0	1
206			min	-403.005	3	0	1	-15.973	4	0	1	-.01	4	0	1
207		9	max	1061.059	2	0	1	.091	9	0	1	0	9	0	1
208			min	-402.957	3	0	1	-16.029	4	0	1	-.011	4	0	1
209		10	max	1061.124	2	0	1	.091	9	0	1	0	9	0	1
210			min	-402.908	3	0	1	-16.085	4	0	1	-.013	4	0	1
211		11	max	1061.189	2	0	1	.091	9	0	1	0	9	0	1
212			min	-402.86	3	0	1	-16.142	4	0	1	-.014	4	0	1
213		12	max	1061.254	2	0	1	.091	9	0	1	0	9	0	1
214			min	-402.811	3	0	1	-16.198	4	0	1	-.016	4	0	1
215		13	max	1061.318	2	0	1	.091	9	0	1	0	9	0	1
216			min	-402.763	3	0	1	-16.254	4	0	1	-.017	4	0	1
217		14	max	1061.383	2	0	1	.091	9	0	1	0	9	0	1
218			min	-402.714	3	0	1	-16.31	4	0	1	-.019	4	0	1
219		15	max	1061.448	2	0	1	.091	9	0	1	0	9	0	1
220			min	-402.666	3	0	1	-16.366	4	0	1	-.02	4	0	1
221		16	max	1061.512	2	0	1	.091	9	0	1	0	9	0	1
222			min	-402.617	3	0	1	-16.422	4	0	1	-.021	4	0	1
223		17	max	1061.577	2	0	1	.091	9	0	1	0	9	0	1
224			min	-402.568	3	0	1	-16.478	4	0	1	-.023	4	0	1
225		18	max	1061.642	2	0	1	.091	9	0	1	0	9	0	1
226			min	-402.52	3	0	1	-16.534	4	0	1	-.024	4	0	1
227		19	max	1061.707	2	0	1	.091	9	0	1	0	9	0	1
228			min	-402.471	3	0	1	-16.59	4	0	1	-.026	4	0	1
229	M10	1	max	252.241	1	.692	4	.967	5	0	1	0	4	0	1
230			min	-327.436	3	.174	15	-.105	1	-.001	5	0	3	0	1
231		2	max	252.338	1	.654	4	.88	5	0	1	0	4	0	15
232			min	-327.363	3	.165	15	-.105	1	-.001	5	0	3	0	4
233		3	max	252.434	1	.616	4	.792	5	0	1	0	4	0	15
234			min	-327.291	3	.156	15	-.105	1	-.001	5	0	3	0	4
235		4	max	252.53	1	.578	4	.705	5	0	1	0	4	0	15
236			min	-327.219	3	.147	15	-.105	1	-.001	5	0	3	0	4
237		5	max	252.627	1	.541	4	.618	5	0	1	0	5	0	15
238			min	-327.146	3	.138	15	-.105	1	-.001	5	0	3	0	4
239		6	max	252.723	1	.503	4	.53	5	0	1	0	5	0	15
240			min	-327.074	3	.129	15	-.105	1	-.001	5	0	3	0	4
241		7	max	252.82	1	.465	4	.443	5	0	1	0	5	0	15
242			min	-327.002	3	.12	15	-.105	1	-.001	5	0	3	0	4
243		8	max	252.916	1	.427	4	.356	5	0	1	0	5	0	15
244			min	-326.93	3	.111	15	-.105	1	-.001	5	0	3	0	4
245		9	max	253.012	1	.389	4	.268	5	0	1	0	5	0	15
246			min	-326.857	3	.102	15	-.105	1	-.001	5	0	3	0	4
247		10	max	253.109	1	.351	4	.181	5	0	1	0	5	0	15
248			min	-326.785	3	.094	15	-.105	1	-.001	5	0	3	0	4
249		11	max	253.205	1	.314	4	.094	5	0	1	0	5	0	15
250			min	-326.713	3	.085	15	-.105	1	-.001	5	0	3	0	4
251		12	max	253.301	1	.276	4	.006	5	0	1	0	5	0	15
252			min	-326.641	3	.076	15	-.105	1	-.001	5	0	3	0	4
253		13	max	253.398	1	.238	4	0	10	0	1	0	5	0	15
254			min	-326.568	3	.067	15	-.105	1	-.001	5	0	3	0	4
255		14	max	253.494	1	.2	4	0	10	0	1	0	5	0	15
256			min	-326.496	3	.058	15	-.179	4	-.001	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	253.59	1	.162	4	0	10	0	1	0	5	0	15
258			min	-326.424	3	.049	15	-.266	4	-.001	5	0	3	0	4
259		16	max	253.687	1	.124	4	0	10	0	1	0	5	0	15
260			min	-326.351	3	.04	15	-.353	4	-.001	5	0	3	0	4
261		17	max	253.783	1	.087	4	0	10	0	1	0	5	0	15
262			min	-326.279	3	.026	9	-.441	4	-.001	5	0	3	0	4
263		18	max	253.88	1	.051	3	0	10	0	1	0	5	0	15
264			min	-326.207	3	.002	9	-.528	4	-.001	5	0	3	0	4
265		19	max	253.976	1	.028	3	0	10	0	1	0	5	0	15
266			min	-326.135	3	-.023	9	-.615	4	-.001	5	0	3	0	4
267	M11	1	max	55.644	2	1.812	6	.144	1	0	4	0	5	0	6
268			min	-48.457	9	.424	15	-1.238	5	0	10	0	1	0	15
269		2	max	55.577	2	1.634	6	.144	1	0	4	0	5	0	6
270			min	-48.513	9	.382	15	-1.104	5	0	10	0	1	0	15
271		3	max	55.509	2	1.456	6	.144	1	0	4	0	5	0	2
272			min	-48.569	9	.34	15	-.971	5	0	10	0	1	0	3
273		4	max	55.442	2	1.278	6	.144	1	0	4	0	3	0	15
274			min	-48.625	9	.299	15	-.837	5	0	10	0	1	0	4
275		5	max	55.375	2	1.1	6	.144	1	0	4	0	3	0	15
276			min	-48.681	9	.257	15	-.704	5	0	10	0	1	0	4
277		6	max	55.308	2	.922	6	.144	1	0	4	0	3	0	15
278			min	-48.737	9	.215	15	-.57	5	0	10	0	1	0	4
279		7	max	55.241	2	.744	6	.144	1	0	4	0	3	0	15
280			min	-48.793	9	.173	15	-.437	5	0	10	0	1	0	4
281		8	max	55.174	2	.566	6	.144	1	0	4	0	3	0	15
282			min	-48.849	9	.131	15	-.303	5	0	10	0	4	0	4
283		9	max	55.107	2	.388	6	.144	1	0	4	0	3	0	15
284			min	-48.905	9	.089	15	-.17	5	0	10	0	4	-.001	4
285		10	max	55.04	2	.21	6	.144	1	0	4	0	3	0	15
286			min	-48.961	9	.047	15	-.036	5	0	10	0	4	-.001	4
287		11	max	54.973	2	.04	2	.144	1	0	4	0	3	0	15
288			min	-49.016	9	.003	3	-.024	3	0	10	0	4	-.001	4
289		12	max	54.906	2	-.036	15	.262	4	0	4	0	3	0	15
290			min	-49.072	9	-.147	4	-.024	3	0	10	0	4	-.001	4
291		13	max	54.838	2	-.078	15	.396	4	0	4	0	3	0	15
292			min	-49.128	9	-.325	4	-.024	3	0	10	0	5	-.001	4
293		14	max	54.771	2	-.12	15	.529	4	0	4	0	3	0	15
294			min	-49.184	9	-.503	4	-.024	3	0	10	0	5	-.001	4
295		15	max	54.704	2	-.162	15	.663	4	0	4	0	3	0	15
296			min	-49.24	9	-.681	4	-.024	3	0	10	0	10	0	4
297		16	max	54.637	2	-.204	15	.796	4	0	4	0	3	0	15
298			min	-49.296	9	-.859	4	-.024	3	0	10	0	10	0	4
299		17	max	54.57	2	-.245	15	.93	4	0	4	0	4	0	15
300			min	-49.352	9	-1.037	4	-.024	3	0	10	0	10	0	4
301		18	max	54.503	2	-.287	15	1.064	4	0	4	0	4	0	15
302			min	-49.408	9	-1.215	4	-.024	3	0	10	0	10	0	4
303		19	max	54.436	2	-.329	15	1.197	4	0	4	0	4	0	1
304			min	-49.464	9	-1.393	4	-.024	3	0	10	0	10	0	1
305	M12	1	max	347.927	1	0	1	.507	1	0	1	0	4	0	1
306			min	-118.873	3	0	1	-14.306	5	0	1	0	3	0	1
307		2	max	347.992	1	0	1	.507	1	0	1	0	1	0	1
308			min	-118.825	3	0	1	-14.362	5	0	1	-.001	5	0	1
309		3	max	348.056	1	0	1	.507	1	0	1	0	1	0	1
310			min	-118.776	3	0	1	-14.418	5	0	1	-.003	5	0	1
311		4	max	348.121	1	0	1	.507	1	0	1	0	1	0	1
312			min	-118.728	3	0	1	-14.475	5	0	1	-.004	5	0	1
313		5	max	348.186	1	0	1	.507	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	-118.679	3	0	1	-14.531	5	0	1	-.005	5	0	1
315		6	max	348.25	1	0	1	.507	1	0	1	0	1	0	1
316			min	-118.631	3	0	1	-14.587	5	0	1	-.006	5	0	1
317		7	max	348.315	1	0	1	.507	1	0	1	0	1	0	1
318			min	-118.582	3	0	1	-14.643	5	0	1	-.008	5	0	1
319		8	max	348.38	1	0	1	.507	1	0	1	0	1	0	1
320			min	-118.534	3	0	1	-14.699	5	0	1	-.009	5	0	1
321		9	max	348.445	1	0	1	.507	1	0	1	0	1	0	1
322			min	-118.485	3	0	1	-14.755	5	0	1	-.01	5	0	1
323		10	max	348.509	1	0	1	.507	1	0	1	0	1	0	1
324			min	-118.436	3	0	1	-14.811	5	0	1	-.012	5	0	1
325		11	max	348.574	1	0	1	.507	1	0	1	0	1	0	1
326			min	-118.388	3	0	1	-14.867	5	0	1	-.013	5	0	1
327		12	max	348.639	1	0	1	.507	1	0	1	0	1	0	1
328			min	-118.339	3	0	1	-14.923	5	0	1	-.014	5	0	1
329		13	max	348.703	1	0	1	.507	1	0	1	0	1	0	1
330			min	-118.291	3	0	1	-14.979	5	0	1	-.016	5	0	1
331		14	max	348.768	1	0	1	.507	1	0	1	0	1	0	1
332			min	-118.242	3	0	1	-15.035	5	0	1	-.017	5	0	1
333		15	max	348.833	1	0	1	.507	1	0	1	0	1	0	1
334			min	-118.194	3	0	1	-15.091	5	0	1	-.018	5	0	1
335		16	max	348.897	1	0	1	.507	1	0	1	0	1	0	1
336			min	-118.145	3	0	1	-15.147	5	0	1	-.02	5	0	1
337		17	max	348.962	1	0	1	.507	1	0	1	0	1	0	1
338			min	-118.097	3	0	1	-15.204	5	0	1	-.021	5	0	1
339		18	max	349.027	1	0	1	.507	1	0	1	0	1	0	1
340			min	-118.048	3	0	1	-15.26	5	0	1	-.022	5	0	1
341		19	max	349.092	1	0	1	.507	1	0	1	0	1	0	1
342			min	-118	3	0	1	-15.316	5	0	1	-.024	5	0	1
343	M1	1	max	51.995	1	343.592	3	.383	10	0	1	.026	4	0	2
344			min	2.855	10	-254.011	1	-14.711	4	0	3	0	10	0	3
345		2	max	52.067	1	343.39	3	.383	10	0	1	.023	4	.055	1
346			min	2.915	10	-254.281	1	-14.469	4	0	3	0	10	-.075	3
347		3	max	61.408	1	4.49	4	.383	10	0	5	.019	4	.11	1
348			min	-5.875	3	-21.607	3	-13.387	4	0	1	0	10	-.148	3
349		4	max	61.48	1	4.144	14	.383	10	0	5	.017	4	.11	1
350			min	-5.821	3	-21.809	3	-13.145	4	0	1	0	10	-.143	3
351		5	max	61.553	1	3.879	14	.383	10	0	5	.014	4	.111	1
352			min	-5.766	3	-22.011	3	-12.903	4	0	1	0	10	-.138	3
353		6	max	61.625	1	3.614	14	.383	10	0	5	.011	4	.113	2
354			min	-5.712	3	-22.214	3	-12.661	4	0	1	0	10	-.134	3
355		7	max	61.697	1	3.349	14	.383	10	0	5	.008	4	.116	2
356			min	-5.658	3	-22.416	3	-12.419	4	0	1	0	10	-.129	3
357		8	max	61.769	1	3.084	14	.383	10	0	5	.006	4	.12	2
358			min	-5.604	3	-22.618	3	-12.177	4	0	1	0	10	-.124	3
359		9	max	61.842	1	2.819	14	.383	10	0	5	.003	4	.123	2
360			min	-5.55	3	-22.82	3	-12.166	1	0	1	0	10	-.119	3
361		10	max	61.914	1	2.554	14	.383	10	0	5	.001	3	.127	2
362			min	-5.495	3	-23.023	3	-12.166	1	0	1	0	10	-.114	3
363		11	max	61.986	1	2.289	14	.383	10	0	5	0	3	.131	2
364			min	-5.441	3	-23.225	3	-12.166	1	0	1	-.003	1	-.109	3
365		12	max	62.058	1	2.038	9	.383	10	0	5	0	10	.135	2
366			min	-5.387	3	-23.427	3	-12.166	1	0	1	-.005	1	-.104	3
367		13	max	62.131	1	1.813	9	.383	10	0	5	0	10	.138	2
368			min	-5.333	3	-23.63	3	-12.166	1	0	1	-.008	1	-.099	3
369		14	max	62.203	1	1.588	9	.383	10	0	5	0	10	.142	2
370			min	-5.279	3	-23.832	3	-12.166	1	0	1	-.01	1	-.094	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	62.275	1	1.364	9	.383	10	0	5	0	10	.146	2
372			min	-5.224	3	-24.034	3	-12.166	1	0	1	-.013	1	-.088	3
373		16	max	69.225	2	16.466	2	.387	10	0	1	0	10	.15	2
374			min	-34.665	3	-50.69	3	-12.294	1	0	4	-.016	1	-.083	3
375		17	max	69.297	2	16.197	2	.387	10	0	1	0	10	.147	2
376			min	-34.611	3	-50.893	3	-12.294	1	0	4	-.019	1	-.072	3
377		18	max	-2.398	12	340.097	2	.409	10	0	3	0	10	.074	2
378			min	-52.016	1	-166.354	3	-23.731	4	0	2	-.021	1	-.036	3
379		19	max	-2.362	12	339.827	2	.409	10	0	3	0	10	0	2
380			min	-51.944	1	-166.556	3	-23.489	4	0	2	-.026	4	0	3
381	M5	1	max	129.039	1	1103.768	3	0	11	0	9	.03	4	0	3
382			min	-1.994	3	-811.527	1	-53.112	3	0	3	0	11	0	2
383		2	max	129.111	1	1103.566	3	0	11	0	9	.026	4	.175	1
384			min	-1.94	3	-811.797	1	-53.112	3	0	3	-.004	3	-.239	3
385		3	max	157.424	1	6.266	9	5.717	3	0	3	.021	4	.348	1
386			min	-42.944	3	-75.859	3	-16.504	4	0	4	-.015	3	-.473	3
387		4	max	157.496	1	6.041	9	5.717	3	0	3	.018	4	.353	1
388			min	-42.89	3	-76.061	3	-16.262	4	0	4	-.013	3	-.456	3
389		5	max	157.568	1	5.816	9	5.717	3	0	3	.014	4	.357	1
390			min	-42.836	3	-76.263	3	-16.02	4	0	4	-.012	3	-.44	3
391		6	max	157.64	1	5.591	9	5.717	3	0	3	.011	4	.362	1
392			min	-42.782	3	-76.466	3	-15.778	4	0	4	-.011	3	-.423	3
393		7	max	157.713	1	5.367	9	5.717	3	0	3	.007	4	.372	2
394			min	-42.727	3	-76.668	3	-15.536	4	0	4	-.01	3	-.407	3
395		8	max	157.785	1	5.142	9	5.717	3	0	3	.004	4	.384	2
396			min	-42.673	3	-76.87	3	-15.294	4	0	4	-.008	3	-.39	3
397		9	max	157.857	1	4.917	9	5.717	3	0	3	0	4	.396	2
398			min	-42.619	3	-77.072	3	-15.052	4	0	4	-.007	3	-.373	3
399		10	max	157.929	1	4.692	9	5.717	3	0	3	0	1	.408	2
400			min	-42.565	3	-77.275	3	-14.81	4	0	4	-.006	3	-.357	3
401		11	max	158.002	1	4.468	9	5.717	3	0	3	0	2	.42	2
402			min	-42.511	3	-77.477	3	-14.568	4	0	4	-.006	4	-.34	3
403		12	max	158.074	1	4.243	9	5.717	3	0	3	0	2	.432	2
404			min	-42.456	3	-77.679	3	-14.326	4	0	4	-.009	4	-.323	3
405		13	max	158.146	1	4.018	9	5.717	3	0	3	0	11	.445	2
406			min	-42.402	3	-77.882	3	-14.084	4	0	4	-.012	4	-.306	3
407		14	max	158.219	1	3.793	9	5.717	3	0	3	0	11	.457	2
408			min	-42.348	3	-78.084	3	-13.842	4	0	4	-.015	4	-.289	3
409		15	max	158.291	1	3.568	9	5.717	3	0	3	0	3	.469	2
410			min	-42.294	3	-78.286	3	-13.6	4	0	4	-.018	4	-.272	3
411		16	max	221.612	2	65.832	2	5.693	3	0	3	0	3	.481	2
412			min	-106.368	3	-134.086	3	-12.368	4	0	4	-.021	4	-.255	3
413		17	max	221.684	2	65.562	2	5.693	3	0	3	.002	3	.467	2
414			min	-106.314	3	-134.289	3	-12.126	4	0	4	-.024	4	-.226	3
415		18	max	-1.673	12	1086.514	2	5.261	3	0	4	.003	3	.235	2
416			min	-129.225	1	-524.935	3	-27.147	5	0	9	-.03	4	-.113	3
417		19	max	-1.636	12	1086.244	2	5.261	3	0	4	.004	3	0	3
418			min	-129.153	1	-525.138	3	-26.905	5	0	9	-.035	4	0	2
419	M9	1	max	51.961	1	343.539	3	112.2	4	0	3	0	5	0	2
420			min	-.596	5	-254.01	1	-.383	10	0	1	-.024	1	0	3
421		2	max	52.034	1	343.337	3	112.442	4	0	3	.025	5	.055	1
422			min	-.563	5	-254.28	1	-.383	10	0	1	-.021	1	-.075	3
423		3	max	61.704	1	4.049	9	12.061	1	0	4	.047	5	.109	1
424			min	-6.145	3	-21.52	3	-21.672	5	0	10	-.018	1	-.148	3
425		4	max	61.776	1	3.824	9	12.061	1	0	4	.042	5	.11	1
426			min	-6.091	3	-21.722	3	-21.43	5	0	10	-.016	1	-.143	3
427		5	max	61.848	1	3.599	9	12.061	1	0	4	.037	5	.111	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-6.036	3	-21.924	3	-21.188	5	0	10	-.013	1	-.138	3
429		6	max	61.92	1	3.375	9	12.061	1	0	4	.033	5	.113	2
430			min	-5.982	3	-22.126	3	-20.946	5	0	10	-.011	1	-.133	3
431		7	max	61.993	1	3.15	9	12.061	1	0	4	.028	5	.116	2
432			min	-5.928	3	-22.329	3	-20.704	5	0	10	-.008	1	-.129	3
433		8	max	62.065	1	2.925	9	12.061	1	0	4	.024	5	.12	2
434			min	-5.874	3	-22.531	3	-20.462	5	0	10	-.005	1	-.124	3
435		9	max	62.137	1	2.7	9	12.061	1	0	4	.019	5	.123	2
436			min	-5.82	3	-22.733	3	-20.22	5	0	10	-.003	1	-.119	3
437		10	max	62.209	1	2.476	9	12.061	1	0	4	.015	4	.127	2
438			min	-5.765	3	-22.936	3	-19.978	5	0	10	0	1	-.114	3
439		11	max	62.282	1	2.251	9	12.061	1	0	4	.011	4	.131	2
440			min	-5.711	3	-23.138	3	-19.736	5	0	10	0	10	-.109	3
441		12	max	62.354	1	2.026	9	12.061	1	0	4	.008	4	.135	2
442			min	-5.657	3	-23.34	3	-19.494	5	0	10	0	10	-.104	3
443		13	max	62.426	1	1.801	9	12.061	1	0	4	.008	1	.138	2
444			min	-5.603	3	-23.543	3	-19.252	5	0	10	0	10	-.099	3
445		14	max	62.498	1	1.577	9	12.061	1	0	4	.01	1	.142	2
446			min	-5.549	3	-23.745	3	-19.01	5	0	10	-.002	5	-.094	3
447		15	max	62.571	1	1.352	9	12.061	1	0	4	.013	1	.146	2
448			min	-5.494	3	-23.947	3	-18.768	5	0	10	-.006	5	-.088	3
449		16	max	69.291	2	16.221	2	12.197	1	0	10	.016	1	.15	2
450			min	-35.419	3	-51.041	3	-17.363	5	0	4	-.009	5	-.083	3
451		17	max	69.363	2	15.951	2	12.197	1	0	10	.018	1	.147	2
452			min	-35.365	3	-51.244	3	-17.121	5	0	4	-.013	5	-.072	3
453		18	max	9.177	5	340.097	2	12.694	1	0	2	.021	1	.074	2
454			min	-51.971	1	-166.348	3	-31.177	5	0	3	-.019	5	-.036	3
455		19	max	9.211	5	339.827	2	12.694	1	0	2	.024	1	0	2
456			min	-51.899	1	-166.55	3	-30.935	5	0	3	-.026	5	0	3
457	M13	1	max	112.199	4	253.858	1	.596	5	0	2	.024	1	0	1
458			min	-.383	10	-343.571	3	-51.959	1	0	3	0	5	0	3
459		2	max	107.834	4	180.64	1	1.205	5	0	2	.01	3	.131	3
460			min	-.383	10	-244.078	3	-39.015	1	0	3	-.002	10	-.097	1
461		3	max	103.469	4	107.423	1	1.813	5	0	2	.007	3	.217	3
462			min	-.383	10	-144.585	3	-26.071	1	0	3	-.011	1	-.161	1
463		4	max	99.104	4	34.205	1	2.421	5	0	2	.005	3	.259	3
464			min	-.383	10	-45.092	3	-13.127	1	0	3	-.019	1	-.192	1
465		5	max	94.739	4	54.402	3	3.03	5	0	2	.004	3	.257	3
466			min	-.383	10	-39.013	1	-3.548	3	0	3	-.022	1	-.191	1
467		6	max	90.374	4	153.895	3	12.762	1	0	2	.004	5	.211	3
468			min	-.383	10	-112.23	1	-2.975	3	0	3	-.02	1	-.157	1
469		7	max	86.008	4	253.388	3	25.706	1	0	2	.006	5	.12	3
470			min	-.383	10	-185.448	1	-2.403	3	0	3	-.011	1	-.091	1
471		8	max	81.643	4	352.881	3	38.65	1	0	2	.008	4	.007	1
472			min	-.383	10	-258.665	1	-1.831	3	0	3	0	12	-.014	3
473		9	max	77.278	4	452.374	3	51.595	1	0	2	.023	1	.139	1
474			min	-.383	10	-331.883	1	-1.259	3	0	3	0	3	-.193	3
475		10	max	72.913	4	12.624	5	64.539	1	0	2	.049	1	.302	1
476			min	-.383	10	-551.867	3	.606	12	0	3	-.017	5	-.417	3
477		11	max	49.616	4	331.883	1	7.325	5	0	3	.023	1	.139	1
478			min	-.383	10	-452.374	3	-51.561	1	0	2	-.014	5	-.193	3
479		12	max	45.251	4	258.665	1	7.933	5	0	3	.004	2	.007	1
480			min	-.383	10	-352.881	3	-38.617	1	0	2	-.01	5	-.014	3
481		13	max	40.885	4	185.448	1	8.542	5	0	3	0	10	.12	3
482			min	-.383	10	-253.388	3	-25.673	1	0	2	-.011	1	-.091	1
483		14	max	36.52	4	112.23	1	9.15	5	0	3	-.001	10	.211	3
484			min	-.383	10	-153.895	3	-12.729	1	0	2	-.02	1	-.157	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	32.155	4	39.013	1	10.139	4	0	3	.001	5	.257	3
486			min	-.383	10	-54.401	3	-2.116	2	0	2	-.022	1	-.191	1
487		16	max	27.79	4	45.092	3	13.267	4	0	3	.006	5	.259	3
488			min	-.383	10	-34.205	1	-.404	10	0	2	-.019	1	-.192	1
489		17	max	23.425	4	144.585	3	26.104	1	0	3	.011	5	.217	3
490			min	-.383	10	-107.423	1	.682	10	0	2	-.011	1	-.161	1
491		18	max	19.06	4	244.078	3	39.048	1	0	3	.017	4	.131	3
492			min	-.383	10	-180.64	1	1.768	10	0	2	-.002	10	-.097	1
493		19	max	14.694	4	343.571	3	51.992	1	0	3	.026	4	0	1
494			min	-.383	10	-253.858	1	2.855	10	0	2	0	10	0	3
495	M16	1	max	30.923	5	339.893	2	9.211	5	0	3	.024	1	0	2
496			min	-12.678	1	-166.564	3	-51.901	1	0	2	-.026	5	0	3
497		2	max	26.557	5	241.743	2	9.819	5	0	3	.004	1	.063	3
498			min	-12.678	1	-118.882	3	-38.957	1	0	2	-.022	5	-.129	2
499		3	max	22.192	5	143.593	2	10.428	5	0	3	0	12	.106	3
500			min	-12.678	1	-71.199	3	-26.013	1	0	2	-.019	4	-.215	2
501		4	max	17.827	5	45.443	2	11.036	5	0	3	-.001	12	.127	3
502			min	-12.678	1	-23.517	3	-13.069	1	0	2	-.019	1	-.257	2
503		5	max	13.462	5	24.166	3	11.644	5	0	3	-.002	12	.127	3
504			min	-12.678	1	-52.707	2	-2.231	3	0	2	-.022	1	-.255	2
505		6	max	9.097	5	71.848	3	14.545	4	0	3	-.001	10	.105	3
506			min	-12.678	1	-150.857	2	-1.659	3	0	2	-.019	1	-.21	2
507		7	max	4.731	5	119.531	3	25.764	1	0	3	.003	5	.063	3
508			min	-12.678	1	-249.007	2	-1.086	3	0	2	-.011	1	-.121	2
509		8	max	2.243	3	167.213	3	38.708	1	0	3	.01	4	.011	2
510			min	-12.678	1	-347.157	2	-.514	3	0	2	-.005	3	-.001	3
511		9	max	2.243	3	214.896	3	51.652	1	0	3	.024	1	.187	2
512			min	-12.678	1	-445.307	2	.058	3	0	2	-.005	3	-.086	3
513		10	max	18.546	5	-8.109	15	64.597	1	0	14	.049	1	.407	2
514			min	-12.678	1	-543.457	2	-1.481	3	0	2	-.004	3	-.192	3
515		11	max	14.181	5	445.307	2	6.393	5	0	2	.023	1	.187	2
516			min	-12.658	1	-214.896	3	-51.607	1	0	3	-.011	5	-.086	3
517		12	max	9.816	5	347.157	2	7.002	5	0	2	.004	2	.011	2
518			min	-12.658	1	-167.213	3	-38.663	1	0	3	-.008	5	-.001	3
519		13	max	5.451	5	249.007	2	7.61	5	0	2	0	10	.063	3
520			min	-12.658	1	-119.531	3	-25.719	1	0	3	-.011	1	-.121	2
521		14	max	1.086	5	150.857	2	8.218	5	0	2	0	12	.105	3
522			min	-12.658	1	-71.848	3	-12.774	1	0	3	-.019	1	-.21	2
523		15	max	.409	10	52.707	2	9.183	4	0	2	.003	5	.127	3
524			min	-12.658	1	-24.166	3	-2.157	2	0	3	-.022	1	-.255	2
525		16	max	.409	10	23.517	3	13.114	1	0	2	.007	5	.127	3
526			min	-12.658	1	-45.443	2	-.425	10	0	3	-.019	1	-.257	2
527		17	max	.409	10	71.199	3	26.058	1	0	2	.011	5	.106	3
528			min	-14.776	4	-143.593	2	.661	10	0	3	-.011	1	-.215	2
529		18	max	.409	10	118.882	3	39.002	1	0	2	.017	4	.063	3
530			min	-19.141	4	-241.743	2	1.748	10	0	3	-.002	10	-.129	2
531		19	max	.409	10	166.564	3	51.947	1	0	2	.026	4	0	2
532			min	-23.506	4	-339.893	2	2.361	12	0	3	0	10	0	3
533	M15	1	max	0	1	.824	3	.136	3	0	1	0	1	0	1
534			min	-69.458	3	0	1	0	1	0	3	0	3	0	1
535		2	max	0	1	.732	3	.136	3	0	1	0	1	0	1
536			min	-69.512	3	0	1	0	1	0	3	0	3	0	3
537		3	max	0	1	.641	3	.136	3	0	1	0	1	0	1
538			min	-69.566	3	0	1	0	1	0	3	0	3	0	3
539		4	max	0	1	.549	3	.136	3	0	1	0	1	0	1
540			min	-69.62	3	0	1	0	1	0	3	0	3	0	3
541		5	max	0	1	.458	3	.136	3	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-69.674	3	0	1	0	1	0	3	0	3	0	3
543		6	max	0	1	.366	3	.136	3	0	1	0	1	0	1
544			min	-69.728	3	0	1	0	1	0	3	0	3	0	3
545		7	max	0	1	.275	3	.136	3	0	1	0	3	0	1
546			min	-69.782	3	0	1	0	1	0	3	0	1	0	3
547		8	max	0	1	.183	3	.136	3	0	1	0	3	0	1
548			min	-69.836	3	0	1	0	1	0	3	0	1	0	3
549		9	max	0	1	.092	3	.136	3	0	1	0	3	0	1
550			min	-69.89	3	0	1	0	1	0	3	0	1	0	3
551		10	max	0	1	0	1	.136	3	0	1	0	3	0	1
552			min	-69.944	3	0	1	0	1	0	3	0	1	0	3
553		11	max	0	1	0	1	.136	3	0	1	0	3	0	1
554			min	-69.998	3	-.092	3	0	1	0	3	0	1	0	3
555		12	max	0	1	0	1	.136	3	0	1	0	3	0	1
556			min	-70.052	3	-.183	3	0	1	0	3	0	1	0	3
557		13	max	0	1	0	1	.136	3	0	1	0	3	0	1
558			min	-70.106	3	-.275	3	0	1	0	3	0	1	0	3
559		14	max	0	1	0	1	.136	3	0	1	0	3	0	1
560			min	-70.16	3	-.366	3	0	1	0	3	0	1	0	3
561		15	max	0	1	0	1	.136	3	0	1	0	3	0	1
562			min	-70.214	3	-.458	3	0	1	0	3	0	1	0	3
563		16	max	0	1	0	1	.136	3	0	1	0	3	0	1
564			min	-70.268	3	-.549	3	0	1	0	3	0	1	0	3
565		17	max	0	1	0	1	.136	3	0	1	0	3	0	1
566			min	-70.322	3	-.641	3	0	1	0	3	0	1	0	3
567		18	max	0	1	0	1	.136	3	0	1	0	3	0	1
568			min	-70.376	3	-.732	3	0	1	0	3	0	1	0	3
569		19	max	0	1	0	1	.136	3	0	1	0	3	0	1
570			min	-70.43	3	-.824	3	0	1	0	3	0	1	0	1
571	M16A	1	max	0	2	1.961	4	.239	4	0	3	0	3	0	1
572			min	-157.988	4	0	2	-.053	3	0	1	0	4	0	1
573		2	max	0	2	1.743	4	.217	4	0	3	0	3	0	2
574			min	-158	4	0	2	-.053	3	0	1	0	4	0	4
575		3	max	0	2	1.525	4	.195	4	0	3	0	3	0	2
576			min	-158.011	4	0	2	-.053	3	0	1	0	4	0	4
577		4	max	0	2	1.307	4	.173	4	0	3	0	3	0	2
578			min	-158.023	4	0	2	-.053	3	0	1	0	1	-.001	4
579		5	max	0	2	1.09	4	.151	4	0	3	0	3	0	2
580			min	-158.035	4	0	2	-.053	3	0	1	0	1	-.002	4
581		6	max	0	2	.872	4	.128	4	0	3	0	3	0	2
582			min	-158.046	4	0	2	-.053	3	0	1	0	1	-.002	4
583		7	max	0	2	.654	4	.106	4	0	3	0	3	0	2
584			min	-158.058	4	0	2	-.053	3	0	1	0	1	-.002	4
585		8	max	0	2	.436	4	.084	4	0	3	0	5	0	2
586			min	-158.07	4	0	2	-.053	3	0	1	0	1	-.002	4
587		9	max	0	2	.218	4	.062	4	0	3	0	5	0	2
588			min	-158.081	4	0	2	-.053	3	0	1	0	1	-.002	4
589		10	max	0	2	0	1	.046	1	0	3	0	5	0	2
590			min	-158.093	4	0	1	-.053	3	0	1	0	1	-.002	4
591		11	max	0	2	0	2	.046	1	0	3	0	5	0	2
592			min	-158.105	4	-.218	4	-.053	3	0	1	0	1	-.002	4
593		12	max	0	2	0	2	.046	1	0	3	0	5	0	2
594			min	-158.116	4	-.436	4	-.053	3	0	1	0	1	-.002	4
595		13	max	.007	1	0	2	.046	1	0	3	0	5	0	2
596			min	-158.128	4	-.654	4	-.053	3	0	1	0	9	-.002	4
597		14	max	.079	1	0	2	.046	1	0	3	0	5	0	2
598			min	-158.14	4	-.872	4	-.053	5	0	1	0	3	-.002	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.151	1	0	2	.046	1	0	3	0	4	0	2
600			min	-158.151	4	-1.09	4	-.075	5	0	1	0	3	-.002	4
601		16	max	.223	1	0	2	.046	1	0	3	0	4	0	2
602			min	-158.163	4	-1.307	4	-.098	5	0	1	0	3	-.001	4
603		17	max	.295	1	0	2	.046	1	0	3	0	1	0	2
604			min	-158.175	4	-1.525	4	-.12	5	0	1	0	3	0	4
605		18	max	.367	1	0	2	.046	1	0	3	0	1	0	2
606			min	-158.204	5	-1.743	4	-.142	5	0	1	0	3	0	4
607		19	max	.439	1	0	2	.046	1	0	3	0	1	0	1
608			min	-158.275	5	-1.961	4	-.164	5	0	1	0	3	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	1	.005	2	.002	1	8.691e-4	5	NC	3	NC	1
2			min	-.003	3	-.005	3	-.008	5	-1.795e-4	1	5552.937	2	NC	1
3		2	max	.002	1	.005	2	.002	1	8.879e-4	5	NC	3	NC	1
4			min	-.003	3	-.004	3	-.008	5	-1.718e-4	1	6034.955	2	NC	1
5		3	max	.002	1	.005	2	.002	1	9.067e-4	5	NC	1	NC	1
6			min	-.002	3	-.004	3	-.008	5	-1.642e-4	1	6604.045	2	NC	1
7		4	max	.002	1	.004	2	.001	1	9.256e-4	5	NC	1	NC	1
8			min	-.002	3	-.004	3	-.007	5	-1.565e-4	1	7280.82	2	NC	1
9		5	max	.001	1	.004	2	.001	1	9.444e-4	5	NC	1	NC	1
10			min	-.002	3	-.004	3	-.007	5	-1.488e-4	1	8092.643	2	NC	1
11		6	max	.001	1	.003	2	.001	1	9.633e-4	5	NC	1	NC	1
12			min	-.002	3	-.004	3	-.007	5	-1.411e-4	1	9076.45	2	NC	1
13		7	max	.001	1	.003	2	0	1	9.821e-4	5	NC	1	NC	1
14			min	-.002	3	-.003	3	-.006	5	-1.334e-4	1	NC	1	NC	1
15		8	max	.001	1	.003	2	0	1	1.001e-3	5	NC	1	NC	1
16			min	-.002	3	-.003	3	-.006	5	-1.257e-4	1	NC	1	NC	1
17		9	max	.001	1	.002	2	0	1	1.02e-3	5	NC	1	NC	1
18			min	-.002	3	-.003	3	-.005	5	-1.18e-4	1	NC	1	NC	1
19		10	max	0	1	.002	2	0	1	1.039e-3	5	NC	1	NC	1
20			min	-.001	3	-.003	3	-.005	5	-1.104e-4	1	NC	1	NC	1
21		11	max	0	1	.002	2	0	1	1.057e-3	5	NC	1	NC	1
22			min	-.001	3	-.003	3	-.005	5	-1.027e-4	1	NC	1	NC	1
23		12	max	0	1	.001	2	0	1	1.076e-3	5	NC	1	NC	1
24			min	-.001	3	-.002	3	-.004	5	-9.499e-5	1	NC	1	NC	1
25		13	max	0	1	.001	2	0	1	1.095e-3	5	NC	1	NC	1
26			min	0	3	-.002	3	-.004	5	-8.73e-5	1	NC	1	NC	1
27		14	max	0	1	0	2	0	1	1.114e-3	5	NC	1	NC	1
28			min	0	3	-.002	3	-.003	5	-7.962e-5	1	NC	1	NC	1
29		15	max	0	1	0	2	0	1	1.133e-3	5	NC	1	NC	1
30			min	0	3	-.001	3	-.002	5	-7.193e-5	1	NC	1	NC	1
31		16	max	0	1	0	2	0	1	1.152e-3	5	NC	1	NC	1
32			min	0	3	-.001	3	-.002	5	-6.425e-5	1	NC	1	NC	1
33		17	max	0	1	0	2	0	1	1.171e-3	5	NC	1	NC	1
34			min	0	3	0	3	-.001	5	-5.656e-5	1	NC	1	NC	1
35		18	max	0	1	0	2	0	1	1.189e-3	5	NC	1	NC	1
36			min	0	3	0	3	0	5	-4.888e-5	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	1.208e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-4.119e-5	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	1.879e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-5.5e-4	5	NC	1	NC	1
41		2	max	0	14	0	2	.003	5	2.611e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	1	-5.535e-4	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	14	0	2	.006	5	3.342e-5	1	NC	1	NC	1
44			min	0	2	-.001	3	0	1	-5.57e-4	5	NC	1	NC	1
45		4	max	0	14	0	2	.009	4	4.073e-5	1	NC	1	NC	1
46			min	0	2	-.002	3	0	1	-5.606e-4	5	NC	1	NC	1
47		5	max	0	14	0	2	.012	4	4.805e-5	1	NC	1	NC	1
48			min	0	2	-.003	3	0	9	-5.641e-4	5	NC	1	NC	1
49		6	max	0	14	0	2	.015	4	5.536e-5	1	NC	1	NC	1
50			min	0	2	-.003	3	0	9	-5.676e-4	5	NC	1	NC	1
51		7	max	0	14	0	2	.018	4	6.268e-5	1	NC	1	NC	1
52			min	0	2	-.004	3	0	9	-5.711e-4	5	NC	1	NC	1
53		8	max	0	14	0	2	.02	4	6.999e-5	1	NC	1	NC	1
54			min	0	2	-.004	3	0	9	-5.747e-4	5	NC	1	NC	1
55		9	max	0	14	0	2	.023	4	7.73e-5	1	NC	1	NC	1
56			min	0	2	-.005	3	0	10	-5.782e-4	5	NC	1	NC	1
57		10	max	0	14	.001	2	.026	4	8.462e-5	1	NC	1	NC	1
58			min	0	2	-.005	3	0	10	-5.817e-4	5	NC	1	NC	1
59		11	max	0	14	.002	2	.028	4	9.193e-5	1	NC	1	NC	1
60			min	0	2	-.006	3	0	10	-5.853e-4	5	NC	1	NC	1
61		12	max	0	14	.002	2	.031	4	9.925e-5	1	NC	1	NC	1
62			min	0	2	-.006	3	0	10	-5.888e-4	5	NC	1	NC	1
63		13	max	0	14	.003	2	.033	4	1.066e-4	1	NC	1	NC	1
64			min	0	2	-.006	3	0	10	-5.923e-4	5	NC	1	NC	1
65		14	max	0	14	.003	2	.036	4	1.139e-4	1	NC	1	NC	1
66			min	0	2	-.006	3	0	10	-5.959e-4	5	NC	1	NC	1
67		15	max	0	14	.004	2	.038	4	1.212e-4	1	NC	1	NC	1
68			min	0	2	-.007	3	0	10	-5.994e-4	5	NC	1	NC	1
69		16	max	0	14	.005	2	.04	4	1.285e-4	1	NC	1	NC	1
70			min	0	2	-.007	3	0	10	-6.029e-4	5	9142.315	2	NC	1
71		17	max	0	14	.006	2	.042	4	1.358e-4	1	NC	1	NC	1
72			min	0	2	-.007	3	0	10	-6.065e-4	5	7770.866	2	NC	1
73		18	max	0	14	.007	2	.044	4	1.431e-4	1	NC	3	NC	1
74			min	0	2	-.007	3	0	10	-6.1e-4	5	6717.76	2	NC	1
75		19	max	0	14	.008	2	.047	4	1.504e-4	1	NC	3	NC	1
76			min	0	2	-.007	3	0	10	-6.135e-4	5	5899.813	2	NC	1
77	M4	1	max	.002	1	.006	2	0	10	1.979e-3	5	NC	1	NC	1
78			min	0	3	-.005	3	-.049	4	-1.538e-4	1	NC	1	392.499	4
79		2	max	.002	1	.006	2	0	10	1.979e-3	5	NC	1	NC	1
80			min	0	3	-.005	3	-.045	4	-1.538e-4	1	NC	1	427.828	4
81		3	max	.001	1	.006	2	0	10	1.979e-3	5	NC	1	NC	1
82			min	0	3	-.004	3	-.041	4	-1.538e-4	1	NC	1	469.87	4
83		4	max	.001	1	.005	2	0	10	1.979e-3	5	NC	1	NC	1
84			min	0	3	-.004	3	-.037	4	-1.538e-4	1	NC	1	520.394	4
85		5	max	.001	1	.005	2	0	10	1.979e-3	5	NC	1	NC	1
86			min	0	3	-.004	3	-.033	4	-1.538e-4	1	NC	1	581.807	4
87		6	max	.001	1	.004	2	0	10	1.979e-3	5	NC	1	NC	1
88			min	0	3	-.004	3	-.029	4	-1.538e-4	1	NC	1	657.459	4
89		7	max	.001	1	.004	2	0	10	1.979e-3	5	NC	1	NC	1
90			min	0	3	-.003	3	-.026	4	-1.538e-4	1	NC	1	752.12	4
91		8	max	.001	1	.004	2	0	10	1.979e-3	5	NC	1	NC	1
92			min	0	3	-.003	3	-.022	4	-1.538e-4	1	NC	1	872.771	4
93		9	max	0	1	.003	2	0	10	1.979e-3	5	NC	1	NC	1
94			min	0	3	-.003	3	-.019	4	-1.538e-4	1	NC	1	1029.975	4
95		10	max	0	1	.003	2	0	10	1.979e-3	5	NC	1	NC	1
96			min	0	3	-.002	3	-.016	4	-1.538e-4	1	NC	1	1240.334	4
97		11	max	0	1	.003	2	0	10	1.979e-3	5	NC	1	NC	1
98			min	0	3	-.002	3	-.013	4	-1.538e-4	1	NC	1	1531.187	4
99		12	max	0	1	.002	2	0	10	1.979e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	3	-.002	3	-.01	4	-1.538e-4	1	NC	1	1950.222	4
101		13	max	0	1	.002	2	0	10	1.979e-3	5	NC	1	NC	1
102			min	0	3	-.002	3	-.007	4	-1.538e-4	1	NC	1	2586.881	4
103		14	max	0	1	.002	2	0	10	1.979e-3	5	NC	1	NC	1
104			min	0	3	-.001	3	-.005	4	-1.538e-4	1	NC	1	3625.649	4
105		15	max	0	1	.001	2	0	10	1.979e-3	5	NC	1	NC	1
106			min	0	3	-.001	3	-.004	4	-1.538e-4	1	NC	1	5499.91	4
107		16	max	0	1	.001	2	0	10	1.979e-3	5	NC	1	NC	1
108			min	0	3	0	3	-.002	4	-1.538e-4	1	NC	1	9441.609	4
109		17	max	0	1	0	2	0	10	1.979e-3	5	NC	1	NC	1
110			min	0	3	0	3	0	4	-1.538e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	10	1.979e-3	5	NC	1	NC	1
112			min	0	3	0	3	0	4	-1.538e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	1.979e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-1.538e-4	1	NC	1	NC	1
115	M6	1	max	.006	1	.018	2	0	9	9.202e-4	4	NC	3	NC	1
116			min	-.008	3	-.013	3	-.008	5	-8.849e-8	2	1710.596	2	7389.299	3
117		2	max	.006	1	.016	2	0	9	9.389e-4	4	NC	3	NC	1
118			min	-.008	3	-.013	3	-.008	5	-8.382e-8	2	1826.677	2	7912.218	3
119		3	max	.005	1	.015	2	0	9	9.577e-4	4	NC	3	NC	1
120			min	-.008	3	-.012	3	-.008	5	-8.487e-7	1	1959.238	2	8525.052	3
121		4	max	.005	1	.014	2	0	9	9.764e-4	4	NC	3	NC	1
122			min	-.007	3	-.011	3	-.007	5	-2.34e-6	1	2111.587	2	9247.926	3
123		5	max	.005	1	.013	2	0	9	9.951e-4	4	NC	3	NC	1
124			min	-.007	3	-.011	3	-.007	5	-3.832e-6	1	2287.984	2	NC	1
125		6	max	.004	1	.012	2	0	9	1.014e-3	4	NC	3	NC	1
126			min	-.006	3	-.01	3	-.007	5	-5.323e-6	1	2494.011	2	NC	1
127		7	max	.004	1	.011	2	0	9	1.032e-3	4	NC	3	NC	1
128			min	-.006	3	-.009	3	-.006	5	-6.815e-6	1	2737.115	2	NC	1
129		8	max	.004	1	.01	2	0	9	1.051e-3	4	NC	3	NC	1
130			min	-.005	3	-.009	3	-.006	5	-8.307e-6	1	3027.46	2	NC	1
131		9	max	.003	1	.009	2	0	9	1.07e-3	4	NC	3	NC	1
132			min	-.005	3	-.008	3	-.006	5	-9.798e-6	1	3379.285	2	NC	1
133		10	max	.003	1	.008	2	0	9	1.089e-3	4	NC	3	NC	1
134			min	-.004	3	-.007	3	-.005	5	-1.129e-5	1	3813.164	2	NC	1
135		11	max	.003	1	.007	2	0	9	1.107e-3	4	NC	3	NC	1
136			min	-.004	3	-.007	3	-.005	5	-1.278e-5	1	4359.965	2	NC	1
137		12	max	.002	1	.006	2	0	9	1.126e-3	4	NC	3	NC	1
138			min	-.003	3	-.006	3	-.004	5	-1.427e-5	1	5068.207	2	NC	1
139		13	max	.002	1	.005	2	0	9	1.145e-3	4	NC	3	NC	1
140			min	-.003	3	-.005	3	-.004	5	-1.576e-5	1	6018.757	2	NC	1
141		14	max	.002	1	.004	2	0	9	1.163e-3	4	NC	1	NC	1
142			min	-.002	3	-.004	3	-.003	5	-1.726e-5	1	7357.189	2	NC	1
143		15	max	.001	1	.003	2	0	9	1.182e-3	4	NC	1	NC	1
144			min	-.002	3	-.003	3	-.002	5	-1.875e-5	1	9374.65	2	NC	1
145		16	max	0	1	.002	2	0	1	1.201e-3	4	NC	1	NC	1
146			min	-.001	3	-.003	3	-.002	5	-2.024e-5	1	NC	1	NC	1
147		17	max	0	1	.002	2	0	1	1.22e-3	4	NC	1	NC	1
148			min	0	3	-.002	3	-.001	5	-2.173e-5	1	NC	1	NC	1
149		18	max	0	1	0	2	0	1	1.238e-3	4	NC	1	NC	1
150			min	0	3	0	3	0	4	-2.322e-5	1	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.257e-3	4	NC	1	NC	1
152			min	0	1	0	1	0	1	-2.471e-5	1	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	1.126e-5	1	NC	1	NC	1
154			min	0	1	0	1	0	1	-5.721e-4	4	NC	1	NC	1
155		2	max	0	9	.001	2	.003	4	1.085e-5	1	NC	1	NC	1
156			min	0	2	-.001	3	0	1	-5.637e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	9	.002	2	.006	4	1.044e-5	1	NC	1	NC	1
158			min	0	2	-.003	3	0	1	-5.553e-4	4	NC	1	NC	1
159		4	max	0	9	.003	2	.009	4	1.004e-5	1	NC	1	NC	1
160			min	0	2	-.004	3	0	1	-5.469e-4	4	NC	1	NC	1
161		5	max	0	9	.004	2	.012	4	9.631e-6	1	NC	1	NC	1
162			min	0	2	-.006	3	0	1	-5.385e-4	4	NC	1	NC	1
163		6	max	0	9	.005	2	.015	4	9.225e-6	1	NC	1	NC	1
164			min	0	2	-.007	3	0	1	-5.302e-4	4	8748.546	2	NC	1
165		7	max	0	9	.006	2	.018	4	2.409e-5	3	NC	3	NC	1
166			min	0	2	-.008	3	0	1	-5.218e-4	4	7237.41	2	NC	1
167		8	max	0	9	.008	2	.021	4	4.144e-5	3	NC	3	NC	1
168			min	0	2	-.01	3	0	1	-5.134e-4	4	6124.783	2	NC	1
169		9	max	0	9	.009	2	.024	4	5.879e-5	3	NC	3	NC	1
170			min	0	2	-.011	3	0	1	-5.05e-4	4	5267.039	2	NC	1
171		10	max	0	9	.01	2	.027	4	7.614e-5	3	NC	3	NC	1
172			min	-.001	2	-.012	3	0	1	-4.967e-4	4	4584.475	2	NC	1
173		11	max	0	9	.011	2	.03	4	9.349e-5	3	NC	3	NC	1
174			min	-.001	2	-.013	3	0	1	-4.883e-4	4	4029.038	2	NC	1
175		12	max	0	9	.013	2	.032	4	1.108e-4	3	NC	3	NC	1
176			min	-.001	2	-.014	3	0	1	-4.799e-4	4	3569.749	2	NC	1
177		13	max	0	9	.014	2	.035	4	1.282e-4	3	NC	3	NC	1
178			min	-.001	2	-.015	3	0	9	-4.715e-4	4	3185.5	2	NC	1
179		14	max	0	9	.016	2	.037	4	1.455e-4	3	NC	3	NC	1
180			min	-.002	2	-.016	3	0	9	-4.631e-4	4	2861.233	2	NC	1
181		15	max	0	9	.018	2	.039	4	1.629e-4	3	NC	3	NC	1
182			min	-.002	2	-.017	3	0	9	-4.548e-4	4	2585.8	2	NC	1
183		16	max	0	9	.02	2	.042	4	1.803e-4	3	NC	3	NC	1
184			min	-.002	2	-.018	3	0	9	-4.464e-4	4	2350.7	2	NC	1
185		17	max	0	9	.021	2	.044	4	1.976e-4	3	NC	3	NC	1
186			min	-.002	2	-.019	3	0	9	-4.38e-4	4	2149.306	2	NC	1
187		18	max	0	9	.023	2	.046	4	2.15e-4	3	NC	3	NC	1
188			min	-.002	2	-.019	3	0	9	-4.296e-4	4	1976.363	2	NC	1
189		19	max	.001	9	.025	2	.048	4	2.323e-4	3	NC	3	NC	1
190			min	-.002	2	-.02	3	0	9	-4.212e-4	4	1827.654	2	NC	1
191	M8	1	max	.005	2	.02	2	0	9	1.81e-3	4	NC	1	NC	1
192			min	-.002	3	-.015	3	-.05	4	-1.845e-4	3	NC	1	383.719	4
193		2	max	.005	2	.019	2	0	9	1.81e-3	4	NC	1	NC	1
194			min	-.002	3	-.014	3	-.046	4	-1.845e-4	3	NC	1	418.259	4
195		3	max	.004	2	.018	2	0	9	1.81e-3	4	NC	1	NC	1
196			min	-.002	3	-.013	3	-.042	4	-1.845e-4	3	NC	1	459.364	4
197		4	max	.004	2	.017	2	0	9	1.81e-3	4	NC	1	NC	1
198			min	-.002	3	-.012	3	-.038	4	-1.845e-4	3	NC	1	508.76	4
199		5	max	.004	2	.016	2	0	9	1.81e-3	4	NC	1	NC	1
200			min	-.001	3	-.012	3	-.034	4	-1.845e-4	3	NC	1	568.805	4
201		6	max	.004	2	.015	2	0	9	1.81e-3	4	NC	1	NC	1
202			min	-.001	3	-.011	3	-.03	4	-1.845e-4	3	NC	1	642.77	4
203		7	max	.003	2	.013	2	0	9	1.81e-3	4	NC	1	NC	1
204			min	-.001	3	-.01	3	-.026	4	-1.845e-4	3	NC	1	735.321	4
205		8	max	.003	2	.012	2	0	9	1.81e-3	4	NC	1	NC	1
206			min	-.001	3	-.009	3	-.023	4	-1.845e-4	3	NC	1	853.284	4
207		9	max	.003	2	.011	2	0	9	1.81e-3	4	NC	1	NC	1
208			min	-.001	3	-.008	3	-.019	4	-1.845e-4	3	NC	1	1006.987	4
209		10	max	.003	2	.01	2	0	9	1.81e-3	4	NC	1	NC	1
210			min	0	3	-.007	3	-.016	4	-1.845e-4	3	NC	1	1212.662	4
211		11	max	.002	2	.009	2	0	9	1.81e-3	4	NC	1	NC	1
212			min	0	3	-.007	3	-.013	4	-1.845e-4	3	NC	1	1497.04	4
213		12	max	.002	2	.008	2	0	9	1.81e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	3	-.006	3	-.01	4	-1.845e-4	3	NC	1	1906.749	4
215		13	max	.002	2	.007	2	0	9	1.81e-3	4	NC	1	NC	1
216			min	0	3	-.005	3	-.008	4	-1.845e-4	3	NC	1	2529.243	4
217		14	max	.001	2	.006	2	0	9	1.81e-3	4	NC	1	NC	1
218			min	0	3	-.004	3	-.005	4	-1.845e-4	3	NC	1	3544.903	4
219		15	max	.001	2	.004	2	0	9	1.81e-3	4	NC	1	NC	1
220			min	0	3	-.003	3	-.004	4	-1.845e-4	3	NC	1	5377.482	4
221		16	max	0	2	.003	2	0	9	1.81e-3	4	NC	1	NC	1
222			min	0	3	-.002	3	-.002	4	-1.845e-4	3	NC	1	9231.542	4
223		17	max	0	2	.002	2	0	9	1.81e-3	4	NC	1	NC	1
224			min	0	3	-.002	3	0	4	-1.845e-4	3	NC	1	NC	1
225		18	max	0	2	.001	2	0	9	1.81e-3	4	NC	1	NC	1
226			min	0	3	0	3	0	4	-1.845e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	1.81e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-1.845e-4	3	NC	1	NC	1
229	M10	1	max	.002	1	.005	2	0	3	1.835e-4	1	NC	3	NC	1
230			min	-.002	3	-.005	3	-.003	4	-3.959e-4	3	5563.113	2	NC	1
231		2	max	.002	1	.005	2	0	3	1.945e-4	4	NC	3	NC	1
232			min	-.002	3	-.004	3	-.003	4	-3.848e-4	3	6046.237	2	NC	1
233		3	max	.002	1	.005	2	0	3	2.376e-4	4	NC	1	NC	1
234			min	-.002	3	-.004	3	-.003	4	-3.736e-4	3	6616.675	2	NC	1
235		4	max	.002	1	.004	2	0	3	2.807e-4	4	NC	1	NC	1
236			min	-.002	3	-.004	3	-.003	4	-3.624e-4	3	7295.105	2	NC	1
237		5	max	.001	1	.004	2	0	3	3.239e-4	4	NC	1	NC	1
238			min	-.002	3	-.004	3	-.003	4	-3.513e-4	3	8108.981	2	NC	1
239		6	max	.001	1	.003	2	0	3	3.67e-4	4	NC	1	NC	1
240			min	-.002	3	-.004	3	-.003	4	-3.401e-4	3	9095.365	2	NC	1
241		7	max	.001	1	.003	2	0	3	4.101e-4	4	NC	1	NC	1
242			min	-.002	3	-.004	3	-.003	4	-3.29e-4	3	NC	1	NC	1
243		8	max	.001	1	.003	2	0	3	4.532e-4	4	NC	1	NC	1
244			min	-.001	3	-.003	3	-.003	4	-3.178e-4	3	NC	1	NC	1
245		9	max	.001	1	.002	2	0	3	4.964e-4	4	NC	1	NC	1
246			min	-.001	3	-.003	3	-.003	4	-3.067e-4	3	NC	1	NC	1
247		10	max	0	1	.002	2	0	3	5.395e-4	4	NC	1	NC	1
248			min	-.001	3	-.003	3	-.003	4	-2.955e-4	3	NC	1	NC	1
249		11	max	0	1	.002	2	0	3	5.826e-4	4	NC	1	NC	1
250			min	-.001	3	-.003	3	-.003	4	-2.844e-4	3	NC	1	NC	1
251		12	max	0	1	.001	2	0	3	6.257e-4	4	NC	1	NC	1
252			min	0	3	-.002	3	-.003	4	-2.732e-4	3	NC	1	NC	1
253		13	max	0	1	0	2	0	3	6.688e-4	4	NC	1	NC	1
254			min	0	3	-.002	3	-.002	4	-2.621e-4	3	NC	1	NC	1
255		14	max	0	1	0	2	0	3	7.12e-4	4	NC	1	NC	1
256			min	0	3	-.002	3	-.002	4	-2.509e-4	3	NC	1	NC	1
257		15	max	0	1	0	2	0	3	7.551e-4	4	NC	1	NC	1
258			min	0	3	-.002	3	-.002	4	-2.398e-4	3	NC	1	NC	1
259		16	max	0	1	0	2	0	3	7.982e-4	4	NC	1	NC	1
260			min	0	3	-.001	3	-.001	4	-2.286e-4	3	NC	1	NC	1
261		17	max	0	1	0	2	0	3	8.413e-4	4	NC	1	NC	1
262			min	0	3	0	3	0	4	-2.175e-4	3	NC	1	NC	1
263		18	max	0	1	0	2	0	3	8.845e-4	4	NC	1	NC	1
264			min	0	3	0	3	0	4	-2.063e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	9.276e-4	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-1.952e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	8.909e-5	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-4.227e-4	4	NC	1	NC	1
269		2	max	0	9	0	2	.002	4	7.188e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-4.65e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	9	0	2	.005	4	5.466e-5	3	NC	1	NC	1
272			min	0	2	-.001	3	0	3	-5.073e-4	4	NC	1	NC	1
273		4	max	0	9	0	2	.007	4	3.745e-5	3	NC	1	NC	1
274			min	0	2	-.002	3	-.001	3	-5.496e-4	4	NC	1	NC	1
275		5	max	0	9	0	2	.009	4	2.024e-5	3	NC	1	NC	1
276			min	0	2	-.003	3	-.002	3	-5.919e-4	4	NC	1	NC	1
277		6	max	0	9	0	2	.012	4	3.028e-6	3	NC	1	NC	1
278			min	0	2	-.003	3	-.002	3	-6.342e-4	4	NC	1	NC	1
279		7	max	0	9	0	2	.014	4	2.09e-6	10	NC	1	NC	1
280			min	0	2	-.004	3	-.002	3	-6.765e-4	4	NC	1	NC	1
281		8	max	0	9	0	2	.017	4	2.385e-6	10	NC	1	NC	1
282			min	0	2	-.005	3	-.002	3	-7.188e-4	4	NC	1	NC	1
283		9	max	0	9	0	2	.019	5	2.68e-6	10	NC	1	NC	1
284			min	0	2	-.005	3	-.002	3	-7.611e-4	4	NC	1	NC	1
285		10	max	0	9	.001	2	.021	5	2.974e-6	10	NC	1	NC	1
286			min	0	2	-.006	3	-.002	3	-8.034e-4	4	NC	1	NC	1
287		11	max	0	9	.002	2	.024	5	3.269e-6	10	NC	1	NC	1
288			min	0	2	-.006	3	-.003	3	-8.457e-4	4	NC	1	NC	1
289		12	max	0	9	.002	2	.026	5	3.564e-6	10	NC	1	NC	1
290			min	0	2	-.006	3	-.003	3	-8.881e-4	4	NC	1	NC	1
291		13	max	0	9	.003	2	.028	5	3.859e-6	10	NC	1	NC	1
292			min	0	2	-.006	3	-.003	3	-9.304e-4	4	NC	1	NC	1
293		14	max	0	9	.003	2	.031	5	4.154e-6	10	NC	1	NC	1
294			min	0	2	-.007	3	-.003	3	-9.727e-4	4	NC	1	NC	1
295		15	max	0	9	.004	2	.033	5	4.448e-6	10	NC	1	NC	1
296			min	0	2	-.007	3	-.002	3	-1.015e-3	4	NC	1	NC	1
297		16	max	0	9	.005	2	.035	5	4.743e-6	10	NC	1	NC	1
298			min	0	2	-.007	3	-.002	3	-1.057e-3	4	9153.918	2	NC	1
299		17	max	0	9	.006	2	.038	5	5.038e-6	10	NC	1	NC	1
300			min	0	2	-.007	3	-.002	3	-1.1e-3	4	7779.607	2	NC	1
301		18	max	0	9	.007	2	.04	5	5.333e-6	10	NC	3	NC	1
302			min	0	2	-.007	3	-.002	3	-1.142e-3	4	6724.555	2	NC	1
303		19	max	0	9	.008	2	.042	5	5.628e-6	10	NC	3	NC	1
304			min	0	2	-.007	3	-.002	1	-1.184e-3	4	5905.256	2	NC	1
305	M12	1	max	.002	1	.006	2	.002	1	2.454e-3	4	NC	1	NC	1
306			min	0	3	-.005	3	-.046	5	-5.621e-6	10	NC	1	417.079	5
307		2	max	.002	1	.006	2	.001	1	2.454e-3	4	NC	1	NC	1
308			min	0	3	-.005	3	-.043	5	-5.621e-6	10	NC	1	454.611	5
309		3	max	.001	1	.006	2	.001	1	2.454e-3	4	NC	1	NC	1
310			min	0	3	-.004	3	-.039	5	-5.621e-6	10	NC	1	499.274	5
311		4	max	.001	1	.005	2	.001	1	2.454e-3	4	NC	1	NC	1
312			min	0	3	-.004	3	-.035	5	-5.621e-6	10	NC	1	552.946	5
313		5	max	.001	1	.005	2	.001	1	2.454e-3	4	NC	1	NC	1
314			min	0	3	-.004	3	-.031	5	-5.621e-6	10	NC	1	618.185	5
315		6	max	.001	1	.004	2	0	1	2.454e-3	4	NC	1	NC	1
316			min	0	3	-.004	3	-.028	5	-5.621e-6	10	NC	1	698.548	5
317		7	max	.001	1	.004	2	0	1	2.454e-3	4	NC	1	NC	1
318			min	0	3	-.003	3	-.024	5	-5.621e-6	10	NC	1	799.101	5
319		8	max	.001	1	.004	2	0	1	2.454e-3	4	NC	1	NC	1
320			min	0	3	-.003	3	-.021	5	-5.621e-6	10	NC	1	927.262	5
321		9	max	0	1	.003	2	0	1	2.454e-3	4	NC	1	NC	1
322			min	0	3	-.003	3	-.018	5	-5.621e-6	10	NC	1	1094.246	5
323		10	max	0	1	.003	2	0	1	2.454e-3	4	NC	1	NC	1
324			min	0	3	-.002	3	-.015	5	-5.621e-6	10	NC	1	1317.689	5
325		11	max	0	1	.003	2	0	1	2.454e-3	4	NC	1	NC	1
326			min	0	3	-.002	3	-.012	5	-5.621e-6	10	NC	1	1626.627	5
327		12	max	0	1	.002	2	0	1	2.454e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	3	-.002	3	-.009	5	-5.621e-6	10	NC	1	2071.71	5
329		13	max	0	1	.002	2	0	1	2.454e-3	4	NC	1	NC	1
330			min	0	3	-.002	3	-.007	5	-5.621e-6	10	NC	1	2747.933	5
331		14	max	0	1	.002	2	0	1	2.454e-3	4	NC	1	NC	1
332			min	0	3	-.001	3	-.005	5	-5.621e-6	10	NC	1	3851.232	5
333		15	max	0	1	.001	2	0	1	2.454e-3	4	NC	1	NC	1
334			min	0	3	-.001	3	-.003	5	-5.621e-6	10	NC	1	5841.892	5
335		16	max	0	1	.001	2	0	1	2.454e-3	4	NC	1	NC	1
336			min	0	3	0	3	-.002	5	-5.621e-6	10	NC	1	NC	1
337		17	max	0	1	0	2	0	1	2.454e-3	4	NC	1	NC	1
338			min	0	3	0	3	0	5	-5.621e-6	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	2.454e-3	4	NC	1	NC	1
340			min	0	3	0	3	0	5	-5.621e-6	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	2.454e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	-5.621e-6	10	NC	1	NC	1
343	M1	1	max	.005	3	.021	3	.004	5	6.458e-3	1	NC	1	NC	1
344			min	-.005	2	-.018	2	0	9	-8.51e-3	3	NC	1	NC	1
345		2	max	.005	3	.011	3	.006	5	3.161e-3	1	NC	4	NC	1
346			min	-.005	2	-.01	1	-.001	1	-4.179e-3	3	5008.146	3	NC	1
347		3	max	.005	3	.002	3	.008	5	1.654e-4	5	NC	4	NC	1
348			min	-.005	2	-.002	1	-.002	1	-7.585e-5	1	2600.548	3	NC	1
349		4	max	.005	3	.006	2	.011	5	1.576e-4	5	NC	4	NC	1
350			min	-.005	2	-.005	3	-.002	1	-5.902e-5	1	1862.214	3	7268.083	5
351		5	max	.005	3	.012	2	.014	5	1.498e-4	5	NC	4	NC	1
352			min	-.005	2	-.011	3	-.002	1	-4.278e-5	9	1511.964	3	5177.186	5
353		6	max	.005	3	.017	2	.016	5	1.421e-4	5	NC	4	NC	1
354			min	-.005	2	-.016	3	-.002	1	-3.011e-5	9	1292.473	2	3963.78	5
355		7	max	.005	3	.021	2	.019	5	1.343e-4	5	NC	4	NC	1
356			min	-.006	2	-.02	3	-.002	1	-1.745e-5	9	1154.862	2	3182.179	5
357		8	max	.005	3	.024	2	.022	5	1.265e-4	5	NC	5	NC	1
358			min	-.006	2	-.022	3	-.001	1	-4.778e-6	9	1069.143	2	2643.06	5
359		9	max	.005	3	.026	2	.025	5	1.223e-4	4	NC	5	NC	1
360			min	-.006	2	-.023	3	0	1	-9.682e-7	10	1019.076	2	2249.169	4
361		10	max	.005	3	.026	2	.028	4	1.185e-4	4	NC	5	NC	1
362			min	-.006	2	-.024	3	0	9	-1.546e-6	10	996.96	2	1945.74	4
363		11	max	.005	3	.026	2	.032	4	1.147e-4	4	NC	5	NC	1
364			min	-.006	2	-.023	3	0	9	-2.124e-6	10	1000.092	2	1714.048	4
365		12	max	.005	3	.024	2	.035	4	1.108e-4	4	NC	4	NC	1
366			min	-.006	2	-.021	3	0	10	-2.702e-6	10	1029.738	2	1533.282	4
367		13	max	.005	3	.022	2	.038	4	1.07e-4	4	NC	4	NC	1
368			min	-.006	2	-.018	3	0	10	-3.28e-6	10	1091.774	2	1389.895	4
369		14	max	.005	3	.017	2	.041	4	1.092e-4	1	NC	4	NC	1
370			min	-.006	2	-.014	3	0	10	-3.858e-6	10	1199.606	2	1274.742	4
371		15	max	.005	3	.012	2	.044	4	1.26e-4	1	NC	4	NC	1
372			min	-.006	2	-.01	3	0	10	-4.435e-6	10	1382.456	2	1181.471	4
373		16	max	.005	3	.005	2	.047	4	2.502e-4	4	NC	4	NC	1
374			min	-.006	2	-.004	3	0	10	-4.867e-6	10	1711.078	2	1105.559	4
375		17	max	.005	3	.002	3	.049	4	4.081e-3	4	NC	4	NC	1
376			min	-.006	2	-.003	2	0	10	-1.822e-6	10	2405.642	2	1043.786	4
377		18	max	.005	3	.009	3	.051	4	4.258e-3	2	NC	4	NC	1
378			min	-.006	2	-.013	2	0	10	-2.179e-3	3	4647.749	2	993.575	4
379		19	max	.005	3	.016	3	.053	4	8.58e-3	2	NC	1	NC	1
380			min	-.006	2	-.023	2	0	9	-4.441e-3	3	NC	1	954.176	4
381	M5	1	max	.014	3	.066	3	.004	5	9.256e-6	4	NC	1	NC	1
382			min	-.018	2	-.058	1	0	9	0	1	NC	1	NC	1
383		2	max	.014	3	.036	3	.006	5	7.737e-5	5	NC	4	NC	1
384			min	-.018	2	-.03	1	0	9	-1.152e-5	9	1584.62	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.014	3	.008	3	.008	5	1.487e-4	3	NC	5	NC	1
386			min	-.018	2	-.005	1	0	9	-2.285e-5	9	823.15	3	NC	1
387		4	max	.014	3	.018	2	.011	5	1.494e-4	5	NC	5	NC	1
388			min	-.018	2	-.016	3	0	9	-2.141e-5	9	590.018	3	NC	1
389		5	max	.014	3	.038	2	.014	5	1.544e-4	5	NC	5	NC	1
390			min	-.018	2	-.035	3	0	9	-1.998e-5	9	473.919	2	NC	1
391		6	max	.014	3	.054	2	.017	5	1.594e-4	5	NC	5	NC	1
392			min	-.018	2	-.05	3	0	9	-1.855e-5	9	403.759	2	NC	1
393		7	max	.014	3	.067	2	.02	5	1.643e-4	5	NC	5	NC	1
394			min	-.018	2	-.062	3	0	9	-1.712e-5	9	360.644	2	NC	1
395		8	max	.014	3	.077	2	.023	4	1.693e-4	5	NC	5	NC	1
396			min	-.018	2	-.069	3	0	9	-1.568e-5	9	333.776	2	NC	1
397		9	max	.014	3	.083	2	.027	4	1.743e-4	5	NC	5	NC	1
398			min	-.018	2	-.073	3	0	9	-1.425e-5	9	318.07	2	NC	1
399		10	max	.014	3	.085	2	.03	4	1.793e-4	5	NC	5	NC	1
400			min	-.018	2	-.074	3	0	9	-1.282e-5	9	311.112	2	NC	1
401		11	max	.014	3	.084	2	.034	4	1.843e-4	5	NC	5	NC	1
402			min	-.018	2	-.071	3	0	9	-1.139e-5	9	312.051	2	NC	1
403		12	max	.014	3	.078	2	.037	4	1.893e-4	5	NC	5	NC	1
404			min	-.018	2	-.065	3	0	9	-9.956e-6	9	321.281	2	NC	1
405		13	max	.014	3	.069	2	.04	4	1.944e-4	4	NC	5	NC	1
406			min	-.018	2	-.056	3	0	9	-8.524e-6	9	340.636	2	NC	1
407		14	max	.014	3	.056	2	.043	4	2.001e-4	4	NC	5	NC	1
408			min	-.018	2	-.045	3	0	9	-7.092e-6	9	374.302	2	NC	1
409		15	max	.014	3	.038	2	.046	4	2.058e-4	4	NC	5	NC	1
410			min	-.018	2	-.031	3	0	9	-5.66e-6	9	431.411	2	NC	1
411		16	max	.014	3	.017	2	.048	4	3.63e-4	4	NC	5	NC	1
412			min	-.018	2	-.014	3	0	9	-4.954e-6	9	534.081	2	NC	1
413		17	max	.014	3	.005	3	.05	4	4.128e-3	4	NC	5	NC	1
414			min	-.018	2	-.01	2	0	9	-2.153e-5	9	751.246	2	NC	1
415		18	max	.014	3	.027	3	.052	4	2.12e-3	4	NC	4	NC	1
416			min	-.018	2	-.041	2	0	9	-1.105e-5	9	1451.896	2	NC	1
417		19	max	.014	3	.049	3	.053	4	4.11e-6	5	NC	1	NC	1
418			min	-.018	2	-.074	2	0	9	-4.699e-7	3	NC	1	NC	1
419	M9	1	max	.005	3	.021	3	.004	5	8.517e-3	3	NC	1	NC	1
420			min	-.005	2	-.018	2	0	9	-6.458e-3	1	NC	1	NC	1
421		2	max	.005	3	.011	3	.003	4	4.236e-3	3	NC	4	NC	1
422			min	-.005	2	-.01	1	0	10	-3.178e-3	1	5010.706	3	NC	1
423		3	max	.005	3	.002	3	.003	4	4.189e-5	1	NC	4	NC	1
424			min	-.005	2	-.002	1	0	3	-3.487e-5	5	2601.913	3	NC	1
425		4	max	.005	3	.006	2	.004	4	2.668e-5	1	NC	4	NC	1
426			min	-.005	2	-.005	3	-.001	3	-5.05e-5	5	1863.19	3	NC	1
427		5	max	.005	3	.012	2	.005	4	1.366e-5	11	NC	4	NC	1
428			min	-.005	2	-.011	3	-.002	3	-6.677e-5	4	1512.722	3	NC	1
429		6	max	.005	3	.017	2	.007	4	6.152e-6	11	NC	4	NC	1
430			min	-.005	2	-.016	3	-.003	3	-8.541e-5	4	1292.72	2	NC	1
431		7	max	.005	3	.021	2	.01	4	-4.461e-8	10	NC	4	NC	1
432			min	-.005	2	-.02	3	-.003	3	-1.041e-4	4	1155.093	2	7726.235	4
433		8	max	.005	3	.024	2	.012	4	5.25e-7	10	NC	5	NC	1
434			min	-.006	2	-.022	3	-.003	3	-1.227e-4	4	1069.366	2	5309.222	4
435		9	max	.005	3	.026	2	.016	4	1.095e-6	10	NC	5	NC	1
436			min	-.006	2	-.024	3	-.004	3	-1.413e-4	4	1019.297	2	3924.807	4
437		10	max	.005	3	.026	2	.019	4	1.664e-6	10	NC	5	NC	1
438			min	-.006	2	-.024	3	-.004	3	-1.6e-4	4	997.184	2	3053.724	4
439		11	max	.005	3	.026	2	.023	5	2.234e-6	10	NC	5	NC	1
440			min	-.006	2	-.023	3	-.004	3	-1.786e-4	4	1000.323	2	2468.329	4
441		12	max	.005	3	.024	2	.027	5	2.803e-6	10	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.006	2	-.021	3	-.003	3	-1.972e-4	4	1029.983	2	2055.331	4
443		13	max	.005	3	.022	2	.031	5	3.373e-6	10	NC	5	NC	1
444			min	-.006	2	-.018	3	-.003	3	-2.159e-4	4	1092.04	2	1751.493	5
445		14	max	.005	3	.017	2	.035	5	3.943e-6	10	NC	4	NC	1
446			min	-.006	2	-.014	3	-.003	3	-2.345e-4	4	1199.903	2	1522.164	5
447		15	max	.005	3	.012	2	.039	5	4.512e-6	10	NC	4	NC	1
448			min	-.006	2	-.01	3	-.002	3	-2.532e-4	4	1382.801	2	1347.001	5
449		16	max	.005	3	.005	2	.043	5	4.929e-6	10	NC	4	NC	1
450			min	-.006	2	-.004	3	-.002	1	-1.525e-4	1	1711.5	2	1210.814	5
451		17	max	.005	3	.002	3	.046	5	3.982e-3	4	NC	4	NC	1
452			min	-.006	2	-.003	2	-.002	1	-8.454e-5	1	2406.189	2	1101.659	4
453		18	max	.005	3	.009	3	.05	4	2.191e-3	3	NC	4	NC	1
454			min	-.006	2	-.013	2	-.001	1	-4.258e-3	2	4648.77	2	1012.943	4
455		19	max	.005	3	.016	3	.053	4	4.44e-3	3	NC	1	NC	1
456			min	-.006	2	-.023	2	0	9	-8.58e-3	2	NC	1	941.765	4
457	M13	1	max	0	9	.021	3	.005	3	3.639e-3	3	NC	1	NC	1
458			min	-.004	5	-.018	2	-.005	2	-3.25e-3	2	NC	1	NC	1
459		2	max	0	9	.065	3	.003	3	4.517e-3	3	NC	4	NC	1
460			min	-.004	5	-.051	1	-.005	2	-4.043e-3	2	2185.615	3	NC	1
461		3	max	0	9	.101	3	.005	9	5.394e-3	3	NC	4	NC	1
462			min	-.004	5	-.079	1	-.004	2	-4.835e-3	2	1188.895	3	NC	1
463		4	max	0	9	.126	3	.007	9	6.272e-3	3	NC	5	NC	2
464			min	-.004	5	-.099	1	-.005	2	-5.627e-3	2	908.76	3	9870.807	1
465		5	max	0	9	.137	3	.008	9	7.15e-3	3	NC	5	NC	2
466			min	-.004	5	-.107	1	-.006	2	-6.419e-3	2	825.887	3	9469.19	1
467		6	max	0	9	.133	3	.007	9	8.028e-3	3	NC	5	NC	1
468			min	-.004	5	-.105	1	-.008	2	-7.212e-3	2	852.093	3	NC	1
469		7	max	0	9	.118	3	.008	3	8.906e-3	3	NC	5	NC	1
470			min	-.004	5	-.095	1	-.011	2	-8.004e-3	2	984.579	3	NC	1
471		8	max	0	9	.097	3	.01	3	9.784e-3	3	NC	4	NC	1
472			min	-.004	5	-.079	1	-.014	2	-8.796e-3	2	1266.117	3	NC	1
473		9	max	0	9	.076	3	.012	3	1.066e-2	3	NC	4	NC	1
474			min	-.004	5	-.065	1	-.017	2	-9.588e-3	2	1740.443	3	8635.991	2
475		10	max	0	9	.066	3	.014	3	1.154e-2	3	NC	4	NC	1
476			min	-.004	5	-.058	1	-.018	2	-1.038e-2	2	2108.778	3	7819.577	2
477		11	max	0	9	.076	3	.015	3	1.066e-2	3	NC	4	NC	1
478			min	-.004	5	-.065	1	-.017	2	-9.588e-3	2	1740.443	3	8636.033	2
479		12	max	0	9	.097	3	.015	3	9.786e-3	3	NC	4	NC	1
480			min	-.004	5	-.079	1	-.014	2	-8.796e-3	2	1266.116	3	8955.289	3
481		13	max	0	9	.118	3	.015	3	8.909e-3	3	NC	5	NC	1
482			min	-.004	5	-.095	1	-.011	2	-8.004e-3	2	984.579	3	9367.504	3
483		14	max	0	9	.134	3	.014	3	8.032e-3	3	NC	5	NC	1
484			min	-.004	5	-.105	1	-.008	2	-7.212e-3	2	852.093	3	NC	1
485		15	max	0	9	.137	3	.012	3	7.156e-3	3	NC	5	NC	2
486			min	-.004	5	-.107	1	-.006	2	-6.419e-3	2	825.887	3	9470.174	1
487		16	max	0	9	.127	3	.01	3	6.279e-3	3	NC	5	NC	2
488			min	-.004	5	-.099	1	-.005	2	-5.627e-3	2	908.76	3	9877.023	1
489		17	max	0	9	.102	3	.008	3	5.402e-3	3	NC	4	NC	1
490			min	-.004	5	-.079	1	-.004	2	-4.835e-3	2	1188.895	3	NC	1
491		18	max	0	9	.065	3	.006	3	4.525e-3	3	NC	4	NC	1
492			min	-.004	5	-.051	1	-.005	2	-4.043e-3	2	2185.615	3	NC	1
493		19	max	0	9	.021	3	.005	3	3.648e-3	3	NC	1	NC	1
494			min	-.004	5	-.018	2	-.005	2	-3.251e-3	2	NC	1	NC	1
495	M16	1	max	0	9	.016	3	.005	3	3.923e-3	2	NC	1	NC	1
496			min	-.053	4	-.023	2	-.006	2	-2.746e-3	3	NC	1	NC	1
497		2	max	0	9	.039	3	.006	3	4.883e-3	2	NC	4	NC	1
498			min	-.053	4	-.067	2	-.005	2	-3.389e-3	3	2167.302	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	0	9	.058	3	.008	4	5.843e-3	2	NC	5	NC	1
500			min	-.053	4	-.105	2	-.004	2	-4.032e-3	3	1177.026	2	NC	1
501		4	max	0	9	.072	3	.01	3	6.803e-3	2	NC	5	NC	1
502			min	-.053	4	-.13	2	-.005	2	-4.675e-3	3	897.12	2	NC	1
503		5	max	0	9	.079	3	.012	3	7.763e-3	2	NC	5	NC	2
504			min	-.053	4	-.141	2	-.006	2	-5.317e-3	3	811.584	2	9678.73	1
505		6	max	0	9	.078	3	.013	3	8.724e-3	2	NC	5	NC	1
506			min	-.053	4	-.139	2	-.008	2	-5.96e-3	3	831.269	2	NC	1
507		7	max	0	9	.072	3	.014	3	9.684e-3	2	NC	5	NC	1
508			min	-.053	4	-.124	2	-.011	2	-6.603e-3	3	949.21	2	NC	1
509		8	max	0	9	.063	3	.015	3	1.064e-2	2	NC	5	NC	1
510			min	-.053	4	-.103	2	-.014	2	-7.246e-3	3	1196.841	2	9699.877	3
511		9	max	0	9	.054	3	.014	3	1.16e-2	2	NC	4	NC	1
512			min	-.053	4	-.083	2	-.017	2	-7.889e-3	3	1596.753	2	8455.24	2
513		10	max	0	9	.049	3	.014	3	1.256e-2	2	NC	4	NC	3
514			min	-.053	4	-.074	2	-.018	2	-8.532e-3	3	1892.646	2	7667.481	2
515		11	max	0	9	.054	3	.013	3	1.16e-2	2	NC	4	NC	1
516			min	-.053	4	-.083	2	-.017	2	-7.888e-3	3	1596.753	2	8455.269	2
517		12	max	0	9	.063	3	.012	3	1.064e-2	2	NC	5	NC	1
518			min	-.053	4	-.103	2	-.014	2	-7.244e-3	3	1196.841	2	NC	1
519		13	max	0	9	.072	3	.011	3	9.684e-3	2	NC	5	NC	1
520			min	-.053	4	-.124	2	-.011	2	-6.601e-3	3	949.21	2	NC	1
521		14	max	0	9	.078	3	.01	3	8.724e-3	2	NC	5	NC	1
522			min	-.053	4	-.139	2	-.008	2	-5.957e-3	3	831.269	2	NC	1
523		15	max	0	9	.079	3	.009	3	7.764e-3	2	NC	5	NC	2
524			min	-.053	4	-.141	2	-.006	2	-5.313e-3	3	811.584	2	9691.362	1
525		16	max	0	9	.072	3	.007	3	6.804e-3	2	NC	5	NC	1
526			min	-.053	4	-.13	2	-.005	2	-4.669e-3	3	897.12	2	NC	1
527		17	max	0	9	.058	3	.006	3	5.844e-3	2	NC	5	NC	1
528			min	-.053	4	-.105	2	-.004	2	-4.026e-3	3	1177.026	2	NC	1
529		18	max	0	9	.039	3	.005	3	4.884e-3	2	NC	4	NC	1
530			min	-.053	4	-.067	2	-.005	2	-3.382e-3	3	2167.302	2	NC	1
531		19	max	0	9	.016	3	.005	3	3.924e-3	2	NC	1	NC	1
532			min	-.053	4	-.023	2	-.006	2	-2.738e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	3.236e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-4.367e-4	5	NC	1	NC	1
535		2	max	0	3	0	5	.003	4	7.622e-4	3	NC	1	NC	1
536			min	0	4	-.002	1	0	3	-4.771e-4	2	NC	1	NC	1
537		3	max	0	3	0	5	.006	4	1.201e-3	3	NC	1	NC	1
538			min	0	4	-.003	1	-.003	3	-9.1e-4	2	NC	1	8959.174	4
539		4	max	0	3	0	5	.01	4	1.64e-3	3	NC	1	NC	9
540			min	-.001	4	-.005	1	-.006	3	-1.343e-3	2	NC	1	5963.918	4
541		5	max	0	3	.001	5	.012	4	2.078e-3	3	NC	3	NC	9
542			min	-.002	4	-.006	1	-.01	3	-1.776e-3	2	9541.951	2	4280.039	3
543		6	max	0	3	.001	5	.015	4	2.517e-3	3	NC	3	8893.288	9
544			min	-.002	4	-.007	1	-.014	3	-2.209e-3	2	8030.56	2	3098.591	3
545		7	max	0	3	.002	5	.017	4	2.956e-3	3	NC	5	6942.523	9
546			min	-.002	4	-.008	1	-.018	3	-2.641e-3	2	7121.658	2	2412.153	3
547		8	max	0	3	.002	5	.019	1	3.394e-3	3	NC	5	5886.756	15
548			min	-.003	4	-.009	1	-.022	3	-3.074e-3	2	6576.18	2	1982.531	3
549		9	max	0	3	.002	5	.023	1	3.833e-3	3	NC	5	5950.712	15
550			min	-.003	4	-.009	1	-.026	3	-3.507e-3	2	6282.571	2	1702.17	3
551		10	max	0	3	.002	5	.025	1	4.272e-3	3	NC	5	6325.565	15
552			min	-.004	4	-.009	1	-.029	3	-3.94e-3	2	6189.688	2	1517.337	3
553		11	max	0	3	.003	5	.027	1	4.71e-3	3	NC	5	7104.258	15
554			min	-.004	4	-.009	1	-.032	3	-4.373e-3	2	6282.571	2	1399.893	3
555		12	max	0	3	.003	5	.028	1	5.149e-3	3	NC	5	8521.78	15

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.005	4	-.009	1	-.033	3	-4.806e-3	2	6576.18	2	1335.824	3
557		13	max	0	3	.003	5	.028	1	5.587e-3	3	NC	5	NC	15
558			min	-.005	4	-.008	1	-.032	3	-5.239e-3	2	7121.658	2	1320.871	3
559		14	max	0	3	.003	5	.026	1	6.026e-3	3	NC	3	NC	5
560			min	-.005	4	-.007	1	-.03	3	-5.672e-3	2	8030.56	2	1360.533	3
561		15	max	0	3	.003	5	.023	1	6.465e-3	3	NC	3	NC	5
562			min	-.006	4	-.006	1	-.026	3	-6.104e-3	2	9541.951	2	1475.72	3
563		16	max	0	3	.004	5	.017	1	6.903e-3	3	NC	1	NC	4
564			min	-.006	4	-.005	1	-.02	3	-6.537e-3	2	NC	1	1723.524	3
565		17	max	0	3	.004	5	.009	1	7.342e-3	3	NC	1	NC	4
566			min	-.007	4	-.004	9	-.011	3	-6.97e-3	2	NC	1	2283.302	3
567		18	max	0	3	.004	5	.001	9	7.781e-3	3	NC	1	NC	4
568			min	-.007	4	-.003	9	-.005	2	-7.403e-3	2	NC	1	4062.632	3
569		19	max	.001	3	.004	3	.016	3	8.219e-3	3	NC	1	NC	1
570			min	-.007	4	-.001	9	-.018	2	-7.836e-3	2	NC	1	NC	1
571	M16A	1	max	0	2	0	3	.005	3	2.433e-3	3	NC	1	NC	1
572			min	-.002	4	-.002	4	-.006	2	-2.429e-3	2	NC	1	NC	1
573		2	max	0	2	0	12	0	9	2.329e-3	3	NC	1	NC	1
574			min	-.002	4	-.005	4	-.001	2	-2.315e-3	2	NC	1	NC	1
575		3	max	0	2	-.001	12	.004	1	2.224e-3	3	NC	1	NC	4
576			min	-.002	4	-.008	4	-.004	3	-2.2e-3	2	9979.303	4	6413.176	3
577		4	max	0	2	-.002	12	.006	1	2.119e-3	3	NC	1	NC	4
578			min	-.002	4	-.01	4	-.007	3	-2.086e-3	2	6846.385	4	4868.898	3
579		5	max	0	2	-.003	12	.008	1	2.015e-3	3	NC	3	NC	6
580			min	-.002	4	-.012	4	-.01	3	-1.972e-3	2	5342.303	4	4196.295	3
581		6	max	0	2	-.003	12	.009	1	1.91e-3	3	NC	3	NC	9
582			min	-.002	4	-.014	4	-.011	5	-1.858e-3	2	4496.113	4	3898.005	3
583		7	max	0	2	-.004	12	.01	1	1.806e-3	3	NC	12	NC	9
584			min	-.002	4	-.016	4	-.014	5	-1.744e-3	2	3987.241	4	3817.59	3
585		8	max	0	2	-.004	12	.01	1	1.701e-3	3	NC	12	NC	9
586			min	-.001	4	-.017	4	-.016	5	-1.63e-3	2	3681.841	4	3623.805	5
587		9	max	0	2	-.004	12	.009	1	1.597e-3	3	NC	12	NC	9
588			min	-.001	4	-.017	4	-.018	5	-1.515e-3	2	3517.457	4	3216.939	5
589		10	max	0	2	-.004	12	.008	1	1.492e-3	3	NC	12	NC	9
590			min	-.001	4	-.018	4	-.019	5	-1.401e-3	2	3465.454	4	2994.208	5
591		11	max	0	2	-.004	12	.007	1	1.387e-3	3	NC	12	NC	9
592			min	-.001	4	-.017	4	-.02	5	-1.287e-3	2	3517.457	4	2909.465	5
593		12	max	0	2	-.004	12	.006	1	1.283e-3	3	NC	12	NC	9
594			min	0	4	-.016	4	-.02	5	-1.173e-3	2	3681.841	4	2948.184	5
595		13	max	0	2	-.004	12	.004	1	1.178e-3	3	NC	12	NC	2
596			min	0	4	-.015	4	-.018	5	-1.059e-3	2	3987.241	4	3121.46	5
597		14	max	0	2	-.003	12	.003	1	1.074e-3	3	NC	3	NC	1
598			min	0	4	-.013	4	-.017	5	-9.446e-4	2	4496.113	4	3473.208	5
599		15	max	0	2	-.003	12	.002	1	9.691e-4	3	NC	3	NC	1
600			min	0	4	-.011	4	-.014	5	-8.304e-4	2	5342.303	4	4109.655	5
601		16	max	0	2	-.002	12	0	1	8.645e-4	3	NC	1	NC	1
602			min	0	4	-.009	4	-.011	5	-7.163e-4	2	6846.385	4	5295.475	5
603		17	max	0	2	-.002	12	0	9	7.599e-4	3	NC	1	NC	1
604			min	0	4	-.006	4	-.007	5	-6.021e-4	2	9979.303	4	7845.112	5
605		18	max	0	2	0	12	0	9	7.08e-4	4	NC	1	NC	1
606			min	0	4	-.003	4	-.004	5	-4.88e-4	2	NC	1	NC	1
607		19	max	0	1	0	1	0	1	7.653e-4	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-3.738e-4	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

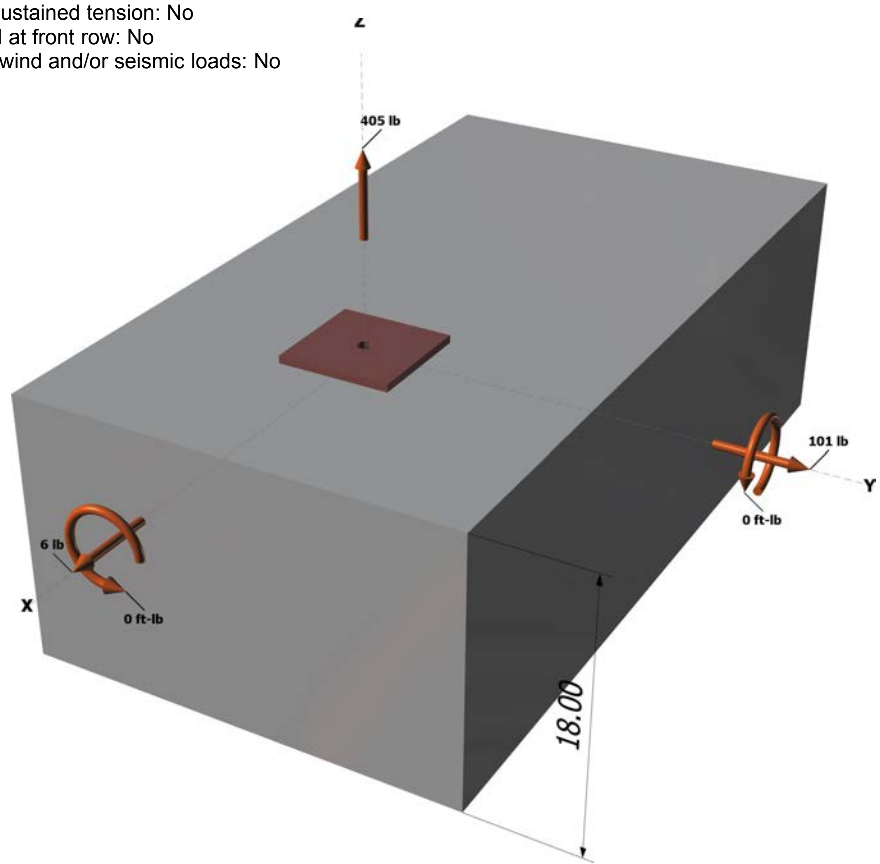
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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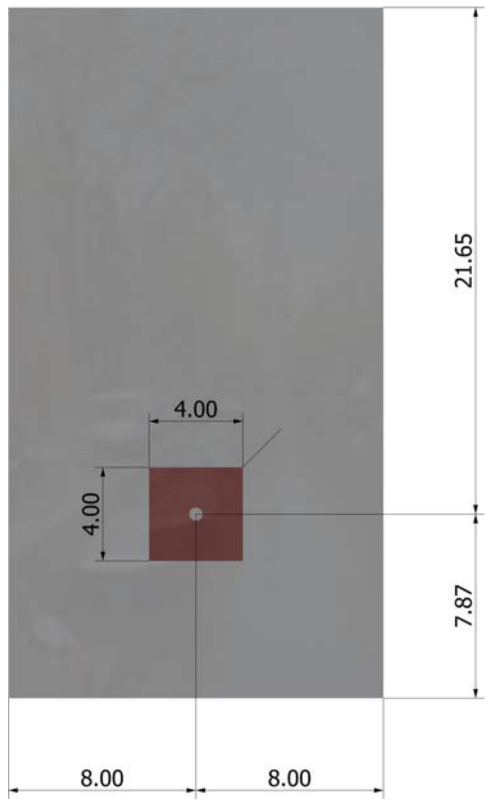


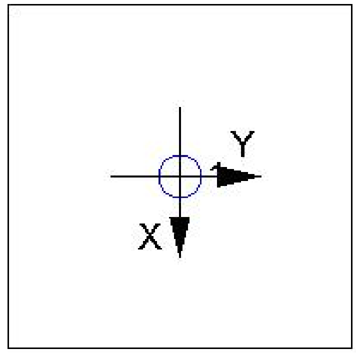
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

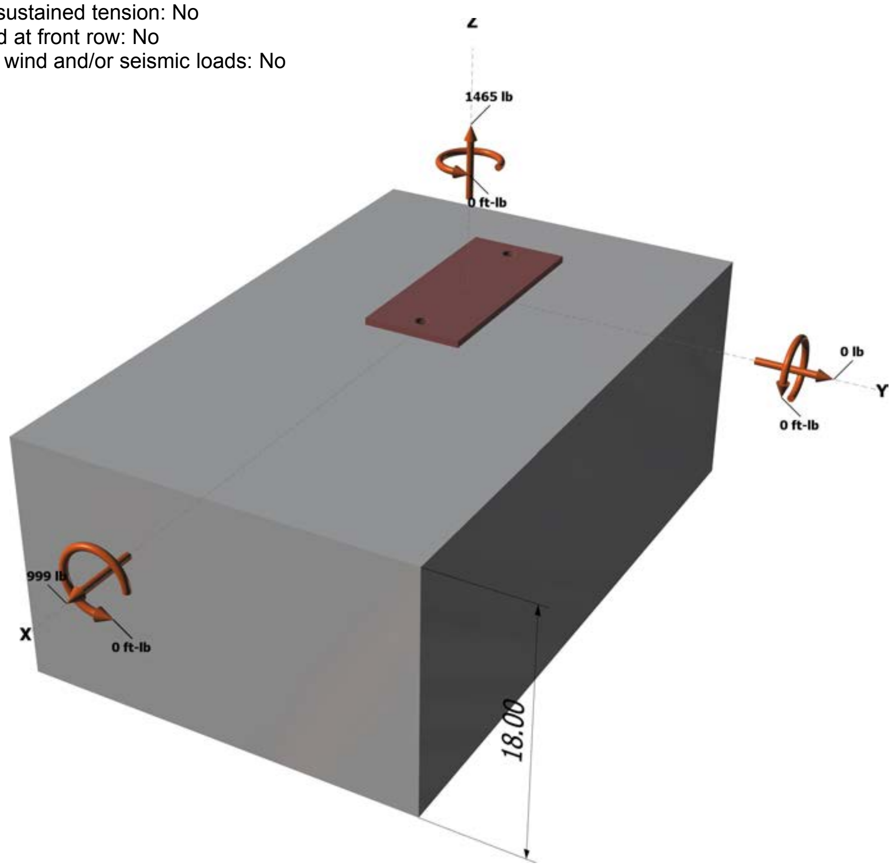
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

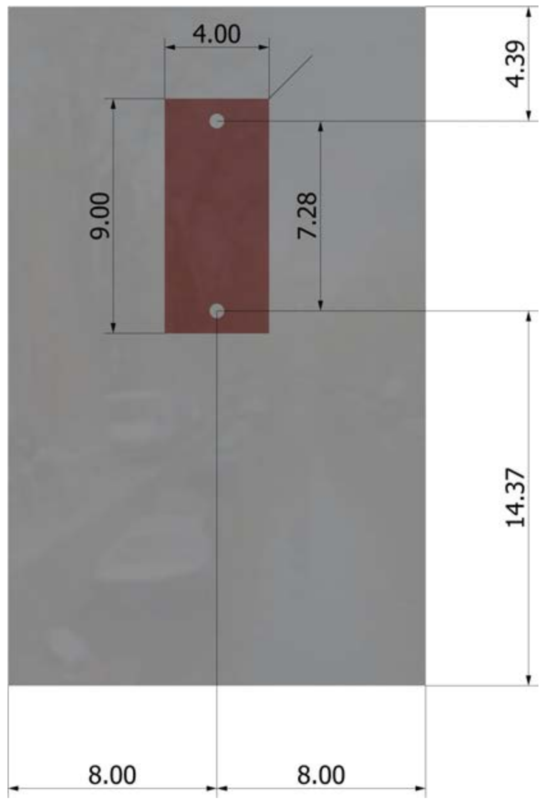
Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



<Figure 2>



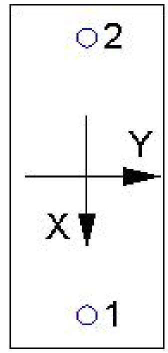
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\,\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\,\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, $øN_n$ (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, $øV_n$ (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer’s product literature for hole cleaning and installation instructions.