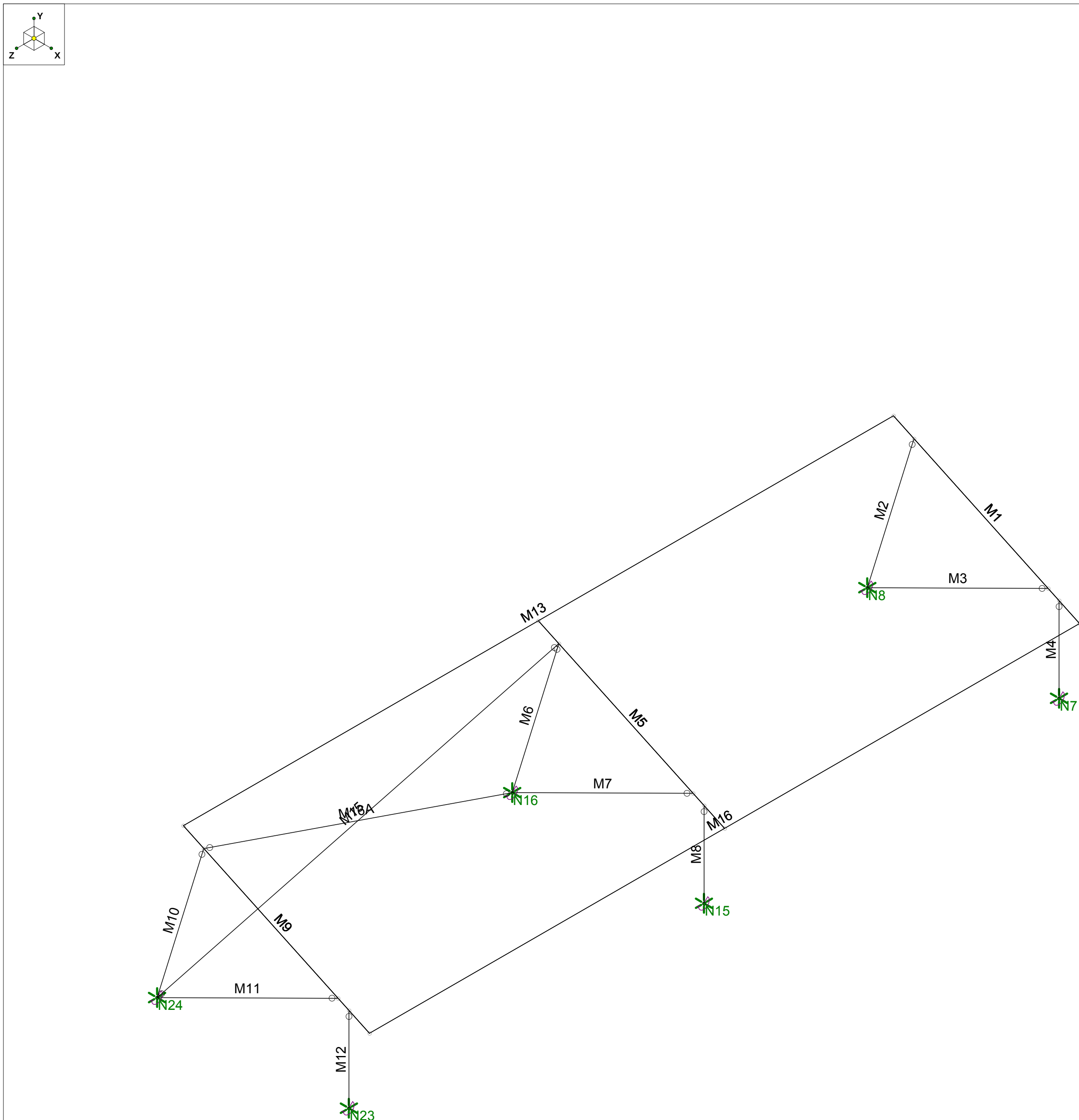


Schletter, Inc.		25° Tilt w/ Seismic Design
HCV	Standard PVMini Racking System	
	Representative Calculations - ASCE 7-10	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. PVMini ground mount system.

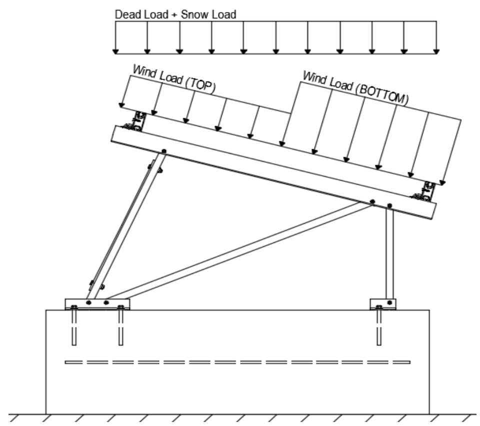
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to aluminum struts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum			Minimum	
Height =	1700	mm	Height =	1550	mm
Width =	1050	mm	Width =	970	mm
Dead Load =	3.00	psf	Dead Load =	1.75	psf

Modules Per Row = 1
Module Tilt = 25°
Maximum Height Above Grade = 3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-10 - Chapter 26-31, Wind Loads
- ASCE 7-10 - Chapter 7, Snow Loads
- ASCE 7-10 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2012, 2015
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} = 3.00 psf

g_{MIN} = 1.75 psf

Self-weight of the PV modules.

2.2 Snow Loads

Ground Snow Load, P_g = 30.00 psf

Sloped Roof Snow Load, P_s = 18.56 psf *(ASCE 7-10, Eq. 7.4-1)*

I_s = 1.00

C_s = 0.82

C_e = 0.90

C_t = 1.20

2.3 Wind Loads

Design Wind Speed, V = 160 mph
Height ≤ 15 ft

Exposure Category = C
Importance Category = II

Peak Velocity Pressure, q_z = 40.19 psf *Including the gust factor, G=0.85. (ASCE 7-10, Eq. 27.3-1)*

Pressure Coefficients

$Cf+_{TOP}$	=	1.1	(Pressure)
$Cf+_{BOTTOM}$	=	1.7	
$Cf-_{TOP}$	=	-2.2	(Suction)
$Cf-_{BOTTOM}$	=	-1	

Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0611-1e. Negative forces are applied away from the surface.

2.4 Seismic Loads

S_S =	2.50	R =	1.25
S_{DS} =	1.67	C_S =	0.8
S_1 =	1.00	ρ =	1.3
S_{D1} =	1.00	Ω =	1.25
T_a =	0.04	C_d =	1.25

ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

<u>Strength Design, LRFD</u>

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.5W
1.2D + 1.0W + 0.5S
0.9D + 1.0W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

<u>Allowable Stress Design, ASD</u>

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 0.6W
1.0D + 0.75L + 0.45W + 0.75S
0.6D + 0.6W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M13	Top
M16	Bottom

Diagonal Struts	Location
M3	Outer
M7	Inner
M11	Outer

Front Reactions	Location
N7	Outer
N15	Inner
N23	Outer

Girders	Location
M1	Outer
M5	Inner
M9	Outer

Rear Struts	Location
M2	Outer
M6	Inner
M10	Outer

Rear Reactions	Location
N8	Outer
N16	Inner
N24	Outer

Front Struts	Location
M4	Outer
M8	Inner
M12	Outer

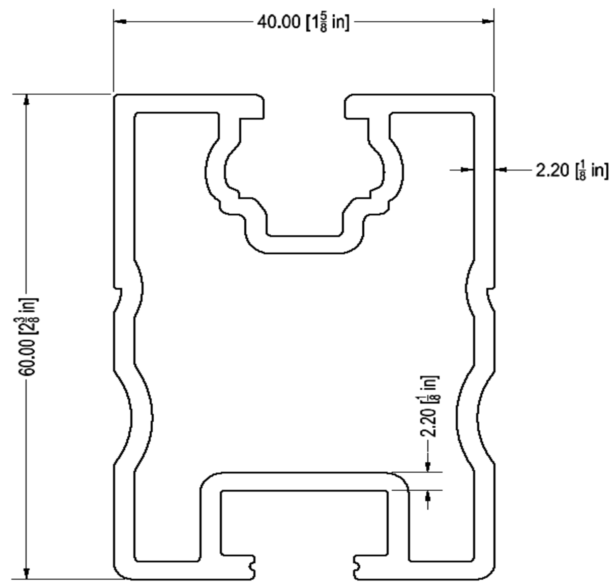
Bracing
M15
M16A

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

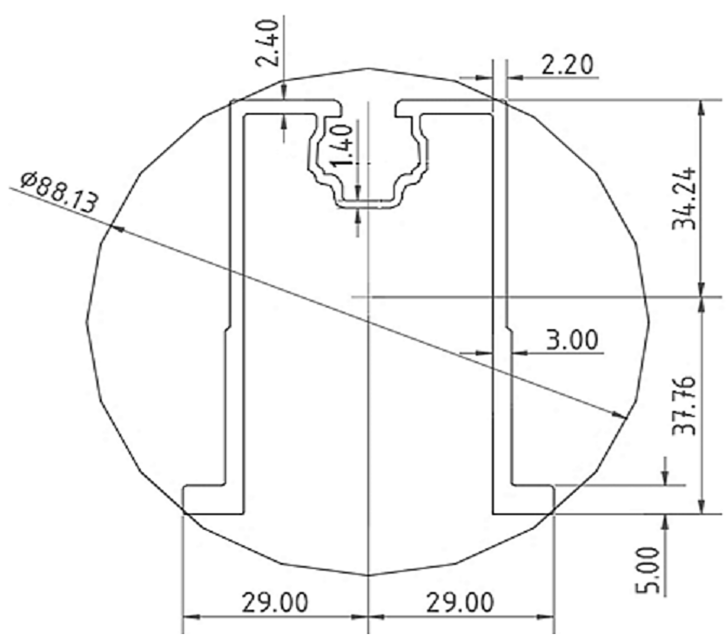
Purlin Type =	**ProfiPlus**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	42	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.99	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	28.47	ksi
S_y =	0.51	in^3
S_x =	0.37	in^3
E =	10100	ksi
I_y =	0.60	in^4
I_x =	0.29	in^4
A =	0.90	in^2
g =	1.08	lbs/ft
M_y =	-0.330	k-ft
M_z =	-0.015	k-ft
$M_{y\ allowable}$ =	1.276	k-ft
$M_{z\ allowable}$ =	0.871	k-ft
Utilization =	28%	



4.2 Girder Design

Loads from purlins are transferred using an inclined girder, which is connected to a set of aluminum struts. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

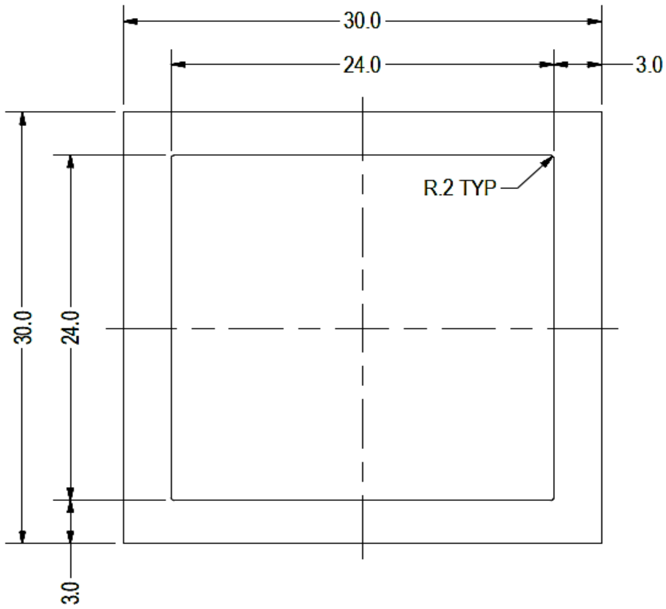
Girder Type =	**Flex Profi**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	33.78	in
$\Phi F_{ty\ AXIAL}$ =	14.29	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	29.73	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	13.46	ksi
S_y =	0.59	in^3
S_x =	0.46	in^3
E =	10100	ksi
I_y =	0.88	in^4
I_x =	0.52	in^4
A =	0.89	in^2
g =	1.07	lbs/ft
M_y =	-0.444	k-ft
M_z =	-0.020	k-ft
P_n =	0.148	k
$M_{y\ allowable}$ =	1.459	k-ft
$M_{z\ allowable}$ =	0.513	k-ft
$P_{n\ allowable}$ =	12.764	k
Utilization =	35%	



4.3 Front Strut Design

The front aluminum strut connects a portion of the girder to the foundation. Vertical girder forces are then transferred down through the strut into the foundation. The strut is attached with single M8 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

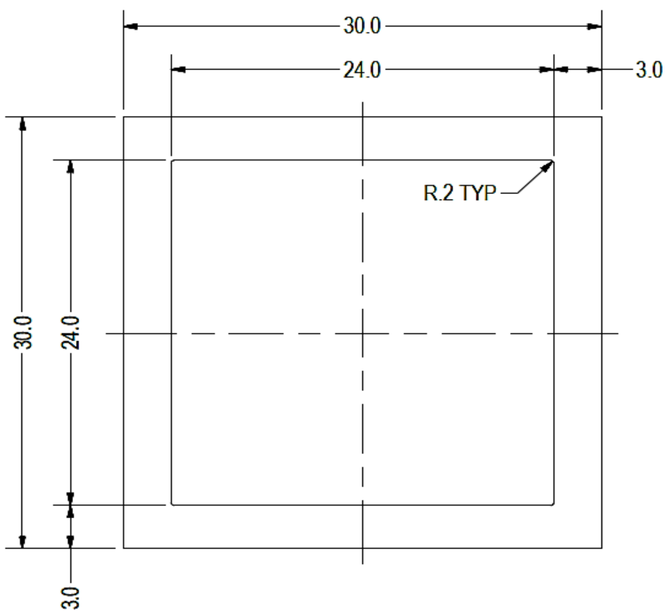
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	18.00	in
$\Phi F_{ty\ AXIAL}$ =	24.52	ksi
$\Phi F_{ty\ BENDING}$ =	31.19	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	-0.023	k-ft
P_n =	0.129	k
$M_{y\ allowable}$ =	0.423	k-ft
$M_{z\ allowable}$ =	0.423	k-ft
$P_{n\ allowable}$ =	12.310	k
Utilization =	6%	



4.4 Diagonal Strut Design

A diagonal aluminum strut braces the support structure. It connects at a front portion of the girder and transfers horizontal forces to the rear foundation connection. The strut is attached with single M8 bolts at each end. See Appendix A.4 for detailed member calculations. Section units are in (mm).

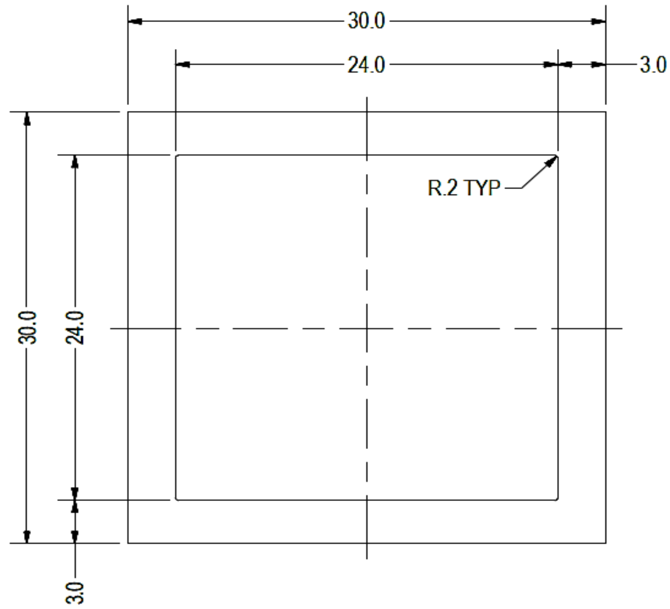
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	46.38	in
$\Phi F_{ty\ AXIAL}$ =	7.60	ksi
$\Phi F_{ty\ BENDING}$ =	29.80	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.426	k
$M_{y\ allowable}$ =	0.404	k-ft
$M_{z\ allowable}$ =	0.404	k-ft
$P_{n\ allowable}$ =	3.814	k
Utilization =	11%	



4.5 Rear Strut Design

An aluminum strut connects the rear portion of the girder to the rear foundation connection. Both vertical and horizontal forces are transferred from the girder. The strut is attached with single M8 bolts at each end. See Appendix A.5 for detailed member calculations. Section units are in (mm).

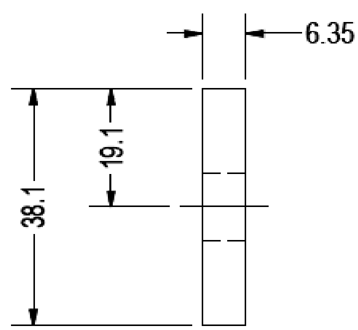
Strut Type =	**30x30x3**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	36.18	in
$\Phi F_{ty\ AXIAL}$ =	11.59	ksi
$\Phi F_{ty\ BENDING}$ =	30.23	ksi
S_y =	0.16	in^3
S_x =	0.16	in^3
E =	10100	ksi
I_y =	0.10	in^4
I_x =	0.10	in^4
A =	0.50	in^2
g =	0.60	lbs/ft
M_y =	0.000	k-ft
M_z =	0.000	k-ft
P_n =	0.613	k
$M_{y\ allowable}$ =	0.410	k-ft
$M_{z\ allowable}$ =	0.410	k-ft
$P_{n\ allowable}$ =	5.820	k
Utilization =	11%	



4.6 Cross Brace Design

In order to resist weak side loading, aluminum cross bracing kits are provided. The cross bracing is attached at one end of a rear aluminum strut diagonally down to the bottom end of an adjacent strut. Single M10 bolts are provided at each of the cross bracing. Section units are in (mm).

Brace Type =	**1.5x0.25**	
Aluminum Type =	6061-T6	
F_{ty} =	35	ksi
Φ =	0.90	
S_y =	0.02	in^3
E =	10100	ksi
I_y =	33.25	in^4
A =	0.38	in^2
g =	0.45	lbs/ft
M_y =	0.002	k-ft
P_n =	0.159	k
$M_{y\ allowable}$ =	0.046	k-ft
$P_{n\ allowable}$ =	11.813	k
Utilization =	6%	



A cross brace kit is required every 34 bays and is to be installed in centermost bays.

5. FOUNDATION DESIGN CALCULATIONS

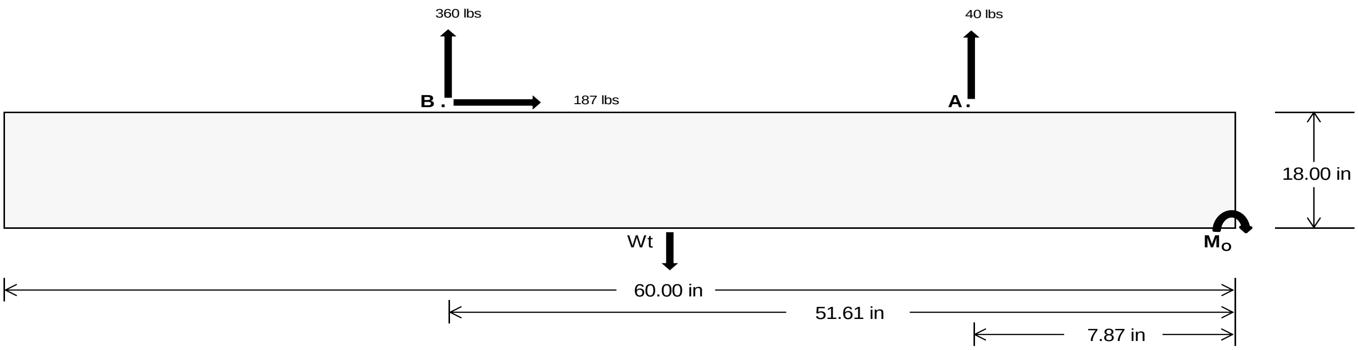
5.1 Helical Pile Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete foundation design.

Maximum	Front	Rear	
Tensile Load =	180.08	1562.90	k
Compressive Load =	994.88	1012.52	k
Lateral Load =	18.85	810.68	k
Moment (Weak Axis) =	0.03	0.00	k

5.2 Design of Ballast Foundations

Ballast foundations are used to secure the racking structure in place. The foundations are checked for potential overturning and sliding. Bearing pressures applied by the racking and ballast foundations are checked against the allowable bearing pressures provided by the IBC table 1806.2 (2012, 2015).



Concrete Properties
Weight of Concrete = 145 pcf
Compressive Strength = 2500 psi
Yield Strength = 60000 psi

Footing Reinforcement
Use fiber reinforcing with (1) #5 rebar.

Overturning Check
M_O = 22267.3 in-lbs
Resisting Force Required = 742.24 lbs
S.F. = 1.67
Weight Required = 1237.07 lbs
Minimum Width = 20 in in
Weight Provided = 1812.50 lbs

A minimum 60in long x 20in wide x 18in tall ballast foundation is required to resist overturning.

Sliding
Force = 187.04 lbs
Friction = 0.4
Weight Required = 467.61 lbs
Resisting Weight = 1812.50 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 20in wide x 18in tall ballast foundation to resist sliding. Friction is OK.

Cohesion
Sliding Force = 187.04 lbs
Cohesion = 130 psf
Area = 8.33 ft^2
Resisting = 906.25 lbs
Additional Weight Required = 0 lbs

Use a 60in long x 20in wide x 18in tall ballast foundation. Cohesion is OK.

Shear Key
Additional Force = 0 lbs
Lateral Bearing Pressure = 200 psf/ft
Required Depth = 0.00 ft
f'_c = 2500 psi
Length = 8 in

Shear key is not required.

Bearing Pressure

	Ballast Width			
	20 in	21 in	22 in	23 in
P_{ftg} = (145 pcf)(5 ft)(1.5 ft)(1.67 ft) =	1813 lbs	1903 lbs	1994 lbs	2084 lbs

ASD LC	1.0D + 1.0S				1.0D + 0.6W				1.0D + 0.75L + 0.45W + 0.75S				0.6D + 0.6W			
Width	20 in	21 in	22 in	23 in	20 in	21 in	22 in	23 in	20 in	21 in	22 in	23 in	20 in	21 in	22 in	23 in
F_A	310 lbs	310 lbs	310 lbs	310 lbs	397 lbs	397 lbs	397 lbs	397 lbs	504 lbs	504 lbs	504 lbs	504 lbs	-81 lbs	-81 lbs	-81 lbs	-81 lbs
F_B	213 lbs	213 lbs	213 lbs	213 lbs	425 lbs	425 lbs	425 lbs	425 lbs	460 lbs	460 lbs	460 lbs	460 lbs	-720 lbs	-720 lbs	-720 lbs	-720 lbs
F_V	21 lbs	21 lbs	21 lbs	21 lbs	331 lbs	331 lbs	331 lbs	331 lbs	263 lbs	263 lbs	263 lbs	263 lbs	-374 lbs	-374 lbs	-374 lbs	-374 lbs
P_{total}	2336 lbs	2427 lbs	2518 lbs	2608 lbs	2634 lbs	2725 lbs	2816 lbs	2906 lbs	2777 lbs	2867 lbs	2958 lbs	3048 lbs	286 lbs	341 lbs	395 lbs	450 lbs
M	220 lbs-ft	220 lbs-ft	220 lbs-ft	220 lbs-ft	462 lbs-ft	462 lbs-ft	462 lbs-ft	462 lbs-ft	495 lbs-ft	495 lbs-ft	495 lbs-ft	495 lbs-ft	586 lbs-ft	586 lbs-ft	586 lbs-ft	586 lbs-ft
e	0.09 ft	0.09 ft	0.09 ft	0.08 ft	0.18 ft	0.17 ft	0.16 ft	0.16 ft	0.18 ft	0.17 ft	0.17 ft	0.16 ft	2.05 ft	1.72 ft	1.48 ft	1.30 ft
L/6	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft	0.83 ft
f_{min}	248.7 psf	247.2 psf	245.8 psf	244.6 psf	249.6 psf	248.1 psf	246.7 psf	245.4 psf	261.9 psf	259.8 psf	257.9 psf	256.1 psf	0.0 psf	0.0 psf	0.0 psf	0.0 psf
f_{max}	312.0 psf	307.5 psf	303.4 psf	299.7 psf	382.6 psf	374.8 psf	367.6 psf	361.1 psf	404.4 psf	395.5 psf	387.4 psf	380.1 psf	252.9 psf	166.6 psf	141.4 psf	130.8 psf

Maximum Bearing Pressure = 404 psf
Allowable Bearing Pressure = 1500 psf

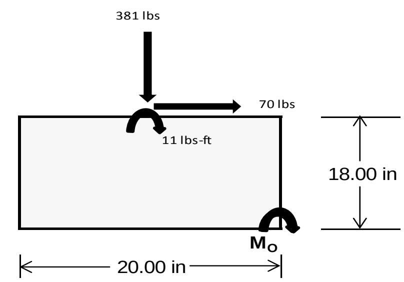
Use a 60in long x 20in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Seismic Design

Overturning Check

M_O =	201.7 ft-lbs
Resisting Force Required =	242.01 lbs
S.F. =	1.67
Weight Required =	403.35 lbs
Minimum Width =	20 in in
Weight Provided =	1812.50 lbs

A minimum 60in long x 20in wide x 18in tall ballast foundation is required to resist overturning.



Bearing Pressure

ASD LC	1.238D + 0.875E			1.1785D + 0.65625E + 0.75S			0.362D + 0.875E		
Width	20 in			20 in			20 in		
Support	Outer	Inner	Outer	Outer	Inner	Outer	Outer	Inner	Outer
F_Y	109 lbs	44 lbs	50 lbs	201 lbs	381 lbs	156 lbs	76 lbs	-35 lbs	18 lbs
F_V	11 lbs	93 lbs	11 lbs	8 lbs	70 lbs	8 lbs	11 lbs	93 lbs	11 lbs
P_{total}	2353 lbs	2288 lbs	2294 lbs	2337 lbs	2517 lbs	2292 lbs	732 lbs	621 lbs	675 lbs
M	31 lbs-ft	154 lbs-ft	32 lbs-ft	22 lbs-ft	116 lbs-ft	25 lbs-ft	31 lbs-ft	154 lbs-ft	32 lbs-ft
e	0.01 ft	0.07 ft	0.01 ft	0.01 ft	0.05 ft	0.01 ft	0.04 ft	0.25 ft	0.05 ft
L/6	0.28 ft	1.53 ft	1.64 ft	1.65 ft	1.57 ft	1.65 ft	1.58 ft	1.17 ft	1.57 ft
f_{min}	269.1 sqft	208.0 sqft	261.6 sqft	270.9 sqft	252.1 sqft	264.3 sqft	74.5 sqft	8.0 sqft	67.3 sqft
f_{max}	295.7 psf	341.1 psf	288.9 psf	290.0 psf	351.9 psf	285.6 psf	101.2 psf	141.1 psf	94.6 psf

Maximum Bearing Pressure = 352 psf
Allowable Bearing Pressure = 1500 psf

Use a 60in long x 20in wide x 18in tall ballast foundation for an acceptable bearing pressure.

Foundation Requirements: 60in long x 20in wide x 18in tall ballast foundation and fiber reinforcing with (1) #5 rebar.

5.3 Foundation Anchors

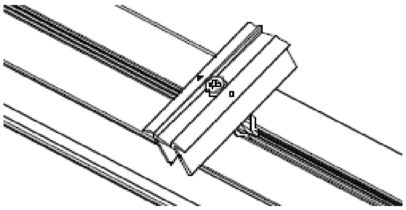
Threaded rods are anchored to the the ballast foundations using the Simpson AT-XP epoxy solution. LRFD load results are compared to the allowable strengths of the epoxy solution. Please see the supplementary calculations provided by the Simpson Anchor Designer software.

6. DESIGN OF JOINTS AND CONNECTIONS

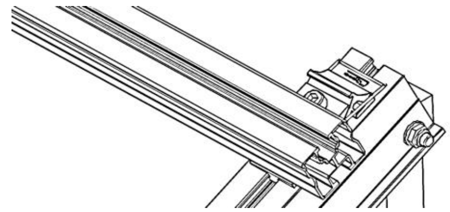
6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of a Schletter, Inc. Klicktop connector. The reliability of calculations is uncertain due to limited standards, therefore the strength of the fasteners has been evaluated by load testing.

Fastening of Modules to Purlins		
Maximum Uplifting Force =	0.834	k
Allowable Uplift =	1.214	k
Utilization =	69%	



Fastening of Purlins to Girders		
Maximum Uplifting Force =	1.044	k
Allowable Uplift =	1.116	k
Utilization =	94%	



6.2 Bolted Connections

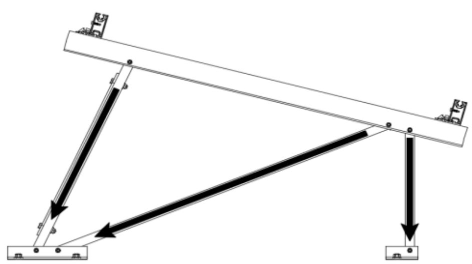
The aluminum struts connect the aluminum girder ends to custom brackets with mounting holes. Cross bracing is attached to rear struts to provide lateral stability. Single M8 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Front Strut		
Maximum Axial Load =	0.765	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	13%	

Rear Strut		
Maximum Axial Load =	1.033	k
M8 Bolt Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	18%	

Diagonal Strut		
Maximum Axial Load =	0.426	k
M8 Bolt Shear Capacity =	5.692	k
Strut Bearing Capacity =	7.952	k
Utilization =	7%	

Bracing		
Maximum Axial Load =	0.159	k
M10 Bolt Capacity =	8.894	k
Strut Bearing Capacity =	7.952	k
Utilization =	2%	



Bolt and bearing capacities are accounting for double shear (ASCE 8-02, Eq. 5.3.4-1). Struts under compression are shown to demonstrate the load transfer from the girder. Single M8 bolts are located at each end of the strut and are subjected to double shear.

7. SEISMIC DESIGN

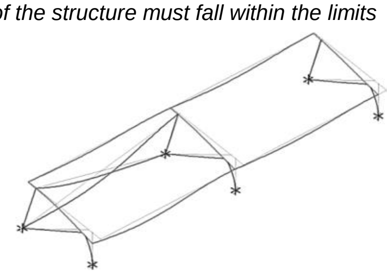
7.1 Seismic Drift

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx} =	30.83	in
Allowable Story Drift for All Other Structures, Δ = {	$0.020h_{sx}$	
	0.617	in
Max Drift, Δ_{MAX} =	0.047	in

0.047 ≤ 0.617, OK.

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **<u>ProfiPlus</u>**

Strong Axis:

3.4.14

L_b = 42.00 in

J = 0.255

109.366

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.0 ksi

3.4.16

b/t = 7.4

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

Weak Axis:

3.4.14

L_b = 42.00 in

J = 0.255

113.57

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.9

3.4.16

b/t = 23.9

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.5 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 23.9

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 30
Cc = 30

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

$\varphi F_L St$= 30.0 ksi
Ix = 250988 mm^4
0.603 in^4
y = 30 mm
Sx = 0.511 in^3
$M_{max}St$ = 1.276 k-ft

3.4.18

h/t = 7.4

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 20
Cc = 20

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

$\varphi F_L Wk$= 28.5 ksi
Iy = 120291 mm^4
0.289 in^4
x = 20 mm
Sy = 0.367 in^3
$M_{max}Wk$ = 0.871 k-ft

Compression

3.4.9

b/t = 7.4
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 23.9
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.5 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 28.47 ksi
A = 578.06 mm^2
0.90 in^2
P_{max} = 25.51 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **Flex Profi**

Strong Axis:
3.4.11

L_b = 33.78 in
ry = 1.374
Cb = 1.30
21.5728

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b} Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2
φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))
φF_L= 29.7 ksi

3.4.15
N/A for Strong Direction

3.4.16
b/t = 4.29

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16
N/A for Strong Direction

Weak Axis:
3.4.11

L_b = 33.78 in
ry = 1.374
Cb = 1.30
24.5845

$$S1 = \frac{1.2(Bc - \frac{\theta_y}{\theta_b} Fcy)}{Dc}$$

S1 = 1.37733

$$S2 = 1.2C_c$$

S2 = 79.2
φF_L= φb[Bc-Dc*Lb/(1.2*ry*√(Cb))
φF_L= 29.7 ksi

3.4.15
b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{5.1Dp}$$

S1 = 3.8

$$S2 = \frac{k_1 Bp}{5.1Dp}$$

S2 = 14.7
F_{UT}= (φbk2*√(BpE))/(5.1b/t)
F_{UT}= 9.4 ksi

3.4.16
N/A for Weak Direction

3.4.16
b/t = 24.46

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
F_{ST}= φb[Bp-1.6Dp*b/t]
F_{ST}= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.16.1

N/A for Weak Direction

3.4.16.2

N/A for Strong Direction

3.4.16.2

b/t = 24.46

t = 2.6

ds = 6.05

rs = 3.49

S = 21.70

ρst = 0.22

F_{UT}= 9.37

F_{ST}= 28.24

φF_L= Fut + (Fst - Fut)ρst < Fst

φF_L= 13.5 ksi

3.4.18

h/t = 24.46

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 34.4

m = 0.70

C_0 = 34.23

Cc = 37.77

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 72.1

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 29.7 ksi

Ix = 364470 mm^4

0.876 in^4

y = 37.77 mm

Sx = 0.589 in^3

M_{max}St = 1.459 k-ft

3.4.18

h/t = 4.29

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 29

Cc = 29

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 13.5 ksi

Iy = 217168 mm^4

0.522 in^4

x = 29 mm

Sy = 0.457 in^3

M_{max}Wk = 0.513 k-ft

Compression

3.4.7

λ = 0.46067

r = 1.374 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.90326

φF_L= φcc(Bc-Dc*λ)

φF_L= 30.1251 ksi

3.4.8

b/t = 24.46
S1 = 3.83
S2 = 10.30
φF_L= (φck2*√(BpE))/(5.1b/t)
φF_L= 10.4 ksi

3.4.9

b/t = 4.29
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L= φyFcy
φF_L= 33.3 ksi

b/t = 24.46
S1 = 12.21
S2 = 32.70
φF_L= φc[Bp-1.6Dp*b/t]
φF_L= 28.2 ksi

3.4.9.1

b/t = 24.46
t = 2.6
ds = 6.05
rs = 3.49
S = 21.70
ρst = 0.22
F_{UT}= 10.43
F_{ST}= 28.24
φF_L= Fut + (Fst - Fut)ρst < Fst
φF_L= 14.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L= φyFcy
φF_L= 33.25 ksi

φF_L= 14.29 ksi
A = 576.21 mm^2
0.89 in^2
P_{max} = 12.76 kips

A.3 Design of Aluminum Struts (Front) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 18.00 in
J = 0.16
47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 31.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0
φF_L= 1.17φyFcy
φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LSt= 31.2 ksi
Ix = 39958.2 mm^4
0.096 in^4
y = 15 mm
Sx = 0.163 in^3
M_{max}St = 0.423 k-ft

Weak Axis:

3.4.14

L_b = 18.00 in
J = 0.16
47.2194

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 31.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LWk= 31.2 ksi
Iy = 39958.2 mm^4
0.096 in^4
x = 15 mm
Sy = 0.163 in^3
M_{max}Wk = 0.423 k-ft

Compression

3.4.7

$\lambda =$ 0.77182

r = 0.437 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^* =$ 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^* =$ 1.23671

$\varphi cc =$ 0.83792

$\varphi F_L = \varphi cc(Bc\text{-}Dc^*\lambda)$

$\varphi F_L =$ 24.5226 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

$\varphi F_L =$ 33.25 ksi

$\varphi F_L =$ 24.52 ksi

A = 323.87 mm^2

0.50 in^2

$P_{max} =$ 12.31 kips

A.4 Design of Aluminum Struts (Diagonal) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:
3.4.14

L_b = 46.38 in
J = 0.16
121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.8 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0
φF_L= 1.17φyFcy
φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LSt= 29.8 ksi
Ix = 39958.2 mm^4
0.096 in^4
y = 15 mm
Sx = 0.163 in^3
M_{max}St = 0.404 k-ft

Weak Axis:
3.4.14

L_b = 46.38 in
J = 0.16
121.663

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L= 29.8

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L= φyFcy
φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9
m = 0.65
C_0 = 15
Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3
φF_L= 1.3φyFcy
φF_L= 43.2 ksi

φF_LWk= 33.3 ksi
Iy = 39958.2 mm^4
0.096 in^4
x = 15 mm
Sy = 0.163 in^3
M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.98863

r = 0.437 in

$$S1^{*} = \frac{Bc - Fcy}{1.6Dc^{*}}$$

$S1^{*}$ = 0.33515

$$S2^{*} = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^{*}$ = 1.23671

φcc = 0.85841

φF_L= (φccFcy)/(λ^2)

φF_L= 7.59722 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 7.60 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 3.81 kips

A.5 Design of Aluminum Struts (Rear) - Aluminum Design Manual, 2005 Edition

Strut = **30x30x3**

Strong Axis:

3.4.14

L_b = 36.18 in

J = 0.16

94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2 ksi

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 30.2 ksi

Ix = 39958.2 mm^4

0.096 in^4

y = 15 mm

Sx = 0.163 in^3

M_{max}St = 0.410 k-ft

Weak Axis:

3.4.14

L_b = 36.18 in

J = 0.16

94.9139

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 30.2

3.4.16

b/t = 7.75

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 7.75

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 15

Cc = 15

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 33.3 ksi

Iy = 39958.2 mm^4

0.096 in^4

x = 15 mm

Sy = 0.163 in^3

M_{max}Wk = 0.450 k-ft

Compression

3.4.7

λ = 1.5514

r = 0.437 in

$$S1^{*} = \frac{Bc - Fcy}{1.6Dc^{*}}$$

$S1^{*}$ = 0.33515

$$S2^{*} = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^{*}$ = 1.23671

φcc = 0.7972

φF_L= (φccFcy)/(λ²)

φF_L= 11.5927 ksi

3.4.9

b/t = 7.75

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 7.75

S1 = 12.21

S2 = 32.70

φF_L= φyFcy

φF_L= 33.3 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φyFcy

φF_L= 33.25 ksi

φF_L= 11.59 ksi

A = 323.87 mm^2

0.50 in^2

P_{max} = 5.82 kips

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				2		
2	Dead Load, Min	DL		-1				2		
3	Snow Load	SL						2		
4	Wind Load - Pressure	WL						2		
5	Wind Load - Suction	WL						2		
6	Seismic - Lateral	EL			.8			4		

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-8.366	-8.366	0	0
2	M16	Y	-8.366	-8.366	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-4.45	-4.45	0	0
2	M16	Y	-4.45	-4.45	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Y	-51.748	-51.748	0	0
2	M16	Y	-51.748	-51.748	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	-123.3	-123.3	0	0
2	M16	y	-190.554	-190.554	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	y	246.6	246.6	0	0
2	M16	y	112.091	112.091	0	0

Member Distributed Loads (BLC 6 : Seismic - Lateral)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	Z	6.693	6.693	0	0
2	M16	Z	6.693	6.693	0	0
3	M13	Z	0	0	0	0
4	M16	Z	0	0	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.5W	Yes	Y		1	1.2	3	1.6	4	.5														
2	LRFD 1.2D + 1.0W + 0.5S	Yes	Y		1	1.2	3	.5	4	1														
3	LRFD 0.9D + 1.0W	Yes	Y		2	.9					5	1												
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3												
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3												
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25												
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25												
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
10	ASD 1.0D + 0.6W	Yes	Y		1	1			4	.6														
11	ASD 1.0D + 0.75L + 0.45W + 0....	Yes	Y		1	1	3	.75	4	.45														
12	ASD 0.6D + 0.6W	Yes	Y		2	.6					5	.6												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65..	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N8	max	185.144	2	256.673	2	.005	10	0	10	0	1	0	1
2		min	-218.361	3	-388.827	3	-2.288	4	0	3	0	1	0	1
3	N7	max	0	4	265.576	1	.047	10	0	10	0	1	0	1
4		min	-.111	2	-29.897	3	-14.165	4	-.022	4	0	1	0	1
5	N15	max	0	15	765.296	2	.072	9	0	9	0	1	0	1
6		min	-1.066	2	-138.525	3	-14.498	5	-.023	4	0	1	0	1
7	N16	max	559.482	2	778.86	2	0	11	0	9	0	1	0	1
8		min	-623.603	3	-1202.232	3	-123.506	4	0	3	0	1	0	1
9	N23	max	0	15	265.88	1	.422	3	0	1	0	1	0	1
10		min	-.111	2	-29.293	3	-13.527	5	-.021	5	0	1	0	1
11	N24	max	185.145	2	258.87	2	84.187	3	0	9	0	1	0	1
12		min	-218.982	3	-388.316	3	-3.201	5	0	3	0	1	0	1
13	Totals:	max	928.483	2	2550.499	2	0	10						
14		min	-1061.126	3	-2177.089	3	-170.845	5						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M2	1	max	198.83	2	.641	6	.963	4	0	10	0	10	0	1
2			min	-348.825	3	.149	15	-.093	3	0	4	0	4	0	1
3		2	max	198.946	2	.596	6	.857	4	0	10	0	5	0	15
4			min	-348.738	3	.139	15	-.093	3	0	4	0	3	0	6
5		3	max	199.063	2	.55	6	.752	4	0	10	0	4	0	15
6			min	-348.65	3	.128	15	-.093	3	0	4	0	3	0	6
7		4	max	199.179	2	.504	6	.646	4	0	10	0	4	0	15
8			min	-348.563	3	.117	15	-.093	3	0	4	0	3	0	6
9		5	max	199.295	2	.459	6	.541	4	0	10	0	4	0	15
10			min	-348.476	3	.106	15	-.093	3	0	4	0	3	0	6
11		6	max	199.412	2	.413	6	.435	4	0	10	0	4	0	15
12			min	-348.389	3	.096	15	-.093	3	0	4	0	3	0	6
13		7	max	199.528	2	.367	6	.33	4	0	10	0	4	0	15
14			min	-348.301	3	.085	15	-.093	3	0	4	0	3	0	6
15		8	max	199.645	2	.322	6	.224	4	0	10	0	4	0	15
16			min	-348.214	3	.074	15	-.093	3	0	4	0	3	0	6
17		9	max	199.761	2	.276	6	.119	4	0	10	0	4	0	15
18			min	-348.127	3	.063	15	-.093	3	0	4	0	3	0	6
19		10	max	199.877	2	.23	6	.068	1	0	10	0	4	0	15
20			min	-348.039	3	.053	15	-.093	3	0	4	0	3	0	6
21		11	max	199.994	2	.185	6	.068	1	0	10	0	4	0	15
22			min	-347.952	3	.042	15	-.114	5	0	4	0	3	0	6
23		12	max	200.11	2	.141	2	.068	1	0	10	0	4	0	15
24			min	-347.865	3	.031	15	-.22	5	0	4	0	3	0	6
25		13	max	200.227	2	.105	2	.068	1	0	10	0	4	0	15
26			min	-347.777	3	.018	12	-.325	5	0	4	0	3	0	6
27		14	max	200.343	2	.07	2	.068	1	0	10	0	4	0	15
28			min	-347.69	3	-.002	3	-.431	5	0	4	0	3	0	6

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
29		15	max	200.459	2	.034	2	.068	1	0	10	0	4	0	15
30			min	-347.603	3	-.029	3	-.536	5	0	4	0	3	0	6
31		16	max	200.576	2	-.002	2	.068	1	0	10	0	4	0	15
32			min	-347.515	3	-.056	3	-.642	5	0	4	0	3	0	6
33		17	max	200.692	2	-.022	15	.068	1	0	10	0	4	0	15
34			min	-347.428	3	-.089	4	-.747	5	0	4	0	3	0	6
35		18	max	200.809	2	-.033	15	.068	1	0	10	0	9	0	15
36			min	-347.341	3	-.135	4	-.853	5	0	4	0	3	0	6
37		19	max	200.925	2	-.044	15	.068	1	0	10	0	9	0	15
38			min	-347.254	3	-.181	4	-.958	5	0	4	0	3	0	6
39	M3	1	max	142.025	2	1.777	6	.01	10	0	5	0	4	0	6
40			min	-129.741	3	.417	15	-1.327	4	0	1	0	10	0	15
41		2	max	141.957	2	1.6	6	.01	10	0	5	0	1	0	2
42			min	-129.793	3	.375	15	-1.194	4	0	1	0	10	0	15
43		3	max	141.888	2	1.422	6	.01	10	0	5	0	1	0	2
44			min	-129.844	3	.333	15	-1.06	4	0	1	0	5	0	3
45		4	max	141.82	2	1.245	6	.01	10	0	5	0	1	0	15
46			min	-129.896	3	.292	15	-.926	4	0	1	0	5	0	4
47		5	max	141.751	2	1.068	6	.01	10	0	5	0	1	0	15
48			min	-129.947	3	.25	15	-.793	4	0	1	0	5	0	4
49		6	max	141.682	2	.891	6	.01	10	0	5	0	1	0	15
50			min	-129.999	3	.208	15	-.659	4	0	1	0	5	0	4
51		7	max	141.614	2	.714	6	.01	10	0	5	0	1	0	15
52			min	-130.05	3	.167	15	-.525	4	0	1	0	5	0	4
53		8	max	141.545	2	.536	6	.01	10	0	5	0	1	0	15
54			min	-130.101	3	.125	15	-.392	4	0	1	0	5	-.001	4
55		9	max	141.477	2	.359	6	.01	10	0	5	0	1	0	15
56			min	-130.153	3	.083	15	-.258	4	0	1	0	5	-.001	4
57		10	max	141.408	2	.182	6	.01	10	0	5	0	1	0	15
58			min	-130.204	3	.042	15	-.125	4	0	1	0	5	-.001	4
59		11	max	141.339	2	.029	2	.034	5	0	5	0	1	0	15
60			min	-130.256	3	-.021	3	-.103	1	0	1	0	5	-.001	4
61		12	max	141.271	2	-.042	15	.168	5	0	5	0	1	0	15
62			min	-130.307	3	-.173	4	-.103	1	0	1	0	5	-.001	4
63		13	max	141.202	2	-.083	15	.301	5	0	5	0	1	0	15
64			min	-130.359	3	-.35	4	-.103	1	0	1	0	5	-.001	4
65		14	max	141.133	2	-.125	15	.435	5	0	5	0	9	0	15
66			min	-130.41	3	-.527	4	-.103	1	0	1	0	5	-.001	4
67		15	max	141.065	2	-.167	15	.569	5	0	5	0	9	0	15
68			min	-130.462	3	-.704	4	-.103	1	0	1	0	5	0	4
69		16	max	140.996	2	-.208	15	.702	5	0	5	0	10	0	15
70			min	-130.513	3	-.881	4	-.103	1	0	1	0	4	0	4
71		17	max	140.928	2	-.25	15	.836	5	0	5	0	10	0	15
72			min	-130.565	3	-1.059	4	-.103	1	0	1	0	4	0	4
73		18	max	140.859	2	-.292	15	.969	5	0	5	0	10	0	15
74			min	-130.616	3	-1.236	4	-.103	1	0	1	0	4	0	4
75		19	max	140.79	2	-.333	15	1.103	5	0	5	0	5	0	1
76			min	-130.667	3	-1.413	4	-.103	1	0	1	0	1	0	1
77	M4	1	max	264.412	1	0	1	.048	10	0	1	0	5	0	1
78			min	-30.771	3	0	1	-13.31	4	0	1	0	2	0	1
79		2	max	264.476	1	0	1	.048	10	0	1	0	10	0	1
80			min	-30.722	3	0	1	-13.366	4	0	1	-.001	4	0	1
81		3	max	264.541	1	0	1	.048	10	0	1	0	10	0	1
82			min	-30.674	3	0	1	-13.422	4	0	1	-.002	4	0	1
83		4	max	264.606	1	0	1	.048	10	0	1	0	10	0	1
84			min	-30.625	3	0	1	-13.478	4	0	1	-.004	4	0	1
85		5	max	264.67	1	0	1	.048	10	0	1	0	10	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
86			min	-30.577	3	0	1	-13.534	4	0	1	-.005	4	0	1
87		6	max	264.735	1	0	1	.048	10	0	1	0	10	0	1
88			min	-30.528	3	0	1	-13.59	4	0	1	-.006	4	0	1
89		7	max	264.8	1	0	1	.048	10	0	1	0	10	0	1
90			min	-30.48	3	0	1	-13.646	4	0	1	-.007	4	0	1
91		8	max	264.865	1	0	1	.048	10	0	1	0	10	0	1
92			min	-30.431	3	0	1	-13.703	4	0	1	-.008	4	0	1
93		9	max	264.929	1	0	1	.048	10	0	1	0	10	0	1
94			min	-30.383	3	0	1	-13.759	4	0	1	-.01	4	0	1
95		10	max	264.994	1	0	1	.048	10	0	1	0	10	0	1
96			min	-30.334	3	0	1	-13.815	4	0	1	-.011	4	0	1
97		11	max	265.059	1	0	1	.048	10	0	1	0	10	0	1
98			min	-30.285	3	0	1	-13.871	4	0	1	-.012	4	0	1
99		12	max	265.123	1	0	1	.048	10	0	1	0	10	0	1
100			min	-30.237	3	0	1	-13.927	4	0	1	-.013	4	0	1
101		13	max	265.188	1	0	1	.048	10	0	1	0	10	0	1
102			min	-30.188	3	0	1	-13.983	4	0	1	-.015	4	0	1
103		14	max	265.253	1	0	1	.048	10	0	1	0	10	0	1
104			min	-30.14	3	0	1	-14.039	4	0	1	-.016	4	0	1
105		15	max	265.317	1	0	1	.048	10	0	1	0	10	0	1
106			min	-30.091	3	0	1	-14.095	4	0	1	-.017	4	0	1
107		16	max	265.382	1	0	1	.048	10	0	1	0	10	0	1
108			min	-30.043	3	0	1	-14.151	4	0	1	-.018	4	0	1
109		17	max	265.447	1	0	1	.048	10	0	1	0	10	0	1
110			min	-29.994	3	0	1	-14.207	4	0	1	-.02	4	0	1
111		18	max	265.512	1	0	1	.048	10	0	1	0	10	0	1
112			min	-29.946	3	0	1	-14.263	4	0	1	-.021	4	0	1
113		19	max	265.576	1	0	1	.048	10	0	1	0	10	0	1
114			min	-29.897	3	0	1	-14.319	4	0	1	-.022	4	0	1
115	M6	1	max	611.16	2	.628	6	.928	4	0	3	0	3	0	1
116			min	-1033.428	3	.141	15	-.296	3	0	5	0	1	0	1
117		2	max	611.277	2	.582	6	.822	4	0	3	0	3	0	15
118			min	-1033.34	3	.13	15	-.296	3	0	5	0	1	0	6
119		3	max	611.393	2	.536	6	.717	4	0	3	0	4	0	15
120			min	-1033.253	3	.119	15	-.296	3	0	5	0	1	0	6
121		4	max	611.509	2	.491	6	.611	4	0	3	0	4	0	15
122			min	-1033.166	3	.108	15	-.296	3	0	5	0	1	0	6
123		5	max	611.626	2	.445	6	.506	4	0	3	0	4	0	15
124			min	-1033.078	3	.098	15	-.296	3	0	5	0	1	0	6
125		6	max	611.742	2	.409	2	.4	4	0	3	0	4	0	15
126			min	-1032.991	3	.087	15	-.296	3	0	5	0	1	0	6
127		7	max	611.859	2	.373	2	.295	4	0	3	0	4	0	15
128			min	-1032.904	3	.076	15	-.296	3	0	5	0	3	0	6
129		8	max	611.975	2	.338	2	.19	4	0	3	0	4	0	15
130			min	-1032.817	3	.066	15	-.296	3	0	5	0	3	0	6
131		9	max	612.091	2	.302	2	.084	4	0	3	0	4	0	15
132			min	-1032.729	3	.053	12	-.296	3	0	5	0	3	0	6
133		10	max	612.208	2	.267	2	.013	9	0	3	0	4	0	15
134			min	-1032.642	3	.035	12	-.296	3	0	5	0	3	0	2
135		11	max	612.324	2	.231	2	.013	9	0	3	0	4	0	15
136			min	-1032.555	3	.017	3	-.296	3	0	5	0	3	0	2
137		12	max	612.441	2	.195	2	.013	9	0	3	0	4	0	15
138			min	-1032.467	3	-.01	3	-.296	3	0	5	0	3	0	2
139		13	max	612.557	2	.16	2	.013	9	0	3	0	4	0	15
140			min	-1032.38	3	-.037	3	-.343	5	0	5	0	3	0	2
141		14	max	612.673	2	.124	2	.013	9	0	3	0	4	0	15
142			min	-1032.293	3	-.063	3	-.449	5	0	5	0	3	0	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
143		15	max	612.79	2	.089	2	.013	9	0	3	0	4	0	15
144			min	-1032.205	3	-.09	3	-.554	5	0	5	0	3	0	2
145		16	max	612.906	2	.053	2	.013	9	0	3	0	4	0	15
146			min	-1032.118	3	-.117	3	-.66	5	0	5	0	3	0	2
147		17	max	613.023	2	.018	2	.013	9	0	3	0	4	0	12
148			min	-1032.031	3	-.143	3	-.765	5	0	5	0	3	0	2
149		18	max	613.139	2	-.018	2	.013	9	0	3	0	4	0	12
150			min	-1031.944	3	-.17	3	-.871	5	0	5	0	3	0	2
151		19	max	613.255	2	-.053	15	.013	9	0	3	0	9	0	12
152			min	-1031.856	3	-.197	3	-.976	5	0	5	0	3	0	2
153	M7	1	max	425.879	2	1.792	4	.026	3	0	9	0	4	0	2
154			min	-334.694	3	.427	15	-1.347	4	0	3	0	3	0	12
155		2	max	425.81	2	1.615	4	.026	3	0	9	0	4	0	2
156			min	-334.746	3	.385	15	-1.213	4	0	3	0	3	0	3
157		3	max	425.741	2	1.437	4	.026	3	0	9	0	9	0	2
158			min	-334.797	3	.343	15	-1.08	4	0	3	0	3	0	3
159		4	max	425.673	2	1.26	4	.026	3	0	9	0	9	0	2
160			min	-334.849	3	.302	15	-.946	4	0	3	0	3	0	3
161		5	max	425.604	2	1.083	4	.026	3	0	9	0	9	0	15
162			min	-334.9	3	.26	15	-.812	4	0	3	0	5	0	3
163		6	max	425.536	2	.906	4	.026	3	0	9	0	9	0	15
164			min	-334.952	3	.218	15	-.679	4	0	3	0	5	0	6
165		7	max	425.467	2	.729	4	.026	3	0	9	0	9	0	15
166			min	-335.003	3	.177	15	-.545	4	0	3	0	5	0	6
167		8	max	425.398	2	.551	4	.026	3	0	9	0	9	0	15
168			min	-335.055	3	.135	15	-.411	4	0	3	0	5	0	6
169		9	max	425.33	2	.374	4	.026	3	0	9	0	9	0	15
170			min	-335.106	3	.093	15	-.278	4	0	3	0	5	-.001	6
171		10	max	425.261	2	.211	2	.026	3	0	9	0	9	0	15
172			min	-335.158	3	.032	12	-.144	4	0	3	0	5	-.001	6
173		11	max	425.193	2	.072	2	.026	3	0	9	0	9	0	15
174			min	-335.209	3	-.063	3	-.011	4	0	3	0	5	-.001	6
175		12	max	425.124	2	-.032	15	.125	5	0	9	0	9	0	15
176			min	-335.26	3	-.167	3	-.003	9	0	3	0	5	-.001	6
177		13	max	425.055	2	-.073	15	.258	5	0	9	0	9	0	15
178			min	-335.312	3	-.335	6	-.003	9	0	3	0	5	-.001	6
179		14	max	424.987	2	-.115	15	.392	5	0	9	0	9	0	15
180			min	-335.363	3	-.512	6	-.003	9	0	3	0	5	-.001	6
181		15	max	424.918	2	-.157	15	.525	5	0	9	0	9	0	15
182			min	-335.415	3	-.689	6	-.003	9	0	3	0	5	0	6
183		16	max	424.85	2	-.198	15	.659	5	0	9	0	9	0	15
184			min	-335.466	3	-.867	6	-.003	9	0	3	0	5	0	6
185		17	max	424.781	2	-.24	15	.793	5	0	9	0	9	0	15
186			min	-335.518	3	-1.044	6	-.003	9	0	3	0	5	0	6
187		18	max	424.712	2	-.282	15	.926	5	0	9	0	9	0	15
188			min	-335.569	3	-1.221	6	-.003	9	0	3	0	3	0	6
189		19	max	424.644	2	-.323	15	1.06	5	0	9	0	9	0	1
190			min	-335.621	3	-1.398	6	-.003	9	0	3	0	3	0	1
191	M8	1	max	764.131	2	0	1	.076	9	0	1	0	4	0	1
192			min	-139.399	3	0	1	-13.594	4	0	1	0	3	0	1
193		2	max	764.196	2	0	1	.076	9	0	1	0	9	0	1
194			min	-139.35	3	0	1	-13.65	4	0	1	-.001	4	0	1
195		3	max	764.261	2	0	1	.076	9	0	1	0	9	0	1
196			min	-139.302	3	0	1	-13.707	4	0	1	-.002	4	0	1
197		4	max	764.325	2	0	1	.076	9	0	1	0	9	0	1
198			min	-139.253	3	0	1	-13.763	4	0	1	-.004	4	0	1
199		5	max	764.39	2	0	1	.076	9	0	1	0	9	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
200			min	-139.205	3	0	1	-13.819	4	0	1	-.005	4	0	1
201		6	max	764.455	2	0	1	.076	9	0	1	0	9	0	1
202			min	-139.156	3	0	1	-13.875	4	0	1	-.006	4	0	1
203		7	max	764.519	2	0	1	.076	9	0	1	0	9	0	1
204			min	-139.108	3	0	1	-13.931	4	0	1	-.007	4	0	1
205		8	max	764.584	2	0	1	.076	9	0	1	0	9	0	1
206			min	-139.059	3	0	1	-13.987	4	0	1	-.009	4	0	1
207		9	max	764.649	2	0	1	.076	9	0	1	0	9	0	1
208			min	-139.011	3	0	1	-14.043	4	0	1	-.01	4	0	1
209		10	max	764.714	2	0	1	.076	9	0	1	0	9	0	1
210			min	-138.962	3	0	1	-14.099	4	0	1	-.011	4	0	1
211		11	max	764.778	2	0	1	.076	9	0	1	0	9	0	1
212			min	-138.914	3	0	1	-14.155	4	0	1	-.012	4	0	1
213		12	max	764.843	2	0	1	.076	9	0	1	0	9	0	1
214			min	-138.865	3	0	1	-14.211	4	0	1	-.014	4	0	1
215		13	max	764.908	2	0	1	.076	9	0	1	0	9	0	1
216			min	-138.816	3	0	1	-14.267	4	0	1	-.015	4	0	1
217		14	max	764.972	2	0	1	.076	9	0	1	0	9	0	1
218			min	-138.768	3	0	1	-14.323	4	0	1	-.016	4	0	1
219		15	max	765.037	2	0	1	.076	9	0	1	0	9	0	1
220			min	-138.719	3	0	1	-14.379	4	0	1	-.018	4	0	1
221		16	max	765.102	2	0	1	.076	9	0	1	0	9	0	1
222			min	-138.671	3	0	1	-14.436	4	0	1	-.019	4	0	1
223		17	max	765.167	2	0	1	.076	9	0	1	0	9	0	1
224			min	-138.622	3	0	1	-14.492	4	0	1	-.02	4	0	1
225		18	max	765.231	2	0	1	.076	9	0	1	0	9	0	1
226			min	-138.574	3	0	1	-14.548	4	0	1	-.021	4	0	1
227		19	max	765.296	2	0	1	.076	9	0	1	0	9	0	1
228			min	-138.525	3	0	1	-14.604	4	0	1	-.023	4	0	1
229	M10	1	max	199.996	2	.673	4	1.028	5	0	1	0	9	0	1
230			min	-275.945	3	.171	15	-.069	1	-.001	5	0	3	0	1
231		2	max	200.113	2	.628	4	.923	5	0	1	0	4	0	15
232			min	-275.857	3	.16	15	-.069	1	-.001	5	0	3	0	4
233		3	max	200.229	2	.582	4	.817	5	0	1	0	4	0	15
234			min	-275.77	3	.149	15	-.069	1	-.001	5	0	3	0	4
235		4	max	200.346	2	.536	4	.712	5	0	1	0	4	0	15
236			min	-275.683	3	.139	15	-.069	1	-.001	5	0	3	0	4
237		5	max	200.462	2	.491	4	.606	5	0	1	0	4	0	15
238			min	-275.596	3	.128	15	-.069	1	-.001	5	0	3	0	4
239		6	max	200.578	2	.445	4	.501	5	0	1	0	4	0	15
240			min	-275.508	3	.117	15	-.069	1	-.001	5	0	3	0	4
241		7	max	200.695	2	.399	4	.395	5	0	1	0	5	0	15
242			min	-275.421	3	.107	15	-.069	1	-.001	5	0	3	0	4
243		8	max	200.811	2	.354	4	.29	5	0	1	0	5	0	15
244			min	-275.334	3	.096	15	-.069	1	-.001	5	0	3	0	4
245		9	max	200.928	2	.308	4	.184	5	0	1	0	5	0	15
246			min	-275.246	3	.085	15	-.069	1	-.001	5	0	3	0	4
247		10	max	201.044	2	.262	4	.079	5	0	1	0	5	0	15
248			min	-275.159	3	.074	15	-.069	1	-.001	5	0	3	0	4
249		11	max	201.16	2	.217	4	.005	10	0	1	0	5	0	15
250			min	-275.072	3	.061	12	-.069	1	-.001	5	0	3	0	4
251		12	max	201.277	2	.171	4	.005	10	0	1	0	5	0	15
252			min	-274.984	3	.044	12	-.145	4	-.001	5	0	3	0	4
253		13	max	201.393	2	.125	4	.005	10	0	1	0	5	0	15
254			min	-274.897	3	.026	12	-.25	4	-.001	5	0	3	0	4
255		14	max	201.51	2	.08	4	.005	10	0	1	0	5	0	15
256			min	-274.81	3	.008	12	-.356	4	-.001	5	0	3	0	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
257		15	max	201.626	2	.034	4	.005	10	0	1	0	5	0	15
258			min	-274.723	3	-.017	3	-.461	4	-.001	5	0	3	0	4
259		16	max	201.742	2	.014	5	.005	10	0	1	0	5	0	15
260			min	-274.635	3	-.043	3	-.567	4	-.001	5	0	3	0	4
261		17	max	201.859	2	0	15	.005	10	0	1	0	5	0	15
262			min	-274.548	3	-.07	3	-.672	4	-.001	5	0	3	0	4
263		18	max	201.975	2	-.012	15	.005	10	0	1	0	5	0	15
264			min	-274.461	3	-.104	6	-.778	4	-.001	5	0	3	0	4
265		19	max	202.092	2	-.022	15	.005	10	0	1	0	5	0	15
266			min	-274.373	3	-.15	6	-.883	4	-.001	5	0	3	0	4
267	M11	1	max	141.645	2	1.77	6	.103	1	0	4	0	5	0	6
268			min	-130.577	3	.412	15	-1.269	5	0	10	0	1	0	15
269		2	max	141.577	2	1.593	6	.103	1	0	4	0	3	0	2
270			min	-130.629	3	.37	15	-1.135	5	0	10	0	1	0	15
271		3	max	141.508	2	1.416	6	.103	1	0	4	0	3	0	2
272			min	-130.68	3	.328	15	-1.001	5	0	10	0	1	0	3
273		4	max	141.439	2	1.238	6	.103	1	0	4	0	3	0	15
274			min	-130.732	3	.287	15	-.868	5	0	10	0	1	0	4
275		5	max	141.371	2	1.061	6	.103	1	0	4	0	3	0	15
276			min	-130.783	3	.245	15	-.734	5	0	10	0	1	0	4
277		6	max	141.302	2	.884	6	.103	1	0	4	0	3	0	15
278			min	-130.835	3	.203	15	-.601	5	0	10	0	4	0	4
279		7	max	141.234	2	.707	6	.103	1	0	4	0	3	0	15
280			min	-130.886	3	.162	15	-.467	5	0	10	0	4	0	4
281		8	max	141.165	2	.53	6	.103	1	0	4	0	3	0	15
282			min	-130.937	3	.12	15	-.333	5	0	10	0	4	-.001	4
283		9	max	141.096	2	.352	6	.103	1	0	4	0	3	0	15
284			min	-130.989	3	.078	15	-.2	5	0	10	0	4	-.001	4
285		10	max	141.028	2	.175	6	.103	1	0	4	0	3	0	15
286			min	-131.04	3	.037	15	-.066	5	0	10	0	4	-.001	4
287		11	max	140.959	2	.029	2	.103	1	0	4	0	3	0	15
288			min	-131.092	3	-.026	3	-.047	3	0	10	0	4	-.001	4
289		12	max	140.891	2	-.046	15	.227	4	0	4	0	3	0	15
290			min	-131.143	3	-.18	4	-.047	3	0	10	0	4	-.001	4
291		13	max	140.822	2	-.088	15	.361	4	0	4	0	3	0	15
292			min	-131.195	3	-.357	4	-.047	3	0	10	0	4	-.001	4
293		14	max	140.753	2	-.13	15	.494	4	0	4	0	3	0	15
294			min	-131.246	3	-.534	4	-.047	3	0	10	0	4	-.001	4
295		15	max	140.685	2	-.171	15	.628	4	0	4	0	3	0	15
296			min	-131.298	3	-.711	4	-.047	3	0	10	0	5	0	4
297		16	max	140.616	2	-.213	15	.762	4	0	4	0	3	0	15
298			min	-131.349	3	-.888	4	-.047	3	0	10	0	5	0	4
299		17	max	140.548	2	-.255	15	.895	4	0	4	0	3	0	15
300			min	-131.401	3	-1.066	4	-.047	3	0	10	0	10	0	4
301		18	max	140.479	2	-.296	15	1.029	4	0	4	0	3	0	15
302			min	-131.452	3	-1.243	4	-.047	3	0	10	0	10	0	4
303		19	max	140.41	2	-.338	15	1.162	4	0	4	0	4	0	1
304			min	-131.503	3	-1.42	4	-.047	3	0	10	0	10	0	1
305	M12	1	max	264.715	1	0	1	.425	1	0	1	0	4	0	1
306			min	-30.166	3	0	1	-12.518	5	0	1	0	3	0	1
307		2	max	264.78	1	0	1	.425	1	0	1	0	1	0	1
308			min	-30.118	3	0	1	-12.574	5	0	1	-.001	5	0	1
309		3	max	264.844	1	0	1	.425	1	0	1	0	1	0	1
310			min	-30.069	3	0	1	-12.63	5	0	1	-.002	5	0	1
311		4	max	264.909	1	0	1	.425	1	0	1	0	1	0	1
312			min	-30.02	3	0	1	-12.686	5	0	1	-.003	5	0	1
313		5	max	264.974	1	0	1	.425	1	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
314			min	-29.972	3	0	1	-12.742	5	0	1	-.005	5	0	1
315		6	max	265.038	1	0	1	.425	1	0	1	0	1	0	1
316			min	-29.923	3	0	1	-12.798	5	0	1	-.006	5	0	1
317		7	max	265.103	1	0	1	.425	1	0	1	0	1	0	1
318			min	-29.875	3	0	1	-12.854	5	0	1	-.007	5	0	1
319		8	max	265.168	1	0	1	.425	1	0	1	0	1	0	1
320			min	-29.826	3	0	1	-12.91	5	0	1	-.008	5	0	1
321		9	max	265.233	1	0	1	.425	1	0	1	0	1	0	1
322			min	-29.778	3	0	1	-12.967	5	0	1	-.009	5	0	1
323		10	max	265.297	1	0	1	.425	1	0	1	0	1	0	1
324			min	-29.729	3	0	1	-13.023	5	0	1	-.01	5	0	1
325		11	max	265.362	1	0	1	.425	1	0	1	0	1	0	1
326			min	-29.681	3	0	1	-13.079	5	0	1	-.011	5	0	1
327		12	max	265.427	1	0	1	.425	1	0	1	0	1	0	1
328			min	-29.632	3	0	1	-13.135	5	0	1	-.013	5	0	1
329		13	max	265.491	1	0	1	.425	1	0	1	0	1	0	1
330			min	-29.584	3	0	1	-13.191	5	0	1	-.014	5	0	1
331		14	max	265.556	1	0	1	.425	1	0	1	0	1	0	1
332			min	-29.535	3	0	1	-13.247	5	0	1	-.015	5	0	1
333		15	max	265.621	1	0	1	.425	1	0	1	0	1	0	1
334			min	-29.487	3	0	1	-13.303	5	0	1	-.016	5	0	1
335		16	max	265.685	1	0	1	.425	1	0	1	0	1	0	1
336			min	-29.438	3	0	1	-13.359	5	0	1	-.017	5	0	1
337		17	max	265.75	1	0	1	.425	1	0	1	0	1	0	1
338			min	-29.39	3	0	1	-13.415	5	0	1	-.019	5	0	1
339		18	max	265.815	1	0	1	.425	1	0	1	0	1	0	1
340			min	-29.341	3	0	1	-13.471	5	0	1	-.02	5	0	1
341		19	max	265.88	1	0	1	.425	1	0	1	0	1	0	1
342			min	-29.293	3	0	1	-13.527	5	0	1	-.021	5	0	1
343	M1	1	max	60.701	1	329.487	3	1.123	10	0	2	.025	4	0	2
344			min	3.26	10	-215.909	2	-14.518	4	0	3	-.002	10	0	3
345		2	max	60.819	1	329.297	3	1.123	10	0	2	.022	4	.047	2
346			min	3.358	10	-216.162	2	-14.276	4	0	3	-.002	10	-.072	3
347		3	max	60.171	3	4.53	4	1.119	10	0	5	.019	4	.093	2
348			min	-10.502	10	-19.391	2	-13.071	4	0	1	-.002	10	-.142	3
349		4	max	60.26	3	4.205	4	1.119	10	0	5	.016	4	.098	2
350			min	-10.404	10	-19.644	2	-12.829	4	0	1	-.001	10	-.138	3
351		5	max	60.348	3	3.881	4	1.119	10	0	5	.013	4	.102	2
352			min	-10.306	10	-19.897	2	-12.587	4	0	1	-.001	10	-.135	3
353		6	max	60.437	3	3.556	4	1.119	10	0	5	.01	4	.106	2
354			min	-10.207	10	-20.15	2	-12.345	4	0	1	0	10	-.131	3
355		7	max	60.525	3	3.294	14	1.119	10	0	5	.008	4	.111	2
356			min	-10.109	10	-20.403	2	-12.103	4	0	1	0	10	-.127	3
357		8	max	60.614	3	3.045	14	1.119	10	0	5	.005	4	.115	2
358			min	-10.011	10	-20.656	2	-11.861	4	0	1	0	10	-.124	3
359		9	max	60.702	3	2.797	14	1.119	10	0	5	.003	3	.119	2
360			min	-9.912	10	-20.909	2	-11.619	4	0	1	0	10	-.12	3
361		10	max	60.791	3	2.548	14	1.119	10	0	5	.002	3	.124	2
362			min	-9.814	10	-21.162	2	-11.445	1	0	1	0	10	-.116	3
363		11	max	60.879	3	2.299	14	1.119	10	0	5	0	3	.129	2
364			min	-9.716	10	-21.415	2	-11.445	1	0	1	-.002	1	-.112	3
365		12	max	60.968	3	2.051	14	1.119	10	0	5	0	10	.133	2
366			min	-9.617	10	-21.669	2	-11.445	1	0	1	-.005	1	-.108	3
367		13	max	61.056	3	1.802	14	1.119	10	0	5	0	10	.138	2
368			min	-9.519	10	-21.922	2	-11.445	1	0	1	-.007	1	-.104	3
369		14	max	61.145	3	1.553	14	1.119	10	0	5	0	10	.143	2
370			min	-9.421	10	-22.175	2	-11.445	1	0	1	-.01	1	-.1	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
371		15	max	61.233	3	1.305	14	1.119	10	0	5	.001	10	.148	2
372			min	-9.322	10	-22.428	2	-11.445	1	0	1	-.012	1	-.096	3
373		16	max	83.049	2	86.985	2	1.128	10	0	1	.001	10	.152	2
374			min	-19.514	3	-121.408	3	-11.539	1	0	5	-.015	1	-.091	3
375		17	max	83.167	2	86.732	2	1.128	10	0	1	.002	10	.133	2
376			min	-19.426	3	-121.598	3	-11.539	1	0	5	-.017	1	-.065	3
377		18	max	-3.359	10	307.312	2	1.176	10	0	5	.002	10	.067	2
378			min	-60.797	1	-149.711	3	-21.511	4	0	2	-.02	4	-.033	3
379		19	max	-3.261	10	307.059	2	1.176	10	0	5	.002	10	0	2
380			min	-60.679	1	-149.901	3	-21.269	4	0	2	-.025	4	0	3
381	M5	1	max	157.062	1	1035.758	3	0	1	0	9	.027	4	0	3
382			min	-6.635	3	-668.111	2	-75.797	3	0	3	0	11	0	2
383		2	max	157.18	1	1035.568	3	0	1	0	9	.023	4	.144	2
384			min	-6.546	3	-668.364	2	-75.797	3	0	3	-.005	3	-.224	3
385		3	max	147.742	3	4.994	9	8.021	3	0	3	.019	4	.287	2
386			min	-21.654	10	-63.844	2	-15.093	4	0	4	-.02	3	-.444	3
387		4	max	147.831	3	4.783	9	8.021	3	0	3	.016	4	.301	2
388			min	-21.556	10	-64.097	2	-14.851	4	0	4	-.019	3	-.43	3
389		5	max	147.919	3	4.572	9	8.021	3	0	3	.013	4	.315	2
390			min	-21.458	10	-64.35	2	-14.609	4	0	4	-.017	3	-.417	3
391		6	max	148.008	3	4.361	9	8.021	3	0	3	.01	4	.329	2
392			min	-21.359	10	-64.603	2	-14.367	4	0	4	-.015	3	-.404	3
393		7	max	148.096	3	4.15	9	8.021	3	0	3	.007	4	.343	2
394			min	-21.261	10	-64.856	2	-14.125	4	0	4	-.013	3	-.39	3
395		8	max	148.185	3	3.939	9	8.021	3	0	3	.003	4	.357	2
396			min	-21.163	10	-65.109	2	-13.883	4	0	4	-.012	3	-.377	3
397		9	max	148.273	3	3.728	9	8.021	3	0	3	0	4	.371	2
398			min	-21.064	10	-65.362	2	-13.641	4	0	4	-.01	3	-.364	3
399		10	max	148.362	3	3.517	9	8.021	3	0	3	0	1	.385	2
400			min	-20.966	10	-65.616	2	-13.399	4	0	4	-.008	3	-.35	3
401		11	max	148.45	3	3.307	9	8.021	3	0	3	0	1	.399	2
402			min	-20.868	10	-65.869	2	-13.157	4	0	4	-.006	3	-.337	3
403		12	max	148.539	3	3.096	9	8.021	3	0	3	0	1	.414	2
404			min	-20.769	10	-66.122	2	-12.915	4	0	4	-.008	4	-.323	3
405		13	max	148.627	3	2.885	9	8.021	3	0	3	0	1	.428	2
406			min	-20.671	10	-66.375	2	-12.673	4	0	4	-.011	4	-.31	3
407		14	max	148.716	3	2.674	9	8.021	3	0	3	0	1	.443	2
408			min	-20.573	10	-66.628	2	-12.431	4	0	4	-.014	4	-.296	3
409		15	max	148.804	3	2.463	9	8.021	3	0	3	0	3	.457	2
410			min	-20.474	10	-66.881	2	-12.189	4	0	4	-.016	4	-.282	3
411		16	max	253.183	2	266.778	2	7.995	3	0	3	.002	3	.469	2
412			min	-59.825	3	-325.831	3	-10.893	4	0	4	-.019	4	-.266	3
413		17	max	253.301	2	266.525	2	7.995	3	0	3	.003	3	.411	2
414			min	-59.737	3	-326.021	3	-10.651	4	0	4	-.021	4	-.196	3
415		18	max	-.877	3	955.085	2	7.381	3	0	4	.005	3	.206	2
416			min	-157.224	1	-453.048	3	-23.769	5	0	9	-.026	4	-.098	3
417		19	max	-.788	3	954.831	2	7.381	3	0	4	.007	3	0	3
418			min	-157.106	1	-453.238	3	-23.527	5	0	9	-.032	4	0	2
419	M9	1	max	60.701	1	329.399	3	100.845	4	0	3	.002	10	0	2
420			min	.282	15	-215.909	2	-1.123	10	0	2	-.023	1	0	3
421		2	max	60.819	1	329.209	3	101.087	4	0	3	.021	5	.047	2
422			min	.318	15	-216.162	2	-1.123	10	0	2	-.02	1	-.072	3
423		3	max	59.525	3	3.816	9	11.445	1	0	1	.041	5	.093	2
424			min	-10.198	10	-19.368	2	-19.398	5	0	10	-.017	1	-.142	3
425		4	max	59.613	3	3.605	9	11.445	1	0	1	.037	5	.098	2
426			min	-10.1	10	-19.622	2	-19.156	5	0	10	-.015	1	-.138	3
427		5	max	59.702	3	3.394	9	11.445	1	0	1	.033	5	.102	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
428			min	-10.001	10	-19.875	2	-18.914	5	0	10	-.012	1	-.134	3
429		6	max	59.79	3	3.184	9	11.445	1	0	1	.029	5	.106	2
430			min	-9.903	10	-20.128	2	-18.672	5	0	10	-.01	1	-.131	3
431		7	max	59.879	3	2.973	9	11.445	1	0	1	.024	5	.111	2
432			min	-9.805	10	-20.381	2	-18.43	5	0	10	-.008	1	-.127	3
433		8	max	59.967	3	2.762	9	11.445	1	0	1	.021	5	.115	2
434			min	-9.706	10	-20.634	2	-18.188	5	0	10	-.005	1	-.124	3
435		9	max	60.056	3	2.551	9	11.445	1	0	1	.017	5	.119	2
436			min	-9.608	10	-20.887	2	-17.946	5	0	10	-.003	1	-.12	3
437		10	max	60.144	3	2.34	9	11.445	1	0	1	.013	4	.124	2
438			min	-9.51	10	-21.14	2	-17.704	5	0	10	0	1	-.116	3
439		11	max	60.233	3	2.129	9	11.445	1	0	1	.01	3	.129	2
440			min	-9.411	10	-21.393	2	-17.462	5	0	10	0	10	-.112	3
441		12	max	60.321	3	1.918	9	11.445	1	0	1	.009	3	.133	2
442			min	-9.313	10	-21.646	2	-17.22	5	0	10	0	10	-.108	3
443		13	max	60.41	3	1.707	9	11.445	1	0	1	.009	3	.138	2
444			min	-9.215	10	-21.899	2	-16.978	5	0	10	0	10	-.104	3
445		14	max	60.498	3	1.496	9	11.445	1	0	1	.01	1	.143	2
446			min	-9.116	10	-22.152	2	-16.736	5	0	10	-.002	5	-.1	3
447		15	max	60.587	3	1.285	9	11.445	1	0	1	.012	1	.148	2
448			min	-9.018	10	-22.405	2	-16.494	5	0	10	-.006	5	-.096	3
449		16	max	83.177	2	86.711	2	11.539	1	0	10	.015	1	.152	2
450			min	-20.678	3	-121.947	3	-15.116	5	0	4	-.009	5	-.092	3
451		17	max	83.295	2	86.458	2	11.539	1	0	10	.017	1	.133	2
452			min	-20.59	3	-122.136	3	-14.874	5	0	4	-.012	5	-.065	3
453		18	max	8.599	5	307.312	2	11.967	1	0	2	.02	1	.067	2
454			min	-60.797	1	-149.701	3	-27.149	5	0	3	-.018	5	-.033	3
455		19	max	8.654	5	307.059	2	11.967	1	0	2	.023	1	0	2
456			min	-60.679	1	-149.89	3	-26.907	5	0	3	-.024	5	0	3
457	M13	1	max	100.844	4	215.849	2	-.282	15	0	2	.023	1	0	2
458			min	-1.123	10	-329.452	3	-60.698	1	0	3	-.002	10	0	3
459		2	max	97.025	4	154.785	2	.314	5	0	2	.015	3	.11	3
460			min	-1.123	10	-235.305	3	-45.228	1	0	3	-.004	2	-.072	2
461		3	max	93.205	4	93.722	2	1.183	5	0	2	.012	3	.183	3
462			min	-1.123	10	-141.158	3	-29.758	1	0	3	-.013	1	-.12	2
463		4	max	89.386	4	32.658	2	2.052	5	0	2	.009	3	.22	3
464			min	-1.123	10	-47.012	3	-14.287	1	0	3	-.021	1	-.145	2
465		5	max	85.566	4	47.135	3	4.603	2	0	2	.006	3	.22	3
466			min	-1.123	10	-28.405	2	-6.945	3	0	3	-.024	1	-.146	2
467		6	max	81.746	4	141.281	3	16.653	1	0	2	.003	5	.183	3
468			min	-1.123	10	-89.469	2	-6.127	3	0	3	-.02	1	-.123	2
469		7	max	80.188	3	235.428	3	32.123	1	0	2	.005	5	.11	3
470			min	-1.123	10	-150.532	2	-5.31	3	0	3	-.011	1	-.076	2
471		8	max	80.188	3	329.575	3	47.594	1	0	2	.007	4	0	5
472			min	-1.123	10	-211.596	2	-4.492	3	0	3	0	3	-.006	2
473		9	max	80.188	3	423.721	3	63.064	1	0	2	.026	1	.088	2
474			min	-1.123	10	-272.659	2	-3.674	3	0	3	-.002	3	-.147	3
475		10	max	80.188	3	-6.687	15	78.534	1	0	2	.054	1	.206	2
476			min	-1.123	10	-517.868	3	2.017	12	0	3	-.015	3	-.33	3
477		11	max	45.059	4	272.659	2	6.822	5	0	3	.026	1	.088	2
478			min	-1.123	10	-423.721	3	-63.064	1	0	2	-.014	3	-.147	3
479		12	max	41.239	4	211.596	2	7.691	5	0	3	.007	2	0	5
480			min	-1.123	10	-329.574	3	-47.593	1	0	2	-.012	3	-.006	2
481		13	max	37.42	4	150.532	2	8.56	5	0	3	.001	10	.11	3
482			min	-1.123	10	-235.428	3	-32.123	1	0	2	-.011	1	-.076	2
483		14	max	33.6	4	89.469	2	9.429	5	0	3	-.001	10	.183	3
484			min	-1.123	10	-141.281	3	-16.653	1	0	2	-.02	1	-.123	2

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
485		15	max	29.781	4	28.405	2	10.66	4	0	3	0	5	.22	3
486			min	-1.123	10	-47.135	3	-4.603	2	0	2	-.024	1	-.146	2
487		16	max	25.961	4	47.012	3	14.752	4	0	3	.005	5	.22	3
488			min	-1.123	10	-32.658	2	-1.396	10	0	2	-.021	1	-.145	2
489		17	max	22.141	4	141.159	3	29.758	1	0	3	.01	5	.183	3
490			min	-1.123	10	-93.722	2	.156	10	0	2	-.013	1	-.12	2
491		18	max	18.322	4	235.305	3	45.228	1	0	3	.016	4	.11	3
492			min	-1.123	10	-154.785	2	1.708	10	0	2	-.004	2	-.072	2
493		19	max	14.502	4	329.452	3	60.698	1	0	3	.025	4	0	2
494			min	-1.123	10	-215.849	2	3.26	10	0	2	-.002	10	0	3
495	M16	1	max	26.897	5	307.133	2	8.654	5	0	3	.023	1	0	2
496			min	-11.951	1	-149.914	3	-60.682	1	0	2	-.024	5	0	3
497		2	max	23.078	5	219.915	2	9.523	5	0	3	.003	9	.05	3
498			min	-11.951	1	-108.077	3	-45.212	1	0	2	-.02	5	-.102	2
499		3	max	19.258	5	132.697	2	10.393	5	0	3	0	3	.084	3
500			min	-11.951	1	-66.239	3	-29.742	1	0	2	-.018	4	-.171	2
501		4	max	15.439	5	45.479	2	11.262	5	0	3	-.001	12	.102	3
502			min	-11.951	1	-24.401	3	-14.272	1	0	2	-.021	1	-.206	2
503		5	max	11.619	5	17.436	3	12.131	5	0	3	-.002	12	.103	3
504			min	-11.951	1	-41.739	2	-4.405	3	0	2	-.024	1	-.206	2
505		6	max	7.8	5	59.274	3	16.669	1	0	3	-.001	10	.088	3
506			min	-11.951	1	-128.956	2	-3.587	3	0	2	-.02	1	-.173	2
507		7	max	3.98	5	101.111	3	32.139	1	0	3	.003	5	.057	3
508			min	-11.951	1	-216.174	2	-2.769	3	0	2	-.011	1	-.106	2
509		8	max	2.489	3	142.949	3	47.61	1	0	3	.009	4	.009	3
510			min	-11.951	1	-303.392	2	-1.952	3	0	2	-.008	3	-.005	2
511		9	max	2.489	3	184.786	3	63.08	1	0	3	.026	1	.13	2
512			min	-11.951	1	-390.61	2	-1.134	3	0	2	-.008	3	-.054	3
513		10	max	16.054	5	-6.575	15	78.55	1	0	14	.054	1	.299	2
514			min	-11.951	1	-477.828	2	-1.105	3	0	2	-.008	3	-.134	3
515		11	max	12.235	5	390.61	2	5.587	5	0	2	.026	1	.13	2
516			min	-11.951	1	-184.786	3	-63.08	1	0	3	-.009	5	-.054	3
517		12	max	8.415	5	303.392	2	6.456	5	0	2	.007	2	.009	3
518			min	-11.951	1	-142.949	3	-47.609	1	0	3	-.007	5	-.005	2
519		13	max	4.596	5	216.174	2	7.325	5	0	2	.001	10	.057	3
520			min	-11.951	1	-101.111	3	-32.139	1	0	3	-.011	1	-.106	2
521		14	max	1.176	10	128.956	2	8.195	5	0	2	0	15	.088	3
522			min	-11.951	1	-59.274	3	-16.669	1	0	3	-.02	1	-.173	2
523		15	max	1.176	10	41.739	2	9.403	4	0	2	.002	5	.103	3
524			min	-11.951	1	-17.436	3	-4.607	2	0	3	-.024	1	-.206	2
525		16	max	1.176	10	24.402	3	14.272	1	0	2	.006	5	.102	3
526			min	-11.951	1	-45.479	2	-1.396	10	0	3	-.021	1	-.206	2
527		17	max	1.176	10	66.239	3	29.742	1	0	2	.01	5	.084	3
528			min	-13.647	4	-132.697	2	.156	10	0	3	-.013	1	-.171	2
529		18	max	1.176	10	108.077	3	45.212	1	0	2	.016	4	.05	3
530			min	-17.466	4	-219.915	2	1.708	10	0	3	-.004	2	-.102	2
531		19	max	1.176	10	149.914	3	60.683	1	0	2	.025	4	0	2
532			min	-21.286	4	-307.133	2	3.26	10	0	3	-.002	10	0	5
533	M15	1	max	0	1	.731	3	.163	3	0	1	0	1	0	1
534			min	-110.834	3	0	1	0	1	0	3	0	3	0	1
535		2	max	0	1	.65	3	.163	3	0	1	0	1	0	1
536			min	-110.899	3	0	1	0	1	0	3	0	3	0	3
537		3	max	0	1	.569	3	.163	3	0	1	0	1	0	1
538			min	-110.964	3	0	1	0	1	0	3	0	3	0	3
539		4	max	0	1	.487	3	.163	3	0	1	0	1	0	1
540			min	-111.029	3	0	1	0	1	0	3	0	3	0	3
541		5	max	0	1	.406	3	.163	3	0	1	0	1	0	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
542			min	-111.094	3	0	1	0	1	0	3	0	3	0	3
543		6	max	0	1	.325	3	.163	3	0	1	0	1	0	1
544			min	-111.16	3	0	1	0	1	0	3	0	3	0	3
545		7	max	0	1	.244	3	.163	3	0	1	0	3	0	1
546			min	-111.225	3	0	1	0	1	0	3	0	1	0	3
547		8	max	0	1	.162	3	.163	3	0	1	0	3	0	1
548			min	-111.29	3	0	1	0	1	0	3	0	1	0	3
549		9	max	0	1	.081	3	.163	3	0	1	0	3	0	1
550			min	-111.355	3	0	1	0	1	0	3	0	1	0	3
551		10	max	0	1	0	1	.163	3	0	1	0	3	0	1
552			min	-111.42	3	0	1	0	1	0	3	0	1	0	3
553		11	max	0	1	0	1	.163	3	0	1	0	3	0	1
554			min	-111.485	3	-.081	3	0	1	0	3	0	1	0	3
555		12	max	0	1	0	1	.163	3	0	1	0	3	0	1
556			min	-111.551	3	-.162	3	0	1	0	3	0	1	0	3
557		13	max	0	1	0	1	.163	3	0	1	0	3	0	1
558			min	-111.616	3	-.244	3	0	1	0	3	0	1	0	3
559		14	max	0	1	0	1	.163	3	0	1	0	3	0	1
560			min	-111.681	3	-.325	3	0	1	0	3	0	1	0	3
561		15	max	0	1	0	1	.163	3	0	1	0	3	0	1
562			min	-111.746	3	-.406	3	0	1	0	3	0	1	0	3
563		16	max	0	1	0	1	.163	3	0	1	0	3	0	1
564			min	-111.811	3	-.487	3	0	1	0	3	0	1	0	3
565		17	max	0	1	0	1	.163	3	0	1	0	3	0	1
566			min	-111.877	3	-.569	3	0	1	0	3	0	1	0	3
567		18	max	0	1	0	1	.163	3	0	1	0	3	0	1
568			min	-111.942	3	-.65	3	0	1	0	3	0	1	0	3
569		19	max	0	1	0	1	.163	3	0	1	0	3	0	1
570			min	-112.007	3	-.731	3	0	1	0	3	0	1	0	1
571	M16A	1	max	0	1	1.908	4	.298	4	0	3	0	3	0	1
572			min	-159.044	4	0	1	-.067	3	0	4	0	4	0	1
573		2	max	0	1	1.696	4	.269	4	0	3	0	3	0	1
574			min	-159.023	4	0	1	-.067	3	0	4	0	4	0	4
575		3	max	0	1	1.484	4	.239	4	0	3	0	3	0	1
576			min	-159.003	4	0	1	-.067	3	0	4	0	4	0	4
577		4	max	0	1	1.272	4	.21	4	0	3	0	3	0	1
578			min	-158.982	4	0	1	-.067	3	0	4	0	4	-.001	4
579		5	max	0	1	1.06	4	.18	4	0	3	0	3	0	1
580			min	-158.962	4	0	1	-.067	3	0	4	0	9	-.002	4
581		6	max	0	1	.848	4	.151	4	0	3	0	3	0	1
582			min	-158.941	4	0	1	-.067	3	0	4	0	9	-.002	4
583		7	max	0	1	.636	4	.121	4	0	3	0	3	0	1
584			min	-158.92	4	0	1	-.067	3	0	4	0	9	-.002	4
585		8	max	0	1	.424	4	.092	4	0	3	0	5	0	1
586			min	-158.9	4	0	1	-.067	3	0	4	0	9	-.002	4
587		9	max	0	1	.212	4	.062	4	0	3	0	5	0	1
588			min	-158.879	4	0	1	-.067	3	0	4	0	9	-.002	4
589		10	max	0	1	0	1	.033	4	0	3	0	5	0	1
590			min	-158.859	4	0	1	-.067	3	0	4	0	9	-.002	4
591		11	max	0	1	0	1	.015	9	0	3	0	5	0	1
592			min	-158.838	4	-.212	4	-.067	3	0	4	0	9	-.002	4
593		12	max	0	1	0	1	.015	9	0	3	0	5	0	1
594			min	-158.818	4	-.424	4	-.067	3	0	4	0	9	-.002	4
595		13	max	0	1	0	1	.015	9	0	3	0	5	0	1
596			min	-158.797	4	-.636	4	-.067	3	0	4	0	3	-.002	4
597		14	max	0	1	0	1	.015	9	0	3	0	5	0	1
598			min	-158.777	4	-.848	4	-.089	5	0	4	0	3	-.002	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
599		15	max	.019	9	0	1	.015	9	0	3	0	5	0	1
600			min	-158.756	4	-1.06	4	-.118	5	0	4	0	3	-.002	4
601		16	max	.092	9	0	1	.015	9	0	3	0	5	0	1
602			min	-158.794	5	-1.272	4	-.148	5	0	4	0	3	-.001	4
603		17	max	.164	9	0	1	.015	9	0	3	0	9	0	1
604			min	-158.844	5	-1.484	4	-.177	5	0	4	0	3	0	4
605		18	max	.237	9	0	1	.015	9	0	3	0	9	0	1
606			min	-158.894	5	-1.696	4	-.207	5	0	4	0	3	0	4
607		19	max	.309	9	0	1	.015	9	0	3	0	9	0	1
608			min	-158.945	5	-1.908	4	-.236	5	0	4	0	5	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M2	1	max	.002	2	.008	2	.001	9	7.583e-4	5	NC	3	NC	1
2			min	-.003	3	-.007	3	-.008	5	-1.888e-4	3	4683.096	2	NC	1
3		2	max	.002	2	.007	2	.001	9	7.783e-4	5	NC	3	NC	1
4			min	-.003	3	-.007	3	-.008	5	-1.788e-4	3	5106.954	2	NC	1
5		3	max	.002	2	.006	2	.001	9	7.983e-4	5	NC	1	NC	1
6			min	-.003	3	-.007	3	-.008	5	-1.689e-4	3	5610.453	2	NC	1
7		4	max	.001	2	.006	2	.001	9	8.182e-4	5	NC	1	NC	1
8			min	-.003	3	-.007	3	-.008	5	-1.59e-4	3	6212.875	2	NC	1
9		5	max	.001	2	.005	2	.001	9	8.382e-4	5	NC	1	NC	1
10			min	-.002	3	-.006	3	-.007	5	-1.49e-4	3	6939.946	2	NC	1
11		6	max	.001	2	.005	2	0	9	8.581e-4	5	NC	1	NC	1
12			min	-.002	3	-.006	3	-.007	5	-1.391e-4	3	7826.57	2	NC	1
13		7	max	.001	2	.004	2	0	9	8.781e-4	5	NC	1	NC	1
14			min	-.002	3	-.006	3	-.007	5	-1.305e-4	1	8921.027	2	NC	1
15		8	max	.001	2	.004	2	0	9	8.981e-4	5	NC	1	NC	1
16			min	-.002	3	-.005	3	-.006	5	-1.221e-4	1	NC	1	NC	1
17		9	max	0	2	.003	2	0	9	9.18e-4	5	NC	1	NC	1
18			min	-.002	3	-.005	3	-.006	5	-1.136e-4	1	NC	1	NC	1
19		10	max	0	2	.003	2	0	9	9.38e-4	5	NC	1	NC	1
20			min	-.002	3	-.005	3	-.006	5	-1.052e-4	1	NC	1	NC	1
21		11	max	0	2	.002	2	0	9	9.58e-4	5	NC	1	NC	1
22			min	-.001	3	-.004	3	-.005	5	-9.678e-5	1	NC	1	NC	1
23		12	max	0	2	.002	2	0	9	9.779e-4	5	NC	1	NC	1
24			min	-.001	3	-.004	3	-.005	5	-8.835e-5	1	NC	1	NC	1
25		13	max	0	2	.001	2	0	9	9.979e-4	5	NC	1	NC	1
26			min	-.001	3	-.003	3	-.004	5	-7.991e-5	1	NC	1	NC	1
27		14	max	0	2	0	2	0	9	1.018e-3	5	NC	1	NC	1
28			min	0	3	-.003	3	-.003	5	-7.148e-5	1	NC	1	NC	1
29		15	max	0	2	0	2	0	9	1.038e-3	5	NC	1	NC	1
30			min	0	3	-.002	3	-.003	5	-6.304e-5	1	NC	1	NC	1
31		16	max	0	2	0	2	0	9	1.058e-3	5	NC	1	NC	1
32			min	0	3	-.002	3	-.002	5	-5.461e-5	1	NC	1	NC	1
33		17	max	0	2	0	2	0	9	1.078e-3	5	NC	1	NC	1
34			min	0	3	-.001	3	-.001	5	-4.617e-5	1	NC	1	NC	1
35		18	max	0	2	0	2	0	9	1.098e-3	5	NC	1	NC	1
36			min	0	3	0	3	0	5	-3.774e-5	1	NC	1	NC	1
37		19	max	0	1	0	1	0	1	1.118e-3	5	NC	1	NC	1
38			min	0	1	0	1	0	1	-2.93e-5	1	NC	1	NC	1
39	M3	1	max	0	1	0	1	0	1	1.372e-5	1	NC	1	NC	1
40			min	0	1	0	1	0	1	-5.198e-4	5	NC	1	NC	1
41		2	max	0	3	0	2	.003	5	1.991e-5	1	NC	1	NC	1
42			min	0	2	0	3	0	9	-5.219e-4	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
43		3	max	0	3	0	2	.005	5	2.61e-5	1	NC	1	NC	1
44			min	0	2	-.002	3	0	9	-5.24e-4	5	NC	1	NC	1
45		4	max	0	3	0	2	.008	5	3.229e-5	1	NC	1	NC	1
46			min	0	2	-.002	3	0	9	-5.261e-4	5	NC	1	NC	1
47		5	max	0	3	0	2	.011	4	3.847e-5	1	NC	1	NC	1
48			min	0	2	-.003	3	0	9	-5.282e-4	5	NC	1	NC	1
49		6	max	0	3	0	2	.013	4	4.466e-5	1	NC	1	NC	1
50			min	0	2	-.004	3	0	9	-5.304e-4	5	NC	1	NC	1
51		7	max	0	3	0	2	.016	4	5.085e-5	1	NC	1	NC	1
52			min	0	2	-.005	3	0	9	-5.325e-4	5	NC	1	NC	1
53		8	max	0	3	0	2	.019	4	5.704e-5	1	NC	1	NC	1
54			min	0	2	-.005	3	0	10	-5.346e-4	5	NC	1	NC	1
55		9	max	0	3	0	2	.021	4	6.323e-5	1	NC	1	NC	1
56			min	0	2	-.006	3	0	10	-5.367e-4	5	NC	1	NC	1
57		10	max	0	3	.001	2	.023	4	6.942e-5	1	NC	1	NC	1
58			min	0	2	-.006	3	0	10	-5.388e-4	5	NC	1	NC	1
59		11	max	0	3	.002	2	.026	4	7.561e-5	1	NC	1	NC	1
60			min	0	2	-.007	3	0	10	-5.41e-4	5	NC	1	NC	1
61		12	max	0	3	.002	2	.028	4	8.18e-5	1	NC	1	NC	1
62			min	0	2	-.007	3	0	10	-5.431e-4	5	NC	1	NC	1
63		13	max	0	3	.003	2	.03	4	8.799e-5	1	NC	1	NC	1
64			min	-.001	2	-.007	3	0	10	-5.452e-4	5	NC	1	NC	1
65		14	max	.001	3	.004	2	.032	4	9.418e-5	1	NC	1	NC	1
66			min	-.001	2	-.007	3	0	10	-5.473e-4	5	NC	1	NC	1
67		15	max	.001	3	.004	2	.034	4	1.004e-4	1	NC	1	NC	1
68			min	-.001	2	-.007	3	0	10	-5.494e-4	5	NC	1	NC	1
69		16	max	.001	3	.005	2	.036	4	1.066e-4	1	NC	1	NC	1
70			min	-.001	2	-.007	3	0	10	-5.516e-4	5	8625.434	2	NC	1
71		17	max	.001	3	.006	2	.037	4	1.127e-4	1	NC	1	NC	1
72			min	-.001	2	-.008	3	0	10	-5.537e-4	5	7356.474	2	NC	1
73		18	max	.001	3	.007	2	.039	4	1.189e-4	1	NC	1	NC	1
74			min	-.002	2	-.007	3	0	10	-5.558e-4	5	6377.183	2	NC	1
75		19	max	.001	3	.008	2	.041	4	1.251e-4	1	NC	3	NC	1
76			min	-.002	2	-.007	3	0	10	-5.579e-4	5	5613.214	2	NC	1
77	M4	1	max	.001	1	.009	2	0	10	2.392e-3	5	NC	1	NC	1
78			min	0	3	-.008	3	-.043	4	-1.345e-4	1	NC	1	447.418	4
79		2	max	.001	1	.008	2	0	10	2.392e-3	5	NC	1	NC	1
80			min	0	3	-.007	3	-.04	4	-1.345e-4	1	NC	1	487.671	4
81		3	max	.001	1	.008	2	0	10	2.392e-3	5	NC	1	NC	1
82			min	0	3	-.007	3	-.036	4	-1.345e-4	1	NC	1	535.571	4
83		4	max	.001	1	.007	2	0	10	2.392e-3	5	NC	1	NC	1
84			min	0	3	-.006	3	-.033	4	-1.345e-4	1	NC	1	593.131	4
85		5	max	0	1	.007	2	0	10	2.392e-3	5	NC	1	NC	1
86			min	0	3	-.006	3	-.029	4	-1.345e-4	1	NC	1	663.094	4
87		6	max	0	1	.006	2	0	10	2.392e-3	5	NC	1	NC	1
88			min	0	3	-.005	3	-.026	4	-1.345e-4	1	NC	1	749.275	4
89		7	max	0	1	.006	2	0	10	2.392e-3	5	NC	1	NC	1
90			min	0	3	-.005	3	-.023	4	-1.345e-4	1	NC	1	857.105	4
91		8	max	0	1	.005	2	0	10	2.392e-3	5	NC	1	NC	1
92			min	0	3	-.005	3	-.019	4	-1.345e-4	1	NC	1	994.536	4
93		9	max	0	1	.005	2	0	10	2.392e-3	5	NC	1	NC	1
94			min	0	3	-.004	3	-.016	4	-1.345e-4	1	NC	1	1173.598	4
95		10	max	0	1	.004	2	0	10	2.392e-3	5	NC	1	NC	1
96			min	0	3	-.004	3	-.014	4	-1.345e-4	1	NC	1	1413.195	4
97		11	max	0	1	.004	2	0	10	2.392e-3	5	NC	1	NC	1
98			min	0	3	-.003	3	-.011	4	-1.345e-4	1	NC	1	1744.462	4
99		12	max	0	1	.003	2	0	10	2.392e-3	5	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
100			min	0	3	-.003	3	-.009	4	-1.345e-4	1	NC	1	2221.704	4
101		13	max	0	1	.003	2	0	10	2.392e-3	5	NC	1	NC	1
102			min	0	3	-.003	3	-.007	4	-1.345e-4	1	NC	1	2946.774	4
103		14	max	0	1	.002	2	0	10	2.392e-3	5	NC	1	NC	1
104			min	0	3	-.002	3	-.005	4	-1.345e-4	1	NC	1	4129.744	4
105		15	max	0	1	.002	2	0	10	2.392e-3	5	NC	1	NC	1
106			min	0	3	-.002	3	-.003	4	-1.345e-4	1	NC	1	6264.108	4
107		16	max	0	1	.001	2	0	10	2.392e-3	5	NC	1	NC	1
108			min	0	3	-.001	3	-.002	4	-1.345e-4	1	NC	1	NC	1
109		17	max	0	1	0	2	0	10	2.392e-3	5	NC	1	NC	1
110			min	0	3	0	3	0	4	-1.345e-4	1	NC	1	NC	1
111		18	max	0	1	0	2	0	10	2.392e-3	5	NC	1	NC	1
112			min	0	3	0	3	0	4	-1.345e-4	1	NC	1	NC	1
113		19	max	0	1	0	1	0	1	2.392e-3	5	NC	1	NC	1
114			min	0	1	0	1	0	1	-1.345e-4	1	NC	1	NC	1
115	M6	1	max	.005	2	.024	2	0	9	7.995e-4	4	NC	3	NC	1
116			min	-.009	3	-.021	3	-.008	5	-9.028e-8	1	1524.508	2	6217.596	3
117		2	max	.005	2	.022	2	0	9	8.198e-4	4	NC	3	NC	1
118			min	-.009	3	-.02	3	-.008	5	-8.525e-8	1	1631.895	2	6618.147	3
119		3	max	.005	2	.021	2	0	9	8.401e-4	4	NC	3	NC	1
120			min	-.008	3	-.019	3	-.008	5	-1.884e-7	9	1755.045	2	7092.351	3
121		4	max	.005	2	.019	2	0	9	8.604e-4	4	NC	3	NC	1
122			min	-.008	3	-.018	3	-.008	5	-9.429e-7	9	1897.14	2	7656.237	3
123		5	max	.004	2	.018	2	0	9	8.808e-4	4	NC	3	NC	1
124			min	-.007	3	-.017	3	-.007	5	-1.697e-6	9	2062.278	2	8331.05	3
125		6	max	.004	2	.016	2	0	9	9.011e-4	4	NC	3	NC	1
126			min	-.007	3	-.016	3	-.007	5	-2.452e-6	9	2255.831	2	9145.371	3
127		7	max	.004	2	.015	2	0	9	9.214e-4	4	NC	3	NC	1
128			min	-.006	3	-.015	3	-.007	5	-3.206e-6	9	2484.973	2	NC	1
129		8	max	.003	2	.013	2	0	9	9.417e-4	4	NC	3	NC	1
130			min	-.006	3	-.014	3	-.006	5	-3.961e-6	9	2759.494	2	NC	1
131		9	max	.003	2	.012	2	0	9	9.621e-4	4	NC	3	NC	1
132			min	-.005	3	-.012	3	-.006	5	-4.715e-6	9	3093.112	2	NC	1
133		10	max	.003	2	.01	2	0	9	9.824e-4	4	NC	3	NC	1
134			min	-.005	3	-.011	3	-.006	5	-5.47e-6	9	3505.652	2	NC	1
135		11	max	.002	2	.009	2	0	9	1.003e-3	4	NC	3	NC	1
136			min	-.004	3	-.01	3	-.005	5	-6.224e-6	9	4026.857	2	NC	1
137		12	max	.002	2	.008	2	0	9	1.023e-3	4	NC	3	NC	1
138			min	-.004	3	-.009	3	-.005	5	-6.978e-6	9	4703.472	2	NC	1
139		13	max	.002	2	.006	2	0	9	1.043e-3	4	NC	3	NC	1
140			min	-.003	3	-.008	3	-.004	5	-7.733e-6	9	5613.41	2	NC	1
141		14	max	.002	2	.005	2	0	9	1.064e-3	4	NC	1	NC	1
142			min	-.003	3	-.006	3	-.003	5	-8.487e-6	9	6896.906	2	NC	1
143		15	max	.001	2	.004	2	0	9	1.084e-3	4	NC	1	NC	1
144			min	-.002	3	-.005	3	-.003	5	-9.242e-6	9	8834.416	2	NC	1
145		16	max	0	2	.003	2	0	9	1.104e-3	4	NC	1	NC	1
146			min	-.002	3	-.004	3	-.002	5	-9.996e-6	9	NC	1	NC	1
147		17	max	0	2	.002	2	0	9	1.125e-3	4	NC	1	NC	1
148			min	-.001	3	-.003	3	-.001	5	-1.075e-5	9	NC	1	NC	1
149		18	max	0	2	0	2	0	9	1.145e-3	4	NC	1	NC	1
150			min	0	3	-.001	3	0	4	-1.151e-5	9	NC	1	NC	1
151		19	max	0	1	0	1	0	1	1.165e-3	4	NC	1	NC	1
152			min	0	1	0	1	0	1	-1.226e-5	9	NC	1	NC	1
153	M7	1	max	0	1	0	1	0	1	5.675e-6	9	NC	1	NC	1
154			min	0	1	0	1	0	1	-5.419e-4	4	NC	1	NC	1
155		2	max	0	3	.001	2	.003	4	5.064e-6	9	NC	1	NC	1
156			min	0	2	-.002	3	0	9	-5.345e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
157		3	max	0	3	.002	2	.006	4	4.454e-6	9	NC	1	NC	1
158			min	0	2	-.003	3	0	9	-5.271e-4	4	NC	1	NC	1
159		4	max	0	3	.003	2	.008	4	3.843e-6	9	NC	1	NC	1
160			min	0	2	-.005	3	0	9	-5.197e-4	4	NC	1	NC	1
161		5	max	0	3	.004	2	.011	4	3.233e-6	9	NC	1	NC	1
162			min	-.001	2	-.007	3	0	9	-5.123e-4	4	NC	1	NC	1
163		6	max	.001	3	.005	2	.014	4	1.819e-5	3	NC	1	NC	1
164			min	-.001	2	-.008	3	0	9	-5.05e-4	4	8505.821	2	NC	1
165		7	max	.001	3	.007	2	.017	4	4.153e-5	3	NC	1	NC	1
166			min	-.002	2	-.01	3	0	9	-4.976e-4	4	7053.472	2	NC	1
167		8	max	.001	3	.008	2	.019	4	6.486e-5	3	NC	1	NC	1
168			min	-.002	2	-.011	3	0	9	-4.902e-4	4	5983.524	2	NC	1
169		9	max	.002	3	.009	2	.022	4	8.819e-5	3	NC	3	NC	1
170			min	-.002	2	-.012	3	0	9	-4.828e-4	4	5157.774	2	NC	1
171		10	max	.002	3	.01	2	.024	4	1.115e-4	3	NC	3	NC	1
172			min	-.002	2	-.014	3	0	9	-4.755e-4	4	4499.64	2	NC	1
173		11	max	.002	3	.012	2	.027	4	1.349e-4	3	NC	3	NC	1
174			min	-.003	2	-.015	3	0	9	-4.681e-4	4	3963.054	2	NC	1
175		12	max	.002	3	.013	2	.029	4	1.582e-4	3	NC	3	NC	1
176			min	-.003	2	-.016	3	0	9	-4.607e-4	4	3518.394	2	NC	1
177		13	max	.003	3	.015	2	.031	4	1.815e-4	3	NC	3	NC	1
178			min	-.003	2	-.017	3	0	9	-4.533e-4	4	3145.531	2	NC	1
179		14	max	.003	3	.016	2	.033	4	2.049e-4	3	NC	3	NC	1
180			min	-.003	2	-.018	3	0	9	-4.459e-4	4	2830.137	2	NC	1
181		15	max	.003	3	.018	2	.035	4	2.282e-4	3	NC	3	NC	1
182			min	-.004	2	-.019	3	0	9	-4.386e-4	4	2561.624	2	NC	1
183		16	max	.003	3	.02	2	.037	4	2.515e-4	3	NC	3	NC	1
184			min	-.004	2	-.02	3	0	9	-4.312e-4	4	2331.919	2	NC	1
185		17	max	.003	3	.022	2	.039	4	2.749e-4	3	NC	3	NC	1
186			min	-.004	2	-.02	3	0	9	-4.238e-4	4	2134.73	2	NC	1
187		18	max	.004	3	.023	2	.04	4	2.982e-4	3	NC	3	NC	1
188			min	-.005	2	-.021	3	0	9	-4.164e-4	4	1965.059	2	NC	1
189		19	max	.004	3	.025	2	.042	4	3.215e-4	3	NC	3	NC	1
190			min	-.005	2	-.022	3	0	9	-4.09e-4	4	1818.892	2	NC	1
191	M8	1	max	.004	2	.027	2	0	9	2.253e-3	4	NC	1	NC	1
192			min	0	3	-.022	3	-.044	4	-2.366e-4	3	NC	1	438.328	4
193		2	max	.003	2	.025	2	0	9	2.253e-3	4	NC	1	NC	1
194			min	0	3	-.02	3	-.04	4	-2.366e-4	3	NC	1	477.766	4
195		3	max	.003	2	.024	2	0	9	2.253e-3	4	NC	1	NC	1
196			min	0	3	-.019	3	-.037	4	-2.366e-4	3	NC	1	524.696	4
197		4	max	.003	2	.022	2	0	9	2.253e-3	4	NC	1	NC	1
198			min	0	3	-.018	3	-.033	4	-2.366e-4	3	NC	1	581.091	4
199		5	max	.003	2	.021	2	0	9	2.253e-3	4	NC	1	NC	1
200			min	0	3	-.017	3	-.03	4	-2.366e-4	3	NC	1	649.639	4
201		6	max	.003	2	.019	2	0	9	2.253e-3	4	NC	1	NC	1
202			min	0	3	-.016	3	-.026	4	-2.366e-4	3	NC	1	734.076	4
203		7	max	.002	2	.018	2	0	9	2.253e-3	4	NC	1	NC	1
204			min	0	3	-.014	3	-.023	4	-2.366e-4	3	NC	1	839.726	4
205		8	max	.002	2	.016	2	0	9	2.253e-3	4	NC	1	NC	1
206			min	0	3	-.013	3	-.02	4	-2.366e-4	3	NC	1	974.379	4
207		9	max	.002	2	.015	2	0	9	2.253e-3	4	NC	1	NC	1
208			min	0	3	-.012	3	-.017	4	-2.366e-4	3	NC	1	1149.822	4
209		10	max	.002	2	.013	2	0	9	2.253e-3	4	NC	1	NC	1
210			min	0	3	-.011	3	-.014	4	-2.366e-4	3	NC	1	1384.579	4
211		11	max	.002	2	.012	2	0	9	2.253e-3	4	NC	1	NC	1
212			min	0	3	-.01	3	-.011	4	-2.366e-4	3	NC	1	1709.156	4
213		12	max	.001	2	.01	2	0	9	2.253e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
214			min	0	3	-.008	3	-.009	4	-2.366e-4	3	NC	1	2176.763	4
215		13	max	.001	2	.009	2	0	9	2.253e-3	4	NC	1	NC	1
216			min	0	3	-.007	3	-.007	4	-2.366e-4	3	NC	1	2887.197	4
217		14	max	.001	2	.007	2	0	9	2.253e-3	4	NC	1	NC	1
218			min	0	3	-.006	3	-.005	4	-2.366e-4	3	NC	1	4046.296	4
219		15	max	0	2	.006	2	0	9	2.253e-3	4	NC	1	NC	1
220			min	0	3	-.005	3	-.003	4	-2.366e-4	3	NC	1	6137.605	4
221		16	max	0	2	.004	2	0	9	2.253e-3	4	NC	1	NC	1
222			min	0	3	-.004	3	-.002	4	-2.366e-4	3	NC	1	NC	1
223		17	max	0	2	.003	2	0	9	2.253e-3	4	NC	1	NC	1
224			min	0	3	-.002	3	0	4	-2.366e-4	3	NC	1	NC	1
225		18	max	0	2	.001	2	0	9	2.253e-3	4	NC	1	NC	1
226			min	0	3	-.001	3	0	4	-2.366e-4	3	NC	1	NC	1
227		19	max	0	1	0	1	0	1	2.253e-3	4	NC	1	NC	1
228			min	0	1	0	1	0	1	-2.366e-4	3	NC	1	NC	1
229	M10	1	max	.002	2	.008	2	0	10	1.809e-4	1	NC	3	NC	1
230			min	-.002	3	-.007	3	-.004	4	-5.284e-4	3	4688.289	2	NC	1
231		2	max	.002	2	.007	2	0	10	1.725e-4	1	NC	3	NC	1
232			min	-.002	3	-.007	3	-.004	4	-5.112e-4	3	5112.764	2	NC	1
233		3	max	.002	2	.006	2	0	3	2.111e-4	4	NC	1	NC	1
234			min	-.002	3	-.007	3	-.004	4	-4.94e-4	3	5617.024	2	NC	1
235		4	max	.002	2	.006	2	0	3	2.558e-4	4	NC	1	NC	1
236			min	-.002	3	-.007	3	-.004	4	-4.768e-4	3	6220.393	2	NC	1
237		5	max	.001	2	.005	2	0	3	3.005e-4	4	NC	1	NC	1
238			min	-.002	3	-.006	3	-.004	4	-4.596e-4	3	6948.656	2	NC	1
239		6	max	.001	2	.005	2	0	3	3.452e-4	4	NC	1	NC	1
240			min	-.002	3	-.006	3	-.004	4	-4.425e-4	3	7836.798	2	NC	1
241		7	max	.001	2	.004	2	0	3	3.899e-4	4	NC	1	NC	1
242			min	-.002	3	-.006	3	-.004	4	-4.253e-4	3	8933.218	2	NC	1
243		8	max	.001	2	.004	2	0	3	4.346e-4	4	NC	1	NC	1
244			min	-.002	3	-.005	3	-.004	4	-4.081e-4	3	NC	1	NC	1
245		9	max	.001	2	.003	2	0	3	4.793e-4	4	NC	1	NC	1
246			min	-.001	3	-.005	3	-.004	4	-3.909e-4	3	NC	1	NC	1
247		10	max	0	2	.003	2	0	3	5.24e-4	4	NC	1	NC	1
248			min	-.001	3	-.005	3	-.004	4	-3.737e-4	3	NC	1	NC	1
249		11	max	0	2	.002	2	0	3	5.687e-4	4	NC	1	NC	1
250			min	-.001	3	-.004	3	-.004	4	-3.565e-4	3	NC	1	NC	1
251		12	max	0	2	.002	2	0	3	6.134e-4	4	NC	1	NC	1
252			min	0	3	-.004	3	-.003	4	-3.393e-4	3	NC	1	NC	1
253		13	max	0	2	.001	2	0	3	6.581e-4	4	NC	1	NC	1
254			min	0	3	-.003	3	-.003	4	-3.221e-4	3	NC	1	NC	1
255		14	max	0	2	0	2	0	3	7.028e-4	4	NC	1	NC	1
256			min	0	3	-.003	3	-.003	4	-3.05e-4	3	NC	1	NC	1
257		15	max	0	2	0	2	0	3	7.475e-4	4	NC	1	NC	1
258			min	0	3	-.002	3	-.002	4	-2.878e-4	3	NC	1	NC	1
259		16	max	0	2	0	2	0	3	7.922e-4	4	NC	1	NC	1
260			min	0	3	-.002	3	-.002	4	-2.706e-4	3	NC	1	NC	1
261		17	max	0	2	0	2	0	3	8.369e-4	4	NC	1	NC	1
262			min	0	3	-.001	3	-.001	4	-2.534e-4	3	NC	1	NC	1
263		18	max	0	2	0	2	0	3	8.816e-4	4	NC	1	NC	1
264			min	0	3	0	3	0	4	-2.362e-4	3	NC	1	NC	1
265		19	max	0	1	0	1	0	1	9.263e-4	4	NC	1	NC	1
266			min	0	1	0	1	0	1	-2.19e-4	3	NC	1	NC	1
267	M11	1	max	0	1	0	1	0	1	1.021e-4	3	NC	1	NC	1
268			min	0	1	0	1	0	1	-4.311e-4	4	NC	1	NC	1
269		2	max	0	3	0	2	.002	4	7.926e-5	3	NC	1	NC	1
270			min	0	2	0	3	0	3	-4.651e-4	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
271		3	max	0	3	0	2	.005	4	5.643e-5	3	NC	1	NC	1
272			min	0	2	-.002	3	0	3	-4.991e-4	4	NC	1	NC	1
273		4	max	0	3	0	2	.007	4	3.36e-5	3	NC	1	NC	1
274			min	0	2	-.002	3	-.001	3	-5.332e-4	4	NC	1	NC	1
275		5	max	0	3	0	2	.009	4	1.077e-5	3	NC	1	NC	1
276			min	0	2	-.003	3	-.002	3	-5.672e-4	4	NC	1	NC	1
277		6	max	0	3	0	2	.011	4	4.352e-6	10	NC	1	NC	1
278			min	0	2	-.004	3	-.002	3	-6.012e-4	4	NC	1	NC	1
279		7	max	0	3	0	2	.014	4	4.965e-6	10	NC	1	NC	1
280			min	0	2	-.005	3	-.002	3	-6.353e-4	4	NC	1	NC	1
281		8	max	0	3	0	2	.016	5	5.577e-6	10	NC	1	NC	1
282			min	0	2	-.005	3	-.002	3	-6.693e-4	4	NC	1	NC	1
283		9	max	0	3	0	2	.018	5	6.19e-6	10	NC	1	NC	1
284			min	0	2	-.006	3	-.003	3	-7.033e-4	4	NC	1	NC	1
285		10	max	0	3	.001	2	.02	5	6.803e-6	10	NC	1	NC	1
286			min	0	2	-.006	3	-.003	3	-7.374e-4	4	NC	1	NC	1
287		11	max	0	3	.002	2	.022	5	7.415e-6	10	NC	1	NC	1
288			min	0	2	-.007	3	-.003	3	-7.714e-4	4	NC	1	NC	1
289		12	max	0	3	.002	2	.024	5	8.028e-6	10	NC	1	NC	1
290			min	0	2	-.007	3	-.003	3	-8.054e-4	4	NC	1	NC	1
291		13	max	0	3	.003	2	.026	5	8.64e-6	10	NC	1	NC	1
292			min	-.001	2	-.007	3	-.003	3	-8.394e-4	4	NC	1	NC	1
293		14	max	.001	3	.004	2	.028	5	9.253e-6	10	NC	1	NC	1
294			min	-.001	2	-.007	3	-.003	3	-8.735e-4	4	NC	1	NC	1
295		15	max	.001	3	.004	2	.03	5	9.865e-6	10	NC	1	NC	1
296			min	-.001	2	-.007	3	-.003	3	-9.075e-4	4	NC	1	NC	1
297		16	max	.001	3	.005	2	.032	5	1.048e-5	10	NC	1	NC	1
298			min	-.001	2	-.008	3	-.003	3	-9.415e-4	4	8635.873	2	NC	1
299		17	max	.001	3	.006	2	.034	5	1.109e-5	10	NC	1	NC	1
300			min	-.001	2	-.008	3	-.003	3	-9.756e-4	4	7364.503	2	NC	1
301		18	max	.001	3	.007	2	.035	5	1.17e-5	10	NC	1	NC	1
302			min	-.002	2	-.008	3	-.002	3	-1.01e-3	4	6383.544	2	NC	1
303		19	max	.001	3	.008	2	.037	5	1.232e-5	10	NC	3	NC	1
304			min	-.002	2	-.008	3	-.002	3	-1.044e-3	4	5618.394	2	NC	1
305	M12	1	max	.001	1	.009	2	.001	1	2.8e-3	4	NC	1	NC	1
306			min	0	3	-.008	3	-.041	5	-1.352e-5	10	NC	1	474.996	5
307		2	max	.001	1	.008	2	.001	1	2.8e-3	4	NC	1	NC	1
308			min	0	3	-.007	3	-.037	5	-1.352e-5	10	NC	1	517.718	5
309		3	max	.001	1	.008	2	.001	1	2.8e-3	4	NC	1	NC	1
310			min	0	3	-.007	3	-.034	5	-1.352e-5	10	NC	1	568.555	5
311		4	max	.001	1	.007	2	.001	1	2.8e-3	4	NC	1	NC	1
312			min	0	3	-.006	3	-.031	5	-1.352e-5	10	NC	1	629.643	5
313		5	max	0	1	.007	2	0	1	2.8e-3	4	NC	1	NC	1
314			min	0	3	-.006	3	-.027	5	-1.352e-5	10	NC	1	703.893	5
315		6	max	0	1	.006	2	0	1	2.8e-3	4	NC	1	NC	1
316			min	0	3	-.005	3	-.024	5	-1.352e-5	10	NC	1	795.352	5
317		7	max	0	1	.006	2	0	1	2.8e-3	4	NC	1	NC	1
318			min	0	3	-.005	3	-.021	5	-1.352e-5	10	NC	1	909.784	5
319		8	max	0	1	.005	2	0	1	2.8e-3	4	NC	1	NC	1
320			min	0	3	-.005	3	-.018	5	-1.352e-5	10	NC	1	1055.628	5
321		9	max	0	1	.005	2	0	1	2.8e-3	4	NC	1	NC	1
322			min	0	3	-.004	3	-.016	5	-1.352e-5	10	NC	1	1245.645	5
323		10	max	0	1	.004	2	0	1	2.8e-3	4	NC	1	NC	1
324			min	0	3	-.004	3	-.013	5	-1.352e-5	10	NC	1	1499.897	5
325		11	max	0	1	.004	2	0	1	2.8e-3	4	NC	1	NC	1
326			min	0	3	-.003	3	-.01	5	-1.352e-5	10	NC	1	1851.42	5
327		12	max	0	1	.003	2	0	1	2.8e-3	4	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
328			min	0	3	-.003	3	-.008	5	-1.352e-5	10	NC	1	2357.834	5
329		13	max	0	1	.003	2	0	1	2.8e-3	4	NC	1	NC	1
330			min	0	3	-.003	3	-.006	5	-1.352e-5	10	NC	1	3127.208	5
331		14	max	0	1	.002	2	0	1	2.8e-3	4	NC	1	NC	1
332			min	0	3	-.002	3	-.004	5	-1.352e-5	10	NC	1	4382.436	5
333		15	max	0	1	.002	2	0	1	2.8e-3	4	NC	1	NC	1
334			min	0	3	-.002	3	-.003	5	-1.352e-5	10	NC	1	6647.126	5
335		16	max	0	1	.001	2	0	1	2.8e-3	4	NC	1	NC	1
336			min	0	3	-.001	3	-.002	5	-1.352e-5	10	NC	1	NC	1
337		17	max	0	1	0	2	0	1	2.8e-3	4	NC	1	NC	1
338			min	0	3	0	3	0	5	-1.352e-5	10	NC	1	NC	1
339		18	max	0	1	0	2	0	1	2.8e-3	4	NC	1	NC	1
340			min	0	3	0	3	0	5	-1.352e-5	10	NC	1	NC	1
341		19	max	0	1	0	1	0	1	2.8e-3	4	NC	1	NC	1
342			min	0	1	0	1	0	1	-1.352e-5	10	NC	1	NC	1
343	M1	1	max	.007	3	.022	3	.005	5	4.721e-3	2	NC	1	NC	1
344			min	-.007	2	-.019	2	0	9	-6.787e-3	3	NC	1	NC	1
345		2	max	.007	3	.013	3	.007	5	2.335e-3	2	NC	4	NC	1
346			min	-.007	2	-.01	2	-.001	9	-3.331e-3	3	5047.71	3	NC	1
347		3	max	.007	3	.004	3	.008	5	2.186e-4	5	NC	4	NC	1
348			min	-.007	2	-.003	2	-.002	9	-7.311e-5	1	2617.759	3	NC	1
349		4	max	.007	3	.004	2	.01	5	2.15e-4	5	NC	4	NC	1
350			min	-.007	2	-.003	3	-.002	9	-6.044e-5	9	1869.633	3	8716.069	5
351		5	max	.007	3	.01	2	.013	5	2.114e-4	5	NC	4	NC	1
352			min	-.007	2	-.01	3	-.002	1	-4.838e-5	9	1513.75	3	6171.568	5
353		6	max	.007	3	.015	2	.015	5	2.077e-4	5	NC	4	NC	1
354			min	-.007	2	-.015	3	-.002	1	-3.632e-5	9	1315.927	3	4702.785	5
355		7	max	.007	3	.019	2	.017	5	2.041e-4	5	NC	4	NC	1
356			min	-.007	2	-.018	3	-.001	9	-2.427e-5	9	1195.891	2	3761.363	5
357		8	max	.007	3	.022	2	.02	5	2.005e-4	5	NC	4	NC	1
358			min	-.007	2	-.021	3	-.001	9	-1.221e-5	9	1104.483	2	3114.975	5
359		9	max	.007	3	.024	2	.023	5	1.986e-4	4	NC	4	NC	1
360			min	-.007	2	-.022	3	0	9	-1.124e-6	10	1050.36	2	2649.028	5
361		10	max	.007	3	.024	2	.025	4	1.989e-4	4	NC	4	NC	1
362			min	-.007	2	-.023	3	0	9	-2.623e-6	10	1025.355	2	2287.313	4
363		11	max	.007	3	.024	2	.028	4	1.992e-4	4	NC	4	NC	1
364			min	-.007	2	-.022	3	0	10	-4.122e-6	10	1026.524	2	2010.308	4
365		12	max	.007	3	.022	2	.031	4	1.996e-4	4	NC	4	NC	1
366			min	-.007	2	-.02	3	0	10	-5.622e-6	10	1055.059	2	1795.553	4
367		13	max	.007	3	.02	2	.034	4	1.999e-4	4	NC	4	NC	1
368			min	-.007	2	-.017	3	0	10	-7.121e-6	10	1116.922	2	1626.297	4
369		14	max	.007	3	.016	2	.036	4	2.002e-4	4	NC	4	NC	1
370			min	-.007	2	-.013	3	0	10	-8.62e-6	10	1225.877	2	1491.302	4
371		15	max	.007	3	.01	2	.039	4	2.005e-4	4	NC	4	NC	1
372			min	-.007	2	-.009	3	0	10	-1.012e-5	10	1412.127	2	1382.814	4
373		16	max	.007	3	.004	2	.041	4	3.455e-4	4	NC	4	NC	1
374			min	-.007	2	-.003	3	0	10	-1.124e-5	10	1749.511	2	1295.351	4
375		17	max	.007	3	.003	3	.043	4	3.934e-3	4	NC	4	NC	1
376			min	-.007	2	-.005	2	0	10	-3.462e-6	10	2473.99	2	1225.067	4
377		18	max	.007	3	.01	3	.045	4	3.259e-3	2	NC	4	NC	1
378			min	-.007	2	-.014	2	0	10	-1.715e-3	3	4791.451	2	1168.889	4
379		19	max	.007	3	.018	3	.047	4	6.575e-3	2	NC	1	NC	1
380			min	-.007	2	-.024	2	0	9	-3.529e-3	3	NC	1	1125.989	4
381	M5	1	max	.02	3	.068	3	.005	5	1.678e-5	4	NC	1	NC	1
382			min	-.023	2	-.057	2	0	9	7.835e-8	11	NC	1	NC	1
383		2	max	.02	3	.039	3	.006	5	1.204e-4	3	NC	4	NC	1
384			min	-.023	2	-.032	2	0	9	-7.772e-6	9	1647.339	3	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
385		3	max	.02	3	.012	3	.008	5	2.295e-4	3	NC	5	NC	1
386			min	-.023	2	-.008	2	0	9	-1.546e-5	9	854.9	3	NC	1
387		4	max	.02	3	.013	2	.01	5	2.231e-4	3	NC	5	NC	1
388			min	-.023	2	-.011	3	0	9	-1.457e-5	9	611.561	3	NC	1
389		5	max	.02	3	.031	2	.013	5	2.168e-4	3	NC	5	NC	1
390			min	-.023	2	-.03	3	0	9	-1.369e-5	9	495.987	3	NC	1
391		6	max	.02	3	.046	2	.015	5	2.164e-4	5	NC	5	NC	1
392			min	-.023	2	-.045	3	0	9	-1.28e-5	9	431.912	3	9175.906	3
393		7	max	.02	3	.058	2	.018	5	2.219e-4	5	NC	5	NC	1
394			min	-.023	2	-.056	3	0	9	-1.191e-5	9	385.947	2	8733.874	3
395		8	max	.02	3	.067	2	.021	5	2.274e-4	5	NC	5	NC	1
396			min	-.023	2	-.063	3	0	9	-1.102e-5	9	356.397	2	8649.932	3
397		9	max	.02	3	.073	2	.024	4	2.329e-4	5	NC	5	NC	1
398			min	-.023	2	-.068	3	0	9	-1.013e-5	9	338.903	2	8858.428	3
399		10	max	.02	3	.076	2	.027	4	2.384e-4	5	NC	5	NC	1
400			min	-.023	2	-.068	3	0	9	-9.245e-6	9	330.821	2	9353.999	3
401		11	max	.02	3	.074	2	.03	4	2.439e-4	5	NC	5	NC	1
402			min	-.023	2	-.066	3	0	9	-8.357e-6	9	331.199	2	NC	1
403		12	max	.02	3	.07	2	.033	4	2.495e-4	4	NC	5	NC	1
404			min	-.023	2	-.06	3	0	9	-7.469e-6	9	340.422	2	NC	1
405		13	max	.019	3	.061	2	.035	4	2.554e-4	4	NC	5	NC	1
406			min	-.023	2	-.052	3	0	9	-6.58e-6	9	360.413	2	NC	1
407		14	max	.019	3	.048	2	.038	4	2.614e-4	4	NC	5	NC	1
408			min	-.023	2	-.041	3	0	9	-5.692e-6	9	395.618	2	NC	1
409		15	max	.019	3	.032	2	.04	4	2.673e-4	4	NC	5	NC	1
410			min	-.023	2	-.026	3	0	9	-4.804e-6	9	455.789	2	NC	1
411		16	max	.019	3	.011	2	.042	4	4.154e-4	4	NC	5	NC	1
412			min	-.023	2	-.01	3	0	9	-4.52e-6	9	564.764	2	NC	1
413		17	max	.019	3	.009	3	.044	4	3.949e-3	4	NC	5	NC	1
414			min	-.023	2	-.014	2	0	9	-1.863e-5	9	798.701	2	NC	1
415		18	max	.019	3	.03	3	.046	4	2.029e-3	4	NC	4	NC	1
416			min	-.023	2	-.044	2	0	9	-9.569e-6	9	1547.126	2	NC	1
417		19	max	.019	3	.052	3	.047	4	6.226e-6	5	NC	1	NC	1
418			min	-.023	2	-.075	2	0	9	-1.422e-6	3	NC	1	NC	1
419	M9	1	max	.007	3	.022	3	.005	5	6.805e-3	3	NC	1	NC	1
420			min	-.007	2	-.019	2	0	9	-4.721e-3	2	NC	1	NC	1
421		2	max	.007	3	.012	3	.004	4	3.361e-3	3	NC	4	NC	1
422			min	-.007	2	-.01	2	0	10	-2.335e-3	2	5050.524	3	NC	1
423		3	max	.007	3	.003	3	.004	4	7.335e-5	1	NC	4	NC	1
424			min	-.007	2	-.003	2	0	10	-3.031e-5	5	2619.248	3	NC	1
425		4	max	.007	3	.004	2	.005	4	5.851e-5	1	NC	4	NC	1
426			min	-.007	2	-.004	3	-.001	3	-3.229e-5	5	1870.676	3	NC	1
427		5	max	.007	3	.01	2	.006	4	4.368e-5	1	NC	4	NC	1
428			min	-.007	2	-.01	3	-.002	3	-3.549e-5	3	1514.54	3	9783.442	3
429		6	max	.007	3	.015	2	.008	4	2.884e-5	1	NC	4	NC	1
430			min	-.007	2	-.015	3	-.003	3	-4.354e-5	3	1316.555	3	8526.611	3
431		7	max	.007	3	.019	2	.01	4	1.4e-5	1	NC	4	NC	1
432			min	-.007	2	-.019	3	-.004	3	-5.16e-5	3	1196.168	2	7806.666	3
433		8	max	.007	3	.022	2	.012	4	-2.295e-7	10	NC	4	NC	1
434			min	-.007	2	-.021	3	-.004	3	-5.965e-5	3	1104.749	2	6257.127	4
435		9	max	.007	3	.024	2	.015	4	1.261e-6	10	NC	4	NC	1
436			min	-.007	2	-.023	3	-.005	3	-6.77e-5	3	1050.623	2	4624.034	4
437		10	max	.007	3	.024	2	.017	4	2.752e-6	10	NC	4	NC	1
438			min	-.007	2	-.023	3	-.005	3	-7.575e-5	3	1025.619	2	3597.399	4
439		11	max	.007	3	.024	2	.021	5	4.243e-6	10	NC	4	NC	1
440			min	-.007	2	-.022	3	-.005	3	-8.381e-5	3	1026.797	2	2907.893	4
441		12	max	.007	3	.022	2	.024	5	5.734e-6	10	NC	4	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
442			min	-.007	2	-.02	3	-.004	3	-9.186e-5	3	1055.346	2	2415.793	5
443		13	max	.007	3	.02	2	.027	5	7.225e-6	10	NC	4	NC	1
444			min	-.007	2	-.017	3	-.004	3	-9.991e-5	3	1117.233	2	2054.594	5
445		14	max	.007	3	.016	2	.031	5	8.716e-6	10	NC	4	NC	1
446			min	-.007	2	-.014	3	-.003	3	-1.08e-4	3	1226.224	2	1785.825	5
447		15	max	.007	3	.01	2	.034	5	1.021e-5	10	NC	4	NC	1
448			min	-.007	2	-.009	3	-.003	3	-1.16e-4	3	1412.529	2	1581.044	5
449		16	max	.007	3	.004	2	.037	5	9.804e-5	5	NC	4	NC	1
450			min	-.007	2	-.003	3	-.002	3	-1.172e-4	3	1750.005	2	1422.237	5
451		17	max	.007	3	.003	3	.041	5	3.922e-3	4	NC	4	NC	1
452			min	-.007	2	-.005	2	-.001	1	-4.946e-5	9	2474.638	2	1297.421	5
453		18	max	.007	3	.01	3	.044	5	1.944e-3	5	NC	4	NC	1
454			min	-.007	2	-.014	2	0	9	-3.259e-3	2	4792.665	2	1195.534	4
455		19	max	.007	3	.018	3	.047	4	3.526e-3	3	NC	1	NC	1
456			min	-.007	2	-.024	2	0	9	-6.575e-3	2	NC	1	1112.034	4
457	M13	1	max	0	9	.022	3	.007	3	3.594e-3	3	NC	1	NC	1
458			min	-.005	5	-.019	2	-.007	2	-3.088e-3	2	NC	1	NC	1
459		2	max	0	9	.052	3	.005	3	4.427e-3	3	NC	4	NC	1
460			min	-.005	5	-.04	2	-.007	2	-3.807e-3	2	2732.871	3	NC	1
461		3	max	0	9	.079	3	.005	3	5.259e-3	3	NC	4	NC	1
462			min	-.005	5	-.058	2	-.007	2	-4.525e-3	2	1476.257	3	NC	1
463		4	max	0	9	.097	3	.006	3	6.092e-3	3	NC	4	NC	1
464			min	-.005	5	-.072	2	-.008	2	-5.243e-3	2	1114.718	3	NC	1
465		5	max	0	9	.106	3	.008	3	6.925e-3	3	NC	4	NC	1
466			min	-.005	5	-.079	2	-.01	2	-5.961e-3	2	993.686	3	NC	1
467		6	max	0	9	.106	3	.01	3	7.758e-3	3	NC	4	NC	1
468			min	-.005	5	-.08	2	-.013	2	-6.68e-3	2	994.828	3	NC	1
469		7	max	0	9	.099	3	.013	3	8.591e-3	3	NC	4	NC	1
470			min	-.005	5	-.076	2	-.016	2	-7.398e-3	2	1096.122	3	NC	1
471		8	max	0	9	.086	3	.015	3	9.424e-3	3	NC	4	NC	1
472			min	-.005	5	-.068	2	-.019	2	-8.116e-3	2	1307.133	3	7222.954	2
473		9	max	0	9	.074	3	.018	3	1.026e-2	3	NC	4	NC	1
474			min	-.005	5	-.061	2	-.022	2	-8.834e-3	2	1614.45	3	5887.846	2
475		10	max	0	9	.068	3	.02	3	1.109e-2	3	NC	4	NC	4
476			min	-.005	5	-.057	2	-.023	2	-9.553e-3	2	1817.769	3	5458.303	2
477		11	max	0	9	.074	3	.021	3	1.026e-2	3	NC	4	NC	1
478			min	-.005	5	-.061	2	-.022	2	-8.834e-3	2	1614.449	3	5855.201	3
479		12	max	0	9	.086	3	.022	3	9.428e-3	3	NC	4	NC	1
480			min	-.005	5	-.068	2	-.019	2	-8.116e-3	2	1307.132	3	5762.353	3
481		13	max	0	9	.099	3	.021	3	8.598e-3	3	NC	4	NC	1
482			min	-.005	5	-.076	2	-.016	2	-7.398e-3	2	1096.121	3	6108.336	3
483		14	max	0	9	.107	3	.019	3	7.767e-3	3	NC	4	NC	1
484			min	-.005	5	-.08	2	-.013	2	-6.68e-3	2	994.827	3	6957.784	3
485		15	max	0	9	.107	3	.017	3	6.937e-3	3	NC	4	NC	1
486			min	-.005	5	-.079	2	-.01	2	-5.962e-3	2	993.685	3	8595.279	3
487		16	max	0	9	.098	3	.014	3	6.106e-3	3	NC	4	NC	1
488			min	-.005	5	-.072	2	-.008	2	-5.243e-3	2	1114.717	3	NC	1
489		17	max	0	9	.079	3	.011	3	5.276e-3	3	NC	4	NC	1
490			min	-.005	5	-.058	2	-.007	2	-4.525e-3	2	1476.256	3	NC	1
491		18	max	0	9	.053	3	.009	3	4.445e-3	3	NC	4	NC	1
492			min	-.005	5	-.04	2	-.007	2	-3.807e-3	2	2732.87	3	NC	1
493		19	max	0	9	.022	3	.007	3	3.614e-3	3	NC	1	NC	1
494			min	-.005	5	-.019	2	-.007	2	-3.089e-3	2	NC	1	NC	1
495	M16	1	max	0	9	.018	3	.007	3	3.824e-3	2	NC	1	NC	1
496			min	-.047	4	-.024	2	-.007	2	-2.818e-3	3	NC	1	NC	1
497		2	max	0	9	.034	3	.009	3	4.715e-3	2	NC	4	NC	1
498			min	-.047	4	-.054	2	-.007	2	-3.434e-3	3	2821.419	2	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
499		3	max	0	9	.048	3	.011	3	5.606e-3	2	NC	4	NC	1
500			min	-.047	4	-.079	2	-.007	2	-4.05e-3	3	1519.651	2	NC	1
501		4	max	0	9	.058	3	.014	3	6.498e-3	2	NC	4	NC	1
502			min	-.047	4	-.098	2	-.008	2	-4.667e-3	3	1141.714	2	NC	1
503		5	max	0	9	.064	3	.016	3	7.389e-3	2	NC	4	NC	1
504			min	-.047	4	-.107	2	-.01	2	-5.283e-3	3	1009.842	2	9242.149	3
505		6	max	0	9	.066	3	.018	3	8.28e-3	2	NC	4	NC	1
506			min	-.047	4	-.108	2	-.013	2	-5.899e-3	3	999.193	2	7671.601	3
507		7	max	0	9	.064	3	.019	3	9.172e-3	2	NC	4	NC	1
508			min	-.047	4	-.102	2	-.016	2	-6.516e-3	3	1081.706	2	6815.64	3
509		8	max	0	9	.059	3	.02	3	1.006e-2	2	NC	4	NC	1
510			min	-.047	4	-.091	2	-.019	2	-7.132e-3	3	1257.149	2	6410.501	3
511		9	max	0	9	.055	3	.02	3	1.095e-2	2	NC	4	NC	4
512			min	-.047	4	-.08	2	-.022	2	-7.748e-3	3	1503.113	2	5877.251	2
513		10	max	0	9	.052	3	.019	3	1.185e-2	2	NC	4	NC	4
514			min	-.047	4	-.075	2	-.023	2	-8.365e-3	3	1658.949	2	5449.007	2
515		11	max	0	9	.055	3	.018	3	1.095e-2	2	NC	4	NC	4
516			min	-.047	4	-.08	2	-.022	2	-7.746e-3	3	1503.113	2	5877.26	2
517		12	max	0	9	.059	3	.017	3	1.006e-2	2	NC	4	NC	1
518			min	-.047	4	-.091	2	-.019	2	-7.128e-3	3	1257.149	2	7207.94	2
519		13	max	0	9	.064	3	.015	3	9.172e-3	2	NC	4	NC	1
520			min	-.047	4	-.102	2	-.016	2	-6.509e-3	3	1081.706	2	9635.039	3
521		14	max	0	9	.066	3	.014	3	8.281e-3	2	NC	4	NC	1
522			min	-.047	4	-.108	2	-.013	2	-5.891e-3	3	999.193	2	NC	1
523		15	max	0	9	.064	3	.012	3	7.39e-3	2	NC	4	NC	1
524			min	-.047	4	-.107	2	-.01	2	-5.273e-3	3	1009.842	2	NC	1
525		16	max	0	9	.058	3	.01	3	6.499e-3	2	NC	4	NC	1
526			min	-.047	4	-.098	2	-.008	2	-4.654e-3	3	1141.714	2	NC	1
527		17	max	0	9	.048	3	.009	3	5.608e-3	2	NC	4	NC	1
528			min	-.047	4	-.079	2	-.007	2	-4.036e-3	3	1519.651	2	NC	1
529		18	max	0	9	.034	3	.008	3	4.716e-3	2	NC	4	NC	1
530			min	-.047	4	-.054	2	-.007	2	-3.417e-3	3	2821.419	2	NC	1
531		19	max	0	9	.018	3	.007	3	3.825e-3	2	NC	1	NC	1
532			min	-.047	4	-.024	2	-.007	2	-2.799e-3	3	NC	1	NC	1
533	M15	1	max	0	1	0	1	0	1	3.745e-4	3	NC	1	NC	1
534			min	0	1	0	1	0	1	-5.435e-4	5	NC	1	NC	1
535		2	max	0	3	0	5	.003	4	7.385e-4	3	NC	1	NC	1
536			min	0	4	-.001	1	0	3	-5.51e-4	5	NC	1	NC	1
537		3	max	0	3	.001	5	.007	4	1.103e-3	3	NC	1	NC	1
538			min	0	4	-.002	1	-.003	3	-7.518e-4	2	NC	1	8474.941	4
539		4	max	0	3	.002	5	.01	4	1.467e-3	3	NC	1	NC	9
540			min	-.001	4	-.004	1	-.006	3	-1.109e-3	2	NC	1	5451.105	4
541		5	max	0	3	.002	5	.014	4	1.831e-3	3	NC	1	NC	9
542			min	-.002	4	-.005	1	-.01	3	-1.466e-3	2	NC	1	3613.336	3
543		6	max	0	3	.003	5	.017	4	2.195e-3	3	NC	3	NC	9
544			min	-.002	4	-.005	1	-.014	3	-1.823e-3	2	9409.995	1	2629.444	3
545		7	max	0	3	.003	5	.019	4	2.559e-3	3	NC	3	8007.131	9
546			min	-.002	4	-.006	1	-.019	3	-2.18e-3	2	8344.968	1	2054.632	3
547		8	max	0	3	.003	5	.021	4	2.923e-3	3	NC	3	6655.587	9
548			min	-.003	4	-.006	1	-.024	3	-2.538e-3	2	7705.791	1	1693.512	3
549		9	max	0	3	.004	5	.022	2	3.287e-3	3	NC	4	5765.616	9
550			min	-.003	4	-.007	1	-.028	3	-2.895e-3	2	7361.749	1	1457.288	3
551		10	max	0	3	.004	5	.024	2	3.651e-3	3	NC	4	5176.916	9
552			min	-.003	4	-.007	9	-.031	3	-3.252e-3	2	7252.91	1	1301.399	3
553		11	max	0	3	.004	5	.026	2	4.015e-3	3	NC	4	5170.668	15
554			min	-.004	4	-.007	9	-.033	3	-3.609e-3	2	7361.749	1	1202.46	3
555		12	max	0	3	.005	5	.026	2	4.379e-3	3	NC	3	5914.856	15

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
556			min	-.004	4	-.006	9	-.034	3	-3.966e-3	2	7705.791	1	1148.861	3
557		13	max	.001	3	.005	5	.025	2	4.743e-3	3	NC	3	7240.164	15
558			min	-.005	4	-.006	9	-.033	3	-4.323e-3	2	8344.968	1	1137.208	3
559		14	max	.001	3	.005	5	.023	1	5.107e-3	3	NC	3	9703.707	15
560			min	-.005	4	-.005	9	-.03	3	-4.68e-3	2	9409.995	1	1172.426	3
561		15	max	.001	3	.005	5	.019	1	5.471e-3	3	NC	1	NC	7
562			min	-.005	4	-.005	9	-.025	3	-5.038e-3	2	NC	1	1272.699	3
563		16	max	.001	3	.005	5	.014	1	5.836e-3	3	NC	1	NC	5
564			min	-.006	4	-.004	9	-.017	3	-5.395e-3	2	NC	1	1487.449	3
565		17	max	.001	3	.005	5	.006	1	6.2e-3	3	NC	1	NC	4
566			min	-.006	4	-.003	9	-.007	3	-5.752e-3	2	NC	1	1971.769	3
567		18	max	.002	3	.005	5	.007	3	6.564e-3	3	NC	1	NC	4
568			min	-.006	4	-.002	9	-.009	2	-6.109e-3	2	NC	1	3510.259	3
569		19	max	.002	3	.005	2	.024	3	6.928e-3	3	NC	1	NC	1
570			min	-.007	4	0	9	-.024	2	-6.466e-3	2	NC	1	NC	1
571	M16A	1	max	.001	2	.002	2	.008	3	1.995e-3	3	NC	1	NC	1
572			min	-.002	4	-.003	4	-.008	2	-2.076e-3	2	NC	1	NC	1
573		2	max	.001	2	0	2	.001	3	1.919e-3	3	NC	1	NC	1
574			min	-.002	4	-.006	4	-.003	2	-1.98e-3	2	NC	1	9670.084	3
575		3	max	0	2	-.001	10	.003	1	1.843e-3	3	NC	1	NC	4
576			min	-.002	4	-.008	4	-.004	5	-1.883e-3	2	NC	1	5472.584	3
577		4	max	0	2	-.002	10	.005	1	1.768e-3	3	NC	1	NC	4
578			min	-.002	4	-.01	4	-.007	3	-1.787e-3	2	7319.697	4	4163.396	3
579		5	max	0	2	-.003	12	.007	1	1.692e-3	3	NC	1	NC	9
580			min	-.002	4	-.012	4	-.01	5	-1.691e-3	2	5711.633	4	3596.776	3
581		6	max	0	2	-.003	12	.008	1	1.616e-3	3	NC	3	NC	9
582			min	-.002	4	-.014	4	-.013	5	-1.595e-3	2	4806.943	4	3350.305	3
583		7	max	0	2	-.004	12	.008	1	1.54e-3	3	NC	3	NC	9
584			min	-.002	4	-.015	4	-.016	5	-1.499e-3	2	4262.891	4	3291.794	3
585		8	max	0	2	-.004	12	.008	1	1.464e-3	3	NC	3	NC	9
586			min	-.001	4	-.016	4	-.019	5	-1.403e-3	2	3936.379	4	3155.261	5
587		9	max	0	2	-.004	12	.008	1	1.388e-3	3	NC	12	NC	9
588			min	-.001	4	-.017	4	-.02	5	-1.307e-3	2	3760.63	4	2838.517	5
589		10	max	0	2	-.004	12	.007	1	1.312e-3	3	NC	12	NC	9
590			min	-.001	4	-.017	4	-.022	5	-1.211e-3	2	3705.032	4	2678.642	5
591		11	max	0	2	-.004	12	.006	1	1.236e-3	3	NC	12	NC	9
592			min	-.001	4	-.016	4	-.022	5	-1.115e-3	2	3760.63	4	2641.779	5
593		12	max	0	2	-.004	12	.005	1	1.16e-3	3	NC	3	NC	9
594			min	0	4	-.015	4	-.021	5	-1.019e-3	2	3936.379	4	2721.564	5
595		13	max	0	2	-.004	12	.004	1	1.084e-3	3	NC	3	NC	1
596			min	0	4	-.014	4	-.019	5	-9.228e-4	2	4262.891	4	2936.569	5
597		14	max	0	2	-.003	12	.003	1	1.008e-3	3	NC	3	NC	1
598			min	0	4	-.012	4	-.017	5	-8.267e-4	2	4806.943	4	3340.943	5
599		15	max	0	2	-.003	12	.001	1	9.325e-4	3	NC	1	NC	1
600			min	0	4	-.01	4	-.014	5	-7.307e-4	2	5711.633	4	4060.64	5
601		16	max	0	2	-.002	12	0	9	8.565e-4	3	NC	1	NC	1
602			min	0	4	-.008	4	-.011	5	-6.346e-4	2	7319.697	4	5409.673	5
603		17	max	0	2	-.001	12	0	9	7.806e-4	3	NC	1	NC	1
604			min	0	4	-.006	4	-.007	5	-5.385e-4	2	NC	1	8365.407	5
605		18	max	0	2	0	12	0	3	8.181e-4	4	NC	1	NC	1
606			min	0	4	-.003	4	-.003	5	-4.425e-4	2	NC	1	NC	1
607		19	max	0	1	0	1	0	1	8.758e-4	4	NC	1	NC	1
608			min	0	1	0	1	0	1	-3.464e-4	2	NC	1	NC	1

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

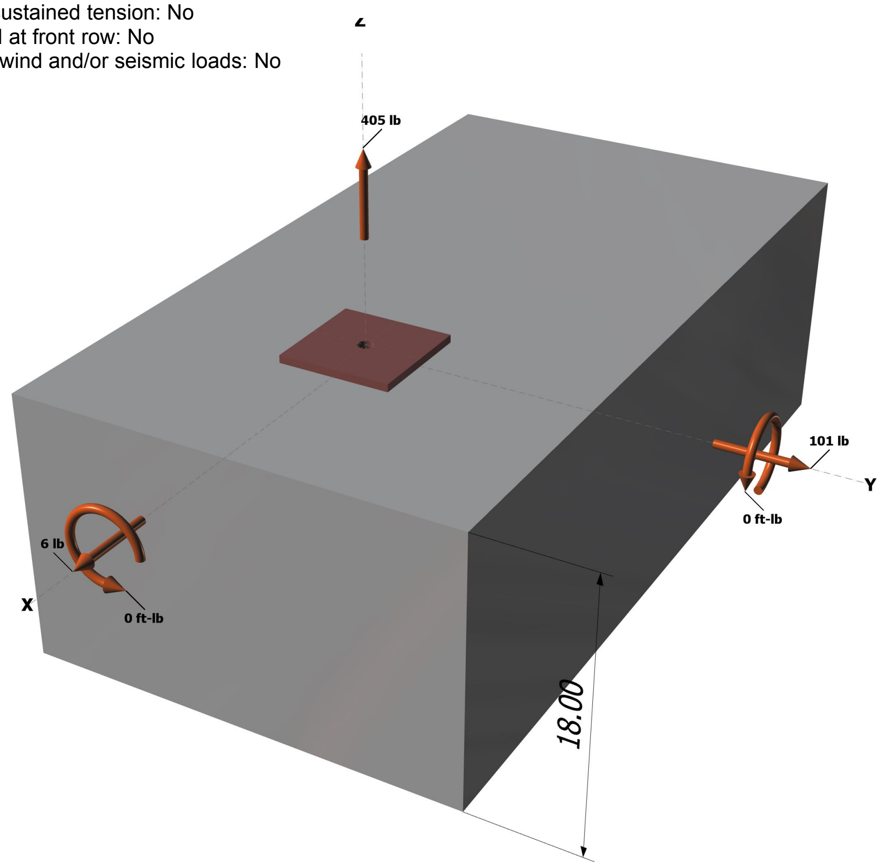
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 4.00 x 4.00 x 0.28

<Figure 1>



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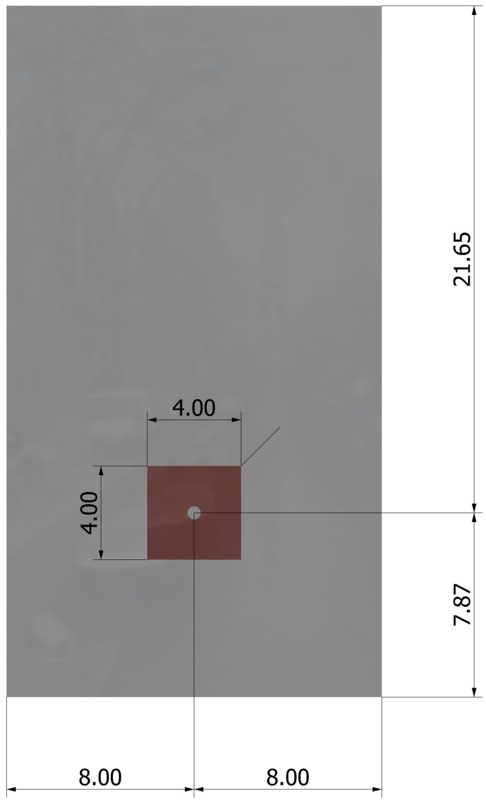


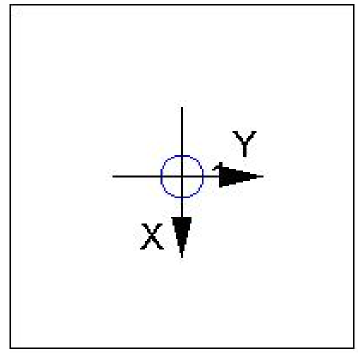
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	405.0	6.0	101.0	101.2
Sum	405.0	6.0	101.0	101.2

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 405
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cb} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-4)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cb} (lb)
253.92	256.00	0.995	1.00	1.000	10469	0.65	6717

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_a = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16a)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	ϕ	ϕN_a (lb)
109.66	109.66	1.000	1.000	9755	0.55	5365

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in y-direction:

$V_{by} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cby} = \phi\,(A_{Vc}/A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cby} (lb)
238.44	288.00	0.897	1.000	1.000	8488	0.70	4411

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cbx} = \phi\,(A_{Vc}/A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
188.88	278.72	0.903	1.000	1.000	8282	0.70	3549

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbx} = \phi\,(2)(A_{Vc}/A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
238.44	288.00	1.000	1.000	1.000	8488	0.70	9838

Shear parallel to edge in y-direction:

$V_{bx} = 7(l_e/d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	7.87	8282

$\phi V_{cby} = \phi\,(2)(A_{Vc}/A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cby} (lb)
188.88	278.72	1.000	1.000	1.000	8282	0.70	7858

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cp} = \phi\min|k_{cp}N_a\,;\,k_{cp}N_{cb}| = \phi\min|k_{cp}(A_{Na}/A_{Na0})\Psi_{ed,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc}/A_{Nco})\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30a)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	109.66	109.66	1.000	1.000	9755	9755

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ	ϕV_{cp} (lb)
253.92	256.00	0.995	1.000	1.000	10469	10334	0.70	13657

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, øN_n (lb)	Ratio	Status
Steel	405	6071	0.07	Pass
Concrete breakout	405	6717	0.06	Pass
Adhesive	**405**	**5365**	**0.08**	**Pass (Governs)**

Shear	Factored Load, V_{ua} (lb)	Design Strength, øV_n (lb)	Ratio	Status
Steel	**101**	**3156**	**0.03**	**Pass (Governs)**
T Concrete breakout y+	101	4411	0.02	Pass
T Concrete breakout x+	6	3549	0.00	Pass
|| Concrete breakout y+	6	9838	0.00	Pass
|| Concrete breakout x+	101	7858	0.01	Pass
Concrete breakout, combined	-	-	0.02	Pass
Pryout	101	13657	0.01	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. D.7.1	0.08	0.00	7.5 %	1.0	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.

Company:	Schletter, Inc.	Date:	12/10/2015
Engineer:	HCV	Page:	1/5
Project:	Standard PVMini - Worst Case		
Address:			
Phone:			
E-mail:			

SIMPSON Strong-Tie®
Anchor Designer™ Software
Version 2.4.5673.0

1.Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General
Design method:ACI 318-05
Units: Imperial units

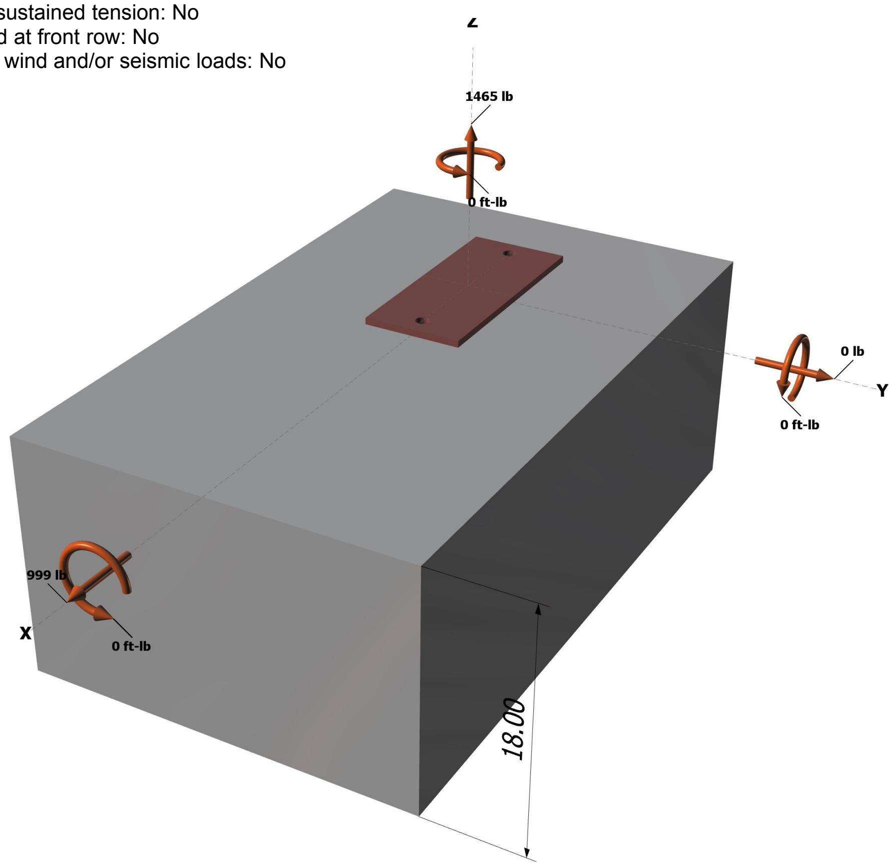
Anchor Information:
Anchor type: Bonded anchor
Material: A193 Grade B8/B8M (304/316SS)
Diameter (inch): 0.500
Effective Embedment depth, h_{ef} (inch): 6.000
Code report: IAPMO UES ER-263
Anchor category: -
Anchor ductility: Yes
h_{min} (inch): 8.50
c_{ac} (inch): 9.67
C_{min} (inch): 1.75
S_{min} (inch): 3.00

Load and Geometry
Load factor source: ACI 318 Section 9.2
Load combination: not set
Seismic design: No
Anchors subjected to sustained tension: No
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: No

Base Material
Concrete: Normal-weight
Concrete thickness, h (inch): 18.00
State: Cracked
Compressive strength, f'_c (psi): 2500
$\Psi_{c,V}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Do not evaluate concrete breakout in tension: No
Do not evaluate concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Periodic
Temperature range, Short/Long: 110/75°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate
Length x Width x Thickness (inch): 9.00 x 4.00 x 0.28

<Figure 1>



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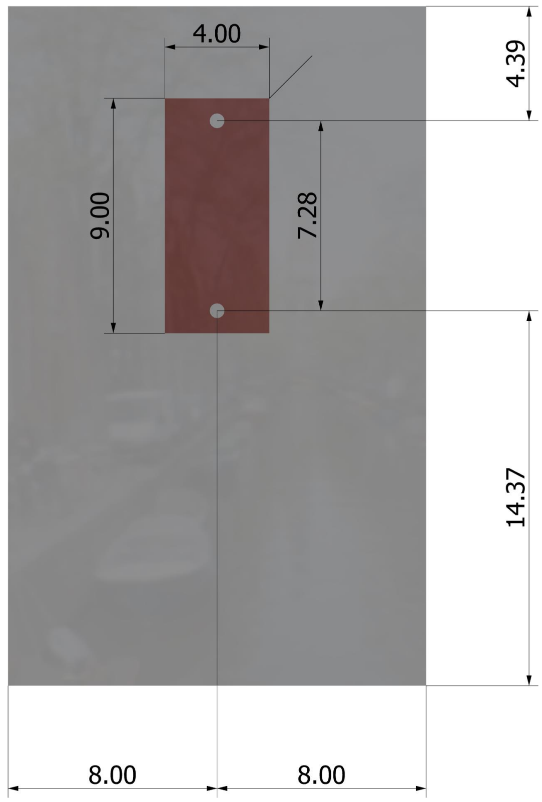


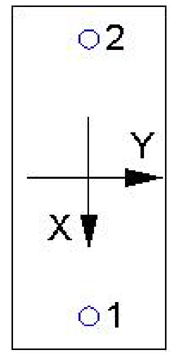
Recommended Anchor
Anchor Name: AT-XP® - AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS)
Code Report: IAPMO UES ER-263

3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)
1	732.5	499.5	0.0	499.5
2	732.5	499.5	0.0	499.5
Sum	1465.0	999.0	0.0	999.0

Maximum concrete compression strain (‰): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 1465
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension(Sec. D.5.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
8095	0.75	6071

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. D-7)

k_c	λ	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	2500	5.333	10469

$\phi N_{cbg} = \phi\,(A_{Nc} / A_{Nco})\,\Psi_{ec,N}\,\Psi_{ed,N}\,\Psi_{c,N}\,\Psi_{cp,N} N_b$ (Sec. D.4.1 & Eq. D-5)

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
314.72	256.00	1.000	0.865	1.00	1.000	10469	0.65	7233

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$\tau_{k,cr} = \tau_{k,cr} f_{short\text{-}term} K_{sat}$

$\tau_{k,cr}$ (psi)	$f_{short\text{-}term}$	K_{sat}	$\tau_{k,cr}$ (psi)
1035	1.00	1.00	1035

$N_{a0} = \tau_{k,cr} \pi d_a h_{ef}$ (Eq. D-16f)

$\tau_{k,cr}$ (psi)	d_a (in)	h_{ef} (in)	N_{a0} (lb)
1035	0.50	6.000	9755

$\phi N_{ag} = \phi\,(A_{Na} / A_{Na0})\,\Psi_{ed,Na}\,\Psi_{g,Na}\,\Psi_{ec,Na}\,\Psi_{p,Na} N_{a0}$ (Sec. D.4.1 & Eq. D-16b)

A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0}(lb)	ϕ	ϕN_{ag} (lb)
177.03	109.66	0.952	1.021	1.000	1.000	9755	0.55	8418

8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
4855	1.0	0.65	3156

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{bx} (lb)
4.00	0.50	1.00	2500	12.00	15593

$\phi V_{cbx} = \phi\,(A_{Vc} / A_{Vco})\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{bx}$ (Sec. D.4.1 & Eq. D-21)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
288.00	648.00	0.833	1.000	1.000	15593	0.70	4043

Shear parallel to edge in x-direction:

$V_{by} = 7(l_e / d_a)^{0.2}\sqrt{d_a}\lambda\sqrt{f'_c}c_{a1}^{1.5}$ (Eq. D-24)

l_e (in)	d_a (in)	λ	f'_c (psi)	c_{a1} (in)	V_{by} (lb)
4.00	0.50	1.00	2500	8.00	8488

$\phi V_{cbgx} = \phi\,(2)(A_{Vc} / A_{Vco})\Psi_{ec,V}\Psi_{ed,V}\Psi_{c,V}\Psi_{h,V}V_{by}$ (Sec. D.4.1, D.6.2.1(c) & Eq. D-22)

A_{Vc} (in^2)	A_{Vco} (in^2)	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
284.04	288.00	1.000	1.000	1.000	1.000	8488	0.70	11720

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$\phi V_{cpg} = \phi\,\min|k_{cp}N_{ag}\,;\,k_{cp}N_{cbg}| = \phi\,\min|k_{cp}(A_{Na} / A_{Na0})\Psi_{ed,Na}\Psi_{g,Na}\Psi_{ec,Na}\Psi_{p,Na}N_{a0}\,;\,k_{cp}(A_{Nc} / A_{Nco})\Psi_{ec,N}\Psi_{ed,N}\Psi_{c,N}\Psi_{cp,N}N_b|$ (Eq. D-30b)

k_{cp}	A_{Na} (in^2)	A_{Na0} (in^2)	$\Psi_{ed,Na}$	$\Psi_{g,Na}$	$\Psi_{ec,Na}$	$\Psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	177.03	109.66	0.952	1.021	1.000	1.000	9755	15305

A_{Nc} (in^2)	A_{Nco} (in^2)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
314.72	256.00	1.000	0.865	1.000	1.000	10469	11128	0.70

ϕV_{cpg} (lb)
15580

11. Results

Interaction of Tensile and Shear Forces (Sec. D.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	733	6071	0.12	Pass
Concrete breakout	**1465**	**7233**	**0.20**	**Pass (Governs)**
Adhesive	1465	8418	0.17	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	500	3156	0.16	Pass
T Concrete breakout x+	**999**	**4043**	**0.25**	**Pass (Governs)**
|| Concrete breakout y-	**999**	**11720**	**0.09**	**Pass (Governs)**
Pryout	999	15580	0.06	Pass

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status

Sec. D.7.3	0.20	0.25	45.0 %	1.2	Pass

AT-XP w/ 1/2"Ø A193 Gr. B8/B8M (304/316SS) with hef = 6.000 inch meets the selected design criteria.

12. Warnings

- This temperature range is currently outside the scope of ACI 318-11 and ACI 355.4, and is provided for historical purposes.

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.