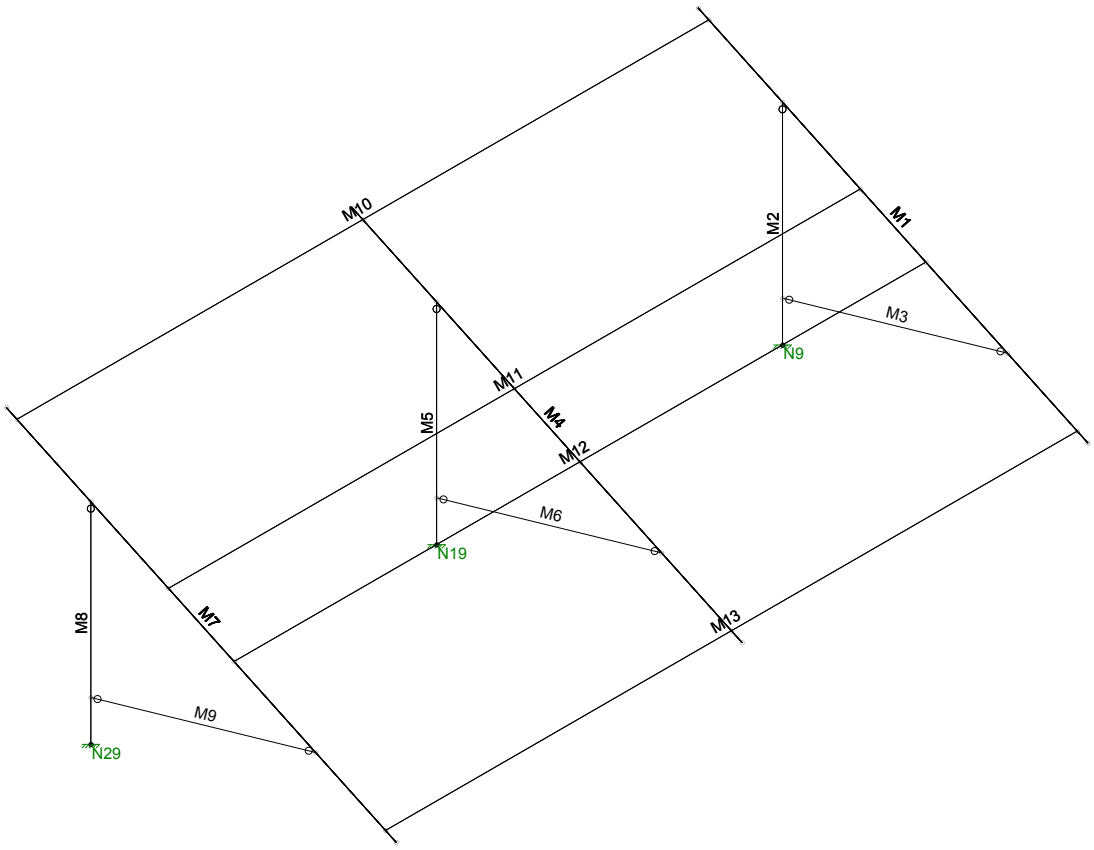


Schletter, Inc.		25° Tilt w/o Seismic Design
HCV	Standard FS Racking System	
	Representative Calculations - ASCE 7-05	

1. INTRODUCTION

1.1 Project Description

The following sections will cover the determination of forces and structural design calculations for the Schletter, Inc. FS ground mount system.

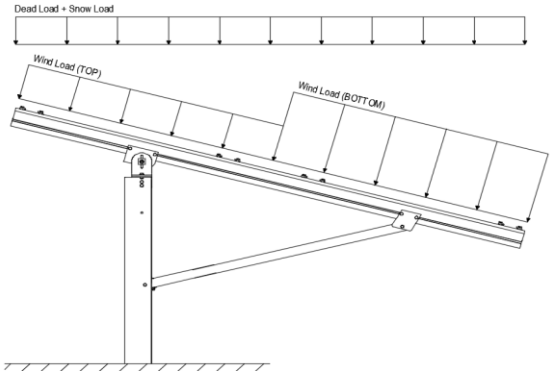
1.2 Construction

Photovoltaic modules are attached to aluminum purlins using clamp fasteners. Purlins are clamped to inclined aluminum girders, which are then connected to galvanized steel posts. Each support structure is equally spaced.

PV modules are required to meet the following specifications:

	Maximum		Minimum	
Height =	2000	mm	1900	mm
Width =	1050	mm	970	mm
Dead Load =	3.00	psf	1.75	psf

Modules Per Row =	2
Module Tilt =	25°
Maximum Height Above Grade =	3 ft



Typical loading conditions of the module dead loads, snow loads, and wind loads are shown on the left.

1.3 Technical Codes

- ASCE 7-05 - Chapter 6, Wind Loads
- ASCE 7-05 - Chapter 7, Snow Loads
- ASCE 7-05 - Chapter 2, Combination of Loads
- International Building Code, IBC, 2003, 2006, 2009
- Aluminum Design Manual, Eighth Edition, 2005

2. LOAD ACTIONS

2.1 Permanent Loads

g_{MAX} =	3.00	psf	*Self-weight of the PV modules.*
g_{MIN} =	1.75	psf	

2.2 Snow Loads

Ground Snow Load, P_g =	30.00	psf	
Sloped Roof Snow Load, P_s =	18.56	psf	*(ASCE 7-05, Eq. 7-2)*
I_s =	1.00		
C_s =	0.82		
C_e =	0.90		
C_t =	1.20		

2.3 Wind Loads

Design Wind Speed, V =	85	mph	Exposure Category = C
Height <	15	ft	Importance Category = II

Peak Velocity Pressure, q_z = 11.34 psf *Including the gust factor, G=0.85. (ASCE 7-05, Eq. 6-15)*

Pressure Coefficients

$Cf+_{TOP}$ =	1.1	*(Pressure)*	*Provided pressure coefficients are the result of wind tunnel testing done by Ruscheweyh Consult. Coefficients are located in test report # 1127/0510-e. Negative forces are applied away from the surface.*
$Cf+_{BOTTOM}$ =	1.7		
$Cf-_{TOP}$ =	-2.2	*(Suction)*	
$Cf-_{BOTTOM}$ =	-1		

2.4 Seismic Loads - N/A

S_S =	0.00		R =	1.25	*ASCE 7, Section 12.8.1.3: A maximum S_s of 1.5 may be used to calculate the base shear, C_s, of structures under five stories and with a period, T, of 0.5 or less. Therefore, a S_{ds} of 1.0 was used to calculate C_s.*
S_{DS} =	0.00		C_S =	0	
S_1 =	0.00		ρ =	1.3	
S_{D1} =	0.00		Ω =	1.25	
T_a =	0.00		C_d =	1.25	

2.5 Combination of Loads

ASCE 7 requires that all structures be checked by specified combinations of loads. Applicable load combinations are provided below.

Strength Design, LRFD

Component stresses are checked using the following LRFD load combinations:

1.2D + 1.6S + 0.8W
1.2D + 1.6W + 0.5S
0.9D + 1.6W [M]
1.54D + 1.3E + 0.2S [R]
0.56D + 1.3E [R]
1.54D + 1.25E + 0.2S [O]
0.56D + 1.25E [O]

(ASCE 7, Eq 2.3.2-1 through 2.3.2-7) & (ASCE 7, Section 12.4.3.2)

Allowable Stress Design, ASD

Member deflection checks and foundation designs are done according to the following ASD load combinations:

1.0D + 1.0S
1.0D + 1.0W
1.0D + 0.75L + 0.75W + 0.75S
0.6D + 1.0W [M]
1.238D + 0.875E [O]
1.1785D + 0.65625E + 0.75S [O]
0.362D + 0.875E [O]

(ASCE 7, Eq 2.4.1-1 through 2.4.1-8) & (ASCE 7, Section 12.4.3.2)

[M] *Uses the minimum allowable module dead load.*
[R] *Include redundancy factor of 1.3.*
[O] *Includes overstrength factor of 1.25. Used to check seismic drift.*

3. STRUCTURAL ANALYSIS

3.1 RISA Results

Appendix B.1 contains outputs from the structural analysis software package, RISA. These outputs are used to accurately determine resultant member and reaction forces from the loads seen throughout Section 2.

3.2 RISA Components

A member and node list has been provided below to correlate the RISA components with the design calculations in Section 4. Items of significance have been listed.

Purlins	Location
M10	Top
M11	Mid-Top
M12	Mid-Bottom
M13	Bottom

Posts	Location
M2	Outer
M5	Inner
M8	Outer

Girders	Location
M1	Outer
M4	Inner
M7	Outer

Reactions	Location
N9	Outer
N19	Inner
N29	Outer

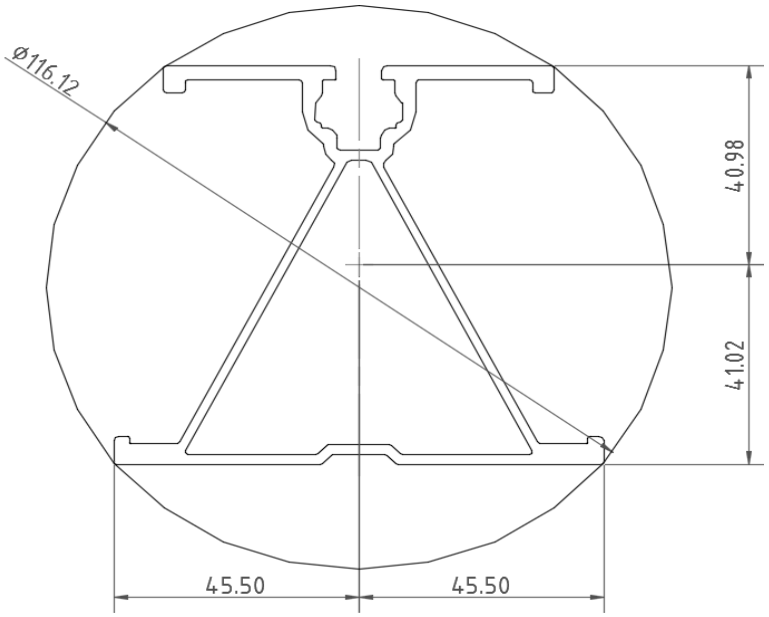
Struts	Location
M3	Outer
M6	Inner
M9	Outer

4. MEMBER DESIGN CALCULATIONS

4.1 Purlin Design

Aluminum purlins are used to transfer loads to the support structure. Purlins are designed as continous beams with cantilevers. These are considered beams with internal hinges that can be joined with splices at 25% of the support respective span. See Appendix A.1 for detailed member calculations. Section units are in (mm).

Purlin Type =	**S1.5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	114	in
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	25.07	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	23.08	ksi
S_y =	1.33	in^3
S_x =	0.6	in^3
E =	10100	ksi
I_y =	2.16	in^4
I_x =	1.07	in^4
A =	1.25	in^2
g =	1.50	lbs/ft
M_y =	1.403	k-ft
M_z =	0.174	k-ft
$M_{y\ allowable}$ =	2.779	k-ft
$M_{z\ allowable}$ =	1.154	k-ft
Utilization =	66%	

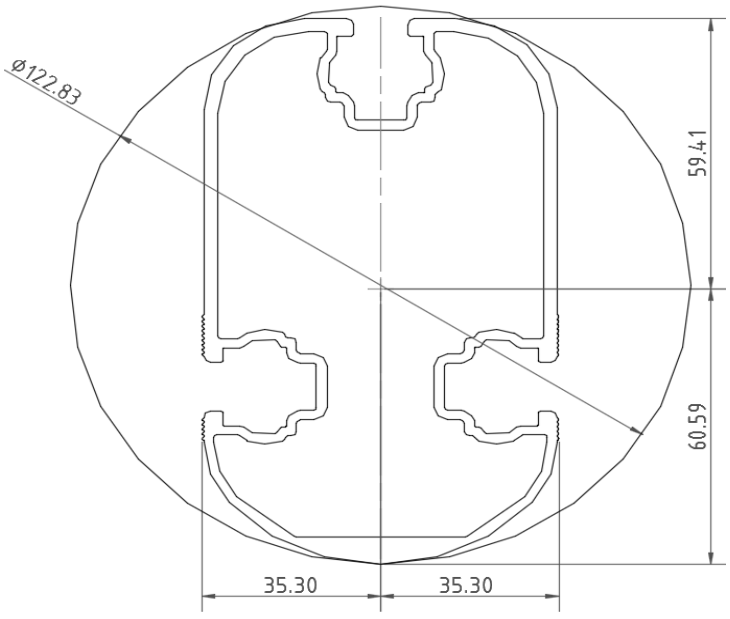


DETAIL VIEW

4.2 Girder Design

Loads from purlins are transferred to the posts using an inclined girder, which is connected to the steel post. Loads on the girder result from the support reactions of the purlins. See Appendix A.2 for detailed member calculations. Section units are in (mm).

Girder Type =	**T5**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	81.77	in
$\Phi F_{ty\ AXIAL}$ =	30.80	ksi
$\Phi F_{ty\ STRONG\text{-}AXIS}$ =	30.06	ksi
$\Phi F_{ty\ WEAK\text{-}AXIS}$ =	31.56	ksi
S_y =	1.98	in^3
S_x =	1.32	in^3
E =	10100	ksi
I_y =	4.74	in^4
I_x =	1.83	in^4
A =	1.93	in^2
g =	2.32	lbs/ft
M_y =	3.148	k-ft
M_z =	0.000	k-ft
P_n =	4.556	k
$M_{y\ allowable}$ =	4.960	k-ft
$M_{z\ allowable}$ =	3.472	k-ft
$P_{n\ allowable}$ =	59.439	k
Utilization =	71%	

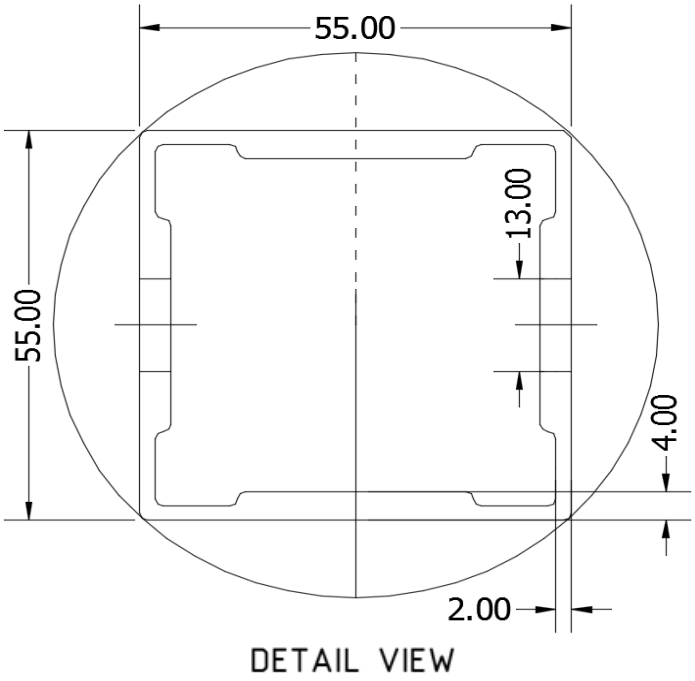


DETAIL VIEW

4.3 Strut Design

The aluminum strut connects a portion of the girder to the galvanized steel post. Girder forces are then transferred down through the strut into the post. The strut is attached with single M10 bolts at each end. See Appendix A.3 for detailed member calculations. Section units are in (mm).

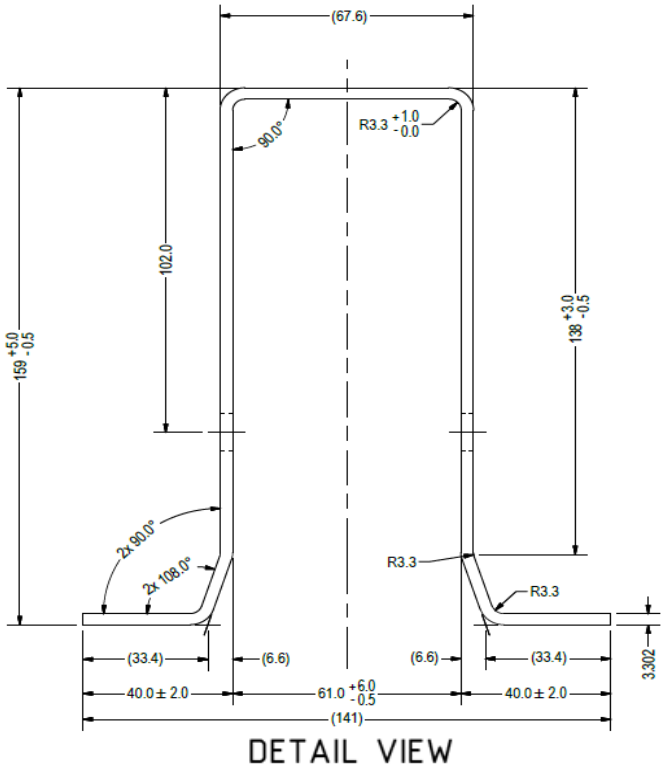
Strut Type =	**55x55**	
Aluminum Type =	6105-T5	
F_{ty} =	35	ksi
L_b =	74.80	in
$\Phi F_{ty\ AXIAL}$ =	9.61	ksi
$\Phi F_{ty\ BENDING}$ =	28.22	ksi
S_y =	0.60	in^3
S_x =	0.60	in^3
E =	10100	ksi
I_y =	0.67	in^4
I_x =	0.67	in^4
A =	0.98	in^2
g =	1.18	lbs/ft
M_y =	0.007	k-ft
M_z =	0.000	k-ft
P_n =	4.678	k
$M_{y\ allowable}$ =	1.408	k-ft
$M_{z\ allowable}$ =	1.408	k-ft
$P_{n\ allowable}$ =	9.441	k
Utilization =	50%	



4.4 Post Design

Galvanized steel posts are a roll formed steel section, that are either ram driven into the ground or placed in a concrete foundation at a defined depth. Embedment depths will be provided on the structural drawings or through a geotechnical testing report. See Appendix A.4 for detailed member calculations. Section units are in (mm).

Post Type =	**FG8**	
Steel Type =	J2340	
F_{ty} =	60	ksi
L_b =	81.31	in
Φ =	0.90	
ΦF_{ty} =	54.00	ksi
S_y =	3.46	in^3
S_x =	1.55	in^3
E =	29000	ksi
I_y =	10.94	in^4
I_x =	4.31	in^4
A =	2.23	in^2
g =	7.59	lbs/ft
M_y =	14.764	k-ft
M_z =	0.000	k-ft
P_r =	6.134	k
$M_{y\ allowable}$ =	19.207	k-ft
$M_{z\ allowable}$ =	14.389	k-ft
P_c =	30.879	k
Utilization =	98%	



5. FOUNDATION DESIGN CALCULATIONS

5.1 Rammed Post Foundations

The following LRFD loads include a safety factor of 1.3, and are to be used in conjunction with a Schletter, Inc. Geotechnical Investigation Report. The forces below should fall within the guidelines provided in the Geotechnical Investigation Report. If a Geotechnical Investigation Report is not present, please proceed to Section 5.2 for a concrete footing design.

Maximum Tensile Load =	4.62	k
Maximum Lateral Load =	2.54	k

5.2 Design of Drilled Shaft Foundations

The galvanized steel post is to be embedded into a cylindrical drilled shaft foundation. For the purpose of design, the post is considered to be fixed to the ground. The applicable lateral force, uplift, and compression resistance checks are seen below.

5.3 Lateral Force Resistance

The equivalent lateral force is applied at the top of the post to determine the required embedment depth. A lateral soil bearing capacity for clay is assumed. Footing is unrestrained at ground level. (IBC, Eq. 18-1)

Lateral Force @ Top of Pole, P =	1.43	k
Height of Pole Above Grade, H =	5.78	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.10	ksf/ft
Isolated Pole Factor, F =	2	
First Trial Depth, D =	3.25	ft

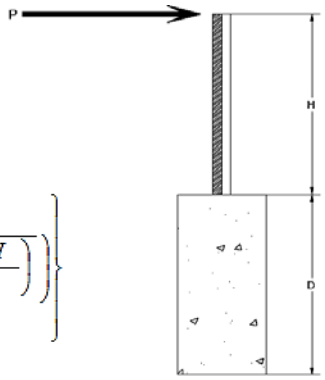
Lateral Bearing @ Bottom =	S_3
Lateral Bearing @ D/3 =	S_1
Required Depth =	D

$$S_3 = Min\ (D, 12')$$

$$S_1 = Min\left(\frac{D}{3}, 12'\right)$$

$$A = 2.34\ P/S_1 B$$

$$D = \left\{0.5A\left(1+\sqrt{1+\left(\frac{4.36\ H}{A}\right)}\right)\right\}$$



Non-Constrained

Lateral Force @ Top of Pole, P =	1.43	k
Height of Pole Above Grade, H =	5.78	ft
Diameter of Pole Footing, B =	2.00	ft
Lateral Soil Bearing Capacity, S =	0.20	ksf/ft

1st Trial @ D_1 =	3.25	ft
Lateral Soil Bearing @ D/3, S_1 =	0.22	ksf
Lateral Soil Bearing @ D, S_3 =	0.65	ksf
Constant 2.34P/(S_1B), A =	7.74	
Required Footing Depth, D =	11.85	ft

2nd Trial @ D_2 =	7.55	ft
Lateral Soil Bearing @ D/3, S_1 =	0.50	ksf
Lateral Soil Bearing @ D, S_3 =	1.51	ksf
Constant 2.34P/(S_1B), A =	3.33	
Required Footing Depth, D =	6.54	ft

3rd Trial @ D_3 =	7.04	ft
Lateral Soil Bearing @ D/3, S_1 =	0.47	ksf
Lateral Soil Bearing @ D, S_3 =	1.41	ksf
Constant 2.34P/(S_1B), A =	3.57	
Required Footing Depth, D =	6.85	ft

4th Trial @ D_4 =	6.95	ft
Lateral Soil Bearing @ D/3, S_1 =	0.46	ksf
Lateral Soil Bearing @ D, S_3 =	1.39	ksf
Constant 2.34P/(S_1B), A =	3.62	
Required Footing Depth, D =	6.92	ft

5th Trial @ D_5 =	6.93	ft
Lateral Soil Bearing @ D/3, S_1 =	0.46	ksf
Lateral Soil Bearing @ D, S_3 =	1.39	ksf
Constant 2.34P/(S_1B), A =	3.63	
Required Footing Depth, D =	7.00	ft

A 2ft diameter x 7ft deep footing unrestrained at ground level is required for the racking structure.

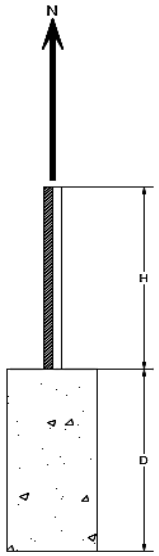
5.4 Uplifting Force Resistance

Uplifting forces of the racking system are checked against the uplift resistance of the soil. Clay soils are assumed.

Weight of Concrete, g_{con} =	145	pcf
Uplifting Force, N =	2.21	k
Footing Diameter, B =	2.00	ft
Factor of Safety =	2.50	
Cohesion =	208.85	psf
γ_s =	120.43	pcf
α =	0.45	
Required Concrete Weight, g =	1.45	k
Required Concrete Volume, V =	10.01	ft^3
Required Footing Depth, D =	3.25	ft

Iteration	z	dz	Qs	Side
1	0.2	0.2	118.10	4.74
2	0.4	0.2	118.10	4.64
3	0.6	0.2	118.10	4.53
4	0.8	0.2	118.10	4.43
5	1	0.2	118.10	4.33
6	1.2	0.2	118.10	4.22
7	1.4	0.2	118.10	4.12
8	1.6	0.2	118.10	4.02
9	1.8	0.2	118.10	3.91
10	2	0.2	118.10	3.81
11	2.2	0.2	118.10	3.71
12	2.4	0.2	118.10	3.60
13	2.6	0.2	118.10	3.50
14	2.8	0.2	118.10	3.39
15	3	0.2	118.10	3.29
16	3.2	0.2	118.10	3.19
17	0	0.0	0.00	3.19
18	0	0.0	0.00	3.19
19	0	0.0	0.00	3.19
20	0	0.0	0.00	3.19
21	0	0.0	0.00	3.19
22	0	0.0	0.00	3.19
23	0	0.0	0.00	3.19
24	0	0.0	0.00	3.19
25	0	0.0	0.00	3.19
26	0	0.0	0.00	3.19
27	0	0.0	0.00	3.19
28	0	0.0	0.00	3.19
29	0	0.0	0.00	3.19
30	0	0.0	0.00	3.19
31	0	0.0	0.00	3.19
32	0	0.0	0.00	3.19
33	0	0.0	0.00	3.19
34	0	0.0	0.00	3.19
Max	3.2	Sum	0.76	

A 2ft diameter x 3.25ft deep footing unrestrained at ground level is required for the racking structure.



5.5 Compressive Force Resistance

Skin friction of the soil is checked against the compression force from the racking and the weight of the drilled shaft foundation. Skin friction starts at 3ft below grade. Clay soils are again assumed.

Depth Below Grade, D =	7.00	ft
Footing Diameter, B =	2.00	ft
Compressive Force, P =	3.93	k
Footing Area =	3.14	ft^2
Circumference =	6.28	ft
Skin Friction Area =	25.13	ft^2
Concrete Weight =	0.145	kcf

Bearing Pressure

Bearing Area =	3.14	ft^2
Bearing Capacity =	1.5	ksf
Resistance =	4.71	k

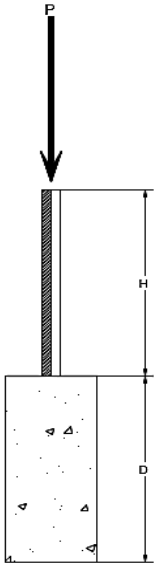
Weight of Concrete

Footing Volume	21.99	ft^3
Weight	3.19	k

Skin Friction Resistance

Skin Friction =	0.15	ksf
Resistance =	3.77	k
1/3 Increase for Wind =	1.33	
Total Resistance =	11.31	k
Applied Force =	7.12	k
Utilization =	63%	

A 2ft diameter footing passes at a depth of 7ft.



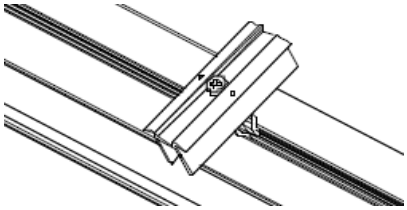
6. DESIGN OF JOINTS AND CONNECTIONS

6.1 Anchorage of Modules to Purlins and Connection of Purlins to Girders

Modules are secured to the purlins with Schletter, Inc. Rapid2+ mounting clamps. Purlins are secured to the girders with the use of 40mm mounting clamps. The reliability of calculations is uncertain due to limited standards, therefore the strength of the clamp fasteners has been evaluated by load testing.

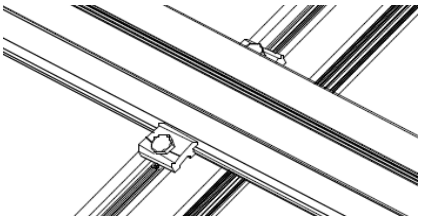
Fastening of Modules to Purlins

Maximum Uplifting Force	=	0.434 k
Allowable Uplift	=	1.214 k
Utilization	=	36%



Fastening of Purlins to Girders

Maximum Uplifting Force	=	1.444 k
Allowable Uplift	=	2.180 k
Utilization	=	66%

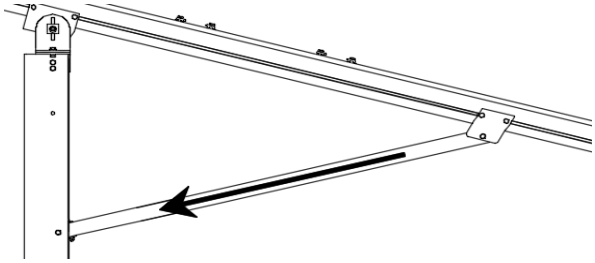


6.2 Strut Connections

The aluminum struts connect the front end of girder to a center section of the steel post. Single M10 bolts are used to attach each end of the strut to the girder and post. ASTM A193/A193M-86 equivalent stainless steel bolts are used.

Maximum Axial Load	=	4.678 k
M10 Bolt Shear Capacity	=	8.894 k
Utilization	=	53%

Bolt capacity is accounting for double shear. (ASCE 8-02, Eq. 5.3.4-1)

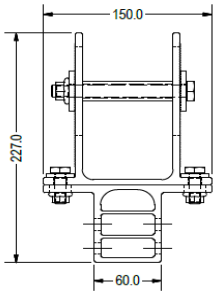


A strut under compression is shown to demonstrate the load transfer from the girder. Single M10 bolts are located at each end of the strut and are subjected to double shear.

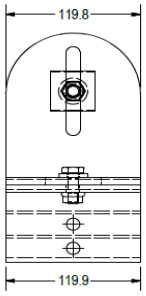
6.3 Girder to Post Connection

In order to connect the girder to the post, custom extruded sections are assembled to create a post head piece. The reliability of calculations is uncertain due to limited standards, therefore the strength of the head piece has been evaluated by load testing.

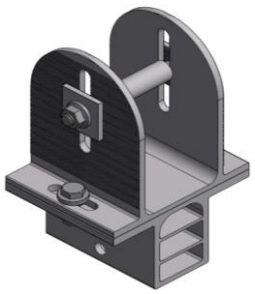
Maximum Tensile Load	=	3.019 k
Allowable Load	=	5.649 k
Utilization	=	53%



FRONT VIEW



SIDE VIEW



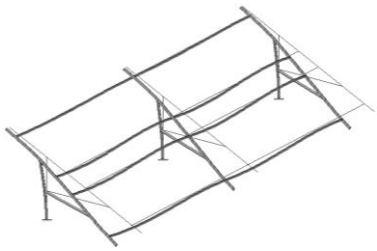
7. SEISMIC DESIGN

7.1 Seismic Drift - N/A

The racking structure has been analyzed under seismic loading. The allowable story drift of the structure must fall within the limits provided by (ASCE 7, Table 12.12-1).

Mean Height, h_{sx}	=	74.39 in
Allowable Story Drift for All Other Structures, Δ	= {	$0.020h_{sx}$
		1.488 in
Max Drift, Δ_{MAX}	=	0 in
N/A		

The racking structure's reaction to seismic loads is shown to the right. The deflections have been magnified to provide a clear portrayal of potential story drift.



APPENDIX A

A.1 Design of Aluminum Purlins - Aluminum Design Manual, 2005 Edition

Purlin = **S1.5**

Strong Axis:		Weak Axis:	
3.4.14		**3.4.14**	
L_b =	114 in	L_b =	114
J =	0.432	J =	0.432
	315.377		200.561
$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$		$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b}Fcy}{1.6Dc}\right)^2$	
S1 =	0.51461	S1 =	0.51461
$S2 = \left(\frac{C_c}{1.6}\right)^2$		$S2 = \left(\frac{C_c}{1.6}\right)^2$	
S2 =	1701.56	S2 =	1701.56
φF_L=	φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]	φF_L=	φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L=	27.5 ksi	φF_L=	28.8
3.4.16		**3.4.16**	
b/t =	32.195	b/t =	37.0588
$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$		$S1 = \frac{Bp - \frac{\theta_y}{\theta_b}Fcy}{1.6Dp}$	
S1 =	12.2	S1 =	12.2
$S2 = \frac{k_1 Bp}{1.6Dp}$		$S2 = \frac{k_1 Bp}{1.6Dp}$	
S2 =	46.7	S2 =	46.7
φF_L=	φb[Bp-1.6Dp*b/t]	φF_L=	φb[Bp-1.6Dp*b/t]
φF_L=	25.1 ksi	φF_L=	23.1 ksi
3.4.16.1	Not Used	**3.4.16.1**	
Rb/t =		N/A for Weak Direction	
$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$			
S1 =	1.1		
$S2 = C_t$			
S2 =	141.0		
φF_L=	1.17φyFcy		
φF_L=	38.9 ksi		
3.4.18		**3.4.18**	
h/t =	37.0588	h/t =	32.195
$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$		$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$	
S1 =	36.9	S1 =	36.9
m =	0.65	m =	0.65
C_0 =	40.985	C_0 =	45.5
Cc =	41.015	Cc =	45.5
$S2 = \frac{k_1 Bbr}{mDbr}$		$S2 = \frac{k_1 Bbr}{mDbr}$	
S2 =	77.2	S2 =	77.3
φF_L=	φb[Bbr-mDbr*h/t]	φF_L=	1.3φyFcy
φF_L=	43.2 ksi	φF_L=	43.2 ksi
φF_LSt=	25.1 ksi	φF_LWk=	23.1 ksi
Ix =	897074 mm^4	Iy =	446476 mm^4
	2.155 in^4		1.073 in^4
y =	41.015 mm	x =	45.5 mm
Sx =	1.335 in^3	Sy =	0.599 in^3
M_{max}St =	2.788 k-ft	M_{max}Wk =	1.152 k-ft

Compression

3.4.9

b/t = 32.195
S1 = 12.21 (See 3.4.16 above for formula)
S2 = 32.70 (See 3.4.16 above for formula)
φF_L = φc[Bp-1.6Dp*b/t]
φF_L = 25.1 ksi

b/t = 37.0588
S1 = 12.21
S2 = 32.70
φF_L = (φck2*√(BpE))/(1.6b/t)
φF_L = 21.9 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b} Fcy}{Dt}\right)^2$$

S1 = 6.87
S2 = 131.3
φF_L = φyFcy
φF_L = 33.25 ksi

φF_L = 21.94 ksi
A = 1215.13 mm^2
1.88 in^2
P_{max} = 41.32 kips

A.2 Design of Aluminum Girders - Aluminum Design Manual, 2005 Edition

Girder = **T5**

Strong Axis:

3.4.14

L_b = 81.7717 in
J = 1.98
105.231

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 30.1 ksi

3.4.16

b/t = 4.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φyFcy
φF_L = 33.3 ksi

Weak Axis:

3.4.14

L_b = 81.7717
J = 1.98
114.202

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56
φF_L = φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]
φF_L = 29.9

3.4.16

b/t = 16.3333

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7
φF_L = φb[Bp-1.6Dp*b/t]
φF_L = 31.6 ksi

3.4.16.1 Used

Rb/t = 20.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b}Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= φb[Bt-Dt*√(Rb/t)]

φF_L= 30.8 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 16.3333

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 37.9

m = 0.63

C_0 = 61.046

Cc = 58.954

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 79.4

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L St$= 30.1 ksi

Ix = 1970917 mm^4

4.735 in^4

y = 61.046 mm

Sx = 1.970 in^3

$M_{max}St$ = 4.935 k-ft

3.4.18

h/t = 4.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b}1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 35

Cc = 35

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

$\varphi F_L Wk$= 31.6 ksi

Iy = 763048 mm^4

1.833 in^4

x = 35 mm

Sy = 1.330 in^3

$M_{max}Wk$ = 3.499 k-ft

Compression

3.4.9

b/t = 4.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

φF_L= φyFcy

φF_L= 33.3 ksi

b/t = 16.3333

S1 = 12.21

S2 = 32.70

φF_L= φc[Bp-1.6Dp*b/t]

φF_L= 31.6 ksi

3.4.10

Rb/t = 20.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

φF_L= φc[Bt-Dt*√(Rb/t)]

φF_L= 30.80 ksi

φF_L= 30.80 ksi

A = 1215.13 mm^2

1.88 in^2

P_{max} = 58.01 kips

A.3 Design of Aluminum Struts - Aluminum Design Manual, 2005 Edition

Strut = **55x55**

Strong Axis:

3.4.14

L_b = 74.8031 in

J = 0.942

116.737

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.9 ksi

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1 Not Used

Rb/t = 0.0

$$S1 = \left(\frac{Bt - 1.17\frac{\theta_y}{\theta_b} Fcy}{1.6Dt}\right)^2$$

S1 = 1.1

$$S2 = C_t$$

S2 = 141.0

φF_L= 1.17φyFcy

φF_L= 38.9 ksi

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LSt= 28.2 ksi

Ix = 279836 mm^4

0.672 in^4

y = 27.5 mm

Sx = 0.621 in^3

M_{max}St = 1.460 k-ft

Weak Axis:

3.4.14

L_b = 74.8031

J = 0.942

116.737

$$S1 = \left(\frac{Bc - \frac{\theta_y}{\theta_b} Fcy}{1.6Dc}\right)^2$$

S1 = 0.51461

$$S2 = \left(\frac{C_c}{1.6}\right)^2$$

S2 = 1701.56

φF_L= φb[Bc-1.6Dc*√((LbSc)/(Cb*√(IyJ)/2))]

φF_L= 29.9

3.4.16

b/t = 24.5

$$S1 = \frac{Bp - \frac{\theta_y}{\theta_b} Fcy}{1.6Dp}$$

S1 = 12.2

$$S2 = \frac{k_1 Bp}{1.6Dp}$$

S2 = 46.7

φF_L= φb[Bp-1.6Dp*b/t]

φF_L= 28.2 ksi

3.4.16.1

N/A for Weak Direction

3.4.18

h/t = 24.5

$$S1 = \frac{Bbr - \frac{\theta_y}{\theta_b} 1.3Fcy}{mDbr}$$

S1 = 36.9

m = 0.65

C_0 = 27.5

Cc = 27.5

$$S2 = \frac{k_1 Bbr}{mDbr}$$

S2 = 77.3

φF_L= 1.3φyFcy

φF_L= 43.2 ksi

φF_LWk= 28.2 ksi

Iy = 279836 mm^4

0.672 in^4

x = 27.5 mm

Sy = 0.621 in^3

M_{max}Wk = 1.460 k-ft

Compression

3.4.7

λ = 1.73045

r = 0.81 in

$$S1^* = \frac{Bc - Fcy}{1.6Dc^*}$$

$S1^*$ = 0.33515

$$S2^* = \frac{Cc}{\pi}\sqrt{Fcy/E}$$

$S2^*$ = 1.23671

φcc = 0.82226

$\varphi F_L = (\varphi ccFcy)/(\lambda^2)$

φF_L = 9.61085 ksi

3.4.9

b/t = 24.5

S1 = 12.21 (See 3.4.16 above for formula)

S2 = 32.70 (See 3.4.16 above for formula)

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

φF_L = 28.2 ksi

b/t = 24.5

S1 = 12.21

S2 = 32.70

$\varphi F_L = \varphi c[Bp-1.6Dp*b/t]$

φF_L = 28.2 ksi

3.4.10

Rb/t = 0.0

$$S1 = \left(\frac{Bt - \frac{\theta_y}{\theta_b}Fcy}{Dt}\right)^2$$

S1 = 6.87

S2 = 131.3

$\varphi F_L = \varphi yFcy$

φF_L = 33.25 ksi

φF_L = 9.61 ksi

A = 663.99 mm^2

1.03 in^2

P_{max} = 9.89 kips

A.4 Design of Galvanized Steel Posts

Post Type = **FG8**

Unbraced Length =	81.31	in	
Pr =	6.13	k	(LRFD Factored Load)
Mr (Strong) =	14.76	k-ft	(LRFD Factored Load)
Mr (Weak) =	0.00	k-ft	(LRFD Factored Load)

Flexural Buckling:

kL/r =	116.99			
4.71√(E/Fy) =	103.55	=>	kL/r	> 4.71√(E/Fy)
Fcr =	18.34	ksi		
Fe =	20.91	ksi		
Pn =	40.9	k		

Torsional/Flexural Torsional Buckling:

Fcr =	13.8471	ksi
Fey =	53.3447	ksi
Fez =	17.7356	ksi
Pn =	30.879	k

Bending (Strong Axis):

Yielding:

Mn =	21.95	k-ft

Flange Local Buckling:

Mn =	19.207	k-ft

Pr/Pc =	0.2207	≥	0.2	
Utilization =	0.98	<	1.0	OK

Bending (Weak Axis):

Yielding:

Mn =	14.65	k-ft

Flange Local Buckling:

Mn =	14.39	k-ft

Pr/Pc =	0.221	≥	0.2	
Utilization =	0.00	<	1.0	OK

Combined Forces

Utilization = 98%

APPENDIX B

B.1

The following pages will contain the results from RISA. Please refer back to Section 2 for load information and Section 4-5 for member and foundation design.

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut...	Area(Me...	Surface(...
1	Dead Load, Max	DL		-1				4		
2	Dead Load, Min	DL		-1				4		
3	Snow Load	SL						4		
4	Wind Load - Pressure	WL						4		
5	Wind Load - Suction	WL						4		
6	Seismic - Lateral	EL								

Member Distributed Loads (BLC 1 : Dead Load, Max)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-9.843	-9.843	0	0
2	M11	Y	-9.843	-9.843	0	0
3	M12	Y	-9.843	-9.843	0	0
4	M13	Y	-9.843	-9.843	0	0

Member Distributed Loads (BLC 2 : Dead Load, Min)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-5.454	-5.454	0	0
2	M11	Y	-5.454	-5.454	0	0
3	M12	Y	-5.454	-5.454	0	0
4	M13	Y	-5.454	-5.454	0	0

Member Distributed Loads (BLC 3 : Snow Load)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	Y	-55.176	-55.176	0	0
2	M11	Y	-55.176	-55.176	0	0
3	M12	Y	-55.176	-55.176	0	0
4	M13	Y	-55.176	-55.176	0	0

Member Distributed Loads (BLC 4 : Wind Load - Pressure)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	-40.939	-40.939	0	0
2	M11	y	-40.939	-40.939	0	0
3	M12	y	-63.27	-63.27	0	0
4	M13	y	-63.27	-63.27	0	0

Member Distributed Loads (BLC 5 : Wind Load - Suction)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M10	y	81.879	81.879	0	0
2	M11	y	81.879	81.879	0	0
3	M12	y	37.218	37.218	0	0
4	M13	y	37.218	37.218	0	0

Load Combinations

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	LRFD 1.2D + 1.6S + 0.8W	Yes	Y		1	1.2	3	1.6	4	.8																
2	LRFD 1.2D + 1.6W + 0.5S	Yes	Y		1	1.2	3	.5	4	1.6																
3	LRFD 0.9D + 1.6W	Yes	Y		2	.9					5	1.6														
4	LATERAL - LRFD 1.54D + 1.3E ...	Yes	Y		1	1.54	3	.2			6	1.3														
5	LATERAL - LRFD 0.56D + 1.3E	Yes	Y		1	.56					6	1.3														
6	LATERAL - LRFD 1.54D + 1.25...	Yes	Y		1	1.54	3	.2			6	1.25														
7	LATERAL - LRFD 0.56D + 1.25E	Yes	Y		1	.56					6	1.25														

Load Combinations (Continued)

	Description	S...	P...	S...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
8																								
9	ASD 1.0D + 1.0S	Yes	Y		1	1	3	1																
10	ASD 1.0D + 1.0W	Yes	Y		1	1			4	1														
11	ASD 1.0D + 0.75L + 0.75W + 0....	Yes	Y		1	1	3	.75	4	.75														
12	ASD 0.6D + 1.0W	Yes	Y		2	.6					5	1												
13	LATERAL - ASD 1.238D + 0.875E	Yes	Y		1	1.2...					6	.875												
14	LATERAL - ASD 1.1785D + 0.65...	Yes	Y		1	1.1...	3	.75			6	.656												
15	LATERAL - ASD 0.362D + 0.875E	Yes	Y		1	.362					6	.875												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N9	max	382.899	2	2365.216	1	172.93	1	.278	1	.002	3	7.819	1
2		min	-624.756	3	-1159.406	3	-133.457	3	-.175	3	-.005	1	.292	15
3	N19	max	1911.872	2	6170.14	1	0	13	0	3	0	3	13.962	1
4		min	-1810.709	3	-3554.009	3	0	1	0	1	0	1	.482	15
5	N29	max	382.899	2	2365.216	1	133.457	3	.175	3	.005	1	7.819	1
6		min	-624.756	3	-1159.406	3	-172.93	1	-.278	1	-.002	3	.292	15
7	Totals:	max	2677.67	2	10900.572	1	0	1						
8		min	-3060.22	3	-5872.822	3	0	3						

Envelope Member Section Forces

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M1	1	max	0	1	.003	1	0	3	0	1	0	1	0	1
2			min	0	1	0	3	0	1	0	1	0	1	0	1
3		2	max	-8.031	12	202.474	3	1.459	3	.037	3	.357	1	.219	1
4			min	-230.917	1	-585.616	1	-171.234	1	-.206	1	.01	12	-.074	3
5		3	max	-8.417	12	201.231	3	1.459	3	.037	3	.245	1	.604	1
6			min	-231.69	1	-587.275	1	-171.234	1	-.206	1	.009	15	-.206	3
7		4	max	-8.804	12	199.987	3	1.459	3	.037	3	.133	1	.99	1
8			min	-232.463	1	-588.933	1	-171.234	1	-.206	1	.005	15	-.338	3
9		5	max	415.657	3	550.575	1	13.932	3	.001	2	.179	1	1.167	1
10			min	-1561.104	1	-179.434	3	-210.062	1	-.029	3	-.032	3	-.399	3
11		6	max	415.077	3	548.917	1	13.932	3	.001	2	.046	2	.807	1
12			min	-1561.877	1	-180.678	3	-210.062	1	-.029	3	-.023	3	-.281	3
13		7	max	414.498	3	547.259	1	13.932	3	.001	2	-.004	15	.447	1
14			min	-1562.65	1	-181.922	3	-210.062	1	-.029	3	-.096	1	-.162	3
15		8	max	413.918	3	545.6	1	13.932	3	.001	2	-.004	12	.088	1
16			min	-1563.423	1	-183.165	3	-210.062	1	-.029	3	-.234	1	-.042	3
17		9	max	402.326	3	3.765	9	27.744	3	-.003	15	.12	1	.016	3
18			min	-1808.682	1	-3.844	2	-261.017	1	-.145	2	.005	15	-.077	2
19		10	max	401.746	3	2.383	9	27.744	3	-.003	15	.038	3	.016	3
20			min	-1809.455	1	-5.502	2	-261.017	1	-.145	2	-.051	1	-.077	1
21		11	max	401.166	3	1.001	9	27.744	3	-.003	15	.057	3	.017	3
22			min	-1810.228	1	-7.16	2	-261.017	1	-.145	2	-.222	1	-.076	1
23		12	max	386.516	3	486.248	3	22.053	2	.196	3	.166	1	.087	1
24			min	-2050.08	1	-470.358	1	-128.514	3	-.261	1	.006	15	-.139	3
25		13	max	385.936	3	485.004	3	22.053	2	.196	3	.152	1	.396	1
26			min	-2050.853	1	-472.016	1	-128.514	3	-.261	1	-.029	3	-.457	3
27		14	max	385.356	3	483.761	3	22.053	2	.196	3	.138	1	.706	1
28			min	-2051.627	1	-473.674	1	-128.514	3	-.261	1	-.113	3	-.775	3
29		15	max	384.776	3	482.517	3	22.053	2	.196	3	.123	1	1.018	1
30			min	-2052.4	1	-475.332	1	-128.514	3	-.261	1	-.197	3	-1.092	3
31		16	max	232.837	1	469.877	1	-4.94	12	.181	1	.01	3	.774	1
32			min	7.785	12	-497.015	3	-154.376	1	-.277	3	-.173	1	-.834	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
33		17	max	232.064	1	468.219	1	-4.94	12	.181	1	.005	3	.466	1
34			min	7.399	12	-498.258	3	-154.376	1	-.277	3	-.274	1	-.507	3
35		18	max	231.291	1	466.561	1	-4.94	12	.181	1	0	3	.16	1
36			min	7.012	12	-499.502	3	-154.376	1	-.277	3	-.375	1	-.18	3
37		19	max	0	1	0	5	0	1	0	1	0	1	0	1
38			min	0	1	-.001	3	0	5	0	1	0	1	0	1
39	M4	1	max	0	1	.007	1	0	1	0	1	0	1	0	1
40			min	0	1	-.001	3	0	1	0	1	0	1	0	1
41		2	max	-15.493	15	614.669	3	0	1	0	1	0	1	.465	1
42			min	-358.703	1	-1529.971	1	0	1	0	1	0	1	-.194	3
43		3	max	-15.727	15	613.426	3	0	1	0	1	0	1	1.47	1
44			min	-359.476	1	-1531.63	1	0	1	0	1	0	1	-.597	3
45		4	max	-15.96	15	612.182	3	0	1	0	1	0	1	2.475	1
46			min	-360.249	1	-1533.288	1	0	1	0	1	0	1	-.999	3
47		5	max	1395.562	3	1532.339	1	0	1	0	1	0	1	2.918	1
48			min	-3948.328	1	-634.582	3	0	1	0	1	0	1	-1.171	3
49		6	max	1394.982	3	1530.681	1	0	1	0	1	0	1	1.913	1
50			min	-3949.101	1	-635.826	3	0	1	0	1	0	1	-.755	3
51		7	max	1394.402	3	1529.022	1	0	1	0	1	0	1	.918	2
52			min	-3949.874	1	-637.07	3	0	1	0	1	0	1	-.337	3
53		8	max	1393.822	3	1527.364	1	0	1	0	1	0	1	.081	3
54			min	-3950.647	1	-638.313	3	0	1	0	1	0	1	-.093	1
55		9	max	1364.978	3	14.274	3	0	1	0	1	0	1	.28	3
56			min	-4280.666	1	-101.423	1	0	1	0	1	0	1	-.565	1
57		10	max	1364.398	3	13.03	3	0	1	0	1	0	1	.271	3
58			min	-4281.439	1	-103.081	1	0	1	0	1	0	1	-.498	1
59		11	max	1363.818	3	11.787	3	0	1	0	1	0	1	.263	3
60			min	-4282.213	1	-104.739	1	0	1	0	1	0	1	-.43	1
61		12	max	1341.091	3	1408.891	3	0	1	0	1	0	1	.072	1
62			min	-4623.045	1	-1546.226	1	0	1	0	1	0	1	-.186	3
63		13	max	1340.511	3	1407.647	3	0	1	0	1	0	1	1.087	1
64			min	-4623.818	1	-1547.884	1	0	1	0	1	0	1	-1.11	3
65		14	max	1339.931	3	1406.404	3	0	1	0	1	0	1	2.103	1
66			min	-4624.591	1	-1549.542	1	0	1	0	1	0	1	-2.033	3
67		15	max	1339.351	3	1405.16	3	0	1	0	1	0	1	3.121	1
68			min	-4625.364	1	-1551.201	1	0	1	0	1	0	1	-2.956	3
69		16	max	359.501	1	1448.917	1	0	1	0	1	0	1	2.376	1
70			min	15.853	15	-1376.702	3	0	1	0	1	0	1	-2.244	3
71		17	max	358.728	1	1447.259	1	0	1	0	1	0	1	1.426	1
72			min	15.619	15	-1377.945	3	0	1	0	1	0	1	-1.341	3
73		18	max	357.955	1	1445.601	1	0	1	0	1	0	1	.477	1
74			min	15.386	15	-1379.189	3	0	1	0	1	0	1	-.436	3
75		19	max	0	1	0	2	0	1	0	1	0	1	0	1
76			min	0	1	-.003	3	0	1	0	1	0	1	0	1
77	M7	1	max	0	1	.003	1	0	1	0	1	0	1	0	1
78			min	0	1	0	3	0	3	0	1	0	1	0	1
79		2	max	-8.031	12	202.474	3	171.234	1	.206	1	-.01	12	.219	1
80			min	-230.917	1	-585.616	1	-1.459	3	-.037	3	-.357	1	-.074	3
81		3	max	-8.417	12	201.231	3	171.234	1	.206	1	-.009	15	.604	1
82			min	-231.69	1	-587.275	1	-1.459	3	-.037	3	-.245	1	-.206	3
83		4	max	-8.804	12	199.987	3	171.234	1	.206	1	-.005	15	.99	1
84			min	-232.463	1	-588.933	1	-1.459	3	-.037	3	-.133	1	-.338	3
85		5	max	415.657	3	550.575	1	210.062	1	.029	3	.032	3	1.167	1
86			min	-1561.104	1	-179.434	3	-13.932	3	-.001	2	-.179	1	-.399	3
87		6	max	415.077	3	548.917	1	210.062	1	.029	3	.023	3	.807	1
88			min	-1561.877	1	-180.678	3	-13.932	3	-.001	2	-.046	2	-.281	3
89		7	max	414.498	3	547.259	1	210.062	1	.029	3	.096	1	.447	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
90			min	-1562.65	1	-181.922	3	-13.932	3	-.001	2	.004	15	-.162	3
91		8	max	413.918	3	545.6	1	210.062	1	.029	3	.234	1	.088	1
92			min	-1563.423	1	-183.165	3	-13.932	3	-.001	2	.004	12	-.042	3
93		9	max	402.326	3	3.765	9	261.017	1	.145	2	-.005	15	.016	3
94			min	-1808.682	1	-3.844	2	-27.744	3	.003	15	-.12	1	-.077	2
95		10	max	401.746	3	2.383	9	261.017	1	.145	2	.051	1	.016	3
96			min	-1809.455	1	-5.502	2	-27.744	3	.003	15	-.038	3	-.077	1
97		11	max	401.166	3	1.001	9	261.017	1	.145	2	.222	1	.017	3
98			min	-1810.228	1	-7.16	2	-27.744	3	.003	15	-.057	3	-.076	1
99		12	max	386.516	3	486.248	3	128.514	3	.261	1	-.006	15	.087	1
100			min	-2050.08	1	-470.358	1	-22.053	2	-.196	3	-.166	1	-.139	3
101		13	max	385.936	3	485.004	3	128.514	3	.261	1	.029	3	.396	1
102			min	-2050.853	1	-472.016	1	-22.053	2	-.196	3	-.152	1	-.457	3
103		14	max	385.356	3	483.761	3	128.514	3	.261	1	.113	3	.706	1
104			min	-2051.627	1	-473.674	1	-22.053	2	-.196	3	-.138	1	-.775	3
105		15	max	384.776	3	482.517	3	128.514	3	.261	1	.197	3	1.018	1
106			min	-2052.4	1	-475.332	1	-22.053	2	-.196	3	-.123	1	-1.092	3
107		16	max	232.837	1	469.877	1	154.376	1	.277	3	.173	1	.774	1
108			min	7.785	12	-497.015	3	4.94	12	-.181	1	-.01	3	-.834	3
109		17	max	232.064	1	468.219	1	154.376	1	.277	3	.274	1	.466	1
110			min	7.399	12	-498.258	3	4.94	12	-.181	1	-.005	3	-.507	3
111		18	max	231.291	1	466.561	1	154.376	1	.277	3	.375	1	.16	1
112			min	7.012	12	-499.502	3	4.94	12	-.181	1	0	3	-.18	3
113		19	max	0	1	0	5	0	5	0	1	0	1	0	1
114			min	0	1	-.001	3	0	1	0	1	0	1	0	1
115	M10	1	max	154.423	1	465.592	1	-6.626	12	.003	1	.427	1	.181	1
116			min	4.943	12	-500.687	3	-231.155	1	-.013	3	.003	3	-.277	3
117		2	max	154.423	1	333.539	1	-4.763	12	.003	1	.207	1	.181	3
118			min	4.943	12	-368.394	3	-185.699	1	-.013	3	-.006	3	-.241	1
119		3	max	154.423	1	201.487	1	-2.9	12	.003	1	.05	2	.5	3
120			min	4.943	12	-236.101	3	-140.242	1	-.013	3	-.012	3	-.523	1
121		4	max	154.423	1	69.434	1	-1.038	12	.003	1	.004	10	.68	3
122			min	4.943	12	-103.807	3	-94.786	1	-.013	3	-.089	1	-.666	1
123		5	max	154.423	1	28.486	3	1.481	3	.003	1	-.007	15	.72	3
124			min	4.943	12	-62.618	1	-49.329	1	-.013	3	-.165	1	-.67	1
125		6	max	154.423	1	160.779	3	4.275	3	.003	1	-.008	15	.62	3
126			min	4.943	12	-194.671	1	-16.148	2	-.013	3	-.193	1	-.534	1
127		7	max	154.423	1	293.073	3	41.584	1	.003	1	-.004	12	.38	3
128			min	4.943	12	-326.723	1	-5.586	10	-.013	3	-.173	1	-.259	1
129		8	max	154.423	1	425.366	3	87.04	1	.003	1	.003	3	.156	1
130			min	4.943	12	-458.775	1	-.524	10	-.013	3	-.105	1	0	12
131		9	max	154.423	1	557.659	3	132.497	1	.003	1	.031	9	.71	1
132			min	4.943	12	-590.828	1	4.538	10	-.013	3	-.052	2	-.518	3
133		10	max	154.423	1	-21.485	15	177.953	1	.013	3	.174	1	1.403	1
134			min	4.943	12	-722.88	1	-15.45	3	-.003	1	-.031	10	-1.176	3
135		11	max	154.423	1	590.828	1	-4.538	10	.013	3	.031	9	.71	1
136			min	4.943	12	-557.659	3	-132.497	1	-.003	1	-.052	2	-.518	3
137		12	max	154.423	1	458.775	1	.524	10	.013	3	.003	3	.156	1
138			min	4.943	12	-425.366	3	-87.04	1	-.003	1	-.105	1	0	12
139		13	max	154.423	1	326.723	1	5.586	10	.013	3	-.004	12	.38	3
140			min	4.943	12	-293.073	3	-41.584	1	-.003	1	-.173	1	-.259	1
141		14	max	154.423	1	194.671	1	16.148	2	.013	3	-.008	15	.62	3
142			min	4.943	12	-160.779	3	-4.275	3	-.003	1	-.193	1	-.534	1
143		15	max	154.423	1	62.618	1	49.329	1	.013	3	-.007	15	.72	3
144			min	4.943	12	-28.486	3	-1.481	3	-.003	1	-.165	1	-.67	1
145		16	max	154.423	1	103.807	3	94.786	1	.013	3	.004	10	.68	3
146			min	4.943	12	-69.434	1	1.038	12	-.003	1	-.089	1	-.666	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
147		17	max	154.423	1	236.101	3	140.242	1	.013	3	.05	2	.5	3
148			min	4.943	12	-201.487	1	2.9	12	-.003	1	-.012	3	-.523	1
149		18	max	154.423	1	368.394	3	185.699	1	.013	3	.207	1	.181	3
150			min	4.943	12	-333.539	1	4.763	12	-.003	1	-.006	3	-.241	1
151		19	max	154.423	1	500.687	3	231.155	1	.013	3	.427	1	.181	1
152			min	4.943	12	-465.592	1	6.626	12	-.003	1	.003	3	-.277	3
153	M11	1	max	238.953	1	468.155	1	-9.265	15	.002	3	.483	1	.129	1
154			min	-156.123	3	-490.126	3	-240.073	1	-.013	1	.018	15	-.276	3
155		2	max	238.953	1	336.102	1	-7.432	15	.002	3	.254	1	.172	3
156			min	-156.123	3	-357.833	3	-194.616	1	-.013	1	.009	15	-.296	1
157		3	max	238.953	1	204.05	1	-5.6	15	.002	3	.072	1	.48	3
158			min	-156.123	3	-225.54	3	-149.16	1	-.013	1	.002	15	-.581	1
159		4	max	238.953	1	71.997	1	-3.767	15	.002	3	.008	10	.648	3
160			min	-156.123	3	-93.246	3	-103.703	1	-.013	1	-.061	1	-.726	1
161		5	max	238.953	1	39.047	3	-1.935	15	.002	3	-.004	12	.677	3
162			min	-156.123	3	-60.055	1	-58.247	1	-.013	1	-.147	1	-.733	1
163		6	max	238.953	1	171.34	3	-.078	12	.002	3	-.005	12	.565	3
164			min	-156.123	3	-192.107	1	-19.987	2	-.013	1	-.184	1	-.6	1
165		7	max	238.953	1	303.634	3	32.666	1	.002	3	-.004	12	.315	3
166			min	-156.123	3	-324.16	1	-6.716	10	-.013	1	-.174	1	-.327	1
167		8	max	238.953	1	435.927	3	78.122	1	.002	3	-.001	12	.085	1
168			min	-156.123	3	-456.212	1	-1.654	10	-.013	1	-.115	1	-.076	3
169		9	max	238.953	1	568.22	3	123.579	1	.002	3	.019	9	.636	1
170			min	-156.123	3	-588.265	1	3.408	10	-.013	1	-.061	2	-.606	3
171		10	max	238.953	1	720.317	1	-7.227	15	.01	2	.146	1	1.327	1
172			min	-156.123	3	-700.513	3	-169.035	1	-.013	1	-.035	10	-1.275	3
173		11	max	238.953	1	588.265	1	-3.408	10	.013	1	.019	9	.636	1
174			min	-156.123	3	-568.22	3	-123.579	1	-.002	3	-.061	2	-.606	3
175		12	max	238.953	1	456.212	1	1.654	10	.013	1	-.001	12	.085	1
176			min	-156.123	3	-435.927	3	-78.122	1	-.002	3	-.115	1	-.076	3
177		13	max	238.953	1	324.16	1	6.716	10	.013	1	-.004	12	.315	3
178			min	-156.123	3	-303.634	3	-32.666	1	-.002	3	-.174	1	-.327	1
179		14	max	238.953	1	192.107	1	19.987	2	.013	1	-.005	12	.565	3
180			min	-156.123	3	-171.34	3	.078	12	-.002	3	-.184	1	-.6	1
181		15	max	238.953	1	60.055	1	58.247	1	.013	1	-.004	12	.677	3
182			min	-156.123	3	-39.047	3	1.935	15	-.002	3	-.147	1	-.733	1
183		16	max	238.953	1	93.246	3	103.703	1	.013	1	.008	10	.648	3
184			min	-156.123	3	-71.997	1	3.767	15	-.002	3	-.061	1	-.726	1
185		17	max	238.953	1	225.54	3	149.16	1	.013	1	.072	1	.48	3
186			min	-156.123	3	-204.05	1	5.6	15	-.002	3	.002	15	-.581	1
187		18	max	238.953	1	357.833	3	194.616	1	.013	1	.254	1	.172	3
188			min	-156.123	3	-336.102	1	7.432	15	-.002	3	.009	15	-.296	1
189		19	max	238.953	1	490.126	3	240.073	1	.013	1	.483	1	.129	1
190			min	-156.123	3	-468.155	1	9.265	15	-.002	3	.018	15	-.276	3
191	M12	1	max	13.857	3	542.67	1	-7.479	12	0	3	.509	1	.146	2
192			min	-49.448	1	-184.884	3	-244.278	1	-.01	1	.008	12	.003	15
193		2	max	13.857	3	391.76	1	-5.616	12	0	3	.275	1	.216	3
194			min	-49.448	1	-128.018	3	-198.822	1	-.01	1	.001	3	-.36	1
195		3	max	13.857	3	240.851	1	-3.754	12	0	3	.09	1	.321	3
196			min	-49.448	1	-71.153	3	-153.365	1	-.01	1	-.006	3	-.694	1
197		4	max	13.857	3	89.941	1	-1.891	12	0	3	.013	10	.366	3
198			min	-49.448	1	-14.287	3	-107.909	1	-.01	1	-.048	1	-.869	1
199		5	max	13.857	3	42.579	3	.164	3	0	3	-.006	15	.351	3
200			min	-49.448	1	-60.969	1	-62.453	1	-.01	1	-.138	1	-.884	1
201		6	max	13.857	3	99.445	3	2.958	3	0	3	-.007	12	.276	3
202			min	-49.448	1	-211.878	1	-23.562	2	-.01	1	-.18	1	-.74	1
203		7	max	13.857	3	156.311	3	28.46	1	0	3	-.004	12	.141	3

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
204			min	-49.448	1	-362.788	1	-8.521	10	-.01	1	-.174	1	-.437	1
205		8	max	13.857	3	213.177	3	73.917	1	0	3	.002	3	.036	2
206			min	-49.448	1	-513.698	1	-3.459	10	-.01	1	-.12	1	-.054	3
207		9	max	13.857	3	270.042	3	119.373	1	0	3	.015	9	.648	1
208			min	-49.448	1	-664.608	1	1.602	10	-.01	1	-.069	2	-.309	3
209		10	max	13.857	3	815.517	1	-6.664	10	.01	1	.132	1	1.429	1
210			min	-49.448	1	-326.908	3	-164.83	1	0	3	-.041	10	-.624	3
211		11	max	13.857	3	664.608	1	-1.602	10	.01	1	.015	9	.648	1
212			min	-49.448	1	-270.042	3	-119.373	1	0	3	-.069	2	-.309	3
213		12	max	13.857	3	513.698	1	3.459	10	.01	1	.002	3	.036	2
214			min	-49.448	1	-213.177	3	-73.917	1	0	3	-.12	1	-.054	3
215		13	max	13.857	3	362.788	1	8.521	10	.01	1	-.004	12	.141	3
216			min	-49.448	1	-156.311	3	-28.46	1	0	3	-.174	1	-.437	1
217		14	max	13.857	3	211.878	1	23.562	2	.01	1	-.007	12	.276	3
218			min	-49.448	1	-99.445	3	-2.958	3	0	3	-.18	1	-.74	1
219		15	max	13.857	3	60.969	1	62.453	1	.01	1	-.006	15	.351	3
220			min	-49.448	1	-42.579	3	-.164	3	0	3	-.138	1	-.884	1
221		16	max	13.857	3	14.287	3	107.909	1	.01	1	.013	10	.366	3
222			min	-49.448	1	-89.941	1	1.891	12	0	3	-.048	1	-.869	1
223		17	max	13.857	3	71.153	3	153.365	1	.01	1	.09	1	.321	3
224			min	-49.448	1	-240.851	1	3.754	12	0	3	-.006	3	-.694	1
225		18	max	13.857	3	128.018	3	198.822	1	.01	1	.275	1	.216	3
226			min	-49.448	1	-391.76	1	5.616	12	0	3	.001	3	-.36	1
227		19	max	13.857	3	184.884	3	244.278	1	.01	1	.509	1	.146	2
228			min	-49.448	1	-542.67	1	7.479	12	0	3	.008	12	.003	15
229	M13	1	max	1.459	3	586.324	1	-7.644	12	.006	3	.415	1	.206	1
230			min	-170.998	1	-203.747	3	-229.422	1	-.023	1	.009	12	-.037	3
231		2	max	1.459	3	435.414	1	-5.782	12	.006	3	.196	1	.148	3
232			min	-170.998	1	-146.881	3	-183.965	1	-.023	1	.002	12	-.333	1
233		3	max	1.459	3	284.505	1	-3.919	12	.006	3	.043	2	.273	3
234			min	-170.998	1	-90.016	3	-138.509	1	-.023	1	-.005	3	-.713	1
235		4	max	1.459	3	133.595	1	-2.057	12	.006	3	.002	10	.338	3
236			min	-170.998	1	-33.15	3	-93.052	1	-.023	1	-.096	1	-.934	1
237		5	max	1.459	3	23.716	3	-.154	3	.006	3	-.007	15	.343	3
238			min	-170.998	1	-23.578	2	-47.596	1	-.023	1	-.17	1	-.995	1
239		6	max	1.459	3	80.582	3	4.655	9	.006	3	-.006	12	.288	3
240			min	-170.998	1	-169.852	2	-14.832	2	-.023	1	-.196	1	-.897	1
241		7	max	1.459	3	137.448	3	43.317	1	.006	3	-.004	12	.173	3
242			min	-170.998	1	-319.134	1	-4.951	10	-.023	1	-.175	1	-.64	1
243		8	max	1.459	3	194.313	3	88.773	1	.006	3	.002	3	-.002	12
244			min	-170.998	1	-470.044	1	.111	10	-.023	1	-.105	1	-.223	1
245		9	max	1.459	3	251.179	3	134.23	1	.006	3	.032	9	.388	2
246			min	-170.998	1	-620.954	1	5.173	10	-.023	1	-.051	2	-.237	3
247		10	max	1.459	3	308.045	3	179.686	1	.023	1	.178	1	1.107	2
248			min	-170.998	1	-771.863	1	7.631	15	-.006	3	-.03	10	-.533	3
249		11	max	1.459	3	620.954	1	-5.173	10	.023	1	.032	9	.388	2
250			min	-170.998	1	-251.179	3	-134.23	1	-.006	3	-.051	2	-.237	3
251		12	max	1.459	3	470.044	1	-.111	10	.023	1	.002	3	-.002	12
252			min	-170.998	1	-194.313	3	-88.773	1	-.006	3	-.105	1	-.223	1
253		13	max	1.459	3	319.134	1	4.951	10	.023	1	-.004	12	.173	3
254			min	-170.998	1	-137.448	3	-43.317	1	-.006	3	-.175	1	-.64	1
255		14	max	1.459	3	169.852	2	14.832	2	.023	1	-.006	12	.288	3
256			min	-170.998	1	-80.582	3	-4.655	9	-.006	3	-.196	1	-.897	1
257		15	max	1.459	3	23.578	2	47.596	1	.023	1	-.007	15	.343	3
258			min	-170.998	1	-23.716	3	.154	3	-.006	3	-.17	1	-.995	1
259		16	max	1.459	3	33.15	3	93.052	1	.023	1	.002	10	.338	3
260			min	-170.998	1	-133.595	1	2.057	12	-.006	3	-.096	1	-.934	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
261		17	max	1.459	3	90.016	3	138.509	1	.023	1	.043	2	.273	3
262			min	-170.998	1	-284.505	1	3.919	12	-.006	3	-.005	3	-.713	1
263		18	max	1.459	3	146.881	3	183.965	1	.023	1	.196	1	.148	3
264			min	-170.998	1	-435.414	1	5.782	12	-.006	3	.002	12	-.333	1
265		19	max	1.459	3	203.747	3	229.422	1	.023	1	.415	1	.206	1
266			min	-170.998	1	-586.324	1	7.644	12	-.006	3	.009	12	-.037	3
267	M2	1	max	2365.216	1	624.486	3	173.27	1	.002	3	.175	3	7.819	1
268			min	-1159.406	3	-380.201	2	-133.356	3	-.005	1	-.278	1	.292	15
269		2	max	2362.294	1	624.486	3	173.27	1	.002	3	.133	3	7.823	1
270			min	-1161.597	3	-380.201	2	-133.356	3	-.005	1	-.222	1	.289	15
271		3	max	2359.372	1	624.486	3	173.27	1	.002	3	.09	3	7.827	1
272			min	-1163.789	3	-380.201	2	-133.356	3	-.005	1	-.167	1	.286	15
273		4	max	2356.45	1	624.486	3	173.27	1	.002	3	.047	3	7.831	1
274			min	-1165.98	3	-380.201	2	-133.356	3	-.005	1	-.111	1	.283	15
275		5	max	1882.76	1	1681.264	1	132.627	1	.002	1	.023	3	7.552	1
276			min	-1013.92	3	51.318	12	-121.266	3	0	3	-.109	1	.231	12
277		6	max	1879.838	1	1681.264	1	132.627	1	.002	1	-.002	15	7.013	1
278			min	-1016.112	3	51.318	12	-121.266	3	0	3	-.067	1	.214	12
279		7	max	1876.917	1	1681.264	1	132.627	1	.002	1	.004	10	6.473	1
280			min	-1018.303	3	51.318	12	-121.266	3	0	3	-.055	3	.198	12
281		8	max	1873.995	1	1681.264	1	132.627	1	.002	1	.034	2	5.934	1
282			min	-1020.494	3	51.318	12	-121.266	3	0	3	-.094	3	.181	12
283		9	max	1871.073	1	1681.264	1	132.627	1	.002	1	.068	2	5.395	1
284			min	-1022.686	3	51.318	12	-121.266	3	0	3	-.133	3	.165	12
285		10	max	1868.151	1	1681.264	1	132.627	1	.002	1	.104	1	4.855	1
286			min	-1024.877	3	51.318	12	-121.266	3	0	3	-.172	3	.148	12
287		11	max	1865.23	1	1681.264	1	132.627	1	.002	1	.146	1	4.316	1
288			min	-1027.068	3	51.318	12	-121.266	3	0	3	-.211	3	.132	12
289		12	max	1862.308	1	1681.264	1	132.627	1	.002	1	.189	1	3.776	1
290			min	-1029.26	3	51.318	12	-121.266	3	0	3	-.25	3	.115	12
291		13	max	1859.386	1	1681.264	1	132.627	1	.002	1	.231	1	3.237	1
292			min	-1031.451	3	51.318	12	-121.266	3	0	3	-.289	3	.099	12
293		14	max	1856.464	1	1681.264	1	132.627	1	.002	1	.274	1	2.697	1
294			min	-1033.642	3	51.318	12	-121.266	3	0	3	-.327	3	.082	12
295		15	max	1853.543	1	1681.264	1	132.627	1	.002	1	.316	1	2.158	1
296			min	-1035.833	3	51.318	12	-121.266	3	0	3	-.366	3	.066	12
297		16	max	1850.621	1	1681.264	1	132.627	1	.002	1	.359	1	1.618	1
298			min	-1038.025	3	51.318	12	-121.266	3	0	3	-.405	3	.049	12
299		17	max	1847.699	1	1681.264	1	132.627	1	.002	1	.402	1	1.079	1
300			min	-1040.216	3	51.318	12	-121.266	3	0	3	-.444	3	.033	12
301		18	max	1844.777	1	1681.264	1	132.627	1	.002	1	.444	1	.539	1
302			min	-1042.407	3	51.318	12	-121.266	3	0	3	-.483	3	.016	12
303		19	max	1841.856	1	1681.264	1	132.627	1	.002	1	.487	1	0	1
304			min	-1044.599	3	51.318	12	-121.266	3	0	3	-.522	3	0	1
305	M5	1	max	6170.14	1	1809.275	3	0	1	0	1	0	1	13.962	1
306			min	-3554.009	3	-1898.295	2	0	1	0	1	0	1	.482	15
307		2	max	6167.219	1	1809.275	3	0	1	0	1	0	1	14.374	1
308			min	-3556.201	3	-1898.295	2	0	1	0	1	0	1	.487	15
309		3	max	6164.297	1	1809.275	3	0	1	0	1	0	1	14.785	1
310			min	-3558.392	3	-1898.295	2	0	1	0	1	0	1	.493	15
311		4	max	6161.375	1	1809.275	3	0	1	0	1	0	1	15.197	1
312			min	-3560.583	3	-1898.295	2	0	1	0	1	0	1	.181	12
313		5	max	4946.057	1	3304.497	1	0	1	0	1	0	1	14.844	1
314			min	-3042.694	3	-9.423	3	0	1	0	1	0	1	-.042	3
315		6	max	4943.135	1	3304.497	1	0	1	0	1	0	1	13.784	1
316			min	-3044.885	3	-9.423	3	0	1	0	1	0	1	-.039	3
317		7	max	4940.214	1	3304.497	1	0	1	0	1	0	1	12.724	1

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
318			min	-3047.076	3	-9.423	3	0	1	0	1	0	1	-.036	3
319		8	max	4937.292	1	3304.497	1	0	1	0	1	0	1	11.663	1
320			min	-3049.268	3	-9.423	3	0	1	0	1	0	1	-.033	3
321		9	max	4934.37	1	3304.497	1	0	1	0	1	0	1	10.603	1
322			min	-3051.459	3	-9.423	3	0	1	0	1	0	1	-.03	3
323		10	max	4931.448	1	3304.497	1	0	1	0	1	0	1	9.543	1
324			min	-3053.65	3	-9.423	3	0	1	0	1	0	1	-.027	3
325		11	max	4928.527	1	3304.497	1	0	1	0	1	0	1	8.482	1
326			min	-3055.842	3	-9.423	3	0	1	0	1	0	1	-.024	3
327		12	max	4925.605	1	3304.497	1	0	1	0	1	0	1	7.422	1
328			min	-3058.033	3	-9.423	3	0	1	0	1	0	1	-.021	3
329		13	max	4922.683	1	3304.497	1	0	1	0	1	0	1	6.362	1
330			min	-3060.224	3	-9.423	3	0	1	0	1	0	1	-.018	3
331		14	max	4919.762	1	3304.497	1	0	1	0	1	0	1	5.301	1
332			min	-3062.416	3	-9.423	3	0	1	0	1	0	1	-.015	3
333		15	max	4916.84	1	3304.497	1	0	1	0	1	0	1	4.241	1
334			min	-3064.607	3	-9.423	3	0	1	0	1	0	1	-.012	3
335		16	max	4913.918	1	3304.497	1	0	1	0	1	0	1	3.181	1
336			min	-3066.798	3	-9.423	3	0	1	0	1	0	1	-.009	3
337		17	max	4910.996	1	3304.497	1	0	1	0	1	0	1	2.121	1
338			min	-3068.989	3	-9.423	3	0	1	0	1	0	1	-.006	3
339		18	max	4908.075	1	3304.497	1	0	1	0	1	0	1	1.06	1
340			min	-3071.181	3	-9.423	3	0	1	0	1	0	1	-.003	3
341		19	max	4905.153	1	3304.497	1	0	1	0	1	0	1	0	1
342			min	-3073.372	3	-9.423	3	0	1	0	1	0	1	0	1
343	M8	1	max	2365.216	1	624.486	3	133.356	3	.005	1	.278	1	7.819	1
344			min	-1159.406	3	-380.201	2	-173.27	1	-.002	3	-.175	3	.292	15
345		2	max	2362.294	1	624.486	3	133.356	3	.005	1	.222	1	7.823	1
346			min	-1161.597	3	-380.201	2	-173.27	1	-.002	3	-.133	3	.289	15
347		3	max	2359.372	1	624.486	3	133.356	3	.005	1	.167	1	7.827	1
348			min	-1163.789	3	-380.201	2	-173.27	1	-.002	3	-.09	3	.286	15
349		4	max	2356.45	1	624.486	3	133.356	3	.005	1	.111	1	7.831	1
350			min	-1165.98	3	-380.201	2	-173.27	1	-.002	3	-.047	3	.283	15
351		5	max	1882.76	1	1681.264	1	121.266	3	0	3	.109	1	7.552	1
352			min	-1013.92	3	51.318	12	-132.627	1	-.002	1	-.023	3	.231	12
353		6	max	1879.838	1	1681.264	1	121.266	3	0	3	.067	1	7.013	1
354			min	-1016.112	3	51.318	12	-132.627	1	-.002	1	.002	15	.214	12
355		7	max	1876.917	1	1681.264	1	121.266	3	0	3	.055	3	6.473	1
356			min	-1018.303	3	51.318	12	-132.627	1	-.002	1	-.004	10	.198	12
357		8	max	1873.995	1	1681.264	1	121.266	3	0	3	.094	3	5.934	1
358			min	-1020.494	3	51.318	12	-132.627	1	-.002	1	-.034	2	.181	12
359		9	max	1871.073	1	1681.264	1	121.266	3	0	3	.133	3	5.395	1
360			min	-1022.686	3	51.318	12	-132.627	1	-.002	1	-.068	2	.165	12
361		10	max	1868.151	1	1681.264	1	121.266	3	0	3	.172	3	4.855	1
362			min	-1024.877	3	51.318	12	-132.627	1	-.002	1	-.104	1	.148	12
363		11	max	1865.23	1	1681.264	1	121.266	3	0	3	.211	3	4.316	1
364			min	-1027.068	3	51.318	12	-132.627	1	-.002	1	-.146	1	.132	12
365		12	max	1862.308	1	1681.264	1	121.266	3	0	3	.25	3	3.776	1
366			min	-1029.26	3	51.318	12	-132.627	1	-.002	1	-.189	1	.115	12
367		13	max	1859.386	1	1681.264	1	121.266	3	0	3	.289	3	3.237	1
368			min	-1031.451	3	51.318	12	-132.627	1	-.002	1	-.231	1	.099	12
369		14	max	1856.464	1	1681.264	1	121.266	3	0	3	.327	3	2.697	1
370			min	-1033.642	3	51.318	12	-132.627	1	-.002	1	-.274	1	.082	12
371		15	max	1853.543	1	1681.264	1	121.266	3	0	3	.366	3	2.158	1
372			min	-1035.833	3	51.318	12	-132.627	1	-.002	1	-.316	1	.066	12
373		16	max	1850.621	1	1681.264	1	121.266	3	0	3	.405	3	1.618	1
374			min	-1038.025	3	51.318	12	-132.627	1	-.002	1	-.359	1	.049	12

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
375		17	max	1847.699	1	1681.264	1	121.266	3	0	3	.444	3	1.079	1
376			min	-1040.216	3	51.318	12	-132.627	1	-.002	1	-.402	1	.033	12
377		18	max	1844.777	1	1681.264	1	121.266	3	0	3	.483	3	.539	1
378			min	-1042.407	3	51.318	12	-132.627	1	-.002	1	-.444	1	.016	12
379		19	max	1841.856	1	1681.264	1	121.266	3	0	3	.522	3	0	1
380			min	-1044.599	3	51.318	12	-132.627	1	-.002	1	-.487	1	0	1
381	M3	1	max	1744.876	1	5.879	4	39.778	1	.016	3	.006	1	0	1
382			min	-570.197	3	1.382	15	-12.472	3	-.047	1	-.002	3	0	1
383		2	max	1744.729	1	5.226	4	39.778	1	.016	3	.02	1	0	15
384			min	-570.307	3	1.228	15	-12.472	3	-.047	1	-.007	3	-.002	4
385		3	max	1744.582	1	4.572	4	39.778	1	.016	3	.035	1	0	15
386			min	-570.417	3	1.075	15	-12.472	3	-.047	1	-.011	3	-.004	4
387		4	max	1744.436	1	3.919	4	39.778	1	.016	3	.049	1	-.001	15
388			min	-570.527	3	.921	15	-12.472	3	-.047	1	-.016	3	-.005	4
389		5	max	1744.289	1	3.266	4	39.778	1	.016	3	.063	1	-.002	15
390			min	-570.637	3	.768	15	-12.472	3	-.047	1	-.02	3	-.007	4
391		6	max	1744.143	1	2.613	4	39.778	1	.016	3	.077	1	-.002	15
392			min	-570.747	3	.614	15	-12.472	3	-.047	1	-.024	3	-.008	4
393		7	max	1743.996	1	1.96	4	39.778	1	.016	3	.091	1	-.002	15
394			min	-570.857	3	.461	15	-12.472	3	-.047	1	-.029	3	-.008	4
395		8	max	1743.849	1	1.306	4	39.778	1	.016	3	.106	1	-.002	15
396			min	-570.967	3	.307	15	-12.472	3	-.047	1	-.033	3	-.009	4
397		9	max	1743.703	1	.653	4	39.778	1	.016	3	.12	1	-.002	15
398			min	-571.077	3	.154	15	-12.472	3	-.047	1	-.038	3	-.009	4
399		10	max	1743.556	1	0	1	39.778	1	.016	3	.134	1	-.002	15
400			min	-571.187	3	0	1	-12.472	3	-.047	1	-.042	3	-.009	4
401		11	max	1743.409	1	-.154	15	39.778	1	.016	3	.148	1	-.002	15
402			min	-571.297	3	-.653	4	-12.472	3	-.047	1	-.047	3	-.009	4
403		12	max	1743.263	1	-.307	15	39.778	1	.016	3	.162	1	-.002	15
404			min	-571.407	3	-1.306	4	-12.472	3	-.047	1	-.051	3	-.009	4
405		13	max	1743.116	1	-.461	15	39.778	1	.016	3	.177	1	-.002	15
406			min	-571.517	3	-1.96	4	-12.472	3	-.047	1	-.056	3	-.008	4
407		14	max	1742.97	1	-.614	15	39.778	1	.016	3	.191	1	-.002	15
408			min	-571.627	3	-2.613	4	-12.472	3	-.047	1	-.06	3	-.008	4
409		15	max	1742.823	1	-.768	15	39.778	1	.016	3	.205	1	-.002	15
410			min	-571.737	3	-3.266	4	-12.472	3	-.047	1	-.065	3	-.007	4
411		16	max	1742.676	1	-.921	15	39.778	1	.016	3	.219	1	-.001	15
412			min	-571.847	3	-3.919	4	-12.472	3	-.047	1	-.069	3	-.005	4
413		17	max	1742.53	1	-1.075	15	39.778	1	.016	3	.233	1	0	15
414			min	-571.957	3	-4.572	4	-12.472	3	-.047	1	-.073	3	-.004	4
415		18	max	1742.383	1	-1.228	15	39.778	1	.016	3	.248	1	0	15
416			min	-572.066	3	-5.226	4	-12.472	3	-.047	1	-.078	3	-.002	4
417		19	max	1742.237	1	-1.382	15	39.778	1	.016	3	.262	1	0	1
418			min	-572.176	3	-5.879	4	-12.472	3	-.047	1	-.082	3	0	1
419	M6	1	max	4678.079	1	5.879	4	0	1	0	1	0	1	0	1
420			min	-1891.626	3	1.382	15	0	1	0	1	0	1	0	1
421		2	max	4677.932	1	5.226	4	0	1	0	1	0	1	0	15
422			min	-1891.736	3	1.228	15	0	1	0	1	0	1	-.002	4
423		3	max	4677.786	1	4.572	4	0	1	0	1	0	1	0	15
424			min	-1891.846	3	1.075	15	0	1	0	1	0	1	-.004	4
425		4	max	4677.639	1	3.919	4	0	1	0	1	0	1	-.001	15
426			min	-1891.956	3	.921	15	0	1	0	1	0	1	-.005	4
427		5	max	4677.492	1	3.266	4	0	1	0	1	0	1	-.002	15
428			min	-1892.066	3	.768	15	0	1	0	1	0	1	-.007	4
429		6	max	4677.346	1	2.613	4	0	1	0	1	0	1	-.002	15
430			min	-1892.176	3	.614	15	0	1	0	1	0	1	-.008	4
431		7	max	4677.199	1	1.96	4	0	1	0	1	0	1	-.002	15

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
432			min	-1892.286	3	.461	15	0	1	0	1	0	1	-.008	4
433		8	max	4677.053	1	1.306	4	0	1	0	1	0	1	-.002	15
434			min	-1892.396	3	.307	15	0	1	0	1	0	1	-.009	4
435		9	max	4676.906	1	.653	4	0	1	0	1	0	1	-.002	15
436			min	-1892.505	3	.154	15	0	1	0	1	0	1	-.009	4
437		10	max	4676.759	1	0	1	0	1	0	1	0	1	-.002	15
438			min	-1892.615	3	0	1	0	1	0	1	0	1	-.009	4
439		11	max	4676.613	1	-.154	15	0	1	0	1	0	1	-.002	15
440			min	-1892.725	3	-.653	4	0	1	0	1	0	1	-.009	4
441		12	max	4676.466	1	-.307	15	0	1	0	1	0	1	-.002	15
442			min	-1892.835	3	-1.306	4	0	1	0	1	0	1	-.009	4
443		13	max	4676.32	1	-.461	15	0	1	0	1	0	1	-.002	15
444			min	-1892.945	3	-1.96	4	0	1	0	1	0	1	-.008	4
445		14	max	4676.173	1	-.614	15	0	1	0	1	0	1	-.002	15
446			min	-1893.055	3	-2.613	4	0	1	0	1	0	1	-.008	4
447		15	max	4676.026	1	-.768	15	0	1	0	1	0	1	-.002	15
448			min	-1893.165	3	-3.266	4	0	1	0	1	0	1	-.007	4
449		16	max	4675.88	1	-.921	15	0	1	0	1	0	1	-.001	15
450			min	-1893.275	3	-3.919	4	0	1	0	1	0	1	-.005	4
451		17	max	4675.733	1	-1.075	15	0	1	0	1	0	1	0	15
452			min	-1893.385	3	-4.572	4	0	1	0	1	0	1	-.004	4
453		18	max	4675.586	1	-1.228	15	0	1	0	1	0	1	0	15
454			min	-1893.495	3	-5.226	4	0	1	0	1	0	1	-.002	4
455		19	max	4675.44	1	-1.382	15	0	1	0	1	0	1	0	1
456			min	-1893.605	3	-5.879	4	0	1	0	1	0	1	0	1
457	M9	1	max	1744.876	1	5.879	4	12.472	3	.047	1	.002	3	0	1
458			min	-570.197	3	1.382	15	-39.778	1	-.016	3	-.006	1	0	1
459		2	max	1744.729	1	5.226	4	12.472	3	.047	1	.007	3	0	15
460			min	-570.307	3	1.228	15	-39.778	1	-.016	3	-.02	1	-.002	4
461		3	max	1744.582	1	4.572	4	12.472	3	.047	1	.011	3	0	15
462			min	-570.417	3	1.075	15	-39.778	1	-.016	3	-.035	1	-.004	4
463		4	max	1744.436	1	3.919	4	12.472	3	.047	1	.016	3	-.001	15
464			min	-570.527	3	.921	15	-39.778	1	-.016	3	-.049	1	-.005	4
465		5	max	1744.289	1	3.266	4	12.472	3	.047	1	.02	3	-.002	15
466			min	-570.637	3	.768	15	-39.778	1	-.016	3	-.063	1	-.007	4
467		6	max	1744.143	1	2.613	4	12.472	3	.047	1	.024	3	-.002	15
468			min	-570.747	3	.614	15	-39.778	1	-.016	3	-.077	1	-.008	4
469		7	max	1743.996	1	1.96	4	12.472	3	.047	1	.029	3	-.002	15
470			min	-570.857	3	.461	15	-39.778	1	-.016	3	-.091	1	-.008	4
471		8	max	1743.849	1	1.306	4	12.472	3	.047	1	.033	3	-.002	15
472			min	-570.967	3	.307	15	-39.778	1	-.016	3	-.106	1	-.009	4
473		9	max	1743.703	1	.653	4	12.472	3	.047	1	.038	3	-.002	15
474			min	-571.077	3	.154	15	-39.778	1	-.016	3	-.12	1	-.009	4
475		10	max	1743.556	1	0	1	12.472	3	.047	1	.042	3	-.002	15
476			min	-571.187	3	0	1	-39.778	1	-.016	3	-.134	1	-.009	4
477		11	max	1743.409	1	-.154	15	12.472	3	.047	1	.047	3	-.002	15
478			min	-571.297	3	-.653	4	-39.778	1	-.016	3	-.148	1	-.009	4
479		12	max	1743.263	1	-.307	15	12.472	3	.047	1	.051	3	-.002	15
480			min	-571.407	3	-1.306	4	-39.778	1	-.016	3	-.162	1	-.009	4
481		13	max	1743.116	1	-.461	15	12.472	3	.047	1	.056	3	-.002	15
482			min	-571.517	3	-1.96	4	-39.778	1	-.016	3	-.177	1	-.008	4
483		14	max	1742.97	1	-.614	15	12.472	3	.047	1	.06	3	-.002	15
484			min	-571.627	3	-2.613	4	-39.778	1	-.016	3	-.191	1	-.008	4
485		15	max	1742.823	1	-.768	15	12.472	3	.047	1	.065	3	-.002	15
486			min	-571.737	3	-3.266	4	-39.778	1	-.016	3	-.205	1	-.007	4
487		16	max	1742.676	1	-.921	15	12.472	3	.047	1	.069	3	-.001	15
488			min	-571.847	3	-3.919	4	-39.778	1	-.016	3	-.219	1	-.005	4

Envelope Member Section Forces (Continued)

	Member	Sec		Axial[lb]	LC	y Shear[lb]	LC	z Shear[lb]	LC	Torque[k-ft]	LC	y-y Mome...	LC	z-z Mome...	LC
489		17	max	1742.53	1	-1.075	15	12.472	3	.047	1	.073	3	0	15
490			min	-571.957	3	-4.572	4	-39.778	1	-.016	3	-.233	1	-.004	4
491		18	max	1742.383	1	-1.228	15	12.472	3	.047	1	.078	3	0	15
492			min	-572.066	3	-5.226	4	-39.778	1	-.016	3	-.248	1	-.002	4
493		19	max	1742.237	1	-1.382	15	12.472	3	.047	1	.082	3	0	1
494			min	-572.176	3	-5.879	4	-39.778	1	-.016	3	-.262	1	0	1

Envelope Member Section Deflections

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
1	M1	1	max	-.019	15	.041	3	.015	1	7.556e-3	3	NC	3	NC	1
2			min	-.517	1	-1.069	1	0	12	-2.69e-2	1	99.383	1	NC	1
3		2	max	-.019	15	.02	3	0	12	7.315e-3	3	NC	12	NC	2
4			min	-.517	1	-.927	1	-.01	1	-2.557e-2	1	110.377	1	6018.406	1
5		3	max	-.019	15	0	3	0	12	6.841e-3	3	5738.119	12	NC	3
6			min	-.517	1	-.788	1	-.023	1	-2.294e-2	1	123.763	1	4077.177	1
7		4	max	-.019	15	-.012	12	0	3	6.368e-3	3	4079.013	12	NC	3
8			min	-.517	1	-.658	1	-.026	1	-2.031e-2	1	139.548	1	3920.994	1
9		5	max	-.019	15	-.018	12	.002	3	6.131e-3	3	4192.382	15	NC	3
10			min	-.516	1	-.544	1	-.023	1	-1.843e-2	1	157.179	1	4437.215	1
11		6	max	-.019	15	-.016	15	.002	3	6.504e-3	3	4636.456	15	NC	3
12			min	-.516	1	-.448	1	-.015	1	-1.844e-2	1	175.843	1	6354.987	1
13		7	max	-.019	15	-.014	15	.002	3	6.876e-3	3	5122.708	15	NC	1
14			min	-.515	1	-.365	1	-.005	1	-1.846e-2	1	196.091	1	NC	1
15		8	max	-.019	15	-.011	15	0	1	7.248e-3	3	5682.805	15	NC	1
16			min	-.515	1	-.289	1	0	10	-1.847e-2	1	219.239	1	NC	1
17		9	max	-.019	15	-.008	15	0	10	7.951e-3	3	6376.581	15	NC	1
18			min	-.514	1	-.214	1	0	3	-1.762e-2	1	248.056	1	NC	1
19		10	max	-.019	15	-.005	15	.001	1	8.965e-3	3	7286.113	15	NC	1
20			min	-.513	1	-.137	1	-.001	3	-1.594e-2	1	286.386	1	NC	1
21		11	max	-.019	15	-.003	15	.001	1	9.979e-3	3	8528.165	15	NC	1
22			min	-.512	1	-.06	1	0	3	-1.426e-2	1	339.689	1	NC	1
23		12	max	-.019	15	.019	1	.004	3	9.29e-3	3	NC	15	NC	1
24			min	-.512	1	-.023	3	-.006	1	-1.179e-2	1	418.989	1	NC	1
25		13	max	-.019	15	.097	1	.009	3	6.794e-3	3	NC	15	NC	1
26			min	-.511	1	-.02	3	-.009	1	-8.47e-3	1	544.146	1	NC	1
27		14	max	-.019	15	.169	1	.014	3	4.297e-3	3	NC	5	NC	1
28			min	-.51	1	-.009	3	-.007	2	-5.153e-3	1	750.741	1	9526.609	3
29		15	max	-.018	15	.23	1	.014	3	1.801e-3	3	NC	5	NC	1
30			min	-.509	1	.008	15	-.002	2	-1.836e-3	1	1106.944	1	9498.172	3
31		16	max	-.018	15	.275	1	.013	1	4.698e-3	3	NC	3	NC	2
32			min	-.509	1	.01	15	0	15	-3.552e-3	1	1712.023	1	6762.623	1
33		17	max	-.018	15	.308	1	.016	1	8.227e-3	3	NC	5	NC	2
34			min	-.509	1	.012	15	0	15	-5.857e-3	1	2229.332	3	5528.307	1
35		18	max	-.019	15	.334	1	.008	1	1.176e-2	3	NC	2	NC	2
36			min	-.509	1	.013	15	0	15	-8.163e-3	1	1146.829	3	7336.516	1
37		19	max	-.019	15	.358	1	0	15	1.356e-2	3	NC	1	NC	1
38			min	-.509	1	.014	15	-.013	1	-9.339e-3	1	761.217	3	NC	1
39	M4	1	max	-.015	12	.194	3	0	1	0	1	NC	3	NC	1
40			min	-.998	1	-2.149	1	0	1	0	1	52.571	1	NC	1
41		2	max	-.015	12	.134	3	0	1	0	1	3882.002	12	NC	1
42			min	-.998	1	-1.853	1	0	1	0	1	59.062	1	NC	1
43		3	max	-.015	12	.078	3	0	1	0	1	2045.926	15	NC	1
44			min	-.998	1	-1.563	1	0	1	0	1	67.165	1	NC	1
45		4	max	-.015	12	.03	3	0	1	0	1	2312.152	15	NC	1
46			min	-.998	1	-1.297	1	0	1	0	1	76.884	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
47		5	max	-.015	12	-.001	3	0	1	0	1	2607.101	15	NC	1
48			min	-.997	1	-1.069	1	0	1	0	1	87.717	1	NC	1
49		6	max	-.016	12	-.011	12	0	1	0	1	2913.747	15	NC	1
50			min	-.996	1	-.887	1	0	1	0	1	98.858	1	NC	1
51		7	max	-.016	12	-.012	12	0	1	0	1	3243.445	15	NC	1
52			min	-.994	1	-.734	1	0	1	0	1	110.625	1	NC	1
53		8	max	-.016	12	-.009	12	0	1	0	1	3624.036	15	NC	1
54			min	-.992	1	-.596	1	0	1	0	1	124.025	1	NC	1
55		9	max	-.017	12	-.007	12	0	1	0	1	4114.953	15	NC	1
56			min	-.991	1	-.456	1	0	1	0	1	141.4	1	NC	1
57		10	max	-.017	12	-.008	12	0	1	0	1	4803.671	15	NC	1
58			min	-.989	1	-.306	1	0	1	0	1	166.218	1	NC	1
59		11	max	-.018	12	-.005	15	0	1	0	1	5824.534	15	NC	1
60			min	-.987	1	-.149	1	0	1	0	1	203.836	1	NC	1
61		12	max	-.018	12	.016	1	0	1	0	1	7481.671	15	NC	1
62			min	-.985	1	-.03	3	0	1	0	1	267.017	1	NC	1
63		13	max	-.018	12	.18	1	0	1	0	1	NC	15	NC	1
64			min	-.984	1	-.039	3	0	1	0	1	386.219	1	NC	1
65		14	max	-.019	12	.327	1	0	1	0	1	NC	5	NC	1
66			min	-.982	1	-.03	3	0	1	0	1	632.529	3	NC	1
67		15	max	-.019	12	.441	1	0	1	0	1	NC	5	NC	1
68			min	-.98	1	.007	12	0	1	0	1	769.833	3	NC	1
69		16	max	-.019	12	.508	1	0	1	0	1	NC	2	NC	1
70			min	-.98	1	.017	15	0	1	0	1	1429.876	3	NC	1
71		17	max	-.019	12	.538	1	0	1	0	1	NC	1	NC	1
72			min	-.98	1	.018	15	0	1	0	1	6785.58	3	NC	1
73		18	max	-.019	12	.546	1	0	1	0	1	NC	1	NC	1
74			min	-.98	1	.019	15	0	1	0	1	876.855	3	NC	1
75		19	max	-.019	12	.547	1	0	1	0	1	NC	1	NC	1
76			min	-.98	1	.019	15	0	1	0	1	459.088	3	NC	1
77	M7	1	max	-.019	15	.041	3	0	12	2.69e-2	1	NC	3	NC	1
78			min	-.517	1	-1.069	1	-.015	1	-7.556e-3	3	99.383	1	NC	1
79		2	max	-.019	15	.02	3	.01	1	2.557e-2	1	NC	12	NC	2
80			min	-.517	1	-.927	1	0	12	-7.315e-3	3	110.377	1	6018.406	1
81		3	max	-.019	15	0	3	.023	1	2.294e-2	1	5738.119	12	NC	3
82			min	-.517	1	-.788	1	0	12	-6.841e-3	3	123.763	1	4077.177	1
83		4	max	-.019	15	-.012	12	.026	1	2.031e-2	1	4079.013	12	NC	3
84			min	-.517	1	-.658	1	0	3	-6.368e-3	3	139.548	1	3920.994	1
85		5	max	-.019	15	-.018	12	.023	1	1.843e-2	1	4192.382	15	NC	3
86			min	-.516	1	-.544	1	-.002	3	-6.131e-3	3	157.179	1	4437.215	1
87		6	max	-.019	15	-.016	15	.015	1	1.844e-2	1	4636.456	15	NC	3
88			min	-.516	1	-.448	1	-.002	3	-6.504e-3	3	175.843	1	6354.987	1
89		7	max	-.019	15	-.014	15	.005	1	1.846e-2	1	5122.708	15	NC	1
90			min	-.515	1	-.365	1	-.002	3	-6.876e-3	3	196.091	1	NC	1
91		8	max	-.019	15	-.011	15	0	10	1.847e-2	1	5682.805	15	NC	1
92			min	-.515	1	-.289	1	0	1	-7.248e-3	3	219.239	1	NC	1
93		9	max	-.019	15	-.008	15	0	3	1.762e-2	1	6376.581	15	NC	1
94			min	-.514	1	-.214	1	0	10	-7.951e-3	3	248.056	1	NC	1
95		10	max	-.019	15	-.005	15	.001	3	1.594e-2	1	7286.113	15	NC	1
96			min	-.513	1	-.137	1	-.001	1	-8.965e-3	3	286.386	1	NC	1
97		11	max	-.019	15	-.003	15	0	3	1.426e-2	1	8528.165	15	NC	1
98			min	-.512	1	-.06	1	-.001	1	-9.979e-3	3	339.689	1	NC	1
99		12	max	-.019	15	.019	1	.006	1	1.179e-2	1	NC	15	NC	1
100			min	-.512	1	-.023	3	-.004	3	-9.29e-3	3	418.989	1	NC	1
101		13	max	-.019	15	.097	1	.009	1	8.47e-3	1	NC	15	NC	1
102			min	-.511	1	-.02	3	-.009	3	-6.794e-3	3	544.146	1	NC	1
103		14	max	-.019	15	.169	1	.007	2	5.153e-3	1	NC	5	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
104			min	-.51	1	-.009	3	-.014	3	-4.297e-3	3	750.741	1	9526.609	3
105		15	max	-.018	15	.23	1	.002	2	1.836e-3	1	NC	5	NC	1
106			min	-.509	1	.008	15	-.014	3	-1.801e-3	3	1106.944	1	9498.172	3
107		16	max	-.018	15	.275	1	0	15	3.552e-3	1	NC	3	NC	2
108			min	-.509	1	.01	15	-.013	1	-4.698e-3	3	1712.023	1	6762.623	1
109		17	max	-.018	15	.308	1	0	15	5.857e-3	1	NC	5	NC	2
110			min	-.509	1	.012	15	-.016	1	-8.227e-3	3	2229.332	3	5528.307	1
111		18	max	-.019	15	.334	1	0	15	8.163e-3	1	NC	2	NC	2
112			min	-.509	1	.013	15	-.008	1	-1.176e-2	3	1146.829	3	7336.516	1
113		19	max	-.019	15	.358	1	.013	1	9.339e-3	1	NC	1	NC	1
114			min	-.509	1	.014	15	0	15	-1.356e-2	3	761.217	3	NC	1
115	M10	1	max	.001	1	.346	1	.509	1	7.934e-3	3	NC	1	NC	1
116			min	0	12	.014	15	.019	15	1.514e-4	15	NC	1	NC	1
117		2	max	.001	1	.373	3	.578	1	9.121e-3	3	NC	5	NC	3
118			min	0	12	.01	15	.021	15	1.409e-4	15	1292.157	3	3340.357	1
119		3	max	.001	1	.535	3	.683	1	1.031e-2	3	NC	5	NC	3
120			min	0	12	.007	15	.025	15	1.305e-4	15	674.777	3	1310.349	1
121		4	max	0	1	.653	3	.796	1	1.149e-2	3	NC	5	NC	3
122			min	0	12	-.005	10	.029	15	1.2e-4	15	499.877	3	795.344	1
123		5	max	0	1	.712	3	.894	1	1.268e-2	3	NC	5	NC	3
124			min	0	12	-.004	10	.031	12	7.726e-5	10	442.499	3	593.401	1
125		6	max	0	1	.708	3	.963	1	1.387e-2	3	NC	5	NC	3
126			min	0	12	.007	15	.03	12	-5.681e-5	10	445.481	3	503.135	1
127		7	max	0	1	.651	3	.998	1	1.506e-2	3	NC	4	NC	3
128			min	0	12	.01	15	.027	12	-1.909e-4	10	501.547	3	466.755	1
129		8	max	0	1	.561	3	1.003	1	1.624e-2	3	NC	2	NC	3
130			min	0	12	.014	15	.023	12	-3.249e-4	10	625.002	3	461.799	1
131		9	max	0	1	.494	1	.99	1	1.743e-2	3	NC	5	NC	3
132			min	0	12	.018	15	.02	12	-4.91e-4	2	826.248	3	474.064	1
133		10	max	0	1	.546	1	.98	1	1.862e-2	3	NC	5	NC	3
134			min	0	1	.019	15	.019	12	-7.502e-4	2	974.741	3	484.341	1
135		11	max	0	12	.494	1	.99	1	1.743e-2	3	NC	5	NC	3
136			min	0	1	.018	15	.02	12	-4.91e-4	2	826.248	3	474.064	1
137		12	max	0	12	.561	3	1.003	1	1.624e-2	3	NC	2	NC	3
138			min	0	1	.014	15	.023	12	-3.249e-4	10	625.002	3	461.799	1
139		13	max	0	12	.651	3	.998	1	1.506e-2	3	NC	4	NC	3
140			min	0	1	.01	15	.027	12	-1.909e-4	10	501.547	3	466.755	1
141		14	max	0	12	.708	3	.963	1	1.387e-2	3	NC	5	NC	3
142			min	0	1	.007	15	.03	12	-5.681e-5	10	445.481	3	503.135	1
143		15	max	0	12	.712	3	.894	1	1.268e-2	3	NC	5	NC	3
144			min	0	1	-.004	10	.031	12	7.726e-5	10	442.499	3	593.401	1
145		16	max	0	12	.653	3	.796	1	1.149e-2	3	NC	5	NC	3
146			min	0	1	-.005	10	.029	15	1.2e-4	15	499.877	3	795.344	1
147		17	max	0	12	.535	3	.683	1	1.031e-2	3	NC	5	NC	3
148			min	-.001	1	.007	15	.025	15	1.305e-4	15	674.777	3	1310.349	1
149		18	max	0	12	.373	3	.578	1	9.121e-3	3	NC	5	NC	3
150			min	-.001	1	.01	15	.021	15	1.409e-4	15	1292.157	3	3340.357	1
151		19	max	0	12	.346	1	.509	1	7.934e-3	3	NC	1	NC	1
152			min	-.001	1	.014	15	.019	15	1.514e-4	15	NC	1	NC	1
153	M11	1	max	.002	1	-.001	15	.512	1	1.001e-2	1	NC	1	NC	1
154			min	-.001	3	-.024	3	.019	15	1.536e-4	12	NC	1	NC	1
155		2	max	.002	1	.114	3	.563	1	1.122e-2	1	NC	5	NC	3
156			min	-.001	3	-.187	1	.02	12	3.112e-5	3	1354.986	1	4458.179	1
157		3	max	.002	1	.238	3	.66	1	1.242e-2	1	NC	5	NC	3
158			min	-.001	3	-.331	1	.02	12	-1.423e-4	3	732.14	1	1540.018	1
159		4	max	.001	1	.32	3	.771	1	1.362e-2	1	NC	5	NC	3
160			min	0	3	-.423	1	.021	12	-3.158e-4	3	564.023	1	882.042	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
161		5	max	.001	1	.346	3	.871	1	1.482e-2	1	NC	5	NC	3
162			min	0	3	-.453	1	.022	12	-4.892e-4	3	525.521	1	635.532	1
163		6	max	0	1	.313	3	.946	1	1.602e-2	1	NC	5	NC	3
164			min	0	3	-.419	1	.022	12	-6.627e-4	3	570.417	1	525.762	1
165		7	max	0	1	.232	3	.989	1	1.723e-2	1	NC	5	NC	3
166			min	0	3	-.333	1	.021	12	-8.361e-4	3	727.125	1	478.454	1
167		8	max	0	1	.123	3	1.001	1	1.843e-2	1	NC	5	NC	3
168			min	0	3	-.219	1	.02	12	-1.01e-3	3	1142.779	1	466.015	1
169		9	max	0	1	.022	3	.994	1	1.963e-2	1	NC	4	NC	3
170			min	0	3	-.113	1	.018	12	-1.183e-3	3	2426.208	1	472.83	1
171		10	max	0	1	-.002	15	.986	1	2.083e-2	1	NC	3	NC	3
172			min	0	1	-.065	1	.018	12	-1.356e-3	3	4990.788	1	480.716	1
173		11	max	0	3	.022	3	.994	1	1.963e-2	1	NC	4	NC	3
174			min	0	1	-.113	1	.018	12	-1.183e-3	3	2426.208	1	472.83	1
175		12	max	0	3	.123	3	1.001	1	1.843e-2	1	NC	5	NC	3
176			min	0	1	-.219	1	.02	12	-1.01e-3	3	1142.779	1	466.015	1
177		13	max	0	3	.232	3	.989	1	1.723e-2	1	NC	5	NC	3
178			min	0	1	-.333	1	.021	12	-8.361e-4	3	727.125	1	478.454	1
179		14	max	0	3	.313	3	.946	1	1.602e-2	1	NC	5	NC	3
180			min	0	1	-.419	1	.022	12	-6.627e-4	3	570.417	1	525.762	1
181		15	max	0	3	.346	3	.871	1	1.482e-2	1	NC	5	NC	3
182			min	-.001	1	-.453	1	.022	12	-4.892e-4	3	525.521	1	635.532	1
183		16	max	0	3	.32	3	.771	1	1.362e-2	1	NC	5	NC	3
184			min	-.001	1	-.423	1	.021	12	-3.158e-4	3	564.023	1	882.042	1
185		17	max	.001	3	.238	3	.66	1	1.242e-2	1	NC	5	NC	3
186			min	-.002	1	-.331	1	.02	12	-1.423e-4	3	732.14	1	1540.018	1
187		18	max	.001	3	.114	3	.563	1	1.122e-2	1	NC	5	NC	3
188			min	-.002	1	-.187	1	.02	12	3.112e-5	3	1354.986	1	4458.179	1
189		19	max	.001	3	-.001	15	.512	1	1.001e-2	1	NC	1	NC	1
190			min	-.002	1	-.024	3	.019	15	1.536e-4	12	NC	1	NC	1
191	M12	1	max	0	3	-.01	15	.514	1	9.561e-3	1	NC	1	NC	1
192			min	0	1	-.253	1	.019	15	2.146e-4	12	NC	1	NC	1
193		2	max	0	3	.059	3	.558	1	1.048e-2	1	NC	5	NC	3
194			min	0	1	-.484	1	.02	15	2.134e-4	12	983.813	1	5259.112	1
195		3	max	0	3	.13	3	.651	1	1.141e-2	1	NC	5	NC	3
196			min	0	1	-.686	1	.024	15	2.122e-4	12	526.759	1	1672.238	1
197		4	max	0	3	.172	3	.76	1	1.233e-2	1	NC	15	NC	3
198			min	0	1	-.826	1	.026	12	2.111e-4	12	397.398	1	927.017	1
199		5	max	0	3	.183	3	.862	1	1.325e-2	1	NC	15	NC	3
200			min	0	1	-.892	1	.027	12	2.099e-4	12	356.806	1	655.789	1
201		6	max	0	3	.163	3	.94	1	1.418e-2	1	NC	15	NC	3
202			min	0	1	-.88	1	.026	12	2.087e-4	12	363.463	1	535.791	1
203		7	max	0	3	.119	3	.986	1	1.51e-2	1	NC	15	NC	3
204			min	0	1	-.804	1	.023	12	2.076e-4	12	413.529	1	482.95	1
205		8	max	0	3	.063	3	1.003	1	1.602e-2	1	NC	5	NC	3
206			min	0	1	-.691	1	.021	12	2.064e-4	12	520.576	1	466.805	1
207		9	max	0	3	.012	3	.998	1	1.695e-2	1	NC	5	NC	3
208			min	0	1	-.581	1	.018	12	2.053e-4	12	694.964	1	470.954	1
209		10	max	0	1	-.008	12	.992	1	1.787e-2	1	NC	3	NC	3
210			min	0	1	-.529	1	.017	12	2.041e-4	12	824.202	1	477.676	1
211		11	max	0	1	.012	3	.998	1	1.695e-2	1	NC	5	NC	3
212			min	0	3	-.581	1	.018	12	2.053e-4	12	694.964	1	470.954	1
213		12	max	0	1	.063	3	1.003	1	1.602e-2	1	NC	5	NC	3
214			min	0	3	-.691	1	.021	12	2.064e-4	12	520.576	1	466.805	1
215		13	max	0	1	.119	3	.986	1	1.51e-2	1	NC	15	NC	3
216			min	0	3	-.804	1	.023	12	2.076e-4	12	413.529	1	482.95	1
217		14	max	0	1	.163	3	.94	1	1.418e-2	1	NC	15	NC	3

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
218			min	0	3	-.88	1	.026	12	2.087e-4	12	363.463	1	535.791	1
219		15	max	0	1	.183	3	.862	1	1.325e-2	1	NC	15	NC	3
220			min	0	3	-.892	1	.027	12	2.099e-4	12	356.806	1	655.789	1
221		16	max	0	1	.172	3	.76	1	1.233e-2	1	NC	15	NC	3
222			min	0	3	-.826	1	.026	12	2.111e-4	12	397.398	1	927.017	1
223		17	max	0	1	.13	3	.651	1	1.141e-2	1	NC	5	NC	3
224			min	0	3	-.686	1	.024	15	2.122e-4	12	526.759	1	1672.238	1
225		18	max	0	1	.059	3	.558	1	1.048e-2	1	NC	5	NC	3
226			min	0	3	-.484	1	.02	15	2.134e-4	12	983.813	1	5259.112	1
227		19	max	0	1	-.01	15	.514	1	9.561e-3	1	NC	1	NC	1
228			min	0	3	-.253	1	.019	15	2.146e-4	12	NC	1	NC	1
229	M13	1	max	0	3	.031	3	.517	1	1.802e-2	1	NC	1	NC	1
230			min	-.002	1	-.999	1	.019	15	-2.635e-3	3	NC	1	NC	1
231		2	max	0	3	.125	3	.591	1	2.019e-2	1	NC	5	NC	3
232			min	-.001	1	-1.34	1	.021	15	-3.177e-3	3	668.359	1	3085.188	1
233		3	max	0	3	.207	3	.7	1	2.236e-2	1	NC	15	NC	3
234			min	-.001	1	-1.653	1	.024	12	-3.719e-3	3	348.622	1	1243.13	1
235		4	max	0	3	.265	3	.815	1	2.453e-2	1	9245.055	15	NC	3
236			min	-.001	1	-1.904	1	.025	12	-4.261e-3	3	251.93	1	764.374	1
237		5	max	0	3	.293	3	.914	1	2.67e-2	1	7748.691	15	NC	3
238			min	0	1	-2.074	1	.025	12	-4.804e-3	3	212.161	1	574.575	1
239		6	max	0	3	.292	3	.983	1	2.887e-2	1	7148.633	15	NC	3
240			min	0	1	-2.157	1	.024	12	-5.346e-3	3	196.976	1	489.465	1
241		7	max	0	3	.266	3	1.018	1	3.104e-2	1	7062.435	15	NC	3
242			min	0	1	-2.161	1	.022	12	-5.888e-3	3	196.177	1	455.435	1
243		8	max	0	3	.224	3	1.022	1	3.321e-2	1	7314.517	15	NC	3
244			min	0	1	-2.111	1	.019	12	-6.43e-3	3	205.123	1	451.402	1
245		9	max	0	3	.184	3	1.009	1	3.538e-2	1	7728.311	15	NC	3
246			min	0	1	-2.041	1	.017	12	-6.973e-3	3	218.752	1	463.777	1
247		10	max	0	1	.165	3	.998	1	3.755e-2	1	7975.146	15	NC	3
248			min	0	1	-2.004	1	.015	12	-7.515e-3	3	226.784	1	473.913	1
249		11	max	0	1	.184	3	1.009	1	3.538e-2	1	7728.311	15	NC	3
250			min	0	3	-2.041	1	.017	12	-6.973e-3	3	218.752	1	463.777	1
251		12	max	0	1	.224	3	1.022	1	3.321e-2	1	7314.517	15	NC	3
252			min	0	3	-2.111	1	.019	12	-6.43e-3	3	205.123	1	451.402	1
253		13	max	0	1	.266	3	1.018	1	3.104e-2	1	7062.435	15	NC	3
254			min	0	3	-2.161	1	.022	12	-5.888e-3	3	196.177	1	455.435	1
255		14	max	0	1	.292	3	.983	1	2.887e-2	1	7148.633	15	NC	3
256			min	0	3	-2.157	1	.024	12	-5.346e-3	3	196.976	1	489.465	1
257		15	max	0	1	.293	3	.914	1	2.67e-2	1	7748.691	15	NC	3
258			min	0	3	-2.074	1	.025	12	-4.804e-3	3	212.161	1	574.575	1
259		16	max	.001	1	.265	3	.815	1	2.453e-2	1	9245.055	15	NC	3
260			min	0	3	-1.904	1	.025	12	-4.261e-3	3	251.93	1	764.374	1
261		17	max	.001	1	.207	3	.7	1	2.236e-2	1	NC	15	NC	3
262			min	0	3	-1.653	1	.024	12	-3.719e-3	3	348.622	1	1243.13	1
263		18	max	.001	1	.125	3	.591	1	2.019e-2	1	NC	5	NC	3
264			min	0	3	-1.34	1	.021	15	-3.177e-3	3	668.359	1	3085.188	1
265		19	max	.002	1	.031	3	.517	1	1.802e-2	1	NC	1	NC	1
266			min	0	3	-.999	1	.019	15	-2.635e-3	3	NC	1	NC	1
267	M2	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
268			min	0	1	0	1	0	1	0	1	NC	1	NC	1
269		2	max	0	3	0	15	0	3	1.737e-3	1	NC	1	NC	1
270			min	0	1	-.002	1	0	1	-5.676e-4	3	NC	1	NC	1
271		3	max	0	3	0	15	0	3	3.474e-3	1	NC	2	NC	1
272			min	0	1	-.009	1	0	1	-1.135e-3	3	7903.573	1	NC	1
273		4	max	0	3	0	15	0	3	5.212e-3	1	NC	3	NC	1
274			min	0	1	-.02	1	-.002	1	-1.703e-3	3	3511.744	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
275		5	max	0	3	-.001	15	.001	3	5.759e-3	1	NC	3	NC	1
276			min	0	1	-.035	1	-.002	1	-1.863e-3	3	1967.206	1	NC	1
277		6	max	0	3	-.002	15	.002	3	5.207e-3	1	NC	3	NC	1
278			min	0	1	-.055	1	-.004	1	-1.647e-3	3	1258.381	1	NC	1
279		7	max	0	3	-.003	15	.003	3	4.654e-3	1	NC	5	NC	1
280			min	0	1	-.079	1	-.005	1	-1.431e-3	3	878.976	1	NC	1
281		8	max	0	3	-.004	15	.003	3	4.102e-3	1	NC	5	NC	1
282			min	0	1	-.106	1	-.006	1	-1.215e-3	3	652.303	1	NC	1
283		9	max	0	3	-.005	15	.003	3	3.549e-3	1	NC	15	NC	1
284			min	0	1	-.137	1	-.007	1	-9.987e-4	3	505.979	1	NC	1
285		10	max	0	3	-.006	15	.003	3	2.997e-3	1	NC	15	NC	1
286			min	-.001	1	-.171	1	-.008	1	-7.825e-4	3	405.925	1	NC	1
287		11	max	0	3	-.008	15	.003	3	2.471e-3	2	9173.876	15	NC	1
288			min	-.001	1	-.207	1	-.009	1	-5.663e-4	3	334.461	1	NC	1
289		12	max	0	3	-.009	15	.003	3	1.985e-3	2	7730.448	15	NC	3
290			min	-.001	1	-.246	1	-.01	1	-3.502e-4	3	281.6	1	9435.152	1
291		13	max	0	3	-.01	15	.002	3	1.499e-3	2	6630.809	15	NC	3
292			min	-.001	1	-.287	1	-.01	1	-1.34e-4	3	241.376	1	9135.641	1
293		14	max	0	3	-.012	15	0	3	1.013e-3	2	5773.46	15	NC	3
294			min	-.002	1	-.33	1	-.01	1	1.387e-5	15	210.045	1	9242.662	1
295		15	max	0	3	-.014	15	0	15	5.266e-4	2	5091.898	15	NC	2
296			min	-.002	1	-.374	1	-.01	1	-2.579e-5	9	185.16	1	9873.454	1
297		16	max	0	3	-.015	15	0	15	5.145e-4	3	4541.285	15	NC	1
298			min	-.002	1	-.42	1	-.009	1	-3.18e-4	1	165.07	1	NC	1
299		17	max	.001	3	-.017	15	0	15	7.307e-4	3	4090.24	15	NC	1
300			min	-.002	1	-.466	1	-.008	1	-8.705e-4	1	148.624	1	NC	1
301		18	max	.001	3	-.019	15	0	10	9.468e-4	3	3716.353	15	NC	1
302			min	-.002	1	-.513	1	-.009	3	-1.423e-3	1	134.998	1	7657.807	3
303		19	max	.001	3	-.02	15	.002	10	1.163e-3	3	3403.27	15	NC	1
304			min	-.002	1	-.561	1	-.013	3	-1.975e-3	1	123.595	1	5283.501	3
305	M5	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
306			min	0	1	0	1	0	1	0	1	NC	1	NC	1
307		2	max	0	3	0	15	0	1	0	1	NC	1	NC	1
308			min	0	1	-.004	1	0	1	0	1	NC	1	NC	1
309		3	max	0	3	0	15	0	1	0	1	NC	3	NC	1
310			min	0	1	-.016	1	0	1	0	1	4451.212	1	NC	1
311		4	max	0	3	-.001	15	0	1	0	1	NC	3	NC	1
312			min	-.001	1	-.036	1	0	1	0	1	1942.664	1	NC	1
313		5	max	0	3	-.002	15	0	1	0	1	NC	3	NC	1
314			min	-.001	1	-.065	1	0	1	0	1	1071.697	1	NC	1
315		6	max	.001	3	-.003	15	0	1	0	1	NC	5	NC	1
316			min	-.002	1	-.102	1	0	1	0	1	677.467	1	NC	1
317		7	max	.001	3	-.005	15	0	1	0	1	NC	12	NC	1
318			min	-.002	1	-.148	1	0	1	0	1	469.378	1	NC	1
319		8	max	.001	3	-.007	15	0	1	0	1	NC	15	NC	1
320			min	-.002	1	-.2	1	0	1	0	1	346.295	1	NC	1
321		9	max	.002	3	-.009	15	0	1	0	1	8026.81	15	NC	1
322			min	-.003	1	-.259	1	0	1	0	1	267.431	1	NC	1
323		10	max	.002	3	-.01	12	0	1	0	1	6657.202	12	NC	1
324			min	-.003	1	-.324	1	0	1	0	1	213.814	1	NC	1
325		11	max	.002	3	-.012	12	0	1	0	1	5936.964	12	NC	1
326			min	-.003	1	-.394	1	0	1	0	1	175.693	1	NC	1
327		12	max	.002	3	-.013	12	0	1	0	1	5356.491	12	NC	1
328			min	-.003	1	-.47	1	0	1	0	1	147.6	1	NC	1
329		13	max	.002	3	-.014	12	0	1	0	1	4878.79	12	NC	1
330			min	-.004	1	-.549	1	0	1	0	1	126.288	1	NC	1
331		14	max	.002	3	-.015	12	0	1	0	1	4478.863	12	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
332			min	-.004	1	-.632	1	0	1	0	1	109.731	1	NC	1
333		15	max	.003	3	-.017	12	0	1	0	1	4139.21	12	NC	1
334			min	-.004	1	-.717	1	0	1	0	1	96.609	1	NC	1
335		16	max	.003	3	-.018	12	0	1	0	1	3847.218	12	NC	1
336			min	-.005	1	-.806	1	0	1	0	1	86.035	1	NC	1
337		17	max	.003	3	-.019	12	0	1	0	1	3593.562	12	NC	1
338			min	-.005	1	-.896	1	0	1	0	1	77.394	1	NC	1
339		18	max	.003	3	-.021	12	0	1	0	1	3371.199	12	NC	1
340			min	-.005	1	-.987	1	0	1	0	1	70.245	1	NC	1
341		19	max	.003	3	-.022	12	0	1	0	1	3174.714	12	NC	1
342			min	-.006	1	-1.078	1	0	1	0	1	64.27	1	NC	1
343	M8	1	max	0	1	0	1	0	1	0	1	NC	1	NC	1
344			min	0	1	0	1	0	1	0	1	NC	1	NC	1
345		2	max	0	3	0	15	0	1	5.676e-4	3	NC	1	NC	1
346			min	0	1	-.002	1	0	3	-1.737e-3	1	NC	1	NC	1
347		3	max	0	3	0	15	0	1	1.135e-3	3	NC	2	NC	1
348			min	0	1	-.009	1	0	3	-3.474e-3	1	7903.573	1	NC	1
349		4	max	0	3	0	15	.002	1	1.703e-3	3	NC	3	NC	1
350			min	0	1	-.02	1	0	3	-5.212e-3	1	3511.744	1	NC	1
351		5	max	0	3	-.001	15	.002	1	1.863e-3	3	NC	3	NC	1
352			min	0	1	-.035	1	-.001	3	-5.759e-3	1	1967.206	1	NC	1
353		6	max	0	3	-.002	15	.004	1	1.647e-3	3	NC	3	NC	1
354			min	0	1	-.055	1	-.002	3	-5.207e-3	1	1258.381	1	NC	1
355		7	max	0	3	-.003	15	.005	1	1.431e-3	3	NC	5	NC	1
356			min	0	1	-.079	1	-.003	3	-4.654e-3	1	878.976	1	NC	1
357		8	max	0	3	-.004	15	.006	1	1.215e-3	3	NC	5	NC	1
358			min	0	1	-.106	1	-.003	3	-4.102e-3	1	652.303	1	NC	1
359		9	max	0	3	-.005	15	.007	1	9.987e-4	3	NC	15	NC	1
360			min	0	1	-.137	1	-.003	3	-3.549e-3	1	505.979	1	NC	1
361		10	max	0	3	-.006	15	.008	1	7.825e-4	3	NC	15	NC	1
362			min	-.001	1	-.171	1	-.003	3	-2.997e-3	1	405.925	1	NC	1
363		11	max	0	3	-.008	15	.009	1	5.663e-4	3	9173.876	15	NC	1
364			min	-.001	1	-.207	1	-.003	3	-2.471e-3	2	334.461	1	NC	1
365		12	max	0	3	-.009	15	.01	1	3.502e-4	3	7730.448	15	NC	3
366			min	-.001	1	-.246	1	-.003	3	-1.985e-3	2	281.6	1	9435.152	1
367		13	max	0	3	-.01	15	.01	1	1.34e-4	3	6630.809	15	NC	3
368			min	-.001	1	-.287	1	-.002	3	-1.499e-3	2	241.376	1	9135.641	1
369		14	max	0	3	-.012	15	.01	1	-1.387e-5	15	5773.46	15	NC	3
370			min	-.002	1	-.33	1	0	3	-1.013e-3	2	210.045	1	9242.662	1
371		15	max	0	3	-.014	15	.01	1	2.579e-5	9	5091.898	15	NC	2
372			min	-.002	1	-.374	1	0	15	-5.266e-4	2	185.16	1	9873.454	1
373		16	max	0	3	-.015	15	.009	1	3.18e-4	1	4541.285	15	NC	1
374			min	-.002	1	-.42	1	0	15	-5.145e-4	3	165.07	1	NC	1
375		17	max	.001	3	-.017	15	.008	1	8.705e-4	1	4090.24	15	NC	1
376			min	-.002	1	-.466	1	0	15	-7.307e-4	3	148.624	1	NC	1
377		18	max	.001	3	-.019	15	.009	3	1.423e-3	1	3716.353	15	NC	1
378			min	-.002	1	-.513	1	0	10	-9.468e-4	3	134.998	1	7657.807	3
379		19	max	.001	3	-.02	15	.013	3	1.975e-3	1	3403.27	15	NC	1
380			min	-.002	1	-.561	1	-.002	10	-1.163e-3	3	123.595	1	5283.501	3
381	M3	1	max	.025	1	0	15	.001	3	1.45e-3	1	NC	1	NC	1
382			min	0	15	-.008	1	-.002	1	-4.22e-4	3	NC	1	NC	1
383		2	max	.025	1	-.002	15	.009	3	2.127e-3	1	NC	1	NC	4
384			min	0	15	-.052	1	-.027	1	-6.575e-4	3	NC	1	2910.235	1
385		3	max	.024	1	-.004	15	.017	3	2.804e-3	1	NC	1	NC	5
386			min	0	15	-.096	1	-.051	1	-8.93e-4	3	NC	1	1473.441	1
387		4	max	.023	1	-.006	15	.025	3	3.482e-3	1	NC	1	NC	5
388			min	0	15	-.139	1	-.075	1	-1.129e-3	3	NC	1	1000.772	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
389		5	max	.023	1	-.008	15	.032	3	4.159e-3	1	NC	1	NC	5
390			min	0	15	-.183	1	-.096	1	-1.364e-3	3	NC	1	769.661	1
391		6	max	.022	1	-.01	15	.039	3	4.836e-3	1	NC	1	NC	5
392			min	0	15	-.226	1	-.116	1	-1.6e-3	3	9670.313	4	635.793	1
393		7	max	.021	1	-.012	15	.045	3	5.514e-3	1	NC	1	NC	5
394			min	0	15	-.27	1	-.133	1	-1.835e-3	3	8575.823	4	551.283	1
395		8	max	.02	1	-.013	15	.049	3	6.191e-3	1	NC	1	NC	5
396			min	0	15	-.313	1	-.147	1	-2.071e-3	3	7918.965	4	495.877	1
397		9	max	.02	1	-.015	15	.053	3	6.868e-3	1	NC	3	NC	5
398			min	0	15	-.355	1	-.158	1	-2.306e-3	3	7565.404	4	459.792	1
399		10	max	.019	1	-.017	15	.055	3	7.546e-3	1	NC	3	NC	5
400			min	0	15	-.398	1	-.165	1	-2.542e-3	3	7453.555	4	438.063	1
401		11	max	.018	1	-.018	15	.057	3	8.223e-3	1	NC	3	NC	5
402			min	0	15	-.44	1	-.167	1	-2.777e-3	3	7565.404	4	428.396	1
403		12	max	.017	1	-.019	15	.056	3	8.9e-3	1	NC	1	NC	5
404			min	0	15	-.482	1	-.165	1	-3.013e-3	3	7918.965	4	430.392	1
405		13	max	.017	1	-.021	15	.054	3	9.578e-3	1	NC	1	NC	5
406			min	0	15	-.524	1	-.157	1	-3.248e-3	3	8575.823	4	445.57	1
407		14	max	.016	1	-.022	15	.05	3	1.025e-2	1	NC	1	NC	5
408			min	0	15	-.566	1	-.144	1	-3.484e-3	3	9670.313	4	478.269	1
409		15	max	.015	1	-.023	12	.044	3	1.093e-2	1	NC	1	NC	5
410			min	0	15	-.608	1	-.125	1	-3.719e-3	3	NC	1	538.457	1
411		16	max	.015	1	-.024	12	.036	3	1.161e-2	1	NC	1	NC	5
412			min	0	15	-.649	1	-.099	1	-3.955e-3	3	NC	1	650.538	1
413		17	max	.014	1	-.025	12	.026	3	1.229e-2	1	NC	1	NC	5
414			min	0	15	-.69	1	-.066	2	-4.19e-3	3	NC	1	888.896	1
415		18	max	.013	1	-.026	12	.014	3	1.296e-2	1	NC	1	NC	5
416			min	0	15	-.731	1	-.029	2	-4.426e-3	3	NC	1	1627.108	1
417		19	max	.012	1	-.027	12	.024	1	1.364e-2	1	NC	1	NC	1
418			min	0	15	-.772	1	-.001	3	-4.661e-3	3	NC	1	NC	1
419	M6	1	max	.046	1	0	15	0	1	0	1	NC	1	NC	1
420			min	.002	15	-.015	1	0	1	0	1	NC	1	NC	1
421		2	max	.044	1	-.002	12	0	1	0	1	NC	1	NC	1
422			min	.002	15	-.099	1	0	1	0	1	NC	1	NC	1
423		3	max	.042	1	-.003	12	0	1	0	1	NC	1	NC	1
424			min	.001	15	-.183	1	0	1	0	1	NC	1	NC	1
425		4	max	.04	1	-.004	12	0	1	0	1	NC	1	NC	1
426			min	.001	15	-.267	1	0	1	0	1	NC	1	NC	1
427		5	max	.038	1	-.005	12	0	1	0	1	NC	1	NC	1
428			min	.001	15	-.351	1	0	1	0	1	NC	1	NC	1
429		6	max	.036	1	-.006	12	0	1	0	1	NC	1	NC	1
430			min	.001	15	-.435	1	0	1	0	1	9670.313	4	NC	1
431		7	max	.035	1	-.007	12	0	1	0	1	NC	1	NC	1
432			min	.001	15	-.519	1	0	1	0	1	8575.823	4	NC	1
433		8	max	.033	1	-.008	12	0	1	0	1	NC	1	NC	1
434			min	.001	15	-.602	1	0	1	0	1	7918.965	4	NC	1
435		9	max	.031	1	-.008	12	0	1	0	1	NC	3	NC	1
436			min	.001	15	-.685	1	0	1	0	1	7565.404	4	NC	1
437		10	max	.029	1	-.009	12	0	1	0	1	NC	3	NC	1
438			min	.001	15	-.768	1	0	1	0	1	7453.555	4	NC	1
439		11	max	.027	1	-.009	12	0	1	0	1	NC	3	NC	1
440			min	.001	15	-.851	1	0	1	0	1	7565.404	4	NC	1
441		12	max	.025	1	-.01	12	0	1	0	1	NC	1	NC	1
442			min	0	15	-.933	1	0	1	0	1	7918.965	4	NC	1
443		13	max	.023	1	-.01	12	0	1	0	1	NC	1	NC	1
444			min	0	15	-1.015	1	0	1	0	1	8575.823	4	NC	1
445		14	max	.021	1	-.01	12	0	1	0	1	NC	1	NC	1

Envelope Member Section Deflections (Continued)

	Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y Ratio	LC	(n) L/z Ratio	LC
446			min	0	15	-1.098	1	0	1	0	1	9670.313	4	NC	1
447		15	max	.019	1	-.01	12	0	1	0	1	NC	1	NC	1
448			min	0	15	-1.179	1	0	1	0	1	NC	1	NC	1
449		16	max	.017	1	-.01	12	0	1	0	1	NC	1	NC	1
450			min	0	10	-1.261	1	0	1	0	1	NC	1	NC	1
451		17	max	.018	3	-.01	12	0	1	0	1	NC	1	NC	1
452			min	0	10	-1.343	1	0	1	0	1	NC	1	NC	1
453		18	max	.019	3	-.01	12	0	1	0	1	NC	1	NC	1
454			min	-.002	10	-1.424	1	0	1	0	1	NC	1	NC	1
455		19	max	.019	3	-.009	12	0	1	0	1	NC	1	NC	1
456			min	-.003	10	-1.505	1	0	1	0	1	NC	1	NC	1
457	M9	1	max	.025	1	0	15	.002	1	4.22e-4	3	NC	1	NC	1
458			min	0	15	-.008	1	-.001	3	-1.45e-3	1	NC	1	NC	1
459		2	max	.025	1	-.002	15	.027	1	6.575e-4	3	NC	1	NC	4
460			min	0	15	-.052	1	-.009	3	-2.127e-3	1	NC	1	2910.235	1
461		3	max	.024	1	-.004	15	.051	1	8.93e-4	3	NC	1	NC	5
462			min	0	15	-.096	1	-.017	3	-2.804e-3	1	NC	1	1473.441	1
463		4	max	.023	1	-.006	15	.075	1	1.129e-3	3	NC	1	NC	5
464			min	0	15	-.139	1	-.025	3	-3.482e-3	1	NC	1	1000.772	1
465		5	max	.023	1	-.008	15	.096	1	1.364e-3	3	NC	1	NC	5
466			min	0	15	-.183	1	-.032	3	-4.159e-3	1	NC	1	769.661	1
467		6	max	.022	1	-.01	15	.116	1	1.6e-3	3	NC	1	NC	5
468			min	0	15	-.226	1	-.039	3	-4.836e-3	1	9670.313	4	635.793	1
469		7	max	.021	1	-.012	15	.133	1	1.835e-3	3	NC	1	NC	5
470			min	0	15	-.27	1	-.045	3	-5.514e-3	1	8575.823	4	551.283	1
471		8	max	.02	1	-.013	15	.147	1	2.071e-3	3	NC	1	NC	5
472			min	0	15	-.313	1	-.049	3	-6.191e-3	1	7918.965	4	495.877	1
473		9	max	.02	1	-.015	15	.158	1	2.306e-3	3	NC	3	NC	5
474			min	0	15	-.355	1	-.053	3	-6.868e-3	1	7565.404	4	459.792	1
475		10	max	.019	1	-.017	15	.165	1	2.542e-3	3	NC	3	NC	5
476			min	0	15	-.398	1	-.055	3	-7.546e-3	1	7453.555	4	438.063	1
477		11	max	.018	1	-.018	15	.167	1	2.777e-3	3	NC	3	NC	5
478			min	0	15	-.44	1	-.057	3	-8.223e-3	1	7565.404	4	428.396	1
479		12	max	.017	1	-.019	15	.165	1	3.013e-3	3	NC	1	NC	5
480			min	0	15	-.482	1	-.056	3	-8.9e-3	1	7918.965	4	430.392	1
481		13	max	.017	1	-.021	15	.157	1	3.248e-3	3	NC	1	NC	5
482			min	0	15	-.524	1	-.054	3	-9.578e-3	1	8575.823	4	445.57	1
483		14	max	.016	1	-.022	15	.144	1	3.484e-3	3	NC	1	NC	5
484			min	0	15	-.566	1	-.05	3	-1.025e-2	1	9670.313	4	478.269	1
485		15	max	.015	1	-.023	12	.125	1	3.719e-3	3	NC	1	NC	5
486			min	0	15	-.608	1	-.044	3	-1.093e-2	1	NC	1	538.457	1
487		16	max	.015	1	-.024	12	.099	1	3.955e-3	3	NC	1	NC	5
488			min	0	15	-.649	1	-.036	3	-1.161e-2	1	NC	1	650.538	1
489		17	max	.014	1	-.025	12	.066	2	4.19e-3	3	NC	1	NC	5
490			min	0	15	-.69	1	-.026	3	-1.229e-2	1	NC	1	888.896	1
491		18	max	.013	1	-.026	12	.029	2	4.426e-3	3	NC	1	NC	5
492			min	0	15	-.731	1	-.014	3	-1.296e-2	1	NC	1	1627.108	1
493		19	max	.012	1	-.027	12	.001	3	4.661e-3	3	NC	1	NC	1
494			min	0	15	-.772	1	-.024	1	-1.364e-2	1	NC	1	NC	1