

# Aim Is All You Need

*A Speculative White Paper On PuffSat Pulsed Propulsion*

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## ABSTRACT

In 2017, Google Research published *Attention Is All You Need* [59]. Their paper introduced the Transformer, which revolutionized how neural networks capture long range dependencies. Just a few years later, OpenAI developed tools like ChatGPT [43] that catapulted AI into mainstream adoption.

But here's the bittersweet truth: While our screens flicker with progress, breakthroughs in space travel and clean energy advance at a slower pace.

### Dude, Where's My Spaceship?

This paper's goal is to enable our progress in physical realms to catch up with our progress online. Our journey requires applying a single unifying idea that is much simpler than attention – *aim*.

Consider a "PuffSat," a single use device that, when triggered, rapidly converts nearly all its mass into a low density gas. The PuffSat can generate gas explosively or by atomizing cold solids or liquids (see Section 2.2). The PuffSat can perform small navigation adjustments using ultra lightweight microthrusters and electronics.

Now, envision a scenario with two rockets. The first rocket deploys a series of these fast moving PuffSats. As shown in Figure 1, the deployed PuffSats precisely follow a path to sequentially gasify and impact a shock absorbing momentum pusher plate on a separate target rocket. These collisions deliver high density jolts of pulsed energy and momentum to the target vehicle, enabling a surprisingly broad range of groundbreaking applications (See Table 1).

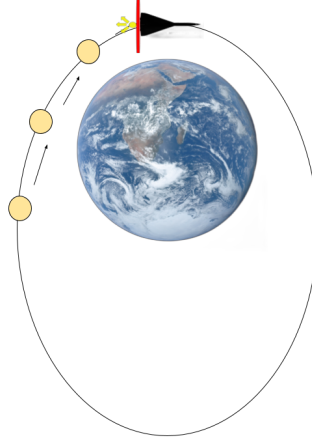


Figure 1: PuffSats from a first rocket (not shown) crash their gas puffs into a second target rocket, transferring momentum for propulsion. [63]

Recent missions such as Proba-3 [14] demonstrate that millimeter-scale formation flying works—at least in high-altitude orbits. Therefore, most PuffSat navigation and control tasks can be handled with robust model predictive control (MPC) [60] and Kalman filtering (see Section 2.1). These classical techniques are data-efficient, easy to interpret, enable clear reasoning about system behavior, and offer formal performance and safety guarantees. For the more demanding conditions near low periapsis, classical control methods can be augmented with neural networks that warm-start control algorithms and learn from residual errors (see Section 2.1).

This speculative white paper is a brainstorming exploration that could be followed by more rigorous analysis. If the ideas prove too advanced for near term implementation, they can instead serve as fodder for hard science fiction. The paper summarizes and updates some of the writings from the author's own blog, "Aim Is All You Need." [50]

## 1 Introduction

Conceived in the 1950s and later popularized by *The Three-Body Problem* [31], Project Orion remains one of the most compelling rockets ever proposed. It uniquely offers specific impulses surpassing those of electric propulsion while

Table 1: A checklist of grand challenges PuffSat pulsed propulsion can solve

<b>Safer Satellite Launch</b>	We'll launch expensive satellites and astronauts without strapping them to fragile extremely high propellant mass fraction rockets. See Section 3.1.
<b>Suborbital Transit</b>	We'll create a viable suborbital travel vehicle allowing passengers to take off from normal airport runways and reach anywhere in the world in less than 2 hours. Noise pollution near population centers will be no worse than it is with conventional aircraft. See Section 3.2.
<b>Rocket Revolution</b>	We'll end the tyranny of the rocket equation. We'll still use small rockets, but giant rockets with high propellant mass fraction will no longer be needed to reach orbit. See Section 5.1
<b>Lunar Lift-off</b>	Launching from the moon may still require volatiles, but not the more difficult task of making and storing high performance rocket fuel. See Section 4.2
<b>Jurassic Dark</b>	As a side effect of our advances, we'll create the field of lunar cold trap paleontology and discover concrete evidence for how life originated on Earth. We'll build a genetic record of extinct species from ancient geological periods, like the dinosaurs. See Section 4.4
<b>Straw Ways To Heaven</b>	We can construct terrestrial megastructures, extending from the ground to the edge of space, without relying on advanced magnetic technologies such as Lofstrom Launch Loops [25]. A particularly ambitious yet beneficial example might be a vacuum tube connecting Earth and space, a "Straw Way To Heaven." See Section 6.1.
<b>Carbon Cancelled</b>	We will solve our energy problems with carbon negative fuel that absorbs the carbon dioxide produced by industry, all while using minimal land and resources. See Section 6.6.
<b>Moon Mining</b>	We'll develop in-situ resource utilization (ISRU) technology, first on our moon (See Section 4.3) and then on icy moons like Saturn's moon Phoebe (See Section 7)
<b>Cosmic Commutes</b>	We'll build fusion powered spaceships with Earth-like artificial gravity that travel on brachistochrone trajectories with constant acceleration and deceleration between destinations. Section 6.7

delivering thrust levels on par with chemical rockets [68]. Orion would propel a spacecraft by directing hypervelocity plasma from nuclear explosions onto a pusher plate. Despite its theoretical promise, Orion faced insurmountable challenges related to political feasibility, radioactive fallout, and the impractical mass requirements stemming from the high minimum yield of nuclear explosions. Nevertheless, Orion conceptually validated the physics of hypervelocity pulsed propulsion.

Our approach replaces nuclear bombs with precisely aimed, hypervelocity gas puffs from specialized "PuffSat" CubeSats (see Section 2.2) sequentially impacting a rocket's pusher plate. These gas puffs can be downscaled to practical sizes. Unlike nuclear explosions, small hypervelocity gas impacts could be efficiently contained within a pulsed propulsion chamber.

Leveraging gravity assists and the Oberth effect [67], hypervelocity PuffSat impacts could achieve high energy densities and specific impulses. Conventional control and estimation methods, which offer dependable results, can form the backbone of PuffSat guidance algorithms. Neural networks optionally augment these systems by adjusting for unmodeled dynamics in complex orbital regimes and by reducing computational latency (see Section 2.1).

This speculative white paper presents a preliminary back of the envelope analysis of what are clearly very ambitious ideas. While rigorous, high fidelity modeling is left for future work, our aim is to stimulate fresh thinking and new research directions. Whether this concept remains a provocative thought experiment, inspires science fiction, or evolves into a transformative 21st-century technology, it underscores bold and novel applications of emerging formation flying capabilities.

## 2 Groundwork And Prior Work For PuffSat Pulsed Propulsion

### 2.1 Navigation For PuffSat Pulsed Propulsion

Millimeter-accuracy CubeSat formation flying is rapidly advancing. The European Space Agency's (ESA) Proba-3 mission recently demonstrated this capability by creating artificial solar eclipses with a precise two satellite formation [14]. The Stanford Space Rendezvous Laboratory's VISORS mission [17], nearing flight readiness (as of August 2025), will showcase millimeter-precision formation flying with 6U CubeSats for 10-second durations at a 600 km altitude [29].

Our hypervelocity PuffSats also employ formation flying algorithms for precise positioning. Both VISORS and Proba-3 require sub-arcsecond pointing alignment for science imaging. PuffSats can tolerate wider rotational misalignment, which relaxes the control problem. Unlike Proba-3 and VISORS, the PuffSat formation is limited to a single orbit. This short duration profile allows us to budget more micro-thruster fuel specifically for correcting stronger perturbations near the PuffSats' lower (200 km) interception altitude. VISORS relies exclusively on cold gas thrusters, but the PuffSats' more dynamic orbital regime may require a hybrid propulsion system—combining more powerful chemical micro-thrusters for primary maneuvers with more responsive cold gas actuators for fine-tuned adjustments. The probability distributions for low-altitude orbital disturbances are similar over minutes-long time frames. This means real-time observations of each PuffSat's perturbed path can refine the initial trajectory guesses used to control later PuffSats. If control remains impractical, we can simplify by increasing the PuffSat interception altitude. If we raise interception to 300 km, a reusable suborbital target rocket (see Section 3.2) would require somewhat higher propellant mass fractions, suffers marginally greater re-entry heating, and benefits slightly less from PuffSat velocity. However, raising interception height may be an acceptable compromise if lower altitudes near 200 km simply prove unmanageable.

To maximize gas mass while minimizing the non-volatile solid mass of the mini-thrusters and electronics, a small number of coordinator satellites with enhanced computing power will track the PuffSats' positions and relay adjustment commands. The coordinator nodes will account for communications and PuffSat actuator latencies when determining PuffSat control trajectories. As shown in Figure 2, these heavier coordinator nodes fly alongside the PuffSats but do not impact the target rocket. The PuffSats themselves carry only simple, low-mass electronics. Because hundreds of PuffSats are required per mission, mass production will help reduce overall costs.

Each PuffSat carries perhaps 100 grams of non-volatile solid mass, including sensors, power systems, microthrusters, and low bandwidth communication links to the coordinator nodes. To prevent this mass from impacting the rocket, we propose several disposal strategies:

- **Discard Before Impact:** The non-volatile solid components could launch slightly away from the rocket just before impact. If explosives are used to gasify the PuffSat (see Section 2.2.1), shaped explosive sections can direct and accelerate the non-volatile solids radially outward at high speed. The shaped explosives ensure the non-volatile solids outrun the expanding gas envelope and clear the target radius prior to impact.
- **Active Elimination:** Equipment on the target rocket could obliterate the non-volatile solids via electric discharges, directed energy beams, or sprays of material that hit the incoming PuffSat solids before pusher plate impact.
- **Passive Routing:** The non-volatile solid components could pass harmlessly through a small aperture in the pusher plate.

All of these impact mitigation techniques would occasionally fail. In this case, the pusher plate itself serves as a last line of defense. A strong, heat tolerant, Kevlar backed pusher plate structurally resembles Whipple shielding [7]. The pusher plate would pulverize the non-volatile solids and prevent catastrophic damage to crewed compartments or high value satellites. The target rocket would then ideally steer out of the PuffSat stream and abort. If carrying people, the target rocket survives reentry with single use but reliable ablative heat shields. The target rocket might carry swappable, redundant pusher plates to allow for mission continuation following a single component failure. Even with redundancy, we retain the capability for reentry in a worst-case multiple-failure scenario.

To ensure a precise interception of the next PuffSat, the target spacecraft's rocket based reaction control system must rapidly adjust its trajectory. It must do this within fractions of a second after each impact, correcting for the difference between the expected and actual momentum transfer from the previous PuffSat. A prerequisite for these hypervelocity PuffSat rendezvous is accurately capturing the position and velocity of the PuffSats. For this, a standard Unscented Kalman Filter (UKF) [61] offers robust state estimation when dynamics are well-modeled and noise is Gaussian. The large formation of PuffSats provides a dense measurement stream, further improving filter performance.

PuffSat interceptions, however, may occur near low periapsis in denser atmospheric layers where drag, gravitational anomalies, sensor dropouts, and outliers challenge UKF's assumptions and accuracy. When such effects become significant, state estimation should be improved with hybrid approaches that augment the UKF with neural networks that learn residuals on real and simulated orbital data [56]. For example, methods like KalmanNet [47] [48] have shown robustness to unmodeled disturbances in simulations. Neural inference scales favorably compared to Kalman filtering, especially as the number of states estimated grows. As a result, neural estimators may support more frequent updates in a large PuffSat formation.

Verifiable, data-efficient, interpretable techniques like model predictive control (MPC) can replan trajectories to correct for momentum prediction errors after PuffSat impacts. Neural networks can warm start conventional tools with good initial guesses to reduce solve times, [18] especially when there are many real-time constraints [3]. However, the control

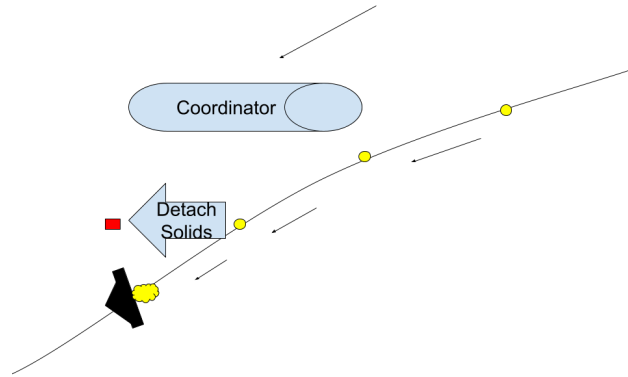


Figure 2: Coordinator nodes (non-impacting) handle measurement and computation; PuffSat solids detach or pass through the pusher plate’s aperture before impact.

law itself could remain grounded in well-understood optimization and stability guarantees. Additionally, reinforcement learning shows promise for developing fast space trajectory recovery algorithms for anomalies like lost PuffSats [76].

While PuffSat navigation enables millimeter-scale centering in front of the pusher plate prior to detonation, gas generation unfolds over a finite duration and lacks comparable precision along the thrust axis. Nevertheless, sub-centimeter lateral positioning ensures that the plume impinges symmetrically—preserving the target vehicle’s inertial stability. The target rocket’s reaction control system would still need high performance to cancel undesirable torques from the occasional PuffSat that hits the pusher plate significantly off-center.

### 2.1.1 Steering PuffSats With High Powered Lasers

Instead of relying on non-volatile solid components, radiation pressure could directly manipulate PuffSats. Coordinator nodes might employ kilowatt-class lasers to adjust PuffSat trajectories. The intense laser light could also induce temporary thermal or photochromic changes in the PuffSat’s skin, altering its shape or color. If these changes briefly persist, the altered solar radiation pressure would magnify PuffSat trajectory changes compared to the laser’s radiation pressure alone. Eliminating non-volatile solid components on PuffSats reduces the risk of pusher plate damage in an accident. The PuffSats cost less without microthrusters and electronics. However, space lasers present several drawbacks compared to microthrusters. They exert weak forces on the PuffSats, demand substantial power sources for coordinator nodes, and are not yet a fully mature technology.

## 2.2 PuffSat Design And Gas Generation Details

The optimal PuffSat design depends on the launch scenario and mission requirements.

### 2.2.1 Explosive PuffSats

Explosive PuffSats are timed to detonate at a precise standoff distance from the pusher plate, rapidly converting their mass into a high-velocity gas disk for maximum momentum transfer. A small shaped section of the PuffSat’s explosive charge can also eject non-volatile solid components away from the rocket before impact, as described in Section 2.1. A failure to detonate at the intended moment could damage the pusher plate or the rocket, so redundant initiation systems are essential.

As shown in Figure 3, each PuffSat carries an onboard detonation mechanism. To ensure reliable detonation, the rocket also releases a microns-thick layer of volatile material, such as water ice, a few meters in front of the pusher plate just before each PuffSat’s arrival. The resulting impact shock ensures the PuffSat’s explosive charge detonates. The ice sheet’s geometry guarantees that a PuffSat cannot hit the rocket without first passing through it. The ice sheet can be a mostly empty grid or lattice, reducing areal density significantly.

If frozen materials prove impractical, the grid could instead be constructed from low-mass plastic explosives, designed to detonate on PuffSat impact. If the rocket misses a PuffSat interception after reaching minimum orbital speed, the explosive grid would unfortunately become space debris. This debris could persist for hours or days until eroded by atomic oxygen or slowed enough by atmospheric drag to re-enter. Another alternative is to replace ice lattices with liquid sprays that induce a shock detonation of the PuffSat’s explosives upon impact.

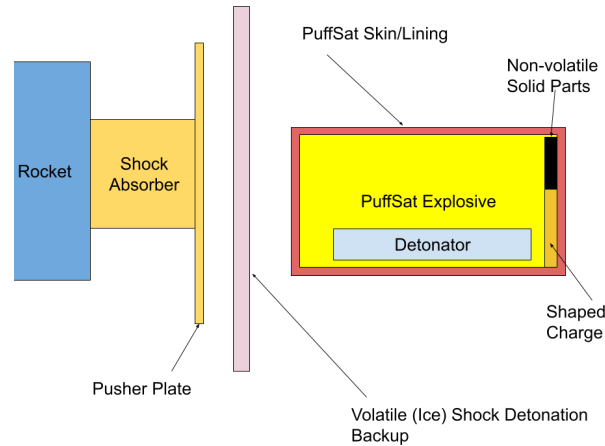


Figure 3: Cross sectional diagram of the key parts of an explosive PuffSat

To prevent outgassing, the explosive materials are encased in very thin layers of high performance polymers or metals. These liners can also reflect sunlight, further reducing temperatures to minimize the escape of volatile materials. Explosive PuffSats are ideal for terrestrial launches, where the necessary chemicals are relatively easy to manufacture.

### 2.2.2 Solid Ice Based PuffSats

PuffSats filled with lunar ice (see Section 4.2) do not primarily rely on chemical reactions to produce gas. Their high tensile skins absorb sunlight, melting the ice to water under mild pressure. Small explosives or an ice grid impactor (see Section 2.2.1) rupture the skin to release the water. However, this release is too slow for complete vaporization before impact, and full vaporization would cool the steam so rapidly that ice crystals would form.

Instead, the water is atomized into fine droplets, a process requiring much less energy than vaporization. To drive atomization, microscopic explosive particles are suspended in the water, either as a colloidal slurry or encapsulated in microbubbles. In microgravity, thermal agitation induces Brownian motion, naturally yielding a stochastically mixed, quasi-uniform explosive particle distribution. These micro explosives are chosen for precise shock sensitivity, ensuring they detonate upon high velocity impact with the incoming ice grid or in response to the main rupture charges. While likely imported from Earth due to manufacturing complexity, the micro explosives' total mass is small compared to the bulk water payload.

Additional ice particles injected by the rocket ahead of the plume induce energetic turbulent mixing. The resulting aerodynamic shear, combined with micro explosive detonations, fully atomizes the water into fine droplets before it reaches the rocket's pusher plate.

### 2.2.3 Liquid Oxygen PuffSats

PuffSats filled with lunar oxygen (see Section 4.3) must also atomize before reaching the pusher plate. To retain liquid oxygen during orbital transit, these PuffSats require thicker skins engineered for elevated internal pressures, cryogenic temperature tolerance, and thermal insulation. To minimize boiling of the highly pressurized LOX (liquid oxygen), PuffSats use high-reflectivity coatings such as emerging "solar white" yttrium oxide composites (see Section 6.7). These coatings are backed by emissive layers that radiate residual heat into space, maintaining cryogenic temperatures without active cooling.

Upon rupture, the thicker balloon skin risks becoming hazardous shrapnel. While PuffSat skins are engineered to retain cryogenic LOX under elevated internal pressure, they need not be shock-resistant. In fact, selecting materials prone to brittle fracture at low temperatures may enhance debris mitigation by ensuring the skin fragments on impact. The rocket releases a denser intercepting ice sheet that shatters the brittle skin in a process analogous to how Whipple shielding breaks up space debris into less threatening dust [7].

As with the icy PuffSats discussed in Section 2.2.2, the liquid oxygen is atomized through a combination of micro explosive detonation, aerodynamic shear, and shock interaction with the ice sheet.



### 2.2.4 Balloons PuffSats

Inflated balloon PuffSats avoid the catastrophic risk of failed detonations. When filled with gaseous water vapor or oxygen, balloon PuffSats can operate without advanced reflective cooling. Project Echo [20] demonstrated that large orbital balloons can be built from low cost materials such as metallized mylar.

At low periapsis, maintaining balloon navigation control and structural integrity is difficult because of atmospheric drag, debris impacts, and radiation pressure. Large balloon surface area also demands more polymer, increasing costs significantly. If high performance polymer costs drop substantially, balloon PuffSats could become a favorable option.

### 2.3 Comparison To Pellet Beam Propulsion Prior Art

In 2001, Gerald Nordley proposed an externally pulsed propulsion system in which hypervelocity pellets, capable of self steering, transfer momentum to a spacecraft via impact with a pusher plate [42]. This concept built upon earlier work by Clifford Singer [52], who envisioned unguided macroscopic projectiles launched at extreme velocities.

Both Singer's and Nordley's designs relied on mass drivers. These devices would need to accelerate sizable objects to very high speeds, posing formidable engineering challenges. To address this, Jordan Kare introduced the SailBeam concept [22], which replaced the mass driver with solar or laser driven miniature sails. Kare further proposed vaporizing the sails upon impact and using a magnetic pusher plate to convert the resulting plasma into thrust.

These pellet stream propulsion ideas often prioritized interstellar speeds over economic feasibility. Instead of using expensive mass drivers or light sails, our PuffSat pulse propulsion system focuses on achieving high speeds primarily through low cost orbital maneuvers. Our PuffSats can weigh kilograms, and are mostly comprised of materials that gasify to biologically compatible chemicals like water vapor, nitrogen, oxygen, and carbon dioxide. This means they generate substantially less pollution for a given  $\Delta V$  (delta-v), which makes them practical for very large scale near-Earth applications.

Although our PuffSats contain electronics, the majority of their mass consists of inexpensive explosives or ices. This composition enables comparable propulsion at significantly lower cost than systems dominated by electronics or solar sail material. Water ice, in particular, is abundant and mineable throughout the solar system. Larger PuffSats can afford heavier electronics than Nordley's snowflake sized guided pellets. While PuffSats could, in principle, interact with magnetic pusher plates, their largely gaseous composition (after gas generation) may make direct kinetic collision a simpler and more robust mechanism for momentum transfer.

### 2.4 Mass Fraction Of Rocket To PuffSat Mass

For PuffSat pulsed propulsion to be a viable option, the ratio of PuffSat gas mass to target rocket mass must be low for relevant rocket velocity changes. We develop a closed form approximation for this ratio (Equation 7 in Appendix A). Since real collisions are not perfectly elastic, our approximation includes an energy loss "fudge factor,"  $f$ . Justification for a high  $f$  comes from Project Orion's findings [19]. The Orion team found that pusher plate collisions could be opaque. This opacity implied minimal kinetic energy loss to pusher plate heating, resulting in a more elastic impact. Pusher plate durability and opacity could be further enhanced by spraying a thin layer of oil on the plate between impacts. Additionally, a curved, roughly parabolic pusher plate would produce a highly collimated gas reflection. Therefore, we select a high  $f = 0.8$ .

Relevant mass ratios and mission scenarios are summarized in Table 2. This table clearly shows that PuffSat pulsed propulsion can lift significant mass into orbit. For instance, if a reusable rocket like SpaceX Starship [53] lifts 25 t of PuffSats into a trans-lunar orbit, they can propel a 32 t target craft into low Earth orbit. This exceeds the Space Shuttle's maximum capacity [69] or the zero fuel mass of smaller regional jets like the Embraer E170 [65].

### 2.5 Handling Space Debris

The non-volatile solid components of each PuffSat risk becoming space debris. To avoid this, we can intercept the PuffSats prior to their orbital periapsis. For example, a PuffSat interception at a 200 km altitude likely follows a predictable trajectory with negligible atmospheric drag. If the PuffSat periapsis is near 50 km, this likely deorbits any non-volatile solid components. They ideally then burn up or fall over remote oceans. PuffSats that miss their target rockets either boil or explode from reentry heating, eliminating the risk of heavy debris reaching the ground. Two other techniques prevent long lasting space debris:

- The J2 perturbation induces a changing argument of periapsis. Any PuffSat orbit designed to avoid specific critical angles will eventually have a periapsis over the equator. Since the Earth is wider at the equator, periapsis will be at a lower atmospheric altitude with much more drag.
- If our PuffSat interceptions occur at night, subsequent daytime periapsis will be over a warmer atmosphere with higher drag at the same altitude.

Table 2: Mass ratio of rocket to PuffSat with fudge factor  $f = 0.8$  [23]

Rocket Final Velocity (km/s)	PuffSat Velocity (km/s)	Rocket Initial Velocity (km/s)	Rocket/PuffSat Mass Ratio	Scenario
7.784	10.916	0	1.28	Eccentric PuffSats with apogee at lunar distance pushes rocket to minimal low Earth orbit. See Section 3.1
0	-7.784	7.784	2.308	Decelerate intercity rocket for powered reentry with retrograde PuffSats in low orbit. See Section 3.2
0	-10.916	7.784	2.97	Decelerate intercity rocket for powered reentry with retrograde PuffSats from lunar orbit. See Section 3.2
23.66	69.272	0	3.83	PuffSats approach Earth from Jupiter retrograde Hohmann trajectory and push the object to escape velocity and then to a periapsis near Parker Space probe. See Section 5.5
40.17	69.272	0	1.85	PuffSats approach Earth from Jupiter retrograde Hohmann trajectory and push the object to escape velocity and then to a periapsis near Parker Space probe but in a retrograde orbit around the Sun. See Section 5.5
10.916	69.272	0	9.331	PuffSats approach Earth from Jupiter and push a rocket into an elliptical orbit. See Section 5.6
3 and 3.7	7.20	0	1.455	Launch PuffSats from the moon to trans-lunar injection orbit with low periapsis on Earth. See Section 4.2
0	-2.38	2.38	2.30	Decelerate trans-lunar payloads to land on the moon, ignoring the moon's speed around Earth. See Section 5.1
24.98	35.25	0	1.29	PuffSats approach Saturn from Phoebe and push a Helium-3 payload into a temporary very low orbit around Saturn. See Section 7.1

Since PuffSats form large formations, care must also be taken to avoid existing satellites. Short seconds-long gaps in the formation could be intentionally introduced to avoid collisions.

## 2.6 PuffSat Deployment Details For Low Earth Orbit Scenario

Let's consider the complexities of launching target rockets into Low Earth Orbit (LEO) with propulsion from PuffSats deployed in highly eccentric Earth orbits.

It's crucial to acknowledge that these PuffSats will not follow strictly identical Keplerian orbits. As the target rocket accelerates, the optimal PuffSat interception point moves along with it, so that successive PuffSats have slightly different orbital elements. For low mass PuffSats, solar radiation pressure will significantly distort their orbits. To simplify orbit planning and maintain consistent effects across the fleet, it's ideal for each PuffSat to remain outside the shadow of the others. This may necessitate slight variations in orbital parameters, such as inclination, for nearby PuffSats. The micro thrusters on each PuffSat make corrections for unmodeled perturbations. We still ensure each PuffSat achieves the correct interception position with the target rocket.

Fortunately, strategically deploying our PuffSats near apoapsis can minimize the  $\Delta V$  required for these inclination changes. Apoapsis PuffSat deployment also minimizes the  $\Delta V$  for appropriate PuffSat spacing. The small  $\Delta V$  changes required at apoapsis should enable practical designs for a very precise mechanical PuffSat launcher onboard our PuffSat deployment rocket.

## 3 To The Moon by Smart Gas Balloon: The Business Case For PuffSat Pulsed Propulsion

### 3.1 Making Starship's Excess Capacity Useful To Satellite Customers

SpaceX's Starship may be the first fully reusable rocket. At scale, this could dramatically reduce space flight costs. However, the rocket's large payload size is probably too big for today's space industry needs. For example, in *The New York Times*

Carissa Christensen, the chief executive of Bryce Tech, an analytics firm that tracks the launch market, says launching Starship frequently will be key to closing SpaceX's business case, but finding

customers to fill the rocket's giant payload capacity will be challenging. "Starship's payload capacity is huge; it's very, very big, and there aren't that many commercial uses today for a rocket that big," she said. "Maybe it'll be so cheap that it makes sense to launch satellites on it if it's not full or near full." [21]

Although many satellites might be too small to fill up Starship, they can still be very expensive to build and test. For an extreme example, the James Webb Telescope [41] cost \$9.7 billion dollars [5] to build. *McKinsey Consulting* argues

Safety and reliability will continue to be overarching concerns, suggesting excellent execution will be table stakes for a competitive launch company. [10]

Once rockets start ferrying astronauts, reliability becomes even more emphatically non-negotiable. Fully stacked, Starship weighs 5 kt at launch [53], yet its empty mass is only 300 t. That's an awfully thin soda can strapped to a 5 kt bomb that we're entrusting with billion dollar satellites or human passengers.

By contrast, a suborbital rocket that merely reaches 200 km in altitude might have a propellant mass fraction under 50 percent. This greater structural margin allows for more robust, reliable engines and extensive payload protection systems. Of course, such a suborbital rocket cannot reach orbit on its own. It needs Starship to "push" it with PuffSat pulsed propulsion.



Figure 4: A fun and of course very technically accurate cartoon about a suborbital rocket's  $\Delta V$  limitations

Starship launches PuffSats for pulsed propulsion into a highly eccentric orbit around Earth, with a low 50 km perigee and a high apogee (See Section 2.5). These PuffSats move near Earth's escape velocity at perigee. The suborbital rocket intercepts the PuffSats with its pusher plate and rides their gas momentum pulses to low Earth orbit. While this approach reduces payload capacity compared to a single rocket system, most satellites are unable to take advantage of Starship's enormous payload volume anyway.

### 3.2 The 200 Mile High Club

SpaceX proposes direct Earth-to-Earth travel [27], ballistically launching passengers directly between cities with Starship from offshore platforms. This idea faces significant challenges:

- **Marine Environmental Impact:** Noise pollution from sea launches could severely harm marine ecosystems, including dolphins and whales.
- **Noise Over Populated Areas:** Starship's descent would generate loud sonic booms over cities.
- **Logistical Inefficiency:** Offshore launch platforms, by necessity located far from land, would add hours to the journey for boarding and departure, undermining the benefit of rapid travel.

A suborbital rocket plane offers a more practical alternative. To reach orbit, the suborbital rocket requires propulsion PuffSats launched by the Starship. Starship can be launched from remote locations where noise pollution is acceptable. Our suborbital rocket plane could take off from conventional urban airports using standard aircraft engines, then switch to rocket propulsion at high altitudes over remote areas to "skip" above the atmosphere and intercept Starship's propulsion PuffSats. While normal airports can handle kerosene or methane fuel, most lack the infrastructure for cryogenic liquid oxygen.

However, two solutions address the liquid oxygen challenge:

- **Air-breathing Scramjets (Optimistic Scenario):** If economical passenger scramjets become feasible, rockets could accelerate to around Mach 7 before a steep climb, eliminating the need for liquid oxygen. This would also reduce propellant mass. Unfortunately, the extreme stress on the airframe makes suborbital rockets more economically viable for the foreseeable future.
- **Mid-air Oxygen Refueling:** Suborbital rocket planes could receive liquid oxygen from specialized aircraft launched from airports equipped with liquid oxygen storage. This avoids retrofitting every urban airport, requiring only a single, strategically located airport near major destinations. Mid-air refueling also reduces our rocket plane's takeoff weight.

A formation of propulsion PuffSats launched in an eccentric Keplerian orbit could only propel the rocket plane on trajectories that bisect the Earth. Since most urban destinations would not align with such trajectories, the rocket plane needs to fire an adjustment burn at least once to reach the destination. Alternatively, a second set of propulsion PuffSats could intercept the rocket plane mid-flight and adjust its trajectory. Furthermore, to avoid a sonic boom upon descent, the plane must decelerate before atmospheric reentry. This deceleration could be provided by yet another set of propulsion PuffSats that were traveling in a retrograde orbit relative to the plane. These reentry PuffSats could be in a circular low Earth orbit rather than a high eccentricity orbit, significantly reducing the mass required.

## 4 I Love ISRU. Cheaper PuffSat Pulsed Propulsion *Without* Giant Reusable Rockets

For PuffSat pulsed propulsion of intercity passengers to achieve genuine economic competitiveness, the cost of launching propulsion PuffSats must be exceptionally low. The rocket plane must be robust enough to guarantee on-time takeoffs and avoid missing its initial PuffSat rendezvous. Rocket acceleration and passenger cabin vibrations must be limited for infants and other susceptible passengers, further increasing costs and  $\Delta V$ . Even highly reusable rockets may prove too expensive, limiting this technology primarily to the very high-end private luxury aviation market. While luxury aviation customers typically prioritize flexibility, PuffSat propelled flights necessitate advance scheduling. Despite these limitations, the potential market for affluent travel between cities like Dubai and Dallas is likely at least an order of magnitude larger than the satellite market.

Still, it would be disappointing if we can't make suborbital travel mainstream. If we can launch our PuffSats without giant rockets, we can reduce cost. After all, "the best part is no part," [54] and a reusable rocket is one heck of a part.

### 4.1 Lunar Volatiles For PuffSat Pulsed Propulsion

Instead of using Starship, lunar volatiles extracted from the moon's permanently shadowed regions could fill our propulsive PuffSats. As shown in Figure 5, these PuffSats could be sent into a trans-lunar injection orbit that intersects our terrestrial suborbital rocket plane. Although PuffSat skins and electronics would likely still be sourced from Earth, volatiles constitute the majority of the PuffSats' mass. One approach to launching these PuffSats into orbit involves using rockets powered by lunar-derived propellants. The space community is enthusiastic about water electrolysis to produce and store cryogenic fuel for lunar rockets [1]. However, this process is energy-intensive and requires complex cryogenic infrastructure, particularly for hydrogen fuel. Moreover, a reusable lunar rocket designed for repeated landings would require approximately 6 km/s of  $\Delta V$ , necessitating propellant mass fractions of about 75% for hydrogen or 81% for methane. While these figures are an improvement over Earth-launched rockets, the high propellant mass fractions remain a significant challenge.

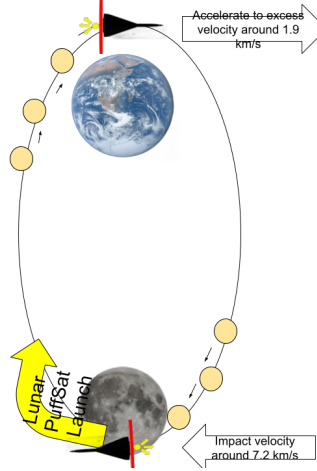


Figure 5: Lunar launched PuffSats replace Starship launched PuffSats [63] [28]

#### 4.2 Lunar Rockets Without Lunar Rocket Fuel

Instead of launching our lunar volatiles towards Earth with conventional rocket fuel, we launch off the moon using the same PuffSat pulsed propulsion we’ve been discussing for terrestrial launches. A rocket launched with PuffSat pulsed propulsion from the lunar surface into a trans lunar injection orbit can burn its engines at periapsis around Earth. Due to the Oberth effect, a small burn near Earth returns the rocket to the moon with a large velocity change. As the rocket approaches the moon, it deploys its payload of PuffSats previously filled with lunar volatiles. These returning PuffSats can push a new, more massive rocket filled with fresh volatiles off the moon. We can then repeat this cycle for exponential growth in lunar PuffSat launch mass capacity. We’ve reduced combustible fuel requirements by burning our rockets near Earth.

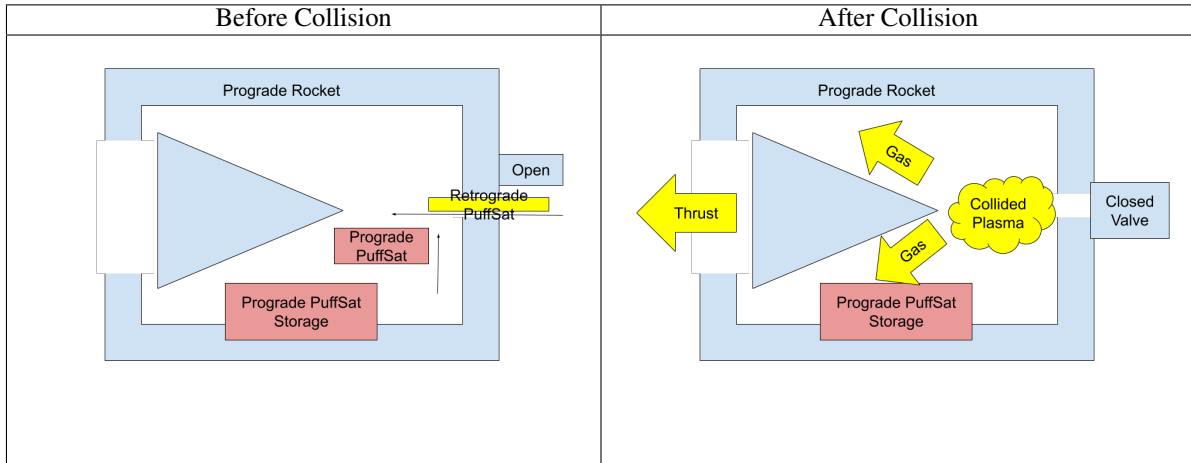


Table 3: A pulsed propulsion chamber. PuffSats enter, collide and produce thrust. The valve, likely a fast rotating door synchronized with PuffSat arrivals, is optional because a small front opening will produce less thrust than a large rear opening. If the explosion turns the gas into plasma, the valve could be magnetic rather than solid state.

However, we ideally don’t want to make any chemical rocket fuel at all. Let’s again use PuffSat propulsion to launch our PuffSat deployment rocket from the lunar surface into a trans-lunar orbit. We also launch a second set of PuffSats from the lunar surface into a retrograde trans-lunar orbit. Using the millimeter precision navigation techniques we’ve discussed, we sequentially collide these retrograde PuffSats with more massive prograde PuffSats the main rocket is carrying. As depicted in Table 3, we trap the exploding gas from these collisions in a pulsed propulsion chamber and redirect this gas for thrust. To leverage the Oberth effect and maximize gas collision velocity, we collide our PuffSats close to periapsis near Earth.

If our colliding PuffSats each travel at  $v_p = 11 \text{ km/s}$ , then from Equation 12 derived in Appendix B, the maximum theoretical combined effective exhaust velocity is  $v_e = \frac{1}{2}v_p = 5.5 \text{ km/s}$ . Suppose this pulsed explosion has significant real world losses for an effective exhaust of  $v_e = 3 \text{ km/s}$ . If the main rocket accelerates at its Earth periapsis with a burn of  $1.9 \text{ km/s}$  it will reach the moon at  $7.2 \text{ km/s}$  [23]. If the rocket deploys propulsion PuffSats on lunar approach, they can push another rocket off the moon with a mass greater than the incoming PuffSats. Specifically, the incoming propulsion PuffSats have enough momentum to start an exponential growth cycle where each loop around the moon launches about 1.455 times the starting mass. If we do this once per lunar month, we have increased our initial launch mass capacity by a factor of 1 million in about 2.8 years [23].

### 4.3 Lunar Oxygen Has Mass And That Is All It Needs

Lunar volatiles like water ice are ideal for filling PuffSats, but they are scarce. However, oxygen is very common in lunar surface minerals. Using solar energy and mining rovers derived from platforms like the IPex Pilot Excavator [35], we can produce oxygen. On the volatile-depleted sunlit lunar surface, finding something to burn oxygen with for rocket propulsion is hard. However, PuffSat pulsed propulsion does not require oxygen combustion, just gas momentum. In shadowed craters or artificial shade, lunar derived oxygen will liquify and perhaps even solidify for storage.

We use some of our lunar PuffSats for pulsed propulsion to lift terrestrial suborbital supply rockets into low Earth orbit. The supplies include solar panels, pusher plates, PuffSat skins, electronics, and rovers. These supply rockets then use conventional engines to gain  $\Delta V$  so they can resupply our lunar surface operations. When they reach the moon, we also use PuffSat pulsed propulsion to decelerate for lunar landing. The deceleration propulsion PuffSats would previously have been launched from the moon's surface into an eccentric lunar orbit opposite to the incoming supplies' velocity. We can optionally reduce terrestrial resupply requirements by embracing basic lunar manufacturing using metals like iron that are byproducts of lunar oxygen production. These lunar metals could be shaped into pusher plate and pulsed propulsion chamber components.

We use the rest of our lunar PuffSats to exponentially grow our PuffSat mass capacity in orbit using the Oberth cycle discussed in Section 4.2. Oxygen production is very energy intensive and lunar regolith will likely degrade machinery somewhat faster than equipment would degrade on Earth. Nevertheless, regolith resistant machines may still enable propulsion at costs that make hypersonic travel scalable.

### 4.4 Jurassic Dark: Lunar Cold Trap Paleontology and PuffSat Mining Ethics

In Section 4.2, we explored using lunar volatiles from permanently shadowed craters for PuffSat pulsed propulsion. These extremely cold craters could also indefinitely preserve DNA and other biomolecules from Earth impact ejecta [11]. While speculative, the potential scientific value of lunar cold trap paleontology obligates us to check for frozen fossil biomarkers as we mine lunar ice for PuffSat propulsion.

We could analyze the volatiles we're extracting to see if they contain homochiral organic molecules, which are only produced by living organisms. Studying samples that contain homochiral molecules would offer a unique window into Earth's entire biological history, potentially revealing how life began. And, of course, the discovery of dinosaur DNA would surely delight *Jurassic Park* [9] fans.

## 5 Sorry, I Don't Need ISRU

### 5.1 The Need For Speed [40]

If our propulsion PuffSats can reach high enough velocities, we could directly launch terrestrial payloads heavier than the PuffSats themselves. This would eliminate the need for lunar ISRU. Repeatedly executing this launch cycle with ever larger (or more numerous) payloads would enable exponential growth in our launch capacity. Consider a rocket launched from Earth carrying pulsed propulsion payload. We send  $\frac{3}{4}$  our payload on a prograde trajectory with a solar periapsis similar to the Parker Space Probe and the remaining quarter on the opposing retrograde trajectory with the same Sun grazing periapsis. These trajectories require high  $\Delta V$  but we can use Jupiter gravity assists to achieve them (See Section 5.5). These payloads release micro-thrust precision steered projectiles (see Section 5.3) which then collide sequentially at periapsis in a pulsed propulsion chamber as described in Appendix B. The resulting plasma can produce effective exhaust velocities of  $100 \text{ km/s}$  or higher. Perhaps we accelerate from  $200 \text{ km/s}$  to  $250 \text{ km/s}$  with Earth crossing speeds around  $150 \text{ km/s}$  [23]. At these Earth crossing velocities, incoming PuffSats could collide with PuffSats aboard a new terrestrial rocket in the rocket's propulsion chamber. With the thrust from these collisions, our payload would then be sent on prograde and retrograde orbits with low solar periapsis, repeating the cycle. If desired, we can optimize exhaust velocity further by lowering the periapsis in steps, allowing our payload to fall significantly towards the Sun after each step. This way, collisions after each periapsis reduction occur at progressively higher velocities for greater effective exhaust velocity. If we double payload mass every 6 months, we increase our initial payload by a factor of 1 million in less than a decade [23].

## 5.2 Radiative Differences From Project Orion

Project Orion required shaped explosives to redirect plasma towards the pusher plate because 80% of the bombs' energy became black body X-ray thermal radiation [51]. In contrast, our proposed system anticipates minimal radiative losses from collisions, even at speeds matching the Parker Solar Probe. Though detailed computer analysis is needed for full confirmation, our reasoning for this low loss stems from

- The colliding atoms in our system have a much lower atomic mass than fissile atoms. For a given total kinetic energy, this means the energy is distributed among a greater number of particles, resulting in a significantly lower average kinetic energy per particle, which directly translates to lower plasma temperatures. Additionally, plasmas formed from lighter elements generally have a higher specific heat capacity, meaning they absorb more energy for a given temperature increase.
- The mean velocity of colliding atoms is likely about  $\frac{1}{5}$  that of atoms in an inefficient 1% yield bomb. Since kinetic energy is proportional to the square of velocity, this alone suggests peak temperatures at least 25 times lower.
- Combined, lower mean velocity and atomic mass imply temperatures might be 200 times less in our collision than in a bomb. Radiative power rises with the fourth power of temperature ( $T^4$ ), so peak radiation flux is likely around 1 billion times less than the least efficient nuclear bombs.
- The colliding masses should be much smaller than a nuclear bomb, with a lower radiative surface area. As the collision plasma expands adiabatically, its volume increases proportionally faster relative to its initial volume compared to a larger bomb plasma for a given absolute linear expansion. This more rapid proportional change in volume leads to a quicker and more substantial decrease in temperature, further reducing radiative output.

Lower temperatures generate longer-wavelength blackbody X-rays compared to those from bombs. This means materials with lower atomic numbers (lower Z) can absorb this radiation and keep the plasma opaque. While Project Orion favored expensive and difficult to work with tungsten [51], these longer wavelengths should allow for the use of cheaper elements to achieve plasma opacity.

## 5.3 Solid Projectiles Rather Than Gas Generating PuffSats

Given the extreme velocities at periapsis, we no longer collide low density PuffSat produced gases because solid objects vaporize into opaque plasma. The real-world efficiency of these plasma explosions is likely high because the extreme temperatures should bring the entire plasma to thermal equilibrium before significant expansion occurs.

We'd make these solid projectiles primarily from cheap low atomic number (low Z) materials like boron nitride, motor oil, and graphite. A small amount of cheap higher Z materials like iron would be included to ensure opacity to the blackbody X-rays produced. All the projectile's mass contributes to propulsion, irrespective of its composition. As shown in Figure 6, the projectiles can contain electronics, heat shielding, and some liquid that passively or actively cools the skin through a centrifugally driven convection cycle. They can also partially be made from batteries so that solar power is not needed too close to the Sun.

## 5.4 Navigation Challenges Near Periapsis

Close solar periapsis involves some unique challenges. Obviously, any sensor dependent on visible light will need to filter interfering solar illumination. Instruments will need to handle heat and solar wind. Relativistic influences perturb the craft more than they would on Earth. High collision speeds demand extremely accurate navigation. The pulsed propulsion chamber may ablate slightly on each pulse. The impacting projectiles must be miniaturized to at most a few kilograms to contain the immense energy from explosions at these velocities.

Perhaps the most significant nuance is the need to adjust for solar weather. Since this weather influences luminosity, it also influences radiation pressure. Fortunately, neural networks appear capable of improving weather predictions [30].

Spacing PuffSats sequentially far apart may be hard. Objects far apart at periapsis get closer together as radial distance grows. As a result, Earth distance propulsion PuffSats would need to impart relatively high acceleration in short times. However, the terrestrial payloads we're directly accelerating this way should be unmanned.

When we lift high value payloads like astronauts into Low Earth Orbit, we use two sets of propulsive PuffSats. First, our Earth crossing PuffSats from the Sun push unmanned payloads into eccentric orbits around Earth. Then these eccentric payloads deploy PuffSats to push vital cargo like people or satellites just as we discussed in Section 3.1.

## 5.5 Initial Periapsis Orbits With Jupiter Gravity Assists

A final issue is placing the initial payload in a retrograde low periapsis solar orbit. The best approach for this is likely using a gravity assist from Jupiter, which was the original plan for the Parker Space Probe mission [37].

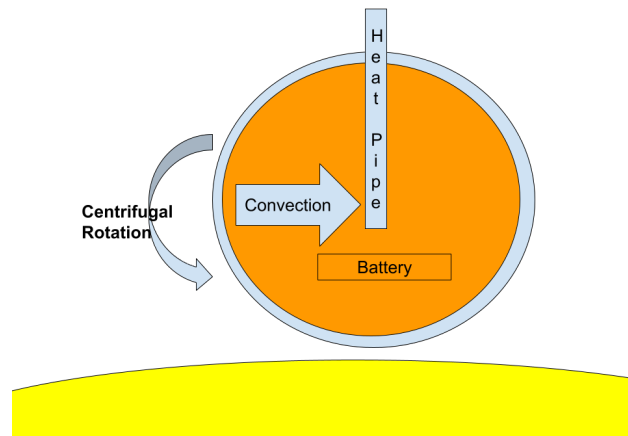


Figure 6: This cross-section shows a projectile with a highly reflective, heat-tolerant skin that is cooled by a centrifugally driven fluid. Heat is radiated away through a pipe that extends into the projectile's shadow. Batteries and electronics provide power.

To operate far from the Sun without large solar arrays, the spacecraft could rely on fuel cells or batteries. If the fuel cells or batteries contain explosive chemicals or have volatile reaction products like water vapor, these chemicals can be harvested for PuffSats gas production. Near Jupiter, the PuffSats volatiles would freeze and serve as effective radiation shielding. Together, the internal power source and shielding infrastructure would permit a close Jupiter flyby that maximizes our gravitational slingshot.

Optionally we can push more mass into the initial orbit by using a Jupiter gravity assist (possibly with a burn at Jupiter to leverage its Oberth effect) to place propulsion PuffSats into a retrograde Hohmann trajectory back to Earth. They would cross Earth at around 69 km/s, which could push a larger terrestrial payload onto prograde and retrograde colliding trajectories at low solar periapsis.

## 5.6 Jupiter-Only Exponential Launch Growth

A simpler way to bootstrap an exponential launch cycle is to use the retrograde Hohmann trajectory from Jupiter described in Section 5.5 but without close solar approaches. PuffSats returning from Jupiter can push more than 9 times their weight into a highly eccentric orbit around Earth. A small conventional burn coupled with solar electric engines and gravity assists with the inner planets can return this payload to Jupiter and restart the cycle. The growth is slow compared to other proposals but may provide sufficient launch capacity to supply the satellite market within a few decades.

We can also combine this Jupiter launch cycle with reusable rockets or the lunar ice based cycle discussed in Section 4.2. By increasing the number of initial PuffSat launches toward Jupiter, we can more rapidly scale up our launch throughput. Once this throughput is established, Earth based payloads can ride the returning PuffSats to orbit, enabling a sustainable and repeatable launch cycle.

## 6 One Hiroshima Per Second. The World Set Free

In Section 5.1, we propelled PuffSats to 150 km/s at 1 au using solar gravity and pulsed propulsion. A 60 TW pulsed heat source, which is equivalent to one Hiroshima bomb per second [66], requires harnessing the kinetic energy of just 5.3 t/s of propulsion mass at these speeds. For context, humanity's total power consumption is approximately 20 TW [49]. Given that typical power plants are roughly one-third efficient, a single one of these pulsed heat sources could meet the energy needs of all human civilization. Remarkably, this concept evokes H.G. Wells's prophetic vision in his 1913 novel, *The World Set Free*, where he imagined atomic bombs as a "blazing continual explosion" [62].

Using kinetic projectiles to generate terrestrial power only makes sense if it achieves massive economies of scale that outperform the linear costs and land use efficiency of conventional renewables. Let's explore how to build such a truly ambitious megastructure, and then explain why it's economically attractive in Section 6.4.



## 6.1 Straw Ways To Heaven

The most common proposal for utilizing space-based power on Earth involves wireless power transfer from orbiting power plants to terrestrial rectenna arrays [33]. Unfortunately, long distance wireless transfer requires breakthroughs in wireless beam focusing [70] and large radiators for dissipating heat. Moreover, the required wireless transmission infrastructure, both in space and on Earth, would be colossal. Given these challenges, let's investigate terrestrial solutions which directly convert kinetic impact energy to electricity on Earth.

To deliver kinetic energy projectiles to Earth, the projectiles must be able to withstand atmospheric entry. One solution is to build a vacuum tunnel, extending from Earth's surface to space, precisely aligned to allow incoming projectiles to pass through unimpeded. The tunnel is suspended from an anchor point as depicted in Figure 7. Enthusiasts have proposed numerous physically plausible structures that could support an anchor hoisted above Earth's atmosphere. These include Lofstrom Launch Loops [25], tethered and global orbital rings, space elevators, and space fountains [2]. However, these ambitious ideas generally suffer from very low Technology Readiness Levels (TRLs), meaning they are far from practical implementation.

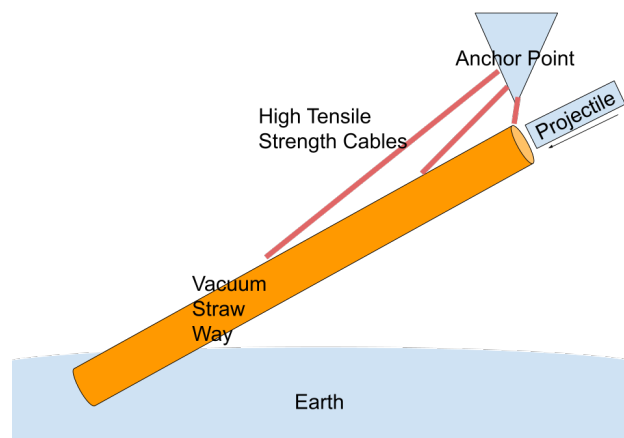


Figure 7: Vacuum tube suspended from cables allows projectiles through the atmosphere

Fortunately, PuffSat pulsed propulsion offers a promising path to position an anchor point above Earth. While this technology also lacks significant technical maturity, we would have already developed it to highly reliable standards if we were using it to direct projectiles at Earth using the techniques from Section 5.1.

A heavy lift rocket, such as SpaceX's Super Heavy [71], lifts the anchor point (and the vacuum tube it is connected to) to its initial height. We then indefinitely hover the anchor point using equal mass PuffSats that collide their gas output head on in a pulsed propulsion chamber (described in Section 4.2), redirecting thrust downward. The propulsion chamber exhaust can be angled slightly to provide thrust vectoring to counter atmospheric winds on the vacuum tube and support cables. A reaction control system on the anchor point adjusts the pulsed propulsion chamber so it stays precisely positioned for the next PuffSat collision. If these PuffSats meet at  $v_p = 11 \text{ km/s}$  at an average mass flow rate of  $1 \text{ t/s}$  they can theoretically suspend more than  $1100 \text{ t}$ .

In reality, energy losses would reduce thrust. For robust operations, we would need to lift redundant anchor points and vacuum tubes. Together, redundancy and energy losses imply we will need additional PuffSat propulsion collision mass per second. Nevertheless, lifting a few tons per second of propulsion PuffSat mass from Earth (as in Section 3.1) or the moon (as in Section 4.2) seems economically viable if we use our vacuum tube to cleanly produce all the energy required by mankind.

## 6.2 Vacuum Tube Details

To mitigate micrometeorite risk in the upper atmosphere, the vacuum tube incorporates sacrificial shielding or modular, swappable segments. A thin wire mesh embedded in the tube wall could detect conductivity changes caused by tears or punctures. Briefly increasing the current through these wires would cause localized heating, melting the surrounding material and heat-sealing small breaches. Redundant parallel tubes may also be deployed to ensure continuous operation despite localized damage.

The tube's walls taper with altitude, reflecting the reduced structural demands of maintaining vacuum at high elevations. The tube's optimal form will be maintained by cables with adjustable lengths connected to a central anchor point. The

tube can curve to compensate for Coriolis forces during projectile flight. The anchor point itself will rotate throughout the day to track the Sun. Sensors along the vacuum tube measure and broadcast the tube's position and shape, allowing incoming projectiles to navigate through it accurately.

To keep the vacuum tube aloft, PuffSat propulsion will be employed, even during inactive nighttime hours. Alternatively, for maintenance, the tube could be lowered at night and then re-hoisted by a heavy-lift rocket the following day.

Creating a high vacuum in long tunnels presents a challenge, though it's successfully achieved in facilities like the Large Hadron Collider. Fortunately, our system benefits from the projectiles themselves acting as a natural vacuum pump. Stray atoms will tend to be bounced downwards by projectile collisions. While some atoms may sputter off the projectiles, these will also be directed downwards. Ultra high vacuum equipment at the bottom of the tunnel will effectively remove these atoms, ensuring the vacuum remains strong.

High vacuum can be also maintained using NEG (non-evaporable getter) [16] thin film coatings placed at intervals along the tube, which chemically absorb reactive atoms. To achieve low temperatures at high altitudes, small tube sections can leverage both passive radiative cooling via high-albedo "solar white" films [57] and active refrigeration from ultralight solar-powered units. At these cold spots, we use small-scale cryopumping to remove noble gases like argon and other chemicals that NEG coatings can't adsorb.

Projectiles that catastrophically miss the vacuum tube cause only moderate Chelyabinsk level [46] ground effects because their extreme velocity guarantees they burn up at high altitudes. Assuming our vacuum tubes are in remote areas, this causes minimal disturbances to population centers. The vacuum tube itself is likely destroyed, but redundant vacuum tubes would then be moved into place.

### 6.3 Power Plant And Vacuum Air Lock Exchange Details

Beneath the vacuum tube, we propose excavating a massive steam chamber designed to vaporize incoming projectiles. These chambers would be substantial construction projects, engineered to withstand sudden changes in pressure and temperature. Suppose a  $0.1 \text{ km}^3$  steam chamber containing  $50 \text{ kg/m}^3$  steam receives a  $600 \text{ TJ}$  kinetic impact. As a simplification, let's say the steam has a constant specific heat of  $3.5 \text{ kJ}/(\text{kg}^\circ\text{C})$ . In this case the temperature change is  $\frac{600 \text{ TJ}}{5 \times 10^9 \text{ kg} \times 3500 \text{ J}/(\text{kg}^\circ\text{C})} = 34.2^\circ\text{C}$ . An impact of this magnitude every 10 seconds produces the heat to continuously provide all humanity's energy. This steam chamber would be connected to thousands of turbines and a massive cooling loop to harness and dissipate this energy.

Releasing large amounts of heat into the atmosphere would lead to unacceptable local temperature increases. Using a coolant loop that exchanges heat with deep ocean water will also have environmental consequences. Spreading  $40 \text{ TW}$  of heat over  $10 \text{ km}^3$  of deep ocean water would increase its temperature by  $\frac{40 \text{ TW} \cdot 3600 \text{ s/h}}{1 \times 10^{13} \text{ kg} \cdot 4186 \text{ J}/(\text{kg}^\circ\text{C})} = 3.44^\circ\text{C/h}$ . This rapid temperature change could severely damage local marine habitats.

However, considering the limited marine life found far above the ocean floor and below the sunlit zone, the broader deep sea ecology beyond the directly heated zone would remain stable. When compared to the widespread impacts of global anthropogenic climate change or even the significant displacement of wildlife from building solar farms, the environmental harm from this specific heat rejection method appears minimal.

An air lock separates the steam chamber from the rest of the tunnel as shown in Figure 8. A spinning door with a tip speed of  $300 \text{ m/s}$  could close a  $30 \text{ cm}$  diameter aperture in  $1 \text{ ms}$ . Even a  $5 \text{ m}$  long air lock is long enough to prevent steam molecules from traversing the air lock in this short time. We swap in a new air lock segment between kinetic projectile impacts. This gives us time to restore the high vacuum in the airlock segment before it's used again.

### 6.4 With Economies Of Scale, Our Ambitions Can Scale Too

While a global power plant requires a massive initial capital investment, its costs scale favorably with output. The cost of suspending a large vacuum tube depends very little on the plant's generating capacity. The cost of deep sea cooling loops would also be amortized across the entire planetary scale facility. A multi-terawatt installation could achieve significant per-watt cost reductions through bulk procurement of thousands of identical turbine and generator units.

Mass production reduces the cost of projectile electronics and micro thrusters. The cost of these components per projectile also remains nearly the same as individual projectile size increases. Ten seconds of planetary scale power corresponds to  $20 \text{ TW} \times 10 \text{ s} \approx 5.56 \times 10^7 \text{ kW h} = \$555,556$  at 1 cent per kilowatt-hour. This energy cost would likely dwarf the material costs of the projectiles themselves.

Power from our plant could be globally distributed by supertanker-sized batteries that connect to urban power grids at coastal ports. While the cost of utility-scale batteries is progressively declining, it remains a significant hurdle. Current battery designs prioritize efficient energy storage and release. However, if energy efficiency becomes less critical, we could design cheaper low performance batteries. Given that our power source exhibits strong cost efficiencies, we could

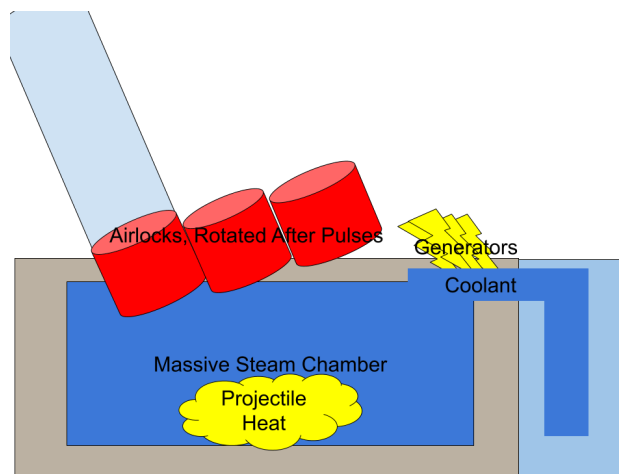


Figure 8: Diagram of the power plant and vacuum air lock system; new air lock segments are rotated in between impacts.

simply increase the power output to compensate for any energy losses incurred by using these more affordable batteries for distribution.

Batteries are environmentally attractive, but our world still depends heavily on fossil fuels. Very low cost power can cheaply produce hydrocarbon fuels from water and carbon dioxide. The hydrogen can come from electrolysis, while carbon dioxide comes from biomass, heating carbonates, industrial waste, or direct air/ocean capture.

Though the power plant and distribution infrastructure would cost billions to construct and operate, the revenue generated is staggering. Ultimately, we'd spend billions to make trillions annually from a planetary-scale plant. Turns out, if *Superman* wants to be as rich as *Lex Luthor*, he should get limitless energy not from the light of a yellow sun, but from its gravity [55].

## 6.5 Comparison To Project PACER

Project PACER was a 1970s Los Alamos concept to generate power by extracting steam from nuclear bombs detonated in a salt cavern [39]. Later improvements protected the cavern walls with an artificial waterfall of tritium breeding liquid salts [4].

Unlike PACER, our proposal does not produce radioactive waste or encourage the mass production of nuclear weapons. Should a liquid wall be needed to protect the chamber, it can be made from cheap materials like water. Tritium breeding and extraction are not required. Most critically, our design eliminates the need for a biological shield, simplifying the direct coupling of steam to turbines. This direct steam cycle enables the rapid heat exchange with the environment necessary to build terawatt-scale power plants.

## 6.6 To Solve Climate Change, Make The Earth A Death Star

A *Death Star* [64] is a giant sphere with a narrow 1 meter opening where you can shoot something down to create an explosion inside the main reactor. Building a *Death Star* from scratch would be a huge undertaking. Fortunately, if we build the Straw Way To Heaven described in Section 6.1, we're living on one. Although our Straw Way generator produces clean energy from incoming projectiles, its power production is restricted to daytime hours when the straw can face the sun. Also, a limitless clean energy source would only slow climate change. Industrial carbon emissions from steel, cement, agriculture, and other processes would still heat the planet [6].

### 6.6.1 That's No Moon [26]. Oh Wait, It's Literally Our Moon

Projectiles made from lunar materials could enter a terrestrial Straw Way from high angles of attack around the clock. Lunar regolith is primarily carbon depleted rock [38]. If this rock was heated, vaporized, and pressurized as it fell into deep ocean water, it would rapidly absorb carbon dioxide to form carbonates that negate industrial carbon pollution.

To generate 60 TW of heat from lunar bombardment, we'd need an astonishing 1 kt/s of lunar mass to pass through the terrestrial vacuum tube. Such a vast quantity is daunting, but the momentum for launching off the moon could come from kinetic projectiles inbound from the Sun (as described in Section 5.1). Beyond providing thrust, these projectiles aimed at the Moon could vaporize lunar regolith. The resulting thermal energy could be harnessed for electricity

generation or to power chemical and industrial processes directly. This lunar power source could support large scale mining and production of the oxygen gas used in PuffSat pulsed propulsion (as discussed in Section 4.3).

## 6.7 Fusion Propulsion And Epstein Drives

The fast projectiles from Section 5.1 could propel a spacecraft around the inner solar system at relatively high speeds. As our technology advances, we'd want to travel on brachistochrone trajectories under constant Earth gravity acceleration between the planets as envisioned in *The Expanse* [8]. Evaporative cooling and advanced heat shields like NASA's yttrium oxide based "solar white" might enable spacecraft to approach the Sun to 2 solar radii [57]. At this close solar periapsis, prograde and retrograde projectile collision velocities would exceed 869 km/s [23] in the reference frame of a fusion pulsed propulsion chamber on the target rocket.

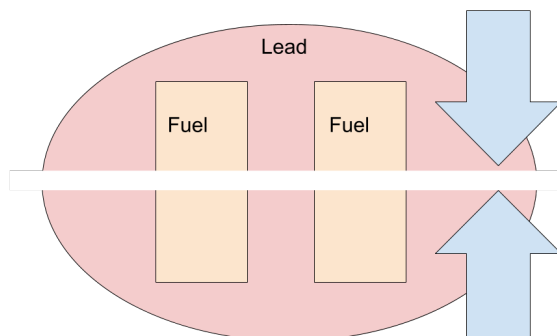


Figure 9: A lead tamper generates immense shock heating around fusion fuel and compresses it to ignition conditions during head-on collisions. Lead embedded in the fuel also serves as a superheated Teller-Ulam style spark plug [73] for fusion.

A 1979 Los Alamos Impact Fusion workshop concluded speeds of just 200 km/s might be sufficient for precompressed gram sized fusion fuel projectiles to ignite [45]. Larger projectiles would likely be easier to confine long enough for high fusion energy gain. A lead tamper, as depicted in Figure 9 surrounding a few hundred grams of fusion fuel could ignite fusion explosions and trigger immense exhaust velocities. Shocked lead would reach even higher temperatures than the fuel because its high atomic number implies greater energy per atom (see Section 5.2). Therefore, lead or another high-Z material is centrally embedded in the fusion fuel at the tip of the colliding masses. This embedded lead serves as a "spark plug" for fusion, analogous to the secondary fission bomb in Teller-Ulam style [73] nuclear explosions. Pulsed fusion propulsion would likely employ the shaped nuclear charges Project Orion explored to redirect energy and thrust. With mostly aneutronic fusion fuel, projectiles could reach velocities on the order of thousands of kilometers per second. This is because aneutronic fusion directly converts energy into charged particle kinetic energy, bypassing the mass penalty of neutron shielding. A seed of deuterium-tritium could ignite a larger deuterium and helium-3 mixture to achieve aneutronic fusion rocket speeds. As the spacecraft accelerates, it can also reach speeds where it triggers fusion by crashing into slower moving fusion fuel targets. If carefully planned, these chains of fast-moving projectiles could essentially create interplanetary highways, allowing people to travel between planets under comfortable artificial Earth gravity in time frames comparable to ocean liners crossing the Atlantic.

## 6.8 The Sixth Question For Climate Change

Bill Gates' excellent book, *How to Avoid a Climate Disaster* [15], details five practical questions [12] any effective climate solution must address. Our Straw Way To Heaven (see Section 6.1) addresses Gates' questions better than other alternatives. It completely negates carbon emissions, reverses cement emissions, provides indefinite global power, occupies minimal space, and boasts marginal costs that decline rapidly with output.

Yet, I respectfully propose a sixth question that could galvanize the public to enthusiastically support a particular climate solution. Beyond just reducing our electric bills and helping the environment, how will this breakthrough drastically improve daily life? An investment on the scale required to solve climate change should ideally grant human society new abilities, such as hypervelocity transport and affordable space travel. PuffSat pulsed propulsion can achieve all of these things.

## 7 When We Get Greedy, We'll Go to Phoebe

In Section 5.1 we discussed using Sun-grazing Oberth maneuvers to accelerate projectiles to 150 km/s at 1 au. These high velocities enable the large  $\Delta V$  required to place the next suborbital rocket into prograde and retrograde colliding orbits near the Sun. However, as detailed in Section 5.4, such close solar approaches introduce severe engineering and operational challenges—potentially increasing projectile costs compared to less extreme solar encounters.

Orbits with higher apoapsis require less  $\Delta V$  to shed orbital angular momentum and lower their periapsis. For example, transferring to a solar impact trajectory from Saturn requires only about 10 km/s, compared to roughly 30 km/s from Earth. This makes Saturn a more efficient departure point for reaching the inner solar system or the Sun.

Saturn's irregular moon Phoebe lies just  $180^\circ - 173.4^\circ = 6.6^\circ$  from the solar ecliptic [72], giving it a favorable alignment for interplanetary transfers. Its high altitude orbit around Saturn yields a low orbital velocity, enabling efficient low  $\Delta V$  transfers to elliptical trajectories that match Phoebe's apoapsis and dip toward Saturn at periapsis. From Phoebe, a prograde rocket could be launched to collide with retrograde payloads also originating from Phoebe. These collisions could take place in a pulsed propulsion chamber near Saturn, enabling highly efficient Oberth maneuvers. With careful targeting to avoid Saturn's rings, this method could launch spacecraft toward the inner solar system. Precisely aiming such collisions near Saturn is challenging, but likely easier than attempting similar maneuvers at the extreme conditions of close solar periapsis described in Section 5.1. PuffSats launched from Saturn toward Earth could power a Straw Way generator (see Section 6.1) or deliver suborbital rockets into orbit (see Section 3.1).

These rockets could also return to Phoebe at high speeds, launching additional mass toward Saturn via pulsed propulsion. This bootstrapped launch cycle from Phoebe mirrors the lunar exponential growth loop discussed in Section 4.2, but benefits both from Phoebe's lower escape velocity and from Saturn's larger gravitational Oberth effect. Power for mining operations on Phoebe could come from solar energy concentrated using lenses made from Phoebe's native ice or locally produced plastic. Fission reactors transported from Earth are another possibility, as is thermal energy generated by returning impactors.

With an estimated composition of nearly 50% ice by mass [72], Phoebe offers essentially unlimited volatile resources to fill PuffSats. Unlike the Moon's permanently shadowed ice deposits, Phoebe's ice-rich regions receive direct sunlight. Although faint, this illumination enables solar concentrators to generate power directly adjacent to mining operations. Phoebe's abundant water could be used to wash regolith from equipment, mitigating the mechanical fouling that plagues lunar hardware. In addition, Phoebe's regolith—composed largely of frozen volatiles—is likely softer and less abrasive than the Moon's harsh dust, reducing wear on machinery. By contrast, lunar volatiles are scarce, and oxygen extraction from lunar regolith (see Section 4.3) is highly energy-intensive.

Phoebe's ultra-low gravity makes it difficult to anchor mining infrastructure securely. However, its volatile-rich composition allows a supplemental solution: thermal retro-rockets powered by in-situ steam. To save energy, icy reaction mass could also be launched mechanically from Phoebe's surface without first converting it to steam. If Phoebe's gravity proves too low for certain operations, Iapetus could serve as a potential backup site. Similarly, Jupiter's moon Himalia may support analogous maneuvers if exploration reveals significant volatile deposits.

Mining moons like Phoebe to supply PuffSat payloads is easier than mining them for terrestrial raw materials. PuffSats are optimized for high-velocity flybys, not deceleration, which slashes their required  $\Delta V$ . This eliminates the need for costly braking maneuvers. Unlike mining for ice or gold, the large-scale extremely high energy density pulses created by inbound PuffSats are a resource that simply cannot be created on Earth with any known technology, save for nuclear weapons.

### 7.1 Mining Helium-3

Helium-3 for aneutronic fusion may be available on the Earth's moon [13], but likely not in quantities to support large scale fast interplanetary transport like discussed in Section 6.7. However, the gas giants contain inexhaustible supplies of helium-3 [44]. A nuclear fission thermal rocket or scram jet could extract helium 3 and hydrogen while flying in Saturn's atmosphere and then jump a few thousand kilometers above the atmosphere. It could then separate from a payload carrying mined Helium-3, falling back to Saturn to mine more. An accident on such a fission rocket would cause no harm, because waste would simply fall into Saturn's core. Propulsion PuffSats from Phoebe could then send the Helium-3 payload into the inner solar system for use in fusion rockets.

If fission rockets prove politically unpalatable, chemical rockets may also work. Chemical rocket fuel powers a motor in Saturn's atmosphere for the energy to mine helium-3. The rocket then fires its rockets to hop above Saturn's atmosphere. Propulsion PuffSats from Phoebe push the rocket into a stable orbit where it is refueled and releases its helium-3 payload. Then new propulsion rockets decelerate the refueled rocket so that it falls into Saturn's atmosphere for another mining round.

## 8 War, Policy, And Pulsed Propulsion

### 8.1 Fusion Rockets And The Outer Space Treaty

The Outer Space Treaty [58] prohibits nuclear weapons in space. The legality of pure fusion rockets like those discussed in Section 6.7 requires clarification, likely through international dialogue and new legal frameworks.

### 8.2 Hackers Must Be Prevented From Causing Catastrophic Explosions

As previously discussed, the energy projectiles for the Straw Way To Heaven discussed in Section 6.1 are intentionally designed to burn up high in the atmosphere without causing damage in case of a mishap. However, there is a danger a hacker could manipulate micro-thrusters on the projectiles to enter the atmosphere simultaneously rather than in sequence, leading to larger Tunguska [32] sized multi-megaton explosions. We can mitigate this risk with standard software security practices like using memory safe languages and authenticated communication.

### 8.3 Risk Of PuffSat Sabotage

PuffSat pulsed propulsion might be useful for launching military assets like Golden Dome [36] or the Brilliant Boulders [24] discussed on the blog related to this paper [50]. The PuffSats described in Section 4.2 are likely vulnerable to destruction from high powered terrestrial lasers by a military adversary. Nations will need to defend their payloads from sabotage by hostile actors.

### 8.4 Aviation Exclusion Zone Needed For Straw Ways

Since the Straw Way To Heaven (see Section 6.1) is a fixed structure in the sky, we will need regulations to ban aviation next to it. This seems feasible given the straw way will be placed in a remote area. The host nation must also guard the Straw Way against sabotage.

## 9 Conclusion And Future Directions

This paper has introduced the transformative potential of PuffSat pulsed propulsion. We've demonstrated how a PuffSat's intricate navigation, made viable by advancements in CubeSat formation flying, could revolutionize hypersonic intercity transport. PuffSats also offers a novel approach to reverse global warming, provide limitless affordable power, and even enable human colonization of the solar system with fusion power.

Our next steps involve simulating the fundamental physics and prototyping the control software for PuffSat pulsed propulsion, ensuring the most accurate simulations possible. We also plan to solicit feedback on current challenges impeding these concepts and assess their economic and technical surmountability.

If the basic physics of PuffSat pulsed propulsion work, we'd likely proceed with different technologies in different time frames. An aspirational "Elon time" [74] roadmap of when each technology could be developed is proposed in Table 4.

Aspirational Time Frame	Action
Now	Prototype satellite launch and hypersonic travel using PuffSat pulsed propulsion from PuffSats launched by large reusable rockets
Now	Prototype satellite launch using reverse Hohmann transfer from Jupiter as described in Section 5.6
Near Term	Prototype launches using lunar volatiles or mined lunar oxygen instead of large reusable rockets
Mid Term	Prototype leveraging close solar approaches or material from Phoebe/Saturn for PuffSat pulsed propulsion
Mid to Long Term	Prototype constructing a Straw Way To Heaven and energy infrastructure based on it
After the Singularity (Far Distant Future)	Prototype fusion rockets and interplanetary highways

Table 4: Proposed schedule for future work

Marc Andreessen once said "software is eating the world" [34]. If control software enables PuffSat pulsed propulsion, it will devour the solar system as well.

## A Derivation Of PuffSat Mass/Rocket Mass Continuous Approximation

We want to approximate the ratio of the total PuffSat mass  $m_p$  with all PuffSats traveling at velocity  $v_p$  for a sequence of PuffSats to push a rocket with mass  $m_r$  with initial velocity  $v_{ri}$  to final velocity  $v_{rf}$ . Let's initially naively assume every collision is perfectly elastic in one dimension. We'll use calculus to get a closed form expression by solving for a

rocket continuously bombarded by infinitesimal PuffSats each with mass  $dm_p$ . (Note: Grok [75] helped with some of the math for this derivation and parts of this derivation are copied from Grok results directly)

The initial velocities are

- Mass  $m_r$ : Velocity  $v_r$ .
- PuffSat: Mass  $dm_p$ , velocity  $v_p$ .

After the collision, let:

- Mass  $m_r$ : Velocity  $v_r + dv_r$ .
- PuffSat: Velocity  $v'_p$ .

### A.1 By Conservation Of Momentum

$$\begin{aligned}
 m_r v_r + dm_p v_p &= m_r (v_r + dv_r) + dm_p v'_p \\
 m_r v_r + dm_p v_p &= m_r v_r + m_r dv_r + dm_p v'_p \\
 dm_p v_p &= m_r dv_r + dm_p v'_p \\
 m_r dv_r &= dm_p (v_p - v'_p)
 \end{aligned} \tag{1}$$

### A.2 Velocity Change Of $m_r$

For an elastic collision

$$v'_p = \frac{2m_r}{m_r + m_p} v_r + \frac{m_p - m_r}{m_r + m_p} v_p \tag{2}$$

Since  $m_r \gg m_p$  we plug  $m_p = 0$  into Equation 2 and find

$$v'_p = 2v_r - v_p \tag{3}$$

Substituting  $v'_p$  from Equation 3 into Equation 1:

$$\begin{aligned}
 m_r dv_r &= dm_p (v_p - (2v_r - v_p)) \\
 m_r dv_r &= dm_p (v_p - 2v_r + v_p) \\
 m_r dv_r &= dm_p (2v_p - 2v_r) \\
 m_r dv_r &= 2dm_p (v_p - v_r) \\
 dv_r &= \frac{2(v_p - v_r)}{m_r} dm_p
 \end{aligned} \tag{4}$$

### A.3 Integrate Over Many Collisions

The velocity of  $m_r$  changes from  $v_{ri}$  to  $v_{rf}$  as more PuffSats collide. Integrate Equation 4:

$$\int_{v_{ri}}^{v_{rf}} dv_r = \int_0^{m_p} \frac{2(v_p - v_r)}{m_r} dm_p$$

The left-hand side is:

$$\int_{v_{ri}}^{v_{rf}} dv_r = v_{rf} - v_{ri}$$

For the right-hand side, treat  $v_r$  as a function of the accumulated PuffSat mass  $m_p$ . However, we need to express  $v_r$  in terms of  $m_p$ . From Equation 4:

$$\frac{dv_r}{v_p - v_r} = \frac{2dm_p}{m_r} \tag{5}$$

Since  $v_p$  is constant,  $dv_p = 0$  and  $dv_r = -d(v_p - v_r)$ , so we can rewrite Equation 5 as:

$$-\frac{d(v_p - v_r)}{v_p - v_r} = \frac{2dm_p}{m_r}$$

Integrate both sides: - Left:  $\int_{v_p-v_{ri}}^{v_p-v_{rf}} -\frac{d(v_p-v_r)}{v_p-v_r} = \int_{v_{ri}}^{v_{rf}} \frac{dv_r}{v_p-v_r}$

$$= [-\ln |v_p - v_r|]_{v_{ri}}^{v_{rf}} = \ln \left| \frac{v_p - v_{ri}}{v_p - v_{rf}} \right|$$

- Right:  $\int_0^{m_p} \frac{2dm_p}{m_r} = \frac{2m_p}{m_r}$  Equate:

$$\ln \left| \frac{v_p - v_{ri}}{v_p - v_{rf}} \right| = \frac{2m_p}{m_r}$$

Solve for  $m_p$ :

$$\begin{aligned} \left| \frac{v_p - v_{ri}}{v_p - v_{rf}} \right| &= e^{2m_p/m_r} \\ m_p &= \frac{m_r}{2} \ln \left| \frac{v_p - v_{ri}}{v_p - v_{rf}} \right| \end{aligned} \quad (6)$$

#### A.4 Interpret The Absolute Value

The absolute value accounts for the direction of velocities: - If  $v_p > v_{ri}$  and  $v_p > v_{rf}$ , then  $v_p - v_{ri}$  and  $v_p - v_{rf}$  are positive, so:

$$m_p = \frac{m_r}{2} \ln \left( \frac{v_p - v_{ri}}{v_p - v_{rf}} \right)$$

#### A.5 Compute PuffSat To Rocket Mass Ratio, With A Fudge Factor For Real World Losses

We can then solve for the total PuffSat to rocket ratio, with a fudge factor  $f$  between 0 and 1 to account for the coefficient of restitution and imperfect spread of gaseous volatiles off the pusher plate. Let's naively assume this fudge factor is the same for each collision even though in practice it would likely vary as the relative velocity of the PuffSats and the rocket change.

$$\frac{m_r}{m_p} = \frac{2f}{\ln \left( \frac{v_p - v_{ri}}{v_p - v_{rf}} \right)} \quad (7)$$

### B Deriving Effective Exhaust Velocity for Idealized 100% Efficient Prograde/Retrograde PuffSat Collision Rocket Thrust

Suppose a retrograde PuffSat with  $m_{rp}$  and a prograde PuffSat with  $m_{pp}$  collide in a pulsed rocket propulsion chamber, as depicted in Table 3. We want to find the maximum exhaust velocity  $v_e$  for the prograde rocket when engine efficiency is 100% and we expel all the combined gas behind us (in the retrograde direction). For simplicity we say

$$m_{rp} + m_{pp} = 1 \quad (8)$$

Each PuffSat has velocity  $v_p$  so the retrograde PuffSat has velocity  $2v_p$  in the reference frame of the prograde PuffSat. In the prograde reference frame, kinetic energy is

$$E = \frac{m_{rp}(2v_p)^2}{2} = 2m_{rp}v_p^2 \quad (9)$$

Let  $v_g$  be gas exhaust velocity expelled from the rocket, and assume this mass is infinitesimal compared to the entire prograde payload. Applying mass from Equation 8 and kinetic energy from Equation 9, we have

$$2m_{rp}v_p^2 = \frac{v_g^2}{2} \quad (10)$$

and solving for  $v_g$  we get

$$v_g = \sqrt{4v_p^2 m_{rp}} = 2v_p \sqrt{m_{rp}} \quad (11)$$

Total momentum change is

$$(m_{rp} + m_{pp})v_g - 2v_p m_{rp} = v_g - 2v_p m_{rp} = 2v_p(\sqrt{m_{rp}} - m_{rp})$$

Differentiating and solving for zero, it's easy to show that

$$m_{rp} = \frac{1}{4}, v_g = v_p, v_e = \frac{v_p}{2} \quad (12)$$



## C AI And Citations Transparency Acknowledgement

The ideas in this paper come from the author. However, some artwork was created with AI tools. AI tools also helped suggest writing improvements. It's possible the AI training might regurgitate writing from other authors. Please inform me if you see this, so I can add citations.

More generally, I am not an expert in the field, so it's possible I failed to cite prior work for some of the ideas presented. Please let me know if I inadvertently present any novel concepts that are actually from others, so I may cite relevant work. Note that I am also less rigorous with citations to my own blog than with other writings.

The author previously worked at Netflix, which produces content related to some popular culture titles referenced in the paper. However, I am no longer employed there and am not a major investor. The author's blog is not monetized and is primarily to further explain this paper's ideas. In short, I do not believe I have any financial conflicts of interest at the present time.

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