

## 6.5 First-order and second order Lecture 3g

### Continuous-time systems

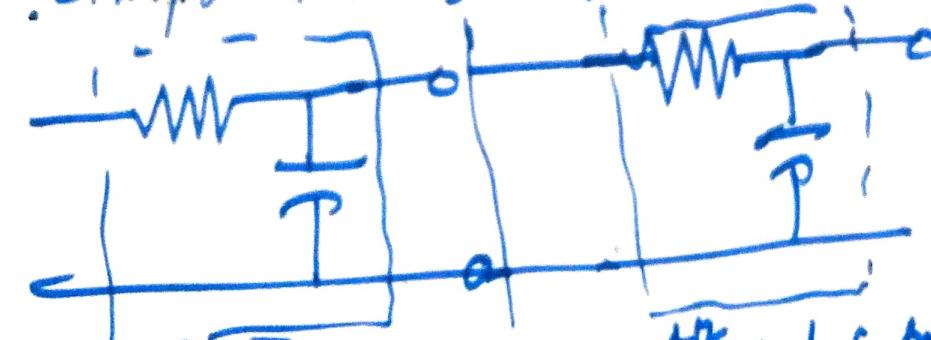
Why 1<sup>st</sup> and 2<sup>nd</sup> order?

⇒ Most of the higher order systems (including in control system) can be modeled in terms of 1<sup>st</sup> and 2<sup>nd</sup> order primitives.

#### (case I) First order Systems

Order of system = Order Differential equation determining dynamics of underlying system.

A. Simple RC series circuit:



1<sup>st</sup> order system

1<sup>st</sup> order system.

Fig. 2<sup>nd</sup> order as cascade of two 1<sup>st</sup> order sysys

①

In chapter 1, Differential Equations determine  
dynamics & RC effect.

$$(RC) \frac{dy(t)}{dt} + y(t) = x(t)$$

$$\text{Let } RC = T$$

∴ Generalized mathematical model for  
First-order system is

$$I. \frac{dy(t)}{dt} + y(t) = x(t)$$

Chapter 4 ⇒ Frequency response of RC circuit  
problem by convolution method

$$I = F\left\{\frac{dy(t)}{dt}\right\} + F\{y(t)\} = X\{H(j\omega)\}$$

$$\therefore H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{1}{1+j\omega T}$$

$$\therefore h(t) = F^{-1}\{H(j\omega)\} = F^{-1}\left\{\frac{1}{1+j\omega T}\right\}$$

$$② h(t) = \left(\frac{1}{T}\right) \left\{ F^{-1}\left\{\frac{1}{j\omega + \frac{1}{T}}\right\} \right\}$$

$$h(t) = \left(\frac{1}{t}\right) \cdot e^{-\frac{E}{kT}} \cdot u(t)$$

$$\tau_{\text{HOM}} = \frac{-1/kT}{e^{-\frac{E}{kT}} \cdot u(t)} \rightarrow f(\frac{E}{kT})$$

$$H_{\text{OM}} = \frac{1}{1 + f(\frac{E}{kT})} \rightarrow F(f(\frac{E}{kT}))$$

$\Sigma$  inverse relationship between time & frequency

dimens.  $\rightarrow$  Heisenberg's uncertainty.

$\therefore$  step response of first order system is given by.

$$S(t) = \int_{-\infty}^t h(\tau) d\tau = \int_{-\infty}^t \left[ \frac{1}{\tau} e^{-\frac{E}{kT} \cdot u(\tau)} \right] d\tau$$

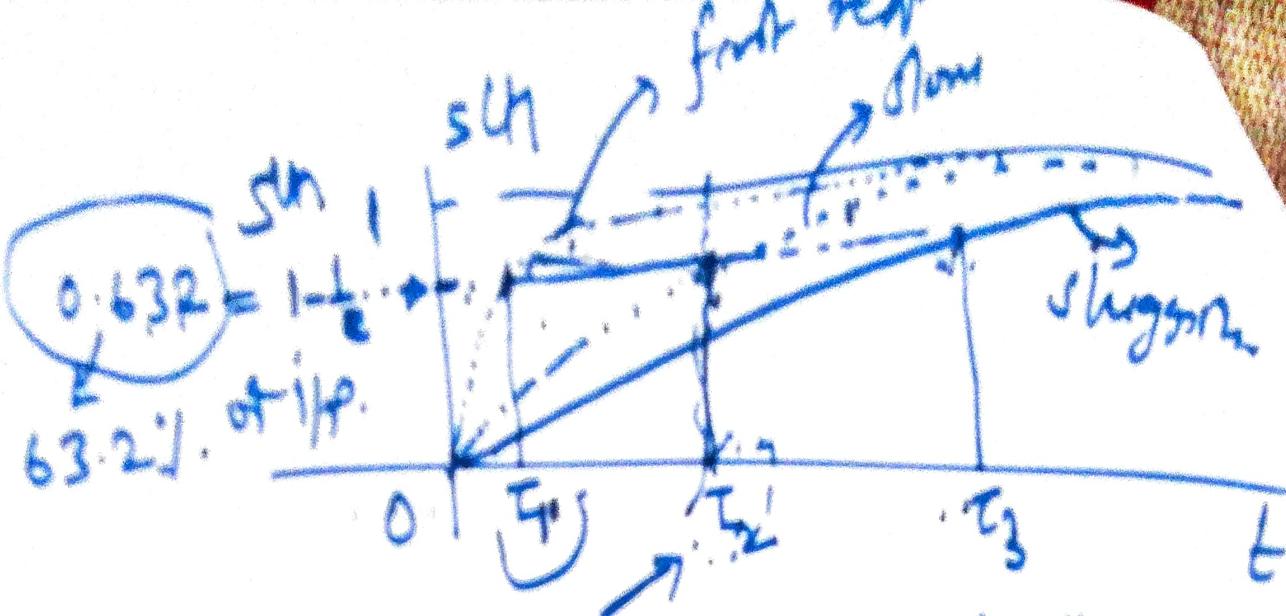
$$S(t) = \left[ 1 - e^{-\frac{E}{kT} \cdot u(t)} \right] u(t)$$

At  $t = T$ ,

$$S(T) = \left[ 1 - e^{-\frac{E}{kT} \cdot u(T)} \right] u(T)$$

$$= \left[ 1 - \frac{1}{e} \right] (u(T))^{S(t)}$$

$$S(T) = \frac{e-1}{e+1} = \frac{2.718281828459045}{2.718281828459045} = 0.632$$



Time constant of the first order system.

→ Time constant ( $\tau$ ) indicates speed of response (fast, slow, slugger).

$$\tau_1 < \tau_2 < \tau_3$$

$$H(\omega) = \frac{1}{1 + j\omega\tau}$$

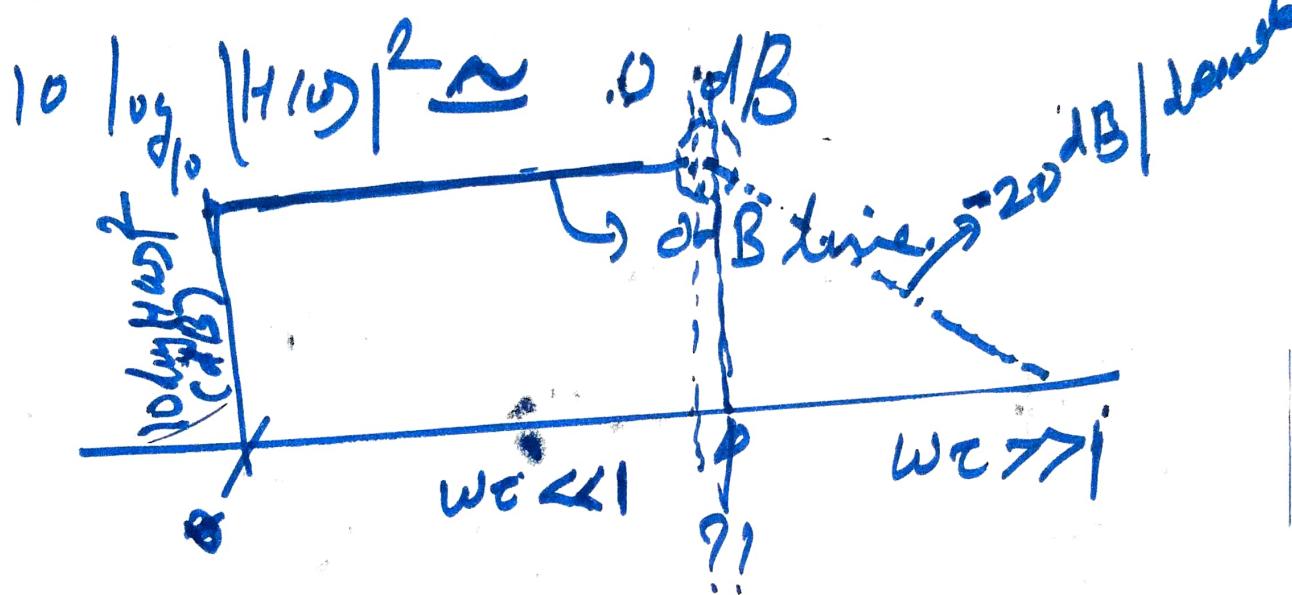
$$|H(\omega)|^2 = \frac{|H(\omega)|^2}{|X(\omega)|^2} = \frac{1 + \tau^2}{1 + j\omega\tau|^2} = \frac{1}{1 + \omega^2\tau^2}$$

$$\begin{aligned} 10 \log_{10} [ |H(\omega)|^2 ] &= 10 \log_{10} \left( \frac{1}{1 + \omega^2\tau^2} \right) \\ &= (10 \log_{10} 1) - 10 \log_{10} (1 + \omega^2\tau^2). \end{aligned}$$

$$10 \log_{10} |H(\omega)|^2 = -10 \log_{10} [1 + (\omega\tau)^2] \quad \dots$$

Case I)  $\omega\tau \ll 1 \rightarrow (\omega\tau)^2 \ll 1$

$$\therefore 1 + (\omega\tau)^2 \approx \cancel{(\omega\tau)^2} \quad 1$$



Case II)  $\omega\tau \gg 1$

$$1 + (\omega\tau)^2 \approx (\omega\tau)^2$$

$$\therefore 10 \log_{10} |H(\omega)|^2 \approx -10 \log_{10} (\omega\tau)^2$$

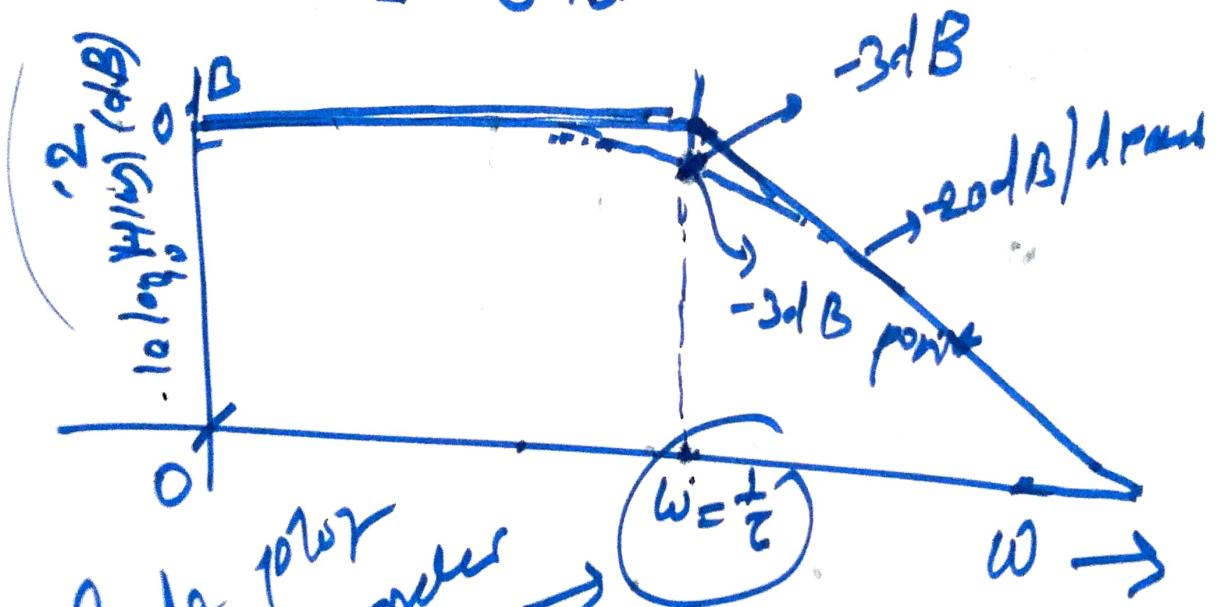
$$\approx -20 \log_{10} (\omega) - 20 \log_{10} (\tau)$$

where  $y = mx + f$  / decade

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$$\text{Let } \omega = \frac{1}{\tau}$$

$$\begin{aligned} \therefore 10 \log_{10} |H(\omega)|^2 &= -10 \log_{10} [1 + (\omega\tau)^2] \\ &= -10 \log_{10} [1 + \left(\frac{1}{\tau} \times \tau\right)^2] \\ &= -10 \log_{10} (2) \\ &\approx -3 \text{ dB} \end{aligned}$$



Bode plot for first order system  
Break Frequency.  
Magnitude

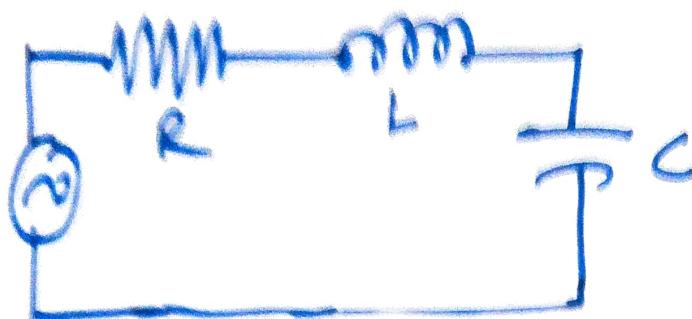
→ sketch phase plot - Homework.

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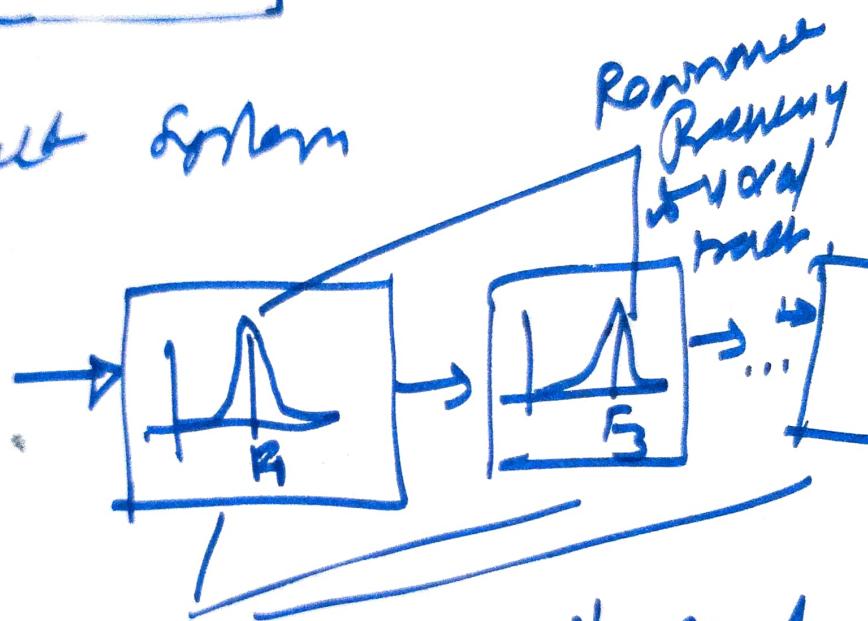
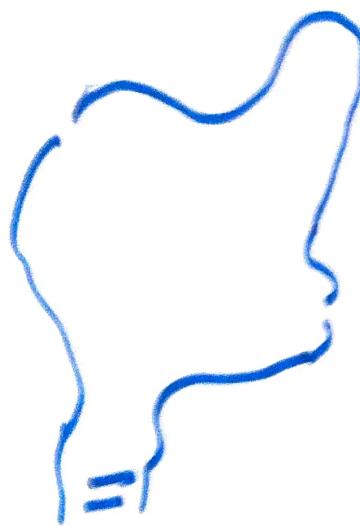
## use II Second Order Systems.

Examples: →

① Series RLC circuit.



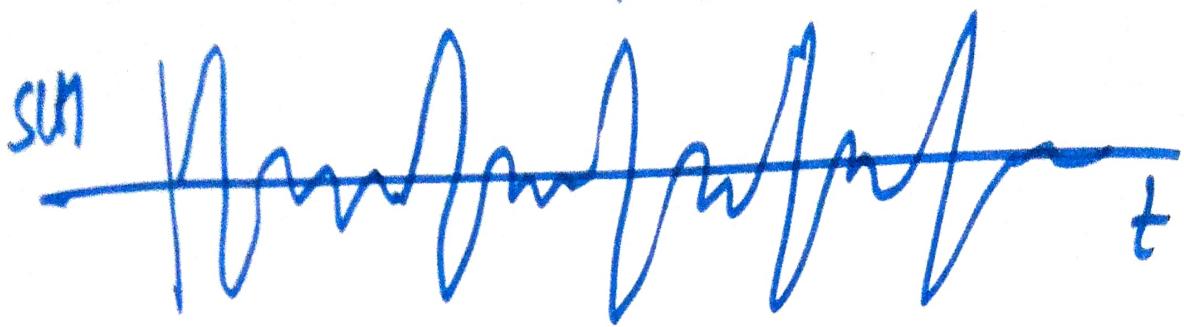
② Vocal Tract system



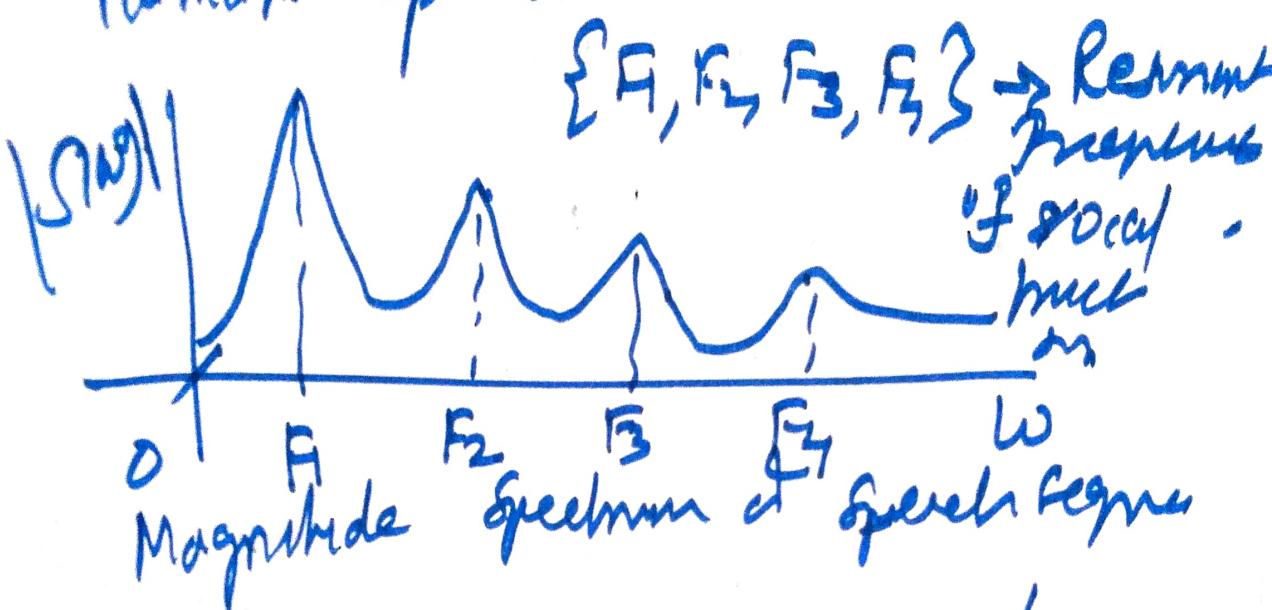
Example of several second order sysm

Maurice Schröder (Bell Labs): Human beings produce and perceive sounds by spectral peaks than spectral valley.

Vowel 'ai' /ai/

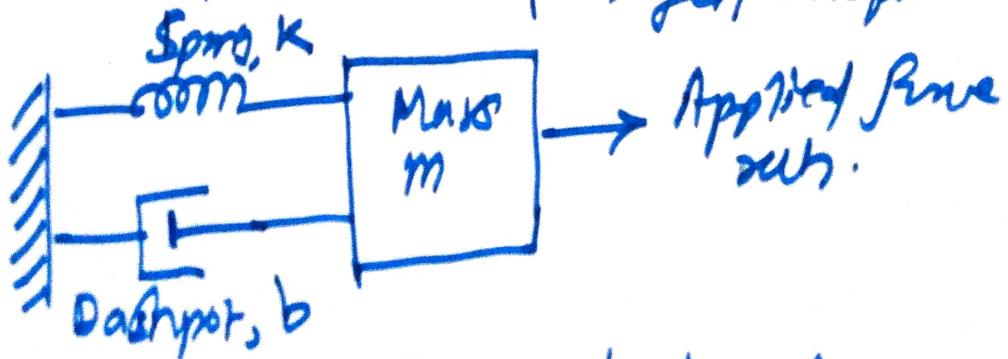


Human speech



→ Each of  $F_i$ 's → corresponds to a 2nd order system.

③ Mass-spring-damper system  $\rightarrow$  get Displacement.



Ideal SHM  $\rightarrow$  (No dashpot),  $b=0$ .

$$\sum F = m \cdot a$$

(Net force)

$$m \frac{d^2 y_m}{dt^2} = x_m - k \cdot y_m - b \frac{dy_m}{dt}$$

$$\frac{d^2 y_m}{dt^2} + \left(\frac{b}{m}\right) \frac{dy_m}{dt} + \left(\frac{k}{m}\right) \cdot y_m = \left(\frac{1}{m}\right) \cdot x_m$$

— P2

2nd order Differential Equations.

$$\frac{d^2 y_m}{dt^2} + 2\zeta \cdot \omega_n \frac{dy_m}{dt} + \omega_n^2 \cdot y_m = \omega_n^2 \cdot x_m$$

— P3

$$2\zeta \omega_n = \gamma_m$$

$$\omega_n^2 = \gamma_m \rightarrow \omega = \sqrt{\gamma_m}$$

$$\therefore 2\zeta (\sqrt{\gamma_m}) = b/m$$

$$\therefore \zeta = \frac{b}{2\sqrt{\gamma_m}} = \frac{\text{damping}}{\text{ratio}} = R(b, k, \omega)$$

Objective is to find Bode Plot, for 2<sup>nd</sup> order system

→ Use CTFB, Amplitude term

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{\dots \omega_n^2}{(j\omega)^2 + 2\xi\omega_n(j\omega) + \omega_n^2}$$

$$(j\omega)^2 + 2\xi\omega_n(j\omega) + \omega_n^2 \Rightarrow ax^2 + bx + c$$

where  $x = j\omega$ .

$$\zeta_1, \zeta_2 = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$= \frac{-2\xi\omega_n \pm \sqrt{(-2\xi\omega_n)^2 - 4 \times 1 \times \omega_n^2}}{2 \times 1}$$

$$\zeta_1, \zeta_2 = -\xi\omega_n \pm \omega_n \sqrt{\xi^2 - 1}$$

$$\boxed{\zeta_1, \zeta_2 = -\xi\omega_n \pm j\omega_n \sqrt{1 - \xi^2}}$$

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: Complex zeros.

$$H(\omega) = \frac{A_1}{\omega_n^2}$$

Using method of Partial Fraction Expan.

$$= \frac{A_1}{j\omega - c_1} + \frac{A_2}{j\omega - c_2}$$

$$A_2 = -A_1$$

$$H(\omega) = \frac{A_1}{j\omega - c_1} - \frac{A_1}{j\omega - c_2}$$

$$\mathcal{F}\{H(\omega)\} = A_1 \mathcal{F}\left\{\frac{1}{j\omega - c_1}\right\} - A_1 \mathcal{F}\left\{\frac{1}{j\omega - c_2}\right\}$$

$$h_h = A_1 [e^{c_1 t} \cdot u_h] - A_1 [e^{c_2 t} \cdot u_h]$$

$$= A_1 [e^{c_1 t} - e^{c_2 t}] \cdot u_h$$

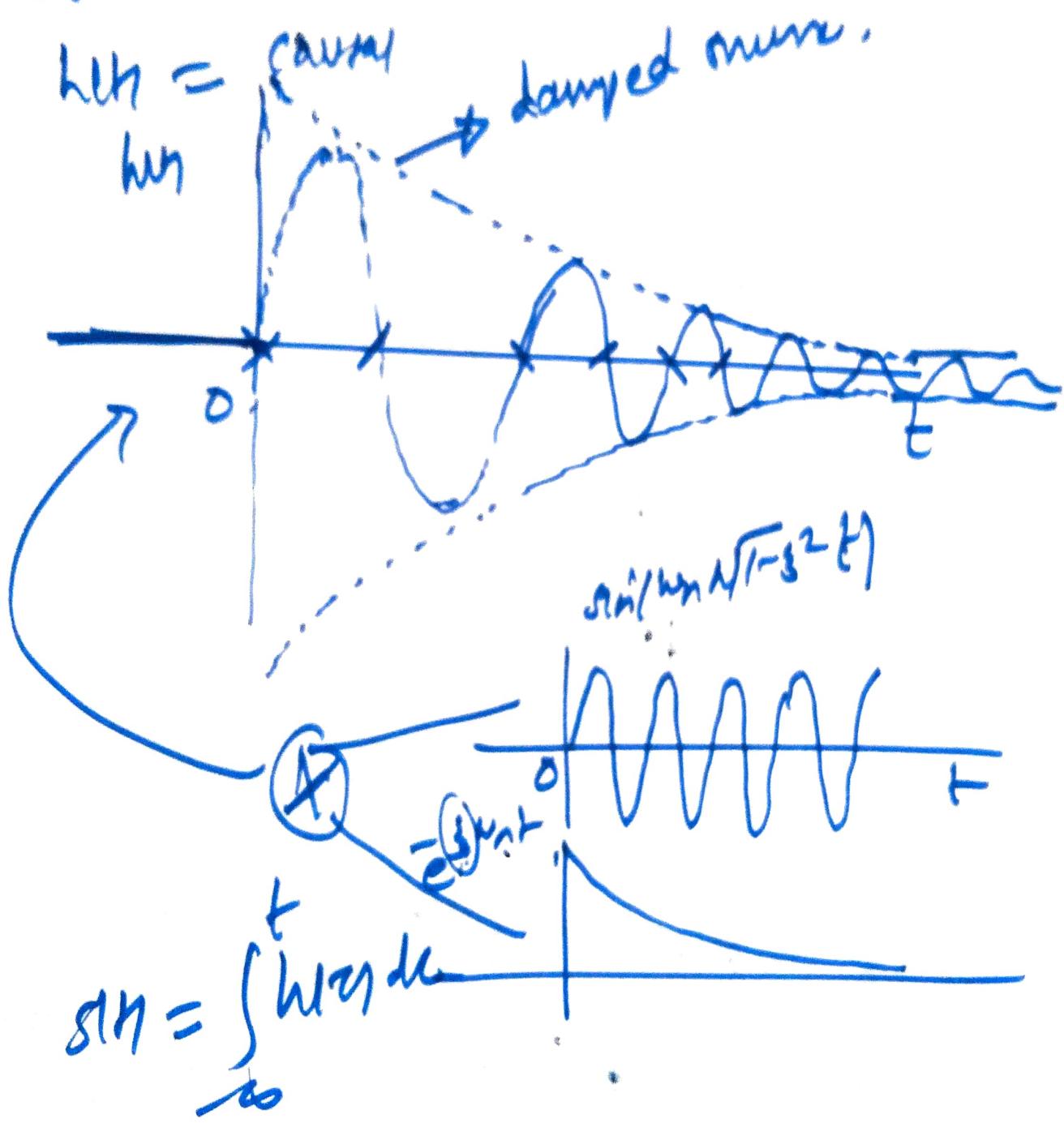
$$= A \underbrace{\left[ \frac{e^{(j\omega_n t + j\ln N\sqrt{s^2})t}}{e^{-j\omega_n t}} \cdot \frac{(-j\omega_n - j\ln N\sqrt{s^2})}{2j} \right]}_{u_h}$$

$$= \frac{e^{-j\omega_n t}}{2j} \cdot A(j) \left( \frac{e^{j\ln N\sqrt{s^2}t} - e^{-j\ln N\sqrt{s^2}t}}{2j} \right)$$

$$hH = \left( \frac{w_n}{\sqrt{1-\xi^2}} \right) e^{-\xi w_n t} \cdot x \sin(w_n \sqrt{1-\xi^2} t)$$

*constant*

(2j). A1



① ②

~~- frequency content of LRC circuit analysis~~

(1) LRC circuit

- ② LRC damped oscillation.
- ③ Resonance in LRC are due to or because frequency of source

$$\omega = \omega_n \sqrt{1-\xi^2}$$

$$x_n(\omega t) = \sin[\omega_n \sqrt{1-\xi^2} \cdot t]$$

If  $\xi = 0 \rightarrow$  i.e., No damping

$$\omega = \omega_n \sqrt{1-0/2} \Rightarrow$$

$\omega = \omega_n =$  undamped natural  
frequency of system

# Bode Plot

$$H(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n j\omega + \omega_n^2}$$

$$|H(j\omega)|^2 = \frac{|\omega_n|^2}{|(j\omega)^2 + 2\zeta\omega_n j\omega + \omega_n^2|^2}$$

$$\log_{10}|H(j\omega)|^2 = \log_{10} [ \dots ]$$

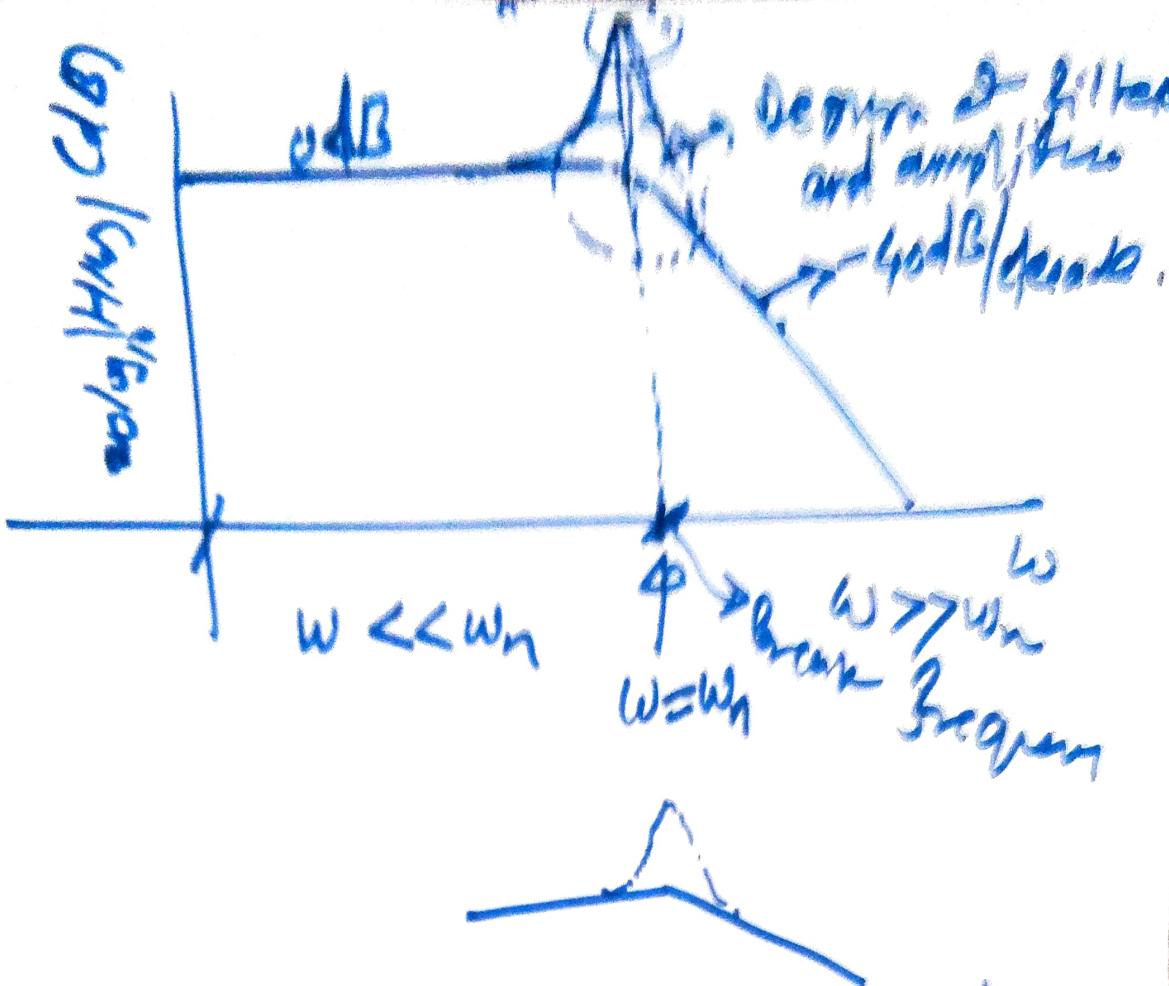
$$= \frac{(1)}{\left[ \left( 1 - \frac{\omega^2}{\omega_n^2} \right) + j 2\zeta \left( \frac{\omega}{\omega_n} \right)^2 \right]}$$

$$= 0 - j 2\zeta \log_{10} \left[ \left[ 1 - \left( \frac{\omega}{\omega_n} \right)^2 \right]^2 + 4\zeta^2 \left( \frac{\omega}{\omega_n} \right)^2 \right]$$

$$y = \begin{cases} 0 \text{ dB} & \omega \ll \omega_n \\ -40 \log(\omega) + 40 \log(\omega_n) & \omega > \omega_n \end{cases}$$

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$m = -40 \text{ dB/decade}$



Imp Note: The fact that a peak in Bode plot for 2nd order system is downed at  $w=w_n$ . This fact is used to design filters and Regency selective amplifiers.

$$20 \log_{10} |H(jw)| (\text{dB}) = -10 \log \left\{ \frac{\left[ 1 - \left( \frac{w}{w_n} \right)^2 \right]^2 + 4S^2 \left( \frac{w}{w_n} \right)^2}{1} \right\}$$

$\frac{d \log f(w)}{dw} = \frac{1}{f(w_n)} \times f'(w) = 0$

$$\frac{\partial f(w)}{\partial w} = 0$$

$$\frac{\partial}{\partial \omega} \left\{ \left[ 1 - \frac{\omega}{\bar{\omega}_n} \right]^2 + 4\zeta^2 \left( \frac{\omega}{\bar{\omega}_n} \right)^2 \right\} = 0$$

$$2 \left[ 1 - \frac{\omega^2}{\bar{\omega}_n^2} \right] \times \left( 0 - \frac{2\omega}{\bar{\omega}_n^2} \right)$$

$$+ 4\zeta^2 \times \frac{2\omega}{\bar{\omega}_n^2} = 0$$

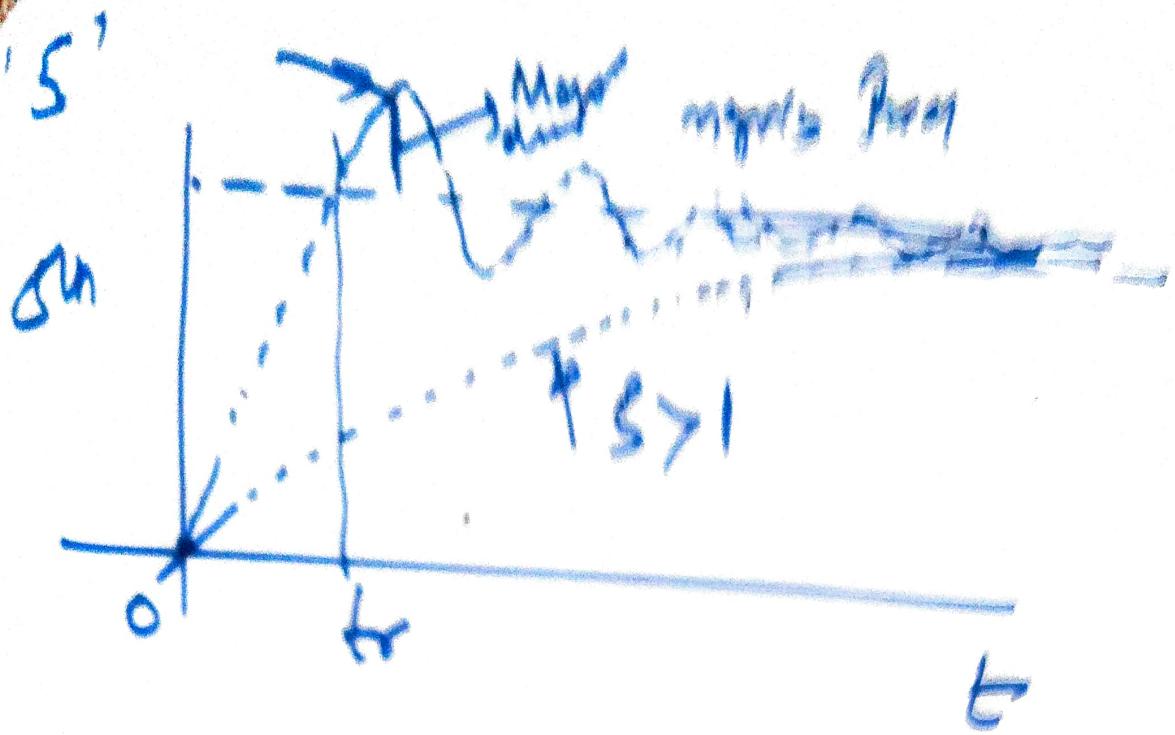
$$\boxed{\omega_{max} = \bar{\omega}_n \sqrt{1 - 2\zeta^2}}$$

$\zeta < 1 \rightarrow$  the system has damped oscillatory behavior.  
 $\zeta = 1 \rightarrow$  underdamped

$$\zeta = 1 \rightarrow c_1 \mp c_2 \Rightarrow \text{critically damped}$$

$\zeta > 1 \rightarrow$  overdamped

(16)



(17)