

Q. Justification for the term Group Delay find out why $D(\omega) = -\frac{d[\text{Re } H(\omega)]}{d\omega}$ is called group delay ??

Problem: → consider the impulse response of an all-pass system with a group delay that varies with frequency. The frequency response $H(\omega)$ [or $H(j\omega)$] for this problem is the product of three factors.

$$H(\omega) = \prod_{i=1}^3 H_i(\omega) = H_1(\omega) \cdot H_2(\omega) \cdot H_3(\omega)$$

where

$$H_i(\omega) = \text{all-pass characteristic} = \frac{\alpha_i + j\beta_i}{\alpha_i - j\beta_i}$$

$$H_i(\omega) = \frac{1 + \left(\frac{j\omega}{\omega_i}\right)^2 - 2j\zeta_i(\omega/\omega_i)}{1 + \left(\frac{j\omega}{\omega_i}\right)^2 + 2j\zeta_i(\omega/\omega_i)}$$

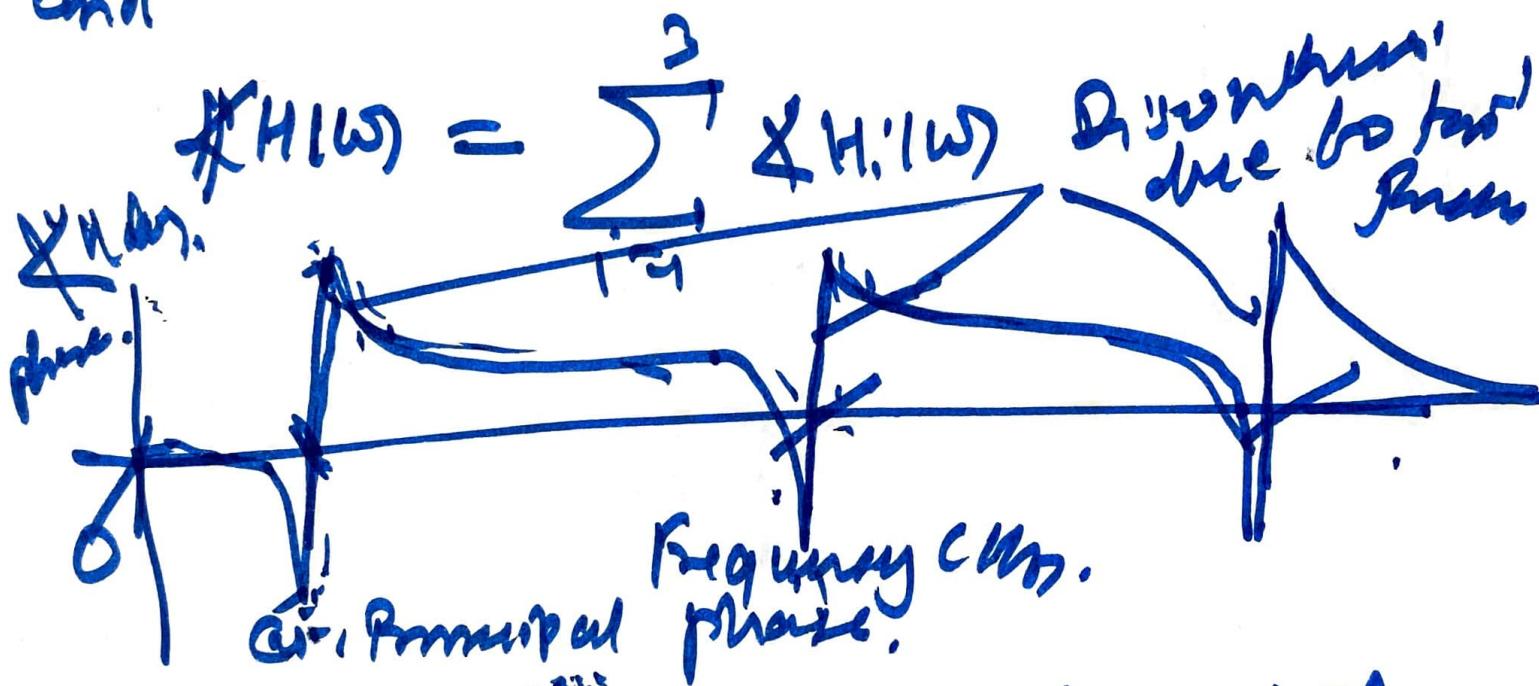
$$\omega_i = 2\pi f_i, \quad f_1 \approx 50 \text{ Hz}, \quad f_2 \approx 150 \text{ Hz}, \quad f_3 \approx 300 \text{ Hz}$$

$$|H_i(\omega)| = 1$$

The phase for each $H_i(\omega)$ can be determined as

$$\chi_{H_i(\omega)} = -2\text{tg}^{-1} \left(\frac{2\zeta_i(\omega/\omega_i)}{1 - (\omega/\omega_i)^2} \right)$$

and



$$\tan^{-1} \left(\frac{2\zeta_i + \omega}{1 - \omega^2/\omega_i^2} \right) = \tan^{-1} \left(\frac{2\zeta_i + \omega}{1 - \omega^2/\omega_i^2} \right) \\ = \tan^{-1} (2\zeta_i \omega + \omega) = \tan^{-1} (\omega)$$

Phase wrapping.

It creates discontinuity in phase.

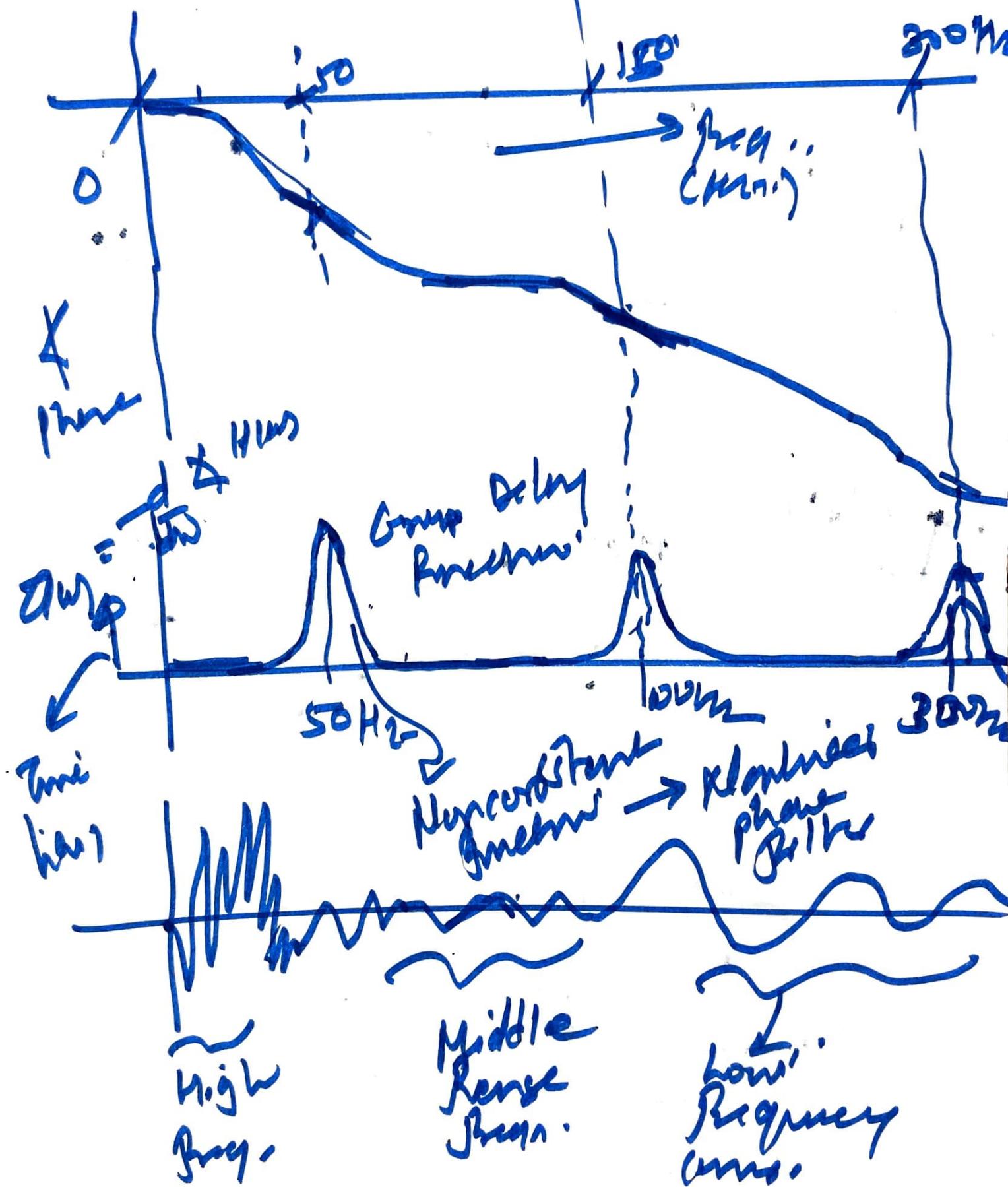
Problem: $\frac{d}{d\omega} \chi_{H(\omega)}$; is not possible

$$\therefore \Delta\omega = \frac{d}{d\omega} \chi_{H(\omega)}$$

(2)

to evaluate
at discontinuity

∴ Me medium phase unwrapping.



③

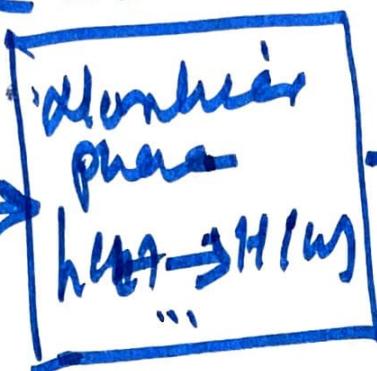
~~Meaning of the term Group Delay.~~

~~group = speed~~

$$w(t) = \sum h_n e^{j\omega_n t}$$

$$\Delta h_n$$

$$w(t) \rightarrow$$



$$y(t) = \sum h_n e^{j\omega_n t}$$

$$\Delta h_n$$

$$\Delta h_n$$

$$5 \text{ ms}$$

$$2$$

$$X(H(\omega))$$

phase

$$\int h_n d\omega = 1$$

$$\phi$$

$$10^\circ \dots$$

up to $\omega/2\pi$

$$35^\circ$$

$$50\text{Hz}$$

$$150\text{Hz}$$

$$300\text{Hz}$$

\Rightarrow Prime contains all the freq. components

$$= \sum h_n e^{j\omega_n t}$$

$$F_C \rightarrow$$

$$\omega_2$$

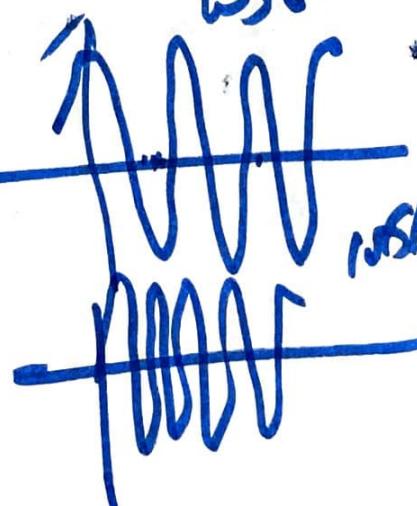
$$\omega_1$$

$$-\omega_1$$

$$0$$

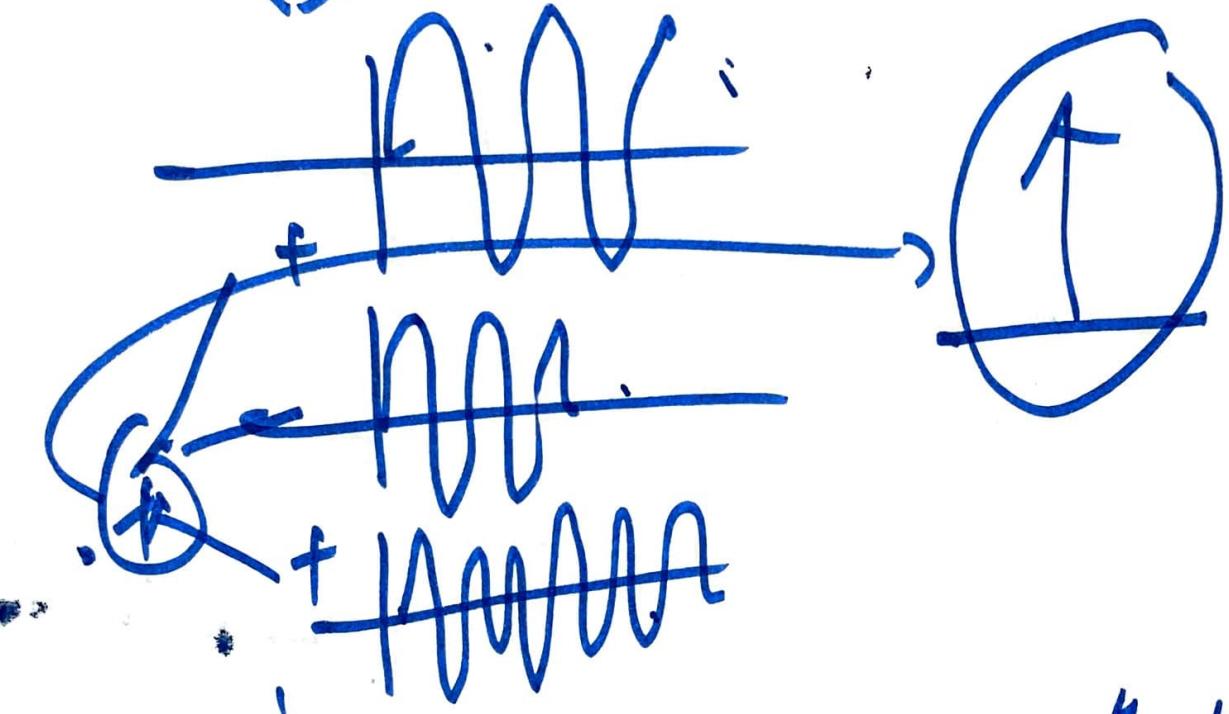
$$-\omega_2$$

frequency (Hz),
 $\cos(\omega t)$



4

$$f(t) \cong \sum_{n=1}^{\infty} \cos(\omega_n t)$$

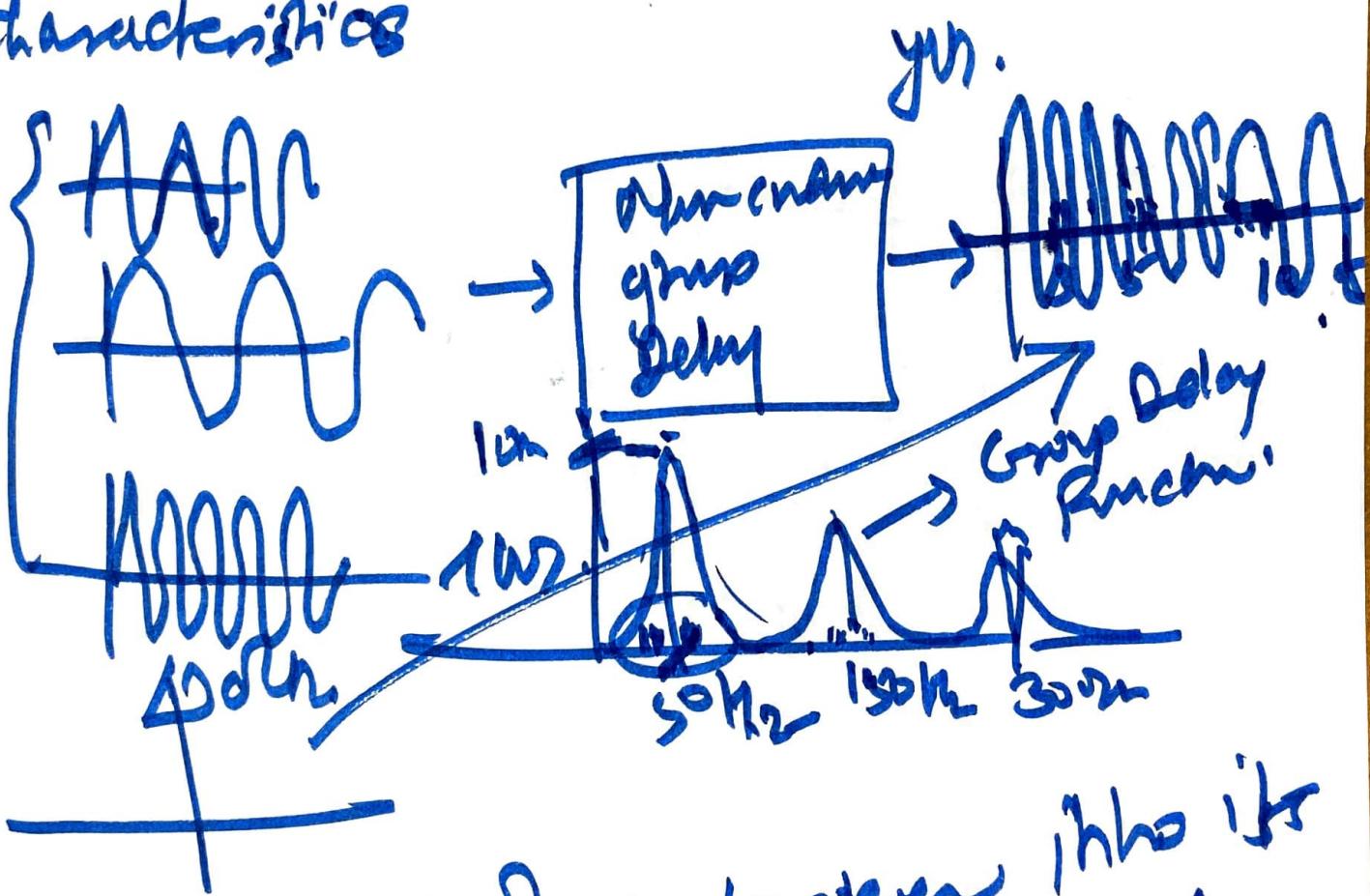


Therefore $f(t)$ is such a signal that it is formed by adder's midline number sinusoides & infinitesimal small frequencies.

∴ When an impulse is passed through a linear phase filter then the output signal is $y(t) = f(t - \tau)$ i.e. all the midline must be experience the same amount of delay equal to the slope of phase function of the R.F. i.e. all the sinusoids in $f(t)$ will be in a subtracting

that they form the impulse at a delay of 5 seconds.

On the other hand, if we pass the same impulse, $\delta(t)$ through a filter having nonlinear phase characteristics



\therefore In [Figure] is broken into its different arrivals appearing at different locations (determined by nonlinearity of group delay pulse). This phenomenon is called as pulse dispersion.

* Applications of Group Delay Function.
EWS.

1) Telecommunication Networks.

EWS is used to assess quality
of telecommunication transmission
(characteristics). → Bell Labs, USA.

PP. 435

2) Speech Technology

(Design of Vocoder → Prof. Meioliki
Kurokawa,
Japan.

3) EWS is used as feature set for
speech and speaker recognition,
anti-spouting algorithms in voice
biometrics,

4) Detection of Normal vs. Whined
speech
↳ American has a Patent
↳ Voice Assistant

⑥ TWS is to perform speech segmentation at syllable-level

$$\overline{\text{cpT}|\text{cpT}} = \overline{\text{cpT}} + \overline{\text{cpT}}$$

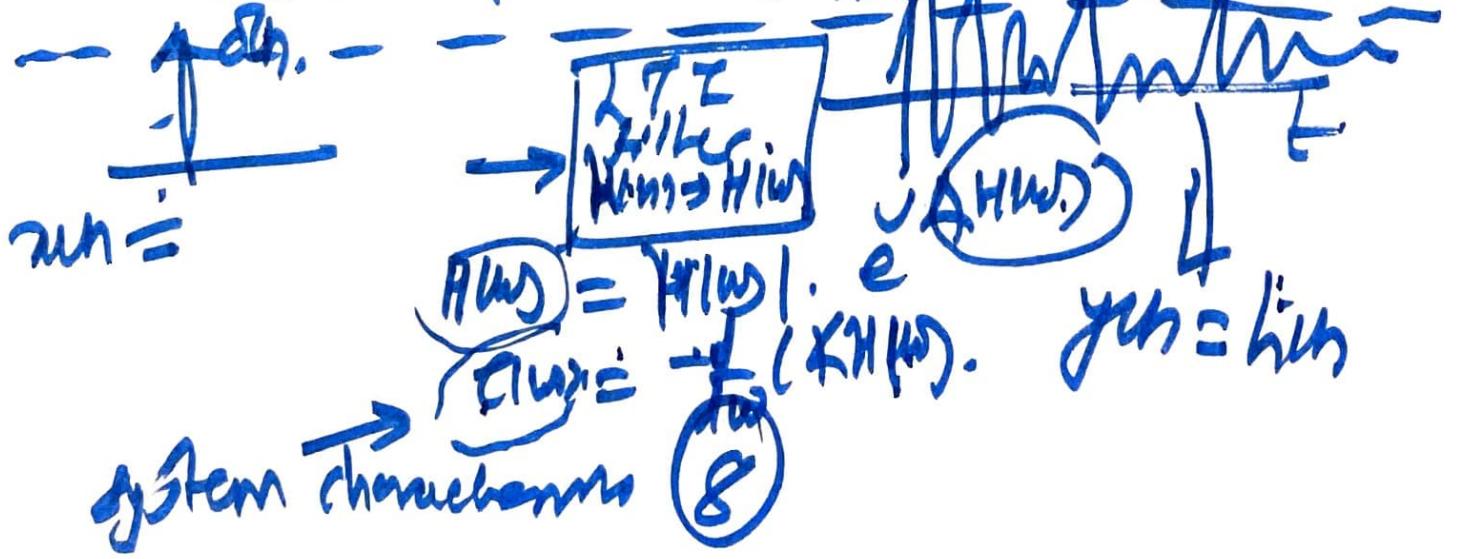
$\xrightarrow{\text{syllable}}$

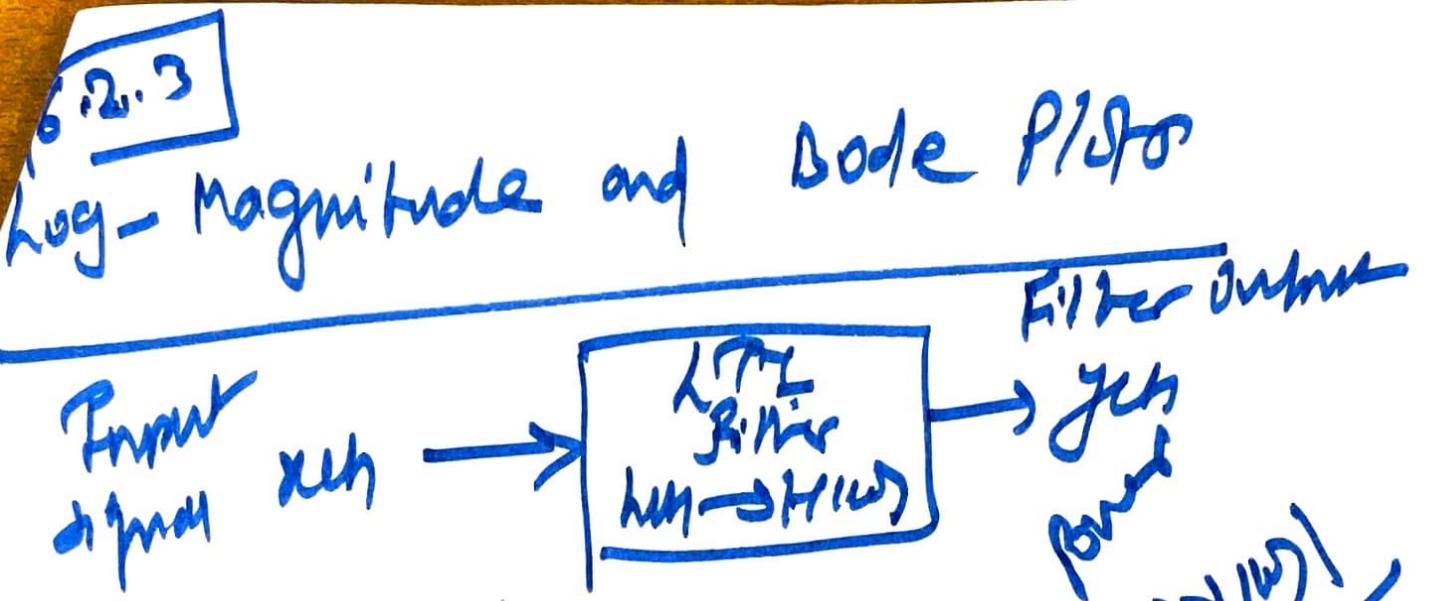
(TWS)-

⑦ TWS is ~~not~~ noise-robust

[Autocorrelation Function: $R_{xx}(\tau)$
is also noise-robust]

⑧ TWS has good spectral resolution. \Rightarrow good capability to resolve spectral peaks in Frequency-domain.

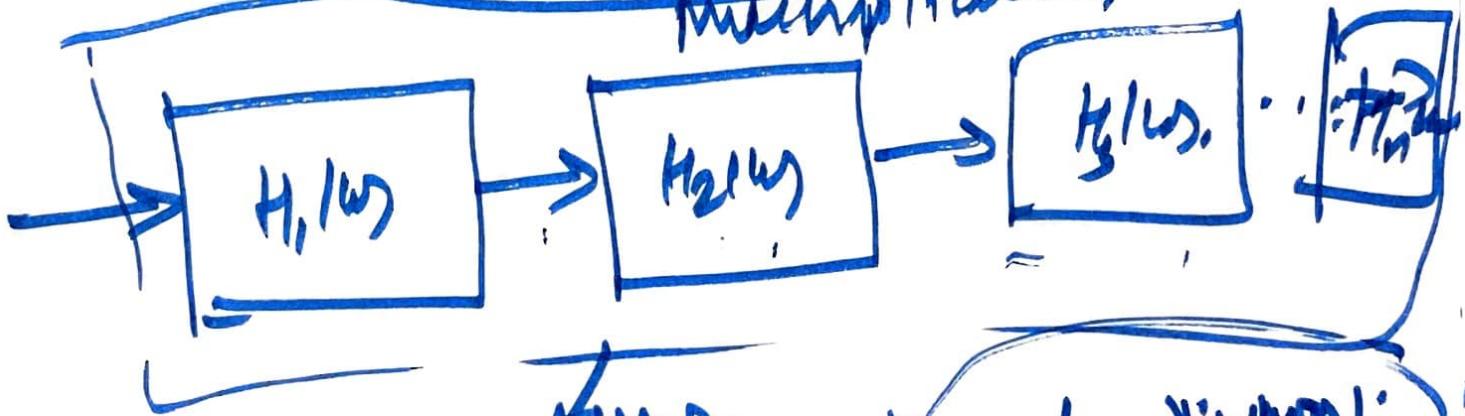




$$\therefore y(j\omega) = X(j\omega) \cdot H(j\omega)$$

$|y(j\omega)| = |X(j\omega)| \cdot |H(j\omega)|$

Multiplication



$$\log_{10} |y(j\omega)| = \log_{10} |H(j\omega)| + \log_{10} |X(j\omega)|$$

$\log_{10} |H(j\omega)|$ $\frac{|H(j\omega)|^2}{|X(j\omega)|^2} = \frac{A(j\omega)^2}{|X(j\omega)|^2}$

①

Power ratio Φ $\frac{A(j\omega)^2}{|X(j\omega)|^2}$ = $\frac{\text{Output power}}{\text{Input power}}$

$$\text{decibel} = 20 \log_{10} |H(\omega)|^2 \text{ dB}$$

Cascade of ten LTI systems.

In the humor inventor of Telephone
Bell Labs \Rightarrow Alexander Graham Bell

$$20 \log_{10} |H(\omega)| = 0 \text{ dB}$$

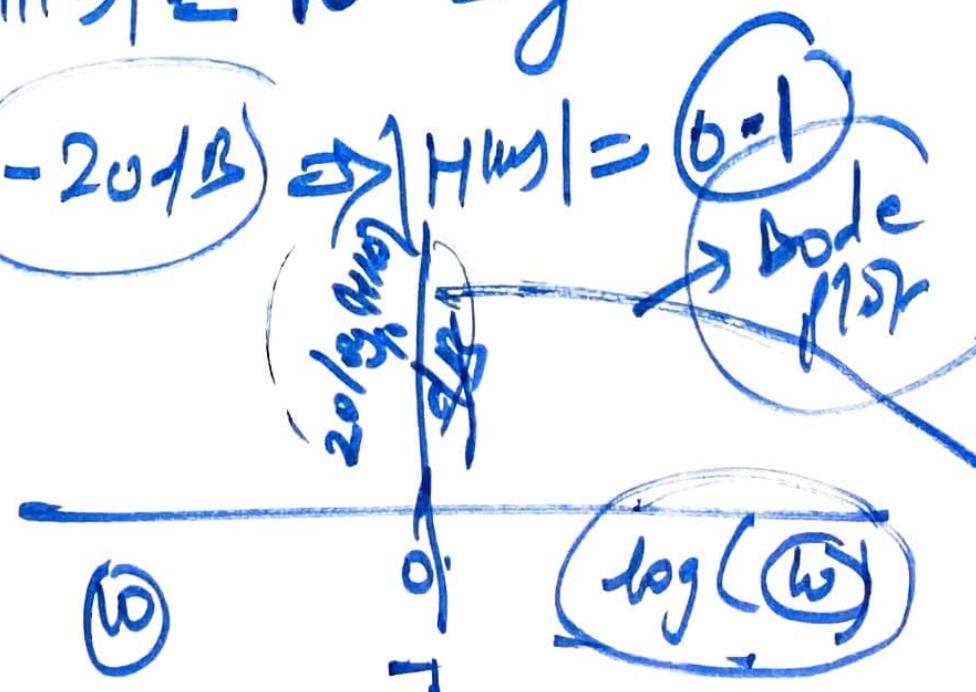
\rightarrow LTI filter has
 magnitude spectrum =

$$20 \log_{10} |H(\omega)| = 20 \text{ dB.}$$

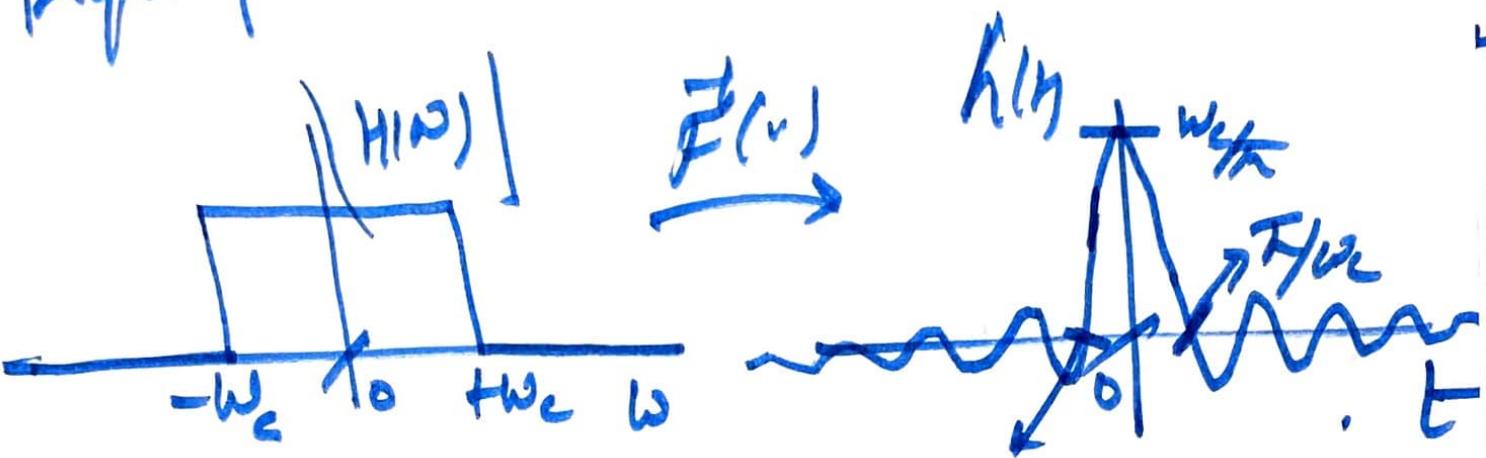
$$\Rightarrow |H(\omega)| = 10 = \text{gain}$$

$$20 \log_{10} |H(\omega)| = -20 \text{ dB} \Rightarrow |H(\omega)| = 0.1$$

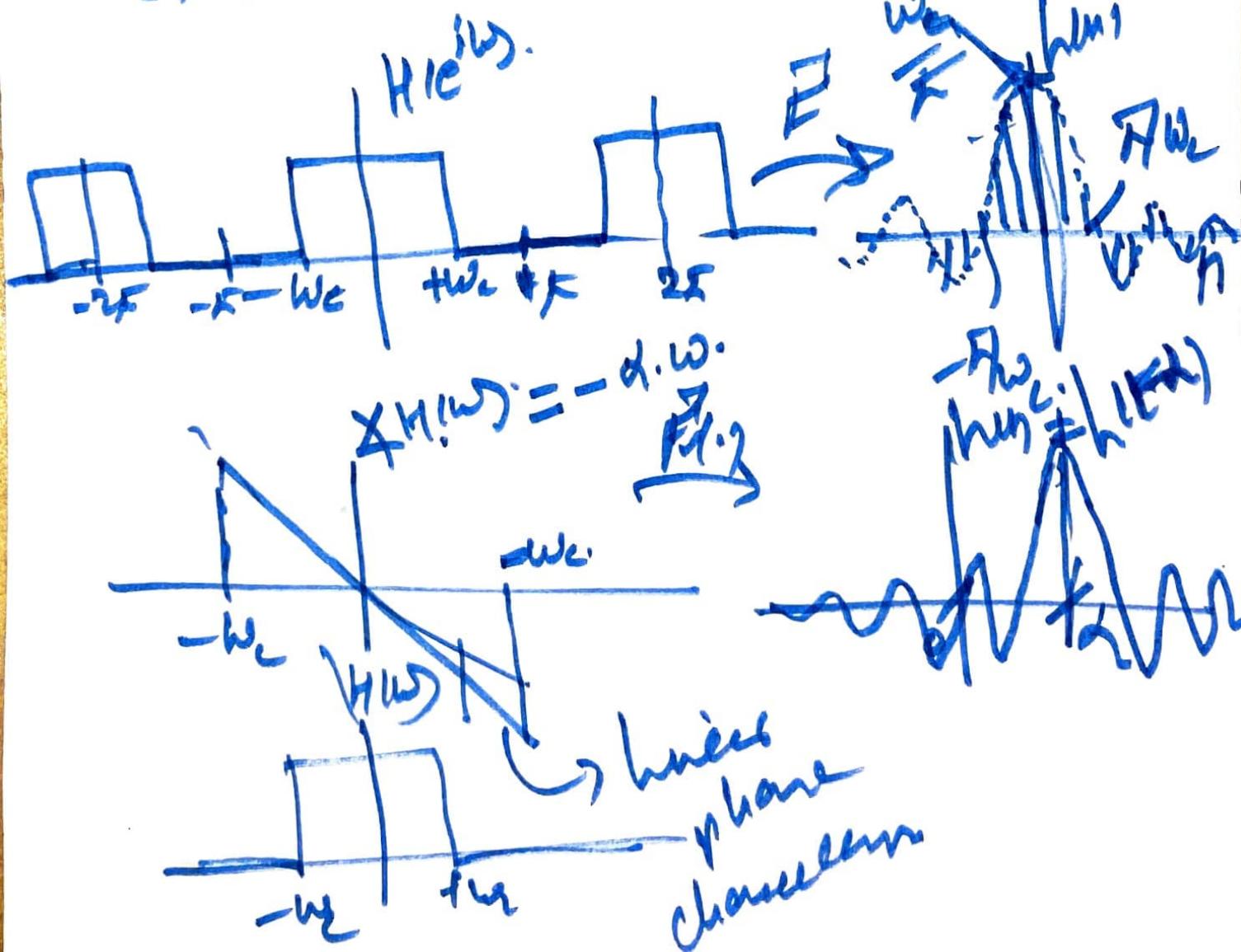
CTP
 openodic
 in frequency



3 Time domain Properties of Ideal Frequency selective filters.



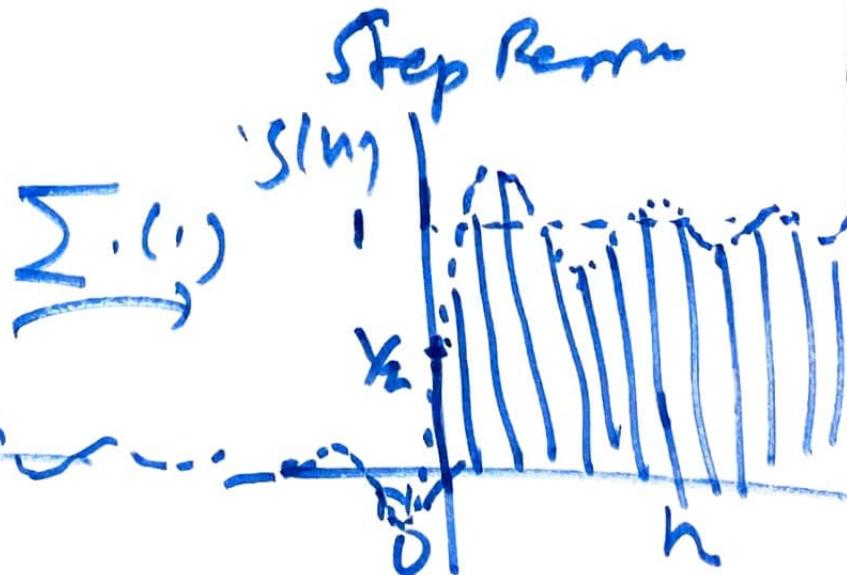
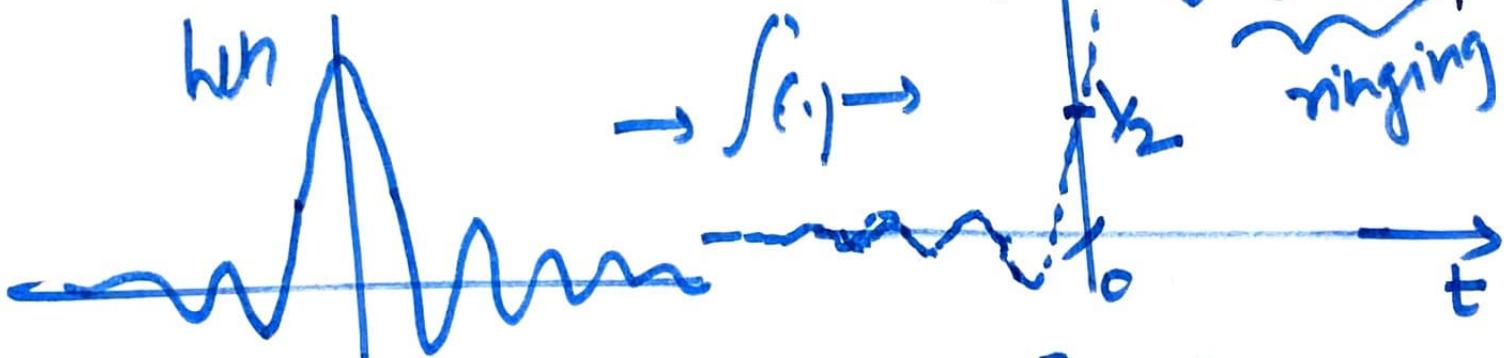
(a) Ideal LPF [continuous-time]



Step Response of the LTI Filter

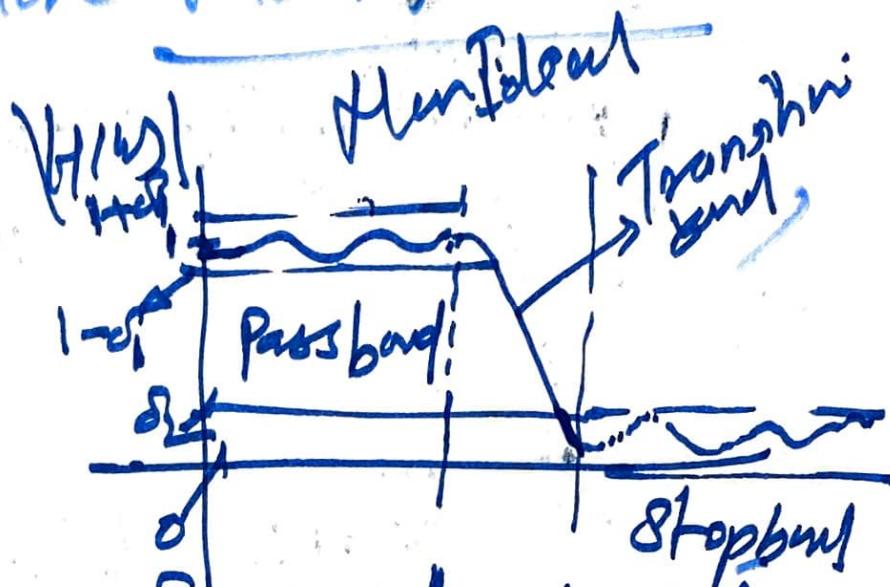
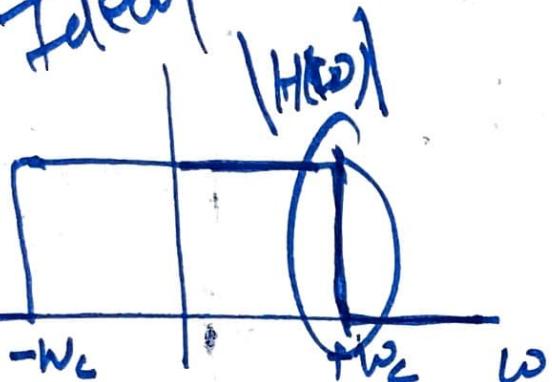
$$S(t) = \int_{-\infty}^t h(\tau) d\tau$$

$$S(n) = \sum_{k=-\infty}^{n-1} h(k)$$



4] Time-domain and Frequency-Domain Aspects of Non-Ideal Filters.

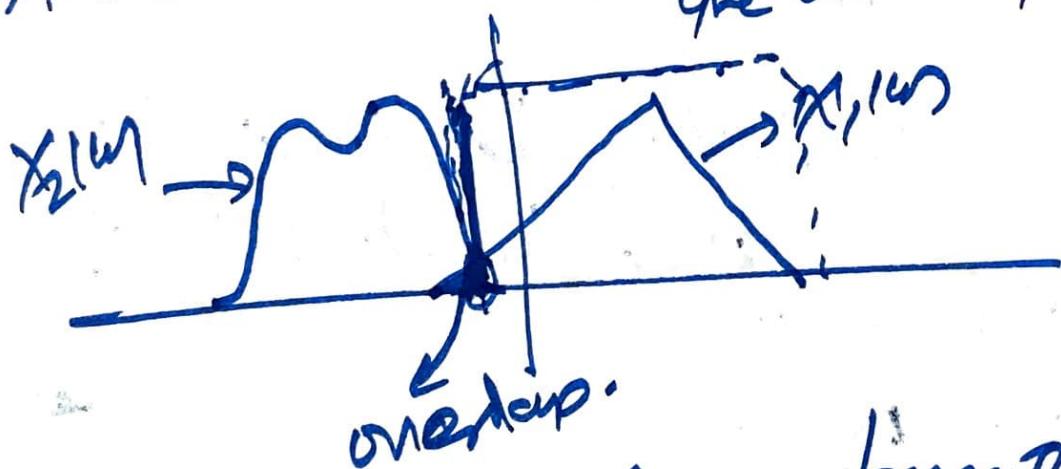
Ideal



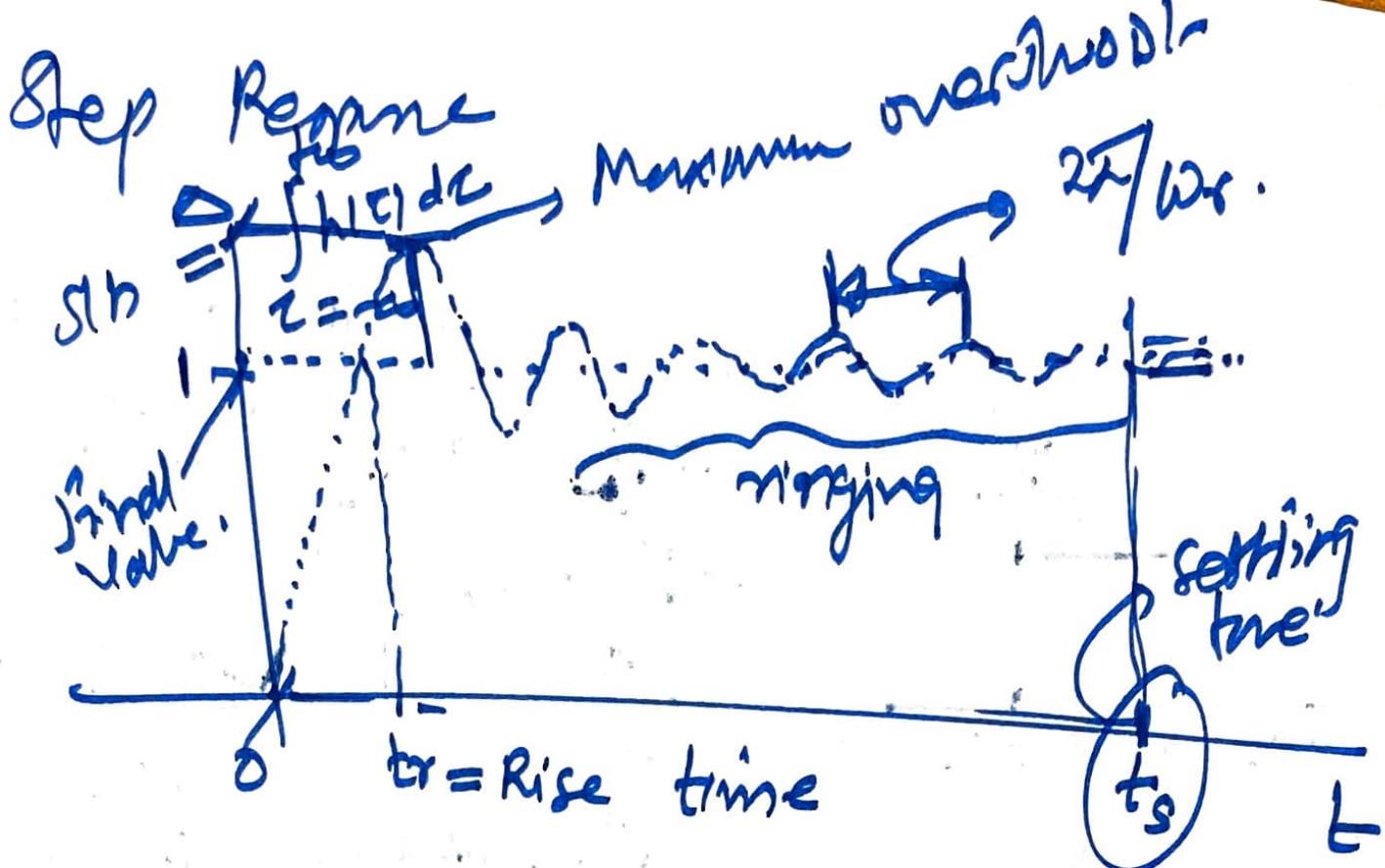
Ideal

$$x_{in} = \tilde{x}_1(\omega) + \tilde{x}_2(\omega)$$

$$x_{in} = x_1(\omega) + x_2(\omega) \rightarrow x_1(\omega) \text{ & } x_2(\omega) \text{ are overlapping spectra}$$



To achieve sharp transition band, we need large cascade pulse & electric components R , i.e. of resistors, multipliers, and adders. \Rightarrow very costly



1) Rise time (t_r) \Rightarrow the interval over which the step response of the filter rises towards its final value

2) Ringing \rightarrow oscillatory behavior of step response after t_r .
If ringing is present.

3) Overshoot (Δ) \rightarrow

4) Ringing frequency (ω_r)

5) Settling time (t_s) \Rightarrow time required for the step response to settle down within a specified tolerance of its final value.