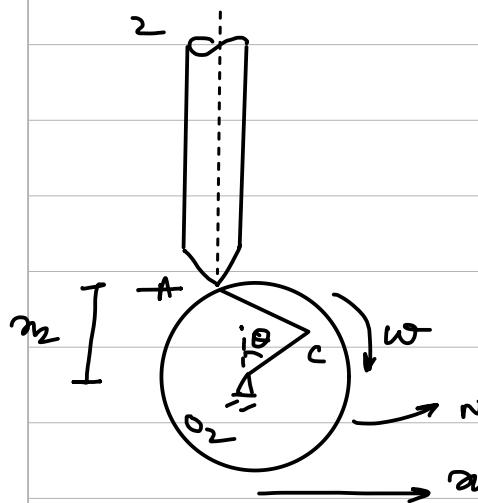


17th Feb.

CIRCULAR DISC & KNIFE EDGE



$$AC = a$$

$$O_2C = e$$

$$\cos \theta = \frac{r^2 + e^2 - a^2}{2re}$$

Need not be perfect circle

$$r^2 - (2e \cos \theta)r + (e^2 - a^2) = 0$$

$$r = e \cos \theta \pm \sqrt{e^2 \cos^2 \theta - (e^2 - a^2)}$$

$$r = e \cos \theta + \sqrt{a^2 - e^2 \cos^2 \theta}$$

take root such that, $\theta = 0^\circ$, $r = a$

$$V = \frac{dr}{dt} \quad a = \frac{d^2r}{dt^2}$$

$$V = \omega \cdot \frac{dr}{d\theta}$$

$$= \omega \cdot \left[-e \sin \theta - \frac{e^2 \cos \theta \sin \theta \cos \theta}{2 \sqrt{a^2 - e^2 \sin^2 \theta}} \right]$$

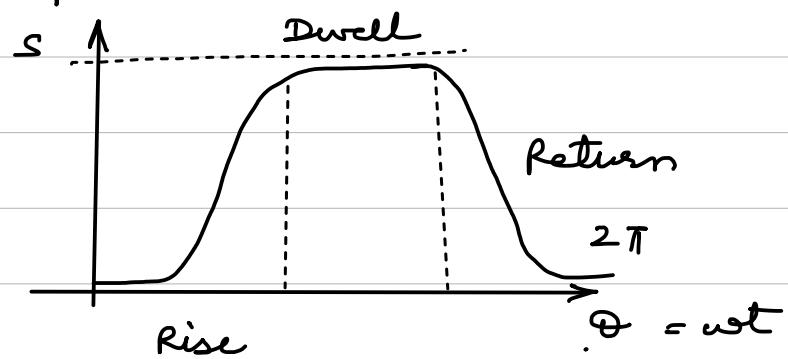
$$= -\omega e \sin \theta$$

$$= \left[1 + \frac{e \cos \theta}{\sqrt{a^2 - e^2 \sin^2 \theta}} \right]$$

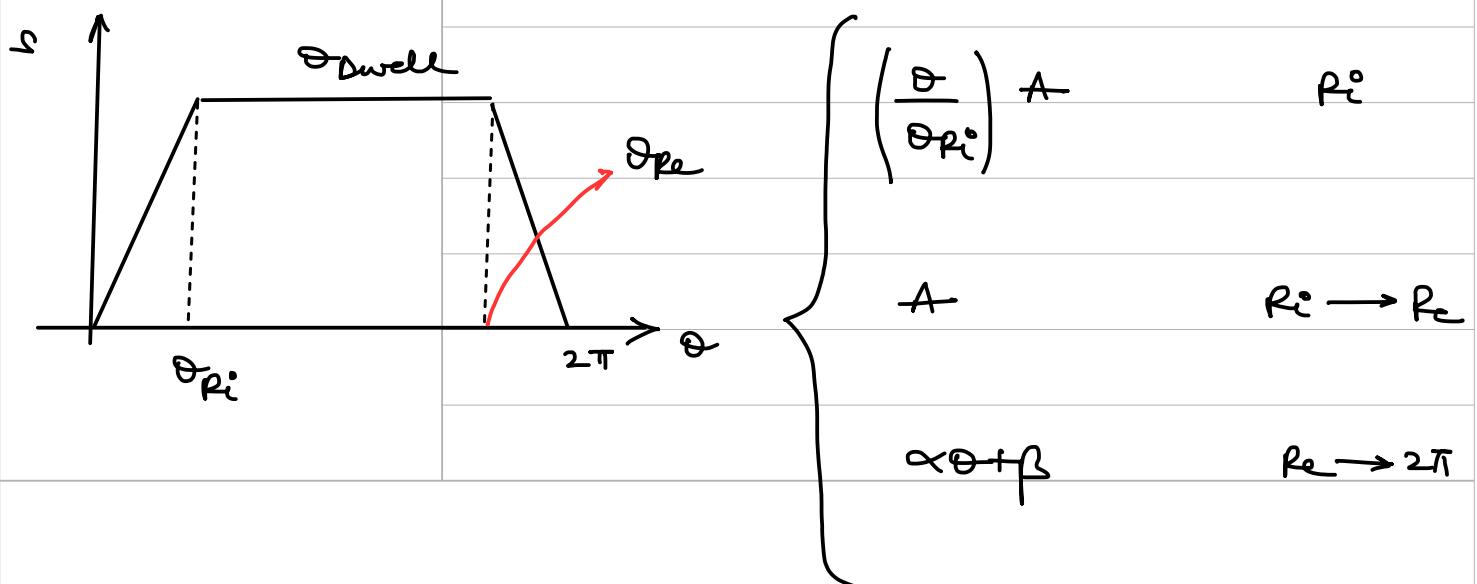
Similarly, $a =$

No control on the resulting velocities and acceleration. High values of v and a can lead to noise and vibration.

In the context of translating follower, usually the displacement (s), can be expressed as,

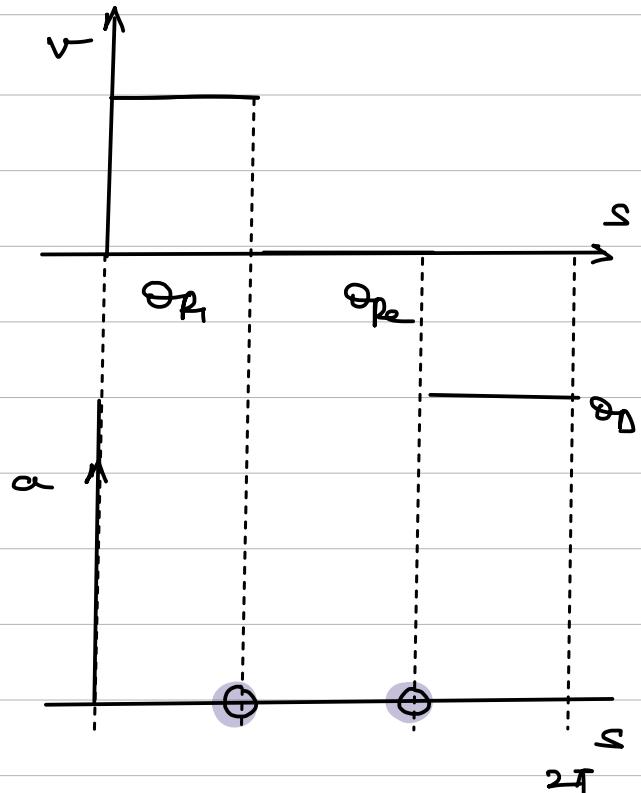


To model it, I can



ASG ✓ DNIZI ✓

$$v_{pi} = \frac{\omega A}{\theta_{pi}}$$



Higher Order Polynomials or Trig.

$$s = A \left[\frac{\theta}{\theta_{pi}} - \frac{1}{2\pi} \left[\sin \left(\frac{2\pi\theta}{\theta_{pi}} \right) \right] \right]$$

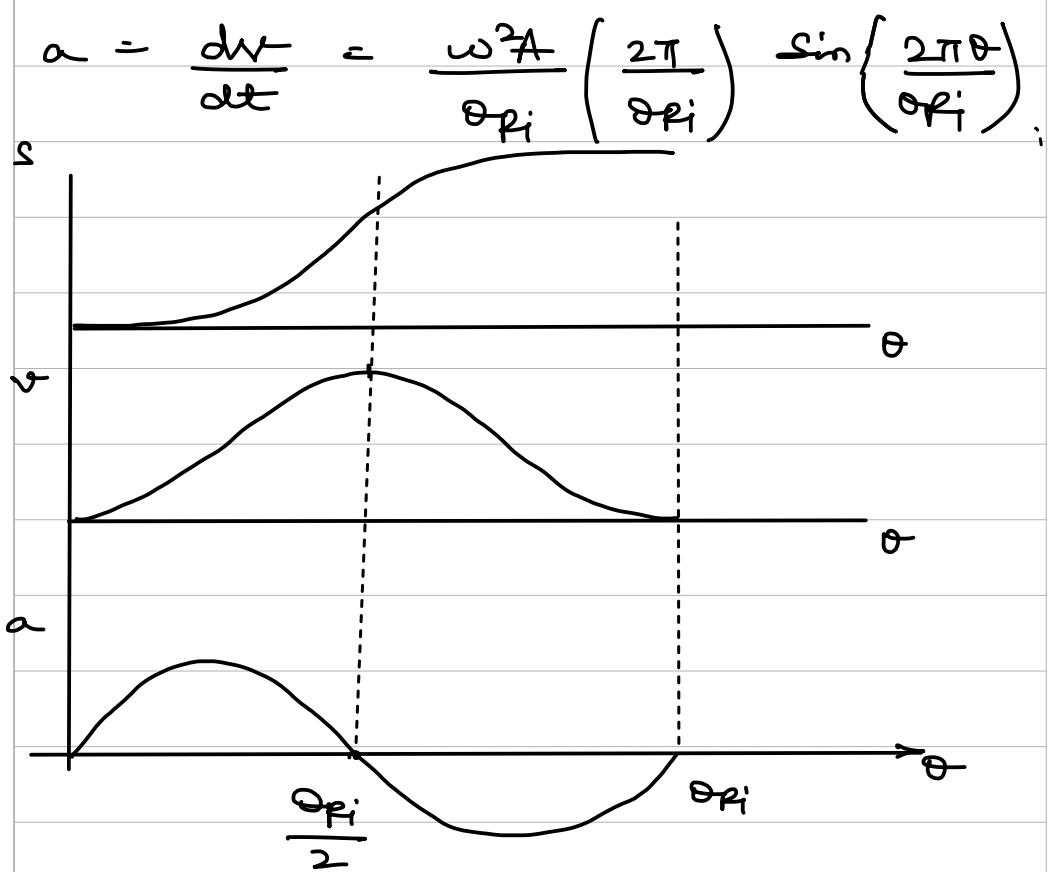
$$s(0) = 0 \quad ; \quad s(\theta_{pi}) = A$$

$$v = \frac{ds}{dt} = \frac{ds}{d\theta} \cdot \frac{d\theta}{dt} = \omega \cdot \frac{d\theta}{dt}$$

$$= A \left[\frac{1}{\theta_{pi}} - \frac{1}{2\pi} \left(\frac{2\pi}{\theta_{pi}} \right) \times \cos \left(\frac{2\pi\theta}{\theta_{pi}} \right) \right] \omega$$

$$= \frac{Aw}{\theta_{pi}} \left[1 - \cos \left(\frac{2\pi\theta}{\theta_{pi}} \right) \right]$$

Acceleration will lead to inertial forces.



Cycloidal curve ensures zero velocity and zero acceleration at the rise's rise

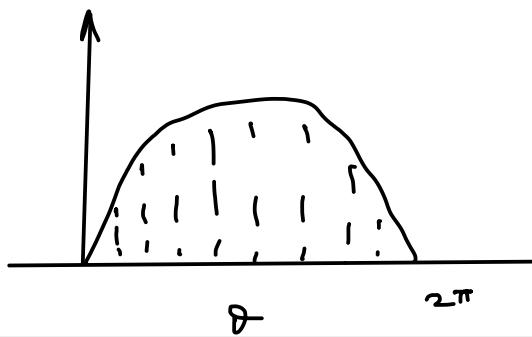
Given displacement profile, design the cam.

CAM - SYNTH.

KNIFE-EDGE translating follower
 → some displacement function:
 $s(\theta)$

$$\theta \in [0, 2\pi]$$

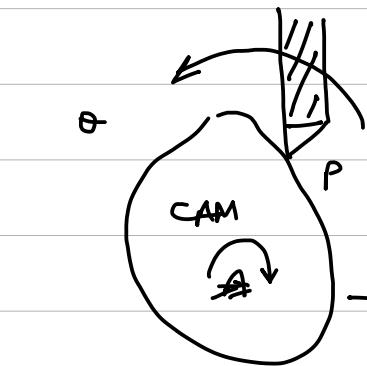
$$s(\theta) \in [s(\theta_1), s(2\pi)]$$



→ Angle of CAM

GRAPHICAL APPROACH:

No offset here.



KINEMATIC

INVERSION

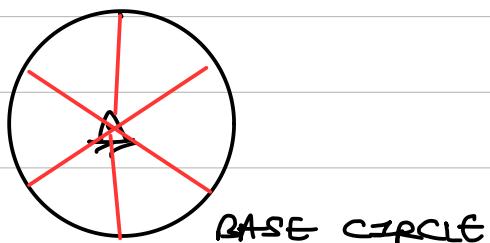


Relative motion

b/w bodies remain
same

wrt CAM → anti clockwise ground.

Follows certain
no. of points.



Part of CAM.

CAM synthesis :

Principle of Inversion.

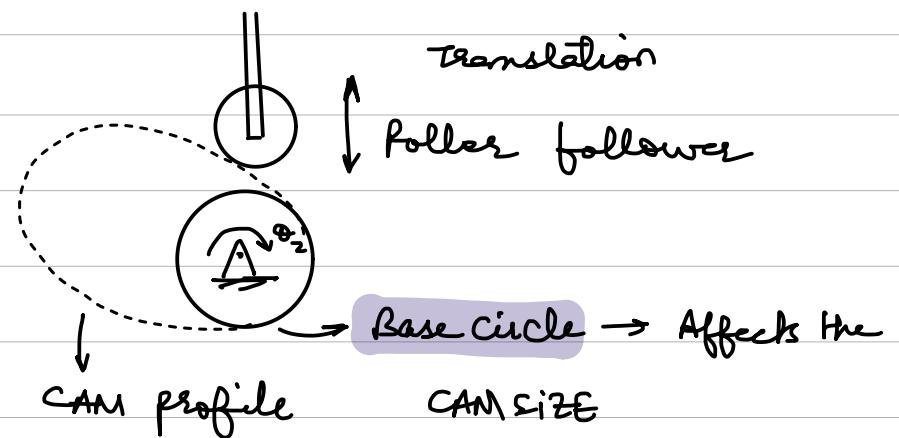
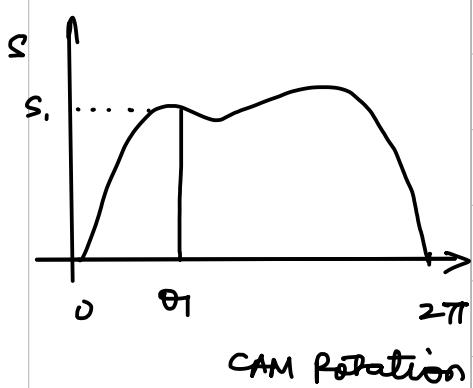
1. Translating Knife edge follower [No offset]
2. Roller follower [No offset] translating

$$S = r \left[\frac{\theta}{\omega r} - \frac{1}{2\pi} \sin\left(\frac{2\pi\theta}{\omega r}\right) \right]$$

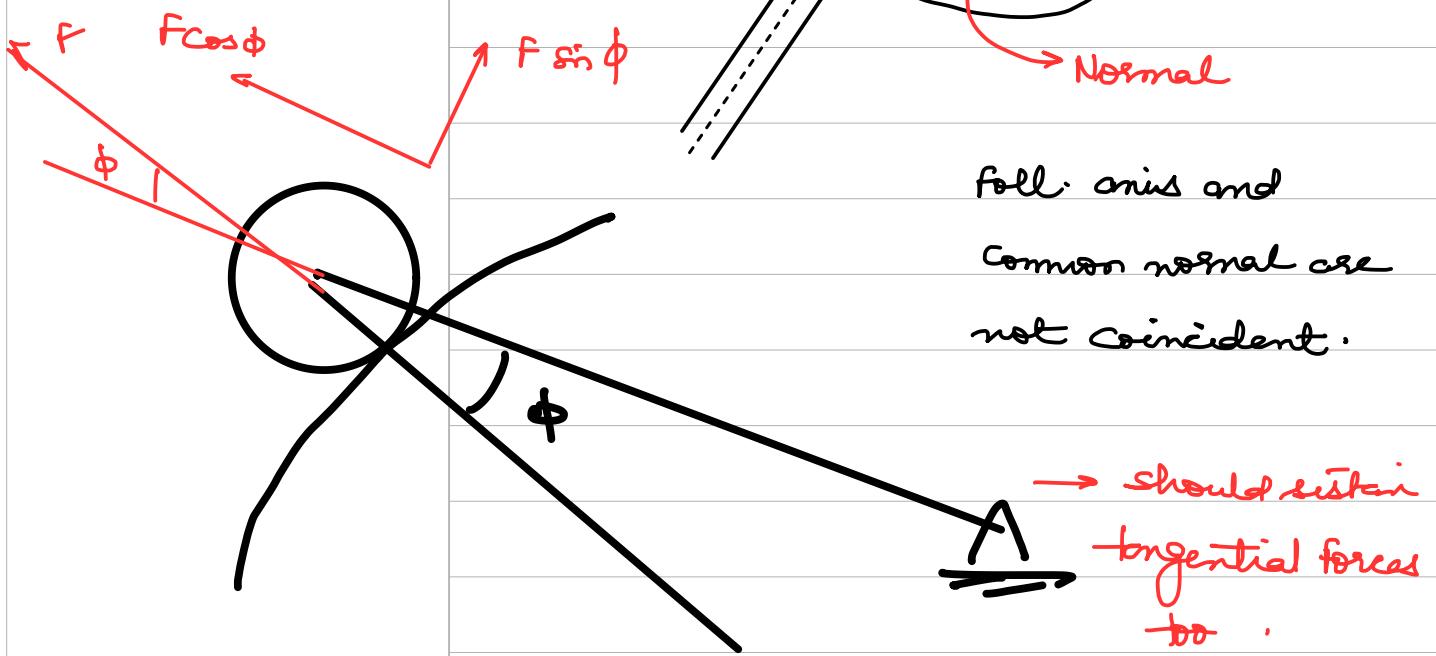
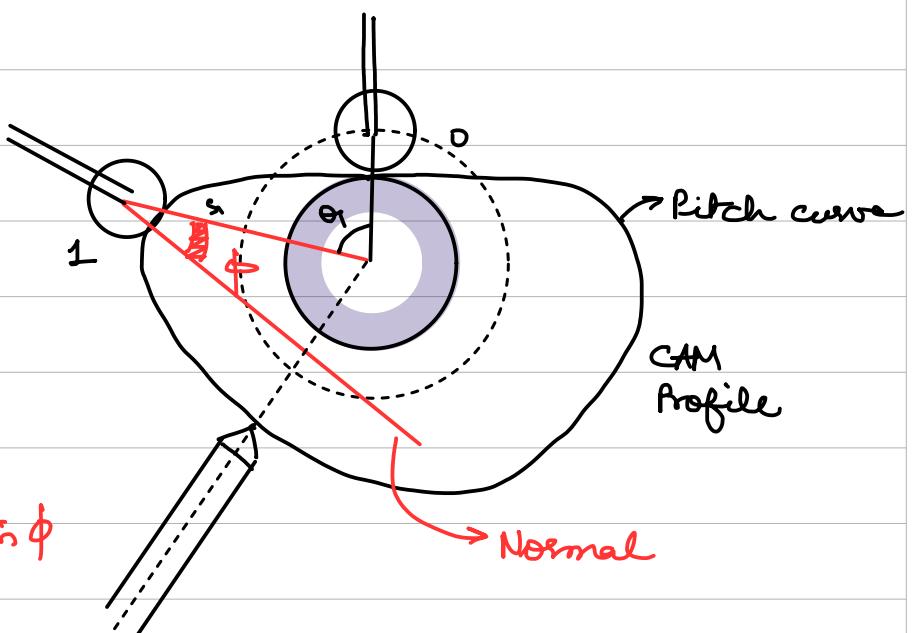


CAM rotation

How do you imply convexity?



ϕ = Pressure angle



$\rightarrow 20^\circ < \phi < 30^\circ$ for optimal working.

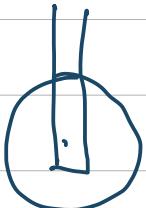
greater the value of r_b , smaller the ϕ .

This was
Pratik
Saini&Son

Woo hoo! - by Pratham Bharatara
(with disappointment in Tanmay)

Follower #2:

Roller follower

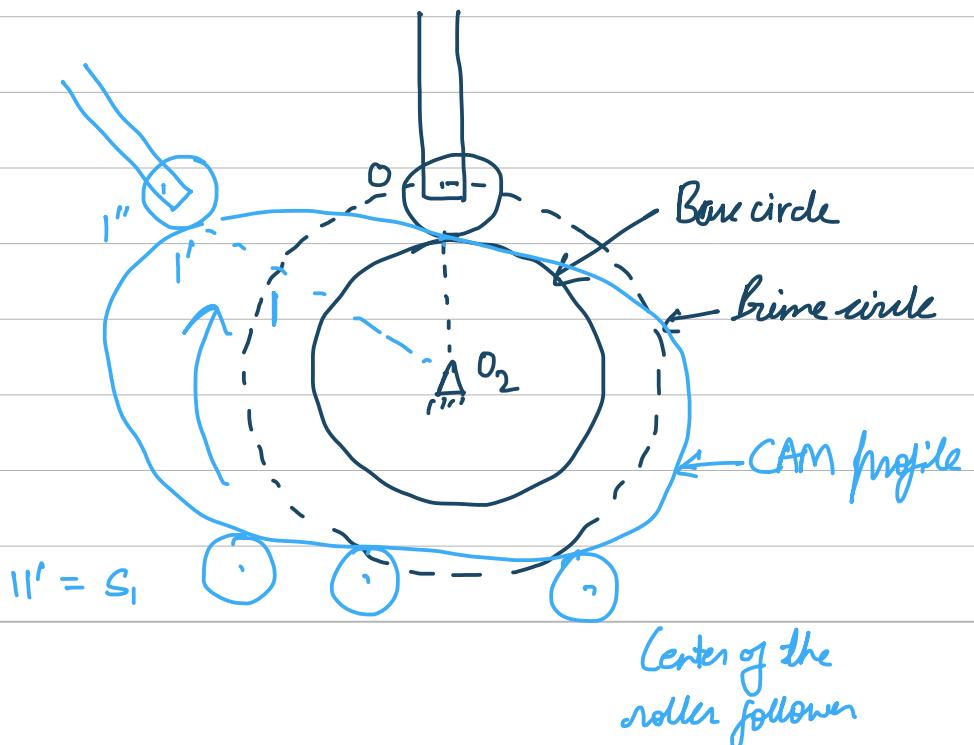


Translating and Rotating

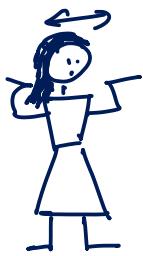
Given: Displacement profile of roller follower
To find: CAM profile

We have to assume values for radius of roller and base circle.

Assume clockwise motion



CAM profile is tangent to all the circles (roller follower) identified through process of inversion.



Wine

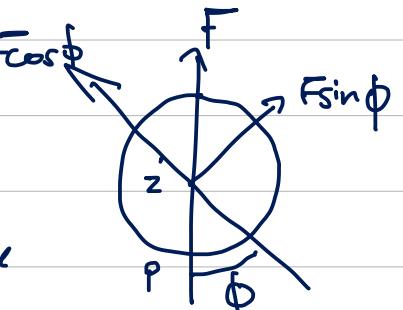
Theory of envelopes

We want to find a curve which envelopes a family of given circles.

FBD at 2

In general, the common normal at the point of contact, need not coincide with the follower axis.

The corresponding angle is called preure angle.

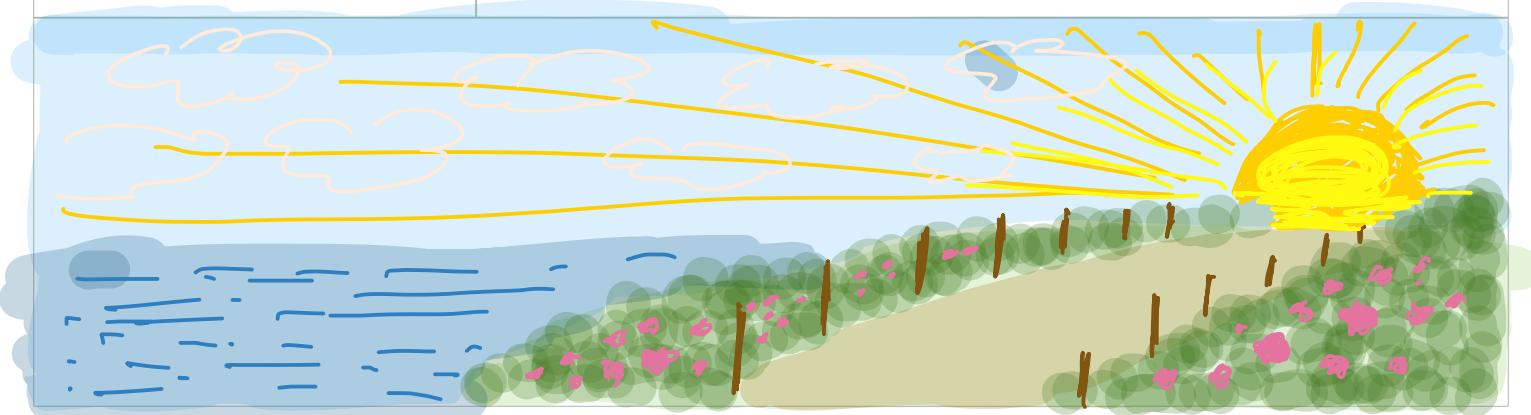
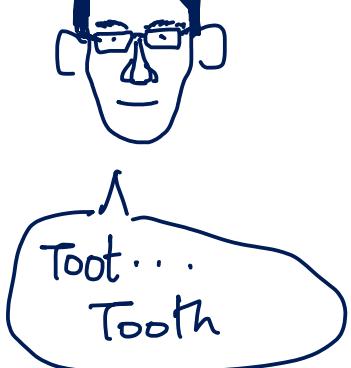


Recommended angle

$\phi \leq 20^\circ \text{ to } 30^\circ$

-

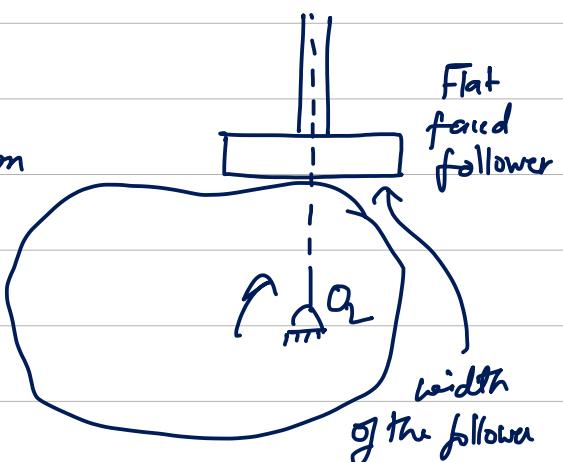
Increasing the base circle radius, will bring down the preure angle.



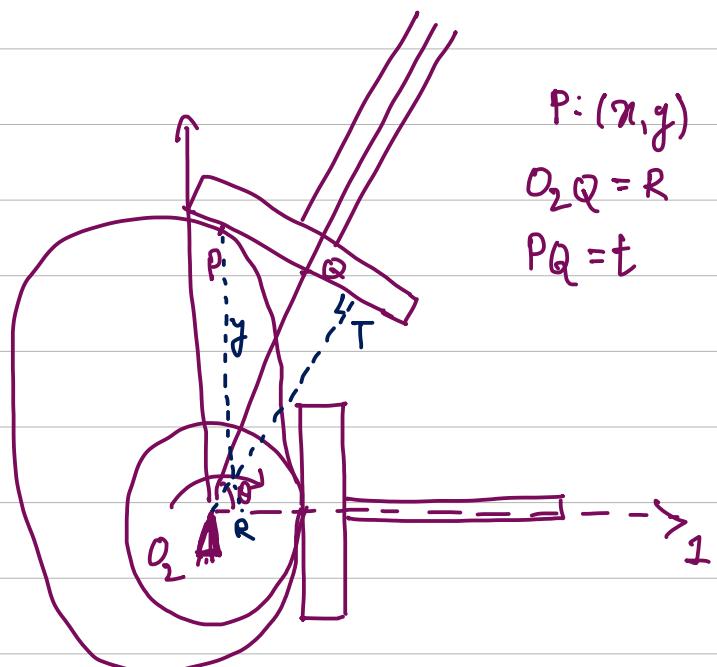
Analytical approach:

Translating flat-faced follower.

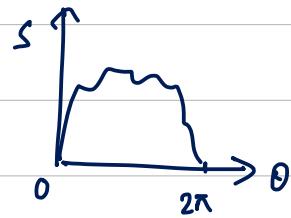
The flat line of the follower is the common tangent at the point of contacts.



The contact point P changes with the angle through which CAM rotates.



Displacement function $s = f(\theta)$



From fixed point O_2 , the radial distance of follower is

$$R(\theta) = r_b + f(\theta)$$

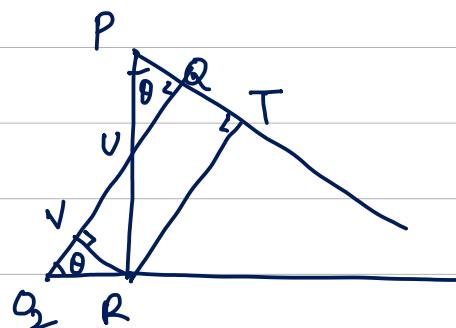
↑
Base circle radius

$$PR = y$$

$$O_2 R = \mathcal{N}$$

In ΔPRT,

$$RT = PR \sin \theta$$



$$Q_2 Q = Q_2 V + V Q$$

$$= D_2 V + RT$$

$$PQ = PT - QT$$

$$= PT - VR = PR \cos \theta - Q_R \sin \theta$$

$$t = y \cos \theta - x \sin \theta$$

Tangent to the CAM at (x, y) :

$$\left(\frac{dy}{dx} \right)_{\tan \theta}$$