

One-Way (Single Factor) ANOVA Table



■ TABLE 3.3

The Analysis of Variance Table for the Single-Factor, Fixed Effects Model

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F_0
Between treatments	$SS_{\text{Treatments}} = n \sum_{i=1}^k (\bar{y}_{i.} - \bar{y}_{..})^2$	$k - 1$	$MS_{\text{Treatments}} = \frac{SS_{\text{Treatments}}}{df}$	$F_0 = \frac{MS_{\text{Treatments}}}{MS_E}$
Error (within treatments)	$SS_E = SS_T - SS_{\text{Treatments}}$	$N - k$	MS_E	
Total	$SS_T = \sum_{i=1}^k \sum_{j=1}^n (y_{ij} - \bar{y}_{..})^2$	$N - 1$		

Compare with

$$F_{\text{crit}} = F_{1-\alpha, k-1, N-k}$$

$$F_0 > F_{\text{crit}} \rightarrow H_1 \checkmark \quad \text{other } H_0 \checkmark$$

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Example



$$y_{ij} \quad i \rightarrow 1-k \quad k=4$$

$$j \rightarrow 1-n_i$$

e.g. $y_{13} = \underline{63}$, $y_{34} = \underline{67}$

$$y_{ij} = \mu + \tau_i + \varepsilon_{ij} \quad \checkmark \quad (\text{effects model})$$

$$y_{ij} = \bar{y} + (\bar{y}_i - \bar{y}) + (y_{ij} - \bar{y}_i)$$

$$\sum \sum y_{ij}^2 = N \bar{y}^2 + \sum n_i (\bar{y}_i - \bar{y})^2 + \sum \sum (y_{ij} - \bar{y}_i)^2$$

\downarrow SS_T \downarrow SS_m \downarrow $SS_{\text{treatment}}$ \downarrow SS_{error}

$k =$

	1	2	3	4
j	Stainless Steel	Carbon Steel	Nickel Alloy	High Speed Steel
1	62	63	68	56
2	60	67	66	62
3	63	71	71	60
4	59	64	67	61
5	NaN	65	68	63
6	NaN	66	68	64
7	NaN	NaN	NaN	63
8	NaN	NaN	NaN	59

$n_1 = 4$ $n_2 = 6$ $n_3 = 6$ $n_4 = 8$

y_{ij}

j^{th} observation for i^{th} metal

Here, $i = 1, 2, 3, 4$

(4 levels of variable 'metal')

$$N = \sum n_i = 4 + 6 + 6 + 8 = 24$$

j	SS	CS	NA	HSS	
1	65	63	67	56	$\varepsilon_{ij} = 0$
2	65	63	67	50	
3	65	63	67	50	
4	65	63	67	50	

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Example



$$SS_T = \sum \sum y_{ij}^2 = \frac{62^2 + 60^2 + \dots + 63^2 + \dots + 59^2}{24 \text{ terms}}$$

$$= 98644 \quad (\text{dof} = 24)$$

$$SS_{\text{mean}} = N \bar{y}^2 = 24 \times 64^2 = 98304 \quad (\text{dof} = 1)$$

$$SS_{\text{treatment}} = \sum_{i=1}^k n_i (\bar{y}_i - \bar{y})^2$$

$$= 4(61-64)^2 + 6(66-64)^2 + 6(68-64)^2 + 8(61-64)^2$$

$$= 228 \quad (\text{dof} = k-1 = 3)$$

$$SS_{\text{error}} = \sum \sum (y_{ij} - \bar{y}_i)^2 = \frac{62-64)^2 + \dots + \dots + \dots}{24 \text{ terms}}$$

j	Stainless Steel	Carbon Steel	Nickel Alloy	High Speed Steel
1	62	63	68	56
2	60	67	66	62
3	63	71	71	60
4	59	64	67	61
5	NaN	65	68	63
6	NaN	66	68	64
7	NaN	NaN	NaN	63
8	NaN	NaN	NaN	59

$$\bar{y} = 64$$

$$y_{ij} \quad N=24$$

j^{th} observation for i^{th} metal

Here, $i = 1, 2, 3, 4$

(4 levels of variable 'metal')

$$\bar{y}_1 = 61, \bar{y}_2 = 66, \bar{y}_3 = 68, \bar{y}_4 = 61$$

$$n_1 = 4, n_2 = 6, n_3 = 6, n_4 = 8$$

OR by subtra

$$SS_{\text{error}} = SS_T - SS_{\text{mean}} - SS_{\text{treat}} = 112$$

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Example



j	Stainless Steel	Carbon Steel	Nickel Alloy	High Speed Steel
1	62	63	68	56
2	60	67	66	62
3	63	71	71	60
4	59	64	67	61
5	NaN	65	68	63
6	NaN	66	68	64
7	NaN	NaN	NaN	63
8	NaN	NaN	NaN	59

y_{ij}

j^{th} observation for i^{th} metal

Here, $i = 1, 2, 3, 4$

(4 levels of variable 'metal')

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Example



CEP2022_Notebook (2.2)

j	Stainless Steel	Carbon Steel	Nickel Alloy	High Speed Steel
1	62	63	68	56
2	60	67	66	62
3	63	71	71	60
4	59	64	67	61
5	NaN	65	68	63
6	NaN	66	68	64
7	NaN	NaN	NaN	63
8	NaN	NaN	NaN	59

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The Analysis of Variance Table for the Single-Factor, Fixed Effects Model

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	F_0
Between treatments	228	3 ✓	$\frac{228}{3} = 76$	$\frac{MS_{tr}}{MS_{er}} = \frac{76}{5.6} = 13.57$
Error (within treatments)	112	$N-k = 20$ ✓	$\frac{112}{20} = 5.6$	
Total	98644	24	~	
mean	98304	1	~	

compare with
 $F_{1-\alpha, 3, 20}$
 $F_{0.95, 3, 20}$

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Summary: Tests on Variances



■ TABLE 2.8

Tests on Variances of Normal Distributions

Hypothesis	Test Statistic	Fixed Significance Level Criteria for Rejection
$H_0: \sigma^2 = \sigma_0^2$ $H_1: \sigma^2 \neq \sigma_0^2$		$\chi_0^2 > \chi_{\alpha/2, n-1}^2$ or $\chi_0^2 < \chi_{1-\alpha/2, n-1}^2$
$H_0: \sigma^2 = \sigma_0^2$ $H_1: \sigma^2 < \sigma_0^2$	$\chi_0^2 = \frac{(n-1)S^2}{\sigma_0^2}$	$\chi_0^2 < \chi_{1-\alpha, n-1}^2$
$H_0: \sigma^2 = \sigma_0^2$ $H_1: \sigma^2 > \sigma_0^2$		$\chi_0^2 > \chi_{\alpha, n-1}^2$
$H_0: \sigma_1^2 = \sigma_2^2$ $H_1: \sigma_1^2 \neq \sigma_2^2$	$F_0 = \frac{S_1^2}{S_2^2}$	$F_0 > F_{\alpha/2, n_1-1, n_2-1}$ or $F_0 < F_{1-\alpha/2, n_1-1, n_2-1}$
$H_0: \sigma_1^2 = \sigma_2^2$ $H_1: \sigma_1^2 < \sigma_2^2$	$F_0 = \frac{S_2^2}{S_1^2}$	$F_0 > F_{\alpha, n_2-1, n_1-1}$
$H_0: \sigma_1^2 = \sigma_2^2$ $H_1: \sigma_1^2 > \sigma_2^2$	$F_0 = \frac{S_1^2}{S_2^2}$	$F_0 > F_{\alpha, n_1-1, n_2-1}$

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Example



The engineer is interested in determining if the RF power setting affects the etch rate, and she has run a completely randomized experiment with four levels of RF power and five replicates (see Table1).

We will use the analysis of variance to test, $H_0: \mu_1 = \mu_2 = \mu_3 = \mu_4$

against the alternative, H_1 : Some means are different (OR at least one mean is different)

RF Power (W)	Observed Etch Rate (Å/min)				
	1	2	3	4	5
160	575	542	530	539	570
180	565	593	590	579	610
200	600	651	610	637	629
220	725	700	715	685	710

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$k=4$, $N=20$, $n_i=5$

$$SS_T = \sum \sum y_{ij}^2 = 7704511$$

$$SS_m = N \bar{y}^2 = 20 \times 617.75^2 =$$

$$SS_{\text{treatment}} = \sum_{i=1}^k n_i (\bar{y}_i - \bar{y})^2$$

$$= 5 \times (551.2 - 617.75)^2 +$$

$$5 \times (587.4 - 617.75)^2 +$$

$$5 \times (625.4 - 617.75)^2 + 5 \times (707 - 617.75)^2$$

$$SS_{\text{error}} = (575 - 551.2)^2 + (542 - 551.2)^2 + \dots \\ + (565 - 587.4)^2 + (593 - 587.4)^2 + \dots$$

$$\left. \begin{aligned} \bar{y}_1 &= 551.2 \\ \bar{y}_2 &= 587.4 \\ \bar{y}_3 &= 625.4 \\ \bar{y}_4 &= 707 \end{aligned} \right\}$$

RF Power (W)	Observed Etch Rate (Å/min)				
	1	2	3	4	5
160	575	542	530	539	570 ✓
180	565	593	590	579	610
200	600	651	610	637	629
220	725	700	715	685	710

$$\bar{y} = 617.75$$

$$= SS_T - SS_m - SS_{\text{treatment}}$$

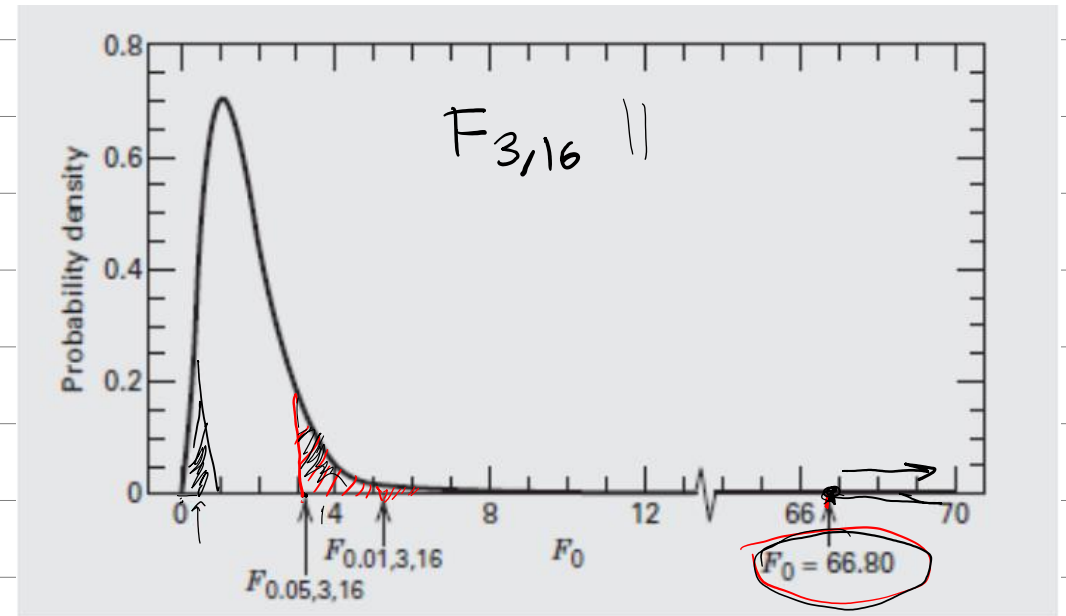
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	SS	DOF	MS ^{SS/DOF}	F ₀
SS _T	7704511	20	✓	
SS _m	7632301.25	1	✓	
SS _{treat}	66870.55	k-1 = 3	22290.18	$\frac{MS_{treat}}{MS_{error}} = 66.80$
SS _{error}	5339.20	16	333.08	

$$66.80 > 3.16$$

p value = ?

RF Power (W)	Observed Etch Rate (Å/min)				
	1	2	3	4	5
160	575	542	530	539	570
180	565	593	590	579	610
200	600	651	610	637	629
220	725	700	715	685	710



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ANOVA: Residuals



- Residuals are the difference between what is ACTUALLY observed (Experiment) vs. what is PREDICTED from a model that is used to adequately describe the data

$$\epsilon_{ij} = y_{ij} - \widetilde{y}_{ij}$$

- In One-way ANOVA, what is the model?

$$\underline{y}_{ij} = \mu + \underline{\tau}_i + \epsilon_{ij}$$

μ = grand mean

τ_j = treatment mean

ϵ_{ij} = error

- What is the prediction?

$$\widetilde{y}_{ij} = \mu + \tau_i \quad \text{"Effects Model"}$$

- Remember**, we had assumed that the residuals (or errors) are random and **normally distributed**.

So is that assumption valid IF we use the particular model? -> Model Adequacy Check!

$$\epsilon_{ij} = y_{ij} - \overline{y}_i$$

$$\epsilon_{ij} = y_{ij} - \frac{\mu + \tau_i}{1} = \overline{y}_i$$

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ANOVA: Model Adequacy Checking



Normality Assumption can be checked using several methods

- A dot diagram
- Histogram of residuals
- Normal probability plot

$$\frac{1 - 0.5}{n}$$

Etch Rate Data and Residuals from Example 3.1^a

Power (w)	Observations (<i>j</i>)					$\hat{y}_{ij} = \bar{y}_{i\cdot}$
	1	2	3	4	5	
160	23.8 ✓ ✓ 575 (13)	-9.2 ✓ 542 (14)	-21.2 530 (8)	-12.2 539 (5)	18.8 570 (4)	551.2 ✓
180	-22.4 565 (18)	5.6 593 (9)	2.6 590 (6)	-8.4 579 (16)	22.6 610 (17)	587.4
200	-25.4 600 (7)	25.6 651 (19)	-15.4 ✓ 610 (10)	11.6 637 (20)	3.6 → 629 (1)	625.4
220	18.0 → 725 (2)	-7.0 700 (3)	8.0 715 (15)	-22.0 685 (11)	3.0 710 (12)	707.0

y_1
 y_2
 y_3
 y_4

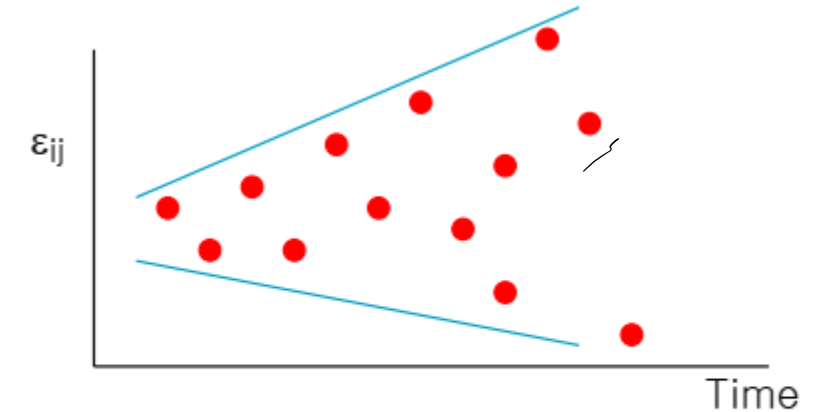
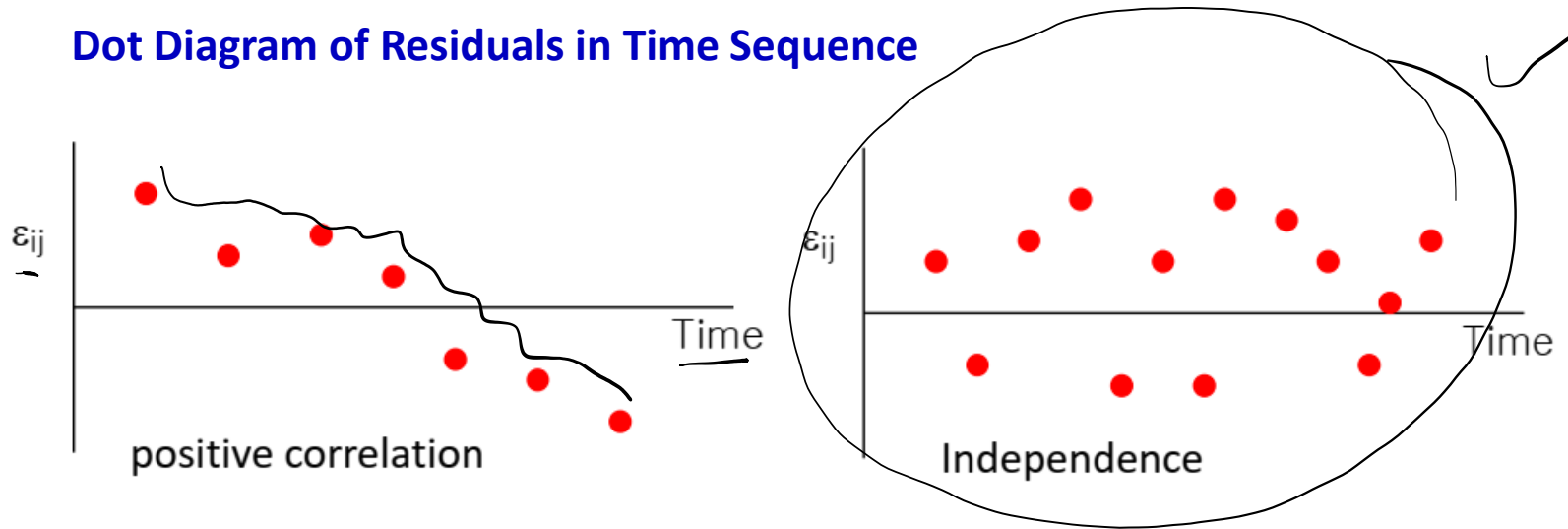
^aThe residuals are shown in the box in each cell. The numbers in parentheses indicate the order in which each experimental run was made.

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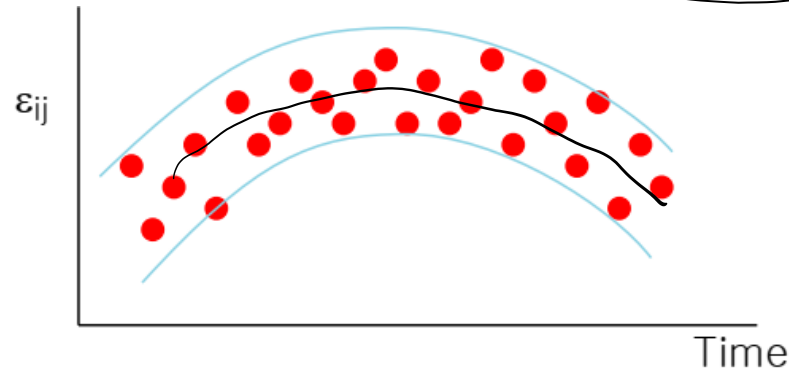
Model Adequacy Checking



Dot Diagram of Residuals in Time Sequence



The variance is not constant, but increases with time.



Model is not adequate, a quadratic term (may be interaction term) is needed in the model.

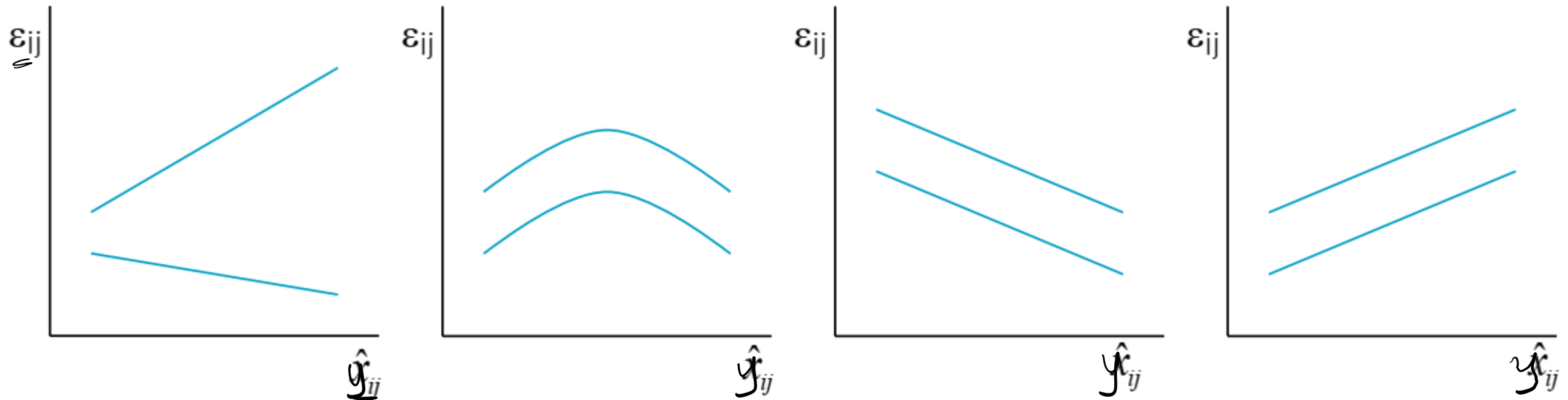
If the model is adequate and the assumptions are satisfied, the errors or residuals, ϵ_{ij} , should have NO structure.

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Model Adequacy Checking



Dot Diagram of Residuals (Errors) vs Model Predictions



If the model is adequate and the assumptions are satisfied, the errors or residuals, ϵ_{ij} , should be INDEPENDENT of observations

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ANOVA: Model Adequacy Checking



Etch Rate Data and Residuals from Example 3.1^a

Power (w)	Observations (j)					$\hat{y}_{ij} = \bar{y}_i$
	1	2	3	4	5	
160	23.8 575 (13)	-9.2 542 (14)	-21.2 530 (8)	-12.2 539 (5)	18.8 570 (4)	551.2
180	-22.4 565 (18)	5.6 593 (9)	2.6 590 (6)	-8.4 579 (16)	22.6 610 (17)	587.4
200	-25.4 600 (7)	25.6 651 (19)	-15.4 610 (10)	11.6 637 (20)	3.6 629 (1)	625.4
220	18.0 725 (2)	-7.0 700 (3)	8.0 715 (15)	-22.0 685 (11)	3.0 710 (12)	707.0

^aThe residuals are shown in the box in each cell. The numbers in parentheses indicate the order in which each experimental run was made.

A rough check for outliers may be made by examining the **standardized residuals**

$$d_{ij} = \frac{e_{ij}}{\sqrt{MS_E}} \quad (3.18)$$

If the errors ϵ_{ij} are $N(0, \sigma^2)$, the standardized residuals should be approximately normal with mean zero and unit variance. Thus, about 68 percent of the standardized residuals should fall within the limits ± 1 , about 95 percent of them should fall within ± 2 , and virtually all of them should fall within ± 3 . A residual bigger than 3 or 4 standard deviations from zero is a potential outlier.

For the tensile strength data of Example 3.1, the normal probability plot gives no indication of outliers. Furthermore, the largest standardized residual is

$$d_1 = \frac{e_1}{\sqrt{MS_E}} = \frac{25.6}{\sqrt{333.70}} = \frac{25.6}{18.27} = 1.40$$

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