ME 794 SDOE Quiz 4

Date: March 21, 2024 **Time:** 90 minutes **Marks:** 20

- Be clear, show all steps, and mention any assumptions you make with appropriate justifications.
- Use of a non-programmable calculator is permitted (no sharing). You must not use notes, cell phones, or other assistance in this exam.
- 1. An engineer is interested in the effects of plasma treatment time (A), flow rate (B), and input power (C) on the water contact angle of droplets on the fine polished SS surface. Two levels of each factor are chosen, and three replicates of a 2³ factorial design are run. The results are as follows:

A [s]	B [litter/min]	C [W]	First replicate	Second replicate	Third replicate
30	4	3.2	22	31	25
60	4	3.2	32	43	29
30	8	3.2	35	34	50
60	8	3.2	55	47	46
30	4	6.5	44	45	38
60	4	6.5	40	37	36
30	8	6.5	60	50	54
60	8	6.5	39	41	47

- a) Estimate the factor effects.
- b) Estimate the effects 95% confidence interval values after calculating the pooled sample variance S_p^2 .
- c) Write down a regression model for predicting water contact angle based on the results of this experiment.

$$(\bar{y} = a_0 + a_1X_1 + a_2X_2 + a_3X_3 + a_4X_1X_2 + a_5X_1X_3 + a_6X_2X_3 + a_7X_1X_2X_3)$$

- 2. The following output was obtained from a computer program that performed a two-factor ANOVA on a factorial experiment.
 - a) State the statistical model used in factorial experiments.
 - b) Fill in the blanks in the ANOVA table.
 - d) How many replicates of the experiment were performed?
 - e) What conclusions would you draw about this experiment based on the F values (= 0.05)?

Formula Sheet

[15]

[5]

```
Finsher to Q1

E_{A} = \frac{34.67.49.33.437.67.42.33}{42.33.437.67.42.33} - (26439.4)
= \frac{5.9}{4} \times \frac
\begin{array}{c} 3-1 \\ 52^2 = \frac{(34.67.32)^2 + (34.67.43)^2 + (24.67-29)^2}{3-1} = 54.33 \\ 53^2 = \frac{64.25}{54^2} = \frac{24.33}{55^2} = \frac{12.1}{56^2} = \frac{4.33}{56^2} \end{array}
                                                                                                                   \Rightarrow Sp^{2} = \frac{\sum S_{i}^{2}}{8\lambda(3-1)} = \frac{21+54.33+64.25+24.33+12.1+4.33}{16}
where all experiment \frac{425.33+17.33}{8\lambda(3-1)} = \frac{13.937}{16}
= \frac{1}{6} \cdot \frac{6i+1}{5} \cdot \frac{5p^{2}}{6}
= \frac{1}{6} \cdot \frac{6i+1}{6} \cdot \frac{5p^{2}}{6} \cdot \frac{1}{6} \cdot \frac{1
```

C) Regression under
$$5 = a_0 + a_1 x_1 + a_2 x_2 + a_3 x_3 + a_4 x_1 x_2 + a_5 x_1 x_3$$

$$+ a_6 x_2 x_3 + a_7 x_1 x_2 x_3$$

$$\Rightarrow a_0 = \frac{59}{8} = 7 \frac{26 + 34 \cdot 67 + 29 \cdot 67 \cdot 149 \cdot 33 \cdot 42 \cdot 33 + 37 \cdot 67}{8}$$

$$54 \cdot 67 + 42 \cdot 3^3 = 40.833 : a_0$$

$$50 : due to $6 : = 79 = 40.833 + 0.3325 \times 1 + 11.3325 \times 2 + \frac{20167}{2}$

$$2 = \frac{26 + 34 \cdot 67 + 29 \cdot 67 \cdot 149 \cdot 33 \cdot 42 \cdot 33 + 37 \cdot 67}{2}$$

$$1 = \frac{10.8325 \times 14 \cdot 1.6725 \times 142 - 8.8325 \times 143 - 2.8325 \times 143}{2} = \frac{2.8325 \times 143}{2}$$$$

Source	DF	SS	MS	F
Α	1		0.0002	
В	_	180.3768		
Interaction	3	8.479		
Error	8	158.797		
Total	15	347.653		

```
Source DoF SS MS F Ftable

B 1 0.0002 0.0002 1.007 x105 5.32

Interaction 3 8.479 2.826 0.1256 3.029 4.07

Error 8 158.797 19.85

TOTAL 15 347.653

DoF A \rightarrow 9-1=1 \therefore 9=2

Interaction \rightarrow (9-1) (b-1) = 3 \therefore b=4

DOF B \rightarrow b-1 \therefore DOF B = 3

DOF of total \Rightarrow abn-1=15 \therefore n=2

Solution for question 2
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_) Estect model

8	ч	6		8-33	6.33	8.33		-5:33	-5.33	- 2:33	
14	5	8	=	8-33	8-33	8.33	+	0.67	0.67	0.67	
L 14	6	[0]		8-33	8.33	8-33		1.63	1.63	1.67_	

			7	7		٦.
+	3:67	~ 3·3 <u>3</u>	~ 0.33	-1.67	1:33	0.33
		~ 3:33				
	L3.67	~ 2-33	-0.35	ΓO-33	-0.67	0.33

.: Sum of all integes is

	-		7	(7		7		c		7
_	64	لما	36		69-39	69.39	69.39		5.43	5.43	5.13
	196	25	64	5	69.39	68.39	68.39	t	0.45	04	045
					69.39						

_		-	. (7
13.47	11.07	0-11		2.79	1.37	0.1(
13-47						
13.47				1		- 1

... Sum of Square one

Total = 733

Mean = 624:51

Block = 74.0(

Treatment = 26-01

 $F_{0.05}$, 2, 4 = 6.94 $F_{0.05}$ table = 6.63

	ν_1	Degrees of Freedom for the Numerator (ν_1)												
ν_2		1	2	3	4	5	6	7	8	9	10	12	15	20
		161.4	199.5	215.7	224.6	230.2	234.0	236.8	238.9	240.5	241.9	243.9	245.9	248.0
	2	18.51	19.00	19.16	19.25	19.30	19.33	19.35	19.37	19.38	19.40	19.41	19.43	19.45
	3	10.13	9.55	9.28	9.12	9.01	8.94	8.89	8.85	8.81	8.79	8.74	8.70	8.66
	4	7.71	6.94	6.59	6.39	6.26	6.16	6.09	6.04	6.00	5.96	5.91	5.86	5.80
	5	6.61	5.79	5.41	5.19	5.05	4.95	4.88	4.82	4.77	4.74	4.68	4.62	4.56
	6	5.99	5.14	4.76	4.53	4.39	4.28	4.21	4.15	4.10	4.06	4.00	3.94	3.87
	7	5.59	4.74	4.35	4.12	3.97	3.87	3.79	3.73	3.68	3.64	3.57	3.51	3.44
	8	5.32	4.46	4.07	3.84	3.69	3.58	3.50	3.44	3.39	3.35	3.28	3.22	3.15
2	9	5.12	4.26	3.86	3.63	3.48	3.37	3.29	3.23	3.18	3.14	3.07	3.01	2.94
۳ ر	10	4.96	4.10	3.71	3.48	3.33	3.22	3.14	3.07	3.02	2.98	2.91	2.85	2.77
ato	11	4.84	3.98	3.59	3.36	3.20	3.09	3.01	2.95	2.90	2.85	2.79	2.72	2.65
Ė	12	4.75	3.89	3.49	3.26	3.11	3.00	2.91	2.85	2.80	2.75	2.69	2.62	2.54
Ö	13	4.67	3.81	3.41	3.18	3.03	2.92	2.83	2.77	2.71	2.67	2.60	2.53	2.46
Ğ	14	4.60	3.74	3.34	3.11	2.96	2.85	2.76	2.70	2.65	2.60	2.53	2.46	2.39
r the	15	4.54	3.68	3.29	3.06	2.90	2.79	2.71	2.64	2.59	2.54	2.48	2.40	2.33
for	16	4.49	3.63	3.24	3.01	2.85	2.74	2.66	2.59	2.54	2.49	2.42	2.35	2.28
lom	17	4.45	3.59	3.20	2.96	2.81	2.70	2.61	2.55	2.49	2.45	2.38	2.31	2.23
eeq	18	4.41	3.55	3.16	2.93	2.77	2.66	2.58	2.51	2.46	2.41	2.34	2.27	2.19
of Freedom for the Denominator (ν_2)	19	4.38	3.52	3.13	2.90	2.74	2.63	2.54	2.48	2.42	2.38	2.31	2.23	2.16

Table: $F_{0.05,v1,v2}$

 	df – Deg	gree of fre	eedom		V.	rea und	er the c	e such that urve after t
		6		0	t_a	is 'α'	as show	n in Fig.
df/p	0.40	0.25	0.10	0.05	0.025	0.01	0.005	0.0005
Г	0.324920	1.000000	3.077684	6.313752	12.70620	31.82052	63.65674	636.6192
2	0.288675	0.816497	1.885618	2.919986	4.30265	6.96456	9.92484	31.5991
3	0.276671	0.764892	1.637744	2.353363	3.18245	4.54070	5.84091	12.9240
4	0.270722	0.740697	1.533206	2.131847	2.77645	3.74695	4.60409	8.6103
5	0.267181	0.726687	1.475884	2.015048	2.57058	3.36493	4.03214	6.8688
6	0.264835	0.717558	1.439756	1.943180	2.44691	3.14267	3.70743	5.9588
7	0.263167	0.711142	1.414924	1.894579	2.36462	2.99795	3.49948	5.4079
8	0.261921	0.706387	1.396815	1.859548	2.30600	2.89646	3.35539	5.0413
9	0.260955	0.702722	1.383029	1.833113	2.26216	2.82144	3.24984	4.7809
10	0.260185	0.699812	1.372184	1.812461	2.22814	2.76377	3.16927	4.5869
11	0.259556	0.697445	1.363430	1.795885	2.20099	2.71808	3.10581	4.4370
12	0.259033	0.695483	1.356217	1.782288	2.17881	2.68100	3.05454	4.3178
13	0.258591	0.693829	1.350171	1.770933	2.16037	2.65031	3.01228	4.2208
14	0.258213	0.692417	1.345030	1.761310	2.14479	2.62449	2.97684	4.1405
15	0.257885	0.691197	1.340606	1.753050	2.13145	2.60248	2.94671	4.0728
16	0.257599	0.690132	1.336757	1.745884	2.11991	2.58349	2.92078	4.0150
17	0.257347	0.689195	1.333379	1.739607	2.10982	2.56693	2.89823	3.9651
18	0.257123	0.688364	1.330391	1.734064	2.10092	2.55238	2.87844	3.9216
19	0.256923	0.687621	1.327728	1.729133	2.09302	2.53948	2.86093	3.8834
20	0.256743	0.686954	1.325341	1.724718	2.08596	2.52798	2.84534	3.8495
21	0.256580	0.686352	1.323188	1.720743	2.07961	2.51765	2.83136	3.8193
22	0.256432	0.685805	1.321237	1.717144	2.07387	2.50832	2.81876	3.7921
23	0.256297	0.685306	1.319460	1.713872	2.06866	2.49987	2.80734	3.7676
24	0.256173	0.684850	1.317836	1.710882	2.06390	2.49216	2.79694	3.7454
25	0.256060	0.684430	1.316345	1.708141	2.05954	2.48511	2.78744	3.7251
26	0.255955	0.684043	1.314972	1.705618	2.05553	2.47863	2.77871	3.7066
27	0.255858	0.683685	1.313703	1.703288	2.05183	2.47266	2.77068	3.6896
28	0.255768	0.683353	1.312527	1.701131	2.04841	2.46714	2.76326	3.6739
29	0.255684	0.683044	1.311434	1.699127	2.04523	2.46202	2.75639	3.6594
30	0.255605	0.682756	1.310415	1.697261 nd of P	2.04227	2.45726	2.75000	3.6460