

# Bartlett Test

Note that for calculating the confidence intervals, we assumed that the true variance  $\sigma^2$  is the same for all observations and that the observations are independent.

- How can we check if this assumption is valid? **Bartlett Test**

$$H_0 : \sigma_1^2 = \sigma_2^2 = \dots = \sigma_m^2 = \sigma_y^2$$

$$H_1 : \text{at least one } \sigma_i^2 \neq \sigma_j^2, i \neq j$$

$$\chi_{cal}^2 = \frac{M}{C}$$

where

$$M = (N - m) \ln(s_p^2) - \sum_{i=1}^m (n_i - 1) \ln(s_i^2)$$

$$C = 1 + \frac{1}{3(m-1)} \left[ \left( \sum_{i=1}^m \frac{1}{n_i - 1} \right) - \frac{1}{N - m} \right]$$

$$m = 2^k \quad (\text{Total experiments})$$

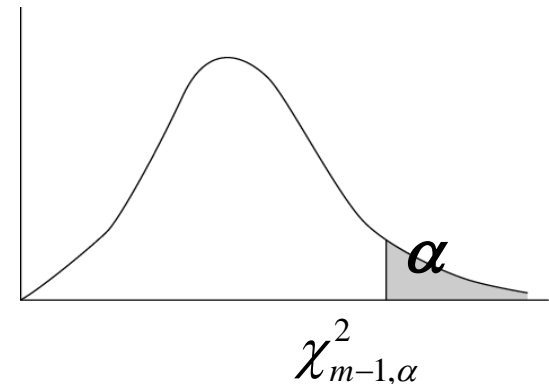
$$\text{Sample size} = n$$

$$N = n_1 + n_2 + \dots + n_m$$

The value of  $M$  will be large if the sample variances  $s_i^2$  differ greatly in magnitude, and will be zero if all the sample variances are exactly equal.

We will reject  $H_0$  if  $\chi_{cal}^2$  is too large, i.e.,

$$\chi_{cal}^2 > \chi_{m-1, \alpha}^2$$



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# Bartlett Test

## Example: Bartlett Test

$$\chi^2_{v=m-1} = \frac{M}{C} \quad \text{where, } M = (N - m) \ln(s_p^2) - \sum_{i=1}^m (n_i - 1) \ln(s_i^2), \quad \text{and} \quad C = 1 + \frac{1}{3(m-1)} \left[ \left( \sum_{i=1}^m \frac{1}{n_i - 1} \right) - \frac{1}{N - m} \right]$$

Here, N = 16, m = 8

$$S_1^2 = 24.5, S_2^2 = 21.78, S_3^2 = 134.48, S_4^2 = 242.0,$$

$$S_5^2 = 3.92, S_6^2 = 8.82, S_7^2 = 33.62, S_8^2 = 72.00$$

$$S_p^2 = \frac{[(y_{a1} - \bar{y}_1)^2 + (y_{b1} - \bar{y}_1)^2 + \dots + (y_{a8} - \bar{y}_8)^2 + (y_{b8} - \bar{y}_8)^2]}{(2-1) + \dots + (2-1)} = 67.64$$

$$\begin{aligned} M &= (16 - 8) \ln 67.64 - [(2 - 1) \ln 24.5 + (2 - 1) \ln 21.78 \\ &\quad + (2 - 1) \ln 134.48 + (2 - 1) \ln 242 + (2 - 1) \ln 3.92 \\ &\quad + (2 - 1) \ln 8.82 + (2 - 1) \ln 33.62 + (2 - 1) \ln 72.0] \\ &= 5.713 \end{aligned}$$

$$\chi^2_{\text{cal}} = \frac{5.713}{1.357} = 4.21 \quad \chi^2_{7, \alpha=0.05} = 14.1$$

The value of  $M$  will be large if the sample variances  $s_i^2$  differ greatly in magnitude, and will be zero if all the sample variances are exactly equal.

We will reject  $H_0$  if  $\chi^2_{\text{cal}}$  is too large, i.e.,  $\chi^2_{\text{cal}} > \chi^2_{m-1, \alpha}$

$$\begin{aligned} C &= 1 + \frac{1}{3(8-1)} \left[ \left( \sum_{i=1}^8 \frac{1}{2-1} \right) - \frac{1}{16-8} \right] \\ &= 1 + \frac{1}{21} [8 - 5] = 1.357 \end{aligned}$$

Test #	X1	X2	X3	Y <sub>ai</sub> (kpsi)	Y <sub>bi</sub> (kpsi)	Average (kpsi)
1	-1	-1	-1	84	91	87.5
2	1	-1	-1	90.6	84	87.3
3	-1	1	-1	69.6	86	77.8
4	1	1	-1	76	98	87
5	-1	-1	1	77.7	80.5	79.1
6	1	-1	1	99.7	95.5	97.6
7	-1	1	1	82.7	74.5	78.6
8	1	1	1	93.7	81.7	87.7

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# Example

The yield form, a certain chemical depends on

either the **chemical formulation of the input materials** or **the mixer speed, or both**.

A 2-level factorial design was run with three replicates and the yield data are shown below.

Find Main and Interaction Effects and their Confidence Intervals, and Significance using ANOVA

$x_1$	$x_2$	$y_a$	$y_b$	$y_c$	$\bar{y}$
-1	-1	10	20	30	20
1	-1	40	30	50	40
-1	1	60	30	60	50
1	1	40	45	50	45

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$x_1$	$x_2$	$y_a$	$y_b$	$y_c$	$\bar{y}$
-1	-1	10	20	30	20
1	-1	40	30	50	40
-1	1	60	30	60	50
1	1	40	45	50	45

$$E_1 = \frac{1}{2} (-20 + 40 + (-50) + 45)$$

$$E_1 = 7.5 \quad \checkmark$$

$$E_2 = \frac{1}{2} (-20 - 40 + 50 + 45) = 17.5 \quad \checkmark$$

$$E_{12} = \frac{1}{2} (20 - 40 - 50 + 45) = -12.5 \quad \checkmark$$

What are sample variances? How to find confidence intervals for  $E_1, E_2, E_{12}$ ?

$$S_1^2 = \frac{\sum (y_i - \bar{y})^2}{n-1} = \frac{(10-20)^2 + (20-20)^2 + (30-20)^2}{2} = 100$$

$$S_2^2 = \frac{(40-40)^2 + (30-40)^2 + (50-40)^2}{2} = 100$$

$$S_3^2 = 300$$

$$S_4^2 = 25$$

pooled variance

$$S_p^2 = \frac{\sum \text{DOF} \times S_i^2}{T \text{DOF}} = \frac{2(100) + 2(100) + 2(300) + 2(25)}{2+2+2+2} = 131.25$$

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$x_1$	$x_2$	$y_a$	$y_b$	$y_c$	$\bar{y}$
-1	-1	10	20	30	20
1	-1	40	30	50	40
-1	1	60	30	60	50
1	1	40	45	50	45

$$V(E_1) = \sigma^2/3$$

$$\underline{V(E_2)} = \sigma^2/3 = V(E_{12})$$

Confidence interval  $E_i \pm t_{v,\alpha} \sqrt{\frac{S_p^2}{3}}$

at 95% confidence  $t_{v,\alpha} = t_{8,0.025} = 2.306$  from table

$$E_i \pm 2.306 \sqrt{\frac{131.25}{3}} = E_i \pm 15.25$$

78

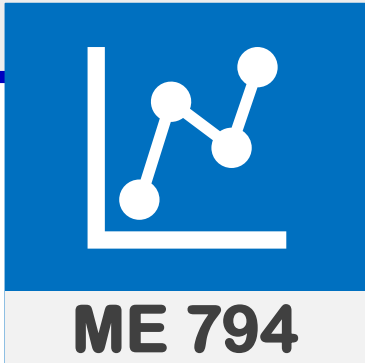
Confidence interval for  $E_1$   $V(y) = c^2 V(\bar{y})$

$$V(E_1) = V\left(\frac{\bar{y}_2 - \bar{y}_1 + \bar{y}_4 - \bar{y}_3}{2}\right)$$

$$= \frac{1}{4} V\left(\frac{\bar{y}_{2a} + \bar{y}_{2b} + \bar{y}_{2c}}{3} - \frac{\bar{y}_{1a} + \bar{y}_{1b} + \bar{y}_{1c}}{3} + \frac{\bar{y}_{4a} + \bar{y}_{4b} + \bar{y}_{4c}}{3} - \frac{\bar{y}_{3a} + \bar{y}_{3b} + \bar{y}_{3c}}{3}\right)$$

$$= \frac{1}{36} 12 V(y_i) = \frac{12}{36} \sigma^2 = \frac{1}{3} \sigma^2$$

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# Statistical Design of Experiments

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## Response Surface Methodology

**Acknowledgement: Design and Analysis of Experiments by Montegamory.** Some of the course material has been adopted from similar courses taught previously by Prof. Shiv Kapoor (UofI), and Prof. Suhas Joshi (IITB).

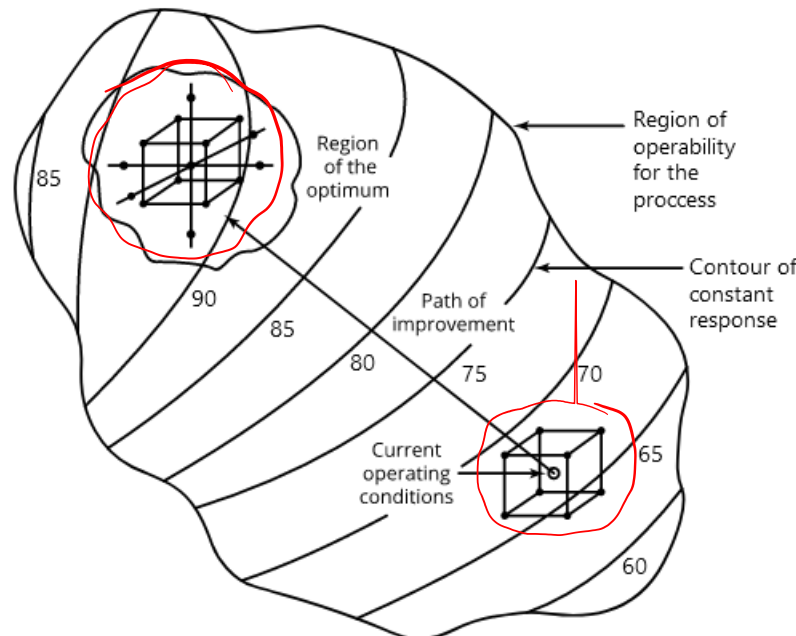
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# Goal of RSM

- So far, the focus of the design of experiments was '**factor screening**' – which factors strongly affect the process, which factors are less important, how the factors interact ..
- After screening, we now shift our focus to **optimization** – which factor level combinations give us maximum (e.g. yield) or minimum (e.g. cost), or target result.
- *The objective of Response Surface Methods (RSM) is optimization, finding the best set of factor levels to achieve some goal.*



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# Example

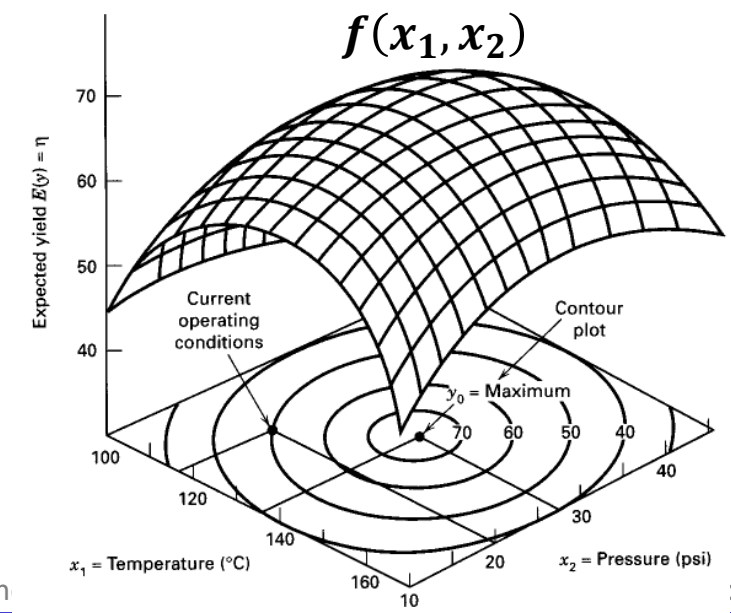
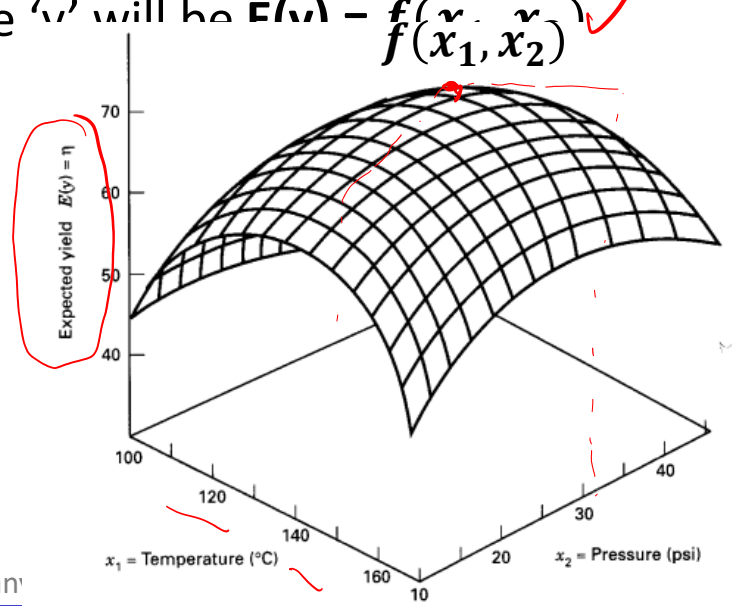
Suppose, yield ( $y$ ) of a chemical process depends on temperature ( $x_1$ ) and pressure ( $x_2$ ). The chemical engineer would like to find out which levels of temperature and pressure give the maximum yield.

One may write, 
$$\bar{y} = f(x_1, x_2) + \bar{\epsilon}$$

Where ' $\epsilon$ ' is the error/noise observed in response ' $y$ '

The expected value of the response ' $y$ ' will be  $E(y) = f(x_1, x_2)$  ✓

One could show this graphically,



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# Sequential Process

## 'RSM' is sequential procedure

- In most problems, *the exact relationship between the response variable and the independent variables is unknown*
- Therefore, the first step in RSM is to *find a suitable approximation* of the true functional relationship between response and independent variables.
- Typically, the approximations are in the *form of low-order polynomials* in some region of independent variables

For example, if response ( $y$ ) is well modeled by linear function of independent variables ( $x_1, x_2, x_3, \dots, x_k$ ), then we can write the approximate function as **'first order model'**

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \dots + \beta_k x_k + \epsilon$$

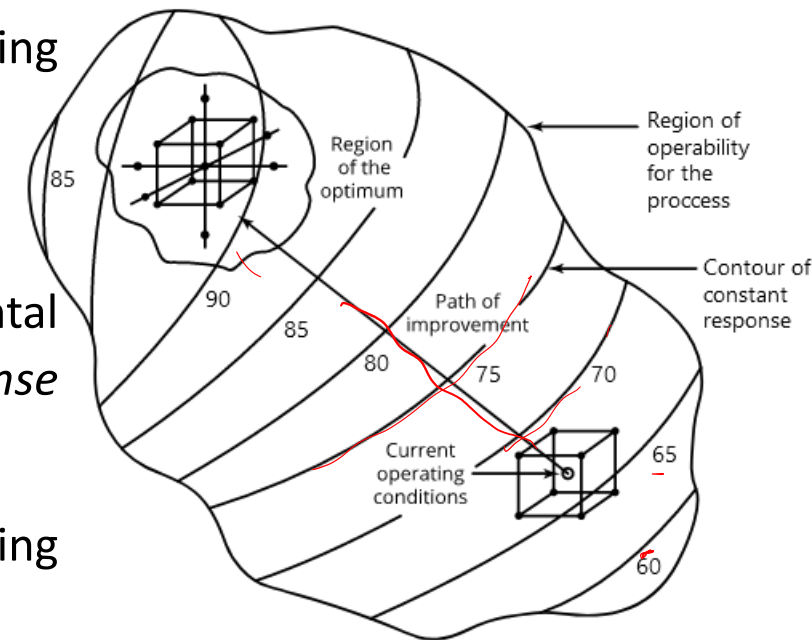
If there is curvature/non-linearity in the system, we must use polynomial of 2<sup>nd</sup> or higher degree,

For example, **second degree model** :  $y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{i=1}^k \sum_{j=1}^k \beta_{ij} x_i x_j + \epsilon$

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- In real-problems, it is unlikely that these polynomials will provide reasonable approximation of the true functional relationship over the ENTIRE range of independent variables, but they work quite well for a relatively small region
- The coefficients in the RSM models (model parameters) are estimated using least square method (least square fitting)
- The response surface analysis is then performed on the fitted surface
- The model parameters can be obtained more effectively if proper experimental designs are used to collect the data (responses). Designs for fitting the response surfaces are called response surface designs.
- Often we start at a point that is far from optimum such as the existing operating conditions. If the region is linear, we use first order model.
- We then take the shortest and most efficient path towards the optimum
- As we near the optimum, there may be non-linearities, so we can employ higher order models



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# Method of Steepest Ascent

- If we want to find maximum response, then we will be 'climbing the hill', if we want to minimize the response, we will be 'descending into a valley'
- We then take the shortest and most efficient path towards the optimum
- 'Method of steepest ascent' is a procedure of moving sequentially along path of steepest ascent, i.e., direction of the maximum increase in response.
- If minimization is desired, we follow the 'method steepest descent'

- If we use first order model,

$$\hat{y} = \hat{\beta}_0 + \sum_{i=1}^k \hat{\beta}_i x_i$$

Then, the contours of  $y$  will be a set of parallel lines

So the path of steepest ascent will be along a line perpendicular to the contour from center of the region

The actual step-size will be dependent on other practical considerations

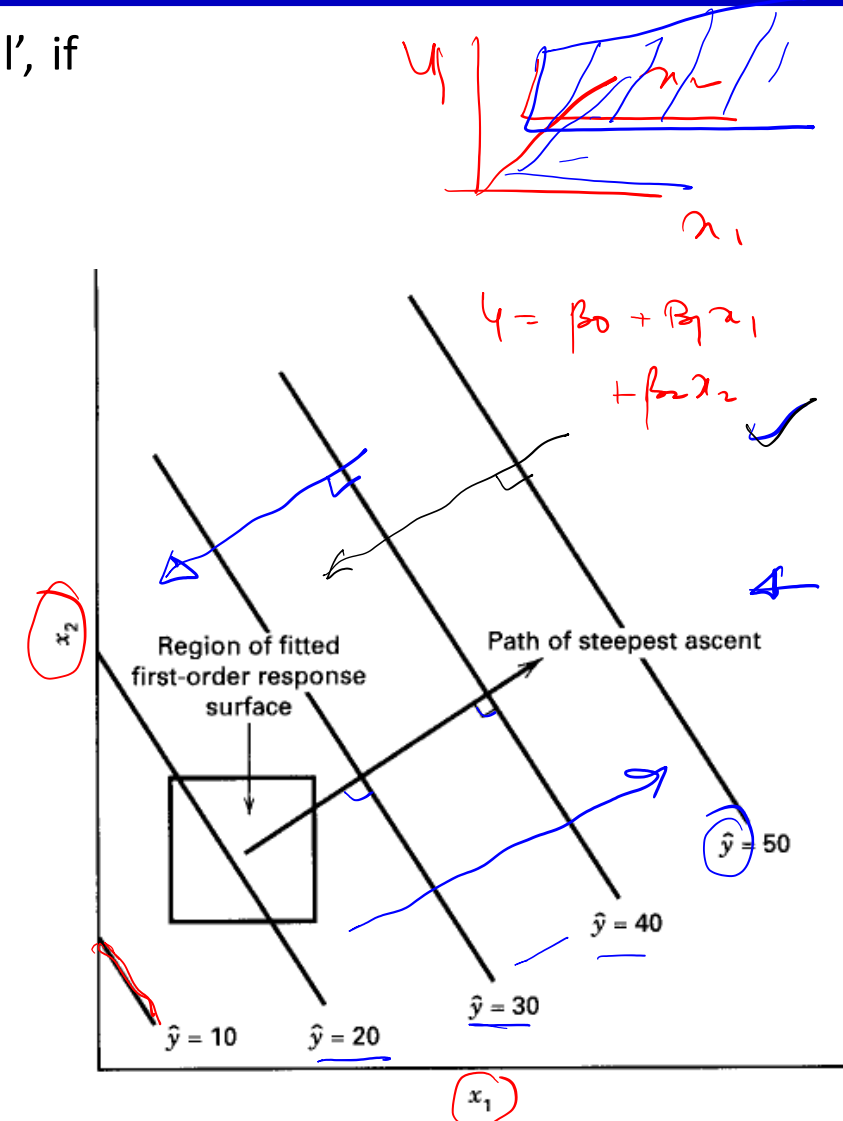


Figure 11-4 First-order response surface and path of steepest ascent.

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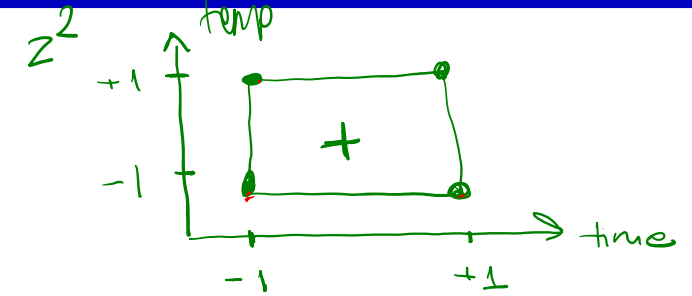
# Example

A chemical engineer is interested in determining the operating conditions that maximize the yield of a process. Two controllable variables influence process yield: reaction time and reaction temperature. The engineer is currently operating the process with a reaction time of 35 minutes and a temperature of 155°F, which result in yields of around 40 percent.

$\xi_1$  reaction time       $\xi_2$  temperature

Region of (30, 40) minutes of time, and (150, 160) F temperature was explored and responses were collected.

Note the experimental design is  $2^2$  factorial design augmented by five center points. 5 replications at the center point [35, 155] allow estimation of error as well as help us determine adequacy of linear (first-order) model



$$\boxed{x_1} = \frac{\xi_1 - 35}{5} \quad \text{and} \quad \boxed{x_2} = \frac{\xi_2 - 155}{5}$$

Time, Temp				
Natural Variables		Coded Variables		Response y
$\xi_1$	$\xi_2$	$x_1$	$x_2$	
30	150	-1	-1	39.3
30	160	-1	1	40.0
40	150	1	-1	40.9
40	160	1	1	41.5
35	155	0	0	40.3
35	155	0	0	40.5
35	155	0	0	40.7
35	155	0	0	40.2
35	155	0	0	40.6

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# 2<sup>2</sup> Factorial Analysis

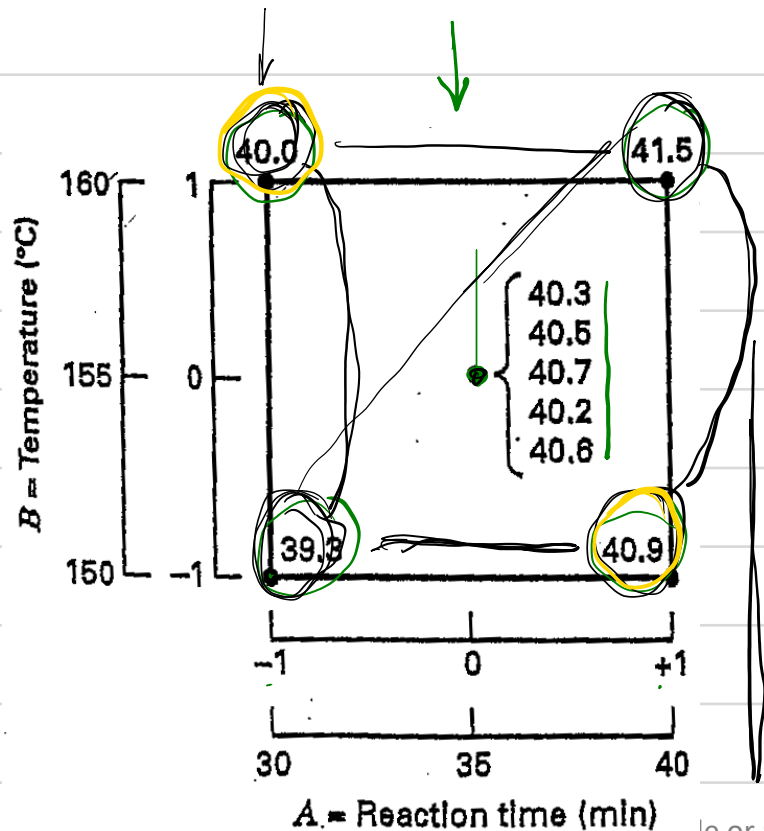
Can we find which terms are important?

What will be the first-order model?

Will a first-order model be appropriate?

First order model,  $y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \varepsilon$

obs predicted,  $\hat{y} = \hat{\beta}_0 + \hat{\beta}_1 x_1 + \hat{\beta}_2 x_2$



Natural Variables		Coded Variables		Response y
$\xi_1$	$\xi_2$	$x_1$	$x_2$	
30	150	-1	-1	39.3
30	160	-1	1	40.0
40	150	1	-1	40.9
40	160	1	1	41.5
35	155	0	0	40.3
35	155	0	0	40.5
35	155	0	0	40.7
35	155	0	0	40.2
35	155	0	0	40.6

First let's find out (DIY)  
 $\beta_0, \beta_1, \beta_2, \beta_{12}$

$$\beta_0 = \frac{(39.3 + 40.0 + 40.9 + 41.5)}{4} = 40.425 \quad \checkmark$$

$$\beta_1 = \frac{1}{2} (-39.3 - 40.0 + 40.9 + 41.5) = 1.55 \quad \checkmark$$

$$\beta_2 = \frac{1}{2} (-39.3 + 40.0 - 40.9 + 41.5) = 0.65 \quad \checkmark$$

$$\beta_{12} = -0.05 \quad \checkmark$$



# ANOVA

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \epsilon$$

can we reduce this to a 1-order model

$$+ (\beta_{11} x_1^2 + \beta_{22} x_2^2)$$

SS<sub>T</sub>, SS<sub>mean</sub>

ANOVA TABLE

	DF	SS	MS	F <sub>0</sub>
Total	9			
x <sub>1</sub>	1	2.4025	→	55.87
x <sub>2</sub>	1	0.4225		9.83
x <sub>1</sub> x <sub>2</sub>	1 ✓	0.0025		0.06
mean	1	.		
ε	5-1 ✓	0.172		

and 1 ?

$$SS_{x_1} = 2 \left( (39.65 - 40.425)^2 + (41.2 - 40.425)^2 \right)$$

$$SS_{x_2} = 2 \left( (40.1 - 40.425)^2 + (40.75 - 40.425)^2 \right)$$

$$SS_{x_1 x_2} = 2 \left( (40.45 - 40.425)^2 + (40.9 - 40.425)^2 \right)$$

$$= 0.0025$$

$$\epsilon = (y_1 - \bar{y}_c)^2 + (y_2 - \bar{y}_c)^2 + \dots + (y_5 - \bar{y}_c)^2$$

$$= (40.3 - 40.46)^2 + ( )^2 + \dots + (40.6 - 40.46)^2$$

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# ANOVA

$$\text{Find } \underline{SS_{\text{quad}}} = \frac{n_F n_c (\bar{y}_F - \bar{y}_c)^2}{n_F + n_c} = \frac{4 \times 5 (40.425 - 40.46)^2}{9}$$

Another check of the adequacy of the straight-line model is obtained by applying the check for pure quadratic curvature effect described in Section 6-6. Recall that this consists of comparing the average response at the four points in the factorial portion of the design, say  $\bar{y}_F = 40.425$ , with the average response at the design center, say  $\bar{y}_C = 40.46$ . If there is quadratic curvature in the true response function, then  $\bar{y}_F - \bar{y}_C$  is a measure of this curvature. If  $\beta_{11}$  and  $\beta_{22}$  are the coefficients of the “pure quadratic” terms  $x_1^2$  and  $x_2^2$ , then  $\bar{y}_F - \bar{y}_C$  is an estimate of  $\beta_{11} + \beta_{22}$ . In our example, an estimate of the pure quadratic term is

$$\begin{aligned}\hat{\beta}_{11} + \hat{\beta}_{22} &= \bar{y}_F - \bar{y}_C \\ &= 40.425 - 40.46 \\ &= -0.035\end{aligned}$$

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# 'Climbing the hill'

$$\frac{0.325}{0.775} = 0.42$$

$$\hat{y} = 40.44 + 0.775x_1 + 0.325x_2$$

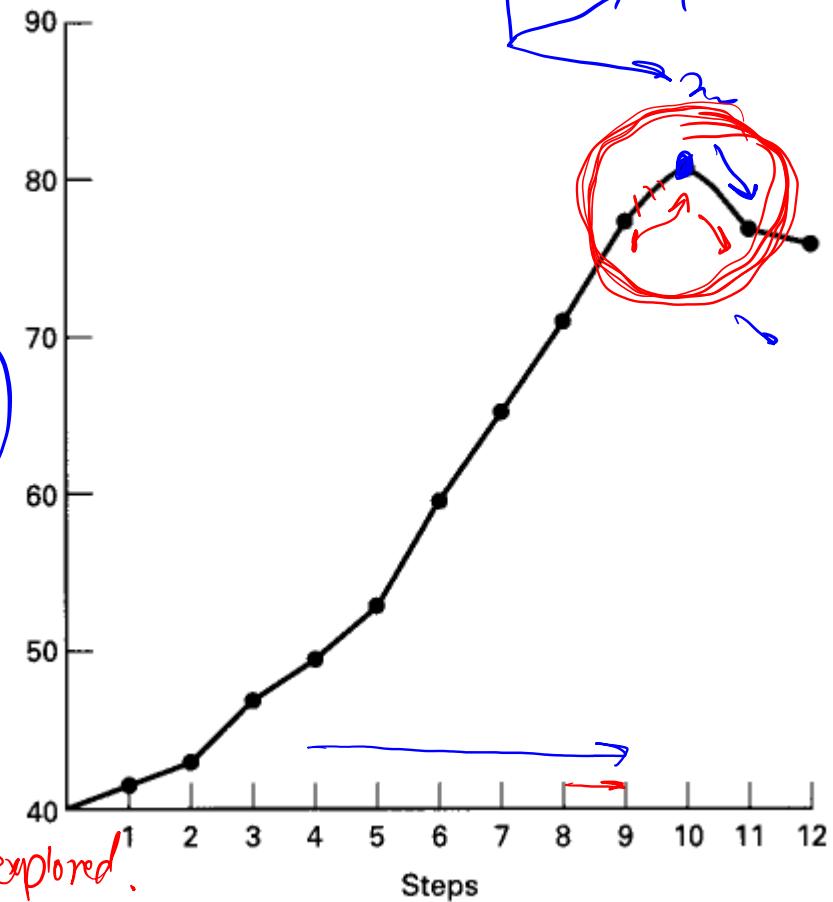
Only applicable in region explored. ✓

note that  $\hat{y} = f(x_1, x_2)$  is a plane

Table 11-3 Steepest Ascent Experiment for Example 11-1

Steps	Coded Variables		Natural Variables		Response y
	$x_1$	$x_2$	$\xi_1$	$\xi_2$	
Origin	0	0	35	155	40.44 ✓
$\Delta$	1.00	0.42	5	2	
Origin + $\Delta$	1.00	0.42	40	157	41.0 ✓
Origin + 2 $\Delta$	2.00	0.84	45	159	42.9 ✓
Origin + 3 $\Delta$	3.00	1.26	50	161	47.1 ✓
Origin + 4 $\Delta$	4.00	1.68	55	163	49.7
Origin + 5 $\Delta$	5.00	2.10	60	165	53.8
Origin + 6 $\Delta$	6.00	2.52	65	167	59.9
Origin + 7 $\Delta$	7.00	2.94	70	169	65.0
Origin + 8 $\Delta$	8.00	3.36	75	171	70.4
Origin + 9 $\Delta$	9.00	3.78	80	173	77.6
Origin + 10 $\Delta$	10.00	4.20	85	175	80.3
Origin + 11 $\Delta$	11.00	4.62	90	179	76.2
Origin + 12 $\Delta$	12.00	5.04	95	181	75.1

Yield



New model needs to be employed around [85, 175] as we are outside the region you explored!