

ME 202

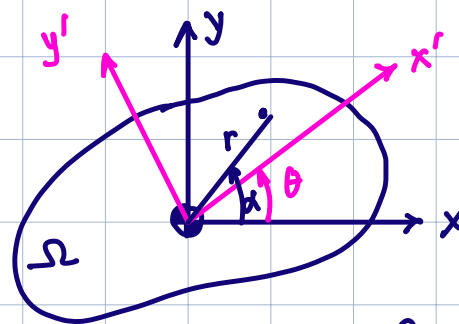
06 APR 2023

Unsymmetric Bending

Review on moment of inertia/second

moment of area

$\rho = 1$



Ω 2D planar c/s

● centroid

$$I_{xx} = \int_{\Omega} y^2 da,$$

$$I_{yy} = \int_{\Omega} x^2 da, \quad I_{xy} = - \int_{\Omega} xy da$$

$$x' = x \cos \theta + y \sin \theta$$

$$y' = -x \sin \theta + y \cos \theta$$

$$I_{x'x'} = I'_{xx} = \int_{\Omega} y'^2 da'$$

$$da' = J da$$

$$dx' dy' = J dx dy$$

$$J = \begin{vmatrix} \frac{\partial x'}{\partial x} & \frac{\partial x'}{\partial y} \\ \frac{\partial y'}{\partial x} & \frac{\partial y'}{\partial y} \end{vmatrix}$$

$$dx' = \cos \theta dx + \sin \theta dy$$

$$dy' = -\sin \theta dx + \cos \theta dy$$

$$J = \begin{vmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{vmatrix}$$

$$= 1$$

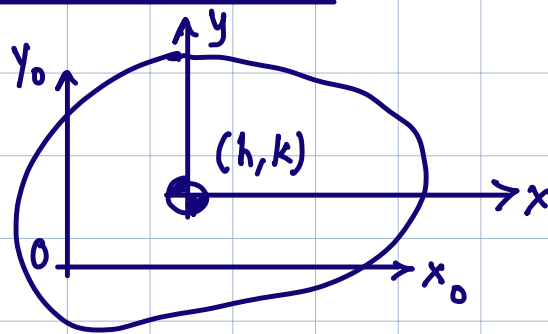
$$I'_{xx} = \int_{\Omega} (-x \sin \theta + y \cos \theta)^2 dx dy$$

$$= \sin^2 \theta \int_{\Omega} x^2 da + \cos^2 \theta \int_{\Omega} y^2 da - 2 \sin \theta \cos \theta \int_{\Omega} xy da$$

$$\begin{aligned}
 I_{xx}' &= I_{xx} \cos^2 \theta + I_{yy} \sin^2 \theta + 2 \sin \theta \cos \theta I_{xy} \\
 I_{yy}' &= I_{xx} \sin^2 \theta + I_{yy} \cos^2 \theta - 2 \sin \theta \cos \theta I_{xy} \\
 I_{xy}' &= (I_{yy} - I_{xx}) \sin \theta \cos \theta + I_{xy} (\cos^2 \theta - \sin^2 \theta)
 \end{aligned}$$

same as stress transf. rules

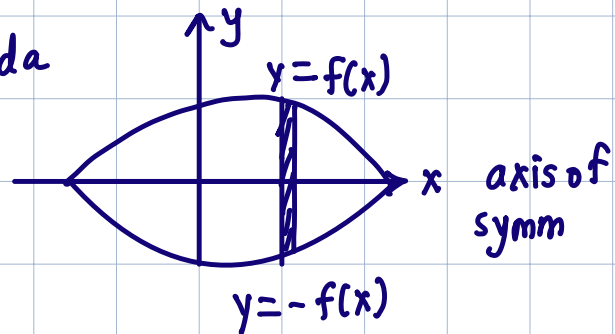
Parallel Axis Thm



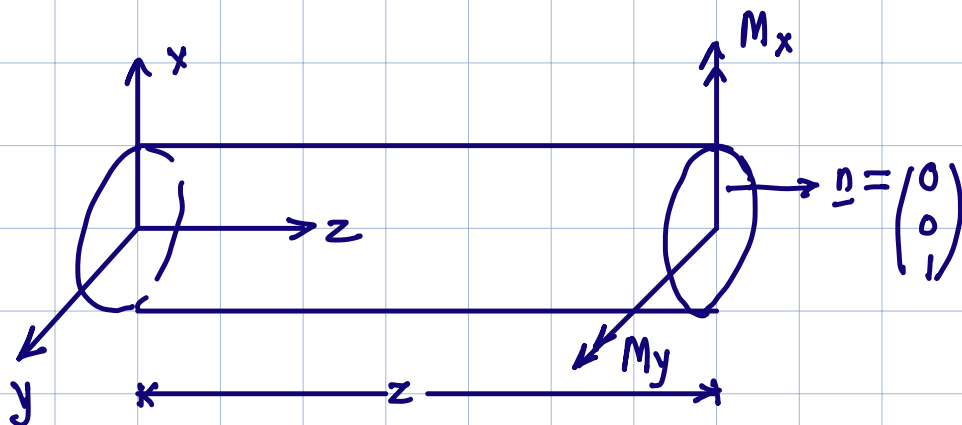
$$x = x_0 - h, \quad y = y_0 - k$$

$$\begin{aligned}
 I_{xx}^0 &= I_{xx} + A k^2, & I_{yy}^0 &= I_{yy} + A h^2 \\
 I_{xy}^0 &= I_{xy} - A h k
 \end{aligned}$$

$$I_{xy} = - \int_{\Omega} xy da$$



Return to Bending



$$\sigma_{zz} = (Ax + By) = E \epsilon_{zz} \quad \text{uniaxial}$$

$$\epsilon_{zz} = -x \frac{d^2 u}{dz^2} - y \frac{d^2 v}{dz^2}$$

u disp along x , v disp along y

$$\underline{t} = \underline{\sigma} \underline{n} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \sigma_{zz} \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

Eqm on c/s,

Force Eqm $\int_{\Omega} \underline{t} \, da = \underline{0}$

$$\underline{t} = \begin{pmatrix} \cancel{\sigma_{xz}} \\ \cancel{\sigma_{yz}} \\ \sigma_{zz} \end{pmatrix}^0 = \begin{pmatrix} 0 \\ 0 \\ \sigma_{zz} \end{pmatrix}$$

$$\int_{\Omega} \sigma_{zz} \, da = 0 \quad \text{equating } \underline{e}_z \text{ components}$$

$$A \int_{\Omega} x \, da + B \int_{\Omega} y \, da = 0$$

$\forall A, B$
 \uparrow
 for all

$\Rightarrow \left. \begin{matrix} x\text{-axis} \\ y\text{-axis} \end{matrix} \right\} \text{ centroidal axes}$

Moment Eqm on c/s

$$\int_{\Omega} (\underline{x} \times \underline{t}) \, da = M_x \underline{e}_x + M_y \underline{e}_y$$

$$\underline{e}_x (y \cancel{\sigma_{zz}} - z \cancel{\sigma_{zy}}) - \underline{e}_y (x \cancel{\sigma_{zz}} - z \cancel{\sigma_{zx}}) + \underline{e}_z (x \cancel{\sigma_{zy}} - y \cancel{\sigma_{zx}})$$

$$M_x = \int_{-h}^h y \sigma_{zz} dx dy \quad \text{Equating } e_x, e_y \text{ components}$$

$$M_y = - \int_{-h}^h x \sigma_{zz} dx dy$$

$$- \int_{-h}^h x (A x + B y) dx dy = M_y$$

$$-A I_{yy} + B I_{xy} = M_y$$

$$-A I_{xy} + B I_{xx} = M_x$$

known/given

calculated from geom

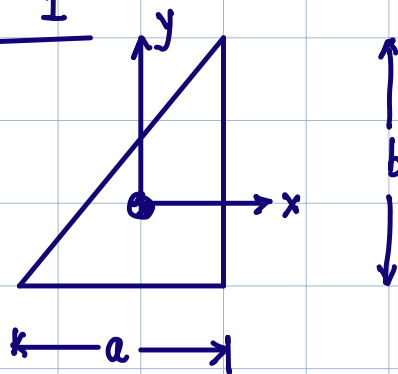
$$A = - \left(\frac{M_y I_{xx} - M_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) = -E \frac{d^2 u}{dz^2}$$

$$B = - \left(\frac{-M_x I_{yy} + M_y I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) = -E \frac{d^2 v}{dz^2}$$

Symm bending earlier

$$I_{xy} = 0, \quad M_y \neq 0, \quad M_x = 0, \quad A = -\frac{M_y}{I_{yy}}, \quad B = 0$$

Problem 1



c/s of a cantilever, $L = 1 \text{ m}$

$$\underline{M} = \begin{pmatrix} M_x \\ M_y \end{pmatrix} = \begin{pmatrix} 10 \text{ Nm} \\ 0 \end{pmatrix} \quad @ \quad z = L$$

Calculate max horiz and vert disp

$u_{\max}, \quad v_{\max}$

$$E = 100 \text{ GPa}, \quad a = 10 \text{ mm}, \quad b = 20 \text{ mm}$$

Obtain eqn of neutral line

Points on the triangle with max, min σ_{zz} .

$$\sigma_{zz} = Ax + By$$

$Ax + By = c$
family of
lines

neutral
line

$$\sigma_{zz} = 0$$

neutral
plane

