

TO DO LIST

- ☐ 2D axisymmetric problems
radial coordinates r
- ☐ Energy methods beam deflections
- ☐ Elastic instability buckling
- ☐ Unsymmetric bending
- ☐ Torsion, Back to Square One

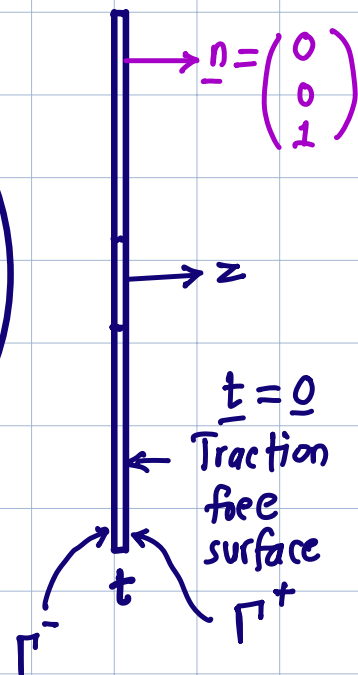
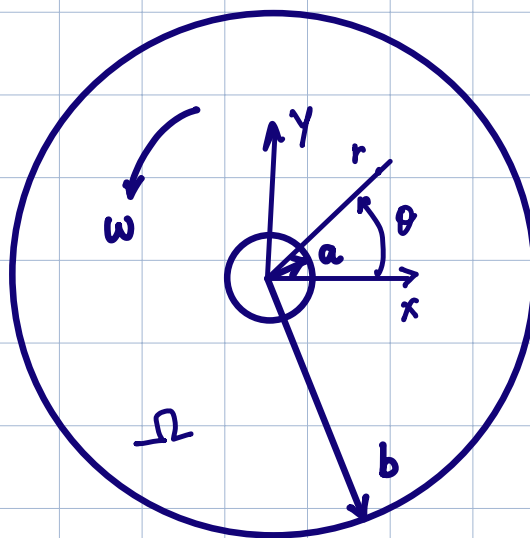
ME 202

TUE 28 FEB 2023

Ref:
Srinath
Sadd

In-plane
loading

$$t \ll a < b$$



3D \longrightarrow 2D \longrightarrow 1D* Axisymmetric
"Plane stress"

Cylindrical Coordinates r, θ, z

$$x = r \cos \theta, \quad y = r \sin \theta, \quad z = z$$

$$\underline{\underline{\sigma}} = \begin{pmatrix} \sigma_{rr} & \sigma_{r\theta} & \cancel{\sigma_{rz}} \\ \sigma_{\theta r} & \sigma_{\theta\theta} & \cancel{\sigma_{\theta z}} \\ \cancel{\sigma_{zr}} & \cancel{\sigma_{z\theta}} & \cancel{\sigma_{zz}} \end{pmatrix}$$

$\underline{t} = \underline{\underline{\sigma}} \underline{n}$ on Γ
 Static Equilibrium
 on a surface $\Sigma \underline{F} = \underline{0}$
 with normal \underline{n}

$$\begin{pmatrix} t_r \\ t_\theta \\ t_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \sigma_{rr} & \sigma_{r\theta} & \sigma_{rz} \\ & \sigma_{\theta\theta} & \sigma_{\theta z} \\ & & \sigma_{zz} \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

given

$$0 = \sigma_{rz} \cdot 1, \quad 0 = \sigma_{\theta z} \cdot 1, \quad 0 = \sigma_{zz} \cdot 1 \quad \text{on } \Gamma^+$$

$$0 = \sigma_{rz}(-1), \quad 0 = \sigma_{\theta z}(-1), \quad 0 = \sigma_{zz}(-1) \quad \text{on } \Gamma^-$$

$$\Rightarrow \sigma_{rz} = 0, \quad \sigma_{\theta z} = 0, \quad \sigma_{zz} = 0 \quad \text{in } \Omega$$

Plane stress assumption

In-plane loading only

Hooke's Law in 3D

$$\epsilon_{rr} = \frac{\sigma_{rr}}{E} - \frac{\nu}{E} (\sigma_{\theta\theta} + \cancel{\sigma_{zz}}) = \frac{\partial u_r}{\partial r}$$

$$\epsilon_{\theta\theta} = \frac{\sigma_{\theta\theta}}{E} - \frac{\nu}{E} (\sigma_{rr} + \cancel{\sigma_{zz}}) = \frac{1}{r} \left(u_r + \frac{\partial u_\theta}{\partial \theta} \right)$$

$$\epsilon_{zz} = \frac{\cancel{\sigma_{zz}}}{E} - \frac{\nu}{E} (\sigma_{rr} + \sigma_{\theta\theta}) = \frac{\partial u_z}{\partial z}$$

$$\epsilon_{rz} = \frac{1+\nu}{E} \cancel{\sigma_{rz}} = 0$$

$$\epsilon_{\theta z} = \frac{1+\nu}{E} \cancel{\sigma_{\theta z}} = 0$$

$$\epsilon_{r\theta} = \frac{1+\nu}{E} \sigma_{r\theta}$$

$$= \frac{1}{2} \left(\frac{1}{r} \frac{\partial u_r}{\partial \theta} + \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r} \right),$$

$$\underline{\epsilon} = \begin{pmatrix} \epsilon_{rr} & \epsilon_{r\theta} & 0 \\ \epsilon_{r\theta} & \epsilon_{\theta\theta} & 0 \\ 0 & 0 & \epsilon_{zz} \end{pmatrix}$$

$$\frac{\partial u_z}{\partial z} = -\frac{\nu}{E} (\sigma_{rr} + \sigma_{\theta\theta})$$

$$= -\frac{\nu}{E} (\sigma_{xx} + \sigma_{yy})$$

$$u_z \approx -\frac{\nu t}{E} (\sigma_{xx} + \sigma_{yy})$$

$$u_\theta = 0$$

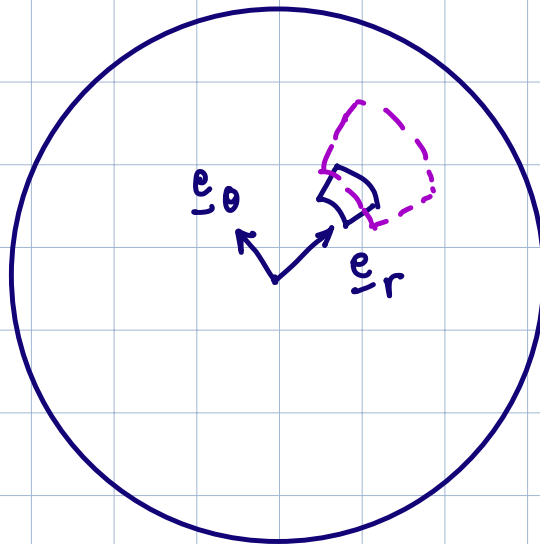
$$\frac{\partial \psi}{\partial \theta} = 0$$

$$grw^2$$

$$\frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_{r\theta}}{\partial \theta} + \frac{\partial \sigma_{zr}}{\partial z} + \frac{1}{r} (\sigma_{rr} - \sigma_{\theta\theta}) + b_r = 0$$

$$\frac{\partial \sigma_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_{\theta\theta}}{\partial \theta} + \frac{\partial \sigma_{\theta z}}{\partial z} + \frac{2}{r} \sigma_{r\theta} + b_\theta = 0 \quad \checkmark$$

$$\frac{\partial \sigma_{rz}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_{\theta z}}{\partial \theta} + \frac{\partial \sigma_{zz}}{\partial z} + \frac{1}{r} \sigma_{rz} + b_z = 0 \quad \checkmark$$



$$\frac{d}{dr} \sigma_{rr} + \frac{1}{r} (\sigma_{rr} - \sigma_{\theta\theta}) + grw^2 = 0 \quad r\text{-direction}$$

Stress FormulationODE in $\tau_{rr}(r)$

Depends on BCs.

Displacement FormulationODE in $u_r(r)$ ① Spinning freely at constant ω
Ensemble

BCs

Inner radius traction free

Outer || @ $r=a$.

$$\underline{n} = \begin{pmatrix} -1 \\ 0 \\ 0 \end{pmatrix} \left. \vphantom{\begin{pmatrix} -1 \\ 0 \\ 0 \end{pmatrix}} \right\} \text{ in } r, \theta, z \text{ coords}$$

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \tau_{rr} & \tau_{r\theta} \\ \tau_{r\theta} & \tau_{\theta\theta} \end{pmatrix} \begin{pmatrix} -1 \\ 0 \end{pmatrix} \quad \underline{t} = \underline{\mathcal{L}} \underline{n}$$

$$\Rightarrow 0 = \tau_{rr}(-1) \Rightarrow \tau_{rr}(a) = 0$$

$$\tau_{rr}(b) = 0$$

Aside $w=0$, internal pressure = p_a
external pressure = p_b

$$\underline{t} = \underline{\sigma} \underline{n} \Rightarrow \begin{pmatrix} +p_a \\ 0 \end{pmatrix} = \begin{pmatrix} \tau_{rr} & 0 \\ 0 & \tau_{\theta\theta} \end{pmatrix} \begin{pmatrix} -1 \\ 0 \end{pmatrix}$$

$$\tau_{rr}(a) = -p_a$$

$$\tau_{rr}(b) = -p_b$$

$$u(r) = u_r(r)$$

$$\epsilon_{rr} = \frac{1}{E} (\tau_{rr} - \nu \tau_{\theta\theta}) = \frac{du}{dr}$$

$$\epsilon_{\theta\theta} = \frac{u}{r} = \frac{1}{E} (\tau_{\theta\theta} - \nu \tau_{rr})$$

$$u = \frac{r}{E} (\tau_{\theta\theta} - \nu \tau_{rr}) \Rightarrow \frac{du}{dr} =$$

$$\Rightarrow \tau_{\theta\theta} = \tau_{rr} + \nu \tau_{rr}'$$

$$' \equiv \frac{d}{dr}$$

←
equate
↓

plug into eqn

$$r \frac{d^2 \sigma_{rr}}{dr^2} + 3 \frac{d\sigma_{rr}}{dr} = 0$$

$$\sigma_{rr} = C_1 + \frac{C_2}{r^2}, \quad \sigma_{\theta\theta} = C_1 - \frac{C_2}{r^2}$$

C_1, C_2 from TBCs on σ_{rr}

$$\sigma_{rr} = \frac{p_a a^2 - p_b b^2}{b^2 - a^2} - \frac{a^2 b^2}{r^2} \left(\frac{p_a - p_b}{b^2 - a^2} \right)$$

$$\sigma_{\theta\theta} = \underbrace{\quad} + \underbrace{\quad}$$

$$u = \frac{1-\nu}{E} \frac{p_a a^2 - p_b b^2}{b^2 - a^2} r + \frac{1+\nu}{E} \frac{a^2 b^2}{r^2} \frac{p_a - p_b}{b^2 - a^2}$$

Displacement Approach

Invert Hooke's Law

$$\begin{cases} \tau_{rr} = \frac{E}{1-\nu^2} \left(\epsilon_{rr} + \nu \epsilon_{\theta\theta} \right) \\ \tau_{\theta\theta} = \frac{E}{1-\nu^2} \left(\epsilon_{\theta\theta} + \nu \epsilon_{rr} \right) \end{cases}$$

→ Into eqn

$$\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} - \frac{u}{r^2} = 0$$

$$\frac{d}{dr} \left[\frac{1}{r} \frac{d}{dr} (ur) \right] = 0$$

$$u = C_1 r + \frac{C_2}{r}$$

Useful for DBCs.