

Shear Stresses in Beams Due to Shear Force

Shear Stress in Beam Due To Bending

Moment & shear force

$V = V_x$

$M = M_y$

BOTE (Back of the envelope) shear stress traction free

$$\tau_{zx} = \frac{V}{A}$$

want variation

2D Equilibrium in $z-x$ plane with no body force

$$\frac{\partial \tau_{zz}}{\partial z} + \frac{\partial \tau_{zx}}{\partial x} + \frac{\partial \tau_{zy}}{\partial y} = 0 \quad \begin{matrix} \text{no action} \\ \text{along } y\text{-dir.} \end{matrix}$$

$M(z) = BM \text{ at } z, \quad V(z) = SF \text{ at } z, \quad M' = -V$

$\tau_{zz} = -\frac{M(z)}{I} x \quad M(z) = M_y$

$I = I_{yy}$

$$\frac{\partial \tau_{zz}}{\partial z} = -\frac{x}{I} \frac{dM}{dz} = \frac{Vx}{I}$$

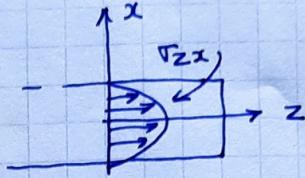
$\Rightarrow \frac{\partial \tau_{zx}}{\partial x} = -\frac{Vx}{I}$ from equilibrium

$\tau_{zx} = -\frac{V(z)}{I} \frac{x^2}{2} + f(z)$

$\tau_{zx}(x = \pm \frac{h}{2}) = 0$

$$0 = -\frac{V(z)}{I} \frac{h^2}{4} + f(z) \Rightarrow f(z) = \frac{V(z)}{I} \frac{h^2}{4}$$

$$\tau_{zx} = \frac{V(z)}{2I} \left(\frac{h^2}{4} - x^2 \right)$$



quadratic/parabolic profile/distribution

$$\text{Max } \tau_{zx}^{\max} = \frac{V}{2 \cdot \frac{bh^3}{12}} \cdot \frac{h^2}{4} = \frac{3}{2} \frac{V}{bh} = \frac{3}{2} \frac{V}{A}$$

$$= 1.5 \tau_{zx}^{\text{avg}}$$

for rectangular c/s

Also, resultant shear force

$$\text{check } \int_{-h/2}^{h/2} \tau_{zx} \cdot b dx = \frac{bV}{2I} \int_{-h/2}^{h/2} \left(\frac{h^2}{4} - x^2 \right) dx$$

$$= \frac{b \cdot V}{2 \cdot \frac{bh^3}{12}} \frac{h^3}{6}$$

$$= V \quad \text{makes sense. sanity check.}$$

Resultant of τ_{zx} should add upto V .

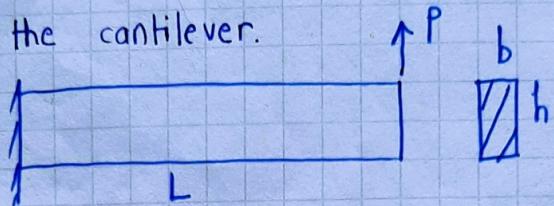
Weak form of TBC

$$\int_{-h/2}^{h/2} b \tau_{zx} dx = V$$

Use this insight + the fact that τ_{zx} varies parabolically to calculate $\tau_{zx}(z, x)$ for other c/s.

How big is σ_{zx} vs σ_{zz} ? When can it be ignored?

Consider the cantilever.



$$M(z) = P(L-z) \quad V(z) = P$$

$$\sigma_{zz} = -\frac{M}{I} \cdot x = -\frac{P(L-z)}{bh^3/12} \cdot x$$

$$\sigma_{zx} = \frac{V}{2I} \left(\frac{h^2}{4} - x^2 \right) = \frac{P}{2bh^3/12} \left(\frac{h^2}{4} - x^2 \right)$$

Compare σ_{zz}^{\max} to σ_{zx}^{\max} (not occurring at same point)

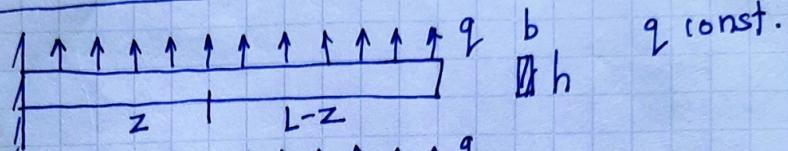
$$\sigma_{zz}^{\max} = \underbrace{\frac{P}{I}L}_{\frac{1}{2}} \frac{h}{2}, \quad \sigma_{zx}^{\max} = \underbrace{\frac{P}{(2I)}}_{\frac{1}{4}} \frac{h^2}{4}$$

$Lh \gg h^2/4$ for thin beams

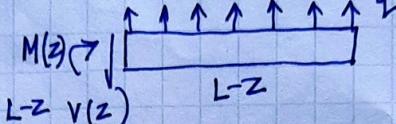
$\sigma_{zz}^{\max} \gg \sigma_{zx}^{\max}$ for thin beams

↑
can be safely ignored.

Relative strength of all σ_{zz} , σ_{zx} , σ_{xx} for cantilever with UDL.



q const.



$$V(z) = \int_0^{L-z} q(\xi) d\xi = q(L-z)$$

$$M(z) = \int_0^{L-z} q(\xi) \xi d\xi = \frac{q}{2} [\xi^2]_0^{L-z} = \frac{q}{2} (L-z)^2 = q(L-z) \frac{(L-z)}{2}$$

check $V' = -q = -q(z) \checkmark$

$$M' = -\frac{q}{2} 2(L-z) = -V(z) \checkmark$$

$$\sigma_{zz} = -\frac{M(z) x}{I}, \quad \sigma_{zx} = \frac{V(z)}{2I} \left(\frac{h^2}{4} - x^2 \right)$$

$$\sigma_{xx} = \frac{q(z)}{2I} \left(\frac{h^2}{4} x - \frac{x^3}{3} \right), \quad V_{max} = qL$$

$$q_{max} = q, \quad M_{max} = qL^2/2$$

All max not at same point
(0, x) but in any case

$$\sigma_{zz}^{max} = \frac{qL^2}{2} \cdot \frac{h}{2} \cdot \frac{12}{bh^3} = 3 \frac{q}{b} \left(\frac{L}{h} \right)^2$$

$$\sigma_{zx}^{max} = \frac{qL}{2} \cdot \frac{12}{bh^3} \cdot \frac{h^2}{4} = \frac{3}{2} \frac{q}{b} \left(\frac{L}{h} \right)^1$$

$$\sigma_{xx}^{max} = \frac{q}{2b} = \frac{1}{2} \frac{q}{b} \left(\frac{L}{h} \right)^0$$

for thin beam, $L \gg h$, $(L/h)^2 \gg (L/h)^1 \gg (L/h)^0$

$$\sigma_{zz}^{max} \gg \sigma_{zx}^{max} \gg \sigma_{xx}^{max}$$