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ME 202

10 APR 2023

TORSION OF PRISMATIC SHAFTS (Non-circular cross-sections)

Refs □ Advanced Mechanics of Solids
Srinath

□ Elasticity: Theory, Application, Numerics
Sadd

Goal:



Airfoil cross-section

Torsional stiffness

$$T = K_t \alpha$$

↑

goal of theory

$$\theta = \alpha L$$

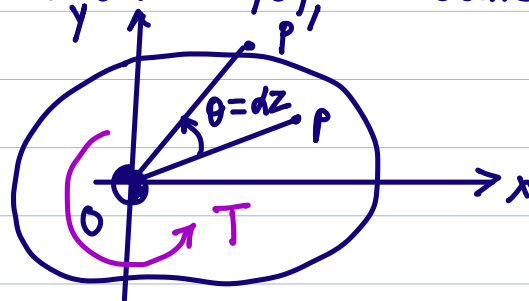
Torsion of Non-circular cross-sections

- Angle of Twist
- T_{\max} for safe operation c/s Wing / Turbine blade

Theory based on circular c/s, at some z .

⊙ centroid

origin here for now.



$$OP = OP'$$

$\theta = \alpha z$, α unit angle of twist
small angles. rad/m

Applied torque $\underline{T} = T \underline{e}_z$

$$u = -\alpha y z$$

$$v = +\alpha x z$$

$$w = w(x, y) \text{ warping.}$$



from expt observations

or prove formally $w \neq 0$ for non-circ c/s later.

Ang. Disp α \rightarrow Strains \rightarrow Stresses \rightarrow Torque T

$$\text{Goal: } T = K_t \alpha$$

\uparrow
Torsional stiffness (G , geometry)

Stress Formulation

$$\epsilon_{xx} = \frac{\partial u}{\partial x} = 0, \quad \epsilon_{yy} = \frac{\partial v}{\partial y} = 0$$

$$\epsilon_{xy} = \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) = 0$$

$$\epsilon_{zz} = \frac{\partial w}{\partial z} = 0$$

$$\epsilon_{zx} = \frac{1}{2} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) = \frac{1}{2} \left(\frac{\partial w}{\partial x} - \alpha y \right)$$

$$\epsilon_{zy} = \frac{1}{2} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) = \frac{1}{2} \left(\frac{\partial w}{\partial y} + \alpha x \right)$$

Stresses Hooke's Law

$$\sigma_{zx} = 2G \epsilon_{zx} = G \left(\frac{\partial w}{\partial x} - \alpha y \right)$$

$$\sigma_{zy} = 2G \epsilon_{zy} = G \left(\frac{\partial w}{\partial y} + \alpha x \right)$$

All other stresses zero.

Equilibrium

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xz}}{\partial z} + b_x = 0 \quad \checkmark$$

$$\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{yz}}{\partial z} + b_y = 0 \quad \checkmark$$

$$\frac{\partial \sigma_{xz}}{\partial x} + \frac{\partial \sigma_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + b_z = 0$$

$$\frac{\partial \sigma_{xz}}{\partial x} + \frac{\partial \sigma_{yz}}{\partial y} = 0 \quad (1) \quad \text{Eqm}$$

Need another equation.

$$\frac{\partial \sigma_{yz}}{\partial x} = G \left(\frac{\partial^2 w}{\partial x \partial y} + \alpha \right), \quad \frac{\partial \sigma_{xz}}{\partial y} = G \left(\frac{\partial^2 w}{\partial x \partial y} - \alpha \right)$$

$$\frac{\partial \sigma_{zx}}{\partial y} - \frac{\partial \sigma_{zy}}{\partial x} = -2G\alpha \quad (2)$$

Hooke's Law +
Strain Disp.

Need to solve (1), (2)

2 PDEs of 1st order \rightarrow 1 PDE of 2nd order

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Introduce a scalar function $\varphi(x,y)$. Standard
Prandtl stress function technique

$$\tau_{xz} = \frac{\partial \varphi}{\partial y}, \quad \tau_{yz} = -\frac{\partial \varphi}{\partial x}$$

"potential theory"

(1) Eqm is automatically taken care of.

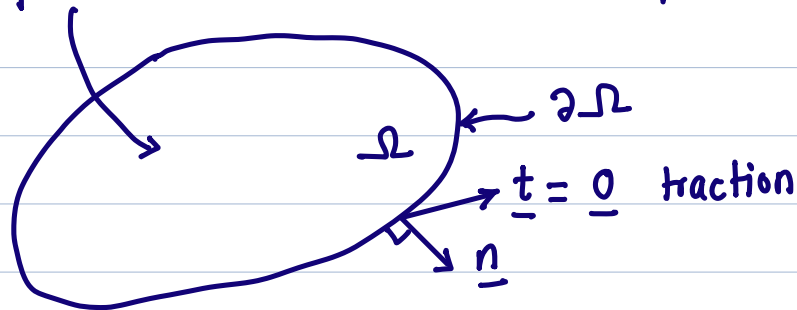
Need to solve (2)

$$\frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial y^2} = -2G\alpha \quad \text{in } \Omega$$

$$\nabla^2 \varphi = -2G\alpha$$

Poisson Eqn in Ω

given
 Ω : c/s of
shaft



Need $\varphi(x,y)$

What are BCs on $\partial\Omega$? Lateral surface
of shaft

Traction Free $\underline{t} = \underline{\sigma} \underline{n}$

$$\begin{pmatrix} t_x \\ t_y \\ t_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} 0 & 0 & \tau_{xz} \\ 0 & 0 & \tau_{yz} \\ \tau_{xz} & \tau_{yz} & 0 \end{pmatrix} \begin{pmatrix} n_x \\ n_y \\ 0 \end{pmatrix} \quad \begin{matrix} \checkmark \\ \checkmark \\ \checkmark \leftarrow BC \end{matrix}$$

given traction free

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$$t_z = 0 \Rightarrow \sigma_{xz} n_x + \sigma_{yz} n_y = 0$$

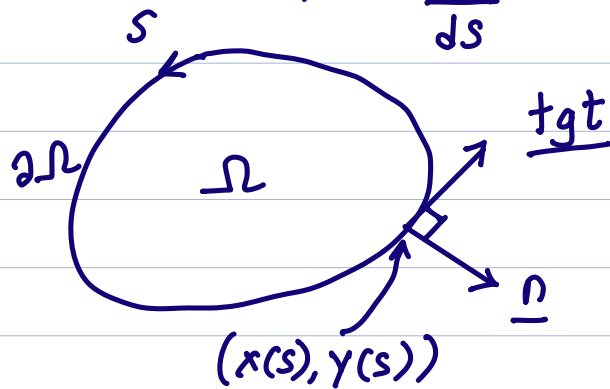
$$\frac{\partial \varphi}{\partial y} \frac{dy}{ds} - \frac{\partial \varphi}{\partial x} \left(-\frac{dx}{ds} \right) = 0, \quad n_x = \frac{dy}{ds}$$

$$n_y = -\frac{dx}{ds}$$

$$\frac{d\varphi}{ds} = 0 \quad \text{along } \partial\Omega$$

$$\underline{\text{tgt}} = \left(\frac{dx}{ds}, \frac{dy}{ds} \right)$$

$$\underline{n} = \underline{\text{tgt}} \times \underline{e}_z$$



$$\begin{aligned} &= \left(\frac{dx}{ds} \underline{e}_x + \frac{dy}{ds} \underline{e}_y \right) \times \underline{e}_z \\ &= \left(\frac{dy}{ds} \underline{e}_x - \frac{dx}{ds} \underline{e}_y \right) \end{aligned} \quad \underbrace{\frac{\partial \varphi}{\partial x} \frac{dx}{ds} + \frac{\partial \varphi}{\partial y} \frac{dy}{ds}}_{\substack{\text{on } \partial\Omega \\ \frac{d\varphi}{ds} = 0}} = 0$$

$$\frac{d\varphi}{ds} = 0 \quad \text{along } \partial\Omega \Rightarrow \varphi = c \quad \text{on } \partial\Omega$$

constant

Arb set $c = 0$

$$\text{alt, } \Phi = \varphi - c = 0 \quad \text{on } \partial\Omega$$

Torsion Problem Find $\varphi(x, y)$ s.t.
 Poisson's Eqn $\nabla^2 \varphi = -2G\alpha$ in Ω
 with $\varphi = 0$ on $\partial\Omega$
 Dirichlet BC

$$T = \int_{\Omega} (x \sigma_{yz} - y \sigma_{xz}) dx dy$$

$$T = - \int_{\Omega} \left(x \frac{\partial \varphi}{\partial x} + y \frac{\partial \varphi}{\partial y} \right) dx dy \rightarrow (*)$$

An easier way to write (*) is by applying
 Green / Gauss / Div Thm.

$$\frac{\partial}{\partial x} (\varphi x) = x \frac{\partial \varphi}{\partial x} + \varphi, \quad \frac{\partial}{\partial y} (\varphi y) = y \frac{\partial \varphi}{\partial y} + \varphi$$

$$T = - \int_{\Omega} \left(\frac{\partial}{\partial x} (\varphi x) + \frac{\partial}{\partial y} (\varphi y) \right) dx dy + 2 \int_{\Omega} \varphi dx dy$$

$\underbrace{\hspace{10em}}_{\text{div} \begin{pmatrix} \varphi x \\ \varphi y \end{pmatrix}}$

$$= - \int_{\partial\Omega} (\varphi_x n_x + \varphi_y n_y) ds + 2 \int_{\Omega} \varphi dx dy$$

$\xrightarrow{\text{orange arrow}} 0$
 $\varphi = 0$ on $\partial\Omega$ TBC

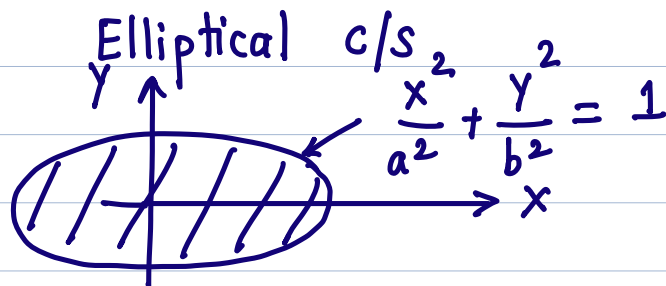
$$T = 2 \int_{\Omega} \varphi dx dy$$

Div Thm

$$\int_{\Omega} \nabla \cdot \underline{\Psi} \, dx dy = \int_{\partial \Omega} \underline{\Psi} \cdot \underline{n} \, ds$$

$$T = 2 \int_{\Omega} \varphi \, dx dy$$

Example



Try $\varphi(x,y) = K \left(\frac{x^2}{a^2} + \frac{y^2}{b^2} - 1 \right)$ $\varphi = 0$ on $\partial \Omega$ ✓

$$\nabla^2 \varphi = -2Gd \Rightarrow \frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial y^2} = -2Gd$$

$$K \left(\frac{2}{a^2} + \frac{2}{b^2} \right) = -2Gd \Rightarrow K = -\frac{Gd a^2 b^2}{a^2 + b^2} \checkmark$$

$$T = 2 \int_{\Omega} \varphi \, dx dy = 2K \int_{\Omega} \left(\frac{x^2}{a^2} + \frac{y^2}{b^2} - 1 \right) dx dy$$

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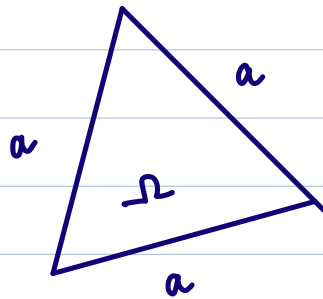
$$T = \frac{\pi a^3 b^3 G \alpha}{a^2 + b^2}$$

Torsional stiffness

$$\alpha = \frac{T(a^2 + b^2)}{\pi a^3 b^3 G}$$

can be expt verified
in a lab

Problem Equilateral Triangle Cross-section



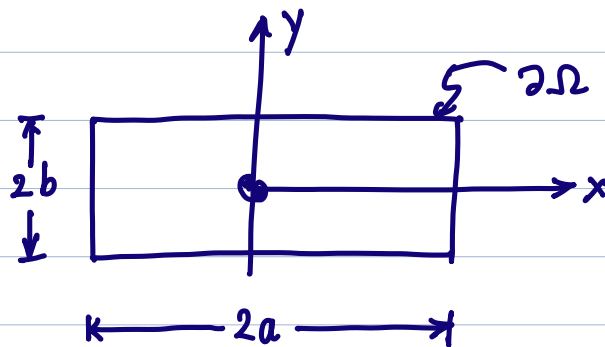
Goal $T = K_t \alpha$

Find $\varphi(x, y)$ s.t. $\nabla^2 \varphi = -2G\alpha$ inside Ω

$\varphi = 0$ on $\partial\Omega$

$\varphi = K \underbrace{F(x, y)}$

$T = 2 \int_{\Omega} \varphi \, da$



Try Same trick $\varphi(x, y) = K(x-a)(x+a)(y-b)(y+b)$
 $= K(x^2 - a^2)(y^2 - b^2)$

$\varphi = 0$ on $\partial\Omega$

↓
Does not work

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$$\nabla^2 \varphi = \frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial y^2} = K(y^2 - b^2) + K(x^2 - a^2)$$

$$\neq -2Gd \quad \forall x, y \in \Omega$$

↑
for all

Work: Fourier series

Consider, thin rectangle $a \gg b$

