

Bending  $\sigma_{zz} = -\frac{Mx}{I} = \frac{32M}{\pi D^3}$ ,  $I = \frac{J}{2}$

Torsion  $\sigma_{xz} = -G\alpha y = 0$ ,  $\sigma_{yz} = +G\alpha x = -\frac{16T}{\pi D^3}$

$\sigma_{yy} = 0$  locally yz plane 2D stress

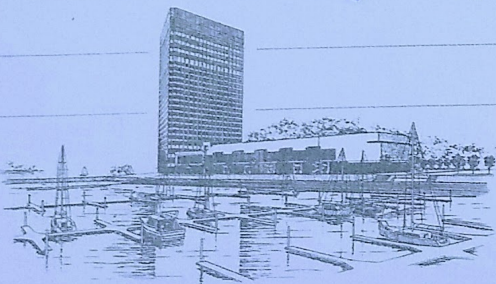
$\sigma_N^{\max} = \frac{\sigma_{zz} + \sigma_{yy}}{2} + \sqrt{\left(\frac{\sigma_{zz} - \sigma_{yy}}{2}\right)^2 + \sigma_{zy}^2}$

Plug in  $M = 4000 \times 10^3 \text{ Nmm}$ ,  $T = 2000 \times 10^3 \text{ Nmm}$   
 $\sigma_y = 500 \text{ N/mm}^2$  to get  
 $D = 44.191 \text{ mm}$

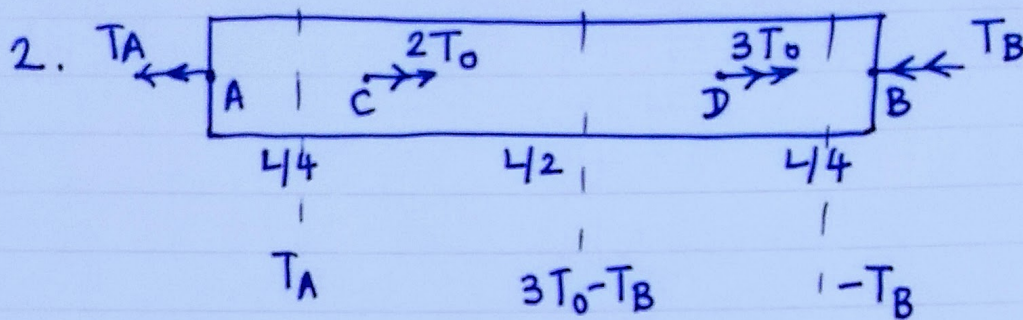
$\sigma_s^{\max} = \sqrt{\left(\frac{\sigma_{zz} - \sigma_{yy}}{2}\right)^2 + \sigma_{zy}^2} = \frac{\sigma_y}{2}$  max shear stress theory

Plug in given values to get  
 $D = 44.997 \text{ mm}$

In practice, choose  
 $D = \max(44.191, 44.997)$   
 $\approx 45 \text{ mm dia shaft}$







$$\text{Torque Balance} \Rightarrow T_A + T_B = 5T_0 \Rightarrow T_A = 5T_0 - T_B$$

$$\text{Total angular deflection} = 0$$

$$\Rightarrow \underbrace{\frac{(5T_0 - T_B)L}{GJ} \frac{1}{4}}_{\theta_{CA}} + \underbrace{\frac{(3T_0 - T_B)L}{GJ} \frac{1}{2}}_{\theta_{DC}} + \underbrace{\frac{(-T_B)L}{GJ} \frac{1}{4}}_{\theta_{BD}} = 0$$

$$\theta_{XY} \equiv \theta @ X \text{ wrt } Y = \theta_X - \theta_Y$$

$$\text{solve } T_B = 11T_0/4, T_A = 5T_0 - T_B = 9T_0/4$$

$$\theta_{CA} = \frac{(5T_0 - T_B)L}{GJ} \frac{1}{4} = \frac{9}{16} \frac{T_0 L}{GJ} = \theta_C$$

$$\theta_{DC} = \frac{(3T_0 - T_B)L}{GJ} \frac{1}{2} = \frac{T_0 L}{8GJ}$$

$$\theta_{DA} = \left( \frac{9}{16} + \frac{1}{8} \right) \frac{T_0 L}{GJ} = \frac{11T_0 L}{16GJ}$$

