

Supplementary Document

Asymptotically Stabilizing Virtual Constraint Controllers for Multi-Domain Periodic Gaits of 3D Quadruped Locomotion*

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PROOF OF THEOREM 1

Proof: For the continuous-time domain $v \in \mathcal{V}$, let us define the flow map according to the following policy

$$\mathcal{F}_v(x, \xi_v) := \varphi_v(T_v(x, \xi_v); x, \xi_v) \quad (22)$$

that represents the state solution $\varphi_v(t; x, \xi_v)$ evaluated on the switching manifold $\hat{\mathcal{S}}_{v \rightarrow \mu(v)}(\xi_v)$. For single-contact domains $v \in \mathcal{V}$, the decoupling matrix $A_v(x, \xi_v)$ in (13) is square and assumed to be full-rank on an open neighborhood of $\bar{\mathcal{O}}_v$ for every $\xi_v \in \Xi_v$. Hence, the feedback driving $y_v(x, \xi_v)$ to zero is unique on each zero dynamics manifold $\mathcal{Z}_v(\xi_v)$. According to the construction procedure, the orbit $\bar{\mathcal{O}}_v$ is also common to all zero dynamics manifolds, i.e., $\bar{\mathcal{O}}_v \subset \mathcal{Z}_v(\xi_v)$ for all $\xi_v \in \Xi_v$. Therefore, the control restricted to the orbit $\bar{\mathcal{O}}_v$ is independent of ξ_v , i.e.,

$$\left. \frac{\partial}{\partial \xi_v} \Gamma_v(x, \xi_v) \right|_{\bar{\mathcal{O}}_v} = 0. \quad (23)$$

This together with [1, Lemma 1] shows that $\bar{\mathcal{O}}_v$ is an invariant integral curve of $\dot{x} = f_v^{\text{cl}}(x, \xi_v)$ for all $\xi_v \in \Xi_v$. If we define the initial and final states on the orbit $\bar{\mathcal{O}}_v$ as x_{0v}^* and x_{fv}^* , respectively, one can conclude that

$$\mathcal{F}_v(x_{0v}^*, \xi_v) = x_{fv}^*, \quad \forall \xi_v \in \Xi_v. \quad (24)$$

We also remark that

$$\{x_{fv}^*\} := \bar{\mathcal{O}}_v \cap \hat{\mathcal{S}}_{v \rightarrow \mu(v)}(\xi_v), \quad \forall \xi_v \in \Xi_v. \quad (25)$$

For multi-contact domains $v \in \mathcal{V}$, the decoupling matrix $A_v(x, \xi_v)$ in (9) is not square and the feedback deriving $y_v(x, \xi_v)$ to zero is not unique. In fact, the I-O linearizing control (11) presents the minimum 2-norm solution that solves the output zeroing problem, i.e.,

$$\begin{aligned} \Gamma_v(x, \xi_v) &= \underset{u}{\operatorname{argmin}} \frac{1}{2} \|u\|_2^2 \\ \text{s.t.} \quad & A_v(x, \xi_v) u + b_v(x, \xi_v) = -w_v. \end{aligned}$$

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From Assumption 3, there is a nominal controller parameter ξ_v^* for which the minimum 2-norm solution $\Gamma_v(x, \xi_v)$ coincides with the nominal control trajectory, i.e.,

$$\Gamma_v(x^*(t, v), \xi_v) = u^*(t, v). \quad (26)$$

In other words, $\bar{\mathcal{O}}_v$ is an integral curve of the closed-loop ODE $\dot{x} = f_v^{\text{cl}}(x, \xi_v^*)$. Consequently,

$$\mathcal{F}_v(x_{0v}^*, \xi_v^*) = x_{fv}^*. \quad (27)$$

Next, let us define the mapping $\mathcal{G}_v: \Xi_v \rightarrow \mathbb{R}^{2n_q}$ by

$$\mathcal{G}_v(\xi_v) := \mathcal{F}_v(x_{0v}^*, \xi_v) - x_{fv}^*. \quad (28)$$

From the transversality assumption and [1, Theorem 2], one can show that \mathcal{G}_v is differentiable with respect to ξ_v at $\xi_v = \xi_v^*$. This latter fact together with $\mathcal{G}_v(\xi_v^*) = 0$ and $p_v = \dim(\xi_v) > \dim(\mathcal{G}_v) = 2n_q$ implies that there is a nonempty set $\hat{\Xi}_v \subset \Xi_v$ such that (i) $\xi_v^* \in \hat{\Xi}_v$ and (ii) $\mathcal{G}_v(\xi_v) = 0$ for all $\xi_v \in \hat{\Xi}_v$, or equivalently,

$$\mathcal{F}_v(x_{0v}^*, \xi_v) = x_{fv}^*, \quad \forall \xi_v \in \hat{\Xi}_v. \quad (29)$$

Equation (29) also implies that

$$P_v(x_{f\mu^{-1}(v)}^*, \xi_v) = x_{fv}^*, \quad \forall \xi_v \in \hat{\Xi}_v \quad (30)$$

which in turn results in the existence of an invariant fixed point x_1^* for the full-order Poincaré map $P(x, \xi)$. In particular, $P(x_1^*, \xi) = 0$ for all $\xi \in \hat{\Xi}$, where $x_1^* := x_{fv_1}^*$ and $\hat{\Xi} := \hat{\Xi}_{v_1} \times \cdots \times \hat{\Xi}_{v_N}$. The continuous differentiability of the Jacobian matrix $\Psi(\xi)$ with respect to ξ follows from [1, Theorem 2]. ■

REFERENCES

- [1] K. Akbari Hamed, B. Buss, and J. Grizzle, “Exponentially stabilizing continuous-time controllers for periodic orbits of hybrid systems: Application to bipedal locomotion with ground height variations,” *The International Journal of Robotics Research*, vol. 35, no. 8, pp. 977–999, 2016.