

For the beam and loading shown, determine the spring constant k for which the bending moment at B is $MB = -wL/10$.

$$M - \int_0^x \omega d\xi + \omega L + V = 0$$

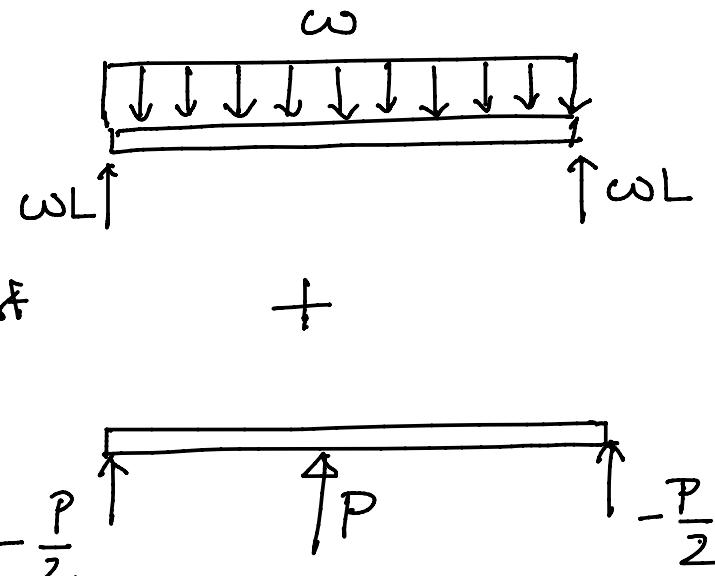
$$\Rightarrow V(x) = -\omega L + \omega x.$$

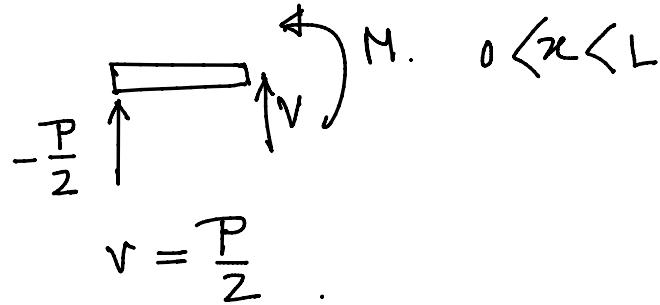
$$-\int_0^x (\omega d\xi) \xi + Vx + M = 0$$

$$\Rightarrow -\frac{\omega x^2}{2} + (\omega x - \omega L)x + M = 0$$

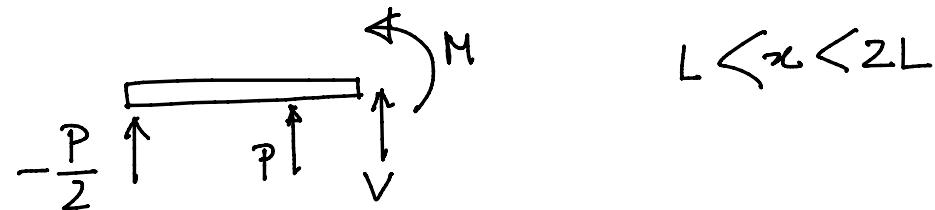
$$\Rightarrow M(x) = \omega L x - \frac{\omega x^2}{2}.$$

Separate problem into 2 parts and find the support reactions.





$$\begin{aligned} Vx + M &= 0 \\ \Rightarrow M &= -Vx = -\frac{P}{2}x. \end{aligned}$$



$$V + P - \frac{P}{2} = 0 \Rightarrow V = -\frac{P}{2}$$

$$PL + Vx + M = 0$$

$$\Rightarrow PL - \frac{P}{2}x + M = 0 \Rightarrow M = \frac{P}{2}x - PL.$$

Combined problem:

$$0 < x < L$$

$$M(x) = \omega Lx - \frac{\omega x^2}{2} - \frac{P}{2}x.$$

$$EI\vartheta'' = -\frac{\omega}{2}x^2 + \omega Lx - \frac{P}{2}x.$$

$$EI\vartheta' = -\frac{\omega}{6}x^3 + \frac{\omega Lx^2}{2} - \frac{P}{4}x^2 + C_1$$

$$EIv = -\frac{\omega}{24}x^4 + \frac{\omega Lx^3}{6} - \frac{P}{12}x^3 + C_1x + C_2$$

$$L < x < 2L$$

$$M(x) = \omega Lx - \frac{\omega x^2}{2} + \frac{P}{2}x - PL$$

$$EI\vartheta'' = -\frac{\omega x^2}{2} + \omega Lx + \frac{P}{2}x - PL.$$

$$EI\vartheta' = -\frac{\omega x^3}{6} + \frac{\omega Lx^2}{2} + \frac{Px^2}{4} - PLx + D_1$$

$$EIv = -\frac{\omega x^4}{24} + \frac{\omega Lx^3}{6} + \frac{Px^3}{12} - \frac{PLx^2}{2} + D_1x + D_2$$

ϑ is positive upwards. For positive ϑ , spring force P is downwards.

$$\text{Hence } P = -k\vartheta(L)$$

Because of symmetry, slope should be zero at $x=L$

$$\therefore -\frac{\omega}{6}L^3 + \frac{\omega}{2}L^3 - \frac{P}{4}L^2 + C_1 = 0 \Rightarrow C_1 = \frac{P}{4}L^2 - \frac{\omega}{3}L^3$$

$$\text{At } x=0, \text{ displacement is } 0 \Rightarrow C_2 = 0$$

$$\therefore EI\vartheta = -\frac{\omega}{24}x^4 + \frac{\omega Lx^3}{6} - \frac{P}{12}x^3 + \left(\frac{P}{4}L^2 - \frac{\omega}{3}L^3\right)x \Rightarrow \vartheta(L) = -\frac{\frac{5}{24}\omega L^4 + \frac{PL^3}{6}}{EI}$$

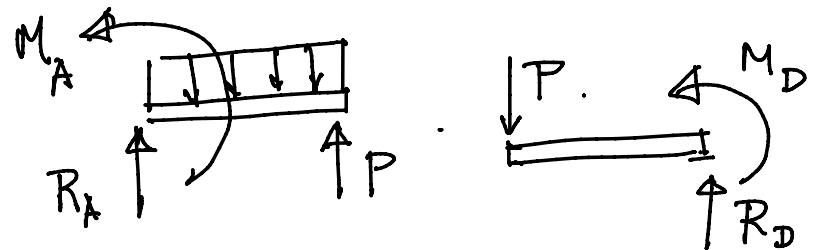
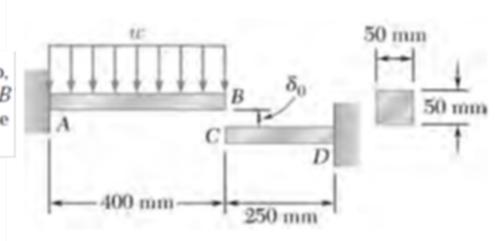
$$M(x) = \omega Lx - \frac{\omega x^2}{2} - \frac{P}{2}x.$$

$$M(L) = \frac{\omega L^2}{2} - \frac{P}{2}L = \frac{\omega L^2}{10} \Rightarrow P = \frac{2}{5}\omega L \Rightarrow -\frac{5}{24}\omega L^4 + \frac{2}{5}\omega L \frac{L^3}{3} = \vartheta(L)EI$$

$$\therefore -k\vartheta(L) = -k\left(-\frac{17}{120}\frac{\omega L^4}{EI}\right) = \frac{17}{5}\omega L \Rightarrow \vartheta(L) = -\frac{17}{120}\frac{\omega L^4}{EI}$$

$$\Rightarrow k = \frac{2}{B} \frac{EI}{L^3} \times \frac{120}{17} 2^4 = \frac{48}{17} \frac{EI}{L^3}$$

Before the uniformly distributed load w is applied, a gap, $\delta_0 = 1.2 \text{ mm}$, exists between the ends of the cantilever bars AB and CD . Knowing that $E = 105 \text{ GPa}$ and $w = 30 \text{ kN/m}$, determine (a) the reaction at A , (b) the reaction at D .



For beam AB .

$$\text{deflection at } B = -\frac{\omega L^4}{8EI} + \frac{PL^3}{3EI}$$

once gap is closed.

$$= -\frac{PL^3}{3EI}$$

$\xrightarrow{\quad \text{L} \quad}$ Standard results

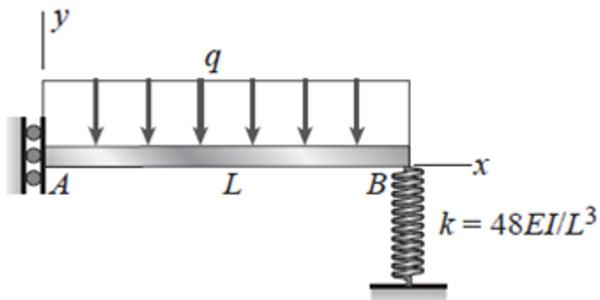
without the initial gap $v_B = v_C$.

$$\text{with initial gap } v_B + \delta_0 = v_C \Rightarrow -\frac{\omega L^4}{8EI} + \frac{PL^3}{3EI} + \delta_0 = -\frac{PL^3}{3EI}$$

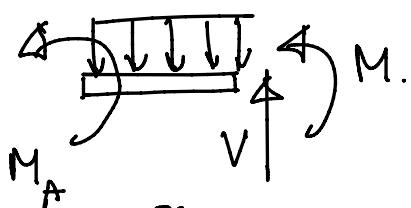
$$R_A = \omega L - P$$

$$\Rightarrow P = \frac{3}{16}\omega L - \frac{3}{2} \frac{EI\delta_0}{L^3}$$

$$R_D = P$$



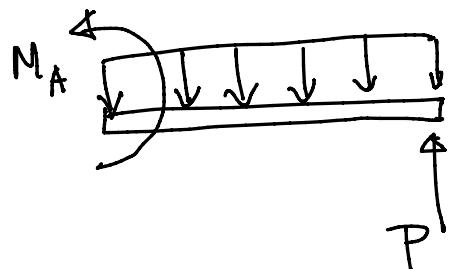
The beam shown in the figure has a guided support at A and a spring support at B . The guided support permits vertical movement but no rotation. Derive the equation of the deflection curve and determine the deflection at end B due to the uniform load of intensity q .



$$V = \int_0^x q d\xi = qx$$

$$M_A - \int_0^x (q d\xi) \xi + Vx + M = 0$$

$$\begin{aligned} \Rightarrow M &= -Vx - M_A + \frac{qx^2}{2} \\ &= -qx^2 + \frac{qL^2}{2} \end{aligned}$$



$$\begin{aligned} P &= qL \\ M_A + PL &= \frac{qL^2}{2} \\ \Rightarrow M_A &= -\frac{qL^2}{2} \end{aligned}$$

Because of a vertical roller support, unlike a cantilever there will be no force reaction at A : Since the roller prevents rotation there will be a moment reaction at A .

$$\begin{aligned} EI\vartheta'' &= M(x) = -\frac{qx^2}{2} + \frac{qL^2}{2} \\ \Rightarrow EI\vartheta' &= -\frac{1}{6}qx^3 + \frac{1}{2}qL^2x + C_1 \quad [\because \vartheta'(0) = 0] \\ \Rightarrow EI\vartheta &= -\frac{1}{24}qx^4 + \frac{1}{4}qL^2x^2 + C_1x + C_2 \end{aligned}$$

$$\Rightarrow \vartheta(L) = -\frac{qL^4}{24EI} + \frac{qL^4}{4EI} + \frac{C_2}{EI} = \frac{5}{24}\frac{qL^4}{EI} + \frac{C_2}{EI}$$

$$\text{But } P = qL = k\vartheta(L) = 48\frac{EI}{L^3} \left(\frac{5}{24}\frac{qL^4}{EI} + \frac{C_2}{EI} \right)$$

$$\therefore qL = 10qL + \frac{48}{L^3}C_2 \Rightarrow C_2 = -\frac{9qL^4}{48}, \therefore \vartheta_B = \vartheta(L) = \frac{qL^4}{48EI}$$

No rotation also implies zero slope at A