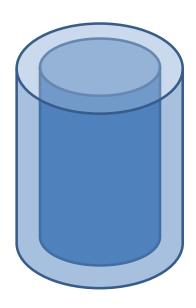
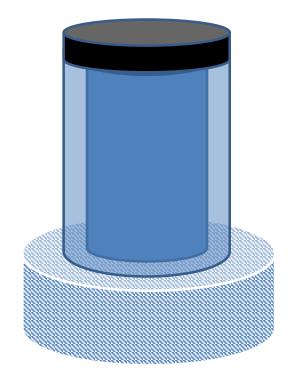
Statically indeterminate problems

Axial loading - I

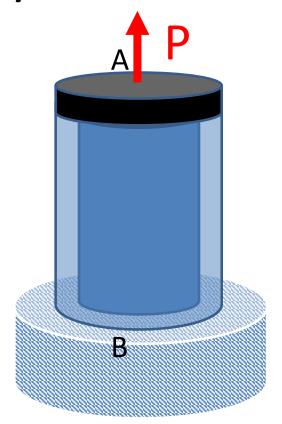
 Consider a solid cylinder of material 1 within a hollow cylinder of material 2. They are bonded together so that they cannot slip at the contacting surface.



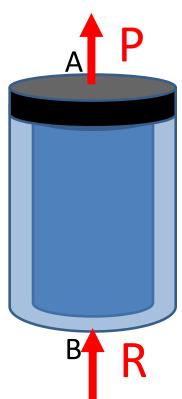
 Now fix the bottom surface of both cylinders, and fix a rigid plate to the top surface. At both ends the two cylinders are bonded rigidly to those two surfaces. Thus if the plate moves up, the bonded surfaces of both cylinders move by the same amount.



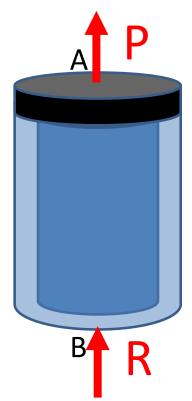
 The plate is now pulled by a force P at point A which is the center of the plate. Point B is the center of the bottom part of the cylinders.



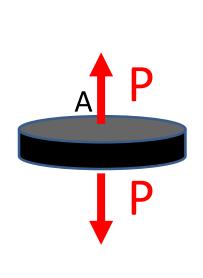
- Free Body Diagram of the entire contraption
- P+R=0
- R=-P

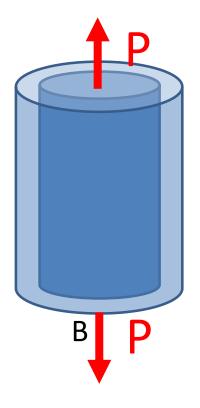


 Free Body Diagram of plate

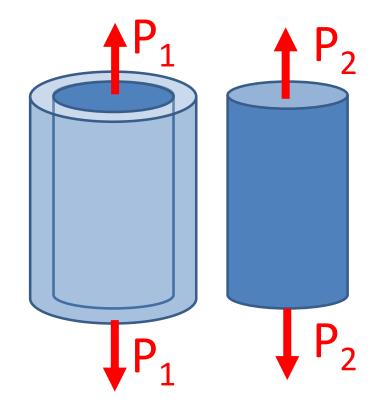


 Free Body Diagram of plate and the two cylinders taken together as one. We have used the fact that R=-P.

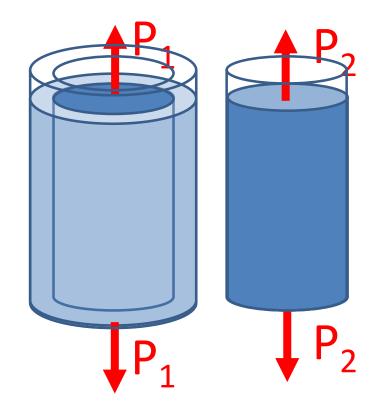




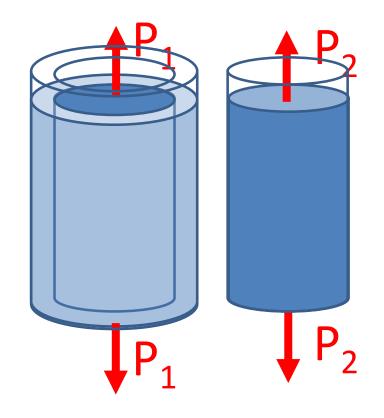
- Free Body Diagram of each cylinder? (Why the question mark?)
- Because it is here that we face the problem of indeterminacy
- All we know is $P_1 + P_2 = P$



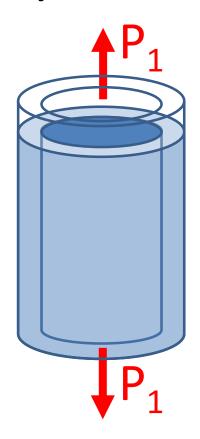
- What is the geometrical constraint?
- Since the top plate is rigid and is rigidly attached to both cylinders and both cylinders are rigidly bonded to each other, the displacement of the top surface for both cylinders must be same under the action of P.



Let the areas of cross section of the cylinders be a₁ and a₂ and the moduli of elasticity be E₁ and E₂. Let the length of the combined cylinder be L.



- For outer cylinder, the displacement of point A with respect to B will be
- $u_{AB1} = P_1 L/(E_1 a_1)$



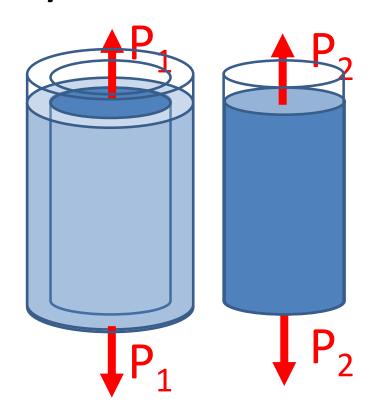
 For inner cylinder, the displacement of point A with respect to B will be

•
$$u_{AB1} = P_2 L/(E_2 a_2)$$



- Applying geometrical constraint $u_{AB1} = u_{AB1}$
- We have $P_1L/(E_1a_1)=P_2L/(E_2a_2)$
- Hence

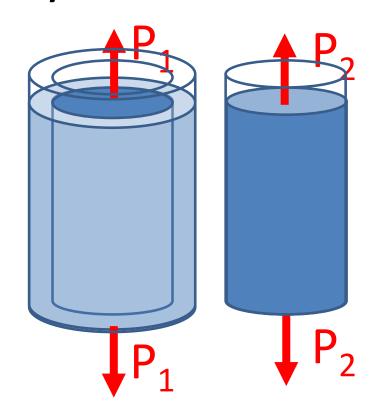
$$P_1 = P_2(E_1a_1)/(E_2a_2)$$



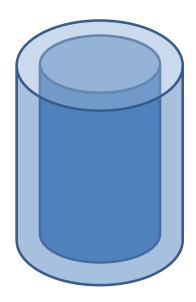
- But $P_1 + P_2 = P$
- Hence

$$P_2(E_1a_1)/(E_2a_2) + P_2 = P$$

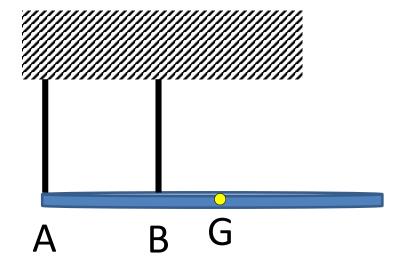
- So
- $P_2 = PE_2a_2/(E_1a_1+E_2a_2)$
- $P_1 = PE_1a_1/(E_1a_1+E_2a_2)$



- Have we done this before ?
- Yes! When we solved for springs in parallel in high school we were actually solving a statically indeterminate problem. Nobody uses that term in high school, that is all.
- This contraption is actually two springs in parallel, with one spring being inside another.



- We first start with a version of the problem that is statically determinate.
- A rigid rod with center of mass at G of weight W is hanging from 2 flexible wires of unstretched length L and area of cross section a each attached at A and B and made of material with modulus of elasticity E. Length of the rigid rod is S. We need to find the tension in each wire when the contraption is in static equilibrium. AB=S/3



We get from the FBD of wires and the rod the following force equilibrium equation

$$T_A + T_B = W$$

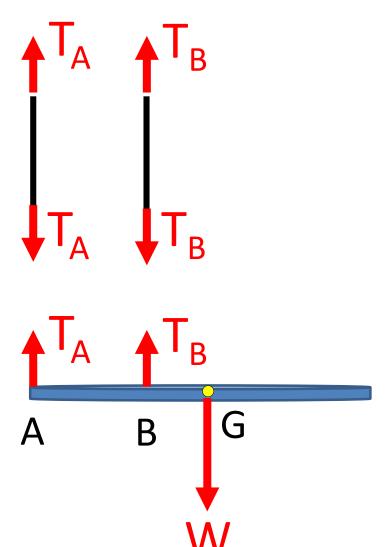
Taking moments about A, we get

$$T_BS/3 = WS/2$$

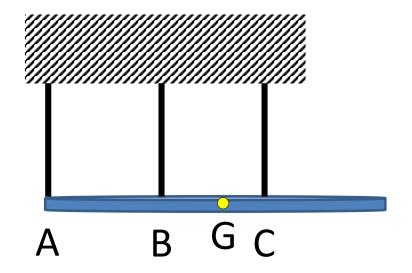
We have two unknowns T_A and T_B

We have two equations

Thus the problem is determinate.



 We now make this problem a version of the problem statically indeterminate by adding another wire identical to the other two at C. We set BC=S/3

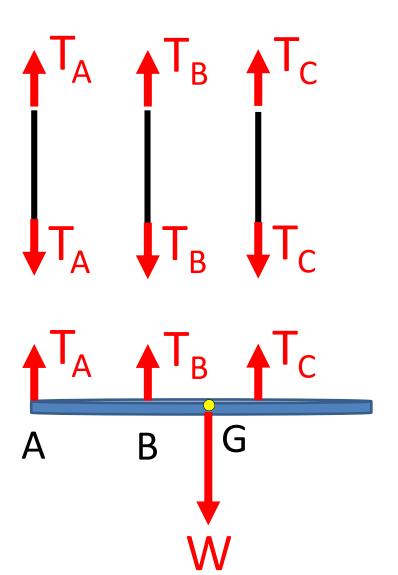


We get from the FBD of wires and the rod the following force equilibrium equation

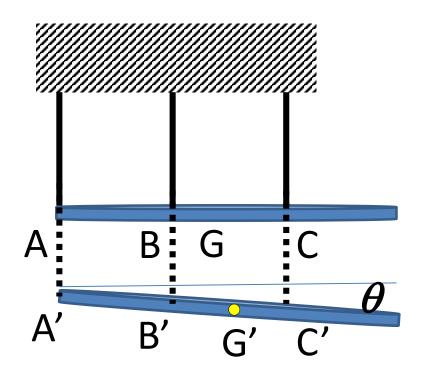
$$T_A + T_B + T_C = W$$

Taking moments about A, we get $T_RS/3 + 2T_CS/3 = WS/2$

We have three unknowns T_A , T_B , T_C . We still have two equations only Thus the problem is cannot be solved as is and is indeterminate.



 We now look at the deformed shape of the contraption. Note that we have assumed that the wires are still vertical and all the points are moving down almost vertically. This is a reasonable assumption if the movement is small. The deformations shown in the figure are of course highly exaggerated.

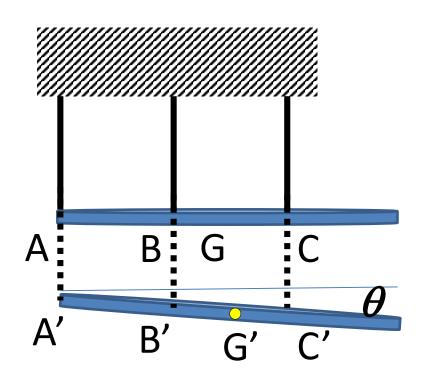


 From our knowledge of elastic deformation we know

$$AA' = \frac{T_A L}{Ea}$$

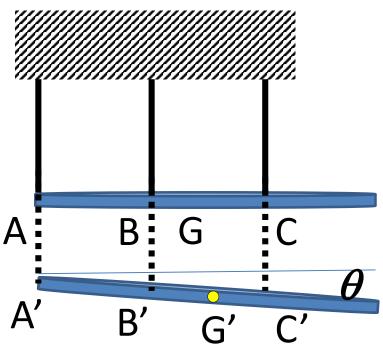
$$BB' = \frac{T_B L}{Ea}$$

$$CC' = \frac{T_C L}{Ea}$$



From geometry we have

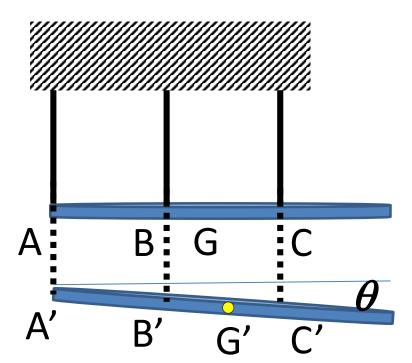
$$\sin \theta = \frac{BB' - AA'}{S/3} = \frac{CC' - AA'}{2S/3}$$



 Combining this knowledge we get

$$\frac{T_B L}{Ea} - \frac{T_A L}{Ea} = \frac{T_C L}{Ea} - \frac{T_A L}{Ea}$$

$$\Rightarrow 2T_B = T_A + T_C$$



We thus have our third equation

Force equilibrium equation

$$T_A + T_B + T_C = W$$

Moment equilibrium equation

$$T_B S/3 + 2T_C S/3 = WS/2$$

From geometrical constraint and deformation

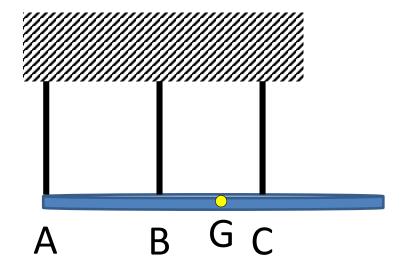
$$T_A + T_C = 2T_B$$

Hence

$$T_B = 4W/12$$
, $T_C = 7W/12$, $T_A = W/12$

An added twist

 The wire at C is replaced by a rope which is initially slack and because it is longer than the wires by an amount d. At equilibrium the rope is tight. Material properties of the rope and area of cross section are the same as that of the wires.



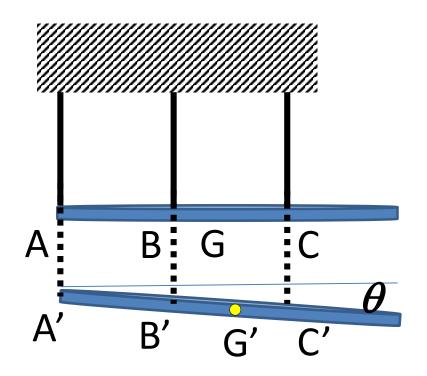
An added twist

 In this case CC' will have two parts.

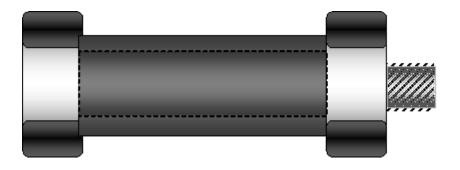
$$AA' = \frac{T_A L}{Ea}$$

$$BB' = \frac{T_B L}{Ea}$$

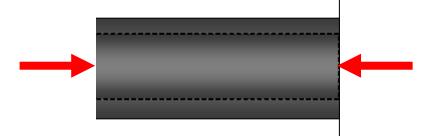
$$CC' - d = \frac{T_C (L + d)}{Ea}$$



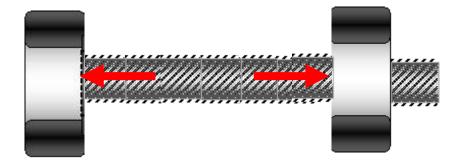
 A brass sleeve of length L is slipped over a steel bolt and is held in place by a nut that is turned just snug. The nut is tightened by one turn. The pitch of the thread is p. What are the forces developed in the bolt and the sleeve? The area of cross section of the bolt is A_s, the sleeve is A_b. Modulus of elasticity for steel and brass are E_s and E_b respectively.



- FBDs
- Nut pushes the sleeve



Sleeve pushes back the nut



- The tightening of the nut means the length of the sleeve should decrease by p. But this will produce a force F in both the bolt and the sleeve which will cause the sleeve to compress and the bolt to expand as see from the FBDs.
- The length of the bolt that will affected by this force will be L-p.
- Hence new length of sleeve = L-FL/(E_bA_b)
- New length of bolt = $(L-p)+F(L-p)/(E_sA_s)$
- These must be the same.

 Using the geometrical constraint of equality of length, we can get the force F. Thereafter it will be possible to find out stresses in the bolt and the sleeve and thus we can get an idea about how much can the nut be tightened without causing any damage.

$$L - \frac{FL}{E_b A_b} = (L - p) + \frac{F(L - p)}{E_s A_s}$$

$$\Rightarrow F = \frac{p}{\frac{L}{E_b A_b} + \frac{(L - p)}{E_s A_s}}$$