

(a) Determine the torque **T** that causes a maximum shearing stress of 45 MPa in the hollow cylindrical steel shaft shown. (b) Determine the maximum shearing stress caused by the same torque **T** in a solid cylindrical shaft of the same cross-sectional area.

SOLUTION

(a) Given shaft: $J = \frac{\pi}{2} \left(c_2^4 - c_1^4 \right)$ $J = \frac{\pi}{2} (45^4 - 30^4) = 5.1689 \times 10^6 \text{ mm}^4 = 5.1689 \times 10^{-6} \text{ m}^4$ $\tau = \frac{Tc}{J} \qquad T = \frac{J\tau}{c}$ $T = \frac{(5.1689 \times 10^{-6})(45 \times 10^6)}{45 \times 10^{-3}} = 5.1689 \times 10^3 \text{ N} \cdot \text{m}$

 $T = 5.17 \text{ kN} \cdot \text{m}$

(b) Solid shaft of same area:

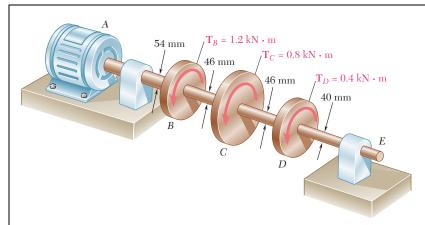
$$A = \pi \left(c_2^2 - c_1^2\right) = \pi (45^2 - 30^2) = 3.5343 \times 10^3 \text{ mm}^2$$

$$\pi c^2 = A \quad \text{or} \quad c = \sqrt{\frac{A}{\pi}} = 33.541 \text{ mm}$$

$$J = \frac{\pi}{2} c^4, \quad \tau = \frac{Tc}{J} = \frac{2T}{\pi c^3}$$

$$\tau = \frac{(2)(5.1689 \times 10^3)}{\pi (0.033541)^3} = 87.2 \times 10^6 \text{ Pa}$$

 $\tau = 87.2 \text{ MPa}$



Under normal operating conditions, the electric motor exerts a torque of 2.4 kN \cdot m on shaft AB. Knowing that each shaft is solid, determine the maximum shearing stress in (a) shaft AB, (b) shaft BC, (c) shaft CD.

SOLUTION

(a) Shaft AB: $T_{AB} = 2.4 \times 10^3 \text{ N} \cdot \text{m}, \quad c = \frac{1}{2}d = 0.027 \text{ m}$

$$\tau_{AB} = \frac{Tc}{J} = \frac{2T}{\pi c^3} = \frac{2(2.4 \times 10^3)}{\pi (0.027)^3} = 77.625 \times 10^6 \,\text{Pa}$$

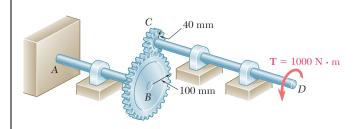
77.6 MPa ◀

(b) Shaft BC: $T_{BC} = 2.4 \text{ kN} \cdot \text{m} - 1.2 \text{ kN} \cdot \text{m} = 1.2 \text{ kN} \cdot \text{m}, \quad c = \frac{1}{2}d = 0.023 \text{ m}$

$$\tau_{BC} = \frac{Tc}{J} = \frac{2T}{\pi c^3} = \frac{(2)(1.2 \times 10^3)}{\pi (0.023)^3} = 62.788 \times 10^6 \,\text{Pa}$$
 62.8 MPa 4

(c) <u>Shaft CD</u>: $T_{CD} = 0.4 \times 10^3 \,\text{N} \cdot \text{m}$ $c = \frac{1}{2}d = 0.023 \,\text{m}$

$$\tau_{CD} = \frac{Tc}{J} = \frac{2T}{\pi c^3} = \frac{(2)(0.4 \times 10^3)}{\pi (0.023)^3} = 20.929 \times 10^6 \,\text{Pa}$$
20.9 MPa



A torque of magnitude $T = 1000 \text{ N} \cdot \text{m}$ is applied at D as shown. Knowing that the diameter of shaft AB is 56 mm and that the diameter of shaft CD is 42 mm, determine the maximum shearing stress in (a) shaft AB, (b) shaft CD.

SOLUTION

$$T_{CD} = 1000 \text{ N} \cdot \text{m}$$

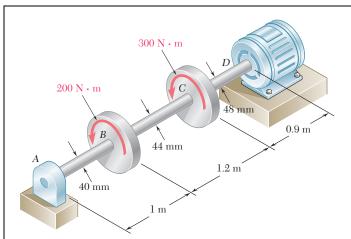
$$T_{AB} = \frac{r_B}{r_C} T_{CD} = \frac{100}{40} (1000) = 2500 \text{ N} \cdot \text{m}$$

(a) Shaft AB:
$$c = \frac{1}{2}d = 0.028 \text{ m}$$

$$\tau = \frac{Tc}{J} = \frac{2T}{\pi c^3} = \frac{(2)(2500)}{\pi (0.028)^3} = 72.50 \times 10^6$$
 72.5 MPa

(b) Shaft *CD*:
$$c = \frac{1}{2}d = 0.020 \text{ m}$$

$$\tau = \frac{Tc}{J} = \frac{2T}{\pi c^3} = \frac{(2)(1000)}{\pi (0.020)^3} = 68.7 \times 10^6$$
 68.7 MPa



The electric motor exerts a 500-N \cdot m torque on the aluminum shaft ABCD when it is rotating at a constant speed. Knowing that G = 27 GPa and that the torques exerted on pulleys B and C are as shown, determine the angle of twist between (a) B and C, (b) B and D.

SOLUTION

(a) Angle of twist between B and C.

$$T_{BC} = 200 \text{ N} \cdot \text{m}, \quad L_{BC} = 1.2 \text{ m}$$

$$c = \frac{1}{2}d = 0.022 \text{ m}, \quad G = 27 \times 10^9 \text{ Pa}$$

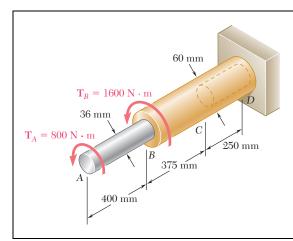
$$J_{BC} = \frac{\pi}{2}c^4 = 367.97 \times 10^{-9} \text{ m}$$

$$\varphi_{B/C} = \frac{TL}{GJ} = \frac{(200)(1.2)}{(27 \times 10^9)(367.97 \times 10^9)} = 24.157 \times 10^{-3} \text{ rad}$$

$$\varphi_{B/C} = 1.384^{\circ} \blacktriangleleft$$

(b) Angle of twist between B and D.

$$\begin{split} T_{CD} &= 500 \text{ N} \cdot \text{m}, \quad L_{CD} = 0.9 \text{ m}, \quad c = \frac{1}{2}d = 0.024 \text{ m}, \quad G = 27 \times 10^9 \text{ Pa} \\ J_{CD} &= \frac{\pi}{2}c^4 = \frac{\pi}{2}(0.024)^4 = 521.153 \times 10^{-9} \text{ m}^4 \\ \varphi_{C/D} &= \frac{(500)(0.9)}{(27 \times 10^9)(521.153 \times 10^9)} = 31.980 \times 10^{-3} \text{ rad} \\ \varphi_{B/D} &= \varphi_{B/C} + \varphi_{C/D} = 24.157 \times 10^{-3} + 31.980 \times 10^{-3} = 56.137 \times 10^{-3} \text{ rad} \\ \end{split}$$



The aluminum rod AB (G = 27 GPa) is bonded to the brass rod BD (G = 39 GPa). Knowing that portion CD of the brass rod is hollow and has an inner diameter of 40 mm, determine the angle of twist at A.

SOLUTION

Rod AB:

$$G = 27 \times 10^9 \,\text{Pa}, \quad L = 0.400 \,\text{m}$$

$$T = 800 \,\text{N} \cdot \text{m} \quad c = \frac{1}{2}d = 0.018 \,\text{m}$$

$$J = \frac{\pi}{2}c^4 = \frac{\pi}{2}(0.018)^4 = 164.896 \times 10^{-9} \,\text{m}$$

$$\varphi_{A/B} = \frac{TL}{GJ} = \frac{(800)(0.400)}{(27 \times 10^9)(164.896 \times 10^{-9})} = 71.875 \times 10^{-3} \,\text{rad}$$

Part BC

$$G = 39 \times 10^9 \,\text{Pa}$$
 $L = 0.375 \,\text{m}$, $c = \frac{1}{2}d = 0.030 \,\text{m}$

$$T = 800 + 1600 = 2400 \text{ N} \cdot \text{m}, \quad J = \frac{\pi}{2}c^4 = \frac{\pi}{2}(0.030)^4 = 1.27234 \times 10^{-6} \text{ m}^4$$

$$\varphi_{B/C} = \frac{TL}{GJ} = \frac{(2400)(0.375)}{(39 \times 10^9)(1.27234 \times 10^{-6})} = 18.137 \times 10^{-3} \text{ rad}$$

Part CD:

$$c_1 = \frac{1}{2}d_1 = 0.020 \text{ m}$$

$$c_2 = \frac{1}{2}d_2 = 0.030 \text{ m}, \quad L = 0.250 \text{ m}$$

$$J = \frac{\pi}{2}\left(c_2^4 - c_1^4\right) = \frac{\pi}{2}(0.030^4 - 0.020^4) = 1.02102 \times 10^{-6} \text{ m}^4$$

$$\varphi_{C/D} = \frac{TL}{GJ} = \frac{(2400)(0.250)}{(39 \times 10^9)(1.02102 \times 10^{-6})} = 15.068 \times 10^{-3} \text{ rad}$$

Angle of twist at A.

$$\varphi_A = \varphi_{A/B} + \varphi_{B/C} + \varphi_{C/D}$$
= 105.080 × 10⁻³ rad

 $\varphi_A = 6.02^{\circ}$

The design specifications of a 1.2-m-long solid transmission shaft require that the angle of twist of the shaft not exceed 4° when a torque of 750 N · m is applied. Determine the required diameter of the shaft, knowing that the shaft is made of a steel with an allowable shearing stress of 90 MPa and a modulus of rigidity of 77.2 GPa.

SOLUTION

$$T = 750 \text{ N} \cdot \text{m}, \quad \varphi = 4^{\circ} = 69.813 \times 10^{-3} \text{ rad},$$

$$L = 1.2 \text{ m}, \quad J = \frac{\pi}{2}c^4$$

$$\tau = 90 \text{ MPa} = 90 \times 10^6 \text{ Pa}$$
 $G = 77.2 \text{ GPa} = 77.2 \times 10^9 \text{ Pa}$

Based on angle of twist.

$$\varphi = \frac{TL}{GJ} = \frac{2TL}{\pi Gc^4}$$

$$c = \sqrt[4]{\frac{2TL}{\pi G \varphi}} = \sqrt[4]{\frac{(2)(750)(1.2)}{\pi (77.2 \times 10^9)(69.813 \times 10^{-3})}} = 18.06 \times 10^{-3} \,\mathrm{m}$$

Based on shearing stress. $\tau = \frac{Tc}{J} = \frac{2T}{\pi c^3}$

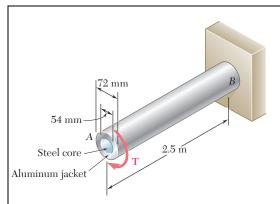
$$= \frac{Tc}{J} = \frac{2T}{\pi c^3}$$

$$c = \sqrt[3]{\frac{2T}{\pi\tau}} = \sqrt[3]{\frac{(2)(750)}{\pi(90 \times 10^6)}} = 17.44 \times 10^{-3} \,\mathrm{m}$$

Use larger value.

$$c = 18.06 \times 10^{-3} \,\mathrm{m} = 18.06 \,\mathrm{mm}$$

 $d = 2c = 36.1 \, \text{mm}$



A torque of magnitude $T = 4 \text{ kN} \cdot \text{m}$ is applied at end A of the composite shaft shown. Knowing that the modulus of rigidity is 77.2 GPa for the steel and 27 GPa for the aluminum, determine (a) the maximum shearing stress in the steel core, (b) the maximum shearing stress in the aluminum jacket, (c) the angle of twist at A.

SOLUTION

Steel core:

$$c_1 = \frac{1}{2} d_1 = 0.027 \text{ m}$$
 $J_1 = \frac{\pi}{2} c_1^4 = \frac{\pi}{2} (0.027)^4 = 834.79 \times 10^{-9}$

$$G_1J_1 = (77.2 \times 10^9)(834.79 \times 10^{-9}) = 64.446 \times 10^3 \text{ N} \cdot \text{m}^2$$

Torque carried by steel core.

$$T_1 = G_1 J_1 \varphi / L$$

Aluminum jacket:

$$c_1 = \frac{1}{2}d_1 = 0.027 \text{ m}, \quad c_2 = \frac{1}{2}d_2 = 0.036 \text{ m}$$

$$J_2 = \frac{\pi}{2} \left(c_2^4 - c_1^4 \right) = \frac{\pi}{2} \left(0.036^4 - 0.027^4 \right) = 1.80355 \times 10^{-6} \text{ m}^4$$

$$G_2 J_2 = (27 \times 10^9)(1.80355 \times 10^{-6}) = 48.70 \times 10^3 \text{ N} \cdot \text{m}^2$$

Torque carried by aluminum jacket. $T_2 = G_2 J_2 \varphi / L$

Total torque:

$$T = T_1 + T_2 = (G_1J_1 + G_2J_2) \varphi/L$$

$$\frac{\varphi}{L} = \frac{T}{G_1 J_1 + G_2 J_2} = \frac{4 \times 10^3}{64.446 \times 10^3 + 48.70 \times 10^3} = 35.353 \times 10^{-3} \text{ rad/m}$$

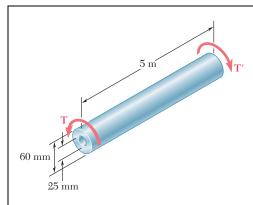
(a) Maximum shearing stress in steel core.

$$\tau = G_1 \gamma = G_1 c_1 \frac{\varphi}{L} = (77.2 \times 10^9)(0.027)(35.353 \times 10^{-3}) = 73.7 \times 10^6 \text{ Pa}$$
 73.7 MPa

(b) <u>Maximum shearing stress in aluminum jacket.</u>

$$\tau = G_2 \gamma = G_2 c_2 \frac{\varphi}{L} = (27 \times 10^9)(0.036)(35.353 \times 10^{-3})$$
 = 34.4 × 10⁶ Pa 34.4 MPa \blacktriangleleft

(c) Angle of twist.
$$\varphi = L \frac{\varphi}{L} = (2.5)(35.353 \times 10^{-3}) = 88.383 \times 10^{-3} \text{ rad}$$
 $\varphi = 5.06^{\circ}$



As the hollow steel shaft shown rotates at 180 rpm, a stroboscopic measurement indicates that the angle of twist of the shaft is 3° . Knowing that G = 77.2 GPa, determine (a) the power being transmitted, (b) the maximum shearing stress in the shaft.

SOLUTION

$$c_2 = \frac{1}{2}d_2 = 30 \text{ mm}$$

$$c_1 = \frac{1}{2}d_1 = 12.5 \text{ mm}$$

$$J = \frac{\pi}{2}\left(c_2^4 - c_1^4\right) = \frac{\pi}{2}[(30)^4 - (12.5)^4]$$

$$= 1.234 \times 10^6 \text{ mm}^4 = 1.234 \times 10^{-6} \text{ m}^4$$

$$\varphi = 3^\circ = 0.05236 \text{ rad}$$

$$\varphi = \frac{TL}{GJ}$$

$$T = \frac{GJ\varphi}{L} = \frac{(77.2 \times 10^9)(1.234 \times 10^{-6})(0.0536)}{5} = 997.61 \text{ N} \cdot \text{m}$$

Angular speed:

$$f = 180 \text{ rpm} = 3 \text{ rev/sec} = 3 \text{ Hz}$$

(a) Power being transmitted.

$$P = 2\pi f T = 2\pi (3)(997.61) = 18.80 \times 10^3 \,\mathrm{W}$$

P = 18.80 kW

(b) <u>Maximum shearing stress</u>.

$$\tau_m = \frac{Tc_2}{J} = \frac{(997.61)(30 \times 10^{-3})}{1.234 \times 10^{-6}}$$

$$= 24.3 \times 10^6 \, \text{Pa}$$

$$\tau_m = 24.3 \text{ MPa}$$