

\vec{b} can vary locally

$$\frac{d}{dt} \int_V F dV = \int_V \frac{\partial F}{\partial t} dV + \int_A F \vec{b} \cdot \vec{n} dA$$

$$\vec{b} = \vec{u}$$

chunk of fluid moves with the fluid

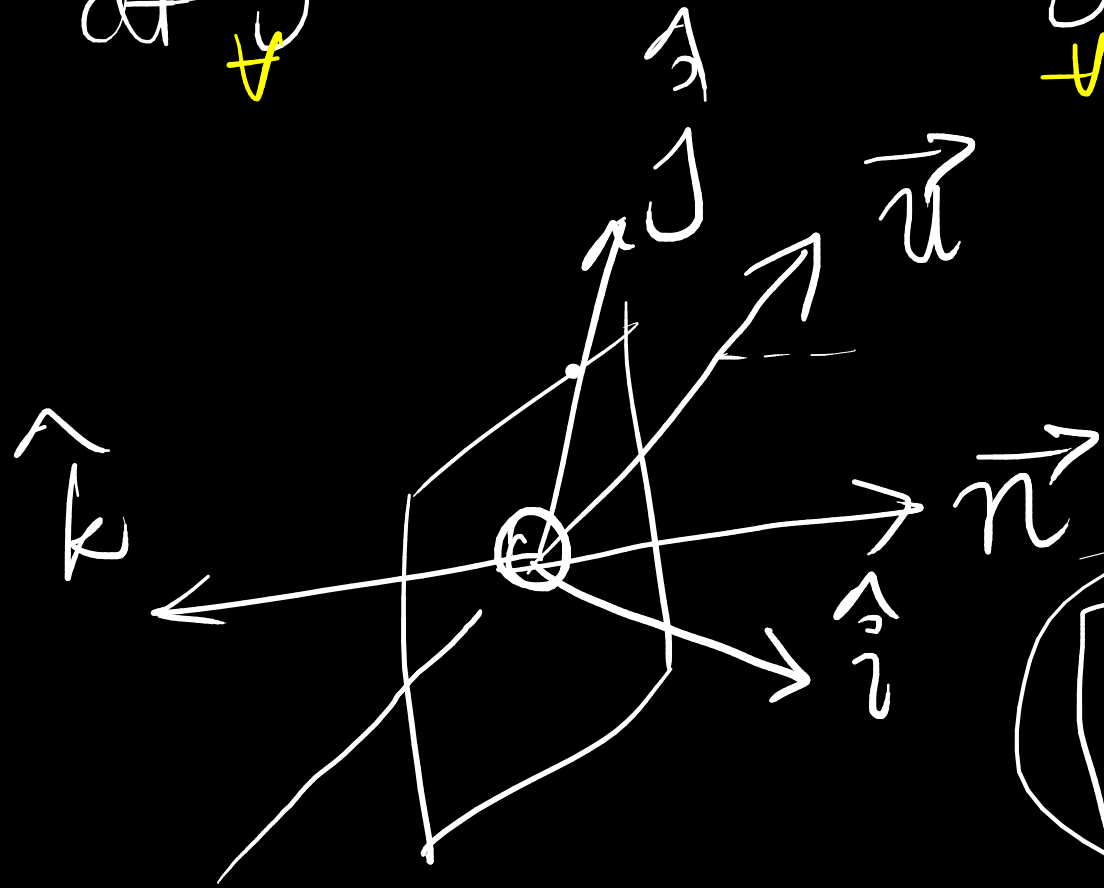
$$\frac{d}{dt} \int_V F dV = \int_V \frac{\partial F}{\partial t} dV + \int_V F \vec{u} \cdot \vec{n} dA$$

(\vec{u}) \nearrow momentum/vol $\rho \vec{u}$

$$\left| \frac{d}{dt} \int_V \rho \vec{u} dV = \int_V \frac{\partial (\rho \vec{u})}{\partial t} dV + \int_A \rho \vec{u} \vec{u} \cdot \vec{n} dA \right.$$

$$\frac{d}{dt} \int_V \rho u dV = \int_V \frac{\partial}{\partial t} (\rho u) + \int_A \rho u \underbrace{\vec{u} \cdot \vec{n} dA}_{\text{flux}}$$

x-mom
↓
entity carried by



$$\vec{u} \cdot \vec{n}$$

$$\left\{ \begin{array}{l} \int \vec{u} \cdot \hat{i} \\ \int \vec{u} \cdot \hat{j} \\ \int \vec{u} \cdot \hat{k} \end{array} \right\} \begin{array}{l} x \text{ mom/vol} \\ y \text{ } \\ z \text{ } \end{array}$$

Cause of the rate of ch-mom

$$\int_V \frac{\partial}{\partial t} (\rho \vec{u}) dV + \int_A \rho \vec{u} \cdot \vec{n} dA = \Sigma F = F_{\text{body}} + F_{\text{surf}}$$

Body force

→ Acts on total volume

Gravity
Electromagnetic
Magnetic
Thermal.

$$\int_V \rho \vec{g} dV$$

$$F_{b,g} =$$

$$\int_V \rho \vec{g} dV$$

○ (x)

○ (y)

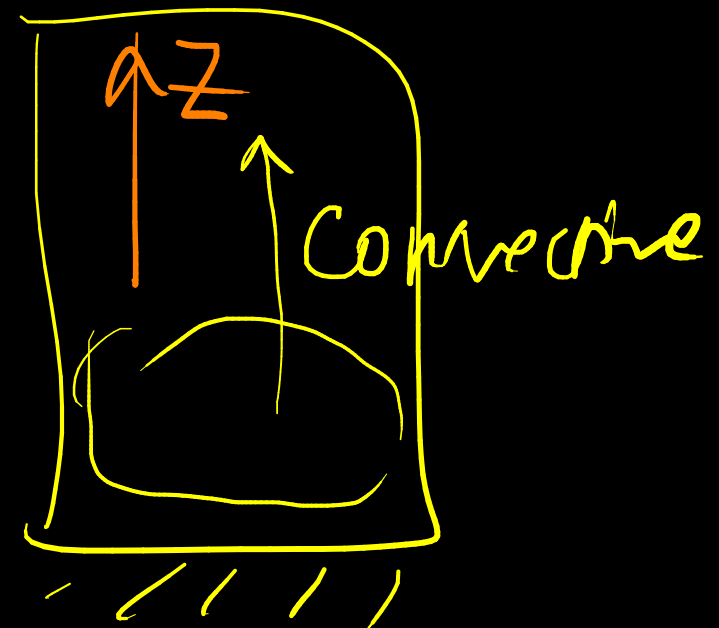
$$= \int_V \rho g dV$$

Conservative

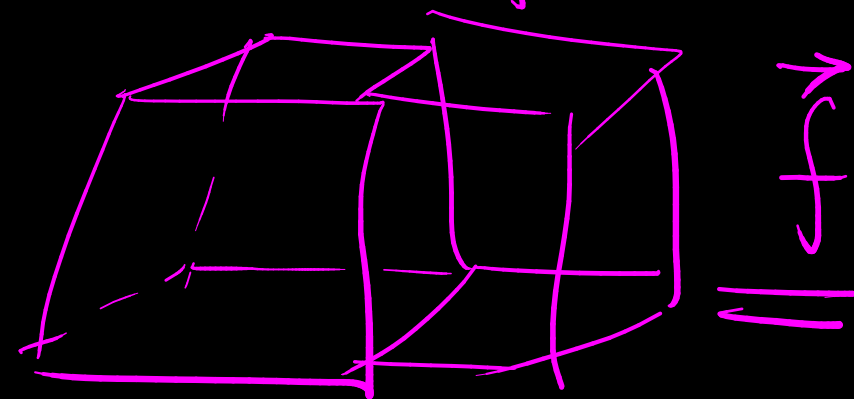
non conservative

$$\vec{F} = -\nabla \phi$$

$$\rho \vec{g} = -\nabla \phi \Rightarrow \phi = -\rho g z$$



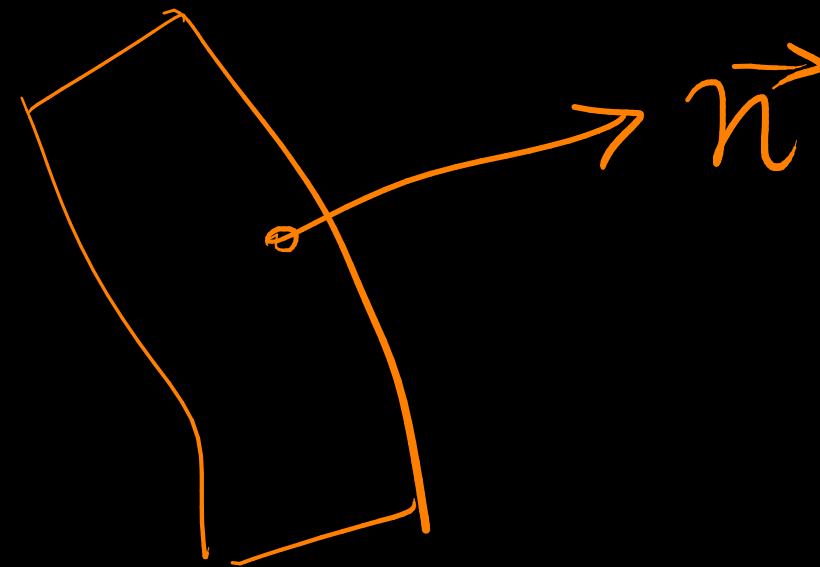
Surface forces



traction
vector

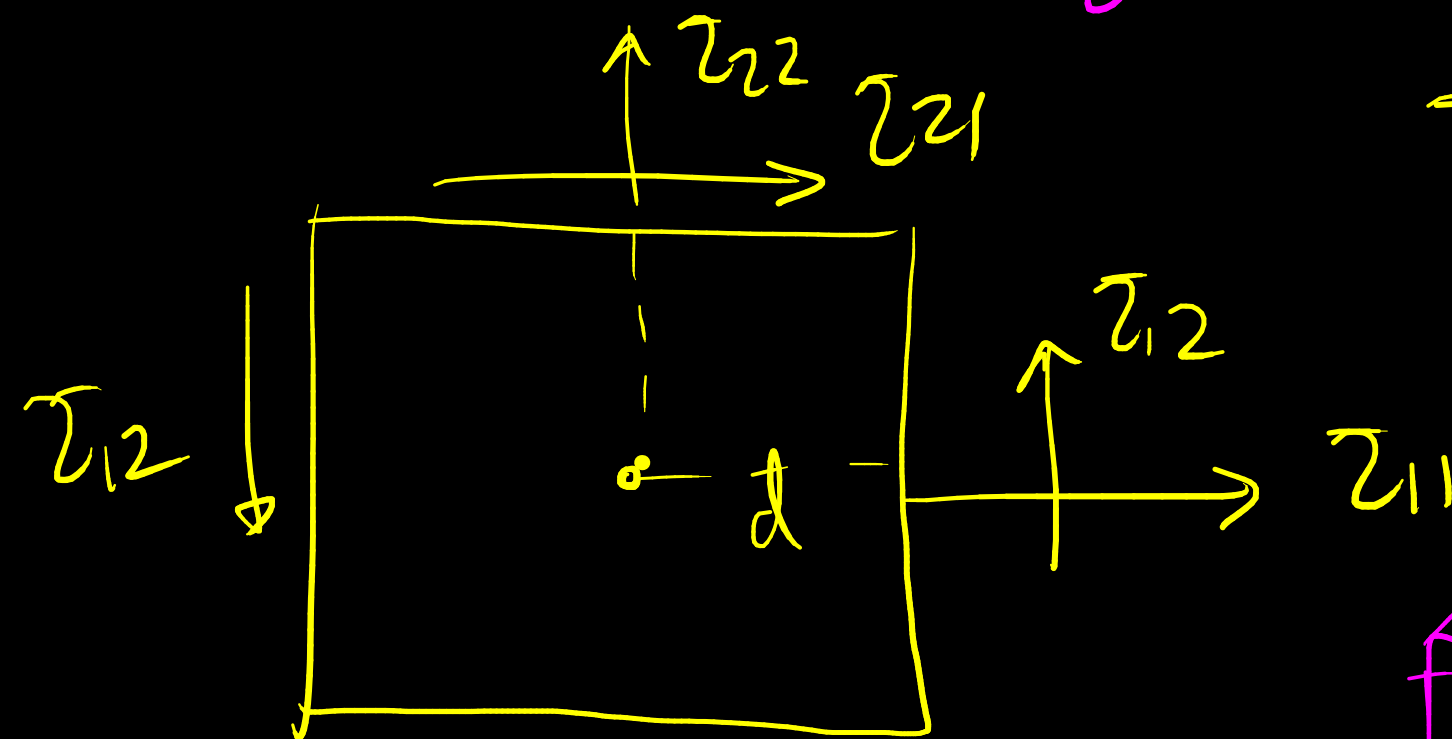
$$\vec{f}_s = \underline{\underline{\tau}} \cdot \vec{n}$$

$$\int_A \vec{f} dA$$



$$f_j = \tau_{ij} n_i$$

Stress tensor is symmetric



$$\tau_{12} - \tau_{21} = \underbrace{\text{net moment}}_d = 0$$

$$\tau_{12} = \tau_{21}$$

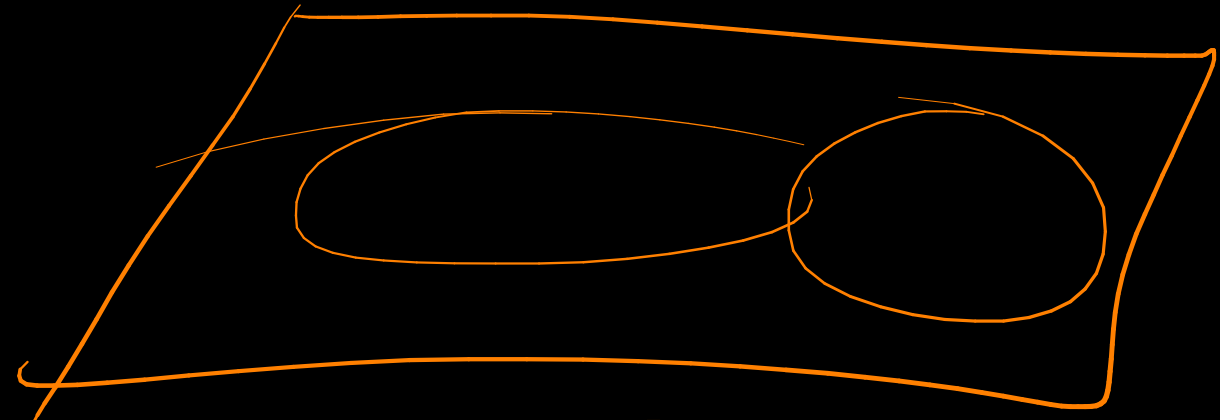
Tensorial

$$// \int_V \frac{\partial}{\partial t} (\rho \vec{u}) dV + \int_A \rho \vec{u} \cdot \vec{n} dA = \int_V \rho \vec{g} dV + \int_A \vec{F} dA$$

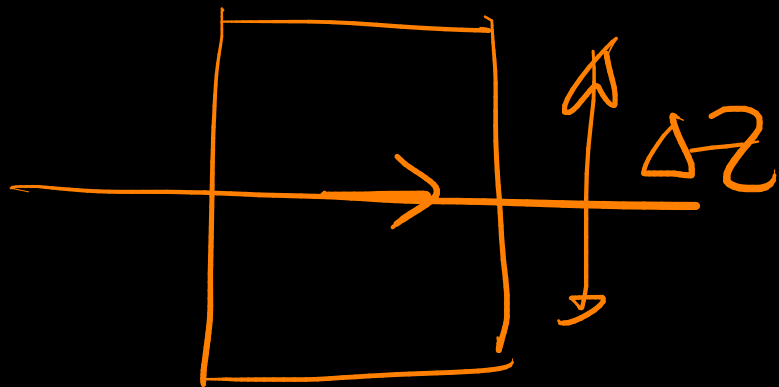
interfacial
forces

surface

Boundary condition



(2)



$$\boxed{\int_V \frac{\partial(\rho \vec{u})}{\partial t} dV} + \int_V \rho \vec{u} \cdot \vec{u} \cdot \vec{n} dA = \int_V \rho \vec{g} dV + \int_A \vec{f} dA$$

→ Any general CV moving w/ $\underline{\vec{b}}$

$$\frac{d}{dt} \int_{V^*} \rho \vec{u} dV =$$

$$\int_{V^*} \frac{\partial(\rho \vec{u})}{\partial t} dV +$$

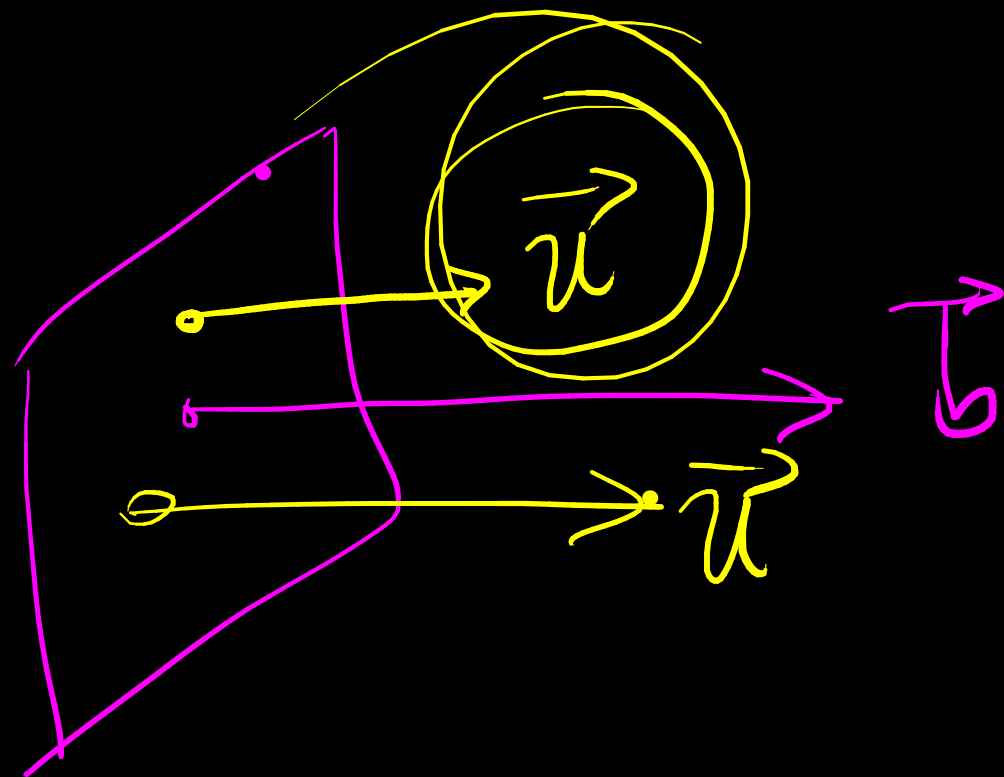
$$\int_A \rho \vec{u} \cdot \vec{b} \cdot \vec{n} dA$$

$$\int \frac{\partial(\rho \vec{u})}{\partial t} dV$$



$$\frac{d}{dt} \int \rho \vec{u} dV - \int \rho \vec{u} \cdot \vec{b} \cdot \vec{n} dA + \int \rho \vec{u} \cdot \vec{u} \cdot \vec{n} dA = \int \rho \vec{g} dV + \int \vec{f} dA$$

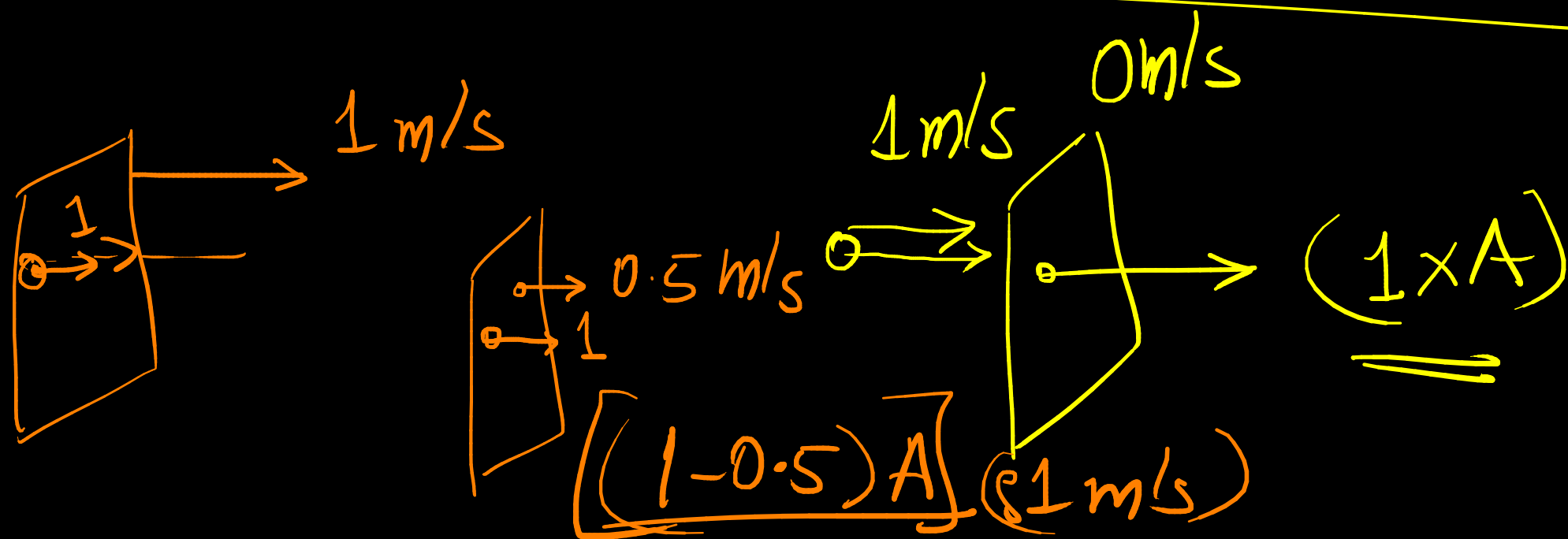
$$\frac{d}{dt} \int \rho \vec{u} dV + \int \rho \vec{u} \cdot (\vec{u} - \vec{b}) \cdot \vec{n} dA = \int \rho \vec{g} dV + \int \vec{f} dA$$

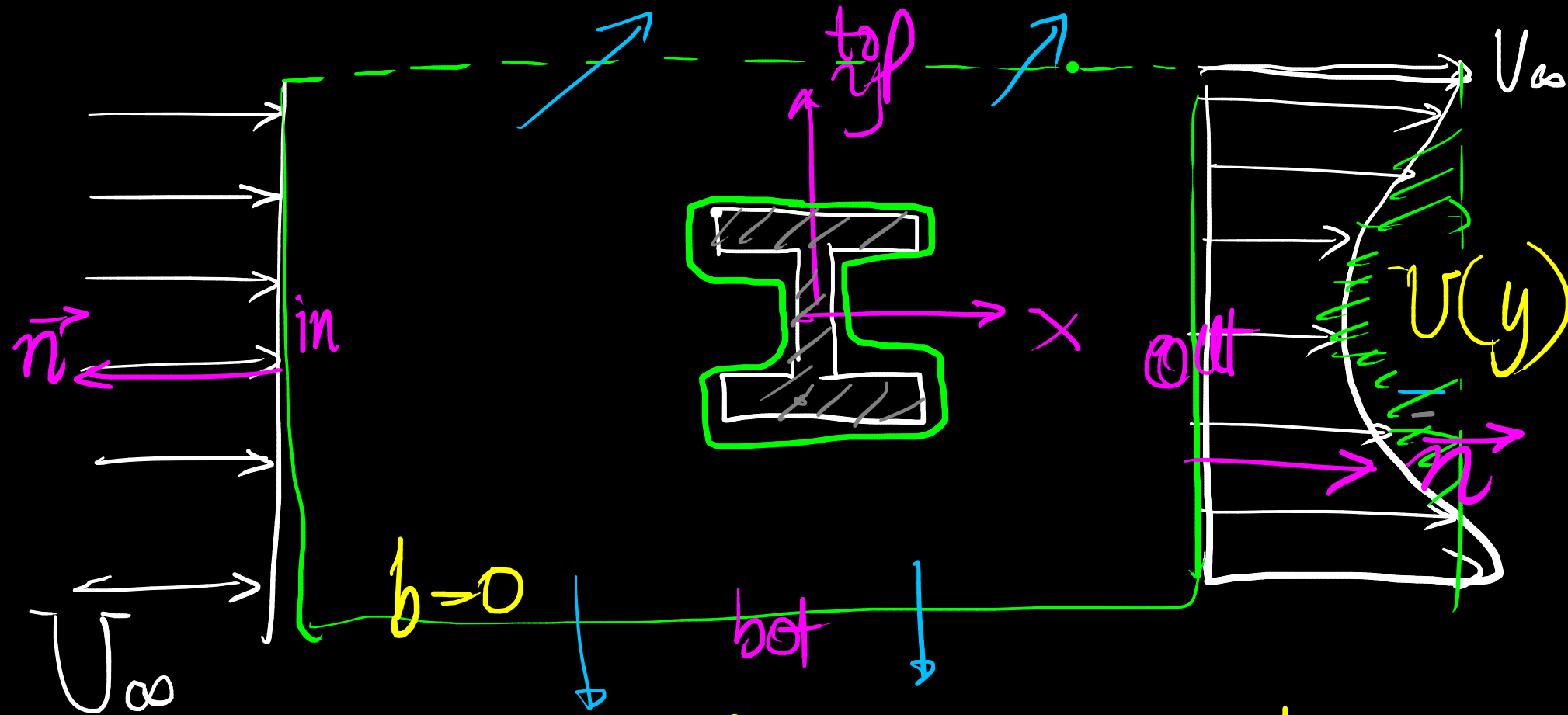


$$(\vec{u} - \vec{b}) \cdot \vec{n} dA$$

Relative flux
to moving CV

no flux if flux crosses at all



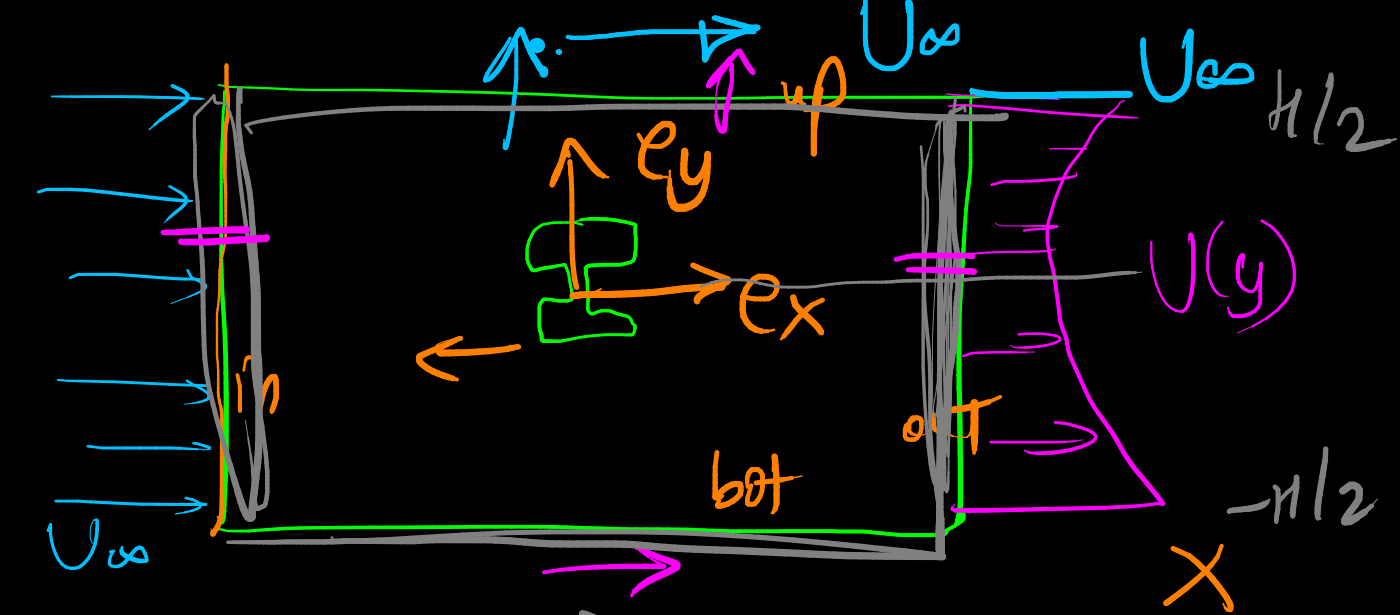


- Find out expr for drag acting on body.

Step 1: Mass conservation

$$\int \rho \vec{u} \cdot \vec{n} dA = 0$$

$$\begin{aligned} & \int_{in} \rho \vec{u} \cdot \vec{n} dA + \int_{out} \rho \vec{u} \cdot \vec{n} dA + \int_{up} \rho \vec{u} \cdot \vec{n} dA + \int_{bot} \rho \vec{u} \cdot \vec{n} dA = 0 \\ & - \int \rho U_{\infty} dA + \int \rho U(y) dA + \left[\int_{up} \rho \vec{u} \cdot \vec{n} dA + \int_{bot} \rho \vec{u} \cdot \vec{n} dA \right] = 0 \end{aligned}$$



$$\boxed{\int_S \vec{u} \cdot \vec{n} dA + \int_{\text{bot}} \rho \vec{u} \cdot \vec{n} dA = \int_S \rho (U_\infty - U(y)) dA}$$

+ve

$$+ \int_S \rho U_\infty^2 dA - \int_S \rho U(y)^2 dA$$

$$+ U_\infty \times \int_S \rho (U_\infty + U(y)) dA = +F_D$$

in: $\vec{u} = U_\infty \vec{e}_x$

$$\int_S \rho \vec{u} \cdot \vec{n} dA = \int_S \rho U_\infty (-U_\infty) dA$$

$$= \int_S \rho U(y) (U(y)) dA$$

up bot:

$$\int_S \rho U_\infty \vec{u} \cdot \vec{n} dA + \int_{\text{bot}} \rho U_\infty \vec{u} \cdot \vec{n} dA,$$

$$= U_\infty \left[\int_{\text{top}} \rho \vec{u} \cdot \vec{n} dA + \int_{\text{bot}} \rho \vec{u} \cdot \vec{n} dA \right]$$

$$l \int_S \rho U_\infty^2 dA - l \int_S \rho U(y)^2 dA$$

$$+ \int_S \rho (-U_\infty^2 + U_\infty U(y)) dy l = F_D$$

$$\boxed{\frac{F_D}{l} = \int_{-h/2}^{h/2} \rho U(y) [U_\infty - U(y)] dy}$$

$$\boxed{U_\infty \vec{e}_x + v \vec{e}_y} \leftarrow$$

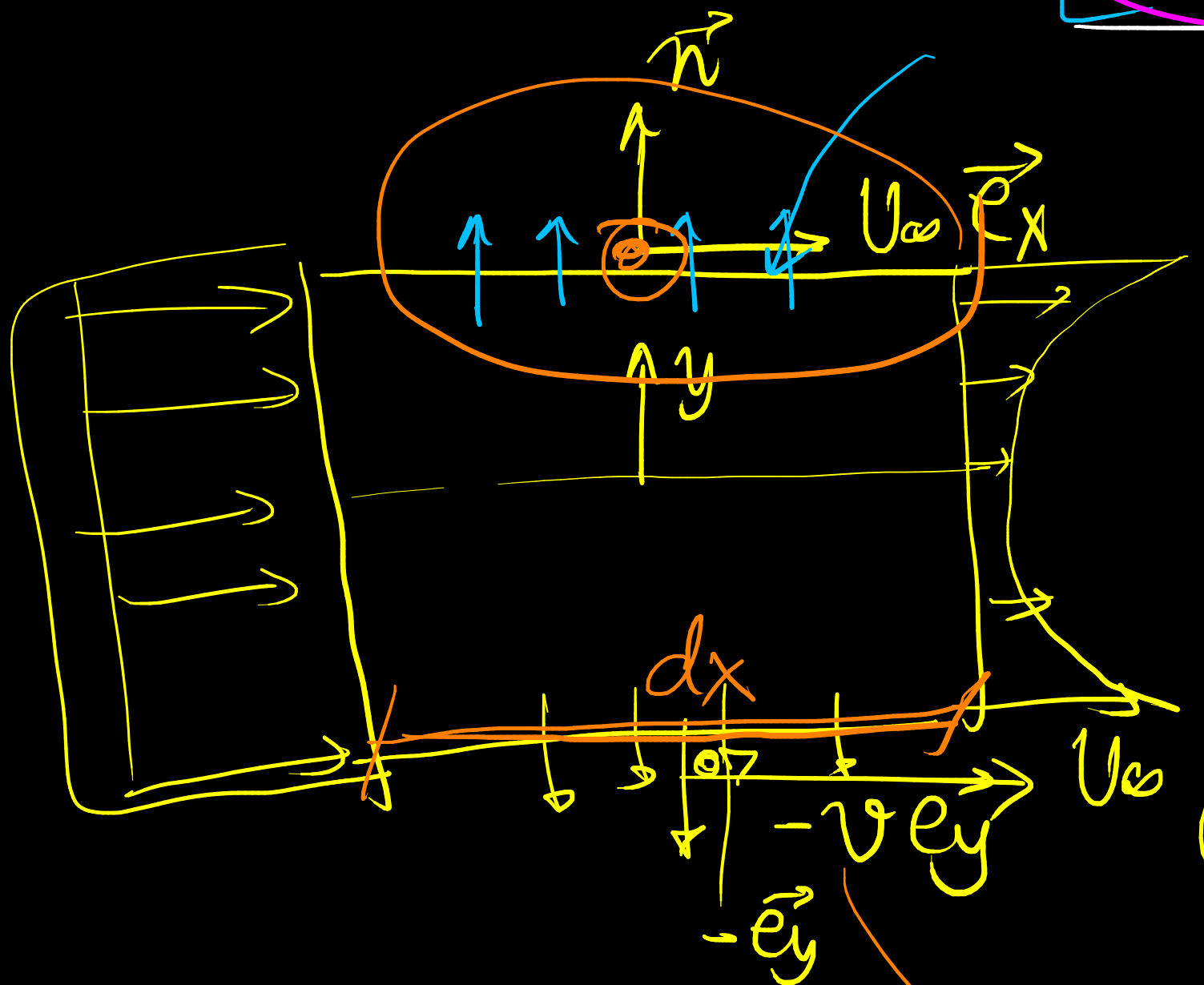
$$\int \boxed{v dx} l$$

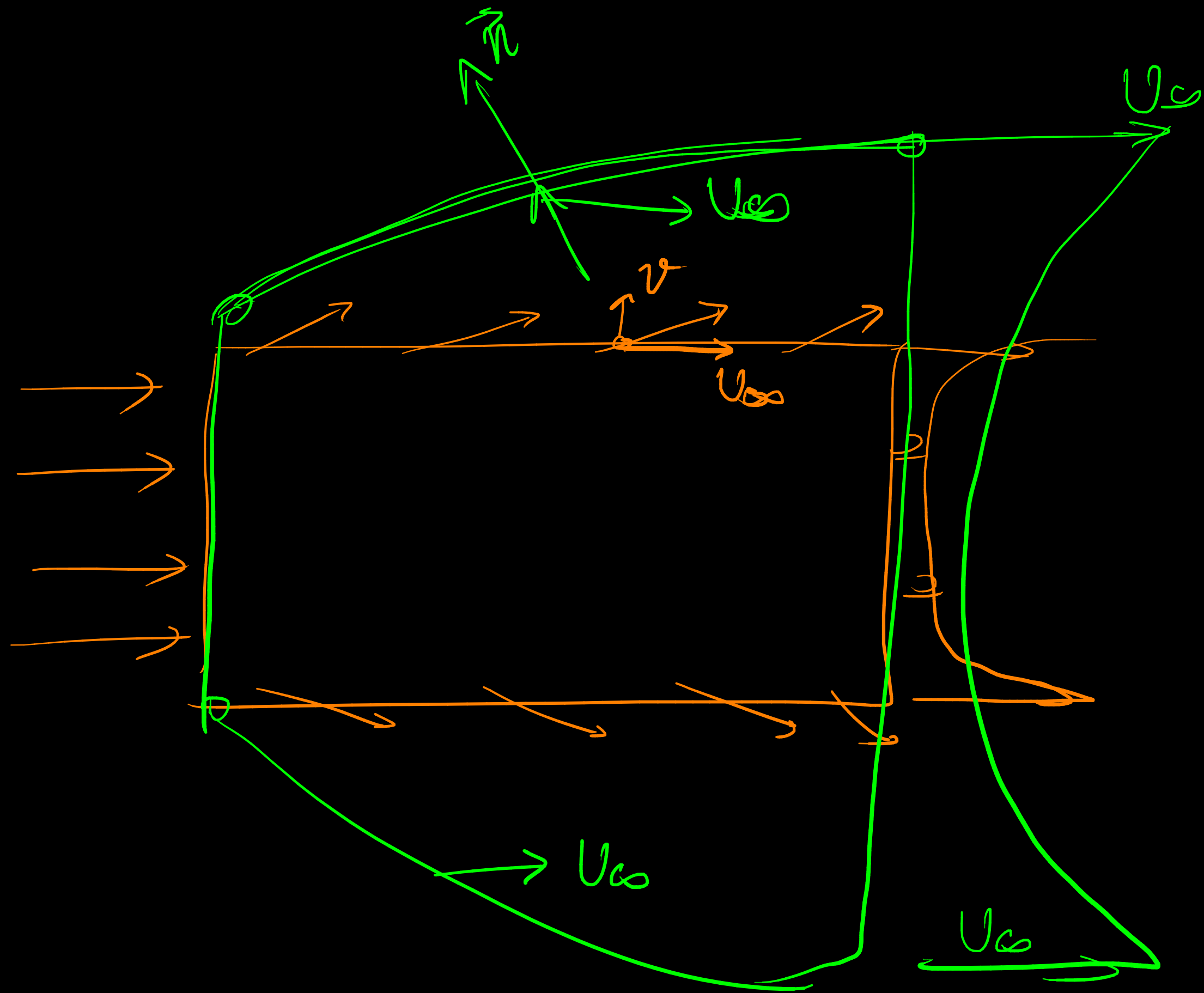
$$\int \rho U_\infty v dx \quad l$$

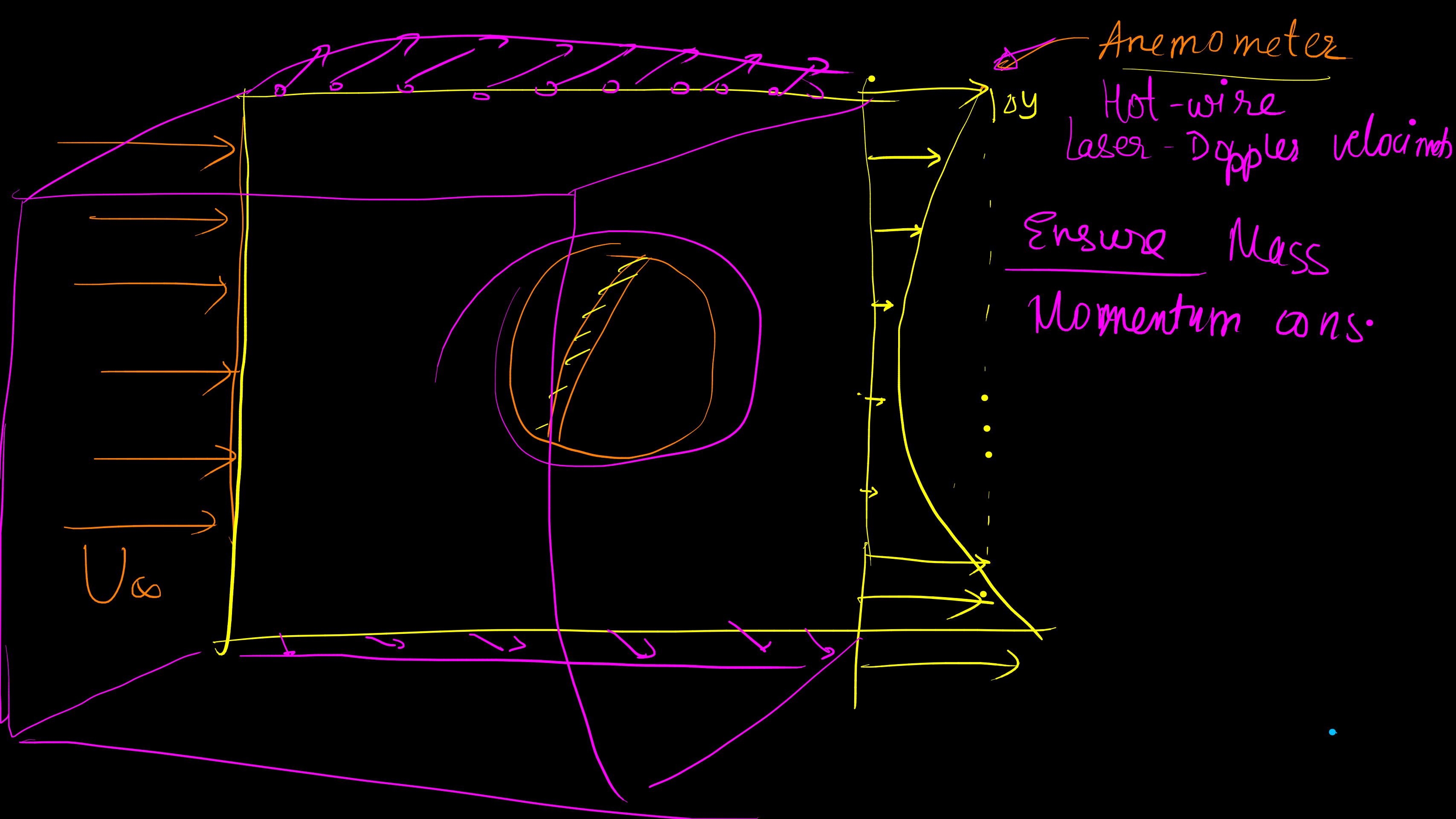
$$\int \rho v v dx$$

$$(U_\infty \vec{e}_x - v \vec{e}_y)$$

$$\int -\rho v v dx$$







Anemometer

Hot-wire
Laser-Doppler velocimetry

Ensure Mass
Momentum cons.

