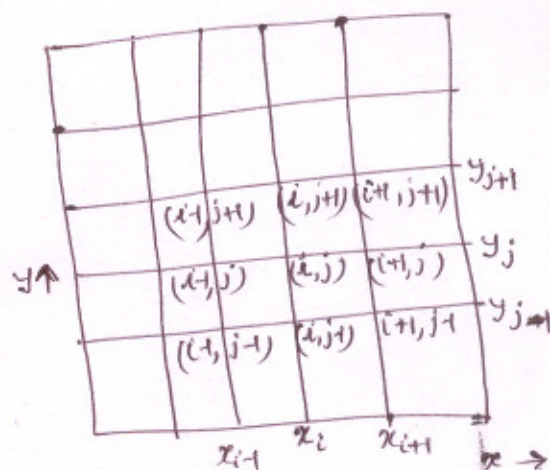
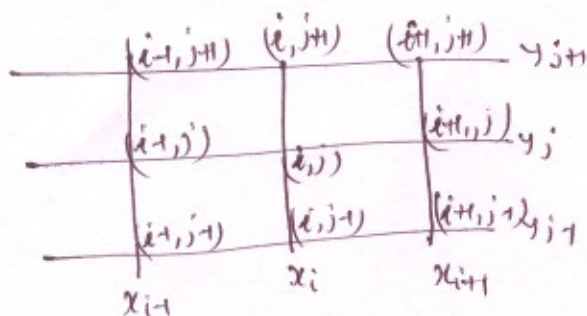


$$\nabla^2 u = u_{xx} + u_{yy}$$



① Explicit method (Five point)

$$u_{xx} + u_{yy} = \frac{1}{h^2} \begin{bmatrix} 1 & -4 & 1 \\ & & \\ & & \end{bmatrix}$$

② Five point diagonal

$$u_{xx} + u_{yy} = \frac{1}{2h^2} \begin{bmatrix} 1 & 0 & 1 \\ 0 & -4 & 0 \\ 1 & 0 & 1 \end{bmatrix}$$

$$\frac{1}{2h^2} [u(x-h, y+h) + u(x+h, y+h) - 4u(x, y) + u(x-h, y-h) + u(x+h, y-h)]$$

$$= (u_{xx} + u_{yy}) + \frac{h^4}{12} \left( \frac{\partial^4 u}{\partial x^4} + 6 \frac{\partial^4 u}{\partial x^2 \partial y^2} + \frac{\partial^4 u}{\partial y^4} \right) + O(h^6).$$

Parabolic PDE  
Dufort-Frankel method

①

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} \quad \text{--- (1) one dimensional diffusion eq.}$$

$$\left. \frac{\partial u}{\partial t} \right|_{(x_i, t_j)} = \left. \frac{\partial^2 u}{\partial x^2} \right|_{(x_i, t_j)}$$

$$\frac{u_i^{j+1} - u_i^{j-1}}{2\Delta t} = \frac{u_{i-1}^j - 2u_i^j + u_{i+1}^j}{\Delta x^2} \quad \text{--- (2)}$$

Now  $y(n+h) = y(n) + h y'(n) + \frac{h^2}{2!} y''(n) + \dots$

$$y(n-h) = y(n) - h y'(n) + \frac{h^2}{2!} y''(n) - \dots$$

$$y(n+h) + y(n-h) = 2y(n) + 2\frac{h^2}{2!} y''(n) + \dots$$

$$\frac{1}{2} [y(n+h) + y(n-h)] = y(n) + O(h^2)$$

$$\text{or } y(n) = \frac{1}{2} [y(n+h) + y(n-h)] + O(h^2)$$

$$\text{So } u_i^j = \frac{1}{2} (u_i^{j+1} + u_i^{j-1}) + O(\Delta t)^2 \quad \text{--- (3)}$$

Now use (3) in (2) we get-

$$\frac{u_i^{j+1} - u_i^{j-1}}{2\Delta t} = \frac{1}{(\Delta x)^2} [u_{i-1}^j - (u_i^{j+1} + u_i^{j-1}) + u_{i+1}^j]$$

$$u_i^{j+1} - u_i^{j-1} = \frac{2\Delta t}{(\Delta x)^2} [u_{i-1}^j - (u_i^{j+1} + u_i^{j-1}) + u_{i+1}^j]$$

Take  $r = \frac{\Delta t}{\Delta x^2}$  mesh ratio parameter

$$(1+2r)u_i^{j+1} - (1-2r)u_i^{j-1} - 2ru_{i+1}^j - 2ru_{i-1}^j = 0$$



or

$$u_t - u_{nn} = \begin{bmatrix} 0 & 1+2r & 0 \\ -2r & 0 & -2r \\ 0 & -1+2r & 0 \end{bmatrix} u_i^j$$

or

$$u_i^{j+1} = \frac{1-2r}{1+2r} u_i^j + \frac{2r}{1+2r} u_{i+1}^j + \frac{2r}{1+2r} u_{i-1}^j$$

$j=1, 2, \dots$

for  $j=1$

$$u_i^2 = \frac{1-2r}{1+2r} u_i^1 + \frac{2r}{1+2r} u_{i+1}^1 + \frac{2r}{1+2r} u_{i-1}^1$$

So we require  $u_i^1$ 's which may be calculate from some other method, e.g., explicit method.

Ex Solve the heat conduction equation (Iyengar P 21)

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2}$$

subject to the initial and boundary conditions

$$u(x, 0) = \sin \pi x, \quad 0 \leq x \leq 1$$

$$u(0, t) = u(1, t) = 0$$

using the following methods

(i) the Schmidt method

(ii) the Laasonen method

(iii) the Crank-Nicolson method

(iv) the Dufort-Frankel method

for  $\Delta x = 1/3$  ( $h = 1/3$ ) and  $\Delta t = 1/36$  ( $k = 1/36$ ).

# Parabolic PDE

①

## Unsteady Heat flow Equation or Diffusion Equation

$$\frac{\partial^2 u}{\partial x^2} = \frac{c\rho}{K} \frac{\partial u}{\partial t} \quad \text{--- (1)}$$

With boundary conditions

B.C.  $u(0,t) = C_1$  ,  $u(L,t) = C_2$  --- (2)

or  $A_1 u(0,t) + B_1 \frac{\partial u}{\partial x}(0,t) = F_1(t)$

$$A_2 u(L,t) + B_2 \frac{\partial u}{\partial x}(L,t) = F_2(t)$$

and

I.C.  $u(x,t)|_{t=0} = f(x)$  --- (3)

### Schmidt method

Explicit Method Using central difference approximation for  $\frac{\partial^2 u}{\partial x^2}$  and forward for  $\frac{\partial u}{\partial t}$  we get-  
 $u(x_i, t_j) = u_i^j$

$$\frac{\partial^2 u}{\partial x^2}(x_i, t_j) = \frac{c\rho}{K} \frac{\partial u}{\partial t}(x_i, t_j)$$

$$\frac{u_{i+1}^j - 2u_i^j + u_{i-1}^j}{\Delta x^2} = \frac{c\rho}{K} \frac{u_i^{j+1} - u_i^j}{\Delta t}$$

$$\frac{K\Delta t}{c\rho\Delta x^2} (u_{i+1}^j - 2u_i^j + u_{i-1}^j) + u_i^j = u_i^{j+1}$$

$$\text{or } u_i^{j+1} = \frac{K\Delta t}{c\rho\Delta x^2} (u_{i+1}^j + u_{i-1}^j) + \left(1 - 2\frac{K\Delta t}{c\rho\Delta x^2}\right) u_i^j \quad \text{--- (4)}$$

If the ratio is chosen so that

$$r = \frac{K\Delta t}{c\rho\Delta x^2} = \frac{1}{2} \quad \text{--- (5)}$$

then (4) becomes

$$u_i^{j+1} = \frac{1}{2} (u_{i+1}^j + u_{i-1}^j) \quad \text{--- (6)}$$



Ex. A large <sup>flat</sup> steel plate is 2 cm thick. If the initial temperature ( $^{\circ}\text{C}$ ) with in the plate are given as a function of distance from one face by the equation

$$u(x,t)|_{t=0} = 100 \sin \frac{\pi x}{2}$$

find the temperature as a function of  $x$  and  $t$  if both faces are maintained at  $0^{\circ}\text{C}$ .

i.e. B.C.  $u(0,t) = u(2,t) = 0$

I.C.  $u(x,0) = 100 \sin \frac{\pi x}{2}$

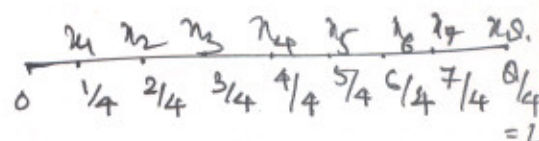
for steel  $k = 0.13 \text{ cal/sec.cm.}^{\circ}\text{C}$

$c = 0.11 \text{ cal/g.}^{\circ}\text{C}$

$\rho = 7.8 \text{ g/cm}^3$

Let  $\Delta x = 0.25$ , gives eight subdiv. of  $x$ -axis.

$\frac{k\Delta t}{c\rho\Delta x^2} = \frac{1}{2} \Rightarrow \Delta t = 0.206 \text{ sec}$



for  $t_0 = 0, t_1 = \Delta t = .206, t_2 = .412, t_3 = .619, \dots$

for  $t = 0$  from (6)

$$u_i^1 = \frac{1}{2} (u_{i+1}^0 + u_{i-1}^0)$$

Now for  $x = x_1$   
i.e.  $i = 1$

$$u_1^1 = \frac{1}{2} (u_2^0 + u_0^0)$$

boundary condition

Similarly for

$i = 7$

$$u_7^1 = \frac{1}{2} (u_8^0 + u_6^0)$$

boundary condition

# Numerical Solution to heat flow example

(3)

t =	x = 0	$\lambda = .25$	$\lambda = .50$	$\lambda = .75$	$\lambda = 1.0$	$\lambda = 1.25$
0	0	30.3	70.7	92.4	100	92.4
.206	0	35.35	65.35	85.35	92.4	85.35
.412	0	32.68	60.35	78.88	85.35	78.88
.619	0	30.18	55.78	77.06	77.08	72.06
.825	0	27.89	51.52	67.33	72.06	67.33
1.031	0	25.76	47.61	62.19	67.33	62.19
	0					

For  $j=0$   $u_i^j = \frac{1}{2} (u_{i+1}^0 + u_{i-1}^0)$

$x_1$   $i=1$   $u_1^1 = \frac{1}{2} (u_2^0 + u_0^0)$   $\rightarrow$  b.c.

$x_2$   $i=2$   $u_2^1 = \frac{1}{2} (u_3^0 + u_1^0)$

$x_3$   $i=3$   $u_3^1 = \frac{1}{2} (u_4^0 + u_2^0)$

Then  $u_i^1$ 's are known, Next-

for  $j=1$   $u_i^2 = \frac{1}{2} (u_{i+1}^1 + u_{i-1}^1)$

$x_1$   $i=1$   $u_1^2 = \frac{1}{2} (u_2^1 + u_0^1)$



# Crank-Nicolson Method (Implicit Method).

(4)

$$\frac{\partial^2 u}{\partial x^2} \bigg|_{(x_i, t_{j+1/2})} = \frac{c \rho}{k} \frac{\partial u}{\partial t} \bigg|_{(x_i, t_{j+1/2})}$$

Central  
 $y'(x) = \frac{y(x+h) - y(x-h)}{2h} + O(h^2)$

Central with spacing  $h/2$   
 $y'(x) = \frac{y(x+h/2) - y(x-h/2)}{h} + O(h^2)$

$$\begin{aligned} y(x+h/2) &= y(x) + h/2 y'(x) + O(h^2) \\ &= y(x) + \frac{1}{2} (y(x+h) - y(x)) + O(h^2) \\ &= \frac{1}{2} [y(x+h) + y(x)] + O(h^2) \end{aligned}$$

$$\frac{1}{2} \left[ \frac{\partial^2 u}{\partial x^2} \bigg|_{(x_i, t_{j+1})} + \frac{\partial^2 u}{\partial x^2} \bigg|_{(x_i, t_j)} \right] = \frac{c \rho}{k} \frac{\partial u}{\partial t} \bigg|_{(x_i, t_{j+1/2})}$$

Central difference  
Approximation

Central difference  
Approximation with  
 $\Delta t/2$  as spacing

$$\begin{aligned} \frac{1}{2} \left[ \frac{u_{i+1}^{j+1} - 2u_i^{j+1} + u_{i-1}^{j+1}}{\Delta x^2} + \frac{u_{i+1}^j - 2u_i^j + u_{i-1}^j}{\Delta x^2} \right] &= \frac{c \rho}{k} \left[ \frac{u_i^{j+1} - u_i^j}{\Delta t} \right] \end{aligned}$$

$$\begin{aligned} \frac{k \Delta t}{2 c \rho \Delta x^2} [u_{i+1}^{j+1} - 2u_i^{j+1} + u_{i-1}^{j+1} + u_{i+1}^j - 2u_i^j + u_{i-1}^j] &= u_i^{j+1} - u_i^j \end{aligned}$$

Take  $r = \frac{k \Delta t}{c \rho \Delta x^2}$

$$r [u_{i+1}^{j+1} - 2u_i^{j+1} + u_{i-1}^{j+1} + u_{i+1}^j - 2u_i^j + u_{i-1}^j] = 2u_i^{j+1} - 2u_i^j$$

$$r u_{i+1}^{j+1} - (2+2r) u_i^{j+1} + r u_{i-1}^{j+1} = -r u_{i+1}^j + (2r-2) u_i^j - r u_{i-1}^j$$

Multiply by  $-1$  on both sides we get-

$$-r u_{i-1}^{j+1} + (2+2r) u_i^{j+1} - r u_{i+1}^{j+1} = r u_{i-1}^j + (2-2r) u_i^j + r u_{i+1}^j$$

$r$  is called mesh ratio parameter

The advantage of the Crank-Nicolson method is that it is stable for any value of  $r$ , although small values are more accurate. Values much larger than unity are not desirable.

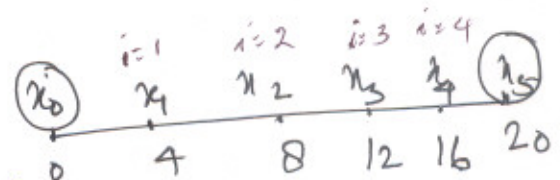
Ex  $\frac{\partial^2 u}{\partial x^2} = \frac{1}{D} \frac{\partial u}{\partial t} \Big|_{\substack{\text{I.C. } u(x,0) = 2.0 \\ \text{B.C.}}}$

$D = 0.119 \text{ cm}^2/\text{sec}$

$u(0,t) = 0.0$

$u(20,t) = 10.0$

Take  $\frac{D \Delta t}{(\Delta x)^2} = 1$ , &  $\Delta x = 4$



then  $\Delta t = 134.4 \text{ sec.}$

for  $r=1$

for  $j=0$  or  $u_{i+1}^{j+1} - 4u_i^{j+1} + u_{i-1}^{j+1} = -u_{i+1}^j - u_{i-1}^j$   
 $-u_{i-1}^{j+1} + 4u_i^{j+1} - u_{i+1}^{j+1} = u_{i-1}^j + u_{i+1}^j$

$i=1$   $-0 + 4u_1 - u_2 = 0 + 2$

$i=2$   $-u_1 + 4u_2 - u_3 = 2 + 2$

$i=3$   $-u_2 + 4u_3 - u_4 = 2 + 2$

$i=4$   $-u_3 + 4u_4 - 10 = 2 + 10.$

or

$4u_1 - u_2 = 2$

$-u_1 + 4u_2 - u_3 = 4$

$-u_2 + 4u_3 - u_4 = 4$

$-u_3 + 4u_4 = 22$

$$\begin{bmatrix} 4 & -1 & 0 & 0 \\ -1 & 4 & -1 & 0 \\ 0 & -1 & 4 & -1 \\ 0 & 0 & -1 & 4 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} = \begin{bmatrix} 2 \\ 4 \\ 4 \\ 22 \end{bmatrix}$$



time in sec	$\lambda=4$	$\lambda=8$	$\lambda=12$	$\lambda=16$
134.4	.986	2.019	3.072	5.992
268.8	1.070	2.363	4.305	6.555
403.2	1.276	2.961	4.762	6.962
537.6	1.471	3.165	5.115	7.159

Convergence of Explicit Method :

$$\frac{\partial U}{\partial t} = \frac{k}{c\rho} \frac{\partial^2 U}{\partial x^2} \quad \text{--- (1)}$$

Explicit method

$$u_i^{j+1} = \frac{k\Delta t}{c\rho\Delta x^2} (u_{i+1}^j + u_{i-1}^j) + \left(1 - \frac{2k\Delta t}{c\rho\Delta x^2}\right) u_i^j$$

Let  $r = \frac{k\Delta t}{c\rho\Delta x^2}$  then

$$u_i^{j+1} = r(u_{i+1}^j + u_{i-1}^j) + (1-2r)u_i^j \quad \text{--- (2)}$$

$u$  - Numerical solution,  $U$  - exact solution

Error  $e = U - u$  or  $u = U - e$

Substituting  $u$  in (2) we get-

$$u_i^{j+1} - e_i^{j+1} = r(u_{i+1}^j - e_{i+1}^j + u_{i-1}^j - e_{i-1}^j) + (1-2r)(u_i^j - e_i^j)$$

$$-e_i^{j+1} = r(u_{i+1}^j + u_{i-1}^j) - r(e_{i+1}^j + e_{i-1}^j) + (1-2r)u_i^j - (1-2r)e_i^j - u_i^{j+1}$$

$$e_i^{j+1} = r(e_{i+1}^j + e_{i-1}^j) - r(u_{i+1}^j + u_{i-1}^j) + (1-2r)e_i^j - (1-2r)u_i^j + u_i^{j+1}$$

$$e_i^{j+1} = r(e_{i+1}^j + e_{i-1}^j) + (1-2r)e_i^j - r(u_{i+1}^j + u_{i-1}^j) - (1-2r)u_i^j + u_i^{j+1} \quad (7)$$

Now

$$u_{i+1}^j = u_i^j + \left(\frac{\partial u}{\partial x}\right)_{i,j} \Delta x + \frac{(\Delta x)^2}{2!} \left(\frac{\partial^2 u}{\partial x^2}\right)(\bar{x}_1, t_j) \quad x_i < \bar{x}_1 < x_{i+1}$$

$$u_{i-1}^j = u_i^j - \left(\frac{\partial u}{\partial x}\right)_{i,j} \Delta x + \frac{(\Delta x)^2}{2!} \left(\frac{\partial^2 u}{\partial x^2}\right)(\bar{x}_2, t_j) \quad x_{i-1} < \bar{x}_2 < x_i$$

$$u_{i+1}^j + u_{i-1}^j = 2u_i^j + (\Delta x)^2 \left(\frac{\partial^2 u}{\partial x^2}\right)(\bar{x}, t_j) \quad x_{i-1} < \bar{x} < x_{i+1}$$

$$u_i^{j+1} = u_i^j + \left(\frac{\partial u}{\partial t}\right)(x_i, \eta) \Delta t \quad t_j < \eta < t_{j+1}$$

Then from (3)

$$e_i^{j+1} = r(e_{i+1}^j + e_{i-1}^j) + (1-2r)e_i^j - \cancel{2r}u_i^j - \frac{(\Delta x)^2}{2!} \left(\frac{\partial^2 u}{\partial x^2}\right)(\bar{x}, t_j) - (1-2r)u_i^j + \cancel{u_i^j} + \Delta t \left(\frac{\partial u}{\partial t}\right)(x_i, \eta)$$

$$e_i^{j+1} = r(e_{i+1}^j + e_{i-1}^j) + (1-2r)e_i^j - \frac{k \Delta t}{c \rho} \left(\frac{\partial^2 u}{\partial x^2}\right)(\bar{x}, t_j) - \Delta t \left(\frac{\partial u}{\partial t}\right)(x_i, \eta)$$

$$e_i^{j+1} = r(e_{i+1}^j + e_{i-1}^j) + (1-2r)e_i^j - \Delta t \left[ \frac{k}{c \rho} \frac{\partial^2 u}{\partial x^2}(\bar{x}, t_j) - \left(\frac{\partial u}{\partial t}\right)(x_i, \eta) \right]$$

$$\text{Now take } 0 < r \leq \frac{1}{2} \quad (2r \leq 1 \text{ w } 1-2r \geq 0) \quad \text{--- (4)}$$

$$|e_i^{j+1}| \leq r(|e_{i+1}^j| + |e_{i-1}^j|) + (1-2r)|e_i^j| + M \Delta t \quad \text{--- (5)}$$

$$\text{Let } \exists M \text{ s.t. } \left| \frac{k}{c \rho} \frac{\partial^2 u}{\partial x^2}(\bar{x}, t_j) - \left(\frac{\partial u}{\partial t}\right)(x_i, \eta) \right| < M$$

$$\text{Take } E^j = \max_i |e_i^j|$$

$$\text{from (5)} \quad |e_i^{j+1}| \leq r(E^j + E^j) + (1-2r)E^j + M \Delta t$$



$$|e_i^{j+1}| \leq E^j + M \Delta t$$

This is true for each  $i$  as r.h.s is independent of  $i$

$$\max_i |e_i^{j+1}| \leq E^j + M \Delta t$$

$$E^{j+1} \leq E^j + M \Delta t \leq E^{j+1} + 2M \Delta t \dots$$

$$\leq E^{j-j} + (j+1)M \Delta t$$

$$= E^0 + M(j+1)\Delta t = E^0 + M t_{j+1}$$

$E^0$  is error at  $t=0$ , so  $E^0=0$  since initial conditions are given

$$\text{So } E^{j+1} \leq M t_{j+1}$$

$$r = \frac{k \Delta t}{c \rho \Delta x^2} \leq \frac{1}{2} \quad \sim \quad \Delta t \leq \frac{1}{2} \frac{c \rho}{k} (\Delta x)^2$$

Now, as  $\Delta x \rightarrow 0$ ,  $\Delta t \rightarrow 0$  and

$$\frac{k}{c \rho} \frac{\partial^2 u}{\partial x^2}(\bar{x}_i, t_j) - \frac{\partial u}{\partial t}(\bar{x}_i, t_j) \rightarrow \left( \frac{k}{c \rho} \frac{\partial^2 u}{\partial x^2} - \frac{\partial u}{\partial t} \right)_{i,j} = 0$$

i.e.  $M \rightarrow 0$  and thus the error goes to zero and the explicit method is convergent for  $r \leq \frac{1}{2}$ .

*M...*

Laasonen method:

$$\frac{\partial^2 u}{\partial x^2} = \frac{c \rho}{k} \frac{\partial u}{\partial t}$$

$$\frac{u_{i+1}^j - 2u_i^j + u_{i-1}^j}{\Delta x^2} = \frac{c \rho}{k} \frac{u_i^j - u_i^{j-1}}{\Delta t}$$

$$\frac{k \Delta t}{c \rho \Delta x^2} (u_{i+1}^j - 2u_i^j + u_{i-1}^j) = u_i^j - u_i^{j-1}$$

$$r (u_{i+1}^j - 2u_i^j + u_{i-1}^j) = u_i^j - u_i^{j-1} \quad r = \frac{k \Delta t}{c \rho \Delta x^2}$$

$$-r (u_{i+1}^j - 2u_i^j + u_{i-1}^j) = u_i^{j-1} - u_i^j$$

$$-r u_{i+1}^j + (1+2r) u_i^j - r u_{i-1}^j = u_i^{j-1}$$

$$\text{or, } -r u_{i+1}^{j+1} + (1+2r) u_i^{j+1} - r u_{i-1}^{j+1} = u_i^j$$

for j=0

$$-r u_{i+1}^1 + (1+2r) u_i^1 - r u_{i-1}^1 = u_i^0$$

i=1

$$-r u_0^1 + (1+2r) u_1^1 - r u_2^1 = u_1^0$$

$$\xrightarrow{\text{BC}} (1+2r) u_1^1 - r u_2^1 = u_1^0 + r u_0^1 \xrightarrow{\text{IC}}$$

i=2

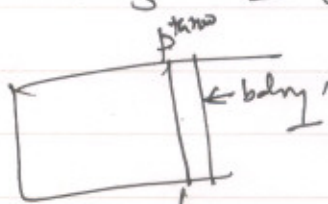
$$-r u_1^1 + (1+2r) u_2^1 - r u_3^1 = u_2^0$$

for p no. of rows

i=p (last value of i)

$$-r u_{p-1}^1 + (1+2r) u_p^1 - r u_{p+1}^1 = u_p^0$$

$$-r u_{p+1}^1 + (1+2r) u_p^1 = u_p^0 + r u_{p+1}^1$$





### Derivative B.C. for Explicit method

$$u_i^{j+1} = r(u_{i+1}^j + u_{i-1}^j) + (1-2r)u_i^j \quad \text{--- } (*)$$

Suppose we have boundary condition of the type

$$\alpha_1 u(0,t) + \beta_1 \frac{\partial u}{\partial x}(0,t) = F_1(t) \quad \text{--- } (1)$$

and

$$\alpha_2 u(b,t) + \beta_2 \frac{\partial u}{\partial x}(b,t) = F_2(t) \quad \text{--- } (2)$$

From (\*) for  $i=0$

$$u_0^{j+1} = r(u_1^j + u_L^j) + (1-2r)u_0^j \quad \text{--- } (3)$$

Now from b.c. (1)

$$\alpha_1 u_0^j + \beta_1 \frac{\partial u}{\partial x}(0,t_j) = F_1(t_j)$$

$$\text{or } \alpha_1 u_0^j + \beta_1 \frac{u_1^j - u_L^j}{2\Delta x} = F_1(t_j) \quad \text{--- } (4)$$

Then eliminating  $u_L^j$  from (3) & (4) we get appropriate discretization.

Similarly for  $i=N$  from (\*) (where total  $N$  number of subdivisions are there for  $x$ -axis).

$$u_N^{j+1} = r(u_R^j + u_{N-1}^j) + (1-2r)u_N^j \quad \text{--- } (5)$$

Now from b.c (2)

$$\alpha_2 u_N^j + \beta_2 \frac{\partial u}{\partial x}(N,t_j) = F_2(t_j)$$

$$\alpha_2 u_N^j + \beta_2 \frac{u_R^j - u_{N-1}^j}{2\Delta x} = F_2(t_j) \quad \text{--- } (6)$$

Now eliminating  $u_R$  from (5) & (6) we get appropriate discretization.

Derivative boundary condition (Explicit method)

$$u_i^{j+1} = r(u_{i+1}^j + u_{i-1}^j) + (1-2r)u_i^j \quad \text{--- (†)}$$

$$\underline{i=0} \quad u_0^{j+1} = r(u_1^j + u_L^j) + (1-2r)u_0^j \quad \text{--- (*)}$$

Now from the derivative B.C. at  $x=0$

$$A_1 u(0,t) + B_1 \frac{\partial u}{\partial x}(0,t) = F_1(t)$$

$$A_1 u_0^j + B_1 \frac{\partial u}{\partial x}(0, t_j) = F_1(t_j)$$

$$f'(0) = \frac{f_1 - f_{-1}}{2\Delta x}$$

$$A_1 u_0^j + B_1 \frac{u_1^j - u_L^j}{2\Delta x} = F_1(t_j) \quad \text{--- (**)}$$

So from (\*) & (\*\*)  $u_L^j$  can be eliminated.

Similarly for other B.C. at  $x=L$

$$A_2 u(b,t) + B_2 \frac{\partial u}{\partial x}(b,t) = F_2(t) \quad \text{--- (1)}$$

From (†) for  $i=b$

$$u_b^{j+1} = r(u_R^j + u_{b-1}^j) + (1-2r)u_b^j \quad \text{--- (2)}$$

Now from (1)

$$A_2 u_b^j + B_2 \frac{(u_R^j - u_b^j)}{2\Delta x} = F_2(t_j)$$

$$f'(b) = \frac{f_R - f_{b-1}}{2\Delta x}$$

So from (2) and (3)  $u_R^j$  can be eliminated. (3)