

# Optimal Strain Sensor Placement Strategy for Deepwater Risers

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# Outline

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**I. Background**

**II. FEM Modelling**

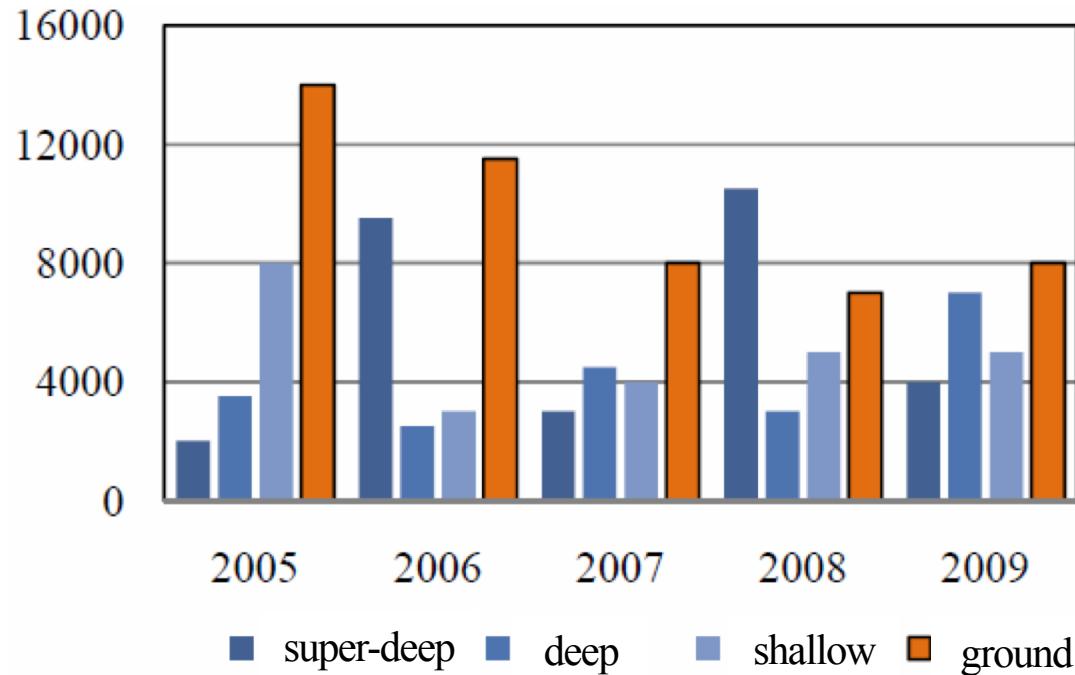
**III. Optimal Sensor Placement Strategy**

**IV. Discussion**

# I.1 Research Need



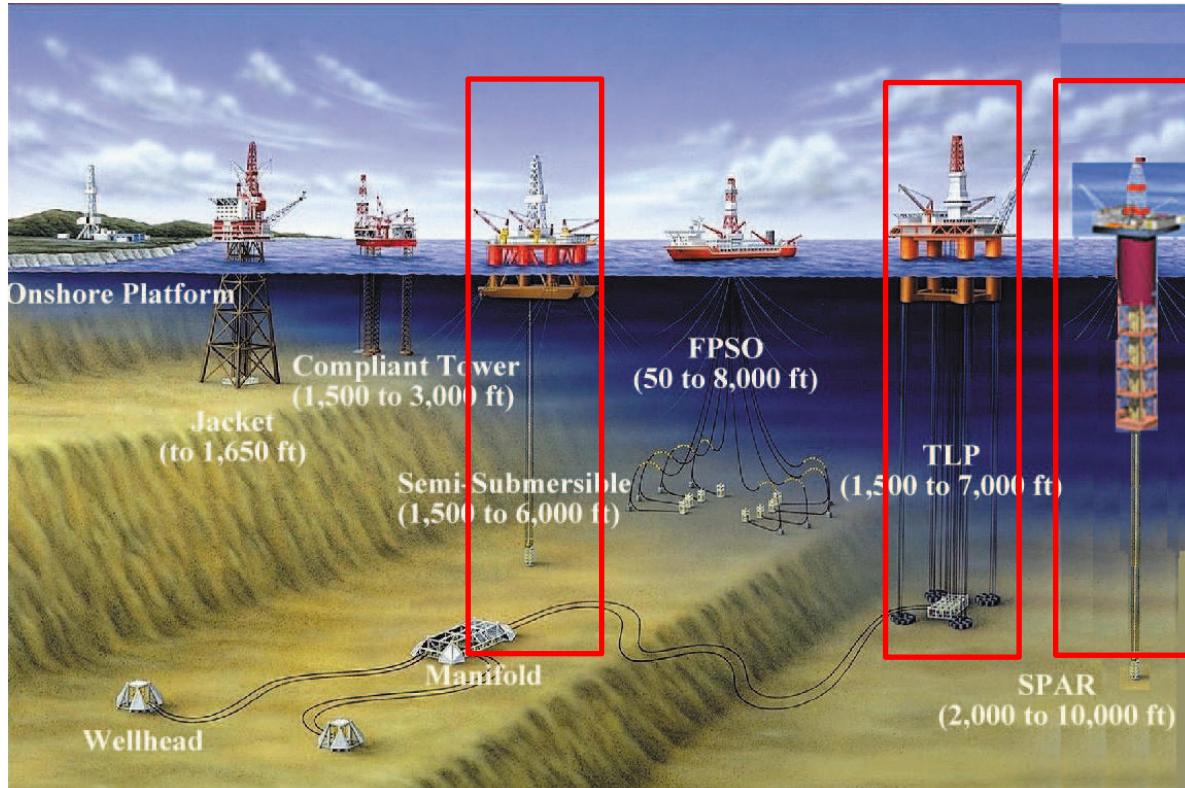
Ocean contains **70%** of the total oil and natural-gas on earth, and in 2015, **12%** are drilled from deep water ( $\geq 900\text{m}$ ).



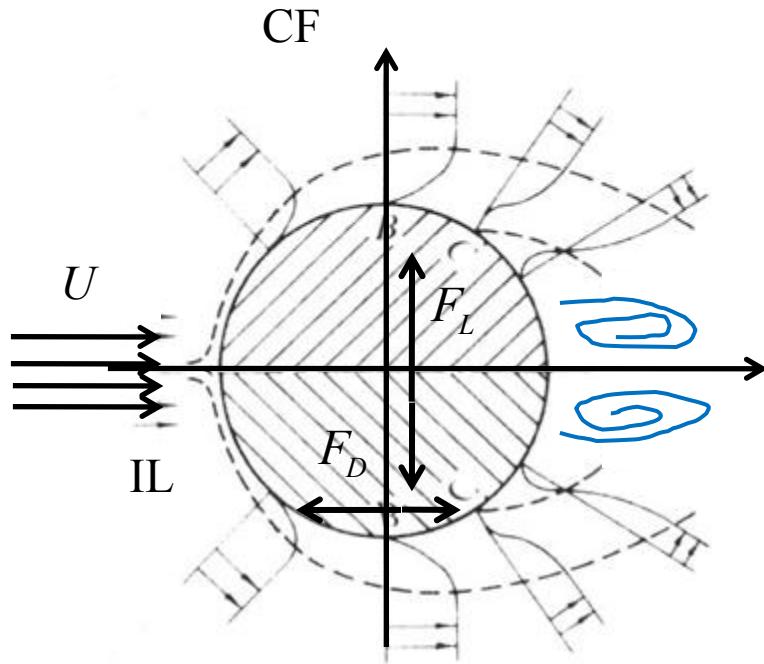
# I.2 Types of Platform



Semi-submersible, **tension-leg (TLP)**, SPAR, FPSO, etc



# I.3 Vortex-induced Vibration: Mechanism



$$F_L = \frac{1}{2} C_L \left( \frac{A}{D} \right) \rho_w D (U_z - \frac{\partial x}{\partial t})^2 \cos \omega_s t$$

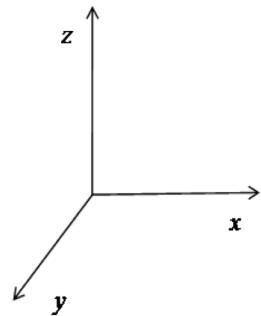
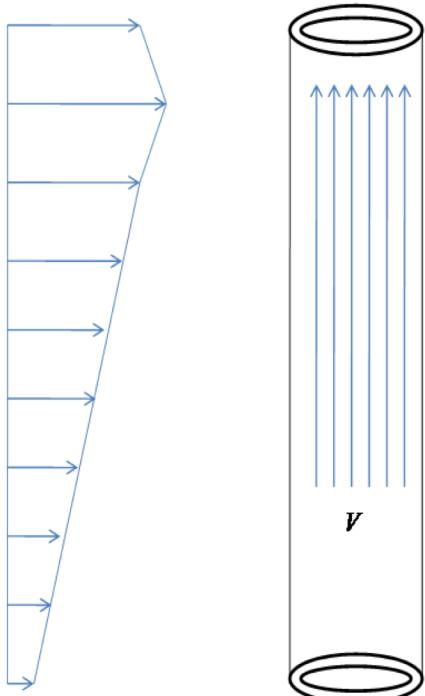
$$F'_D = \frac{1}{2} C'_D \rho_w D U_z^2 \cos \omega'_s t$$

# I.4 Vortex-induced Vibration: Damage on Risers



Time	Cause	Description	Leakage (Barrel)
2002	VIV	Connection Failure from platform	267
2003	Storm	Breakage	1421
2003	Ocean current	Breakage due to fatigue	74
2003	VIV	Breakage due to fatigue	137
2004	Wave load	Connection Failure from platform	48
2004	Storm	Connection Failure from platform	1034
2005	Wave load	Connection Failure from platform	426

# II. Modelling: FEM



The figure shows two free body diagrams of a cylindrical element of length  $dz$  and cross-sectional area  $A_i$ .

**Vertical Force Balance:**

$$\rho_f A_i \left( \frac{\partial^2 y}{\partial t^2} + V^2 \frac{\partial^2 y}{\partial z^2} + 2V \frac{\partial^2 y}{\partial z \partial t} \right) dz$$

$$A_i P_i + A_i \frac{\partial P_i}{\partial z} dz - q dz - q dz - \rho_f A_i g dz = 0$$

$$\sum F_z = 0$$

$$\sum F_y = 0$$

**Horizontal Force Balance:**

$$( \frac{1}{2} (C_s + C_h) \frac{\partial y}{\partial t} + \frac{1}{4} C_m \rho_w \pi D^2 \frac{\partial^2 y}{\partial t^2} ) dz$$

$$T + \frac{\partial T}{\partial z} dz - A_o P_o + A_o \frac{\partial P_o}{\partial z} dz - M + \frac{\partial M}{\partial z} dz - Q + \frac{\partial Q}{\partial z} dz - q dz - q dz - F_L dz - \rho_r A_r g dz - \rho_r A_r \frac{\partial^2 y}{\partial t^2} dz = 0$$

$$\sum F_z = 0$$

$$\sum F_y = 0$$

$$\sum M = 0$$

# II. Modelling: FEM

- **Dynamic Equation**

- Cross-flow

$$m \frac{\partial^2 y}{\partial t^2} + (C_s + C_h) \frac{\partial y}{\partial t} + \frac{\partial}{\partial z} \left\{ [m_f V^2 - T_{top} + (m_r + m_f - \rho_w A_o) g (L - z)] \frac{\partial y}{\partial z} \right\} + EI \frac{\partial^4 y}{\partial z^4} = \frac{1}{2} C_L \left( \frac{A}{D} \right) \rho_w D (U - \frac{\partial x}{\partial t})^2 \cos \omega_s t$$

- In-flow

$$m \frac{\partial^2 x}{\partial t^2} + (C_s + C_h) \frac{\partial x}{\partial t} + \frac{\partial}{\partial z} \left\{ [m_f V^2 - T_{top} + (m_r + m_f - \rho_w A_o) g (L - z)] \frac{\partial x}{\partial z} \right\} + EI \frac{\partial^4 x}{\partial z^4} = \frac{1}{2} C_D \rho_w D U^2 \cos \omega_s t$$

# II. Modelling: Modal Analysis

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- **Modal Analysis**

$$[M][\ddot{u}] + [C][\dot{u}] + [K][u] = [F]$$

$$[u] = \sum_n \phi_n q_n(t)$$

$$M_r \ddot{q}_r(t) + C_r \dot{q}_r(t) + K_r q_r(t) = F_r(t)$$

$$M_r = \phi_r^T [M] \phi_r \quad C_r = \phi_r^T [C] \phi_r \quad K_r = \phi_r^T [K] \phi_r \quad F_r(t) = \phi_r^T [F]$$

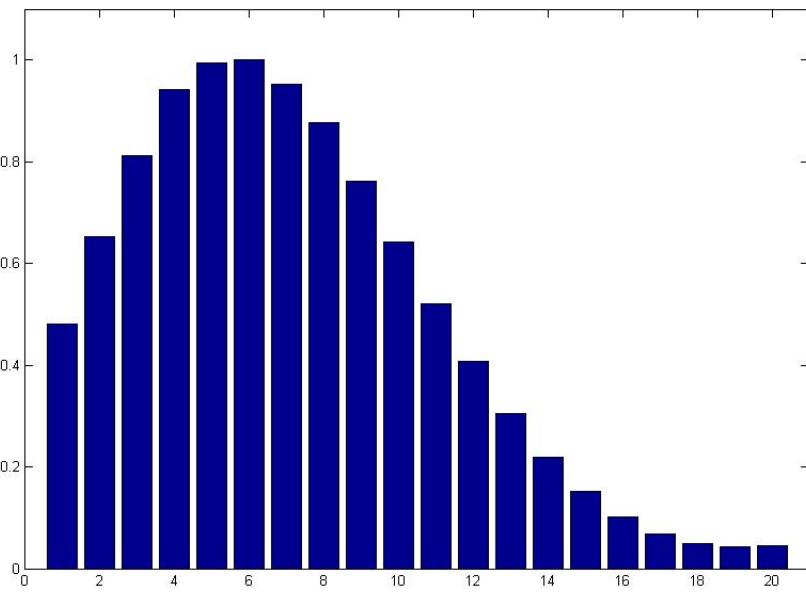
- **Reduction Criterion (Modal Selection)**

$$\prod^r = \frac{|F_r|^2}{2\omega_r C_r}$$

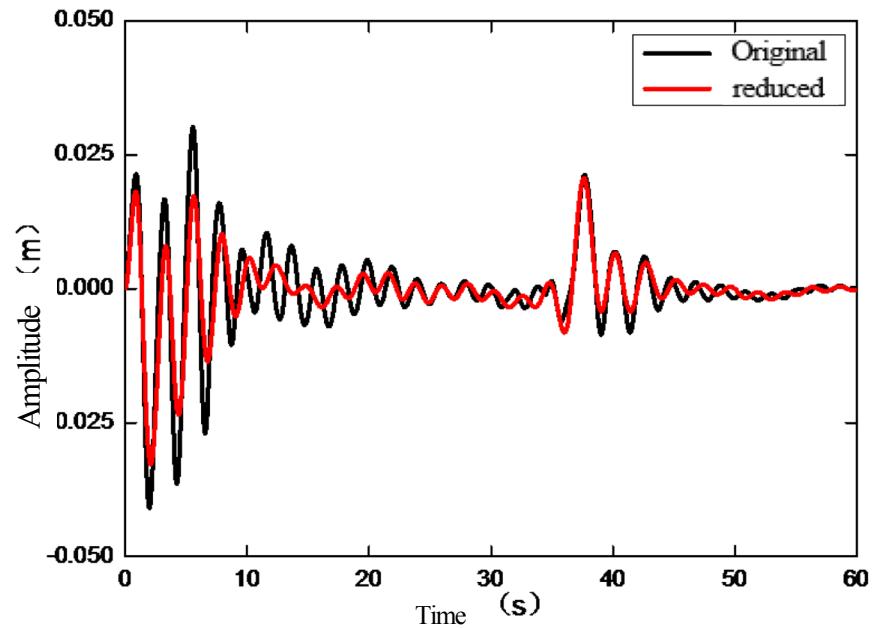
$$\beta_r = \frac{\prod^r}{\prod^{\max}}$$

# II. Modelling: Reduction

- **Reduction**



The relative motion energy of the first 20 mode for riser



The comparison between “reduced” and true model at 24m

# III. Optimal Strain Sensor Placement

- Criterion: based on  $H_2$  norm (modal sensitivity)
  - Function reformulation

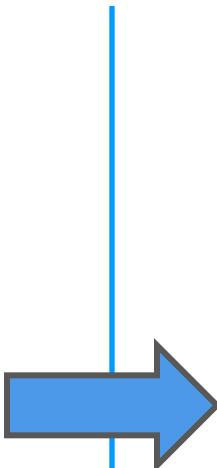
$$M_m \ddot{q}_m + D_m \dot{q}_m + K_m q_m = \phi^T B_o u$$

$$y = C_o \phi q_m + C_o \phi \dot{q}_m$$

$$M_m = \phi^T M \phi = I$$

$$D_m = \phi^T D \phi = diag[2\zeta_1\omega_1, 2\zeta_2\omega_2, \dots, 2\zeta_n\omega_n]$$

$$K_m = \phi^T K \phi = diag[\omega_1^2, \omega_2^2, \dots, \omega_n^2]$$



$$\dot{x} = A_m x + B_m u$$

$$y = C_m x$$

$$x_i = \begin{bmatrix} q_{mi} \\ \dot{q}_{mi} \end{bmatrix}$$

# III. Optimal Strain Sensor Placement

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- Criterion: based on  $H_2$  norm (modal sensitivity)

- Transfer Function (Laplace)

$$G(\omega) = \sum_{i=1}^k G_{mi}(\omega) = \sum_{i=1}^k \frac{(C_{moi} + j\omega C'_{moi})b_{mi}}{\omega_i^2 - \omega^2 + 2j\zeta_i\omega_i\omega}$$

$$G(\omega_i) \cong G_{mi}(\omega_i) = \frac{(-jC_{moi} + \omega_i C'_{moi})b_{mi}}{2\zeta_i\omega_i^2}$$

- $H_2$  norm

$$\|G\|_2^2 = \frac{1}{2\pi} \int_{-\infty}^{\infty} \text{tr}(G^*(\omega)G(\omega))d\omega$$

- For the  $i^{th}$  modal

$$\|G_i\|_2^2 = \sum_{j=1}^r \|G_{ij}\|_2^2$$

$$\|G_{ij}\|_2 = \frac{\|B_{mi}\|_2 \|C_{mji}\|_2}{2\sqrt{\zeta_i\omega_i}}$$

# III. Optimal Strain Sensor Placement

- Criterion: based on  $H_2$  norm (modal sensitivity)

- Optimal Selection Matrix

$$\begin{bmatrix} \sigma_{211} & \sigma_{212} & \cdots & \sigma_{21j} & \cdots & \sigma_{21r} \\ \sigma_{221} & \sigma_{222} & \cdots & \sigma_{22j} & \cdots & \sigma_{22r} \\ \cdots & \cdots & \cdots & \cdots & \cdots & \cdots \\ \sigma_{2i1} & \sigma_{2i2} & \cdots & \sigma_{2ij} & \cdots & \sigma_{2ir} \\ \cdots & \cdots & \cdots & \cdots & \cdots & \cdots \\ \sigma_{2k1} & \sigma_{2k2} & \cdots & \sigma_{2kj} & \cdots & \sigma_{2kr} \end{bmatrix}$$

*i<sup>th</sup> modal*      *j<sup>th</sup> sensor*

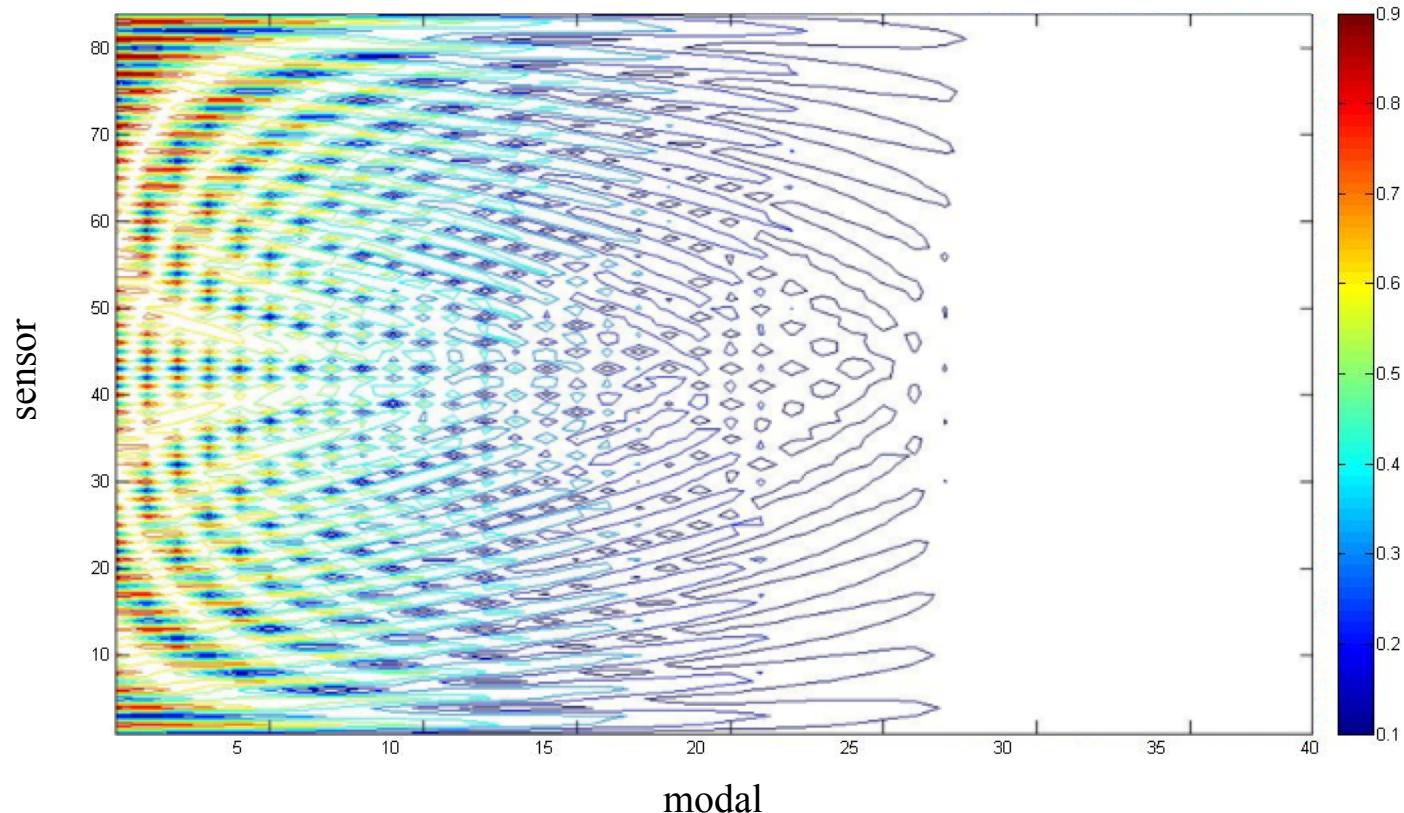
$$\sigma_{2ij} = \frac{\| G_{ij} \|_2}{\| G \|_2}$$

$$\| G \|_2 = \sum_{i=1}^k \| G_i \|_2^2 = \sum_{i=1}^k \sum_{j=1}^r \| G_{ij} \|_2^2$$

# III. Optimal Strain Sensor Placement

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- Criterion: based on  $H_2$  norm
  - Optimal Selection Matrix



# III. Optimal Strain Sensor Placement

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- Criterion: based on  $H_2$  norm
  - Reduction based on sensor sensitive similarity

$$g_i = \begin{bmatrix} \|G_{1i}\|_2^2 \\ \|G_{2i}\|_2^2 \\ \vdots \\ \|G_{ki}\|_2^2 \end{bmatrix}$$

$$r_{ij} = \frac{g_i^T g_j}{\|g_i\|_2 \|g_j\|_2}$$

# III. Optimal Strain Sensor Placement

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- **Procedure**
  - 1. Define the set of candidate locations, determine the number of sensors  $r$  based on the total number of excited modes  $k$  being considered ( $r \geq k$ ).
  - 2. Reduce the candidate set based on modal sensitivity  $\mathbf{H}_2$  (exhaustive search).
  - 3. Make further reduction based on sensor sensitive similarity.

# III. Optimal Strain Sensor Placement

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- Evaluation + Kalman Filter

$$x_k = Fx_{k-1} + Gu_{k-1} + \omega_{k-1}$$
$$y_k = Cx_k + v_k$$

$$\hat{x}_k^+ = \hat{x}_k^- + K_k(y_k - C\hat{x}_k^-)$$

$$K_k = P_k^- C^T (C P_k^- C^T + R_k)^{-1}$$

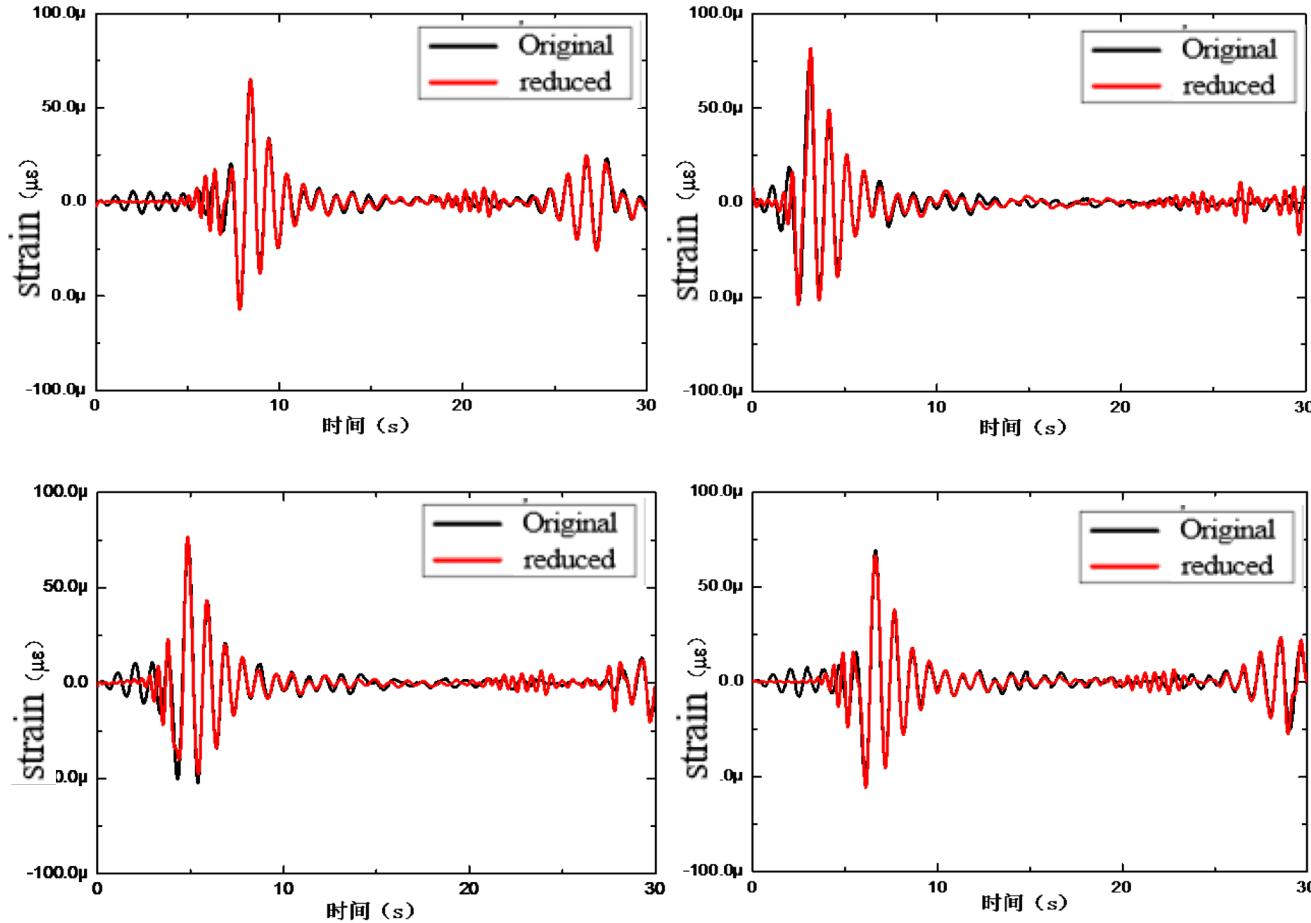
- Criterion

$$\beta = \frac{\sum_i^n \|(\bar{\varepsilon}_i - \varepsilon_i)\|}{\sum_i^n \|(\varepsilon_i)\|}$$

# III. Optimal Strain Sensor Placement

- Result

- 30 strain sensors: [4,7,8,11,12,14,15,16,19,22,23,27,28,29,30,57,60,61,62,63,68,69,70,71,73,74,75,76,79,80]



# III. Optimal Strain Sensor Placement

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- Result
  - Comparison

Comparison of accuracy between different sensor arrangement

	Optimal	Case 1	Case 2	Case 3
$\beta$	0.336	0.344	0.348	0.349

Comparison of accuracy between different number of optimal sensor arrangement

	30	32	34	36	38
$\beta$	0.336	0.332	0.334	0.326	0.326

# IV. Discussion

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- Sensor optimal placement + Kalman Filter
- References
  1. Li, X., Ren, P., Zhou, Z. and Ou, J. An optimized FBG-based fatigue monitoring strategy on deepwater risers. In *Optical Metrology and Inspection for Industrial Applications III*.
  2. Bai, S., Li, X., Xie, Z., Zhou, Z. and Ou, J., 2014. A wireless fatigue monitoring system utilizing a bio-inspired tree ring data tracking technique. *Sensors*.