



# The effects of sulfur, silicon, water, and oxygen fugacity on carbon solubility and partitioning in Fe-rich alloy and silicate melt systems at 3 GPa and 1600 °C: Implications for core–mantle differentiation and degassing of magma oceans and reduced planetary mantles



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## ABSTRACT

The partition coefficient of carbon between Fe-rich alloy melt and silicate melt,  $D_C^{metal/silicate}$  and solubility of C–O–H volatiles in reduced silicate melts are key parameters that need to be quantified in order to constrain the budget and origin of carbon in different planetary reservoirs and subsequent evolution of volatiles in magma oceans (MO) and silicate mantles. In this study, three sets of graphite-saturated experiments have been performed at 3 GPa and 1600 °C to investigate the effects of oxygen fugacity ( $fO_2$ ), sulfur, silicon, and water on the dissolution and partitioning of carbon between Fe-rich alloy melt and silicate melt. The results show that the presence of 0–5 wt% sulfur in alloy melt does not have considerable effect on carbon solubility (~5.6 wt%) in alloy melt, determined by electron microprobe, whereas the presence of 0–10 wt% silicon decreases the carbon solubility from ~5.6 wt% to 1.8 wt%. Carbon solubility (11–192 ppm) in silicate melt, determined by SIMS, is strongly controlled by  $fO_2$  and the bulk water content. Decreasing  $\log fO_2$  from IW-0.6 to IW-4.7 or increasing bulk water content from 0.07 to 0.55 wt% results in significant increase of carbon solubility in silicate melt. Raman and FTIR spectroscopic analyses of silicate glasses show that the carbon species is mostly methane, which is further confirmed by the strong, positive correlation between the non-carbonate carbon and non-hydroxyl hydrogen in silicate melt. The  $D_C^{metal/silicate}$  ranging from 180 to 4600 decreases with decreasing  $fO_2$  or increasing bulk water in silicate melt. In addition, increasing Si in alloy melt also decreases  $D_C^{metal/silicate}$ . Our results demonstrate that  $fO_2$  and bulk water contents in silicate melt play an important role in determining the fractionation of carbon in planetary MO. A reduced, hydrous MO may have led to a considerable fraction of carbon retained in the silicate mantle, whereas an oxidized, dry MO may have lost almost its entire carbon into the core. If delivery of bulk Earth carbon predominantly occurred after >90% of accretion, i.e., in a relatively oxidized MO (IW-2 to IW-1), then with applicable  $D_C^{metal/silicate} > 1000$ , most early Earth carbon would also enter the segregating core. Finally, the predominance of methane in reduced silicate melt with  $fO_2$  below IW-1 also indicates that degassing of a hydrous, solidifying MO may have created a reduced early atmosphere, and degassing from lunar and Martian mantle may have released much more methane than carbon dioxide.

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## 1. Introduction

Carbon, the fourth most abundant element in the Universe, has a significant effect on the planetary atmosphere composition, surface habitability, internal chemical differentiation, physical prop-

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erties and dynamics (e.g., Eggler, 1976; Falloon and Green, 1989; Sleep and Zahnle, 2001; Zahnle et al., 2010; Stanley et al., 2011; Hirschmann, 2012; Dasgupta and Hirschmann, 2010; Dasgupta, 2013; Dasgupta et al., 2013a, 2013b; Sifré et al., 2014). Partition coefficient of carbon between alloy melt and silicate melt,  $D_C^{metal/silicate}$  at conditions similar to a magma ocean (MO) is a key quantity that needs to be determined in order to constrain the origin and initial distribution of carbon between planetary silicate fraction and metallic core (Dasgupta, 2013; Chi et al., 2014). However, so far there are only a few studies that

exclusively constrained the  $D_C^{\text{metal/silicate}}$  relevant for MO (Dasgupta and Walker, 2008; Zhang and Yin, 2012; Dasgupta et al., 2013a; Chi et al., 2014). Only Dasgupta et al. (2013a), Stanley et al. (2014), and Chi et al. (2014) experimentally measured  $D_C^{\text{metal/silicate}}$  (100–5000) as a function of temperature (1350–2100 °C), pressure (1–5 GPa), oxygen fugacity ( $\sim$ 1W–0.4 to 1W–1), silicate melt composition (NBO/T = 0.8–3.6), and alloy melt composition (Fe/Ni ratio). However, all of these studies constructed alloy melt compositions that either had carbon as the only light element (Dasgupta et al., 2013a; Stanley et al., 2014; Chi et al., 2014) or had only a minor presence of sulfur (Dasgupta et al., 2013a). Further, these experiments did not extend to very reducing conditions ( $<1\text{W}-1.5$ ) that may be relevant for early accretion of terrestrial planets such as Earth (e.g., Wood et al., 2006).

Based on cosmochemical and geophysical consideration, and based on high-pressure experimental evidence,  $\sim$ 5–12% light elements mainly including carbon, oxygen, sulfur, and silicon have been proposed in the Earth's outer core to account for the core density deficit (e.g., Allegre et al., 1995; McDonough, 2003; Dasgupta and Walker, 2008; Bouhifd and Jephcoat, 2011; Wood et al., 2013). For instance, recent experimental studies suggested that 1–12 wt% sulfur and/or silicon could be in the Earth's core (Ricolleau et al., 2011; Morard et al., 2013; Siebert et al., 2013). The presence of sulfur, silicon, and carbon in alloy melt may significantly affect the partitioning of siderophile elements such as W, Mo, Ni, and Pb at  $P$ – $T$ – $f\text{O}_2$  conditions of MO (Tuff et al., 2011; Bouhifd et al., 2013; Rai and van Westrenen, 2014). However, whether the presence of sulfur and/or silicon in alloy melt affect the partitioning of carbon remains unknown. Moreover, the effects of dissolved water in silicate melt and low  $f\text{O}_2$  values ( $<1\text{W}-2$ ) on  $D_C^{\text{metal/silicate}}$  have never been investigated systematically. For example, the activity coefficient of carbon in alloy melt could be affected considerably with other interacting light elements in solution owing to strong non-ideal interactions of various light elements such as sulfur and carbon (Corgne et al., 2008; Dasgupta et al., 2009; Tsuno and Dasgupta, 2015) and silicon and carbon (Miettinen, 1998; Kawanishi et al., 2009). Hence one may expect that  $D_C^{\text{metal/silicate}}$  will be considerably lower with higher S/C and/or Si/C ratios of alloy melt than what has been simulated so far in existing experiments.

Understanding the dissolution mechanism of carbon in silicate melt is also of great importance in understanding carbon solubility in silicate melt and thus magma's storage and transport capacities of carbon (Holloway et al., 1992; Kadik et al., 2004; Mysen et al., 2011; Stanley et al., 2011, 2014; Ardia et al., 2013; Dasgupta et al., 2013a; Chi et al., 2014). The species of C–H–O volatiles in reduced silicate melt, which are mainly a multi-function of fugacities of  $\text{H}_2\text{O}$ ,  $\text{H}_2$ , and  $\text{O}_2$ , remain unclear, resulting in the carbon species degassed from reduced, solid planetary mantles such as those in Mars and the Moon remaining unclear and debated (Dasgupta, 2013; Wetzel et al., 2013; Stanley et al., 2014).

We therefore performed experiments investigating systematically (1) the effects of sulfur and/or silicon in Fe-rich alloy melt on C-solubility, (2) water in silicate melt, and  $\log f\text{O}_2$  ranging from  $\sim$ 1W–1 to 1W–5 on C-solubility in silicate melt, and (3) carbon partitioning between alloy melt and silicate melt. All experiments were conducted at a constant pressure (3 GPa) and temperature (1600 °C) and at graphite-saturation. We also performed Raman and FTIR analyses in our silicate glasses to provide important constraints on the variation of the C–H–O species as a function of melt water content and  $\log f\text{O}_2$  down to  $\sim$ 1W–5.

**Table 1**

Chemical compositions of starting materials (in wt%).

Knippa	SiO <sub>2</sub>	TiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Cr <sub>2</sub> O <sub>3</sub>	FeO	MnO
	42.49	3.27	11.76	0.07	11.00	0.22
	MgO	CaO	Na <sub>2</sub> O	K <sub>2</sub> O	P <sub>2</sub> O <sub>5</sub>	Total
	12.33	11.59	3.05	2.03	0.83	99.66
Alloy mix	Fe	Ni	S	Si	Total	
Fe–Ni–S						
S1	89.4	5.6	5	–	100	
S2	91.4	5.6	3	–	100	
S3	87.4	5.6	7	–	100	
S4	84.4	5.6	10	–	100	
Fe–Ni–Si						
Si1	91.4	5.6	–	3	100	
Si2	89.4	5.6	–	5	100	
Si3	87.4	5.6	–	7	100	
Si4	84.4	5.6	–	10	100	
Si5	76.4	5.6	–	18	100	
Si6	79.4	5.6	–	15	100	
Fe–Ni–S–Si						
SSi1	80.9	5.6	3.5	10	100	
SSi2	77.9	5.6	3.5	13	100	
SSi3	74.9	5.6	3.5	16	100	

Knippa: a natural basanite that has been used in many high-pressure partitioning experiments (e.g., Righter et al., 2011; Chi et al., 2014). The major element composition of Knippa basanite was listed in Lewis et al. (1993).

## 2. Methods

### 2.1. Starting materials

Starting materials included  $\sim$ 60–70 wt% silicate powder of a natural basanite (Knippa) and 30–40 wt% metal powder of Fe–Ni–S, Fe–Ni–Si, or Fe–Ni–S–Si mixture. The natural basanite (Table 1) was dehydrated at 1000 °C and  $\log f\text{O}_2$  of  $\sim$ FMQ–2 using a CO–CO<sub>2</sub> Deltech gas mixing furnace for 24 h in order to obtain a relatively low water content. In order to study the effects of silicon and sulfur in alloy melt on carbon partitioning thirteen homogeneous metal mixtures (Table 1) were prepared from analytical grade Fe, Ni, Si, and FeS powders. All the homogeneous mixtures of metal and silicate were stored in a desiccator at 100 °C for  $\geq$ 24 h to remove completely the absorbed ethanol used for homogenization before loading into graphite capsules and subjecting to high  $P$ – $T$  conditions.

### 2.2. High pressure–temperature experiments

Three sets of experiments were conducted to investigate factors that may potentially control carbon solubility and partitioning between alloy melt and silicate melt (Table 2): the first set in the Knippa–Fe–Ni–S system to investigate the effect of sulfur in alloy melt; the second set in the Knippa–Fe–Ni–Si system to investigate the effect of silicon in alloy melt; and the third set in the Knippa–Fe–Ni–S–Si system to investigate the effect of coexistence of sulfur and silicon in alloy melt. These three sets of experiments also allowed us to investigate the effects of  $f\text{O}_2$  and water in silicate melt on solubility of C–O–H volatiles and carbon partitioning (see below).

All the experiments were conducted using an end-loaded piston cylinder device at 3 GPa and 1600 °C at the experimental petrology laboratory of Rice University, following assembly and calibration as given in Tsuno and Dasgupta (2011). Graphite capsule was used in order to study carbon solubility in silicate melt and alloy melt. The use of graphite capsule also allowed achieving temperatures that approach that of planetary magma oceans. Experiments were pressurized first at room temperature and then heated at the rate of 100 °C/min. In order to reduce porosity in the graphite capsules

**Table 2**

Summary of experimental conditions, quench products, estimates of volatile species abundance, and carbon partitioning.

Run no.	P (GPa)	T (°C)	Duration (h)	$f_{O_2}$ ( $\Delta IW^a$ )	$f_{O_2}$ ( $\Delta IW^b$ )	Starting material	Quench phases	Raman	FTIR C <sup>c</sup> (ppm) in SM	FTIR H <sub>2</sub> O <sup>d</sup> (wt%) in SM	FTIR H <sub>2</sub> O <sup>d</sup> (wt%) in SM	SIMS H <sub>2</sub> O (wt%) in SM	NBO/T <sup>e</sup> in SM	H <sub>2</sub> <sup>f</sup> (wt%) in SM	H <sub>2</sub> <sup>f</sup> (wt%) in SM	SIMS C (ppm) in SM	C in AM (wt%)	$D^{metal/silicate}$
<b>Knippa-Fe-Ni-S</b>																		
G315-01	3	1600	2.0	−1.4	−0.64	Knippa + S1	AM + SM	✓	X	X	X	0.22(0)	1.46			46(0)	5.88(39)	1291(86)
G316-02	3	1600	2.0	−1.5	−0.72	Knippa + S2	AM + SM	✓	10(2)	0.23(1)	0.16(1)	0.34(1)	1.48	0.0122	0.02	55(1)	5.61(10)	1016(29)
G317-03	3	1600	2.5	−1.4	−0.59	Knippa + S3	AM + SM + SulfM	✓	9(1)	0.31(0)	0.21(2)	0.47(3)	1.51	0.0178	0.0289	59(2)	5.81(25)	981(57)
G318-04	3	1600	2.0	−1.4	−0.70	Knippa + S4	AM + SM + SulfM	✓	10(1)	0.34(1)	0.24(1)	0.55(1)	1.54	0.023	0.0341	65(1)	5.31(8)	820(17)
<b>Knippa-Fe-Ni-Si</b>																		
G319-05	3	1600	2.0	−2.0	−1.3	Knippa + Si1	AM + SM	✓	n.d	0.19(0)	0.13(0)	0.25(1)	1.22	0.0063	0.0129	22(2)	5.53(15)	2480(216)
G320-06	3	1600	2.3	−2.2	−1.5	Knippa + Si2	AM + SM	✓	n.d	0.21(1)	0.15(1)	0.25(0)	1.14	0.0048	0.0115	18(0)	5.58(15)	3042(94)
G321-07	3	1600	2.0	−2.9	−2.2	Knippa + Si3	AM + SM + Cpx	✓	n.d	0.17(0)	0.12(0)	0.19(0)	0.97	0.0017	0.0073	12(1)	5.66(12)	4612(306)
G322-08	3	1600	2.0	−4.8	−4.2	Knippa + Si4	AM + SM + Cpx	✓	n.d	X	X	0.68(0)	0.88			74(0)	5.07(17)	685(24)
G326-12	3	1600	2.0	−5.4	−4.7	Knippa + Si5	AM + SM	✓	n.d	0.04(0)	0.03(0)	0.12(1)	0.81	0.0093	0.0104	24(2)	1.82(75)	753(315)
G329-15	3	1600	2.0	−5.1	−4.3	Knippa + Si6	AM + SM	✓	n.d	0.03(0)	0.02(0)	0.07(0)	0.88	0.0039	0.0051	11(2)	4.54(19)	4214(646)
<b>Knippa-Fe-Ni-S-Si</b>																		
G330-16	3	1600	2.0	−5.0	−4.2	Knippa + SSi1	AM + SM	✓	n.d	0.15(0)	0.1(0)	0.43(9)	0.89	0.0309	0.0365	96(4)	5.20(9)	540(22)
G331-17	3	1600	2.0	−5.2	−4.4	Knippa + SSi2	AM + SM	✓	n.d	0.09(0)	0.07(0)	0.41(1)	0.88	0.036	0.0383	158(2)	5.02(11)	317(8)
G337-19	3	1600	3.0	−5.3	−4.6	Knippa + SSi3	AM + SM	✓	n.d	0.05(0)	0.03(0)	0.35(1)	0.88	0.0338	0.036	192(1)	3.38(20)	176(11)

The  $f_{O_2}$  prevailing during the experiments was calculated using the equilibrium:  $FeO$  (silicate melt) =  $Fe$  (alloy melt) +  $1/2O_2$ , from which the  $f_{O_2}$  of the experiment relative to  $f_{O_2}$  of the iron-wüstite buffer (IW), at any given  $P$  and  $T$  can be defined as:  $\Delta IW = 2 \log(X_{FeO} \gamma_{FeO} / X_{Fe} \gamma_{Fe})$ ;  $X_{FeO}$  and  $X_{Fe}$  are the mole fractions of  $FeO$  in silicate melt and  $Fe$  in alloy melt, respectively;  $\gamma_{FeO}$  and  $\gamma_{Fe}$  are the activity coefficients of  $FeO$  in silicate melt and  $Fe$  in alloy melt, respectively. Calculation of  $f_{O_2}$  using ideal solution model (ideal  $f_{O_2}$ ) was performed assuming  $\gamma_{FeO} = \gamma_{Fe} = 1$ ; calculation of  $f_{O_2}$  using non-ideal solution model (non-ideal  $f_{O_2}$ ) performed assuming  $\gamma_{FeO} \sim 1.5$  (Holzheid et al., 1997; O'Neill and Eggins, 2002). Activity coefficients of  $Fe$  in Fe-rich melt,  $\gamma_{Fe}$ , were calculated using the  $\epsilon$ -approach, which takes into account the non-ideal interaction between all the components in the Fe-rich alloy melt (Ma, 2001; Chi et al., 2014; Wood et al., 2013). The online "Metal Activity Calculator" (<http://www.earth.ox.ac.uk/~expet/metalact/>) provided by the University of Oxford (Wood et al., 2013) was used to calculate the  $Fe$ -activity in alloy melt. The calculated ideal  $f_{O_2}$  values are in general  $\sim 0.7$  log units lower than the non-ideal  $f_{O_2}$  values. The non-ideal  $f_{O_2}$  for the Knippa-Fe-Ni-S runs were around IW-0.7. The non-ideal  $f_{O_2}$  of the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si runs ranged from IW-1.3 to IW-4.7, decreasing with decreasing  $FeO$  content in silicate melt or increasing  $Si$  content in alloy melt. The  $f_{O_2}$  mentioned in the text refers to non-ideal  $f_{O_2}$ . n.d.: no carbonate was detected by FTIR. ✓: measured; X: not measured. SM – Silicate melt, AM – Alloy melt, Cpx – Clinopyroxene, SulfM – Sulfide melt,  $D^{metal/silicate}$  – C in AM/C in SM. For each sample, 3–6 spots were analyzed by SIMS and 2–5 spots were analyzed by FTIR. Numbers in parentheses are  $1\sigma$  standard deviation based on replicate analyses; 59(2) should be read as  $59 \pm 2$  and 5.88 (39) should be read as  $5.88 \pm 0.39$ .

<sup>a</sup> Ideal  $f_{O_2}$ .

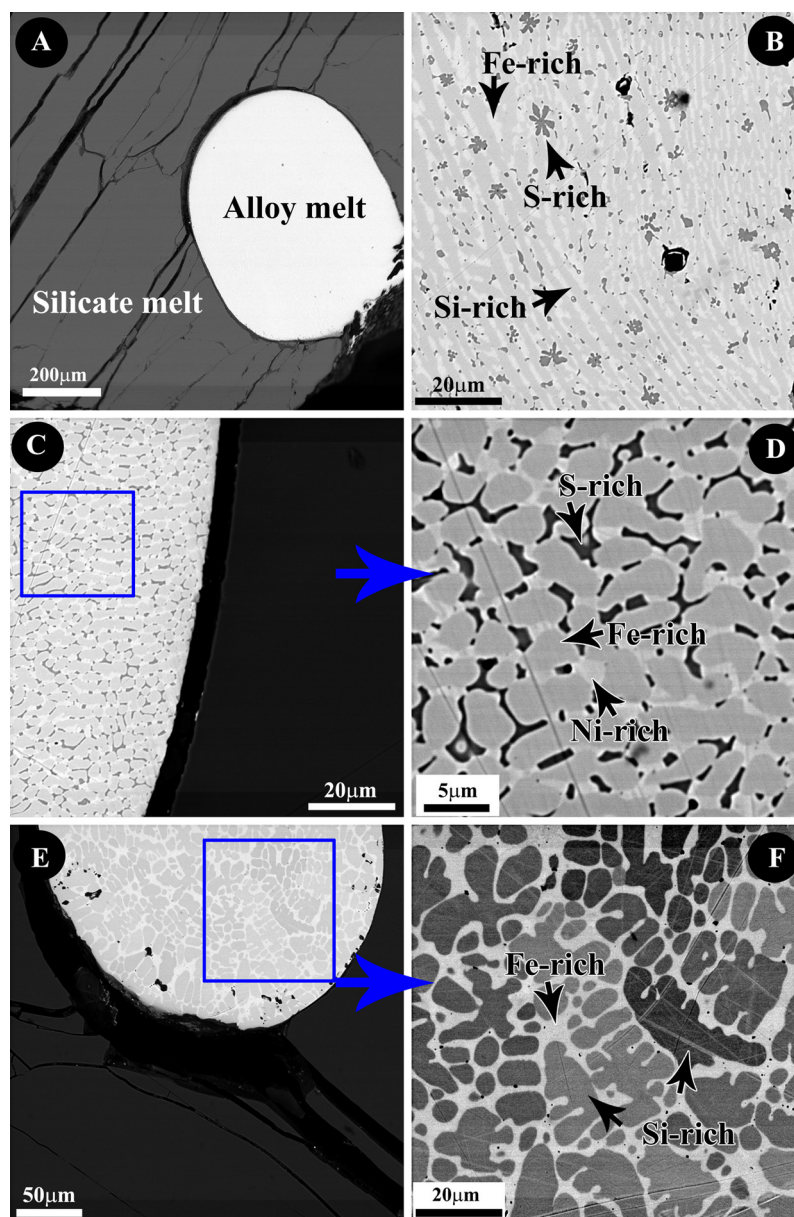
<sup>b</sup> Non-ideal  $f_{O_2}$ .

<sup>c</sup> Carbon as carbonate.

<sup>d</sup> The water content was measured by FTIR using the Beer–Lambert law at extinction coefficient = 60 and 90  $L mol^{-1} cm^{-1}$  for water at  $\sim 3550 cm^{-1}$ , respectively.

<sup>e</sup>  $NBO/T = 2 \text{ total O/T} - 4$  ( $T = Si + Ti + Al + Cr + P$ ).

<sup>f</sup> Non-hydroxyl hydrogen calculated based on difference between bulk water measured by SIMS and water measured by FTIR using the Beer–Lambert law at extinction coefficient = 60 and 90  $L mol^{-1} cm^{-1}$  for water at  $\sim 3550 cm^{-1}$ , respectively. See text for details.



**Fig. 1.** Selected back-scattered electron images of run products. (A) Coexistence of quenched silicate melt and alloy melt from run G321-07 in the Knippa–Fe–Ni–Si system. (B) Detailed texture of quenched alloy melt from run G330-16 in the Knippa–Fe–Ni–S–Si system. (C) Coexistence of quenched silicate melt and alloy melt from run G316-02 in the Knippa–Fe–Ni–S system. (D) Detailed texture of quenched alloy melt in (C). (E) Coexistence of quenched silicate melt and alloy melt from run G326-12 in the Knippa–Fe–Ni–Si system. (F) Detailed texture of quenched alloy melt in (E).

and prevent leakage of alloy melt, experiments were held at 850 °C for 1–3 h, and then raised to the desired, nominal temperature of the experiment. During the run, temperature was monitored and controlled using a type-C thermocouple. All experiments were brought down  $\leq 100$  °C within 10–20 s by switching off the electric power to the heater.

### 2.3. Analytical procedure

The recovered capsules were sectioned longitudinally into two halves using a wire saw. Both halves were mounted in Crystal Bond® and polished with 0.3 μm aluminum slurry on a lapidary wheel. Each of the samples after polishing was immersed into ~100 ml acetone for at least 24 h to remove completely the Crystal Bond. Cameca SX50 and Cameca SX100 electron microprobes were used for determining the major and minor element compositions of silicate melt and the alloy melt, respectively as

well carbon content of alloy melt. A Cameca IMS 1280 ion microprobe was used for determining the bulk carbon and water contents in silicate glasses, and Raman and Fourier transformed infrared (FTIR) spectroscopies were used for determining and quantifying the possible C–H–O species in the silicate glasses following methodologies detailed in recent studies (e.g., Chi et al., 2014; Duncan and Dasgupta, 2014). A complete description of the analytical conditions and instrumental calibration for each of the technique employed is provided in Supplementary Text and Supplementary Figs. 1 and 2.

## 3. Results

### 3.1. Texture of the experimental products

All the experiments produced quenched blobs of alloy melt embedded in silicate glasses (Fig. 1). The alloy melt was exsolved into



a few phases during quenching (Fig. 1), but only runs G317-03 and G318-04, which contained about 7 wt% and 10 wt% sulfur in the starting metal mixture, respectively, had two immiscible alloy melt phases during the run (sulfide liquid and S-poor alloy melt). Runs G321-07 and G322-08 also contained a small fraction of residual clinopyroxene at the bottom of the sample capsules.

### 3.2. Major element composition and estimation of oxygen fugacity

The major element compositions of silicate melt and alloy melt are tabulated in Supplementary Tables 1 and 2, respectively. Compared to the composition of starting silicate, the silicate melt compositions from the Knippa-Fe-Ni-S runs were moderately FeO-rich (15.5–17 wt%), due to oxidation of a small fraction of Fe in the alloy. However, the silicate melts in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si runs became SiO<sub>2</sub>-rich (45–54 wt%) but depleted in FeO (0.1–9.2 wt%) due to the reduction of FeO in silicate melt by Si in alloy melt via the reaction of 2FeO (silicate) + Si (alloy) = SiO<sub>2</sub> (silicate) + 2Fe (alloy). The values of silicate melt NBO/T are in the range of 0.81 to 1.54 (see Table 2). The Ni content of alloy melt ranged from ~4.5 to 7.2 wt%, and the Fe content of alloy melt ranged from ~82 to 92 wt%. The sulfur content in alloy melt in the Knippa-Fe-Ni-S runs ranged from ~2.0 to 5.0 wt%, while Si content in alloy melt in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si runs ranged from <0.1 to ~10 wt%. The sulfur content in sulfide liquid in runs G317-03 and G318-04 was up to ~26 wt%, but the sulfide liquids were not considered further in this study.

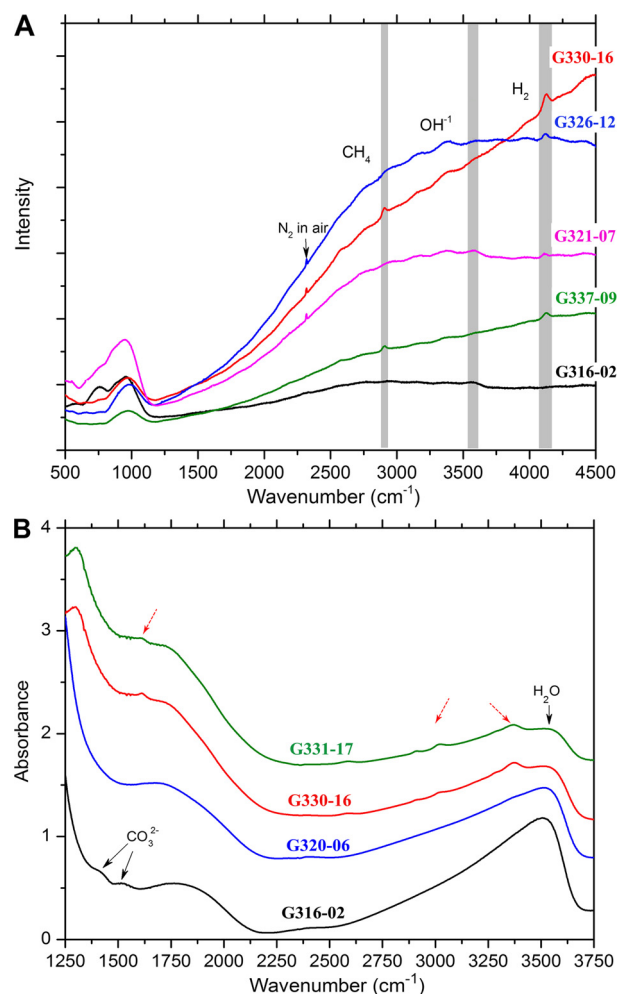
Following the method used in many previous studies (e.g., Bouhifd et al., 2013; Dasgupta et al., 2013a; Chi et al., 2014; Boujibar et al., 2014), the oxygen fugacity,  $f_{O_2}$  prevailing during the experiments was calculated from the equilibrium of Fe-rich alloy melt and FeO-bearing silicate melt. Our experiments covered  $\log f_{O_2}$  range of IW-0.6 to IW-4.7 (see footnote of Table 2).

### 3.3. Bulk water content and C–H–O species in silicate melt

The bulk H contents in silicate melt, expressed as H<sub>2</sub>O and measured by SIMS, ranged from ~0.07 to 0.68 wt% with most values between ~0.25 and 0.45 wt%. The bulk water content in this study was similar to lower, compared to previous, similar studies (Wetzel et al., 2013; Dasgupta et al., 2013a; Chi et al., 2014; Stanley et al., 2014). The variation of water content in our silicate melt allowed us to investigate its effect on carbon solubility in silicate melt and partitioning between alloy melt and silicate melt at a fixed temperature and pressure, and also  $f_{O_2}$  in the runs in the Knippa-Fe-Ni-S system (see below).

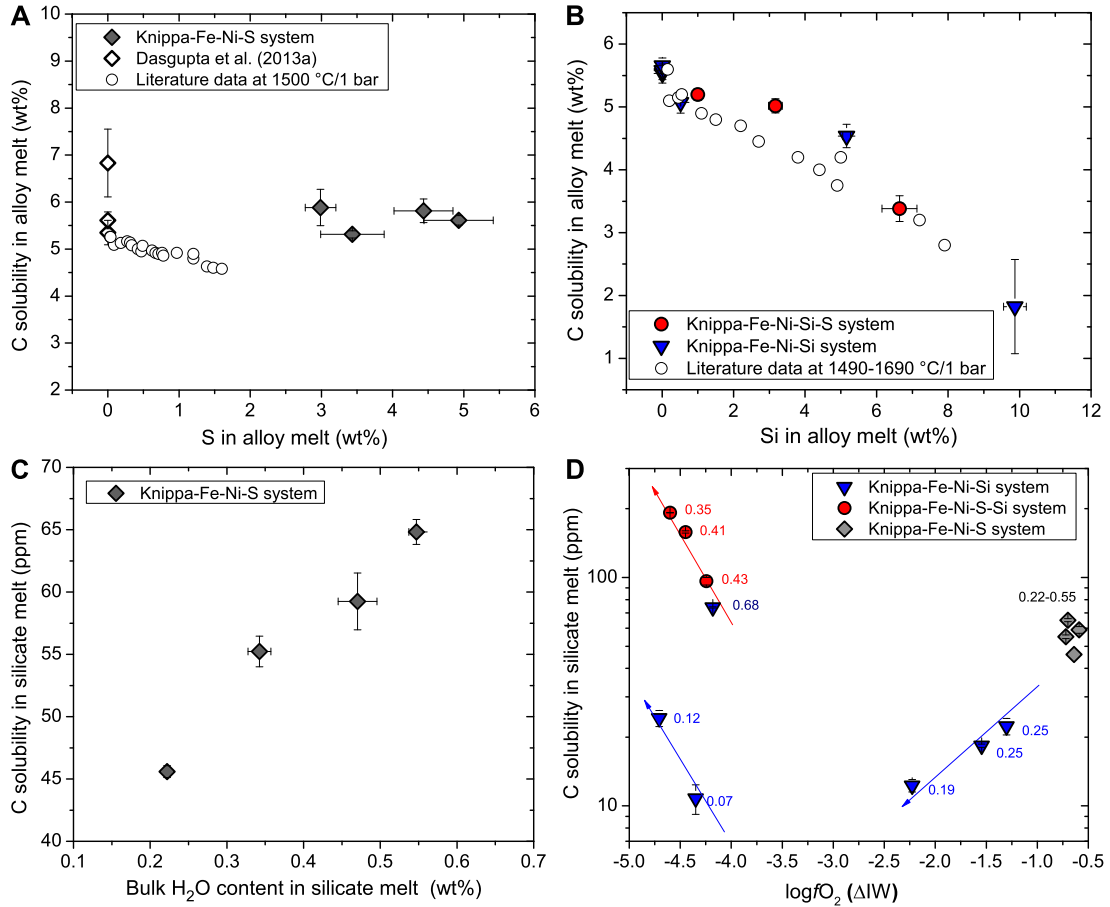
Raman spectra were collected from the silicate glasses of all the runs and typical spectra are shown in Fig. 2A. The recognition of C–H–O species from Raman spectra was affected by fluorescence in all the silicate glasses. However, it remains clear that peaks at ~4100 and 2900 cm<sup>-1</sup> from glasses synthesized at reduced conditions in the Knippa-Fe-Ni-S-Si and Knippa-Fe-Ni-S systems are owing to the presence of molecular hydrogen (H<sub>2</sub>) and methane (CH<sub>4</sub>), respectively. Whereas the asymmetrical broad band between 3350 and 3650 cm<sup>-1</sup> is associated with OH<sup>-</sup> ions and molecular water (Mysen et al., 2009; Dasgupta et al., 2013a; Chi et al., 2014). The iron-carbonyl peak as has been observed by Wetzel et al. (2013) was not observed in our Raman spectra, although our silicate melt (runs in the Knippa-Fe-Ni-S system) had FeO\* content up to 17 wt%. The absence of any features that can be associated with Fe-carbonyl or other Fe–C species suggests that FeO\* content of our experimental melts couldn't possibly have any causal relationship with C solubility.

FTIR spectra were obtained for all the glasses except for runs G315-01 and G322-08, and selected spectra are shown in



**Fig. 2.** Representative Raman (A) and FTIR (B) spectra of experimental silicate glasses from this study showing regions associated with C–H–O volatile species. See Table 2 for experimental conditions corresponding to these experiments. The peaks indicated by dashed arrows in panel (B) remain unspecified, but they might be due to the stretching vibration of N–H (Busigny et al., 2003; Stanley et al., 2014) or organic contamination on the sample surface (e.g., fingerprints). Because these peaks are observed in the most reduced samples ( $\log f_{O_2} < \text{IW}-4$ ), it is highly likely they are due to N–H stretching vibration, but contamination cannot be ruled out for the two peaks at ~3000 cm<sup>-1</sup>. The sample thicknesses for FTIR measurement are 300  $\mu\text{m}$  for G316-02, 340  $\mu\text{m}$  for G320-06, 370  $\mu\text{m}$  for G330-16, and 360  $\mu\text{m}$  for G331-17.

**Fig. 2B.** The samples synthesized at relatively oxidized conditions in the Knippa-Fe-Ni-S system showed carbonate doublets at 1420 and 1510 cm<sup>-1</sup>, which are absent for the samples synthesized at relatively reduced conditions in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si systems. All the spectra had a broad peak at ~3550 cm<sup>-1</sup>, indicating the presence of OH<sup>-</sup> in the glasses. The dissolved OH<sup>-</sup> content and carbonate content were quantified using the Beer–Lambert law. The extinction coefficient ( $\epsilon = 375 \text{ L mol}^{-1} \text{ cm}^{-1}$ ) used in Chi et al. (2014) for a similar melt composition was used for quantifying the carbonate content, and  $\epsilon$  of 60–90 L mol<sup>-1</sup> cm<sup>-1</sup> for water at ~3550 cm<sup>-1</sup> were used for quantifying the H<sub>2</sub>O content. The reason for choosing  $\epsilon$  of 60 and 90 L mol<sup>-1</sup> cm<sup>-1</sup> as two bounds is that these values cover the main range reported for extinction coefficient of water at ~3550 cm<sup>-1</sup> in basaltic to rhyolitic melts (e.g., Stolper, 1982). We note, however, that no correlation has been observed for reported  $\epsilon$  for OH<sup>-</sup> as a function of melt composition, which justifies our choice of using two fixed values of  $\epsilon$  for different experimental glass compositions generated in our study rather than using different  $\epsilon$  for different experiments. The results showed that OH<sup>-</sup> (expressed as H<sub>2</sub>O)



**Fig. 3.** Carbon solubility in alloy melt as a function of S content in alloy melt (A) and Si content in alloy melt (B), and carbon solubility in silicate melt as a function of water content in silicate melt (C) and oxygen fugacity (D). The labeled numbers are bulk water contents in silicate melt in wt%. The data of unfilled diamonds in panel (A) are from 3 GPa, 1600 °C experiments of Dasgupta et al. (2013a), and the literature data (unfilled circles) in panels (A) and (B) are from Bouchard and Bale (1995) and the references therein. Note that unlike 1 bar experiments, carbon solubility in the Fe-rich alloy melt at 3 GPa (this study) does not decrease with increasing sulfur content from 0 to ~5 wt%.

contents in the silicate glasses ranged from ~0.02 to 0.34 wt%, significantly lower than the bulk H<sub>2</sub>O contents determined by SIMS (Table 2), in particular at reduced conditions.

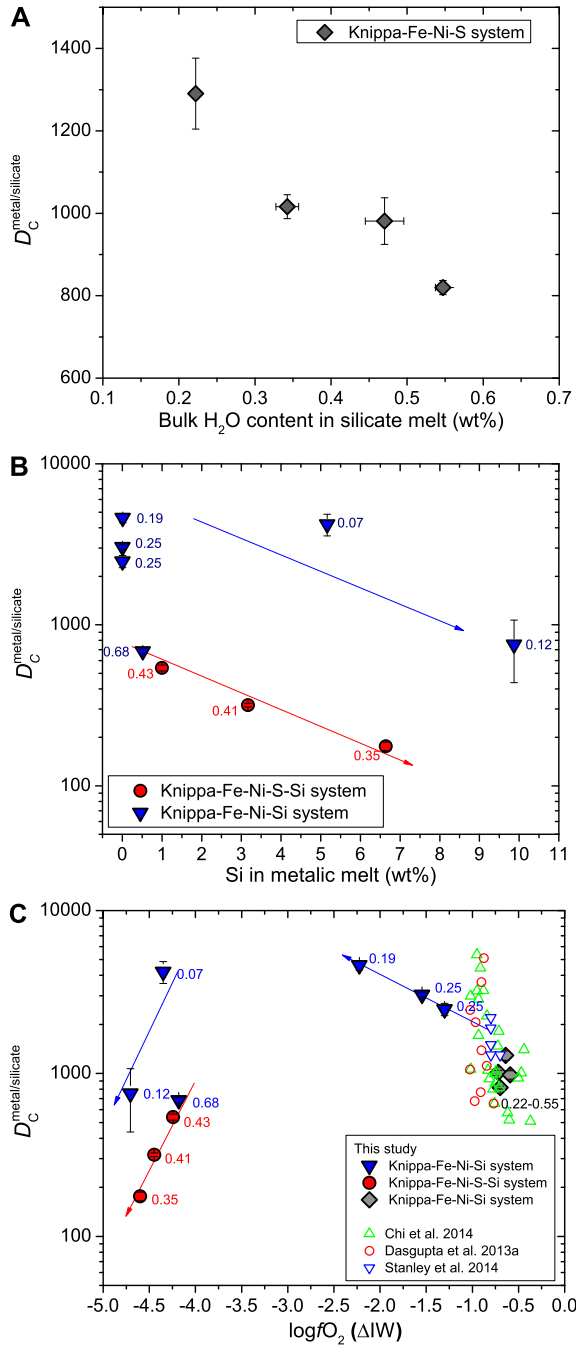
Assuming that the other water is mainly in the form of molecular hydrogen (H<sub>2</sub>), the calculated H<sub>2</sub> contents in silicate melt were between 0.0017 wt% and 0.0383 wt% (Table 2). We point out that H<sub>2</sub> content estimated this way provides an upper bound as clearly a small fraction of the hydrogen not present as OH<sup>−</sup> or H<sub>2</sub>O is present as CH<sub>4</sub> and other ions or molecules bonded to carbon and may be even nitrogen, and molecular H<sub>2</sub> mentioned hereafter refers to all non-hydroxyl hydrogen in silicate melt. The calculated carbon contents in the form of carbonate for the runs in the Knippa-Fe-Ni-S system were ~10 ppm, consistent with the result of 7 ppm of run B70 performed at similar conditions by Chi et al. (2014).

#### 3.4. Carbon contents in Fe-rich alloy melt and silicate melt at graphite-saturation

Carbon solubilities in alloy melt and silicate melt at graphite-saturation are tabulated in both Table 2 and Supplementary Table 2. The C-solubility in alloy melt in the Knippa-Fe-Ni-S system is ~5.6 wt% and appears not to be affected by the presence of sulfur in alloy melt (Fig. 3A). However, the C-solubility in alloy melt in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si systems decreases from ~5.6 wt% to ~1.8 wt% with Si content in alloy melt increasing from <0.1 to ~10 wt% (Fig. 3B).

C-solubility in silicate melt ranges from ~10 to ~190 ppm. It is ~45–65 ppm in the Knippa-Fe-Ni-S system, increasing with increasing water content (Fig. 3C). The C-solubility in silicate melt in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si systems depends not only on water content in silicate melt but also on  $f_{O_2}$  (Fig. 3D). For the runs with ~0.35–0.42 wt% H<sub>2</sub>O in the Knippa-Fe-Ni-S-Si system, the carbon content in silicate melt increases from ~96 to 192 ppm with  $f_{O_2}$  decreasing from IW-4.2 to IW-4.6. The C-solubility in silicate melt in the Knippa-Fe-Ni-Si system is generally lower (~10–25 ppm) and decreases with decreasing  $f_{O_2}$  from IW-1.4 to IW-2.2 and decreasing water content from ~0.25 to 0.19 wt%. However, C-solubility trend reverses and increases with decreasing  $f_{O_2}$  from ~IW-4.3 to IW-4.7 and increasing water content from ~0.07 to 0.12 wt%, as in the case of the C-solubility in silicate melt in the Knippa-Fe-Ni-S-Si system. One sample (run G322-08) with 0.68 wt% H<sub>2</sub>O and  $f_{O_2}$  of IW-4.2 in the Knippa-Fe-Ni-Si system contained ~74 ppm carbon, which appears to be consistent with the solubility values in the Knippa-Fe-Ni-S-Si system.

Using the model of Holloway et al. (1992), the calculated carbon contents in the form of carbonate were ~2 ppm for the runs in the Knippa-Fe-Ni-S system, whereas for the runs in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si systems, they were below 0.5 ppm, indicating negligible carbon as carbonate in reduced silicate melt. Meanwhile, regardless of  $f_{O_2}$  or bulk water content in the runs, a strong, positive correlation was observed between the non-carbonate carbon and molecular H<sub>2</sub> in silicate melt (Fig. 5A). These together with the Raman methane peak (Fig. 2A)

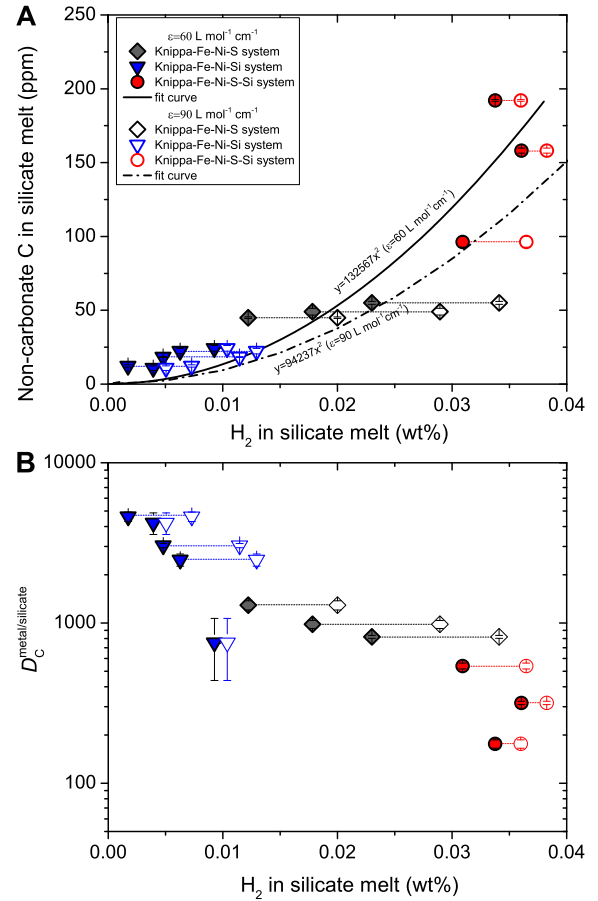


**Fig. 4.** Partition coefficient of carbon between metallic alloy melt and silicate melt ( $D_C^{metal/silicate}$ ) as a function of water content in silicate melt (A), Si content in metallic alloy melt (B), and oxygen fugacity (C). The labeled numbers are bulk water content in silicate melt in wt%. Also plotted for comparison in (C) are previously determined experimental  $D_C^{metal/silicate}$  values from Dasgupta et al. (2013a), Chi et al. (2014), and Stanley et al. (2014) generated over 1–5 GPa, 1350–2000 °C, and bulk silicate melt water content of 0.19–2.06 wt%.

imply that carbon species in silicate melt of the present study is mostly as methane.

### 3.5. Partition coefficient of carbon between alloy melt and silicate melt

$D_C^{metal/silicate}$  was calculated based on the measured carbon contents in alloy melt and silicate melt. The  $D_C^{metal/silicate}$  values in this study varied from 180 to 4600 (Table 2; Fig. 4). The  $D_C^{metal/silicate}$  values in the Knippa-Fe-Ni-S system decrease from



**Fig. 5.** The correlations between molecular  $H_2$  in silicate melt and non-carbonate carbon in silicate melt (A), and  $D_C^{metal/silicate}$  (B) from our 3 GPa, 1600 °C experiments. The strong positive correlation in panel (A) indicates that the carbon species in silicate melt is mostly as hydrogenated carbon (methane). The negative correlation in panel (B) indicates the strong controlling effect of molecular hydrogen in silicate melt or  $fH_2$  on carbon partitioning between alloy melt and silicate melt. The data in panel (A) are fitted as  $y = 132567x^2$  (solid curve) and  $y = 94237x^2$  (dashed curve) where  $x$  and  $y$  refer to  $H_2$  (wt%) and non-carbonate carbon (ppm), respectively, which combined with Eq. (8) can be used to calculate methane content in silicate melt as a function of oxygen fugacity and melt bulk water content (see text). Note that molecular  $H_2$  here refers to all the non-hydroxyl hydrogen in silicate melt and equals the bulk hydrogen determined by SIMS minus the hydroxyl hydrogen determined by FTIR using the Beer–Lambert law (at  $\epsilon_{OH^-} = 60$  and  $90 \text{ L mol}^{-1} \text{ cm}^{-1}$  for closed and open symbols, respectively). Non-carbonate carbon and bulk carbon measured using SIMS are the same for all experiments with  $\log fO_2 < IW-1.3$ . In both panels, the estimates of molecular  $H_2$  in silicate glass from the same experiment are connected by thin dashed line where the two estimates derive from different estimates of the concentration of dissolved  $H_2O$  using different extinction coefficients. The form of the fit chosen in (A) is guided by the assumption that essentially all non-carbonate carbon dissolved in our glasses are in the form of  $CH_4$  and solubility of  $CH_4$  must be proportional to the square of hydrogen fugacity,  $fH_2$  and  $H_2$  solubility in melt is directly proportional to  $fH_2$ .

1300 to 800 with increasing  $H_2O$  content in silicate melt (Fig. 4A). The  $D_C^{metal/silicate}$  values in the Knippa-Fe-Ni-Si and Knippa-Fe-Ni-S-Si systems decrease from 4600 to 180 with increasing Si content in alloy melt (Fig. 4B). Decreasing  $fO_2$  appears to first increase the  $D_C^{metal/silicate}$  value and then decrease the  $D_C^{metal/silicate}$  value (Fig. 4C). It should be noted that  $fO_2$  is negatively correlated with the Si content in alloy melt, therefore the effect of Si in alloy melt and the effect of  $fO_2$  on carbon partitioning are coupled. The water effect on  $D_C^{metal/silicate}$  can also be seen from Fig. 4B and 4C at a given Si content in alloy melt or  $fO_2$ , i.e., increasing water content causes a decrease in  $D_C^{metal/silicate}$ . Fig. 5B shows that regardless of  $fO_2$  or bulk water content,  $D_C^{metal/silicate}$  value is neg-

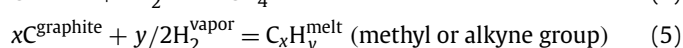
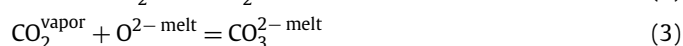
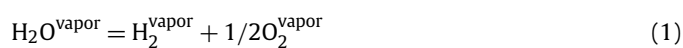
actively correlated with non-hydroxyl hydrogen content in silicate melt, indicating the strong controlling effect of  $f\text{H}_2$  in silicate melt on carbon partitioning.

## 4. Discussion

### 4.1. Effects of $f\text{O}_2$ and water on carbon dissolution in silicate melt

How the dissolution mechanism of carbon in silicate melt changes is the key to understand the effects of water and  $f\text{O}_2$  (Fig. 3), and the effects of melt NBO/T, temperature, and pressure (Dasgupta et al., 2013a; Chi et al., 2014), on carbon solubility in silicate melt. Although previous spectroscopic studies have shown that the carbon species in mafic silicate melt at  $f\text{O}_2$  of around FMQ  $\pm 2$  are dominated by carbonate, the carbon speciation in reduced mafic melt with  $f\text{O}_2$  below the IW buffer remains unclear and more variable (Holloway et al., 1992; Kadik et al., 2004; Mysen et al., 2009, 2011; Ardia et al., 2013; Dasgupta et al., 2013a; Wetzel et al., 2013; Stanley et al., 2011, 2014; Chi et al., 2014). Kadik et al. (2004) suggested that carbon is mainly dissolved as atomic carbon or amorphous carbon in their silicate melt with 1–2 wt%  $\text{H}_2\text{O}$  and  $f\text{O}_2$  of  $\sim\text{IW}-2.3$ , and that Si–C complex might exist in their silicate melt. Conversely, Mysen et al. (2009, 2011) found strong Raman peaks assigned to methane and other hydrogenated carbon species rather than Si–C complex in  $\text{SiO}_2$ – $\text{Na}_2\text{O}$  melt with  $\sim 1$  wt% water and  $f\text{H}_2$  buffered by the IW buffer. Wetzel et al. (2013) showed the presence of iron carbonyl  $[\text{Fe}(\text{CO})_5]$  besides methane in silicate melt with around 0.5 wt% water and  $f\text{O}_2$  below IW–0.5. However, Dasgupta et al. (2013a) and Chi et al. (2014) showed coexisting carbonate and methane and probably other hydrogenated carbon species but no iron carbonyl in silicate melt with  $\sim 0.4$ – $2.0$  wt% water and  $f\text{O}_2$  below IW–0.4. Stanley et al. (2014) showed that their silicate melt with  $\sim 0.4$  wt% water does not contain hydrogenated carbon but probably carbonyl or other C=O bearing species at  $f\text{O}_2$  between IW–0.3 and IW–0.8. For our runs in the Knippa–Fe–Ni–S system, Raman and FTIR spectra show that only a small fraction of carbon is dissolved in the silicate melt as carbonate, and no Raman or FTIR peaks can be assigned to iron carbonyl or Si–C complex. For our runs in the Knippa–Fe–Ni–Si and Knippa–Fe–Ni–S–Si systems, methane is the only observed carbon species in silicate melt. These together with the strong correlation between non-carbonate carbon and molecular  $\text{H}_2$  (Fig. 5A) indicate that in our silicate melt methane is the dominant carbon species.

At a given  $P$ – $T$  and melt composition, the effects of  $\text{H}_2\text{O}$  and  $f\text{O}_2$  on carbon dissolution in silicate melt at graphite-saturation can be better understood with the following reactions:



According to these reactions, the dissolution of carbonate, methane, and/or methyl groups in silicate melt must be controlled by the fugacities of  $\text{H}_2\text{O}$ ,  $\text{H}_2$ , and  $\text{O}_2$  at graphite-saturation. For example, increasing  $f\text{H}_2$  must increase the dissolution of carbon as methane in silicate melt according to reaction (4). In the experiments where  $f\text{O}_2$  is buffered by the coexisting metallic alloy melt and silicate melt,  $f\text{H}_2$  must increase with increasing the bulk  $\text{H}_2\text{O}$  content according to reaction (1), leading to more carbon dissolved as methane or methyl groups in silicate melt according to reactions (4) and (5).

Our experiments in the Knippa–Fe–Ni–S system have nearly identical  $f\text{O}_2$  and carbon contents in the form of carbonate (see Table 2). The observed positive correlation between the bulk water content and the carbon solubility in silicate melt (Fig. 3C) can thus be interpreted as resulting from increasing carbon dissolution as methane with increasing bulk water content in silicate melt according to reactions (1) and (4). For experiments in the Knippa–Fe–Ni–Si system, the decrease in carbon solubility with decreasing  $f\text{O}_2$  from IW–1.3 to IW–2.2 (Fig. 3D) on one hand is because of the decreased carbonate dissolution with decreasing  $f\text{O}_2$ , on the other hand is because of the lower bulk water content, which results in decreased  $f\text{H}_2$ . The increase of carbon solubility with decreasing  $f\text{O}_2$  from IW–4.2 to IW–4.7 in the Knippa–Fe–Ni–Si and Knippa–Fe–Ni–S–Si systems (Fig. 3D) is owing to increased  $f\text{H}_2$  and thus enhanced solubility of methane in silicate melt with decreasing  $f\text{O}_2$  and increasing bulk water content (Table 2 and Fig. 5A). According to this study and Hirschmann et al. (2012), molecular  $\text{H}_2$  may be dominant over  $\text{OH}^-$  and/or  $\text{H}_2\text{O}$  in hydrous silicate melt at  $\log f\text{O}_2 < \text{IW}$ . We thus believe that previous experiments with  $\sim 0.5$  wt% bulk water and  $f\text{O}_2$  below the IW buffer may indeed contain a certain amount of methane, although it was not detected by Raman spectroscopy.

Chi et al. (2014) showed that silicate melt composition may considerably affect the solubility of carbon in silicate melt at  $\text{IW}-1 < \log f\text{O}_2 < \text{IW}$ . Because carbon solubility in more reduced silicate melt ( $\log f\text{O}_2 < \text{IW}-1$ ) is significantly affected by water, the samples with similarly low water contents (0.07–0.25 wt%  $\text{H}_2\text{O}$ ) but different NBO/T values were chosen in order to assess the effect of silicate melt major element composition on carbon solubility in the present reduced silicate melt (runs G319–05, G320–06, G321–07, G326–12, and G329–15). This evaluation shows that carbon solubility range of only  $\sim 11$  ppm exists in these samples with NBO/T ranging from 0.81 to 1.22, which is at least an order of magnitude smaller than the entire range of carbon solubility observed in our glasses. This indicates that the effect of silicate melt major element composition is indeed small compared to the effect of water (see Fig. 5A).

### 4.2. Factors controlling $D_C^{\text{metal/silicate}}$ and parameterization

The factors controlling carbon dissolution in silicate melt and in alloy melt must control  $D_C^{\text{metal/silicate}}$ . It has been shown that 0–5 wt% sulfur in alloy melt does not have considerable effect on carbon solubility, whereas increasing Si decreases the carbon solubility. Therefore, the variation of  $D_C^{\text{metal/silicate}}$  in the Knippa–Fe–Ni–S experiments (Fig. 4A) is simply due to the variation of carbon solubility in silicate melt caused by the variation of bulk water content, whereas for the Knippa–Fe–Ni–Si and Knippa–Fe–Ni–S–Si experiments, the  $D_C^{\text{metal/silicate}}$  variation is a result of combined variation of  $f\text{O}_2$ , bulk water content, and silicon content in alloy melt (Fig. 4B and 4C).

The compiled values of  $D_C^{\text{metal/silicate}}$  from our study and those from literature are plotted in Fig. 4C and in Supplementary Fig. 3. Due to the limited range of carbon solubility in alloy melt (1.82 to 5.88 wt% in this study; 4.5–7.0 wt% in Dasgupta et al., 2013a; 4.4–7.4 wt% in Chi et al., 2014; 6.7–8.3 wt% in Stanley et al., 2014),  $D_C^{\text{metal/silicate}}$  varies mainly as the variation of carbon content in silicate melt, and our  $D_C^{\text{metal/silicate}}$  data obtained at a single  $P$ – $T$  condition cover the previous  $D_C^{\text{metal/silicate}}$  data range (Fig. 4C and Supplementary Fig. 3), indicating again the strong effects of  $f\text{O}_2$  and the bulk water content or the strong effect of  $f\text{H}_2$  on carbon partitioning (Fig. 5B). Fig. 4C shows that  $D_C^{\text{metal/silicate}}$  tends to increase first with decreasing  $f\text{O}_2$  but then decrease with furthering decrease in  $f\text{O}_2$ . The discrete change of  $D_C^{\text{metal/silicate}}$  is owing to



the change of  $fO_2$  and bulk water content dependent change in carbon speciation and solubility in silicate melt, and other parameters as has been discussed above. Using the  $D_C^{metal/silicate}$  compiled in Fig. 4C, two empirical parameterizations were derived.

At  $IW-1.3 < \log fO_2 < IW$ :

$$\log D_C^{metal/silicate} = 2100/T + 260P/T - 0.67NBO/T - 0.32\Delta IW - 1.65X_{H_2O}^{silicate} - 11.5X_{Ni}^{metal} + 2.86 \quad (R^2 = 0.83) \quad (6)$$

At  $\log fO_2 < IW-1.3$  and 3 GPa, 1600 °C:

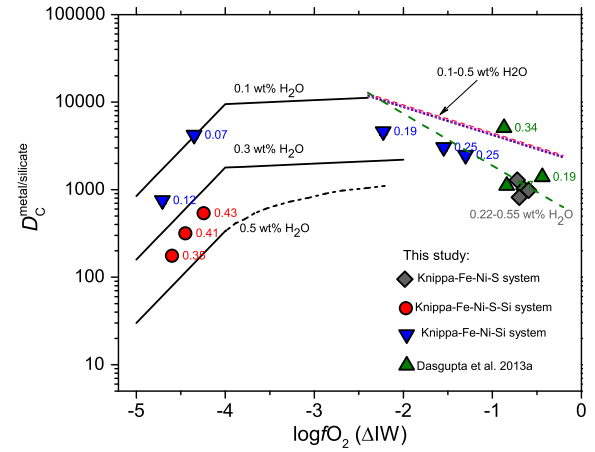
$$\log D_C^{metal/silicate} = -0.33NBO/T + 0.045\Delta IW - 113X_{H_2O}^{silicate} - 5.3X_{Ni}^{metal} - 5.03X_{Si}^{metal} + 5.03 \quad (R^2 = 0.97) \quad (7)$$

$T$  is in K, and  $P$  is in GPa, and  $X$  refers to mole fraction. Eq. (6) uses 41 experiments with data from this study and from Dasgupta et al. (2013a), Chi et al. (2014), Stanley et al. (2014) covering  $P$  of 1–5 GPa and  $T$  of 1350–2100 °C, whereas Eq. (7) uses data only from this study. The main difference between Eq. (6) and the parameterization of Chi et al. (2014) is that the present parameterization includes the term for effect of water in silicate melt and expresses  $fO_2$  in  $\Delta IW$  scale besides adding four more data points from the present study. The reason for deriving two parameterizations is that at  $IW-1.3 < \log fO_2 < IW$  carbonate continues to be a significant C species in silicate melt, while at  $\log fO_2 < IW-1.3$  and modest level of hydration methane appears to be the main C-bearing species in silicate melt.

#### 4.3. Core/mantle partitioning of carbon in MO

Recent studies suggested that planetary core-formation may have occurred as a largely continuous process with core segregation starting well before the end of Earth's accretion, rather than a single event at fixed  $P$ – $T$ – $fO_2$  conditions (e.g., Wade and Wood, 2005; Wood et al., 2006, 2008; Rubie et al., 2011). To satisfy the abundance patterns of mild to moderately siderophile elements in silicate mantle, these authors invoked early accretion of highly reduced materials, followed by gradually oxidized materials. The corresponding  $\log fO_2$  in the MO may have been as low as  $\sim IW-5$  but gradually increased to  $\sim IW-2$  (e.g., Rubie et al., 2011). At reduced conditions, silicon is likely to be the most abundant light elements entering the alloy melt (Wood et al., 2008; Ricolleau et al., 2011; Tsuno et al., 2013; Siebert et al., 2013). The silicon content in our alloy melt is up to 10 wt%, which is at the high end of the estimated, likely silicon in the core-forming alloy melt (Allegre et al., 1995; Ricolleau et al., 2011; Rubie et al., 2011; Siebert et al., 2013). As noted above (see also Fig. 5), hydrogen is important in affecting the dissolution and partitioning of carbon, but its concentration in MO remains largely unknown. Based on the solubility of hydrogen in an MO overlain by a thick steam atmosphere, Hirschmann (2012) and Ardia et al. (2013) proposed that MO hydrogen content  $\leq 1000$  ppm is possible. The estimated water ( $H_2O$ ) content of the bulk Earth by Marty (2012) is between 0.1 and 0.3 wt%. If one assumes that this amount of water was present in Earth's MO,  $H_2O$  content  $\leq 0.3$  wt% ( $\leq 330$  ppm H) may have been possible due to negligible partitioning of H to the core.

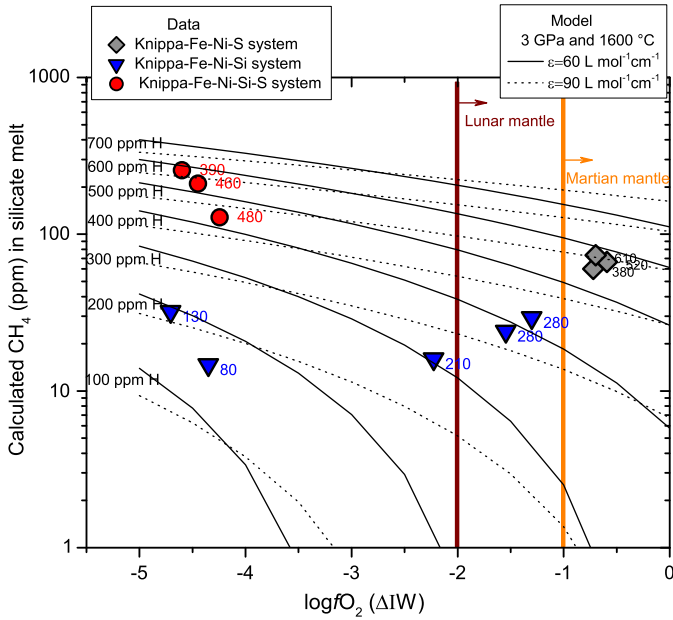
Chi et al. (2014) used their parameterization to predict carbon partitioning between planetary core and mantle at  $P$ – $T$ – $fO_2$  conditions corresponding to the base of the MOs. The results showed that core-formation of both Earth and Mars may have resulted in the entire carbon segregated into the core, but carbon in the lunar mantle could possibly be set up by equilibrium core–mantle



**Fig. 6.** The experimentally measured  $D_C^{metal/silicate}$  from 3 GPa, 1600 °C as a function of estimated  $fO_2$  and bulk water content of silicate melt compared with the existing parameterization that predict the dependence of  $D_C^{metal/silicate}$  on  $fO_2$  and silicate melt water content. The experimental data are from this study and those from Dasgupta et al. (2013a). The plot shows that the calculated  $D_C^{metal/silicate}$  values using Eq. (6) (short dashed lines) do not depend considerably on bulk water content in silicate melt but increase markedly with decreasing oxygen fugacity. However, the  $D_C^{metal/silicate}$  values calculated using Eq. (7) (black solid lines) show a significant dependence on bulk water content in addition to  $fO_2$ . Also plotted for comparison using the long dashed line is the parameterization of Chi et al. (2014). The fit using Eq. (6) and that from Chi et al. (2014) are plotted only down to  $\log fO_2 \sim IW-2.5$  as these fits were derived based on relatively oxidized experiments (see text; Chi et al., 2014), whereas the fit using Eq. (7) is chiefly plotted between  $IW-5$  and  $\sim IW-2$ . The parameters in Eqs. (6) and (7) are fixed at  $X_{Ni}^{metal} = 0.04$ ,  $NBO/T = 0.9$ , values similar to average values in our experiments. Si content in alloy melt is varied from 10 to 0.1 wt% at  $\log fO_2$  from  $IW-5$  to  $IW-4$  according to present study. The labeled numbers are bulk water contents in silicate melt in wt%. The black dashed line refers to possible trend of  $D_C^{metal/silicate}$  with varying  $fO_2$  and melt water content at conditions where our parameterizations do not have good data coverage.

fractionation in an MO. However, limited by their dataset, Chi et al. (2014) did not consider the effects of varying  $\log fO_2$  below  $\sim IW-1.5$  and water in silicate melt on carbon partitioning. The above parameterizations (Eqs. (6) and (7)) allow us to predict the variation of  $D_C^{metal/silicate}$  as the variations of  $fO_2$  and water at 3 GPa and 1600 °C (Fig. 6). Fig. 6 shows that increasing water content in silicate melt significantly lowers  $D_C^{metal/silicate}$  value calculated based on Eq. (7). The extrapolation of Eq. (6) and the parameterization of Chi et al. (2014) to  $\log fO_2 < IW-2$  leads artificially to exceedingly high  $D_C^{metal/silicate}$  values. Therefore, if the  $\log fO_2$  in MO had evolved from  $IW-5$  to  $IW-2$ , and if water content was as high as 0.9 wt% (1000 ppm H), the  $D_C^{metal/silicate}$  value may likely be between 10 and 100 at low  $fO_2$  (Fig. 6). The increase of  $D_C^{metal/silicate}$  with increasing  $\log fO_2$  from  $IW-5$  to  $IW-2$  may also imply that there may have been less carbon segregated into the core during the early accretion of highly reduced material. However, if the MOs were relatively dry with less than 0.1 wt%  $H_2O$ , regardless of  $fO_2$ , carbon should have effectively been segregated into the core because of the exceedingly high  $D_C^{metal/silicate}$ . Furthermore, it should be noted that the present study was performed at a single  $P$ – $T$  condition. Silicon solubility in alloy melt may vary with  $P$ – $T$  and  $fO_2$  (Ricolleau et al., 2011; Tsuno et al., 2013; Siebert et al., 2013), and the molecular  $H_2$  content in silicate melt at a given bulk water content and  $fO_2$  may also vary with varying pressure and temperature (Hirschmann et al., 2012). All these could affect  $D_C^{metal/silicate}$ . Hence to better understand the fractionation of carbon in MO, high  $P$ – $T$  experiments with various  $fO_2$  and water contents are required.

One final consideration is the availability of carbon in terrestrial MO and its relation to the  $fO_2$  evolution of the MO. If carbon (along with sulfur) was not present in the early, reduced stage of



**Fig. 7.** The calculated methane ( $\text{CH}_4$ ) contents in silicate melt (solid and dotted curves) at 3 GPa and 1600 °C as a function of oxygen fugacity and bulk water (H) content in silicate melt, using Eq. (8) and the correlation shown in Fig. 5A. The solid and dotted curves represent model calculations where molecular  $\text{H}_2$  was determined using  $\epsilon_{\text{OH}} = 60$  and  $90 \text{ L mol}^{-1} \text{ cm}^{-1}$ , respectively. The plotted data show the measured abundance of non-carbonate carbon in our experimental silicate melt (Table 2), assumed to be present entirely as methane; the labeled numbers are bulk water (H) contents in silicate melt in ppm. The two vertical lines indicate the lowest oxygen fugacity estimated for lunar mantle and Martian mantle. Our experimental data and model predict the amount of degassed methane from Martian and lunar mantle for a given  $f\text{O}_2$  and bulk 'water' content of planetary basalts saturated with graphite.

MO and was delivered at a late stage (after 90%) of accretion when the terrestrial MO already had evolved to less reduced conditions ( $\sim \text{IW}-2$ ; Wade and Wood, 2005; Wood et al., 2013) then Si in alloy melt and solution of  $\text{CH}_4$  in MO might not have influenced  $D_{\text{C}}^{\text{metal/silicate}}$ . If this was the case, then despite the possibility of achieving a  $D_{\text{C}}^{\text{metal/silicate}} < 100$  in the presence of Si in alloy in a hydrous MO, the  $D_{\text{C}}^{\text{metal/silicate}}$  values for terrestrial core formation would be those  $> 1000$  and effectively all the available carbon would partition to the core of the Earth.

#### 4.4. Carbon degassing from MO and its influence on early planetary atmospheres

The formation of planetary atmosphere may have been coupled with the solidification of planetary MO (e.g., Elkins-Tanton, 2008, 2012). The presence and nature of an atmosphere overlying an MO in turn could significantly influence the thermal evolution of an MO (e.g., Lebrun et al., 2013). However, the redox state of planetary early atmosphere overlying an MO remains unknown (e.g., Hirschmann, 2012; Dasgupta, 2013; Li and Keppler, 2014), in part because the carbon species in the shallow MO have not been constrained.

This study has shown that in modestly hydrated reduced silicate melt with  $f\text{O}_2$  ranging from IW-5 to IW-1, carbon is mainly in the form of  $\text{CH}_4$ , and the carbon content as carbonate is negligible. Thus, carbon in an MO with  $\log f\text{O}_2$  below IW-2 may have been mostly as  $\text{CH}_4$  and degassing of an MO may have only released  $\text{CH}_4$  into the overlying atmosphere, even if the bulk water content in the MO was as low as 0.1–0.3 wt%. The most efficient degassing of an MO may have occurred when it experienced significant solidification and volatile enrichment. A post-differentiation planetary

MO may not have been saturated with elemental carbon, in part because a significant amount of carbon may have been segregated into the core and in part because water (in particular molecular  $\text{H}_2$ ) in the post-differentiation MO may have accumulated to an elevated content such that the carbon solubility in silicate melt is significantly enhanced in the form of  $\text{CH}_4$ . The solubility of carbon in silicate mantle minerals is exceedingly low (Shcheka et al., 2006), so that the residual carbon from core-segregation may have been mainly concentrated in the residual silicate melt in the form of  $\text{CH}_4$  after significant solidification of an MO, together with reduced species such as ammonia and molecular  $\text{H}_2$  (Hirschmann et al., 2012; Bali et al., 2013; Li and Keppler, 2014). Therefore, degassing of such reservoirs enriched in reduced species may have created a reduced early atmosphere consisting mainly of  $\text{CH}_4$ , molecular  $\text{H}_2$ , and ammonia. Thus our study suggests that formation of reduced planetary atmospheres rich in  $\text{CH}_4$  might have occurred for the proto Earth not only as a transient state soon after collision with reduced impactors (Zahnle et al., 2010; Genda and Abe, 2003) but also at a late stage of crystallization of a reduced and hydrated MO.

#### 4.5. Degassing of C–O–H volatiles via partial melting of reduced planetary mantles

Degassing of reduced carbon species from planetary interior to atmosphere may have potentially maintained the planetary surface temperature above the freezing point of water in early planetary history (e.g., Sagan and Mullen, 1972; Ardia et al., 2013; Wetzel et al., 2013). However, it is poorly understood whether degassing of the reduced planetary mantles at post-MO stage such as for the Martian mantle could have released sufficient dose of reduced C–O–H fluids to explain the early episodes of warm Martian climate (Stanley et al., 2011, 2014; Ardia et al., 2013) or whether warm ancient Martian atmosphere was achieved through other degassed volatiles (e.g., Halevy et al., 2007; Richter et al., 2009; Ding et al., 2014, 2015). Because our experimental condition and generated melt compositions at  $\log f\text{O}_2$  of  $\sim \text{IW}$  to IW-2 are closely applicable for mantle melting in reduced rocky planets such as Mars (e.g., Musselwhite et al., 2006; Filiberto et al., 2010; Filiberto and Dasgupta, 2011, 2015), our measured concentrations of C–O–H volatiles in equilibrium with graphite are directly relevant for evolution of magmatic volatiles in such planetary bodies.

It is widely argued that the  $\log f\text{O}_2$  of primary Martian basalts is down to IW-1 and therefore carbon is present in the Martian mantle as graphite/diamond (e.g., Herd et al., 2002; Karner et al., 2007; Wadhwa, 2008; Richter et al., 2008). However, the water content of Martian basalts is subject to considerable controversy, with arguments for both quite dry and hydrous primary magmas with hydrogen content up to 3000 ppm but as low as a few ppm (e.g., Filiberto and Treiman, 2009; McCubbin et al., 2010a, 2010b, 2012; Gaillard et al., 2012). To be able to predict  $\text{CH}_4$  content in silicate melt using the correlation in Fig. 5A, an equation was first derived based on our data in Table 2 for calculating molecular  $\text{H}_2$  content in silicate melt at given  $f\text{O}_2$  and bulk water content:

$$\text{H}_2(\text{wt}\%) = a\text{H}_2\text{O}(\text{wt}\%) - b\Delta\text{IW} - c \quad (8)$$

where  $a = 0.0828\text{--}0.0917$ ,  $b = 0.0052\text{--}0.0036$ , and  $c = 0.0232\text{--}0.0163$ , and  $R^2 = 0.95\text{--}0.97$  for  $\epsilon$  of  $\text{H}_2\text{O}$  varying from 60 to  $90 \text{ L mol}^{-1} \text{ cm}^{-1}$ .

Using Eq. (8), the calculated  $\text{CH}_4$  content in silicate melt at graphite-saturation and at  $\log f\text{O}_2 = \text{IW}-1$  is 3–13 ppm when  $\text{H} = 300$  ppm, 50–80 ppm when  $\text{H} = 500$  ppm, and 150–190 ppm when  $\text{H} = 700$  ppm (Fig. 7). The increase of  $f\text{O}_2$  by one log unit would decrease the amount of  $\text{CH}_4$  dissolved in silicate melt by

less than 50% when  $H \geq 500$  ppm. These results indicate that a considerable amount of  $\text{CH}_4$  may have been in the Martian basalt as long as the estimated water (H) content is applicable to Martian mantle and Martian basalts. Due to the low solubility of carbonate in silicate melt ( $<10$  ppm at 3 GPa, 1600 °C and  $\log f\text{O}_2 = \text{IW}-1$ ), Stanley et al. (2011) concluded that the degassing of  $\text{CO}_2$  to the Martian atmosphere may be insufficient to create greenhouse conditions required by possible presence of liquid water on Martian surface. Our study suggests that degassing of Martian mantle may have released considerable  $\text{CH}_4$  to help maintain Martian surface temperature above the freezing point of water. This is in contrast to previous studies (Stanley et al., 2014) that suggested negligible  $\text{CH}_4$  released from the Martian mantle into atmosphere.

The  $\log f\text{O}_2$  of lunar mantle is between IW-2 and IW (e.g., Wadhwa, 2008; Nicholis and Rutherford, 2009). Wetzell et al. (2013) proposed that degassing of lunar mantle may release reduced carbon species such as  $\text{CH}_4$  and CO into the atmosphere. However, whether degassing of lunar mantle released  $\text{CH}_4$  into the early atmosphere depends not only on  $f\text{O}_2$  but also on the bulk water content in silicate melt. The estimated hydrogen in lunar basalts is 80–1700 ppm (e.g., Hauri et al., 2011; Tartèse and Anand, 2013, and references therein; Barnes et al., 2014). Assuming a  $\log f\text{O}_2$  of IW-2 and hydrogen content of 100–400 ppm for primitive lunar basalts (Tartèse and Anand, 2013), the calculated  $\text{CH}_4$  content in silicate melt is up to 50 ppm (Fig. 7). Thus, the degassing of lunar mantle may also have released much more  $\text{CH}_4$  than  $\text{CO}_2$  into the early atmosphere, as long as a few hundreds ppm water (H) in the primitive lunar basalts. However, it should be noted that the heterogeneous distribution of water in lunar mantle (e.g., Albarède et al., 2014; Robinson and Taylor, 2014) must cause different parts of the lunar mantle to degas carbon with different efficiencies, and extremely dry parts of the lunar mantle may not degas significant quantity of  $\text{CH}_4$ . Furthermore, these calculated values of  $\text{CH}_4$  contents in both lunar and Martian basalts may be maximum because other volatiles such as nitrogen at reduced conditions (Kadik et al., 2011; Li et al., 2013, 2015) may compete for non-hydroxyl hydrogen. However, with 200–600 ppm H and  $\log f\text{O}_2$  of IW-2 to IW, our experiments indeed show 20–70 ppm  $\text{CH}_4$  in silicate melt (see Fig. 7). We also note that the  $\text{CH}_4$  contents in natural basaltic melt (12–260 ppm) at 1600 °C, 3 GPa,  $\log f\text{O}_2$  of IW-0.6 to IW-4.7, and 80–610 ppm H in this study (Fig. 7) are comparable to the  $\text{CH}_4$  solubility (52–363 ppm) in a Fe-free, Mg-poor synthetic haplobasalt at 1400–1450 °C, 0.7–3 GPa,  $\log f\text{O}_2$  of IW-1.4 to IW-4, and 1400–7800 H in Ardia et al. (2013). Future experiments will be required to better understand the effects of temperature, pressure, and melt composition on  $\text{CH}_4$  solubility in natural basalt.

## 5. Conclusions

Our experiments demonstrate:

- (1) Carbon solubility in Fe-rich alloy melt is not affected by the presence of 0–5 wt% S but decreases with increasing Si content from 0 to 10 wt%.
- (2) Carbon solubility in silicate melt depends on both  $f\text{O}_2$  and melt water content. The main carbon species in silicate melt at  $\text{IW}-1 < \log f\text{O}_2 < \text{IW}-5$  is methane and a fraction of carbon is present as  $\text{CO}_3^{2-}$  at  $\log f\text{O}_2$  at least down to IW-0.7.
- (3) The  $D_C^{\text{metal/silicate}}$  ranges from 180 to 4600, decreasing with increasing melt water content and Si content in alloy melt, and decreasing  $\log f\text{O}_2$  from IW-1.5 to IW-5, where methane or methyl group is the dominant form of carbon in basalt and Si becomes an important light element in Fe-rich alloy melt. The trend of decreasing  $D_C^{\text{metal/silicate}}$  with decreasing  $\log f\text{O}_2$  from  $\sim\text{IW}-1.5$  to IW-5 is in contrast with the trend

of increasing  $D_C^{\text{metal/silicate}}$  with decreasing  $\log f\text{O}_2$  down to  $\sim\text{IW}-1.5$  where carbonates continue to be significant fractions of dissolved carbon in basaltic melt (Dasgupta et al., 2013a; Chi et al., 2014). Therefore, in a highly reduced, moderately hydrous MO, a considerable amount of carbon would be retained in the silicate mantle after core-formation; however in a dry MO or if the Earth's carbon was delivered only during late stage of accretion in a relatively oxidized MO (Wood et al., 2013), nearly the entire carbon would be segregated into the core.

- (4) Degassing of the post-core formation MO may have released methane into the early planetary atmospheres, and degassing of reduced planetary mantles such as the ones of Mars and the Moon may have released much more methane than carbon dioxide, which helps maintain an early warm atmosphere of Mars.

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## Appendix A. Supplementary material

Supplementary material related to this article can be found online at <http://dx.doi.org/10.1016/j.epsl.2015.01.017>.

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