

1 GGdirect 1600 0

- Process: $pp \rightarrow \tilde{g}\tilde{g}, \tilde{g} \rightarrow q\tilde{\chi}_1^0$
- Parameters: $(m_{\tilde{g}}, m_{\tilde{\chi}_1^0}) = (1600, 0)$ GeV
- Number of Atom MC events: 619
- Event Generator: MadGraph5 + Pythia6

#	cut name	ϵ_{Exp} (%)	ϵ_{Atom} (%)	$\frac{\text{Atom}}{\text{Exp}}$	$\frac{(\text{Exp}-\text{Atom})}{\text{Error}}$	#/?	R_{Exp} (%)	R_{Atom} (%)	$\frac{\text{Atom}}{\text{Exp}}$	$\frac{(\text{Exp}-\text{Atom})}{\text{Error}}$	$\partial \log \epsilon_{\text{Atom}} / \partial \log x_{\text{cut}}$
1	Preselection, $\text{MET} > 200, p_T^j > 200$	90.18 0.95	91.9 $^{+1.1}_{-1.1}$	1.02	1.18	0	90.18 0.95	91.9 $^{+1.1}_{-1.1}$	1.02	1.18	0.19 $^{+0.3}_{-0.29}$
2	$N_j \geq 2$: 2jl	90.18 \pm 0.95	91.9 $^{+1.1}_{-1.1}$	1.02	1.18	1	100.0 \pm 3.8	100.0 $^{+1.69}_{-1.69}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
3	$\Delta\phi_{\min} > 0.8$: 2jl	54.97 \pm 0.74	56.1 $^{+2.0}_{-2.0}$	1.02	0.53	2	60.96 \pm 3.37	61.04 $^{+2.3}_{-2.3}$	1.0	0.02	0.0 $^{+0.0}_{-0.0}$
4	$p_T^j > 200$: 2jl	54.26 \pm 0.74	55.6 $^{+2.0}_{-2.0}$	1.02	0.63	3	98.71 \pm 2.96	99.11 $^{+5.02}_{-5.02}$	1.0	0.07	0.0 $^{+0.0}_{-0.0}$
5	$\text{MET}/\sqrt{H_T} > 15$: 2jl	29.16 \pm 0.54	45.6 $^{+2.0}_{-2.0}$	1.56	7.94	4	53.74 \pm 2.54	82.01 $^{+4.65}_{-4.65}$	1.53	5.34	0.0 $^{+0.0}_{-0.0}$
6	$m_{\text{eff}}^{\text{inc}} > 1200$: 2jl	29.13 \pm 0.54	45.6 $^{+2.0}_{-2.0}$	1.57	7.95	5	99.9 \pm 2.16	100.0 $^{+6.2}_{-6.2}$	1.0	0.02	0.0 $^{+0.0}_{-0.0}$
7	$p_T^j > 300$: 2jm	89.75 \pm 0.95	91.5 $^{+1.1}_{-1.1}$	1.02	1.21	0	99.52 \pm 114.88	99.56 $^{+155.56}_{-155.56}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
8	$N_j \geq 2$: 2jm	89.75 \pm 0.95	91.5 $^{+1.1}_{-1.1}$	1.02	1.21	7	100.0 \pm 3.79	100.0 $^{+1.7}_{-1.7}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
9	$\Delta\phi_{\min} > 0.4$: 2jm	72.16 \pm 0.85	73.2 $^{+1.8}_{-1.8}$	1.01	0.52	8	80.4 \pm 3.59	80.0 $^{+2.19}_{-2.19}$	1.0	-0.1	0.0 $^{+0.0}_{-0.0}$
10	$p_T^j > 50$: 2jm	72.16 \pm 0.85	73.2 $^{+1.8}_{-1.8}$	1.01	0.52	9	100.0 \pm 3.4	100.0 $^{+3.48}_{-3.48}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
11	$\text{MET}/\sqrt{H_T} > 15$: 2jm	34.76 \pm 0.59	59.5 $^{+2.0}_{-1.9}$	1.71	12.44	10	48.17 \pm 2.85	81.28 $^{+3.39}_{-3.28}$	1.69	7.62	0.0 $^{+0.0}_{-0.0}$
12	$m_{\text{eff}}^{\text{inc}} > 1600$: 2jm	34.28 \pm 0.59	58.2 $^{+2.0}_{-1.9}$	1.7	12.03	11	98.62 \pm 2.35	97.82 $^{+4.59}_{-4.58}$	0.99	-0.16	0.0 $^{+0.0}_{-0.0}$
13	$N_j \geq 2$: 2jt	91.08 \pm 0.95	91.9 $^{+1.1}_{-1.1}$	1.01	0.56	0	101.0 \pm 114.96	100.0 $^{+155.56}_{-155.56}$	0.99	-0.01	0.0 $^{+0.0}_{-0.0}$
14	$\Delta\phi_{\min} > 0.8$: 2jt	54.97 \pm 0.74	56.1 $^{+2.0}_{-2.0}$	1.02	0.53	13	60.35 \pm 3.38	61.04 $^{+2.3}_{-2.3}$	1.01	0.17	0.0 $^{+0.0}_{-0.0}$
15	$p_T^j > 200$: 2jt	54.26 \pm 0.74	55.6 $^{+2.0}_{-2.0}$	1.02	0.63	14	98.71 \pm 2.96	99.11 $^{+5.02}_{-5.02}$	1.0	0.07	0.0 $^{+0.0}_{-0.0}$
16	$\text{MET}/\sqrt{H_T} > 20$: 2jl	16.7 \pm 0.41	15.5 $^{+1.5}_{-1.4}$	0.93	-0.77	15	30.78 \pm 2.24	27.88 $^{+2.88}_{-2.71}$	0.91	-0.79	0.0 $^{+0.0}_{-0.0}$
17	$m_{\text{eff}}^{\text{inc}} > 2000$: 2jt	15.97 \pm 0.4	14.7 $^{+1.5}_{-1.4}$	0.92	-0.82	16	95.63 \pm 1.62	94.84 $^{+12.92}_{-12.88}$	0.99	-0.06	0.0 $^{+0.0}_{-0.0}$
18	$N_j \geq 4$: 4jt	85.7 \pm 0.93	90.0 $^{+1.2}_{-1.2}$	1.05	2.84	0	95.03 \pm 114.64	97.93 $^{+162.79}_{-162.79}$	1.03	0.01	0.0 $^{+0.0}_{-0.0}$
19	$\Delta\phi_{\min}$ cut: 4jt	59.69 \pm 0.77	60.2 $^{+2.0}_{-1.9}$	1.01	0.25	18	69.65 \pm 3.39	66.89 $^{+2.39}_{-2.29}$	0.96	-0.67	0.2 $^{+0.37}_{-0.36}$
20	$p_T^j > 100$: 4jt	59.69 \pm 0.77	60.0 $^{+2.0}_{-1.9}$	1.01	0.15	19	100.0 \pm 3.09	99.67 $^{+4.58}_{-4.57}$	1.0	-0.06	0.0 $^{+0.0}_{-0.0}$
21	$p_T^j > 100$: 4jt	52.27 \pm 0.72	54.4 $^{+2.0}_{-2.0}$	1.04	1.0	20	87.57 \pm 2.99	90.67 $^{+4.4}_{-4.5}$	1.04	0.57	0.0 $^{+0.0}_{-0.0}$
22	Aplanarity > 0.04 : 4jt	35.62 \pm 0.6	54.4 $^{+2.0}_{-2.0}$	1.53	9.0	21	68.15 \pm 2.63	100.0 $^{+5.2}_{-5.2}$	1.47	5.47	0.0 $^{+0.0}_{-0.0}$
23	$\text{MET}/\sqrt{H_T} > 0.2''$: 4jt	25.24 \pm 0.5	35.8 $^{+2.0}_{-1.9}$	1.42	5.37	22	70.86 \pm 2.19	65.81 $^{+4.4}_{-4.25}$	0.93	-1.03	0.0 $^{+0.0}_{-0.0}$
24	$m_{\text{eff}}^{\text{inc}} > 2200$: 4jt	21.38 \pm 0.46	30.2 $^{+1.9}_{-1.8}$	1.41	4.75	23	84.71 \pm 1.93	84.36 $^{+6.94}_{-6.89}$	1.0	-0.05	0.0 $^{+0.0}_{-0.0}$
25	$N_j \geq 5$: 5j	64.34 \pm 0.8	77.3 $^{+1.7}_{-1.7}$	1.2	6.89	0	71.35 \pm 113.22	84.11 $^{+202.48}_{-202.48}$	1.18	0.06	0.0 $^{+0.0}_{-0.0}$
26	$\Delta\phi_{\min}$ cut: 5j	43.61 \pm 0.66	49.8 $^{+2.0}_{-2.0}$	1.14	2.94	25	67.78 \pm 2.92	64.42 $^{+2.95}_{-2.95}$	0.95	-0.81	0.23 $^{+0.4}_{-0.4}$
27	$p_T^j > 100$: 5j	43.61 \pm 0.66	49.8 $^{+2.0}_{-2.0}$	1.14	2.94	26	100.0 \pm 2.64	100.0 $^{+5.68}_{-5.68}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
28	$p_T^j > 50$: 5j	40.18 \pm 0.63	49.8 $^{+2.0}_{-2.0}$	1.24	4.59	27	92.13 \pm 2.59	100.0 $^{+5.68}_{-5.68}$	1.09	1.26	0.0 $^{+0.0}_{-0.0}$
29	Aplanarity > 0.04 : 5j	28.62 \pm 0.53	49.8 $^{+2.0}_{-2.0}$	1.74	10.23	28	71.23 \pm 2.33	100.0 $^{+5.68}_{-5.68}$	1.4	4.69	0.0 $^{+0.0}_{-0.0}$
30	$\text{MET}/m_{\text{eff}}(N_j) > 0.25''$: 5j	14.01 \pm 0.37	23.5 $^{+1.8}_{-1.6}$	1.68	5.78	29	48.95 \pm 1.8	47.19 $^{+4.08}_{-3.73}$	0.96	-0.4	0.0 $^{+0.0}_{-0.0}$
31	$m_{\text{eff}}^{\text{inc}} > 1600$: 5j	13.88 \pm 0.37	23.2 $^{+1.8}_{-1.6}$	1.67	5.67	30	99.07 \pm 1.49	98.72 $^{+10.19}_{-10.18}$	1.0	-0.03	0.0 $^{+0.0}_{-0.0}$
32	$N_j \geq 6$: 6jm	36.83 \pm 0.61	55.5 $^{+2.0}_{-2.0}$	1.51	8.93	0	40.84 \pm 110.75	60.39 $^{+228.25}_{-228.25}$	1.48	0.08	0.0 $^{+0.0}_{-0.0}$
33	$\Delta\phi_{\min}$ cut: 6jm	23.72 \pm 0.49	35.3 $^{+2.0}_{-1.9}$	1.49	5.9	32	64.4 \pm 2.18	63.6 $^{+4.27}_{-4.12}$	0.99	-0.17	0.32 $^{+0.48}_{-0.47}$
34	$p_T^j > 100$: 6jm	23.72 \pm 0.49	35.3 $^{+2.0}_{-1.9}$	1.49	5.9	33	100.0 \pm 1.95	100.0 $^{+7.81}_{-7.81}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
35	$p_T^j > 50$: 6jm	22.56 \pm 0.47	35.3 $^{+2.0}_{-1.9}$	1.56	6.51	34	95.11 \pm 1.92	100.0 $^{+7.81}_{-7.81}$	1.05	0.61	0.0 $^{+0.0}_{-0.0}$
36	Aplanarity > 0.04 : 6jm	16.87 \pm 0.41	35.3 $^{+2.0}_{-1.9}$	2.09	9.48	35	74.78 \pm 1.77	100.0 $^{+7.81}_{-7.81}$	1.34	3.15	0.0 $^{+0.0}_{-0.0}$
37	$\text{MET}/m_{\text{eff}}(N_j) > 0.25''$: 6jm	7.55 \pm 0.27	12.7 $^{+1.4}_{-1.3}$	1.68	3.88	36	44.75 \pm 1.36	35.98 $^{+4.41}_{-4.21}$	0.8	-1.9	0.0 $^{+0.0}_{-0.0}$
38	$m_{\text{eff}}^{\text{inc}} > 1600$: 6jm	7.46 \pm 0.27	12.7 $^{+1.4}_{-1.3}$	1.7	3.94	37	98.81 \pm 1.1	100.0 $^{+15.04}_{-15.04}$	1.01	0.08	0.0 $^{+0.0}_{-0.0}$
39	$N_j \geq 6$: 6jt	36.83 \pm 0.61	55.5 $^{+2.0}_{-2.0}$	1.51	8.93	0	40.84 \pm 110.75	60.39 $^{+228.25}_{-228.25}$	1.48	0.08	0.0 $^{+0.0}_{-0.0}$
40	$\Delta\phi_{\min}$ cut: 6jt	23.72 \pm 0.49	35.3 $^{+2.0}_{-1.9}$	1.49	5.9	39	64.4 \pm 2.18	63.6 $^{+4.27}_{-4.12}$	0.99	-0.17	0.32 $^{+0.48}_{-0.47}$
41	$p_T^j > 100$: 6jt	23.72 \pm 0.49	35.3 $^{+2.0}_{-1.9}$	1.49	5.9	40	100.0 \pm 1.95	100.0 $^{+7.81}_{-7.81}$	1.0	0.0	0.0 $^{+0.0}_{-0.0}$
42	$p_T^j > 100$: 6jt	22.56 \pm 0.47	35.3 $^{+2.0}_{-1.9}$	1.56	6.51	41	95.11 \pm 1.92	100.0 $^{+7.81}_{-7.81}$	1.05	0.61	0.0 $^{+0.0}_{-0.0}$
43	Aplanarity > 0.04 : 6jt	16.87 \pm 0.41	35.3 $^{+2.0}_{-1.9}$	2.09	9.48	42	74.78 \pm 1.77	100.0 $^{+7.81}_{-7.81}$	1.34	3.15	0.0 $^{+0.0}_{-0.0}$
44	$\text{MET}/m_{\text{eff}}(N_j) > 0.25''$: 6jt	10.63 \pm 0.33	20.3 $^{+1.7}_{-1.6}$	1.91	5.92	43	63.01 \pm 1.47	57.51 $^{+5.72}_{-5.58}$	0.91	-0.93	0.0 $^{+0.0}_{-0.0}$
45	$m_{\text{eff}}^{\text{inc}} > 1600$: 6jt	9.9 \pm 0.31	19.0 $^{+1.6}_{-1.5}$	1.92	5.94	44	93.13 \pm 1.28	93.6 $^{+10.8}_{-10.77}$	1.0	0.04	0.0 $^{+0.0}_{-0.0}$

Table 1: